INLAND WETLANDS COMMISSION Telephone (203) 563-0180 Fax (203) 563-0284



TOWN HALL 238 Danbury Road Wilton, Connecticut 06897

### **APPLICATION FOR A SIGNIFICANT REGULATED ACTIVITY**

For Office Use Only:					
	WET#				
Filing Fee \$	Wilton Land Record Map#				
Date of Submission	Volume # Page #				
Date of Acceptance	Assessor's Map # Lot#				
APPLICANT IN	VFORMATION:				
Applicant FDSPIN 141 DR LLC	Agent (if applicable) Lisa Feinberg, Carmody Law				
Address c/o Agent: Carmody Law,	Address c/o Agent: Carmody Law,				
707 Summer St, Stamford, CT 06901	707 Summer St, Stamford, CT 06901				
Telephone c/o Agent: 203-252-2677	Telephone				
<sub>Email_</sub> c/o LFeinberg@carmodylaw.com	<sub>Email</sub> c/o LFeinberg@carmodylaw.com				
PROJECT INF	ORMATION:				
Property Address	4.28 +/- Acres				
Acres of altered Wetlands On-Site 0.0 Acres	Cu. Yds. of Material Excavated 1100 CY				
Linear Feet of Watercourse 317.4 LF (total); 196.2 LF (within site).	Cu. Yds. of Material to be Deposited 8140 CY				
Linear Feet of Open Water 0.0 LF	Acres of altered upland buffer				
Sq. Ft. of proposed and/or altered impervious coverage 126,760 SF (total); 123,710 (onsite)	Sq. Ft. of disturbed land in regulated area 29,320 SF				
<b>APPLICATION REQUIREMENTS:</b>					

Is The Site Within a Public	Water Supply
Watershed Boundary? NO	

Is The Site	Within	5 <u>00 F</u> i	eet of a	Town	Boundary?
NO_	YES*				·

\* If the answer is yes, then the applicant is responsible for notifying the appropriate water authority and/or adjoining community's Wetlands Department. Instructions for notification are available at the office of the commission.

#### Page 2 Application for a Significant Regulated Activity

Project Description and Purpose: See enclosed Project Narrative.

In addition, the applicant shall provide eleven (11) collated copies of the following information as well as an electronic	
submission via email to mike.conklin@wiltonct.org & elizabeth.larkin@wiltonct.org **	

$\checkmark$	A.	Written consent from the owner authorizing the agent to act on his/her behalf				
$\checkmark$	В.	A Location Map at a scale of 1" = 800'				
$\checkmark$	C.	A Site Plan showing existing and proposed features at a scale not to exceed 1" = 40' accurate to the level of a A-2 property and T-2 topographic surveys				
$\checkmark$	D.	Sketch Plans depicting the alternatives considered				
$\checkmark$	E.	Engineering Reports and Analysis and additional drawing to fully describe the proposed project				
$\checkmark$	F.	Sedimentation and Erosion Control Plan, including the Construction Sequence				
$\checkmark$	G.	Names and addresses of adjoining property owners				
$\checkmark$	Н.	A narrative describing, in detail				
		a. the proposed activityc. impactsb. the alternatives consideredd. proposed mitigation measures				
$\checkmark$	I.	Soils Report prepared by a Certified Soil Scientist and Wetlands Map prepared by a Registered Land Surveyor				
$\checkmark$	J.	A Biological Evaluation prepared by a biologist or other qualified professional				
$\checkmark$	K	Description of the chemical and physical characteristics of fill material to be used in the Regulated Area				
$\checkmark$	L.	Description and maps detailing the watershed of the Regulated Area				
(1))	М.	Envelopes addressed to adjacent neighbors, the applicant, and/or agent, with <i>certified</i> postage and no return address				

# \*\*Application materials shall be collated and copies of documents more than two pages in length shall be double sided.

See Section 7 of the Wetlands and Watercourses Regulations of the Town of Wilton for a more detailed description of applications requirements.

The Applicant or his/her agent certifies that he is familiar with the information provided in this application and is aware of the penalties for obtaining a permit through deception, inaccurate or misleading information.

By signing this application, permission is hereby given to necessary and proper inspections of the subject property by the Commissioners and designated agents of the Commission or consultants to the Commission, at reasonable times, both before and after a final decision has been rendered.

Applicant's Signature (By Hand):	man de la	why	Date: (018	121
		0	/	1

Agent's Signature (if applicable, By Hand) Am J. Jempy Date: 6/8/21



Lisa L. Feinberg Partner Direct:203-252-2677 Fax:203-325-8608 LFeinberg@carmodylaw.com

707 Summer Street Stamford, CT 06901

June 8, 2021

#### VIA E-MAIL & HAND DELIVERY

Mike Conklin Inland Wetlands Commission Town of Wilton Town Annex 238 Danbury Road Wilton, CT 06897 <u>mike.conklin@wiltonct.org</u>

#### Re: Inland Wetlands Commission Application *Address*: 141 Danbury Road, Wilton, Connecticut *Applicant*: FDSPIN 141 DR LLC

Dear Mr. Conklin:

Our client, FDSPIN 141 DR LLC (the "Applicant"), seeks Inland Wetlands Commission ("IWC") approval of an Application for a Significant Regulated Activity that, if approved, will facilitate the redevelopment of property located at 141 Danbury Road, Wilton Connecticut (the "Property"). The Property is approximately 4.28+/- acres and is located on the westerly side of Danbury Road. The Property is designated as Tax Lot 2 on Map 70 in a DE-5 Design Enterprise District. The Property is currently improved with a warehouse style office building and a large surface parking lot used by Melissa & Doug, Inc. Melissa & Doug, Inc. will be vacating the Property shortly, and relocating to a larger facility. The proposed redevelopment would remove the existing structure and replace it with a new multi-family residential building, dense landscaping and associated site improvements.

Work within the Regulated Area is intended to restore and enhance the natural characteristics of the Property and significantly improve water quality on the site, and provide outdoor, passive recreation space for the residents. While no adverse impacts are anticipated, Best Management Practices (BMPs) as described in the enclosed application materials are incorporated to avoid and minimize potential adverse environmental impacts.

In furtherance of the proposed applications, please find the following materials:

• 1 check in the amount of \$1,260.00, representing the Application Fee & State Land Use Application Fee;

{S7311987}



- 1 Letter of Authority from the Applicant;
- 11 copies of the IWC Application Form for a Significant Regulated Activity, including a Project Narrative & List of Neighboring Property Owners;
- 11 copies of a letter prepared by Environmental Land Solutions, dated June 7, 2021, entitled "Inland Wetlands Application -141 Danbury Road, Wilton, CT;"
- 11 copies of a letter prepared by William Kenny Associates LLC, dated March 15, 2021, entitled "Wetland and Watercourse Delineation, 141 Danbury Road, Wilton, Connecticut;"
- 11 full-size copies of a Landscape Plan prepared by Environmental Land Solutions, dated June 7, 2021, entitled "LP-1 Landscape and Lighting Plan;"
- 11 full-size copies of plans prepared by Tighe & Bond, dated June 7, 2021, entitled:
  - o "C-001 Site Index, Abbreviations, Notes and Legend;"
  - o "C-101 Site Layout Plan;"
  - o "C-102 Fire Truck Turning Plan;"
  - o "C-201 Grading Plan;"
  - o "C-301 Stormwater Management Plan;"
  - o "C-401 Utility Plan;"
  - o "C-501 Soil Erosion and Sediment Control Plan Initial Phase;"
  - o "C-502 Soil Erosion and Sediment Control Plan Fina, Phase;"
  - o "C-503 Soil Erosion and Sediment Control Details;"
  - o "C-504 Soil Erosion and Sediment Control Details;"
  - o "C-601 Details 1;"
  - o "C-602 Details 2;"
  - o "C- 603 Details 3;"
  - o "C-604 Details 4;"
  - o "C-605 Details 5;"
  - o "C-606 Details 6;"
  - o "C-607 Details 7;"
  - "C-608 Details 8;" and
  - o "C-609 Details 9;"
- 11 full size copies of alternative site designs, prepared by Lessard Design, entitled:
  - "A.01a Full Podium, 4 over 1 Option, Site Analysis" dated March 15, 2020; and
  - "A.01 Illustrative Site Plan 141 Danbury Road, Site Analysis," dated January 21, 2021;
- 11 copies of an Engineering Report prepared by Tighe & Bond, dated June 7, 2021, entitled "Engineering Report, Prepared For: FDSPIN 141 DR, LLC;"



• 11 full-size copies of a Topographic Survey depicting existing site conditions, prepared by D'Andrea Surveying & Engineering, P.C., dated April 22, 2021, entitled "Topographic Survey Depicting 141 Danbury Road in Wilton, Connecticut, Prepared for FDSPIN 141 DR LLC."

Please let me know if you have any questions or require additional materials. We look forward to advice as to when the IWC will conduct a public hearing regarding the enclosed application. Thank you for your time and attention regarding this matter.

Sincerely,

Lisa L. Feinberg

Lisa L. Feinberg

Enclosures

cc: E. Larkin <u>elizabeth.larkin@wiltonct.org</u> M. Wrinn <u>Michael.wrinn@wiltonct.org</u>

## Environmental Land Solutions, LLC

Landscape Architecture & Environmental Planning 8 Knight Street, Suite 203, Norwalk, CT 06851 Tel: (203) 855-7879 Fax: (203) 855-7836

June 7, 2021

Inland Wetlands Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897

Re: Inland Wetlands Application 141 Danbury Road, Wilton, CT

Dear Members of the Commission:

The applicant, FDSPIN 141 DR, LLC, is proposing to redevelop the above referenced property from an existing commercial building to a multi-family residential building. The site fronts on the eastern side of Danbury Road, with the Norwalk River to its west and existing light industry uses to the north and south. Lambert Commons, a multi-family residential development is located across the street.

The Norwalk River and its riparian wetlands occur along the western boundary of the site. Environmental Land Solutions, LLC (ELS) has been authorized by FDSPIN 141 DR, LLC to prepare this biological assessment report as required for this application and to prepare a new riparian buffer planting plan with recreational area to the rear of the site. To complete this evaluation , site visits were made by ELS staff on April 8 and May 8, 2021. Site plans prepared by Tighe & Bond were reviewed as part of this evaluation.

#### **EXISTING CONDITIONS**

The subject  $4.2 \pm$  acre property is located at 141 Danbury Road. The existing building is centrally located with paved parking extending along the south and west portion of the site. The east and north areas of the site are maintained as lawn. The site is presently developed with impervious surfaces covering  $67\% \pm$  of the property that gently slope toward the river. The paved parking lot extends down to the river's edge. Clearing along the rivers edge occurred over the last year and was replanted as part of Corrective Action Permit.

#### Wetlands and Watercourses

The Norwalk River is the predominate wetland resource feature of the site and defines the development to the west. A narrow riparian wetland corridor occurs between the river bank and the parking lot. The wetland line was recently delineated by William Kenny Associates.

The wetland adjacent to the river is a seasonally flooded palustrine wetland. Flagged wetland soils were identified as Rippowam fine sandy loam and Fluvaquent-Udifluvents complex, poorly to well drained alluvial soils. Please refer to the soil report for additional information. The Norwalk River is a perennial watercourse that has been channelized but includes riffle-pool morphology.

The northwest shoreline of the site is defined by riprap, poured and broken pieces of concrete with two sycamore trees on the shoreline. The southwestern shoreline is partially naturalized, but recently cleared of large trees and replanted under a Corrective Action Permit in 2020. This portion of the shoreline is define by a large woodchip berm and 9 planted tree and several shrubs. Existing naturalized vegetation growing along the shoreline includes, Asiatic Bittersweet, Mugwort, Japanese Honeysuckle, Ash saplings, shrub Honeysuckle, Poison Ivy, Garlic Mustard, Euonymus, and Multiflora Rose.

There appears to be no treatment of stormwater runoff from impervious surfaces at the site.

#### Wetland and Watercourse Functions

The functional evaluation of the wetlands is based on professional experience and the suggested criteria cited in the publication entitled "<u>The Highway Methodology Workbook</u> *Supplement*, Wetland Functions and Values, *A Descriptive Approach*," prepared by the US Army Corps of Engineers, NEDEP-360-1-30a, September 1999.

Using this publication, the primary functions provided by the wetlands include sediment retention, nutrient removal and transformation, stormwater storage, wildlife habitat, visual quality, and limited recreational usage such as nature photography and wildlife observations. The Norwalk River corridor functions as a habitat for finfish and aquatic waterfowl and other aquatic-dependent species, serves as a wildlife corridor (together with its fringe wetlands), a groundwater discharge point, and offers recreational potential such as fishing and small craft boating.

#### Wildlife

The existing site provides little to no wildlife habitat due to existing improvement adjoining the river. However, naturalized areas to the south, north and west are expected to support a range of species adapted to suburban residential habitats, small woodland tracts, and woodland edges. Theses may provide habitat for wetland dependent wildlife species within the river and riparian edge and provide a small refuge for suburban tolerant wildlife, and are capable of providing habitats for suburban tolerant wildlife species in the form of cover, nesting areas, and food.

The site is not located within a highlighted DEEP Natural Diversity Data Base (NDDB) map for Wilton (May Dec. 2020).

#### **PROPOSED CONDITIONS**

The development will place a new multi-family single building central locally on the site. The existing paved parking lot adjacent to the river will be removed and a recreational area and planted riparian buffer installed in its place. The bulk of the building is outside of the wetland 100' upland review area, with the closer corner (western) at 88' from the river. Most of the parking is located beneath the building, however some small areas of parking extends outside of the building at the northwestern corner of the building, where the closest corner is  $66' \pm$  from the river. However, all surface parking within 200' + of the river will be constructed with porous pavements. No work is occurring in the wetlands, and 85% of the 100' buffer, totaling  $25,020 \text{ sf} \pm$ , will be refurbished from a paved parking lot to a recreational area for the new residences, with extensive replanting of native trees, shrubs, and perennials.

The new development will slightly increase the impervious surfaces on the site. However, significantly improvements to the river buffer and the new stormwater drainage system will dramatically improve water quality leaving the site. The proposed storm drainage management for the site has been developed by Tighe & Bond to provide collection, removal of suspended solids, treatment and infiltration of the first 1" of rainfall.

The following list reflects the proposed activities within the 100' upland review area of the site that encompasses  $32,640 \pm$  sf of the property. This area is now encumbered by  $25,020 \text{ sf} \pm (75\% \text{ of the upland review area})$  of asphalt surface parking.

- 1. Temporary installation of sediment and erosion controls.
- 2. Removal of surface asphalt, concrete and the underlying base  $(21,140 \pm \text{ sf})$ .
- 3. Installation of pervious asphalt ( $4470 \pm$  sf).
- 4. Construction of building (above the ground) totaling  $315 \pm \text{ sf}$ , in the upland review area.
- 5. Construction of a fire lane with grass pavers  $(3450 \pm \text{ sf})$ .
- 6. Construction of a level spreader.
- 7. Import of topsoil to replace asphalt parking for new landscape areas ( $780 \pm$  cy).
- 8. Landscaping areas with native trees, shrubs, and perennials  $(11,650 \pm \text{ sf})$ .
- 9. Planting of new lawn  $(11,615 \pm \text{sf})$ . 1
- 10. Pervious walking paths  $(9,375 \pm \text{ sf})$ .
- 11. Removal and management of invasive species along the river's edge  $(300' \pm)$ .

#### Wetland/Watercourse Potential Impacts and Mitigation Measures

The majority of the site work proposed within the 100' upland review area is intended to restore and expand the functions provided by the river's riparian buffer, while also providing outdoor recreation spaces for the residences. This will be accomplished by removing existing pavement and providing treatment of stormwater runoff treatment to diminish direct discharge to the river, and significantly planting the 100' upland review area with native plants.

The project does not anticipated any long term impacts to the wetland resources. There are no direct disturbances proposed with this development. However, short term disturbances will be managed adjacent to the resources to prevent exposed soil surfaces from entering the wetland and the river.

The following Best Management Practices (BMPs) have been incorporated into the site plans for the purposes of avoiding and/or minimizing potential adverse environmental impacts disturbances and site improvements over the site.

- a. *erosion and sedimentation controls* the site plans indicate that erosion and sedimentation will be controlled by the use of silt fencing to trap sediments within stormwater runoff, anti-tracking pads to remove sediments from tires of construction vehicles, and watering of the site's soils as needed to prevent dust.
- b. *catch basins fitted with sumps* designed to improve water quality by trapping sediments from roadway stormwater runoff. Accumulated sediments will be periodically removed as needed to maintain the basins in proper working order.
- c. *swirl concentrators* designed to maintain water quality by trapping road sediments, floatables (litter), and vehicle oils and grease from stormwater runoff. Accumulated sediments, litter and oils will be periodically removed as needed to maintain the system in proper working order.
- d. *underground infiltration galleries* designed to store stormwater runoff for a period of time and infiltrate stormwater runoff into the ground. Underground infiltration galleries reduce flooding, recharge groundwater, and remove dissolved pollutants as it filters through the soil below. Underground galleries also reduce thermal pollution associated with heated runoff from pavement areas.
- e. *porous pavement* porous pavement can help reduce runoff by infiltrating rain water and melting snow. These materials allow rain and snow melt to seep through the surface down to underlying layers of soil and gravel. In addition to reducing the runoff, permeable pavements can help filter out pollutants that contribute to water pollution. Permeable pavements can also reduce the need for road salt during the winter months. The western portion of the surface pavement is proposed to be pervious.
- f. *stone trenches* proposed stone trenches surround the western edge of the porous pavement. Stone trenches will capture any excess runoff from the porous pavement.

Stone trenches will help cleanse stormwater runoff collected from the new driveway, building roof, and landscape areas by trapping sediments and removing nutrients through plant uptake, and by infiltration. As infiltration occurs, thermal pollution will be reduced from development areas, runoff volume from the development will be reduced and recharge groundwater will occur.

- g. *overland flow* stormwater runoff flowing over newly vegetated buffer areas will result in the trapping of sediments, uptaking of nutrient by plants, and infiltrating runoff. This BMP will occur over the site's proposed landscaped areas.
- h. *planted buffers* native shade trees, understory trees, shrubs, and herbaceous plants are proposed within the wetland buffer for wildlife habitat and aesthetic purposes. Planted buffers will also help to maintain water quality aiding to remove pollutants within stormwater runoff by plant uptake. The new riparian buffer along the river will change from a width of 0 to  $35' \pm$  to 60 to  $100' \pm$  in width. The new river buffer will include planting of 49 shade and understory trees, over 375 shrubs and over 500 perennials known to benefit pollinators.
- i. *level spreader* a linear level area of stone is proposed at the end of the drainage pipe from the storm drainage system to slow the velocity of the discharged stormwater runoff and prevent erosion.
- j. *control of invasive nonnative plant species* the Landscape Plan indicates the control of Japanese Knotweed, Mugwort, Multiflora Rose, and Porcelainberry for a minium of a two year period during the bonding period and is expected to be included in the regular maintenance for the site.

#### HABITAT IMPROVEMENTS

The existing site is lacking a significant habitat to support local wildlife, primarily due to the existing paved parking lot which consumes most of the river's riparian buffer. The proposed plan will enhance wildlife habitat planting native trees and shrubs that native species, and provide food sources, nesting site, and cover for local and migratory wildlife.

In addition the plan includes:

- 1. Placement of 3 bird houses, final location to be determined in the field.
- 2. Place of one bat box, final location to be determined in the field.
- 3. Provide allowances of some plant debris to remain in riparian buffer, with appropriate signage to alert residence of the areas value.
- 4. Replacement of solid concrete slabs along the river's edge, with broken stones, providing niches for wildlife and allowing vegetation to expand and stabilized the river's edge.
- 5. Planting a grove of American Holly trees within the riparian buffer for food source, nesting and winter protection.

6. Planting perennials in the buffer enhancement area known for their pollinator value.

In addition, the applicant is willing to adopted an Organic Land Care Practice for the on going project maintenance. ELS will submit a packet for the staff's review and adoption for the project.

#### ALTERNATIVES

As part of the application for a Significant Regulated Activity, the applicant has included two earlier versions of the site plan as required by Section 7.5-c of the Inland Wetlands and Watercourses Regulations for the Town of Wilton (the "Regulations"). These preliminary site analysis plans (Sheet A.01A, dated 3/15/20 and Sheet A.01, dated 1/21/21), prepared by Lessard Design, are included as alternative plans that were explored, discussed and ultimately discarded during the design process. It is important to note that, while the disturbance in the regulated area is considered significant based on the thresholds in the Regulations, all work within this area involves landscape enhancements and water quality improvements.

The alternative plans were eliminated after review and further discussion with the design team, town staff and the Planning & Zoning Commission (during a pre-application review). In lieu of utilizing existing developed areas, the applicant was encouraged to relocate units from the rear of the site to the top of the building thereby significantly enhancing the landscape buffer adjacent to the river and adding additional height to the building to compensate for the loss of units at the back of the site.

Both of these alternatives would leave developed areas on the site essentially "undisturbed" with asphalt approaching the river's edge, but do not provide the room to replace and significantly enhance the buffer along the river. Instead, the applicant has chosen to modify the zoning regulations to permit additional height and the consolidation of the development further from the river. This provides an added opportunity for water quality improvements as well as wetland buffer enhancements. These changes make this submitted site plan superior to these earlier plans, as it relates to protection and enhancements to the river and wetland resources.

#### SUMMARY

This proposal has incorporated techniques to reduce impacts to the wetland resources within the site by decreasing the existing impacts to the Norwalk River and its associated resources. The proposed site redevelopment will significantly reduce existing manmade intrusions into the 100' upland review area, improve water quality and significantly expanded native plants on the site. The expanded river buffer will also serve as a passive recreation area for the residents of the new building. These site improvements are expected to enhance the wetland's sediment retention, nutrient removal and transformation, stormwater storage, wildlife habitat, visual quality, and recreational usage.

The proposed site work, taken in total, will provide a net environmental benefit to the Norwalk

River and the riparian wetland. The character and functions of the onsite regulated areas are expected to be significantly improvement after the completion of this site work.

Sincerely,

at the

Kate Throckmorton, ASLA Landscape Architect Professional in Erosion and Sediment Control Certified NOFA Professional

m Matth

Matthew J. Popp, ASLA Professional Wetland Scientist Landscape Architect

Danbury Road 141-wilton-ea.wpd

#### WILLIAM KENNY ASSOCIATES LLC

SOIL SCIENCE ECOLOGICAL SERVICES LAND USE PLANNING LANDSCAPE ARCHITECTURE

March 15, 2021

Mr. Leonard D'Andrea Rocco V. D'Andrea, Inc. Six Neil Lane P. O. Box 549 Riverside, CT 06878

Re: Wetland and Watercourse Delineation 141 Danbury Road, Wilton, Connecticut

Dear Mr. D'Andrea:

As requested, we visited the referenced property to determine the presence or absence of wetlands and/or watercourses, to demarcate (flag) the boundaries of wetlands and watercourses identified, and to identify onsite soil types. This letter includes the methods and results of our investigation, which we completed today, March 15, 2021. In summary, one inland wetland and watercourse system was identified and delineated. The system, which extends and flows north to south along the western property boundary, is a segment of the Norwalk River with a bordering wet floodplain wetland.

#### **Regulatory Definitions**

The Inland Wetlands and Watercourses Act (Connecticut General Statutes §22a-38) defines <u>inland</u> <u>wetlands</u> as "land, including submerged land...which consists of any soil types designated as poorly drained, very poorly drained, alluvial, and floodplain." <u>Watercourses</u> are defined in the act as "rivers, streams, brooks, waterways, lakes, ponds, marshes, swamps, bogs and all other bodies of water, natural or artificial, vernal or intermittent, public or private, which are contained within, flow through or border upon the state or any portion thereof." The Act defines <u>Intermittent Watercourses</u> as having a defined permanent channel and bank and the occurrence of two or more of the following characteristics: A) evidence of scour or deposits of recent alluvium or detritus, B) the presence of standing or flowing water for a duration longer than a particular storm incident, and C) the presence of hydrophytic vegetation.

195 TUNXIS HILL CUTOFF S FAIRFIELD, CT 06825 PHONE: 203 366 0588 FAX: 203 366 0067 www.wkassociates.net

#### Mr. Leonard D'Andrea Re: 141 Danbury Road, Wilton, Connecticut

#### Methodology

A second order soil survey in accordance with the principles and practices noted in the USDA publication *Soil Survey Manual* (1993) was completed at the subject site. The classification system of the National Cooperative Soil Survey was used in this investigation. Soil map units identified at the project site generally correspond to those included in the *Soil Survey of the State of Connecticut* (USDA 2005).

<u>Wetland</u> determinations were completed based on the presence of poorly drained, very poorly drained, alluvial, or floodplain soils. Soil types were identified by observation of soil morphology (soil texture, color, structure, etc.). To observe the morphology of the property's soils, test pits and/or borings (maximum depth of two feet) were completed at the site.

<u>Intermittent watercourse</u> determinations were made based on the presence of a defined permanent channel and bank and the occurrence of two or more of the following characteristics: A) evidence of scour or deposits of recent alluvium or detritus, B) the presence of standing or flowing water for a duration longer than a particular storm incident, and C) the presence of hydrophytic vegetation.

Wetland boundaries were demarcated (flagged) with pink surveyor's tape (hung from vegetation) or small flags (on wire stakes) labeled "William Kenny Associates" that are generally spaced a maximum of every 50 feet. Complete boundaries are located along the lines that connect these sequentially numbered flags. <u>The wetland boundaries are subject to change until adopted by local</u>, state, or federal regulatory agencies.

#### Results

The approximate 4.3-acre commerical property is located at 141 Danbury Road in Wilton, Connecticut. Danbury Road borders the eastern property boundary. Property improvements include a commercial building and an asphalt parking area and driveway. The primary vegetative cover at the property is lawn with other ornamentals and some shade trees. A meadow is present in the southwestern portion of the property.

One inland wetland and watercourse system was identified and delineated. The system, which extends and flows north to south along the western property boundary, is a segment of the Norwalk River with a bordering wet floodplain wetland. Wetland soils are primarily poorly drained and formed from alluvial deposits. The approximate location of the system is shown on the attached map. The boundary of the system was marked at the site with flags numbered 1 to 17.

Three soil map units were identified on the property (two wetland and one upland). Each map unit represents a specific area on the landscape and consists of one or more soils for which the unit is named. Other soils (inclusions that are generally too small to be delineated separately) may account for 10 to 15 percent of each map unit. The mapped units are identified in the following table by name and symbol and typical characteristics (parent material, drainage class, high water table, depth to bedrock, and slope). These characteristics are generally the primary characteristics to be considered in land use planning and management. A description of each characteristic and their land use implications follows the table. A complete description of each soil map unit can be found in the *Soil Survey of the State of Connecticut* (USDA 2005), and at

*https://soilseries.sc.egov.usda.gov/osdname.aspx*. On the day of the review, there was no soil frost and no snow cover. The upland soil was moist and the wetland soil was wet to inundated. The sky was clear and air temperatures were in the 30's ° F.

<u>Sym</u> .	<u>Map Unit</u> <u>Name</u>	Parent <u>Material</u>	<u>Slope</u> (%)	Drainage <u>Class</u>	<u>Hig</u> <u>Depth</u> (ft)	<u>gh Water Ta</u> <u>Kind</u>	able <u>Mos</u> .	Depth To <u>Bedrock</u> (in)
<u>L</u>	Ipland Soil							
308	Udorthents, Smoothed	Excavated or Filled Soil (>2 feet)	0-45	Well Drained to Somewhat Poorly Drained	1.5->6.0	Apparent	Nov-May	>60
<u> /</u>	Vetland Soil							
103	Rippowam fine Sandy loam	Alluvium	0-3	Poorly Drained	0.0-1.5	Apparent	Nov-Jun	>60
109	Fluvaquents- Udifluvents complex, frequently flooded	Alluvium Alluvium	0-3 0-3	Poorly Drained Well Drained	0.0-1.0 >6.0	Apparent 	Oct-May 	>60 >60

Parent material is the unconsolidated organic and mineral material in which soil forms. Soil inherits characteristics, such as mineralogy and texture, from its parent material. Glacial till is unsorted, nonstratified glacial drift consisting of clay, silt, sand, and boulders transported and deposited by glacial ice. Glacial outwash consists of gravel, sand, and silt, which are commonly stratified and deposited by glacial melt water. Alluvium is material such as sand, silt, or clay, deposited on land by streams. Organic deposits consist of decomposed plant and animal parts.

A soil's texture affects the ease of digging, filling, and compacting and the permeability of a soil. Generally sand and gravel soils, such as outwash soils, have higher permeability rates than most glacial till soils. Soil permeability affects the cost to design and construct subsurface sanitary disposal facilities and, if too slow or too fast, may preclude their use. Outwash soils are generally excellent sources of natural aggregates (sand and gravel) suitable for commercial use, such as construction sub base material. Organic layers in soils can cause movement of structural footings. Compacted glacial till layers make excavating more difficult and may preclude the use of subsurface sanitary disposal systems or increase their design and construction costs if fill material is required.

Generally, soils with steeper slopes increase construction costs, increase the potential for erosion and sedimentation impacts, and reduce the feasibility of locating subsurface sanitary disposal facilities.

Drainage class refers to the frequency and duration of periods of soil saturation or partial saturation during soil formation. Seven classes of natural drainage classes exist. They range from excessively drained, where water is removed from the soil very rapidly, to very poorly drained, where water is removed so slowly that free water remains at or near the soil surface during most of the growing season. Soil drainage affects the type and growth of plants found in an area. When landscaping or gardening, drainage class information can be used to assure that proposed plants are adapted to

#### Mr. Leonard D'Andrea Re: 141 Danbury Road, Wilton, Connecticut

existing drainage conditions or that necessary alterations to drainage conditions (irrigation or drainage systems) are provided to assure plant survival.

High water table is the highest level of a saturated zone in the soil in most years. The water table can affect the timing of excavations; the ease of excavating, constructing, and grading; and the supporting capacity of the soil. Shallow water tables may preclude the use of subsurface sanitary disposal systems or increase design and construction costs if fill material is required.

The depth to bedrock refers to the depth to fixed rock. Bedrock depth affects the ease and cost of construction, such as digging, filling, compacting, and planting. Shallow depth bedrock may preclude the use of subsurface sanitary disposal systems or increase design and construction costs if fill material is required.

#### **Conclusions**

Today, we investigated the property at 141 Danbury Road in Wilton, Connecticut and identified and delineated one inland wetland and watercourse system. Thank you for the opportunity to assist you. If you should have any questions or comments, please do not hesitate to contact us.

Sincerely,

William L. Kenny, PWS, PLA Soil Scientist

Enclosure

Ref. No. 4798

Alexander Wojtkowiak Soil Scientist

**308** UDORTHENTS, SMOOTHED JPLAND

FLUVAQUENTS-UDIFLUVENTS COMPLEX **RIPPOWAM FINE SANDY LOAM** WETLAND 103 109



ОАИВИRY ROAD

# NOTES:

INFORMATION SHOWN ON THIS DRAWING, INCLUDING THE WETLAND BOUNDARY, IS APPROXIMATE. THE BOUNDARY IS NOT A SURVEYED REPRESENTATION OF WHAT WAS FIELD MARKED (FLAGGED). •

FLAG # 17

- WETLAND AND SOIL INFORMATION PROVIDED BY WILLIAM KENNY ASSOC. OTHER INFORMATION TAKEN FROM A TOWN OF WILTON GIS MAP.
  - DELINEATION REPORT FOR THE SOIL MAP UNIT NAMES AND ADDITIONAL 308, 103 AND 109 ARE SOIL MAPPING UNIT SYMBOLS. SEE WETLAND RELATED INFORMATION.

SUBSTANTIALLY REPRESENTS THE SOILS **THE FIELD** CERTIFY THAT THIS WETLAND MAP CIENTIS **JS MAPI** VILLIAM L. KE ŴE

# WETLAND & WATERCOURSE MAP

**195 TUNXIS HILL CUTOFF S** FAIRFIELD, CT 06825

**ASSOCIATES LLC** SOIL SCIENCE

WILLIAM KENNY

ECOLOGICAL SERVICES

LAND USE PLANNING

LANDSCAPE ARCHITECTURE

NORTH

Ref. No. 4798

DATE: MARCH 15, 2021 SCALE: NOT TO SCALE

WILTON, CONNECTICUT **141 DANBURY ROAD** 

#### List of Neighboring Property Owners

#### 141 Danbury Rd 5/20/2021 (updated 6/8/2021)

	MBLU	Street Address	Owner's Address
1.	55-1-1	1 Lambert Common	Patricia A Garrett &
			Lorraine Danchise
			1 Lambert Common
			Wilton, CT 06897
2.	55-1-2	2 Lambert Common	Sonya Kelepecsz
			2 Lambert Common
			Wilton, CT 06897
3.	55-1-3	3 Lambert Common	Nanette O Rich
			3 Lambert Common
			Wilton, CT 06897
4.	55-1-4	4 Lambert Common	Olga L Rhodes
			4 Lambert Common
			Wilton, CT 06897
5.	55-1-5	5 Lambert Common	Eileen K Meyers
			5 Lambert Common
			Wilton, CT 06897
6.	55-1-6	6 Lambert Common	Denise Melato
			6 Lambert Common
			Wilton, CT 06897
7.	55-1-7	7 Lambert Common	Irene R Farley
			7 Lambert Common
			Wilton, CT 06897
8.	55-1-8	8 Lambert Common	The Canine Companies Inc
			493 Danbury Rd
			Wilton, CT 06897
9.	55-1-9	9 Lambert Common	Est of Clarice Derubeis
			C/O Elena Rieders Admin
			55 Brambling La
			Voorhees, NJ 08043
10.	55-1-10	10 Lambert Common	Blanche R Goodwin
			10 Lambert Common
			Wilton, CT 06897
11.	55-1-11	11 Lambert Common	OLK Holdings LLC
			20 Colonial Ave
			Princeton Junction, NY 08550
12.	55-1-12	12 Lambert Common	Leslie K Johnson
			Po Box PP
			Mclean, VA 22101

13.	55-1-13	13 Lambert Common	Marie A Ritch
			13 Lambert Common
			Wilton, CT 06897
14.	55-1-14	14 Lambert Common	Sherrill L Werblood
			14 Lambert Common
			Wilton, CT 06897
15.	55-1-15	15 Lambert Common	Carol A Devine
			1446 Unquowa Rd
			Fairfield, CT 06824
16.	55-1-16	16 Lambert Common	Susan A Wall
			16 Lambert Common
			Wilton, CT 06897
17.	55-1-17	17 Lambert Common	Rebecca Tzanos
			17 Lambert Common
			Wilton, CT 06897
18.	55-1-18	18 Lambert Common	Elizabeth Kimball Dempsey Tr
			18 Lambert Common
			Wilton, CT 06897
19.	55-1-19	19 Lambert Common	Meredith Anne Munro MacLaine
			19 Lambert Common
			Wilton, CT 06897
20.	55-1-20	20 Lambert Common	Phyllis F Zappala Trustee
			18 Buttonball La
			Weston, CT 06883
21.	55-1-21	21 Lambert Common	Est Ellen Morrone
			Steven D Smith
			P O Box 390
			C/O Lovejoy And Rimer Pc
			Norwalk, CT 06852
22.	55-1-22	22 Lambert Common	Richard & Edith Canzonetti
			22 Lambert Common
			Wilton, CT 06897
23.	55-1-23	23 Lambert Common	Donald A & Eileen P Allers
			23 Lambert Common
			Wilton, CT 06897
24.	55-1-24	24 Lambert Common	Rita H Hausdorff
			24 Lambert Common
			Wilton, CT 06897
25.	55-1-25	25 Lambert Common	Gabriel C Andreescu &
			Sarah A Andreescu
			25 Lambert Common
			Wilton, CT 06897
26.	55-1-26	26 Lambert Common	Kim Gumsook & Hwi Tae
			26 Lambert Common
			Wilton, CT 06897
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27.	55-1-27	27 Lambert Common	Nancy Burroughs
			27 Lambert Common
			Wilton, CT 06897
28.	55-1-28	28 Lambert Common	Margaret M Kelley
			28 Lambert Common
			Wilton, CT 06897
29.	55-1-29	29 Lambert Common	Catherine J Mannix
			32 Dorothy Rd
			Redding, CT 06896
30.	55-1-30	30 Lambert Common	Mady E McSweeney
			30 Lambert Common
			Wilton, CT 06897
31.	55-1-31	31 Lambert Common	Barbara F Sage
			31 Lambert Common
			Wilton, CT 06897
32.	55-1-32	32 Lambert Common	James M Campbell
_		-	32 Lambert Common
			Wilton, CT 06897
33.	55-1-33	33 Lambert Common	Kurt & Christine Olson
			33 Lambert Common
			Wilton, CT 06897
34.	55-1-34	34 Lambert Common	Mariorie Simpson &
0.11			Samuel Simpson & Sv
			34 Lambert Common
			Wilton, CT 06897
35	55-1-35	35 Lambert Common	Lori A Bufano
	00 1 00		35 Lambert Common
			Wilton, CT 06897
36	55-1-36	36 Lambert Common	Ann Brooke Swenson
50.	00 1 00		36 Lambert Common
			Wilton CT 06897
37	55-1-37	37 Lambert Common	Richard A Edgar &
57.	55 1 57		I orraine Jean Edgar & Sv
			37 Lambert Common Unit #347
			Wilton CT 06897
38	55-1-38	38 Lambert Common	Jeannette R Pascarelli
50.	55 1 50		38 Lambert Common
			Wilton CT 06897
30	55-1-39	39 Lambert Common	Ioseph C & Gail M Cioffi
57.	55-1-57	57 Lamoert Common	30 Lambert Common
			Wilton CT 06897
40	55-1-40	40 Lambert Common	Roslyn Dobey
40.	55-1-40		40 Lambert Common
			Wilton CT 06807
1	1		witton, C1 00077

41.	55-1-41	41 Lambert Common	Mary B Preston
			41 Lambert Common
			Wilton, CT 06897
42.	55-1-42	42 Lambert Common	Denise Robertson
			42 Lambert Common
			Wilton, CT 06897
43.	55-1-43	43 Lambert Common	John Cocozza
			43 Lambert Common
			Wilton, CT 06897
44.	55-1-44	44 Lambert Common	Elizabeth Picone Trustee
			44 Lambert Common
			Wilton, CT 06897
45.	55-1-45	45 Lambert Common	Aaron & Erin Jacobstein
			153 Bob Hill Rd
			Ridgefield, CT 06877
46.	55-1-46	46 Lambert Common	Lin Xin Yu
			46 Lambert Common
			Wilton, CT 06897
47.	55-1-47	47 Lambert Common	Bruce D Hampson
			47 Lambert Common
			Wilton, CT 06897
48.	55-1-48	48 Lambert Common	Janet M Bondeson
			48 Lambert Common
			Wilton, CT 06897
49.	55-1-49	49 Lambert Common	Leslie A Miles
			49 Lambert Common
			Wilton, CT 06897
50.	55-4-1	1 Wilton Hills	James A & Linda L Kaylor
			1 Wilton Hills
			Wilton, CT 06897
51.	55-4-2	2 Wilton Hills	Frank & Carol Gavel
			2 Wilton Hills
			Wilton, CT 06897
52.	55-4-3	3 Wilton Hills	Joseph & Lois Block
			3 Wilton Hills
			Wilton, CT 06897
53.	55-4-4	4 Wilton Hills	Frank L Picchione
			4 Wilton Hills
			Wilton, CT 06897
54.	55-4-5	5 Wilton Hills	Kaushik Ramamoorthy &
			Muthukrishnan Aarthie
			5 Wilton Hills
			Wilton, CT 06897
55.	55-4-6	6 Wilton Hills	Kenneth J Wilchfort
			6 Wilton Hills
			Wilton, CT 06897

56.	55-4-7	7 Wilton Hills	Gregg Feldman Lynn Schlesinger 7 Wilton Hills
			Wilton, CT 06897
57.	55-4-8	8 Wilton Hills	Hollis E Wright-Warren
			8 Wilton Hills
			Wilton, CT 06897
58.	55-4-9	9 Wilton Hills	G William Brautigam &
			Nancy L Brautigam
			9 Wilton Hills
			Wilton, CT 06897
59.	55-4-10	10 Wilton Hills	Mullapudi Venkata Ramakrishna &
			Kakarla Kalyani
			10 Wilton Hills
		4.4 33714. 33714	Wilton, CT 06897
60.	55-4-11	11 Wilton Hills	Fred Rzepka
			25250 Rockside Rd
(1	55 4 12		Bedford Heights, OH 44140
61.	55-4-12	12 Wilton Hills	Jack M & Laura Boyles
			Wilton CT 06807
62	55 / 12	12 Wilton Hills	Charles Calvin Thomas &
02.	55-4-15	13 whon Hills	Batty Wells Thomas
			13 Wilton Hills
			Wilton CT 06897
63.	55-4-14	14 Wilton Hills	Sriram S Belur &
0.5.	00 1 1 1		Brunda B Govinda
			14 Wilton Hills
			Wilton, CT 06897
64.	55-4-15	15 Wilton Hills	Andrew M Schopick
			15 Wilton Hills
			Wilton, CT 06897
65.	55-4-16	16 Wilton Hills	Tsui Tak Kwan
			Kun Sharon
			16 Wilton Hills
			Wilton, CT 06897
66.	55-4-17	17 Wilton Hills	Ajitabh Kaushal &
			Sharan Chetna
			17 Wilton Hills
			Wilton, CT 06897
67.	55-4-18	18 Wilton Hills	Michele A Rudnicki
			18 Wilton Hills
(0)			Wilton, CT 06897
68.	55-5	116 Danbury Rd	KEIF III Danbury Road LLC
			230 Park Ave
			New York, NY 10169

69.	56-1	149 Danbury Rd	Ring's End Inc Po Box 1066
			Darien, CT 06820
70.	56-2	153 Danbury Rd	State of Connecticut
			2800 Berlin Tpke
			Newington, CI 06131
71.	56-3	159 Danbury Rd	State of Connecticut
			2800 Berlin Tpke
			Newington, CT 06131
72.	56-5	Danbury Rd	State of Connecticut
			2800 Berlin Tpke
	56.45		Newington, C1 06131
73.	56-45	156 Danbury Rd	State of Connecticut
			2800 Berlin Tpke
7.4			Newington, C1 06131
/4.	36-46A-BC	Danbury Rd	State of Connecticut
			2800 Berlin Ipke
75	(0.20	111 D 1 D1	Newington, C1 06131
/5.	69-38	111 Danbury Rd	Cubesmart LP
			C/O PIA-CS#831
			Po Box 320099
7(	(0.41	120 Davidara D 1	Alexandria, VA 22320
/0.	69-41	129 Danbury Rd	Ring's End Incorporated
			PO BOX 1000
	70.1	121 Denhum Dd	ECL Wilton LLC
//.	/0-1	131 Danbury Rd	FGI WIIION LLC
			Mt Vernon NV 10550
78	70.2	141 Danhumy Pd	
70.	10-2		Po Box 590
			Westport CT 06881
70	70-3	17 Wolfpit Rd	State of Connecticut
1).	70-5		2800 Berlin Take
			Newington CT 06131
80	70-2A	Danbury Rd	State of Connecticut
00.	10 211	Dunioury Rd	2800 Berlin Trke
			Newington, CT 06131
81.	55-1	1-49 Lambert Common	The Property Group of Ct., Inc.
011			25 Crescent Street
			Stamford, CT 06906
82.	55-4	1-18 Wilton Hills	4 Wilton Hills
			4 Wilton Hills
			Wilton, CT 06897
83.		1-18 Wilton Hills	19 Wilton Hills
			19 Wilton Hills
			Wilton, CT_06897

84.	70-16-1	Danbury Rd	The Conn Light & Power Co
		-	PO Box 270
			Hartford, CT 06141
85.			Metro North
			Ron Bottacari
			347 Madison Avenue
			New York, NY 10022
86.			David Willard
			525 Water Street
			Bridgeport, CT 06601
87.			Seth Cummins, Esq.
			347 Madison Avenue
			New York, NY 10017
88.			Penn Central
			Metro-North Railroad – Suburban
			Station
			4 Penn Central Plaza – Floor 1200
			Philadelphia, PA 19103
89			Penn Central
0,7.			Metro-North Railroad
			4 Penn Central Plaza – Floor 1200
			Philadelphia PA 19103
90			State of Connecticut Dept. of
<i>y</i> 0.			Transportation
			Julie Thomas
			Office of Rail – Union Station – $4^{\text{th}}$
			Floor West
			50 Union Ave.
			New Haven, CT 06519
91.			State of Connecticut Dept. of
			Transportation
			Julie Thomas
			4 Brewery Street
			New Haven, CT 06519
92.			State of Connecticut Dept. of
			Transportation
			Robert Ike
			2800 Berlin Turnpike
			P.O. Box 317546
			Newington, CT 06131
93.			Amy Martinez, Transportation
			Principal Property Agent
			Department of Transportation
			Appraisals/Property Management
			Division
			2800 Berlin Turnpike

		P.O. BOX 317546
		Newington, CT 06131-7546
94.		Sheila Mary Sopper
		Director, Real Estate Development &
		Operations
		National Railroad Passenger
		Corporation (AMTRAK)
		30th Street Station, Floor 5S
		2955 Market Street
		Philadelphia, PA 19104
95.		Alan Warner
		Senior Manager, Real Estate
		Development
		National Railroad Passenger
		Corporation (AMTRAK)
		30th Street Station - 5S-014 - Box 25
		2955 Market Street
		Philadelphia, PA 19104
96.		Theodore Smigelski
		Connecticut Department of
		Transportation
		Office of Rail - Property Management
		Unit
		Component Change Out Building - 4th
		Floor
		4 Brewery Street
		New Haven, CT 06519
1		

LEGEND	
DESCRIPTION	
PROPERTY LINE	
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EASEMENT LINE	
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INDEX CONTOURS	
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MAGNITUDE & DIRECTION OF SLOP	>
STORM DRAIN	
GRAVITY SANITARY SEWER	
SANITARY SEWER FORCE MAIN	
SANITARY SEWER LOW PRESSURE	
WATER SERVICE	
POTABLE WATER	
FIRE SERVICE	
HIGH PRESSURE FIRE SERVICE	
UNDERGROUND ELECTRIC	
PRIMARY ELECTRIC SERVICE	
SECONDARY ELECTRIC	
OVERHEAD ELECTRIC	
TELEPHONE SERVICE	
TEL-DATA SERVICE	
COMMUNICATIONS SERVICE	
CABLE TV SERVICE	
GAS SERVICE	
CHILLED WATER RETURN	
HOT WATER RETORN	
STEAM CONDENSATE	
LOW PRESSURE STEAM	
MEDIUM PRESSURE STEAM	
HIGH PRESSURE STEAM	
OXYGEN SERVICE	
OVERHEAD UTILITY (UNSPECIFIED)	)
CURB	
EDGE OF PAVEMENT	
DIRT ROAD	
SIDEWALK	
RETAINING WALL	
STONE WALL	
FENCE - UNSPECIFIED	
FENCE - CHAIN LINK	
STORM DRAIN STRUCTURES	
SANITARY SEWER MANHOLE	
WATER SERVICE STRUCTURES	
GAS SERVICE STRUCTURES	
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# LEGEND

RESOURCE AREAS VEGETATED WETLAND LIMIT WETLANDS WATER COURSE WETLAND FLAG FLOODWAY SETBACK LINE



# A. GENERAL NOTES

1. THESE DRAWINGS ARE INTENDED FOR REVIEW AND APPROVAL BY THE TOWN OF WILTON AND ARE NOT RELEASED FOR CONSTRUCTION.

- 2. TOPOGRAPHICAL, PROPERTY LINES, EXISTING SITE FEATURES, AND UTILITY INFORMATION TAKEN FROM PLAN ENTITLED "TOPOGRAPHIC SURVEY DEPICTING 141 DANBURY ROAD IN WILTON, CONNECTICUT, PREPARED FOR FDSPIN 141 DR LLC" BY D'ANDREA SURVEYING & ENGINEERING, P.C., DATED APRIL 19, 2021. INFORMATION ON EXISTING UTILITIES HAS BEEN COMPILED FROM AVAILABLE INFORMATION INCLUDING UTILITY COMPANY AND MUNICIPAL RECORD MAPS AND FIELD SURVEY AND IS NOT GUARANTEED CORRECT OR COMPLETE. UTILITIES ARE SHOWN TO ALERT THE CONTRACTOR TO THEIR PRESENCE. THE CONTRACTOR AND/OR RESPONSIBLE PARTY IS SOLELY RESPONSIBLE FOR DETERMINING ACTUAL LOCATIONS AND ELEVATIONS OF ALL UTILITIES INCLUDING SERVICES. PRIOR TO CONSTRUCTION, CONTACT "CALL BEFORE YOU DIG" AT 811 OR 1 800 922 4455 AND VERIFY ALL UNDERGROUND AND OVERHEAD UTILITY LOCATIONS.
- 3. IT IS THE DEVELOPER'S RESPONSIBILITY TO OBTAIN ALL NECESSARY PERMITS AND/OR EASEMENTS FROM STATE AND LOCAL AUTHORITIES AND ANY CONSTRUCTION RIGHTS AND/OR SLOPE RIGHTS AS MAY BE REQUIRED FROM THE PROPERTY OWNERS.
- 4. IT IS THE CONTRACTOR'S RESPONSIBILITY TO ASSURE THAT ALL PIPING IS PROPERLY BEDDED AND STABILIZED IN AREAS OF HIGH GROUND WATER AND/OR UNSTABLE SOIL CONDITIONS.
- 5. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH TOWN OF WILTON AND/OR CONNECTICUT DEPARTMENT OF TRANSPORTATION STANDARDS.
- 6. ANY DRAINAGE STRUCTURES, DITCHES, ASPHALT, CURBS, OTHER EXISTING CONSTRUCTION OR GRASSED AREAS DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO THE ORIGINAL CONDITION.
- 7. FIRE LANE MARKINGS SHALL BE STRIPED IN THE FIELD PER FIRE MARSHAL REVIEW AND DIRECTION IF REQUIRED.
- 8. VERTICAL DATUM IS NAVD88.

#### B. UTI LITY COORDINATION NOTES

- 1. UTILITY LOCATIONS SHOWN ARE APPROXIMATE AND ARE SUBJECT TO FINAL SITE SURVEY. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL ELEVATIONS, PROPERTY LINES, LOCATION OF UTILITIES AND SITE CONDITIONS IN THE FIELD. IF AN UNFORESEEN INTERFERENCE EXISTS BETWEEN AN EXISTING AND A PROPOSED STRUCTURE, THE CONTRACTOR SHALL NOTIFY THE DESIGN ENGINEER SO THAT THE APPROPRIATE REVISIONS CAN BE MADE.
- 2. IT IS THE RESPONSIBILITY OF EACH BIDDER IN EVALUATING THESE PLANS TO MAKE EXAMINATIONS IN THE FIELD BY VARIOUS METHODS AND OBTAIN NECESSARY INFORMATION FROM AVAILABLE RECORDS, UTILITY CORPORATIONS, AND INDIVIDUALS AS TO THE LOCATION OF ALL SUBSURFACE STRUCTURES.
- 3. THE CONTRACTOR IS TO USE CAUTION WHEN WORKING NEAR OR UNDER OVERHEAD AND UNDERGROUND UTILITIES. THE CONTRACTOR IS TO NOTIFY THE UTILITY COMPANIES OF HIS INTENT PRIOR TO THE COMMENCEMENT OF ANY WORK.
- 4. PLANTINGS SHALL NOT BE PLACED ON TOP OF UTILITIES.
- 5. ELECTRICAL CONDUIT SHALL BE INSTALLED BY AN ELECTRICIAN LICENSED IN THE STATE OF CONNECTICUT
- 6. CONTRACTOR SHALL COORDINATE THE EXACT LOCATION OF BUILDING UTILITY SERVICES AND RAIN WATER LEADER LOCATIONS WITH THE MECHANICAL, ELECTRICAL, PLUMBING, AND ARCHITECTURAL DRAWINGS.
- 7. FOR SITE LIGHTING DESIGN, SEE PROJECT LANDSCAPE ARCHITECTURAL DRAWINGS AND SPECIFICATIONS.

#### C. STORM SEWER NOTES

1. STORM SEWER LINES ARE TO BE INSTALLED USING INVERT ELEVATIONS, PIPE SLOPES SHOWN ARE APPROXIMATE AND ARE FOR REFERENCE ONLY.

- 2. APPLICABLE STORM SEWER CONSTRUCTION SHALL CONFORM TO TOWN OF WILTON REQUIREMENTS.
- 3. ROOF DRAINS ARE TO BE CONNECTED TO THE STORM DRAINAGE SYSTEM WHERE SHOWN.
- 4. THE ON-SITE DRAINAGE SYSTEM WILL REMAIN PRIVATE. THE PROPERTY OWNER IS TO PROVIDE REGULAR MAINTENANCE OF THE SYSTEM TO ALLOW IT TO CONTINUALLY FUNCTION AS INTENDED.
- 5. ALL PORTIONS OF THE STORM DRAINAGE SYSTEM ARE TO BE CAPABLE OF HANDLING AASHTO H-20 LOADS.
- 6. ALL REINFORCED CONCRETE PIPE SHALL BE CLASS IV UNLESS OTHERWISE NOTED.
- 7. ALL PVC PIPING TO BE CLASS SDR-35 UNLESS OTHERWISE NOTED. (SDR-21 REQUIRED FOR DEPTHS OVER 12 FEET.)
- 8. ALL CATCH BASINS SHALL HAVE BELL TRAPS EXCEPT IF CONNECTED IN A SERIES, IN WHICH CASE ONLY THE UPPER TWO CATCH BASINS IN THE SERIES SHALL HAVE BELL TRAPS.
- 9. HDPE PIPING SHALL CONFORM TO ASTM F2306.
- 10. THE INSTALLATION OF THE DRAINAGE SYSTEM IS TO BE DONE UNDER THE SUPERVISION OF THE DESIGN ENGINEER LICENSED IN THE STATE OF CONNECTICUT. AFTER CONSTRUCTION, THE ENGINEER IS TO SUBMIT TO THE TOWN OF WILTON WRITTEN CERTIFICATION THAT THE SYSTEM WAS INSTALLED AS PER THE APPROVED DESIGN. A DRAINAGE AS-BUILT DRAWING IS SUBMITTED WITH THIS LETTER TO THE TOWN OF WILTON. A REMINDER TO THE PROPERTY OWNER THAT THE SYSTEM WILL REMAIN PRIVATE AND THAT REGULAR MAINTENANCE WILL BE CRUCIAL TO ITS CONTINUED FUNCTIONING AS INTENDED. ADEQUATE ACCESS TO THE SYSTEM FOR MAINTENANCE PURPOSES IS TO BE PROVIDED.

#### D. SANITARY SEWER & WATER NOTES

- 1. SANITARY SEWER AND WATER LINE CROSSINGS SHALL MAINTAIN AN 18 INCH MINIMUM VERTICAL SEPARATION DISTANCE.
- 2. SEWER AND WATER LINE CROSSING ALL OTHER UTILITIES SHALL MAINTAIN A 12 INCH VERTICAL SEPARATION DISTANCE.
- 3. SANITARY SEWER LINES ARE TO BE INSTALLED USING INVERT ELEVATIONS. PIPE SLOPES SHOWN ARE APPROXIMATE AND ARE FOR REFERENCE ONLY.
- 4. PROPOSED SANITARY SEWER SERVICE IS TO MEET THE REQUIREMENTS OF THE TOWN OF WILTON.
- 5. PROPOSED WATER SERVICE IS TO MEET THE REQUIREMENTS OF THE STATE PLUMBING CODES AND AQUARION WATER COMPANY RULES AND REGULATIONS.

#### E. GRADING NOTES

- 1. AREAS OF DISTURBED EARTH SHALL BE STABILIZED BY MULCHING OR OTHER MEANS. SEEDING OF GRASSED AREAS SHALL BE INITIATED AS SOON AS PRACTICAL AS AN EROSION AND SILTATION CONTROL MEASURE.
- 2. RETAINING WALLS OVER 3' IN HEIGHT ARE TO BE DESIGNED AND CONSTRUCTED UNDER THE SUPERVISION OF A STATE OF CONNECTICUT LICENSED PROFESSIONAL ENGINEER OR ARCHITECT.
- 3. RETAINING WALLS REQUIRING AN ENGINEERED DESIGN SHALL BE SUBMITTED TO AND APPROVED BY THE TOWN OF WILTON WITH CALCULATIONS BEFORE CONSTRUCTION OF THESE WALLS BEGINS.
- 4. RETAINING WALLS ARE TO HAVE PROTECTIVE FENCING WHERE WARRANTED.
- 5. WHERE LEDGE IS TO BE LEFT IN PLACE, THE STABILITY OF THE LEDGE IS TO BE VERIFIED BY A QUALIFIED STATE OF CONNECTICUT LICENSED PROFESSIONAL ENGINEER OR SOIL SCIENTIST.
- 6. ALL LAND CLEARING AND CONSTRUCTION DEBRIS SHALL BE PROPERLY DISPOSED OF OFFSITE.
- 7. THE OWNER IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND/OR EASEMENTS FROM THE STATE OR LOCAL AUTHORITIES AND ANY CONSTRUCTION RIGHTS AS MAY BE REQUIRED FROM ADJOINING PROPERTY OWNER.
- 8. THE CONTRACTOR SHALL ADJUST THE TOP OF FRAME/GRATE ELEVATIONS OF ALL EXISTING AND PROPOSED SANITARY/STORM/WATER MANHOLES, CATCH BASINS, AREA DRAINS, VALVE COVERS AND APPURTENANCES, WITHIN THE PROJECT LIMITS TO MEET THE PROPOSED GRADES PRIOR TO CONSTRUCTION.

ABBREVIATIONS		ABBREVIATIONS CONT'D	
	ABANDON(ED)	N	NORTH
AC	ASBESTOS CEMENT PIPE		
BC	BITUMINOUS CURB		
BEP	BACK FLOW PREVENTOR	NIS	NOT TO SCALE
BIT	BITUMINOUS	N/A	NOT APPLICABLE
BI	BASELINE	N/F	NOW OR FORMERLY
	BUILDING	OC	ON CENTER
BND	BOUND	OCS	OUTLET CONTROL STRUCTURE
BOC	BOTTOM OF CURB	OH	OVERHEAD
BOT	BOTTOM	PB	PLANT BED
BS		PC	POINT OF CURVATURE
BW	BOTTOM OF WALL	PCC	POINT OF COMPOUND
			CURVATURE
CB		PCPP	PERFORATED CORRUGATED
CEM	CEMENT		POLYETHYLENE PIPE
CI		PERF	PERFORATED
		PI	POINT OF INTERSECTION
		PRC	POINT OF REVERSE CURVATURE
		PSF	POUNDS PER SQUARE FOOT
		PSI	POUNDS PER SQUARE INCH
CONC		PT	POINT OF TANGENCY
CPP		PVC	POLYVINYLCHLORIDE
		PVMT	PAVEMENT
CY	CUBIC YARD	R	RADIUS
DH	DRILL HOLE	RCP	REINFORCED CONCRETE PIPE
DI	DUCTILE IRON PIPE	RD	ROOF DRAIN
DIA	DIAMETER	REV	REVISION
	DRAIN MANHOLE	ROW	RIGHT OF WAY
E	EAST	RT	RIGHT
EF	EACH FACE	R&D	REMOVE AND DISPOSE
EG	EXISTING GRADE	R&R	REMOVE AND RESET
EL/ELEV	ELEVATION	R&S	REMOVE AND STACK
ELEC	ELECTRIC	S	SOUTH
EMH	ELECTRIC MANHOLE	SAN	SANITARY
EOP	EDGE OF PAVEMENT	SCH	SCHEDULE
EW	EACH WAY	SF	SQUARE FOOT
EXIST	EXISTING	SMH	SEWER MANHOLE
FES	FLARED END SECTION	SS	STAINLESS STEEL
	FINISH FLOOR	STA	STATION
FM	FORCE MAIN	STL	STEEL
G	GAS	STRM	STORM
GG	GAS GATE	Т	TANGENT LENGTH
GRAN	GRANITE	TC	TOP OF CURB
HC	HANDICAP	TEL	TEL-DATA
HDPE	HIGH DENSITY	TP	TEST PIT
	POLYETHYLENE	TS	TOP OF STEP
HMA	HOT MIX ASPHALT	TW	TOP OF WALL
HYD	HYDRANT	ТҮР	TYPICAL
IN	INCHES	UP	UTILITY POLE
INV	INVERT	W	WATER
IP	IRON PIN	WG	WATER GATE
L	LENGTH OF CURB	WV	WATER VALVE
LP	LIGHT POLE	XFMR	TRANSFORMER
LT	LEFT		
MAX	MAXIMUM		
MH	MANHOLE		
MIN	MINIMUM		
MISC	MISCELLANEOUS		
MON	MONUMENT		
MJ	MECHANICAL JOINT		



LOCATION MAP SCALE: 1" = 1000'

# 1000 Bridgeport Avenue Suite 320 Shelton, CT 06484 (203) 712-1100 B LANDSCAPE ELS ENVIRONMENTAL LAND SOLUTIONS, LL Landscape Architecture and Environmental Plannin 8 KNIGHT STREET, SUITE 203 NORWALK, CONNECTICUT 06851 Tel: (203) 855-7879 Fax: (203) 855-7836 info@elsllc.net www.elsllc.net TOWN SUBMI SSI ON 141 **D**anbu**r**y Roa**d FDSPIN** 141 DR, LLC Wilton, Connecticut MARK DATE DESCRIPTION PROJECT NO: F0173-002 DATE: 06/07/2021 F0173-02-C-001-INDX.dwg TIE DRAWN BY: MDS CHECKED: EWL APPROVED: JWB SITE INDEX, ABBREVIATIONS, NOTES AND LEGEND SCALE: AS SHOWN C-001



AREA AND BULK REQUIREMENTS				
	DE-5	DE-5R	EXISTING	PROPOSED
MIN FRONT YARD	100	75	80.1	80.1
MIN SIDE YARD (EACH)	50	50	49.4	50
MIN. REAR YARD	100	100	167.8	100.33
MIN. PARKING & LOADING SETBACKS (SIDE AND REAR YARDS)	25*	10	0	10
MAX. BUILDING HEIGHT (STORIES/FT)	4/55	4.5/55	2/30	4.5/55
MAX. BUILDING COVERAGE (%)	25%	35%	18.09%	33.21%
MAX. SITE COVERAGE (%)	50%	75%	63.28%	66.44%
MIN. LOT SIZE (ACRES)	5	4	4.28	4.28
MIN. LOT FRONTAGE	150	150	373.41'	373.41'













141 DANBURY ROAD IN WILTON, CONNECTICUT, PREPARED FOR FDSPIN 141 DR LLC" BY D'ANDREA SURVEYING & ENGINEERING, P.C., DATED APRIL 19, 2021, AND IS FOR



F0173-02-C-501-SESC.dwg MDS EWL JWB SOIL EROSION AND SEDIMENT CONTROL PLAN FINAL PHASE 1" = 30'

F0173-002

06/07/2021

THE STORMWATER MANAGEMENT MEASURES WILL ADDRESS THE STORMWATER OUALITY ONCE THE SITE HAS	JUL ENULTION AND SEDIMENT CONTROL MEASURES SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE
BEEN CONSTRUCTED AND STABILIZED. SEDIMENTATION AND EROSION CONTROL MEASURES WILL BE INSTALLED DURING CONSTRUCTION WHICH WILL MINIMIZE ADVERSE IMPACTS FROM CONSTRUCTION ACTIVITIES.	D STANDARDS AND SPECIFICATIONS OF THE "2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL", DEP BULLETIN NO. 34, AND ALL AMENDMENTS AND ADDENDA THERETO AS PUBLISHED BY THE CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION.
ALL SEDIMENTATION AND EROSION CONTROL MEASURES PROPOSED FOR THIS DEVELOPMENT HAVE BEEN DESIGNED IN ACCORDANCE WITH THE "2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENTATION CONTROL " AS PUBLISHED BY THE CONNECTICUT COUNCIL ON SOIL EROSION AND WATER CONSERVATION	ON 2. LAND DISTURBANCE SHALL BE KEPT TO THE MINIMUM NECESSARY FOR CONSTRUCTION OPERATIONS.
ADDITIONAL GUIDELINES HAVE ALSO BEEN FOLLOWED THAT ARE AVAILABLE FROM THE CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION AS RECOMMENDED FOR SEDIMENTATION CONTROL DURING CONSTRUCTION ACTIVITIES.	3. ALL EROSION CONTROL MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLAN AND ELSEWHERE AS ORDERED BY THE ENGINEER.
LISTED BELOW ARE THE EROSION CONTROL NARRATIVE AND THE EROSION CONTROL NOTES.	<ol> <li>ALL CATCH BASINS SHALL BE PROTECTED WITH A SILT SACKS, HAYBALE RING, SILT FENCE OR BLOCK AND STONE INLET PROTECTION THROUGHOUT THE CONSTRUCTION PERIOD AND UNTIL ALL DISTURBED AREAS ARE THOROUGHLY STABILIZED.</li> </ol>
SOIL EROSION AND SEDIMENT CONTROL NARRATIVE:	5. WHENEVER POSSIBLE, EROSION AND SEDIMENT CONTROL MEASURES SHALL BE INSTALLED PRIOR TO
<u>GENERAL</u>	CONSTRUCTION. SEE "EROSION CONTROL NARRATIVE".
1. THE PROPOSED DEVELOPMENT IS ENTITLED 141 DANBURY ROAD, WILTON, CONNECTICUT.	<ol> <li>ADDITIONAL CONTROL MEASURES SHALL BE INSTALLED DURING THE CONSTRUCTION PERIOD AS ORDERED BY TH ENGINEER.</li> </ol>
PROJECT START: FALL 2021 PROJECT COMPLETION: SPRING 2022	7. ALL SEDIMENTATION AND EROSION CONTROL MEASURES SHALL BE MAINTAINED IN EFFECTIVE CONDITION THROUGHOUT THE CONSTRUCTION PERIOD.
B. EROSION CONTROL NARRATIVE REFERS TO DRAWINGS C-501 THROUGH C-504.	8. SEDIMENT REMOVED SHALL BE DISPOSED OF OFF SITE OR IN A MANNER AS REQUIRED BY THE ENGINEER.
<ol> <li>THE PROPOSED SITE DEVELOPMENT WILL CONSIST OF BUILDING DEMOLITION, CLEARING AND GRUBBING THE EXISTING SITE, EXCAVATION, CONSTRUCTION OF SEDIMENTATION/DETENTION BASINS, AND ROUGH GRADING OF BUILDING, PARKING AREAS, SIDEWALKS AND CURBING.</li> </ol>	9. THE CONSTRUCTION CONTRACTOR SHALL BE RESPONSIBLE FOR CONSTRUCTION AND MAINTENANCE OF ALL CONTROL MEASURES THROUGHOUT THE CONSTRUCTION PERIOD.
. THE DEVELOPMENT IS LOCATED IN WILTON, CONNECTICUT AND IS LOCATED ON DANBURY ROAD.	10. ALL DISTURBED AREAS TO BE LEFT EXPOSED FOR MORE THAN 30 DAYS SHALL BE PROTECTED WITH A TEMPORARY VEGETATIVE COVER. SEED THESE AREAS WITH PERENNIAL RYEGRASS AT THE RATE OF 40 LBS. PER ACRE (1 LB. PER 1,000 SQ. FT). APPLY SOIL AMENDMENTS AND MULCH AS REQUIRED TO ESTABLISH A UNIFORM STAND OF VEGETATION OVER ALL DISTURBED AREAS.
CONDUCT A DRE CONSTRUCTION MEETING WITH THE OWNER OF OWNER PERFORMANCE TO THE	11. THE CONSTRUCTION CONTRACTOR SHALL UTILIZE APPROVED METHODS/MATERIALS FOR PREVENTING THE
. CONDUCT A PRE-CONSTRUCTION MEETING WITH THE OWNER OR OWNER'S REPRESENTATIVE, TOWN PLANNER, DESIGN ENGINEER, SITE ENGINEER, CONTRACTOR AND SITE SUPERINTENDENT TO ESTABLISH TH LIMITS OF CONSTRUCTION, CONSTRUCTION PROCEDURES AND MATERIAL STOCKPILE AREAS.	HE BLOWING AND MOVEMENT OF DUST FROM EXPOSED SOIL SURFACES ONTO ADJACENT PROPERTIES AND SITE AREAS.
2. FIELD STAKE THE LIMITS OF CONSTRUCTION.	12. THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A SUPPLY OF SILT FENCE/HAYBALES AND ANTI-TRACKING CRUSHED STONE ON SITE FOR EMERGENCY REPAIRS.
<ol> <li>INSTALL ALL APPLICABLE SOIL AND EROSION CONTROL MEASURES AROUND THE PERIMETER OF THE SITE T THE EXTENT POSSIBLE. THIS WILL INCLUDE SILTATION FENCE AROUND THE PROJECT AS SHOWN ON THE PLANS.</li> </ol>	13. ALL DRAINAGE STRUCTURES SHALL BE PERIODICALLY INSPECTED WEEKLY BY THE CONSTRUCTION CONTRACTOR AND CLEANED TO PREVENT THE BUILD-UP OF SILT.
4. INSTALL CONSTRUCTION ACCESS ROAD AND ANTI-TRACKING PAVEMENT IN THE AREAS AS SHOWN ON THE PLANS. ALL CONSTRUCTION ACCESS SHALL BE INTO THE SITE THROUGH THE ANTI-TRACKING PADS.	14. THE CONSTRUCTION CONTRACTOR SHALL CAREFULLY COORDINATE THE PLACEMENT OF EROSION CONTROL MEASURES WITH THE PHASING OF CONSTRUCTION.
5. ESTABLISH TEMPORARY STAGING AREA.	15. KEEP ALL PAVED SURFACES CLEAN. SWEEP AND SCRAPE BEFORE FORECASTED STORMS.
5. BEGIN BUILDING DEMOLITION AND PAVEMENT REMOVAL.	16. TREAT ALL UNPAVED SURFACE WITH 4" MINIMUM OF TOPSOIL PRIOR TO FINAL STABILIZATION.
7. CONSTRUCT THE INITIAL STORM DRAINAGE AND SEDIMENTATION TRAP AS SHOWN ON THE PLANS.	17. HAYBALE BARRIERS AND SILT FENCING SHALL BE INSTALLED ALONG THE TOE OF CRITICAL CUT AND FILL SLOPES.
<ol> <li>INSTALL WATER QUALITY SYSTEMS AND ASSOCIATED DRAINAGE NETWORK TO THE MAXIMUM EXTENT PRACTICABLE, GRADE THE AREA AROUND THE STORM DRAINAGE SYSTEM AS NECESSARY.</li> </ol>	18. THE CONTRACTOR SHALL NOTIFY THE TOWN OFFICIALS PRIOR TO THE INSTALLATION OF EROSION CONTROLS, CUTTING OF TREES, OR ANY EXCAVATION.
BEGIN ROUGH ROADWAY GRADING.	19. ALL TRUCKS LEAVING THE SITE MUST BE COVERED.
10. INSTALL REMAINING DRAINAGE SYSTEM TO THE EXTENT NECESSARY TO PROVIDE POSITIVE DRAINAGE.	20. SOME CONTROL MEASURES ARE PERMANENT. THESE STRUCTURES SHALL BE CLEANED AND REPLENISHED AT THE END OF CONSTRUCTION LOCATIONS OF THE PERMANENT CONTROL STRUCTURES ARE SHOWN ON THE DRAINAGE
1. BEGIN INSTALLATION OF SANITARY SEWER SYSTEM, WATER AND OTHER UTILITIES TO EXTENT NECESSARY	PLANS.
2. PROVIDE SILT FENCE/HAYBALE BARRIER AROUND SOIL STOCKPILE AREA. PROVIDE TEMPORARY VEGETATIN COVER (DEFINED IN EROSION CONTROL NOTES) ON ALL EXPOSED SURFACES.	VE 21. ALL SEDIMENTATION AND EROSION CONTROLS SHALL BE CHECKED WEEKLY AND/OR AFTER EACH RAIN FALL EVEN NECESSARY REPAIRS SHALL BE MADE WITHOUT DELAY.
.3. BEGIN BUILDING CONSTRUCTION.	22. PRIOR TO ANY FORECASTED RAINFALL, EROSION AND SEDIMENT CONTROLS SHALL BE INSPECTED AND REPAIRED AS NECESSARY.
4. PAVE BINDER COURSE ON PARKING AND DRIVEWAYS FOR NON-POROUS PAVEMENT AREAS.	23. AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, EROSION CONTROLS MAY BE REMOVED ONCE
5. ESTABLISH TEMPORARY VEGETATIVE COVER.	AUTHORIZATION TO DO SO HAS BEEN SECURED FROM THE OWNER. DISTURBED AREAS SHALL BE SEEDED AND MULCHED.
.6. CONSTRUCT DRAINAGE AND SUBBASE FOR POROUS PAVEMENT AND THEN PLACE PAVEMENT COURSE	24. ALL EMBANKMENT SLOPES 3:1 OR GREATER TO BE STABILIZED WITH EROSION CONTROL BLANKET, NORTH AMERICAN GREEN SC150BN OR APPROVED EQUIVALENT, UNLESS OTHERWISE NOTED ON PLANS.
CONSTRUCTION SEQUENCE - FINAL PHASE	
1. REPAIR PERIMETER SEDIMENT & EROSION CONTROLS AS NEEDED.	
2. CLEAN/REPLACE CONTROLS FROM PREVIOUS PHASE AS NEEDED.	
3. FINE GRADE SITE.	RADIUS TO ACCOMMODATE – TURNING MOVEMENTS
4. CONTINUE CONSTRUCTION OF BUILDING.	OF CONSTRUCTION VEHICLES, AS NEEDED.
5. COMPLETE CONSTRUCTION OF SIDEWALKS.	
6. ESTABLISH FINAL VEGETATIVE COVER AND LANDSCAPING.	TO WORK AREA
7. PAVE SURFACE COURSE ON ROADWAYS.	
3. REMOVE EROSION CONTROLS WHEN SITE IS STABILIZED.	CONSTRUCTION ENTRANCE
SILT FENCE	50' MIN. (100' MIN IF TRACKED SEDIMENT < 80% SAND)
	└─ MINIMUM 12' OR WIDTH OF ACCESS ROAD





INLET PROTECTION THROUGHOUT THE CONSTRUCTION PERIOD AI THOROUGHLY STABILIZED.	ND UNTIL ALL DISTURBED AREAS ARE	
WHENEVER POSSIBLE, EROSION AND SEDIMENT CONTROL MEASU CONSTRUCTION. SEE "EROSION CONTROL NARRATIVE".	IRES SHALL BE INSTALLED PRIOR TO	
ADDITIONAL CONTROL MEASURES SHALL BE INSTALLED DURING <sup>-</sup> ENGINEER.	THE CONSTRUCTION PERIOD AS ORDERED BY THE	E 2 STAKES UNPAVED
ALL SEDIMENTATION AND EROSION CONTROL MEASURES SHALL E THROUGHOUT THE CONSTRUCTION PERIOD.	BE MAINTAINED IN EFFECTIVE CONDITION	
SEDIMENT REMOVED SHALL BE DISPOSED OF OFF SITE OR IN A M	ANNER AS REQUIRED BY THE ENGINEER.	
THE CONSTRUCTION CONTRACTOR SHALL BE RESPONSIBLE FOR C CONTROL MEASURES THROUGHOUT THE CONSTRUCTION PERIOD.	CONSTRUCTION AND MAINTENANCE OF ALL	
ALL DISTURBED AREAS TO BE LEFT EXPOSED FOR MORE THAN 30 VEGETATIVE COVER. SEED THESE AREAS WITH PERENNIAL RYEG PER 1,000 SQ. FT). APPLY SOIL AMENDMENTS AND MULCH AS REC VEGETATION OVER ALL DISTURBED AREAS.	DAYS SHALL BE PROTECTED WITH A TEMPORARY RASS AT THE RATE OF 40 LBS. PER ACRE (1 LB. QUIRED TO ESTABLISH A UNIFORM STAND OF	
THE CONSTRUCTION CONTRACTOR SHALL UTILIZE APPROVED MET BLOWING AND MOVEMENT OF DUST FROM EXPOSED SOIL SURFAC AREAS.	THODS/MATERIALS FOR PREVENTING THE CES ONTO ADJACENT PROPERTIES AND SITE	
THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A SUPPLY OF CRUSHED STONE ON SITE FOR EMERGENCY REPAIRS.	SILT FENCE/HAYBALES AND ANTI-TRACKING	
ALL DRAINAGE STRUCTURES SHALL BE PERIODICALLY INSPECTED AND CLEANED TO PREVENT THE BUILD-UP OF SILT.	WEEKLY BY THE CONSTRUCTION CONTRACTOR	
THE CONSTRUCTION CONTRACTOR SHALL CAREFULLY COORDINAT MEASURES WITH THE PHASING OF CONSTRUCTION.	TE THE PLACEMENT OF EROSION CONTROL	DUM
KEEP ALL PAVED SURFACES CLEAN. SWEEP AND SCRAPE BEFORE	FORECASTED STORMS.	1" I REMOV
TREAT ALL UNPAVED SURFACE WITH 4" MINIMUM OF TOPSOIL PRI	OR TO FINAL STABILIZATION.	
HAYBALE BARRIERS AND SILT FENCING SHALL BE INSTALLED ALO	NG THE TOE OF CRITICAL CUT AND FILL SLOPES.	
THE CONTRACTOR SHALL NOTIFY THE TOWN OFFICIALS PRIOR TO CUTTING OF TREES, OR ANY EXCAVATION.	THE INSTALLATION OF EROSION CONTROLS,	
ALL TRUCKS LEAVING THE SITE MUST BE COVERED.		
SOME CONTROL MEASURES ARE PERMANENT. THESE STRUCTURES END OF CONSTRUCTION. LOCATIONS OF THE PERMANENT CONTROPLANS.	S SHALL BE CLEANED AND REPLENISHED AT THE DL STRUCTURES ARE SHOWN ON THE DRAINAGE	
ALL SEDIMENTATION AND EROSION CONTROLS SHALL BE CHECKE NECESSARY REPAIRS SHALL BE MADE WITHOUT DELAY.	D WEEKLY AND/OR AFTER EACH RAIN FALL EVEN	т.
PRIOR TO ANY FORECASTED RAINFALL, EROSION AND SEDIMENT ( AS NECESSARY.	CONTROLS SHALL BE INSPECTED AND REPAIRED	
AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, EROSION AUTHORIZATION TO DO SO HAS BEEN SECURED FROM THE OWNE MULCHED.	CONTROLS MAY BE REMOVED ONCE R. DISTURBED AREAS SHALL BE SEEDED AND	
ALL EMBANKMENT SLOPES 3:1 OR GREATER TO BE STABILIZED W	ITH EROSION CONTROL BLANKET, NORTH	
AMERICAN GREEN SC150BN OR APPROVED EQUIVALENT, UNLESS	OTHERWISE NOTED ON PLANS.	
RADIUS TO ACCOMMODATE – TURNING MOVEMENTS		
OF CONSTRUCTION VEHICLES, AS NEEDED.		
ACCESS ROAD		- 1-1/2" SQ. HARDWOOD S
TO WORK AREA		WEIGHT5 LBS/FT (MIN
	OAD	
CONSTRUCTION     ENTRANCE	ED RC	
	PAV	
50' MIN.		
SEDIMENT < 80% SAND)		
MINIMUM 12' OR WIDTH OF ACCESS ROAD		
WHICHEVER IS GREATER		
<u>PLAN</u>		
6" CRUSHED STONE CTDOT GRADING NO	). 3	FILTER FABRIC, GEOT
	PAVED ROAD	TUCK 6" BELOW GRAD
		SILT FENCE INSTALLATION AT
GEOTEXTILE, MIR	AFI 600X OR APPROVED EQUAL	CATCH BASIN AT LOW POINTS
(REMOVE TOPSOII	L AND ORGANICS)	CAT
ELEVATION		
CONSTRUCTION ENTRA NO SCALE	ANCE	









3. WEDGE LOOSE STRAW BETWEEN BALES TO CREATE A CONTINUOUS BARRIER





4. BACKFILL AND COMPACT EXCAVATED SOIL ON THE UPHILL SIDE OF THE BARRIER TO PREVENT PIPING

# PLACEMENT AND CONSTRUCTION OF HAYBALE BARRIER NO SCALE





NOTES:

- 1. PERFORATIONS SHALL BE CIRCULAR OR SLOTS, NOT TO EXCEED 1/2" DIAMETER.
- 2. SIDE SLOPES TO MEET OSHA TRENCHING REQUIREMENTS.

SUMP PIT DETAIL (IF REQUIRED) NO SCALE








NOTES:

- 1. SIGN LOCATED AT ALL HANDICAPPED PARKING SPACES.
- 2. 18' X 15' D.O.T STANDARD ACCESSIBLE PARKING STALL
- 3. SIGN BACKGROUND BLUE REFLECTIVE
- 4. LETTERS, GRAPHICS & BORDER WHITE REFLECTIVE

ACCESSIBLE PARKING STRIPING DETAILS

NO SCALE





















	CHECKMATE VALVE								
NOMINAL OVERALL PIPE SIZE I.D. LENGTH		NUMBER OF CLAMPS	CUFF DEPTH		BACK PRESSURE RATING				
Inches	Millimeters	Inches	Millimeters		Inches	Millimeters	Feet	Meters	
12	300	23	584	1	2	51	40	12	
14	350	25.75	654	1	4	102	20	6	
16	400	28.61	727	1	4	102	20	6	
18	450	31	787	1	4	102	20	6	
20	500	42.14	1070	2	8	203	20	6	
24	600	47.5	1207	2	8	203	20	6	

### CHECKMATE<sup>®</sup> IN LINE CHECK VALVE DETAIL NO SCALE





NO SCALE





1'-8"







TYPE "C" CATCH BASIN

VARY CROSS SLOPE OF GUTTER TO MATCH CROSS SLOPE OF GRADE



TYPE "C-L" CATCH BASIN NO SCALE

1. REINFORCEMENT SHALL CONFORM TO ASTM A615, GRADE 60.

2. DETAILS ON THIS SHEET SHOW STANDARD REINFORCEMENT. WELDED WIRE FABRIC WITH AN AREA EQUAL TO OR GREATER THAN THE REINFORCING SHOWN MAY BE SUBSTITUTED.

3. ALL LAP SPLICES, DEVELOPMENT LENGTHS, BENDS FOR REINFORCEMENT, AND WELDED WIRE FABRIC SHALL CONFORM TO AASHTO STANDARD SPECIFICATIONS FOR HIGHWAY BRIDGES.

4. ALL REINFORCEMENT SHALL HAVE A MINIMUM CLEAR COVER OF 2", EXCEPT FOR BENEATH BOTTOM REINFORCEMENT IN TOP SLABS, WHERE THE MINIMUM MAY BE  $1\frac{1}{2}$ "

5. MINIMUM CONCRETE COMPRESSIVE STRENGTH FC'=4,000PSI SHALL BE OBTAINED BEFORE SHIPPING.

6. BASES AND RISERS AT A DEPTH OF 20' AND GREATER SHALL BE DESIGNED BY THE CONTRACTOR AND WORKING DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW.

7. SEE STANDARD DRAWING 507-K FOR CATCH BASIN FRAMES AND GRATES.

8. FOR DOT MAINTENANCE PERSONNEL, RISERS MAY BE PREFABRICATED WITH PIPE OPENINGS IN ALL FOUR WALLS. ADEQUATE REINFORCING AROUND PIPE OPENINGS TO CONFORMING TO THESE PLANS SHALL BE PROVIDED. ANY RISERS USED WHERE A PIPE OPENING IS TO REMAIN IN PLACE MUST BE FORMED UP WITH BRICK AS DIRECTED BY THE ENGINEER.

9. RISERS SHALL NEVER HAVE CORNER PIPE ENTRIES. WHERE THE ALIGNMENT OF THE PIPE WITH RESPECT TO THE CORNER OF THE CATCH BASIN CANNOT BE CHANGED, A ROUND STRUCTURE CONFORMING TO ASTM C478 SHALL BE USED. REINFORCING FOR THE ROUND TOP SLAB WITH A RECTANGULAR OPENING SHALL CONFORM TO DETAILS SHOWN HERE.

10. ALL PIPE OPENINGS SHALL BE CLOSED USING MATERIALS WHICH CONFORM TO STATE OF CONNECTICUT STANDARD SPECIFICATIONS SECTION M.08.02. IF THE ENGINEER DETERMINES THAT THE CLOSURE OF ANY PIPE OPENING IS UNSATISFACTORY, THE CONTRACTOR SHALL RECLOSE SAID OPENING AT NO ADDITIONAL COST TO THE STATE. KNOCKOUTS FOR PIPE OPENINGS SHALL NOT RESULT IN A REDUCED

11. THE LATEST STATE OF CONNECTICUT STANDARD SPECIFICATIONS AND SUPPLEMENTALS SHALL GOVERN.

13. WALL THICKNESS OF ALL CB'S OVER 10' DEEP SHALL BE INCREASED TO 12" THICK. INSIDE DIMENSION SHALL REMAIN THE SAME. (THE 12" THICKNESS SHALL START AFTER THE FIRST 10")

14. BUTYL RUBBER JOINT SEAL SHALL CONFORM TO AASHTO M-198 AND MORTAR SHALL CONFORM TO THE LATEST STATE OF CONNECTICUT STANDARD SPECIFICATIONS MATERIAL SECTION M11.04.

15. SHRINKAGE AND TEMPERATURE REINFORCEMENT SHALL BE PROVIDED IN THE TOPS OF SLABS. THE TOTAL AREA OF REINFORCEMENT PROVIDED SHALL BE AT LEAST 0.125 IN<sup>2</sup>/FT IN EACH DIRECTION. THE MAXIMUM SPACING OF THIS REINFORCEMENT SHALL NOT EXCEED 18 INCHES.

16. THE DETAILS SHOWN IN THE PLAN VIEW FOR THE PRECAST CONCRETE ROUND STRUCTURES SHALL ALSO BE USED FOR CONVERTING MANHOLES TO CATCH BASINS.

















* IN DI TO O 2" TO	STURBED GRASS ARE RIGINAL CONDITION V PSOIL (MIN.) OR	EAS, RESTORE WITH:	HODI
SOD	(LIVE SOD ON 4" TOP:	SOIL BED)	PAYN
		S F	SEE PAVEMENT - REPAIR DETAILS
			-
		12' BA	' MIN. PROCESSE SE OR ROLLED (
	LIMIT OF AD REPLACE EX	DITIONAL BACKFIL XCAVATED ROCK O	L MATERIAL TO · R TO BACKFILL
		VERTICAL LINE IN R	LIMIT OF PAYME
		NO RC 6" FRO	OCK SHALL BE CL M OUTSIDE OF P
REFER TO TH FOR TEMPOR PAVEMENT F	HE STANDARD DETAILS RARY AND PERMANENT REPAIR	LIMIT OF BED TO REPLACE	DING MATERIAL EXCAVATED RO
HORIZONTA FOR TEMPO ROCK, BED ADDITIONA	AL PAYMENT LIMITS DRARY PAVEMENT, DING MATERIAL & L BACKFILL MATERIAL	VER LINE	TICAL LIMIT OF P IN ROCK 6" BELC
PIPE SIZE	TRENCH WIDTH		
6"	4'-0"		
8"	4'-0"		
12"	4'-0"		
16"	4'-0"		
20"	5'-0"		
24"	5'-0"		
30"	6'-0"		
36"	6'-0"		
DTE: IF TREI ADD 2'	NCH BOXES ARE USE TO ALL TRENCH WIDT	D THS	
	AQUA	RION	TYPIC
Ster	wards of the Envi	ronment	NOT TO SO

UARION Water Company	GATE VALVE	
he Environment	NOT TO SCALE	SD-2







INSTALLATION IN TRENCH – All direct-buried cables shall be installed at a depth of at least 30 inches in the

- following order: 1. Ensure that the bottom of the trench is well-tamped and free of rocks.
- 2. Install the conduit, gluing all couplings. 3. Install secondaries and other utility cables or conduits in the trench.
- 4. Backfill with 12 inches clean fill not to contain stones larger than 2 inches in maximum diameter.
- 5. Install cable warning tape 12 inches over the conduit.
- 6. Fill in the remainder of the trench with native backfill.





**CROSS SECTION OF JOINT TRENCH** 

The trench shall be backfilled immediately following placement of the conduit.
 1/4–inch–diameter nylon pull line and plastic conduit plugs to be supplied and installed by contractor.

ORIGINAL	SINGLE-F	PHASE PRIMARY CABLE INSTALL	ATION (C)	
6/24/98	I	DIRECT-BURIED - IN CONDUIT	C	
12/18/00	NORTHEAST UTILITIES	CONSTRUCTION STANDARD	DTR 50.103	3









NO 1.	TES: ALL EX AND IN OVER T EXECU
2.	PRIOR OF 4″ (
3.	SAND I COMPA
4.	BACKF MATER SHALL
5.	ALL GA
6.	ALL GA REQUII

1. To inspect, provide access, operate elbow connectors and ventilate the transformer, the above specified clear area distances to buildings or shrubs shall be maintained. The distance from the building is to the concrete transformer pad. Property line shall be considered an obstruction, since fences, shrubs, etc. may be installed at a future date by adjacent property owners. Because of the possibility of cooling fins overhanging the pad, side clearances to be increased to 5 feet for transformers 1000 kVA and larger.

2. If no curb exists, or transformer is located closer than 10 feet to the traveled way, protective vehicle posts () shall be installed as specified in DTR 42.061. 3. Top of transformer pad shall be installed 3 inches above final grade. 4. Transformer shall not be located on steep grades where access to or elbow operation is made difficult.

5. Transformer shall meet the minimum distances to doors, windows, fire escapes, air intakes and walls as specified in DTR 42.061. 6. Transformer *is not* to be located with its doors facing the building.

Refer to DTR 58.301 for specific instructions on the installation of the transformer pad.
 Refer to DSEM Section 06.32 for information on environmental considerations.

L	P	AD-MOUNTED TRANSFORMERS		
D	LOCAT	ION TO BUILDINGS AND ROADW	AYS	
	NORTHEAST UTILITIES	CONSTRUCTION STANDARD	DTR 42.047	6



AGGREGATE 1. "BEDDING MATERIAL

XCAVATION WORK WILL BE IN ACCORDANCE WITH THE DIRECTION OF THE COMPANY IN COMPLIANCE WITH THE REGULATIONS OF THE AUTHORITIES HAVING JURISDICTION THE STREETS, ALLEYS, RIGHT-OF-WAYS, OR PROPERTIES WHERE THE WORK IS TO BE JTED.

R TO THE INSTALLATION OF THE PIPE, SAND PADDING SHALL BE INSTALLED, A MINIMUM (MEASURED AFTER COMPACTION.)

PADDING ABOVE THE GAS PIPE SHALL BE A MINIMUM OF 6" (MEASURED AFTER ACTION).

FILL SHALL BE FREE OF LARGE STONES (6" DIAMETER) WITHIN 1' OF THE PIPE. IF THE RIAL REMOVED FROM THE TRENCH IS NOT SUITABLE FOR BACKFILL, REPLACEMENT FILL BE USED.

AS SERVICE INSTALLATIONS SHALL BE COORDINATED WITH EVERSOURCE.

AS SERVICES SHALL BE INSTALLED ACCORDING TO EVERSOURCE STANDARDS AND IREMENTS.

> GAS SERVICE TRENCH NO SCALE





141 Danbury Road Wilton, Connecticut

# **ENGINEERING REPORT**

Prepared For:

FDSPIN 141 DR, LLC 1 North Water Street, Suite 100 South Norwalk, CT 06854

June 7, 2021





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# Section 1 Introduction and Site Conditions

Tighe & Bond has prepared this report at the request of FDSPIN 141 DR LLC ( "Applicant"), to support their applications to the Town of Wilton Planning & Zoning Commission and Inlands Wetlands Commission for a proposed 4½ story multi-family residential building with 173 apartments.

The project site is located on a 4.28-acre parcel bounded by Danbury Road to the east, the Norwalk River to the west, and commercial properties to the north and south. The proposed development consists of the construction of a 173-unit residential building, atgrade parking, stormwater management systems, utility services, lighting, and associated landscaping. Refer to **Figure 1**, Site Location Map, in **Appendix A**.

Tighe & Bond has inspected the property and analyzed available soils, drainage, utility, wetland, and topographic information. Drainage calculations and stormwater management design have been prepared in accordance with the 2000 Connecticut Department of Transportation (CTDOT) Drainage Manual, and the Connecticut Department of Energy and Environmental (DEEP) Protection 2004 Stormwater Quality Manual. The drainage calculations include a hydrologic and hydraulic analysis of the existing conditions and the proposed development. Specifically, the calculations include an analysis of the on-site stormwater management measures and their performance in handling peak flow attenuation and pollutant removals. The report also includes a summary of the site floodplain management, the available existing and proposed utilities to serve the property, and the proposed soil erosion and sedimentation control measures incorporated during construction.

### **1.1 Existing Conditions**

The existing site consists of a 47,000 square foot commercial building with at-grade parking. The 4.28-acre parcel is located within Wilton's DE-5 Design Enterprise District Zone. A significant portion of the site is impervious with paved parking areas, sidewalks, and building, with landscaping and lawns generally around the perimeter of the site. Utility services to the site include underground water, natural gas, overhead electric, and tele-data, connecting to service mains in Danbury Road.

The site is located on Danbury Road (Route 7) which is a north-south three lane State maintained major arterial roadway. The roadway is generally 40 feet wide along the frontage of the site with two lanes northbound and one lane southbound.

The topography of the site generally slopes from east to west towards the Norwalk River. Due to the lack of drainage structures within the property, stormwater runoff flows overland across the paved and landscaped surfaces. The Norwalk River runs adjacent to the western edge of the property, flowing from north to south. Approximately one third of the property lies within the Special Flood Hazard Zone AE of the Norwalk River.

### 1.2 Project Proposal

The proposed  $4\frac{1}{2}$  story multi-family residential building will be home to 173 apartments consisting of one-bedroom (40), one bedroom & den (4), two-bedroom (107), two

bedroom & den (7), and three-bedroom (15) units. The proposed building is situated in the central portion of the site, with driveway and parking areas along the northern and southern sides. The ground floor will include surface parking spaces (covered and uncovered) as well as utility/trash rooms and building access points. All uncovered parking will be screened from view by landscaping. The existing driveway into the property will be widened to accommodate the traffic to and from the site, with dedicated turning lanes onto Danbury Road. The western end of the property will be converted into green space with associated landscaping and walking paths along the Norwalk River. New utility services to the property are proposed including underground water, natural gas, electric, and tele-data.

Stormwater management will be accommodated on-site. Surface runoff will be collected in catch basins and inlet structures located throughout the site. Underground infiltration and porous pavement systems have been designed to reduce peak flows and provide stormwater treatment, prior to discharge into the Norwalk River. The stormwater management system has been designed to treat the water quality volume and remove a high level of pollutants.

### 1.3 Site Soils

The U.S. Department of Agriculture's National Resource Conservation Service (NRCS) Web Soil Survey indicates the following soil types are present on the site:

**Urban Land (307):** Urban land is mostly covered by streets, parking lots, buildings, and other structures of urban areas. Slopes range from 0 to 45 percent. No drainage class is assigned, and the complex does not meet hydric criteria.

**Rippowam Fine Sandy Loam (103):** This series consist of very deep, poorly drained loamy soils formed in alluvial sediments. They are nearly level soils on flood plains subject to frequent flooding. Slope ranges from 0 to 3 percent.

A copy of the NRCS Soil Resource Report is included in **Appendix B** of this report.

Soil permeability for the site was estimated to be 2 inches per hour for the design of the proposed stormwater management systems. Estimates were conservative based on the soil classifications observed in the soil exploration program previously performed on site by GZA Environmental, LLC. Permeability estimates will be confirmed in the field prior to the completion of construction documents. See **Appendix B** of this report for boring logs and observed groundwater elevations.

### 1.4 Wetlands

Wetlands soils were delineated and flagged by William Kenny Associates LLC, William L. Kenny, soil scientist on March 15, 2021 and located in the field by D'Andrea Surveying & Engineering, P.C. Wetland flags and limits are depicted on the project drawing sheets.

# Section 2 Stormwater Management

### 2.1 Existing Site Hydrologic Analysis

To review the impact of the proposed development on the existing site, an existing conditions hydrologic analysis was performed. Under existing conditions, stormwater runoff from the site generally flows from east to west towards the Norwalk River. Since there are no catch basins or inlet structures on the existing site, runoff flows overland and discharges to the river at the western end of the site. The edge of the river along the property has been designated as the design point for the analysis. The drainage area of the existing site has been delineated into sub-watershed areas. The Existing Conditions Watershed Map (Figure WM-01) is included in **Appendix C** of this report.

Impervious and pervious areas, weighted curve number, and time of concentration were calculated for each watershed area and developed into hydrologic model to determine the project's peak flow and volume, as part of the comparative hydrology analysis. Precipitation data for the hydrologic modeling were developed from NOAA's Atlas 14 Point Precipitation Frequency Estimates online utility. The site specific precipitation depths for a 24-hour durations storm are shown in **Table 2-1**.

# Table 2-124-hour Duration Precipitation Depth

	2-Year	10-Year	25-Year	50-Year	100-Year
Depth (in)	3.54	5.40	6.57	7.44	8.37

A breakdown of existing watershed areas, existing volumetric hydrographs, and existing watershed map are included in **Appendix C** of this report.

### 2.1.1 Floodplain Management

The Federal Emergency Management Agency's Flood Insurance Rate Map (FIRM) for Fairfield County, effective June 18, 2010 and revised October 16, 2013 shows a portion of the site within the floodway and Zone AE of the Norwalk River, as shown in **Figure 2** in **Appendix A**. Refer to **Section 3 Floodplain Management & Hydraulics** of this report for additional information.

### 2.2 Proposed Site Hydrologic and Hydraulic Analysis

A stormwater management system has been designed for the proposed development to reduce peak flows and improve water quality for the site. The proposed drainage system consists of catch basins and inlets throughout the development site as well as water quality structures, underground infiltration systems, porous pavement systems, and outlet protection. The stormwater management system will maintain existing drainage patterns and utilize Best Management Practices for stormwater treatment.

Under proposed conditions, drainage patterns will generally remain the same, flowing in a westerly direction and ultimately discharging to the Norwalk River. Drainage structures

have been located throughout the site to collect stormwater runoff from paved and landscaped surfaces. Due to the location of the proposed building in the central portion of the site, the drainage system has been split into northern and southern systems around the building. Infiltration systems and porous pavement systems have been designed and located on either side of the proposed building, promoting infiltration and treatment of the stormwater runoff. These systems converge into a single outlet pipe located at the western end of the building, with a single outlet located at the southwestern corner of the site. A riprap apron and level spreader have been designed to reduce outlet velocities and provide erosion control prior to discharge to the Norwalk River.

### 2.2.1 Proposed Site Hydrology

The proposed conditions hydrologic analysis consists of sub-watershed areas at each inlet structure of the development property. For each proposed watershed area, weighted curve numbers and times of concentration were calculated and utilized in the proposed conditions hydrologic model. The infiltration and porous pavement systems were also modeled to determine the effectiveness in reducing peak discharges from the site.

**Table 2-2** provides a summary of the peak discharges under existing and proposed conditions for the 2, 10, 25, 50, and 100 year storm events.

			Storm	Frequency (`	Years)	
Discharge Location	Condition	2	10	25	50	100
Norwolk Diver	Existing	7.662	13.50	17.25	20.05	23.05
NOTWAIK RIVER	Proposed	1.185	5.658	9.362	12.19	16.34

# Table 2-2 Summary of Stormwater Peak Discharge (cfs)

The proposed conditions watershed map, curve number and time of concentration worksheets, and volumetric hydrographs are included in **Appendix D**.

### 2.2.2 Water Quality Volume

The water quality volume (WQV) is equivalent to the first inch of runoff from the site that should be captured and treated in order to remove a majority of stormwater pollutants on an average annual basis. For the proposed development, the infiltration and porous pavement systems have been designed to provide the required WQV. **Table 2-3** summarizes the required and provided WQV for the site.

Required WQV		10,342
	North Infiltration System	2,912
Drovided WOV	South Infiltration System	4,641
Provided wQv	North Porous Pavement System	2,313
	South Porous Pavement System	1,414
Total Provided WQV		11,280

# Table 2-3Summary of Water Quality Volume (cu ft)

The water quality volume calculation sheets are included in **Appendix E**.

### 2.2.3 Hydraulic Capacity and Outlet Velocity

The stormwater collection system has been designed to convey the 25-year storm event as required by the CTDOT 2000 Drainage Manual. The system was designed by analyzing sub-areas corresponding to each inlet structure and calculating weighted runoff coefficients and times of concentration. These values were entered into a storm sewers model using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3. Based upon this analysis, the proposed storm system has the capacity to convey the 25-year storm event. At the outlet of the system, a riprap apron and level spreader have been designed to reduce outlet velocities and prevent scour along slopes. Hydraulic calculation worksheets and storm sewers output results are included in **Appendix F**.

### 2.3 Method of Hydrology and Hydraulic Analysis

The following storm drainage design criteria were used for all drainage pipe systems:

- 1. Design storm rainfall data from NOAA Atlas 14 Point Precipitation Frequency Estimates
- 2. Piped storm drainage system and the outlets are designed for a 25-year storm event.
- 3. Minimum time of concentration = 5 minutes
- 4. For SCS peak flow calculations, Curve Number were as follows:
  - a. Impervious (Pavement/Roof Areas) = 98
  - b. Landscaped and Lawn Areas = 69
- 5. For rational peak flow calculations, runoff coefficients were as follows:

- a. Impervious (Pavement/Roof) areas = 0.95
- b. Landscaped and Lawn Areas = 0.30
- 6. Minimum diameter of pipes = 12 inches, excluding roof leaders, underdrains, yard drains and foundation drains
- 7. Minimum pipe slope = 0.5 percent
- 8. Watershed areas delineated using polylines in AutoCAD Civil 3D 2018.
- 9. Comparative hydrology analyzed using Hydraflow Hydrographs Extension for AutoCAD Civil 3D 2018, Version 2018.3
- 10. Storm drainage system analyzed using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3

### 2.4 Best Management Practices

The stormwater management plan for the proposed site uses "Best Management Practices" (BMPs) to remove a high percentage of sediments in accordance with the Connecticut Department of Energy and Environmental Protection "Stormwater General Permit Criteria".

The BMPs include:

<u>Catch Basins and Yard Drains with Sumps</u>: Catch basins and yard drains with sumps collect sediment and prevent discharge of oil and other pollutants into the storm drainage system. All new catch basins and yard drains on-site will have 24-inch sumps.

<u>Hydrodynamic Separators</u>: Hydrodynamic separators serve as pretreatment and prevent transport of oils and sediment further downstream. The proposed stormwater management system utilizes Contech CDS units prior to discharge into the underground infiltration systems. The Contech CDS units have been sized in accordance with the 2004 CTDEEP Stormwater Quality Manual. Sizing calculations are provided in **Appendix E.** 

<u>Underground Infiltration</u>: Underground Infiltration serves as a primary treatment practice, reduces peak flow rates, and promotes groundwater recharge. The proposed stormwater management system utilizes concrete chambers surrounded by stone and filter fabric and an outlet control structure designed to attenuate peak flows.

<u>Level Spreader</u>: Level Spreaders serve as a secondary treatment practice that are utilized to reduce stormwater discharge velocities to non-erosive levels.

### 2.5 Pollutant Loading Analysis

Pollutant loadings for the existing and proposed conditions were calculated using the method prescribed by Debo and Reese in "Municipal Stormwater Management", 1995. This method determines the mass of pollutant loading by inputting the fraction of

impervious area, the contributing area, the mean annual rainfall, and the event mean concentration of pollutant (EMC). The EMC is based upon the pollutant analyzed and the general characteristic of the contributing area – residential, commercial, or open space.

For the proposed conditions, the contributing area was further broken down into contributing areas to certain best management practices (BMPs). Pollutant loading reductions were taken at certain BMPs, depending upon the removal efficiency of the BMP as stated in the 2003 edition of Debo and Reese. Pollutant removal efficiencies for proprietary products were taken from a report entitled "Final Report: Stormwater Treatment Devices Section 319 Project" submitted to the Connecticut Department of Environmental Protection, Bureau of Water Management by the University of Connecticut Department of Natural Resources Management and Engineering, April 15, 2002. This report provides results of field testing for pollutant removal on different types of proprietary stormwater treatment devices installed throughout the State of Connecticut. Based upon these pollutant reductions, we have determined that pollutant loadings will be less for the proposed conditions, as shown in **Table 2-4** below. The pollutant loading calculation sheets are included in **Appendix E**.

# Table 2-4Pollutant Loading Summary

				Pollut	ant		
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre-Treatment	lb/yr/1-in	0.479	0.097	25.480	0.036	0.008	0.034
Proposed, Post-Treatment	lb/yr/1-in	0.296	0.040	5.152	0.015	0.003	0.010
Reduction, Pre to Post Treat		38%	59%	80%	58%	61%	72%

### 2.6 Stormwater Maintenance and Inspection Schedule

Stormwater management systems require periodic maintenance to ensure they function as designed. The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, roof leaders, piping, hydrodynamic separators, underground infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures</u>: The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment.

Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator:</u> The Contech CDS Units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand, and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration</u>: The underground infiltration system will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader</u>: The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plant species or tree saplings.

<u>Pavement:</u> Paved areas shall be swept periodically by the Owner to clean trash and other debris. The Owner will sweep paved areas on its property in the spring to remove winter accumulations of road sand.

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

Maintenance & Inspection Forms are included in Appendix G.

# Section 3 Floodplain Management & Hydraulics

## 3.0 Background

The Norwalk River was studied by FEMA as a part of the Flood Insurance Study (FIS) for Fairfield County, dated June 18, 2010. The 2010 FIS updated the modeling of the Norwalk River that was originally done for the 1982 Town of Wilton Flood Insurance Study by incorporating Letters of Map Revision issued between 1982 and 2010. The river system itself was not restudied. It is important to note that the vertical datum of the two studies was changed from the National Geodetic Vertical Datum of 1929 (NGVD29, prior to 1973 also known as the Sea Level Datum of 1929) to the North American Vertical Datum of 1988 (NAVD88). The modeling data provided by FEMA is in the NGVD29 datum and the reported water surface elevations in the 2010 FIS are in the NAVD88 datum.

The National Oceanic and Atmospheric Administration (NOAA) offers an online utility, VERTCON, to calculate the difference between the two datums at a given latitude and longitude coordinate. In the area of the project, the NGVD29 datum is 1.07 feet higher than the NAVD88 datum. Refer to the VERTCON conversion in **Appendix H**.

### 3.1 Basis of Modeling

Tighe & Bond obtained a copy of the hydraulic model from FEMA for the Norwalk River. This model was used for the hydraulic analysis of the project since it is the effective FEMA model for the project area. The model was developed using the U.S. Army Corps of Engineers HEC-RAS hydraulic analysis modeling environment.

### 3.1.1 Calibrated Model

To verify the accuracy of the modeling provided by FEMA, a model was created to replicate the data in the FIS. This is the calibrated model, also known as the duplicate effective model. The calibrated model encompasses the Norwalk River, generally spanning from Wolfpit Road to Kent Road in Wilton, corresponding with cross sections O and K of the FIS, respectively. The project site at 141 Danbury Road falls between cross sections O and N of the model. The comparison of the 100-year (1% chance) calibrated model water surface elevations with the elevations reported in the FIS Floodway Table are summarized in **Table 3-1**. The output table of the calibrated model is included in **Appendix H**.

	Calibrated Model Cross – Section Number	Water Surface Elevation (NAVD88)		
FIS Cross Section Identifier		Floodway Data Table	Calibrated Model	
К	21745	123.4	123.41	
L	22765	130.6	130.57	
М	24525	138.8 138.69		
N	24597	141.2 140.1		
0	29920	153.1	152.89	

### Table 3-1 Calibrated Model Output

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As shown in the table, the water surface elevations of the Calibrated Model closely mirror the values reported in the FIS Floodway Table. Slight variations in water surface elevations can be attributed to the differences between the HEC-2 and HEC-RAS modeling environments. The effective modeling and data provided by FEMA of the Norwalk River is in or has been developed from HEC-2 modeling. The HEC-RAS modeling environment is the successor to HEC-2 and is FEMA's current standard for flood studies. Based on the results shown, the Calibrated Model is suitable for modeling the proposed conditions of the project.

### 3.2 Flow Rates

The established flow rates for the Norwalk River are documented in Volume 1 of the FIS. Tighe & Bond is not challenging the flow rates established by the FIS and will be using the rates for modeling existing and proposed conditions. The flow rates for the river at the location of the site based on the FIS are summarized in **Table 3-2.** See **Appendix H** for a copy of the Norwalk River discharges included in the FIS.

### 

Frequency (years)	Annual Chance Probability	Flow Rate (cfs)
10	10%	2,980
50	2%	5,840
100	1%	7,455
500	0.2%	12,505

## **3.3 Existing Conditions Model**

In order to best evaluate the impact of the proposed project, we inserted cross sections into the effective model to create an existing conditions model, also known as the corrected effective model. Due to the spacing of the sections in the effective model, the variations in floodplain topography are not accurately reflected in the vicinity of the project area. A total of four cross sections were added to the model and developed from the topographic survey of the site. Since the topographic survey is in the NAVD88 datum, the elevations of the geometry points were converted to NGVD29 before entering into the model. **Figure 3** in **Appendix A** shows the locations of the cross sections through the project site. **Table 3-3** summarizes the resulting water surface elevations of the added sections in the existing conditions model.

100-year Water Surface Elevation (NAVD88)	
146.48	
146.47	
146.46	
146.46	

# Table 3-3Existing Conditions 100-Year Water Surface Elevations (NAVD88)

Refer to **Appendix H** for the model output table of the existing conditions model.

### **3.4 Proposed Conditions Model**

The next step in the modeling process is to determine the resultant water surface elevations of the project, including the proposed building and grading changes. We modified the appropriate sections in the Existing Conditions model accordingly. **Table 3-4a** and **3-4b** compare the proposed conditions results to the existing conditions for the 100-year and 10-year events, respectively.

# Table 3-4a100-Year Water Surface Elevation Comparison (NAVD88)

	100-year Water Surface Elevation (NAVD88)			
Section	Existing	Proposed	Difference	
28020	146.48	146.48	0.00	
27930	146.47	146.47	0.00	
27830	146.46	146.46	0.00	
27790	146.46	146.46	0.00	

# Table 3-4b10-Year Water Surface Elevation Comparison (NAVD88)

	10-year Water Surface Elevation (NAVD88)			
Section	Existing	Proposed	Difference	
28020	144.93	144.93	0.00	
27930	144.93	144.93	0.00	
27830	144.92	144.92	0.00	
27790	144.92	144.92	0.00	

Based upon the hydraulic analysis, the proposed construction will not adversely impact 100-year and 10-year flood elevations along the Norwalk River.

### 3.5 Compliance with Local Floodplain Regulations

Section 29-9.F.7 of the Wilton Zoning Regulations requires the following:

- k. Equal Conveyance: Within the floodplain, except those areas which are tidally influenced, as designated on the Flood Insurance Rate Map (FIRM) for the community, encroachments resulting from filling, new construction or substantial improvements involving an increase in footprint of the structure, are prohibited unless the applicant provides certification by a registered professional engineer demonstrating, with supporting hydrologic and hydraulic analyses performed in accordance with standard engineering practice, that such encroachments shall not result in any (0.00 feet) increase in flood levels (base flood elevation). Work within the floodplain and the land adjacent to the floodplain, including work to provide compensatory storage shall not be constructed in such a way so as to cause an increase in flood stage or flood velocity.
- I. Compensatory Storage: The water holding capacity of the floodplain, except those areas which are tidally influenced, shall not be reduced. Any reduction caused by filling, new construction or substantial improvements involving an increase in footprint to the structure, shall be compensated for by deepening and/or widening of the floodplain, storage shall be provided on-site, unless easements have been gained from adjacent property owners; it shall be provided within the same hydraulic reach and a volume not previously used for flood storage; it shall be hydraulically comparable and incrementally equal to the theoretical volume of flood water at each elevation, up to and including the 100-year flood elevation, which would be displaced by the proposed project. Such compensatory volume shall have an unrestricted hydraulic connection to the same waterway or water body. Compensatory storage can be provided off-site if approved by the municipality.

### 3.5.1 Equal Conveyance

As shown in Table 3-4a, there are no increases in the base flood elevation as a result of the project, so the equal conveyance requirement has been met.

### **3.5.2 Compensatory Storage**

The placement of the building columns and stairways within the floodplain would result in a loss of floodplain storage. Therefore, we propose revised grading to mitigate against the loss of flood storage volume. The grading as proposed results in a net cut of approximately 800 CY within the floodplain boundary, compensating for the approximate 30 CY occupied by the columns and stairways of the proposed building. The project as proposed would not decrease floodplain storage on-site.

# **Section 4 Site Utility Services**

### 4.1 Water and Fire Protection Services

Water and fire protection services to the site will be provided by The Aquarion Water Company (Aquarion). Services to the proposed buildings will be fed from the reported 12-inch main located in Danbury Road. Existing hydrants are located in the vicinity of the project site on the west and east sides of Danbury Road.

The estimated daily water demand for the proposed residential development is approximately 48,000 gallons per day (GPD). The estimated peak hour demand is 100 gallons per minute (GPM), determined using a maximum-to-average-day ratio of 3.0.

### **4.2 Electric Service**

Electric service to the site is provided by Eversource Electric Company. Overhead primary service lines are located on the west side of Danbury Road and enter the site from the north.

### 4.3 Gas Service

Eversource Gas Company provides natural gas service to the project area. Eversource Gas Company maintains a 12-inch gas main located in Danbury Road.

Once the estimated peak demand for the total project is determined, Eversource Gas Company will provide a letter of service availability.

### 4.4 Tele-Data and Cable TV Services

Frontier Communications provides local and long-distance telephone service to the project area and also offers high speed internet and business data services. The existing network in this area is composed of a combination of overhead lines and underground ductbanks. The existing service is provided overhead on the north side of the building. There is also an existing utility pole on the project site along the southerly property line that provides overhead services for 131 Danbury Road. These overhead wires and the routing for this building will need to be relocated in order to accommodate the proposed site improvements. Easements are not identified on the record documents for this utility pole or the service lines.

Telephone service to the proposed development would be provided underground from a utility pole in the adjacent street. The exact location of the service connections will be coordinated with the utility owner during the final design process.

Altice USA provides cable service as well as high speed internet access to the project area. The majority of the existing network runs overhead and follows the same alignment as the telephone service.

### 4.5 Sanitary Sewer Service

The project site is located within the Wilton WPCA Sewershed.

Based on available Town maps, there is a 24-inch gravity sanitary sewer located in Danbury Road. The proposed building will connect to the existing sewage system by constructing a manhole over the existing sewer pipe in the adjacent street frontage. WPCA approval will be required for all sewer connections.

The projected wastewater flows associated with the proposed development were calculated based on the 173 residential units with 317 total bedrooms and a flow rate of 150 gallons per day (GPD) per bedroom. A peaking factor of 4 was applied to the average daily flows to estimate peak flows. **Table 4-1** below summarizes the projected average and peak daily sanitary sewer flows for the site. Refer to **Appendix J** for a full breakdown of the sanitary sewer flow calculations.

Wastewater Requirements					
Development		Design	Design Criteria		Peak Flow
Use	Units / Bedrooms	GPD	Unit	(GPD)	(GPM)*
Residential	173 / 317	150	Per Bedroom	47,550	132

### Table 4-1 - Projected Average and Peak Daily Sanitary Sewer Flows

\* Peak factor of 4 was applied to average daily flows to estimate peak flows; New England Interstate Water Pollution Control Commission, 2011.

# Section 5 Soil Erosion and Sedimentation Control

### 5.1 SESC Narrative

<u>General</u>

The proposed development is entitled "141 Danbury Road" in Wilton, Connecticut.

Estimated: Project Start: Fall 2021 Project Completion: Spring 2022

Erosion Control Narrative refers to drawings C-501 through C-503.

The proposed site development will consist of building demolition, clearing and grubbing the existing site, excavation, construction of sedimentation/detention basins, and rough grading of building, parking areas, sidewalks and curbing.

The development is located in Wilton, Connecticut and is located on Danbury Road.

The stormwater management measures will address the stormwater quality once the site has been constructed and stabilized. Sedimentation and erosion control measures will be installed during construction which will minimize adverse impacts from construction activities.

All sedimentation and erosion control measures proposed for this development have been designed in accordance with the "2002 Connecticut Guidelines for Soil Erosion and Sedimentation Control" as published by the Connecticut Council on Soil Erosion and Water Conservation. Additional guidelines have also been followed that are available from the Connecticut Department of Environmental Protection as recommended for sedimentation control during construction activities.

### Construction Sequence – Initial Phase

- 1. Conduct a pre-construction meeting with the Owner or Owner's Representative, Town Engineer, Design Engineer, Site Engineer, Contractor and Site Superintendent to establish the limits of construction, construction procedures and material stockpile areas.
- 2. Field stake the limits of construction.
- 3. Install all applicable soil and erosion control measures around the perimeter of the site to the extent possible. this will include siltation fence around the project as shown on the plans.
- 4. Install construction access road and anti-tracking pavement in the areas as shown on the plans. All construction access shall be into the site through the anti-tracking pads.

- 5. Establish temporary staging area.
- 6. Begin building demolition and pavement removal.
- 7. Construct the initial storm drainage and sedimentation trap as shown on the plans.
- 8. Install water quality systems and associated drainage network to the maximum extent practicable. Grade the area around the storm drainage system as necessary.
- 9. Begin rough roadway grading.
- 10. Install remaining drainage system to the extent necessary to provide positive drainage.
- 11. Begin installation of sanitary sewer system, water, and other utilities to extent necessary.
- 12. Provide silt fence/haybale barrier around soil stockpile area. Provide temporary vegetative cover (defined in erosion control notes) on all exposed surfaces.
- 13. Begin building construction.
- 14. Pave binder course on parking and driveways for non-porous pavement areas.
- 15. Establish temporary vegetative cover.
- 16. Construct drainage and subbase for porous pavement and place porous pavement course

### Construction Sequence – Final Phase

- 1. Repair perimeter sediment & erosion controls as needed.
- 2. Clean/replace controls from previous phase as needed.
- 3. Fine grade site.
- 4. Continue construction of building.
- 5. Complete construction of sidewalks.
- 6. Establish final vegetative cover and landscaping.
- 7. Pave surface course on roadways.
- 8. Remove erosion controls when site is stabilized.

### **5.2 Soil Erosion and Sedimentation Control Notes**

- 1. All sedimentation and erosion control measures shall be constructed in accordance with the standards and specifications of the "2002 Connecticut Guidelines for Soil Erosion and Sediment Control", DEP Bulletin No. 34, and all amendments and addenda thereto as published by the Connecticut Department of Environmental Protection.
- 2. Land disturbance shall be kept to the minimum necessary for construction operations.
- 3. All erosion control measures shall be installed as shown on the plan and elsewhere as ordered by the engineer.
- 4. All catch basins shall be protected with a silt sacks, haybale ring, silt fence or block and stone inlet protection throughout the construction period and until all disturbed areas are thoroughly stabilized.
- 5. Whenever possible, erosion and sediment control measures shall be installed prior to construction. See "Erosion Control Narrative".
- 6. Additional control measures shall be installed during the construction period as ordered by the engineer.
- 7. All sedimentation and erosion control measures shall be maintained in effective condition throughout the construction period.
- 8. Sediment removed shall be disposed of offsite or in a manner as required by the Engineer.
- 9. The construction contractor shall be responsible for construction and maintenance of all control measures throughout the construction period.
- 10. All disturbed areas to be left exposed for more than 30 days shall be protected with a temporary vegetative cover. Seed these areas with perennial ryegrass at the rate of 40 lbs. per acre (1 lb. per 1,000 sq. ft). Apply soil amendments and mulch as required to establish a uniform stand of vegetation over all disturbed areas.
- 11. The construction contractor shall utilize approved methods/materials for preventing the blowing and movement of dust from exposed soil surfaces onto adjacent properties and site areas.
- 12. The construction contractor shall maintain a supply of silt fence/haybales and antitracking crushed stone on site for emergency repairs.
- 13. All drainage structures shall be periodically inspected weekly by the construction contractor and cleaned to prevent the build-up of silt.
- 14. The construction contractor shall carefully coordinate the placement of erosion control measures with the phasing of construction.
- 15. Keep all paved surfaces clean. Sweep and scrape before forecasted storms.

141 Danbury Road - Engineering Report

- 16. Treat all unpaved surface with 4" minimum of topsoil prior to final stabilization.
- 17. Haybale barriers and silt fencing shall be installed along the toe of critical cut and fill slopes.
- 18. The contractor shall notify the Town officials prior to the installation of erosion controls, cutting of trees, or any excavation.
- 19. All trucks leaving the site must be covered.
- 20. Some control measures are permanent. These structures shall be cleaned and replenished at the end of construction. locations of the permanent control structures are shown on the drainage plans.
- 21. All sedimentation and erosion controls shall be checked weekly and/or after each rain fall event. Necessary repairs shall be made without delay.
- 22. Prior to any forecasted rainfall, erosion and sediment controls shall be inspected and repaired as necessary.
- 23. After all disturbed areas have been stabilized, erosion controls may be removed once authorization to do so has been secured from the Owner. Disturbed areas shall be seeded and mulched.
- 24. All embankment slopes 3:1 or greater to be stabilized with erosion control blanket, North American Green SC150BN or approved equivalent, unless otherwise noted on plans.

# **Tighe&Bond**

**APPENDIX A** 



SITE LOCATION MAP



NORTH

Tighe&Bond www.tighebond.com

04/09/2021

# National Flood Hazard Layer FIRMette



### Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



# **Tighe&Bond**

**APPENDIX B** 



USDA Natural Resources

**Conservation Service**




## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
103	Rippowam fine sandy loam	B/D	0.7	13.8%
307	Urban land	D	4.4	83.3%
W	Water		0.2	2.8%
Totals for Area of Intere	st		5.3	100.0%

#### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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		s-1	24/12	0-2.0	5-10-10-5	ND	Top 2": TOP:	SOIL and grey-b	orown,	TOPSO	L	1		Casing - Conci
							fine to coa	rse SAND.		0.2' FINE COAR SAN	TO SE D			- Auger Spoil
5		s-2	24/16	4.0-6.0	2-3-2-2	ND*	Loose, brown black SILT.	n, fine SAND gr	ading to	4.0'				- Bento Seal
		s-3	24/20	6.0-8.0	3-3-3-3	ND*	Loose black fine Sand o	SILT grading t grading back to	o brown black	SIL AND SAN	T D		Ŀ	PVC Riser
		s-4	24/22	8.0-10.0	6-5-8-9	ND	Silt. Medium dense coarse SAND	, grey-brown,	fine to	8.0'		2	E	
)		s-5	24/16	10.0-12.0	8-10-12-12	ND	Gravel, trac Medium dense	e Rock Fragmen	ts. o coarse	803672248	34.50		E	Scree
								The dravet.		COARS	SE )			- Sand
	_	s-6	24/22	15.0-17.0	5-1-2-3	ND	Very loose, towards tip	grey, fine SAND of spoon.	D, finer	15.0'			E	
		s-7	24/22	17.0-19.0	11-14-18-20	ND	Medium dense	, grey, fine S/	AND.	FINE		3		
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ave	+. E tific beer	cation	= End	of Boring. represent a mes and unde	pproximate bo	oundaries	between soil	types, transi	tions may be	gradual.	Wate	er l	evel rea	dings
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r		s-3	24/12	6.0-8.0	27-24-28-31	ND	Dense ROCK to coarse S Gravel.	FRAGMENTS and f SAND, trace fine	ine rounded					
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t		s-3	24/18	6.0-8.0	12-15-15-19	0.3	Medium dense, red-brown, f	ine to	COAR	SE		H	
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ſ		S-4	24/8	8.0-10.0	14-24-17-24	0.1	Dense, brown-black, coarse				-	E	
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2	•	below	grade.	Well compl	eted to ground	d surface	with 2-inch, schedule 40,	een set at a threaded, f	pproximat lush-joir	ted, s	fe	d PVC	
		3 to 2	feet b	elow grade.	Annulus aro	around well	backfilled with auger spoi	w grade. Be ls from 2 to	entonite s 0 1 feet b	seal pl	ace	d from le.	
		well (	apped w	ith a steel	stick-up cas	ing cemei	ited in place.						
1	ifi	cation	lines	represent a	pproximate bo	undaries	between soil types, transi	tions may be	gradual.	Wate	er l	evel read	dings
	pr	esent	at the	time measur	ements were m	ade.	ructuations of groundwate	r may occur	due to fa	ictors	oth	er than	
-											BOR	ING NO.	MW-7

G	A GE	OENVI ers a	RONMENT/ nd Scier	AL, INC. htists			141 Dant	oury Road		_		E	BORING NO.	. <u>MW-8</u>
	4 Sp umbu 203)	oring Jll, C 268-0	Hill Roa onnectio 808	ad cut 06611			Wilton, Co	onnecticut		_		F	ILE NO.	50642 JMB
Boi	ing	Co.	GZA Dr	illing	Ту	pe	CASING 4 174" HSA	<u>SAMPLER</u> Split Spoon		GROUN		RE	ADINGS	
- ol	emar	h	Al Aug	ustine	1.	D./O.D.		1 3/8"/ 2"	Date	Time	Dept	:h	Casing	Stab. Time
iZ/	Rep	<b>.</b>	ClareA	nn Walsh	Ha	mmer Wt.		140 lbs.	5/30/92		7.8	,	15.0'	0 hrs.
Dat	te St	art	5/30/	92 End 5	/30/92 Ha	mmer Fal	ι	30 in.						
iS.	Elev	<i>.</i>		Datum	Ot	her	1							
	atio	n												
D	СВ		Sa	ample Inform	nation							R	Equ	ipment
H	ADWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSIF	FICATION	Descri	ption	LEXS	Flush m	ount cover
-		S-1	24/0	0-2.0	6-10-14-11	0.7	Medium dens	e, brown, fine	to	FINE	то	1		Auger
					·····		coarse SAND	(auger spoils)	).	.COA SA	ND			Spoils
1										2,0'		11		Seal
				_										Diana
-		s-2	24/8	4.0-6.0	2-2-3-4	0.8	Loose, blac	k-brown, fine S	SAND and	FI	NE			Kiser
- 5							SILI, trace	clay.		SA	ND		H	
		s-3	24/8	6.0-8.0	2-2-2-3	0.9*	Loose, blac	k, fine SAND ar	nd SILT,					
							tittle clay	, trace coarse	sand.			2		
		S-4	24/8	8.0-10.0	5-5-1-10	0.8	Loose, blac SILT, littl	k, fine SAND ar e Clay, trace c	nd coarse					
10		-	-				Sand.	,,		L		-		Screen_
-		s-5	24/10	10.0-12.0	8-11-15-3	0.8	Medium dens coarse SAND	e, black-brown, , trace fine ro	fine to	10.0'	12			
5			-				Gravel.	• • • • • • • • • • • • • • • • • • • •						
E.			-							FINE	TO			- Sand
	-	-								SAI	ND		E.	di l
.5	_		24.440	45 0 47 0	0 45 40 40	0.7								<u> </u>
	-	S-6	24/10	15.0-17.0	8-15-12-10	0.7	SAND, trace	fine rounded G	to coarse Gravel,					ų.
					41.94 No. 100.000		trace Organ	ic matter.		17.0/		- 3		
										E.0	в.			
?0		-												-
	-													
	-													
	-													
25														-
											- 10- Turk IV			
_	1.	Soil	samples	field scree	ened with a	11.7eV p	ortable HNu	photoionization	detector fo	r volati	le org	anic	c	
M	2.	Sampl	e wet.	(cs).	Indicates sam	ple sent	to laborato	10-slot BVC so	nat anatysis.	approvim	ately	15 (	foot	
*	э.	below	grade.	Well comp	leted to grou	nd surfa	ce with 2-in	ch, schedule 40	), threaded,	flush-jo	inted,	so	lid PVC	
4		3 to	2 feet	below grade	. Annulus ar	ound wel	l backfilled	with auger spo	bils from 2 t	o 1 feet	below	gra	ade.	
-		wett	capped		n mounted wet	Cover.	concreted in							_
tr	atif	icatio	on lines	represent	approximate b	oundarie	s between so	il types, trans	sitions may b	e gradua due to	l. Wa	ter	level re	adings
the	se p	resent	t at the	time measu	rements were	made.	, cascacio		cor may occur			В	ORING NO.	MW-8
2												1		
140														

GZ	ZA GE	OENVI ers a	RONMENT nd Scie	AL, INC. ntists			141 Danbury Road		_		1	BORING NO PAGE <u>1</u>	• <u>A-1</u> _ OF 1
20 Ti	04 Sp rumbu 203)	ning Ill, C 268-0	Hill Ro onnecti 808	ad cut 06611			Wilton, Connecticut		_			TLE NO.	50642 JMB
Bor	ring	Co.	GZA Dr	illing	Ту	pe	CASING SAMPLER 2 3/4" HSA Split Spoon		GROUN	DWATER	RE	ADINGS	
FOI	reman	í.	Al Aug	ustine	I.I	D./O.D.	<u> </u>	Date	Time	Dept	h	Casing	Stab. Tir
١ZA	A Rep		ClareA	nn Walsh	Hai	mmer Wt.	140 lbs.					_	
)at	te St	art	5/31/	92 End 5	/31/92 Har	mmer Fal	<u> </u>						
s.	.Elev			Datum	Otl	her							
.00	catio	n											
)	СВ		S	ample Inform	nation			_			R	Equ	ipment
	A L S N W G S	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIPTION & CLASSIF	ICATION	Deșcri	tum ption	LEKS	Ins	stalled
	1	s-1	24/8	0-2.0	6-18-20-17	ND*	Top 3": TOPSOIL.	22	TOPS	OIL	1		
							Bottom 5": Brown, medium t SAND, some Rock Fragments.	o fine	0.25' FINE MEDI SAN	TO			
5		s-2	24/6	4.0-6.0	2-5-6-6	ND*	Loose brown, fine SAND, tr fine Gravel.	ace	4.0'				
-		s-3	24/4	6.0-8.0	4-5-7-15	ND	Medium dense, brown, fine	to	5.0'				
and the second se		s-4	24/4	8.0-10.0	11-13-26-26	ND	fine Gravel. Dense, brown, fine to coar	se	FINE COAF SAM	TO SE ID	2		
0	_						SAND, little fine Gravel, Fragments.	trace Rock	10.07		3		
									E.O.	8.			
5													
0													
5	_												
	1. 2. 3.	Soil compo Sampl E.O.B	samples ounds (V e wet. . = End	field scree OCs). "*" of Boring.	ened with a 10 Indicates samp	).2 eV po ble sent	ortable HNu photoionization to laboratory for addition	detector for al analysis.	• volatil	e orga	nic		
trav	atifi e bee	icatio en mad	n lines le at ti	represent mes and und	approximate be er conditions	oundaries stated.	s between soil types, trans Fluctuations of groundwat	itions may b er may occur	e gradua due to	l. Wat factors	er	level re ther than	adings
.110	se pr	resent	at the	time measu	rements were n	nade.					B	DRING NO.	<u>A-1</u>

Ľ	GZA Engi	GEOENV	IRONMEN and Sci	TAL, INC. entists			141 Danbury Road					BORING NO	- <u>A-2</u>	
L	204 Trum (203	Spring bull ) 268-	Hill R Connect 0808	pad icut 06611			Wilton, Connecticut					PAGE 1 FILE NO. CHKD. BY:	OF 1 50642 JMB	
B	orin	g Co.	_GZA D	rilling	T	ype	CASING SAMPLER 4 174" HSA Split Spoon		GROUN	DWATER	RE	ADINGS		
16	orema	an	<u>AL AU</u>	gustine	I.	.D./O.D.	<u> </u>	Date	Time	Dept	h	Casing	Stab.	Time
1.	ZA RE	ер.	_Clare	Ann Walsh	Ha	ammer Wt.	140 lbs.							_
P	ate :	start	_5/31	/92 End _	5 <u>/31/92</u> Ha	ammer Fal	.l <u>30 in.</u>							
	ocati			Datum	Ot	her	<u>4" HSA</u>							
Б	Ici			ample Infor	mation						_			
ļŝ	A					Field	SAMPLE		Strat	um	RE	Equ	ipment	
4	N I G S	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Testing (ppm)	DESCRIPTION & CLASSIF	ICATION	Descrip	tion	MKS		tutteu	
ł	-	S-1	24/8	0-2.0	6-13-13-12	ND	Top 4": TOPSOIL. Bottom 4": Brown, medium SA	AND and	TOPSO	IL	1			-
11		-					ROCK FRAGMENTS.		0.31					
										1				
1	-	5-2	24.16	6 0-6 0	2440				FINE	то				
1.5	; <b> </b>	102	24/0	4.0-0.0	2-0-4-8	ND*	SAND, little Silt, trace co	ne Darse	MEDIU	IM				_
	-	S-3	24/10	6.0-8.0	2-4-5-4	ND	Sand.		a a taman					
						ND	NO recovery.							
		s-4	24/10	8.0-10.0	20-4-19-15	1.4*	Top 4": Black CLAY and SILT Middle 1": WOOD FIBER.		8.0'		2			
)		5-5	26.78	10 0-12 0	22 16 15 14		Bottom 5": ROCK FRAGMENTS.				3			
	-	3-5	24/0	10.0-12.0	22-10-15-14	1.9	Dense, grey, medium to fine SAND and ROCK FRAGMENTS.		10.0' FINE T	0	~			
1									MEDIUM SA	ND				
Ι.									12.0' E.O.B.	.				
														_
1														
ł														
-														
20														
14														-
4 +														
13														
	_													
25														
11	_													
1 .														
, 1														
1	-													
R	1	Soil a		field server								_		
ENARKS	2.	compou Sample E.O.B.	wet. = End	of Boring.	ned with a 10. Indicates samp	2 eV por ble sent	table HNu photoionization de to laboratory for additiona	etector for l analysis.	volatile	organi	с			
5 8	tifi	cation	lines	represent a	oproximate bou	Indaries	between soil types transit	ione may be	anadust	11		Ville Versioner		_
thios	e bee	n made esent	at tim at the	es and under time measure	r conditions s	tated.	Fluctuations of groundwater	may occur o	due to fac	water tors o	the	evel readi	ngs	
11	-		A 817 - S. MANUER							В	ORI	NG NO. /	1-2	
E													N-C-12	

	A GEO	ENVII	NONMENTA	L, INC. tists		_	141 Danbury Road		-		B	ORING NO	. <u>B-3</u> OF 1	
204	4 Spr	ing l	ill Roa	d ut 06611			Wilton, Connecticut		-		FC	ILE NO.	50642 JMB	
							CASING SAMPLER		GROUN	DWATER	RE/	ADINGS		
Bor	ing (	20.	GZA Dri	lling	Iy	pe	24" HSA Spt 1 30001	Date	Time	Depth	T	Casing	Stab. Ti	me
F	eman		Ron Hol	man	1.	D./O.D.	<u> </u>	(117.00)	Time	8.0/	-	8.0/	0 hrs	
G	Rep	< - N	L. McKe	e, P. Crow	well Ha	mmer Wt.	<u>140 lbs.</u>	6/15/92		0.0	-	0.0	0 11 3	
Dat	e Sta	art	6/13/9	2 End	6/13/92 Ha	mmer Fall	<u>30 in.</u>				-			
( .I	Elev			_ Datum	Ot	her					-			
Loc	atio	n	See Pla	n				-			_			
g .	СВ		Sa	mple Infor	mation		SAMDI F		Stra	tum	RE	Equ	ipment	
E III	ASNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIPTION & CLASSI	FICATION	Descri	ption	MKS		None	_
1 .		s-1	24/14	0-2.0	3-2-7-15	1/0.8	Loose, brown, fine to coa	arse SAND	TOPS	OIL	1			
	-						Silt.	., tittle	0.31					
Ύ1				-			SPECIAL Comments							
ř.				10000000000000000000000000000000000000										
	-	5-2	24/10	2.0-4.0	12-19-24-29	0.4/0.6	Dense, brown, fine to coa	arse SAND	FINE	TO				
		0 2					and fine to coarse GRAVEL Silt.	., little	SA	ND				120
17									GRA	VEL				
									0.000					
4	_	0.7	21/14	4 0-6 0	16-20-44-66	0 2/0 6	Very dense, brown, fine 1	to coarse						
1		5-5	24/10	4.0-0.0	10-20-44-00	0.2/0.0	SAND and fine to coarse (	GRAVEL,						
13							titte sitt.							
			1											
1 5								SAND						
1.		S-4	24/21	6.0-8.0	29-26-26-40	0.4/0.6	and fine to coarse GRAVE	L, little	6.31					
7							Silt. Bottom 18": Brown, fine 1	to medium	FINE	TO				
1							SAND, little Silt.		SA	ND				-
8							12	00000			2		-	
		S-5	24/15	8.0-10.0	20-19-16-13	0.2/0.6	Dense, brown, fine to coa and fine to coarse GRAVE	arse SAND L, little	8.07					
				_			Silt.		FINE	RSE				
1.									GRA	VEL				
											3			-
0									10.0' E.O	.в.				
1									2.12					
111							1							
		1					1							
12		-					1							2
1.	-						1							
3	-	-					1							
1	-	-	-				1							
114		-	-				1							
1.	-	-	-									-		
-	1	Coll	complex	field ee	reened for vol	atile or	anic compounds with an 11	.7 eV portabl	e HNu Mo	del PI-	101			
( iii	1.	phot	cioniza	tion detec	tor. $1/0.8 =$	meter res	sponse of sample/meter rep	oonse of backg	round co	ndition	IS.			
4.6	2.	Samp	e wet a	at approxim	mately 8 feet	below gra	de.							
K	3.	Bori	ng ended	d at approx	ximately 10 fe	et below	grade. E.O.B. = End of B	loring.						
ist ist	rati	ficat	ion line	s represen	t approximate	boundari	es between soil types, tra Fluctuations of grounds	ansitions may water may occu	be gradu ur due to	al. Wa factor	ate s	r level i other tha	eadings	
th	ose p	orese	nt at th	e time mea	surements were	e made.					Г	BORING NO	). <u>B-3</u>	_
4-	-						×			11 - AN - 14				
11														

GEC	ENVIR	ONMENTA	L, INC. tists			141 Danbury Road			BC P/	ORING NO	<u>B-4</u> OF 1
Spr Spr Smbul		ill Roa onnectic 308	d ut 06611			Wilton, Connecticut			F I Cł	ILE NO.	50642 JMB
ing (		GZA Dri	lling	T	ype	CASING SAMPLER	GROUN	IDWATER	REA	DINGS	
eman Rep. e Sta Elev.	art .	Ron Hol L. McKe 6/13/9	.man 22_ P. Crow 22_ End <u>(</u> Datum	I well Ha 5/13/92 Ha O	.D./O.D. ammer Wt. ammer Fall ther	<u>    1 3/8"/ 2"</u> Da <u>    140 lbs.</u> <u>    30 in.</u>	ate Time	Depth	1	Casing	Stab. Tin
ation C B	<u>.</u>	See Pla	mple Infor	mation				L	R	Equ	lipment
A L S O W G S	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	SAMPLE DESCRIPTION & CLASSIFICATIO	N Descri	iption	L M M M		None
	s-1	24/16	0-2.0	3-16-18-21	0.6/0.6	Top 6": Brown to black TOPSOIL. Bottom 10": Brown, fine to coars SAND and fine to coarse GRAVEL, little Silt.	e <u>TOP</u> ! 0.5'	501L	1		
							FINE COA SA AI GRA	E TO RSE ND VD VEL			
_	s-2	6/6	4.0-4.5	64-10/0"	NS	Very dense, fine to coarse SAND and fine to coarse GRAVEL, littl Silt.	e				
	s-3	0/0	5.0	10/0"	NS	No recovery.	5.0' E.0	.В.	2		
											5
_											
1. 2.	Soil phot ppm Borin NS =	samples oionizat = parts ng endec No samp	field scr tion detec per milli at approvole	I reened for vol tor. 1/0.8 = on. kimately 5 fee	latile org meter res et below g	anic compounds with an 11.7 eV p ponse of sample/meter reponse of rade due to auger and spoon refu	ortable HNu Mo background co sal. E.O.B. =	del PI- ndition End of	101 Is. Boi	ring.	
atif e be	icati en ma	on line de at t	s represen imes and u e time mea	t approximate nder conditio surements wer	boundarie ns stated. e made.	es between soil types, transition Fluctuations of groundwater ma	s may be gradu y occur due to	al. Wa factor	ter s o	level r ther that	readings an

	ZA (	GEOENV	RONMENT	AL, INC.			141 Danb	oury Road					BORING NO	- <u>B-4A</u>	-
	204 s rumb 203)	Spring Dull, ( 268-(	Hill Ro Connecti 0808	oad icut 0661	1		Wilton, Co	nnecticut		_			PAGE 1 FILE NO. CHKD. BY:	OF 1 50642 JMB	=
Вс	oring	Co.	GZA DI	rilling		Гуре	<u>CASING</u> _2%" HSA	<u>SAMPLER</u> <u>Split Spoo</u> n		GROUN	DWATER	RE	ADINGŚ		
FC	orema	in D	Ron Ho	olman		I.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. T	ime
Da	te S	p.	6/13	voz End	6/13/02	lammer Wt.		<u>140 lbs.</u>	6/13/92		8.0	'	8.0'	0 hrs	s.
GS	.Ele	v.		Datum	0/15/72 1	ther		<u>30_1n.</u>		-					
[Lo	cati	on	See pl	an (4 feet	t east of B-4)					-					
, Ip	CB		S	ample Info	ormation		T					R	Eau	ipment	
р Т Н	SNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIF	SAMPLE PTION & CLASSIF	FICATION	Stra Descrij	tum otion	EMKS	Ins	talled	-
	-											1		• • •	
11	-		-												
1	-									SEE					
2										8-4	•				
															-
5															
4						_									
		S-1	24/14	4.0-6.0	22-27-42-22	0.4/0.4	Very dense, SAND and fin	brown, fine to e to coarse GRA	coarse AVEL,						
1 5							little Silt.								-
L			_												
6		s-2	24/18	6.0-8.0	18-16-15-16	0.6/0.4	Dense, brown	, fine to coars	se SAND	FINE	70				
7					_		and fine GRAN	/EL, little Sil	lt.	COARS	E				
										GRAVE	L				
8						All Delvare the									-
1. 1	-	S-3	24/14	8.0-10.0	14-15-21-30	0.6/0.6	Dense, brown, and fine to c	fine to coars coarse GRAVEL,	little			2			
9							Silt, trace C	organics.							
10									ł	10.0'		3			-
111										E.O.B	·				
112															
															_
13	-					-									
14															
r l															
R	1.	Soil s photoi	amples onizati	field scre on detecto	ened for volation. $1/0.8 = m$	tile organ	nic compounds	with an 11.7 of	eV portable I	HNu Model	PI-10	1			
R	2.	ppm = Sample	wet at	er million approxima	tely 8 feet be	elow grade			and a starting of		-101101				
Ks		soring	ended	ac approxi	mately 10 feet	below gr	ade. E.O.B.	= End of Borir	ng.						
itra	tifi	cation	lines	represent	approximate b	oundaries	between soil	types, transi	tions may be	gradual	Vato	r 1	evel reco	lings	_
thos	e pr	n made esent	at tim at the	es and und time measu	ler conditions rements were	stated. made.	Fluctuations	of groundwate	r may occur o	due to fa	ctors	oth	er than	ings	_
												BOR	ING NO.	B-4A	

GZA Eng	GEO	ENVIF rs ar	NONMENT/	AL, INC. htists		_	141 Danb	oury Road		_		1	BORING NO PAGE 1	• <u>B-5</u> OF 1
204 Trur (203	Spr mbul 3) 2	ing H L Cc 68-08	iill Roa onnectio 308	ad cut 06611		1	Wilton, Co	nnecticut		-		l	FILE NO. CHKD. BY:	50642 JMB
orii	ng C	o.	GZA Dr	illing	T	уре	CASING 2%" HSA	SAMPLER Split Spoon		GROUN	DWATER	RE	ADINGS	
orer	man	19400 - 1 <del>8</del>	Ron Ho	lman	1	.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. T
ZA F	Rep.		L. McK	ee, P. Cro	well H	ammer Wt.		140 lbs.	6/13/92		8.0'		8.0'	0 hrs
ate	Sta	rt	6/13/	92 End (	6/13/92 H	ammer Fal	ι	30 in.						100.000
S.E	lev.	a		Datum	0,	ther								
ocat	tion		See pl	an										-
c	в		Sa	ample Infor	mation							R	Equ	ipment
ASNG	LOWS	No.	Pen./	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSI	FICATION	Stra Descri	tum ption	EMKS	Ins	None
-	-	5-1	24/4	0-2.0	1-2-14-24	0.4/0.4	Top 2": Brow	wn to black TO	PSOIL.	TOPS	011	1		
F	-				1 2 14 24	0.4/0.4	Bottom 2": I	Brown, medium	to coarse	0.21		1'		
ŀ	+						trace Silt.			0.2				
F	+					-								
2	-	3-2	12/12	2.0-3.0	13-54	0.4/0.4	Very dense	brown fine +	0 000550					
F	-		12/12	2.0 5.0	0.01	0.4/0.4	SAND and fir	ne to coarse G	RAVEL,					
H	-						titte sitt.	5		ETHE	TO			
-	-									COAR	SE			
$\vdash$	-	-7	26/14	4 0-6 0	16-30-34-34	0.4/0.4	Very dense	brown fine *	0 000000	AN				
$\vdash$	-		24/14	4.0-0.0	10-30-34-34	0.4/0.4	SAND and fir	he to coarse G	RAVEL,	GRAV				
$\vdash$	-						cittle sitt.							
$\vdash$	-							i.						
-	-	-	2/ /10	6 0-9 0	32-29-60-57	0.440.4	Vonu danas	hour firs t						
$\vdash$	-	5-4	24/19	0.0-0.0	52-28-60-55	0.4/0.4	SAND and fir	he to coarse G	RAVEL,					
-	-						tittle sitt.							
$\vdash$	-													
$\vdash$	-	-5	26/14	8.0-10.0	12-17-10-19	0 2/0 2	Dense broun	fine to mod	ium SAND	8.0/		2		•
$\vdash$	-		24/14	8.0-10.0	12-17-19-18	0.2/0.2	little fine	to coarse Gra	vel,	ETHE	TO			
-	-						titte sitt.			COAR	SE			
-										SAN				
-	-									10.07		3		
$\vdash$	+									E.O.	в.			
$\vdash$	-													
-	-													
-	-													
-	-	-												
-	-		_											
-														
-	-													
-	-				_									
-	_								7					
1 23		oil s photo pm = ample oring	samples ionizat parts e wet a g ended	field scre ion detecto per million t approxima at approxima	eened for vola or. 1/0.8 = r n. ately 8 feet b imately 10 fee	atile orga meter resp pelow grac at below g	anic compound ponse of samp de. grade. E.O.B	ds with an 11. ole/meter repo	/ eV portable nse of backgr ring.	and cond	ditions			
rat	ific	atio mad	n lines e at ti	represent mes and un	approximate   der condition	boundaries s stated.	s between so Fluctuation	il types, tran ns of groundwa	sitions may b ter may occur	e gradual due to t	. Wat factors	er	level re ther than	adings
ose	pre	sent	at the	time meas	urements were	made.					٦	BC	DRING NO.	B-5
-	1000	-										-		

G	ZA GE	OENVI ers a	RONMENT nd Scie	AL, INC. ntists			141 Danb	ury Road				l	BORING NO	. <u>B-6</u>	
2 T	04 Sp rumbu 203)	oring Ill, C 268-0	Hill Ro onnecti 808	ad cut 06611		internet and	Wilton, Co	nnecticut				i	TILE NO. CHKD. BY	50642 JMB	
Boi	ring	Co.	GZA Dr	illing	T	уре	CASING 2%" HSA	<u>SAMPLER</u> Split Spoon		GROUN	DWATER	RE	ADINGS	_	
Foi	remar	1	Ron Ho	lman	I	.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. 1	ſi
GZ/	A Rep	·-	L. McK	ee, P. Cro	well H	lammer Wt.		140 lbs.	6/13/92		8.5/		8.0'	0 hr	s
Dat	te St	art	6/13/	92 End	<u>6/13/92</u> H	ammer Fal	ι	<u>30 in.</u>							
GS.	.Elev	•		Datum	0	ther						_			_
Loc	catio	n I	See pl	an								_		And the office of the	
	AL		Sa I	ample Into	rmation			SAMPLE		Stra	tum	RE	Equ	ipment	
r H	NWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Testing (ppm)	DESCRIP	TION & CLASSI	FICATION	Descri	ption	MKS	!	None	
		s-1	24/15	0-2.0	6-13-15-27	0.6/0.6	Top 4": Brow Bottom 11":	n to black TO Brown, fine t	PSOIL.	TOPS	DIL	1			
1							SAND and fin	e to coarse G	RAVEL,	0.31					
2		-													
			-												
3															
4		S-2	24/15	4.0-6.0	22-27-61-61	0.4/0.8	Very dense	brown fine to	0.000000	FINE	TO				
			-4715	4.0 0.0		0.4/0.8	SAND and fin	e to coarse G	RAVEL,	SAN	D				
5							there offer			GRAV	EL				
55				_	_										
6		s-3	24/20	6.0-8.0	50-34-44-46	0.6/0.8	Very dense, l	brown, fine to	o coarse						
_							SAND and fin little Silt.	e to coarse GR	RAVEL,						
1															
,															
°[		s-4	24/16	8.0-10.0	26-50-41-19	0.6/0.8	Very dense, I	brown, fine to	coarse			2			
。							little Silt.	e to coarse GM	KAVEL,						
0											_	3			
										10.0' E.O.I	в.				
1															
ł	_														
2					-										
ł															
3	-														
ł		-													
4	-														
t															
1	1.	Soil s	amples	field scre	ened for vola	tile orga	nic compounds	with an 11.7	eV portable	HNu Mode	L PI-10	01		_	-
	2	ppm =	parts	on detecto	or. 1/0.8 = n n.	neter resp	onse of sampl	le/meter repor	nse of backgro	ound cond	itions				
	3.	Boring	ended	at approximat	imately 10 fee	t below g	rade. E.O.B.	= End of Bor	ing.						
				A 4											
ina ive	atifi bee	cation	n lines	represent	approximate b	oundaries stated.	between soil	types, trans	sitions may be	e gradual due to f	. Wate	er	level rea	dings	
105	se pr	esent	at the	time measu	urements were	made.		gi sanana			Γ	BO	RING NO.	B-6	-
-												20			

	04 s	pring	Hill R	ad			141 Dant	oury Road					PAGE 1	OF
(	203)	268-0	Connect: 0808	icut 0661'	1		Wilton, Co	onnecticut	_	_			CHKD. BY:	JMB
Во	ring	Co.	GZA D	rilling		TVDA	CASING	SAMPLER		GROUN	DWATER	RE	ADINGS	- Contraction
Fo	remai	n	Ron He	olman		I.D./O.D.	<u>_24" HSA</u>	1 3/8"/ 2"	Date	Time	Dent		Cooler	lat-1
GZ	A Re	<b>.</b>	L. Mcl	(ee, P. Cro	owell	lammer Wt.		140 lbs.	6/13/92	Time	8 5	.n /		Stab.
Da	te S	tart	6/13/	92 End	6/13/92	ammer Fal	ι	30 in.	5/15/75		0.5		0.0	0
GS	.Elev	<i>.</i>		Datum	(	Other						-		-
Lo	catio	n	See pl	an									-	
DE	CB		S	ample Info	rmation							R	Equ	ipmen
PTH	SNUS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSIF	ICATION	Stra Descri	tum ption	EMK	Ins	talle
_		S-1	24/16	0-2.0	6-10-18-27	0.8/0.8	Top 10": Bro	own to black TO	PSOIL.	TOPS	011	1		vone
1							little fine Bottom 6": E	to coarse Grav Brown, fine to	el. coarse	0.8'		11		
1				_			SAND and fir little Silt.	ne to coarse GR	AVEL,	0.0				
2								in A						
-														
3														
4			and the second second		A REAL PROPERTY AND A REAL									
		s-2	24/18	4.0-6.0	20-26-23-25	0.8/0.8	Dense, brown and fine to	, fine to coars	se SAND	FINE	TO			
5							Silt.	shrively	11466	SAND	5			
	_									GRAVE	EL			
6		5.7	2/ /15	60.00	25.74.70.70	0.011								
	-	3-2	24/15	0.0-8.0	25-31-38-39	0.8/1.0	Very dense, I SAND and find	brown, fine to e to coarse GRA	coarse VEL,					
7							trace Silt.							
ł		-												
8		s-4	24/15	8.0-10.0	21-15-13-24	0.8/1.0	Medium dense	brown fine +	0 coarse			2		
Ì							SAND and fine	to coarse GRA	VEL,			2		
1														
Ľ									ł	10.0'		3		
1										E.O.B	•			
Ĺ	_													
2	_													
+	_													
3	-													
$\left  \right $														
4														
F														
1	1. 9		amples	field core	anad for unla							L		
		hotoi	onizati	on detecto	r. 1/0.8 = m	eter respo	onse of sampl	e/meter reponse	eV portable H e of backgrou	INu Model und condi	PI-10 tions.	1		
1011	2. Š	ample	wet at	approxima at approxim	tely 8.5 feet	below gra	de.	- End of Dania						
[	0.51 1/5 	21 119	enada i		indicety to fee	L Derow gr	aue. E.U.B.	- End of Borir	ig .					
ra	tific	ation	lines	represent	approximate b	oundaries	between soil	types transit	tions may be	anadual	Unto		aval	Iner
ve	beer e pre	made sent	at tim at the	es and und time measu	er conditions rements were	stated.	Fluctuations	of groundwater	may occur o	due to fa	ctors	oth	evel read er than	ings
_			unart (Profiléit)									BOR	ING NO.	B-7

	IZA G Ingin 04 S rumb	EOENV: eers a pring ull, (	Hill R	TAL, INC. entists oad icut 0661	1		141 Danbury Road					BORING NO PAGE 1 FILE NO.	• <u>B-8</u> 0F <u>1</u> 50642
(	203)	268-0	808		-		witton, connecticut					CHKD. BY:	JMB
Во	ring	Co.	GZA D	rilling		Туре	CASING SAMPLER		GROUN	DWATER	RE	ADINGS	
Fo	remar	r	Ron H	olman		I.D./O.D.	<u>1 3/8"/ 2"</u>	Date	Time	Dept	h	Casing	Stab. Tim
GZ	A Rep	<b>.</b>	L. Mcl	Kee, P. Cr	owell	Hammer Wt.	140 lbs.	6/13/92		10.0	,	8.01	0 hrs.
Da	te St	tart	6/13,	/92 End	6/13/92	Hammer Fal	l 30 in.						
GS	.Elev	/.		Datum_		Other							
D	СВ	<u></u>	See pr	ample Info	ormation		1						
EPT	A L S O N W	No.	Pen./	Depth	Blows/6"	Field	SAMPLE DESCRIPTION & CLASSI	ICATION	Stra	tum	REM	Equ Ins	ipment talled
Н	GS	0-1	Rec.	(Ft.)	1.0.04.04	(ppm)			Descri	SCION	ŝ	!	lone
		5-1	24/12	0-2.0	4-8-26-24	0.8/0.8	Top 4": Brown TOPSOIL and ORGANICS.		TOPS	DIL	1		
1							fine to coarse SAND, some	fine to	0.8'				
2								•					
3		-											
			-						FINE	то			
4		s-2	24/10	4-0-6-0	26-48-49-37	0.8/0.8	Venu dense broug and	222700039	COARS	SE )			
_			- 17 12		20 40 47 57	0.0/0.8	fine to coarse SAND and fil coarse GRAVEL trace Silt	ne to	GRAVE	EL			
-	_	s-3	24/17	6.0-8.0	37-22-50-34	0.8/0.8	Top 9": Brown, fine to coar and fine to coarse GRAVEL	rse SAND	_				
		_					Silt. Bottom 8": Orange to brown,	fine	6.8'				
ł							SAND, little fine to coarse Gravel, little Silt.	•	FINE				2
<sup>3</sup>		s-4	24/18	8.0-10.0	14-9-9-15	0.8/0.8	Medium dense, brown, fine t	0	8.01		2		1
L				_			coarse SAND and fine to coa GRAVEL, little Silt.	irse	FINE	ro	-		
L	_								COARS	E ND			
$\mathbf{b}$	-		-		_				GRAVE	L	3		
$\left  \right $	-		_				3 <b>%</b> /		10.0' E.O.B		1		
ᆘ	-	-									1		
, İ				a la constante de la constante									
5	_												-
+	-	-											
+													
F	-	-											
t	1. s	oils	amples	field scre	ened for vola	tile order	ic compounds with an 11 7	W postable	Wu Nodel	D1-10			
LUNY	PPS B	photoi pm = ample oring	onizati parts p wet at ended	on detecto per million approxima at approxi	tely 10 feet 1 mately 10 feet	below grac t below grac	le. ade. E.O.B. = End of Borir	e of backgro	und condi	tions.	1		
ra	tific	ation	lineș	represent	approximate b	oundaries	between soil types, transi	tions may be	gradual.	Wate	r l	evel read	ings
os	e pre	sent	at the	time measu	er conditions rements were	stated. made.	Fluctuations of groundwate	r may occur	due to fa	ctors	oth	er than	
-		-									BOR	ING NO.	<u>B-8</u>

Barling mills read         Differentiation         File NO. 2064/2000           rg Co. GZA Drilling Type         ZAM HSA Solit Spoon         GROUNDWATER READINGS           rg Co. GZA Drilling Type         ZAM HSA Solit Spoon         GROUNDWATER READINGS           Rep. L. McKee, P. Crowell         Hammer Vt100.0.         13/247/21         Date         Cost in a stab. T           Ker, Datum Other         Other         Join         Join         Cost in a stab. T           tow         Datum         Other         SAMPLE         Sample Information	E	ngine	ers a	nd Scie	ntists			141 Danb	ury Road				1	PAGE 1	<u>B-9</u> OF 1
CASING         SAMPLER         GROUNDATER READINGS           man         Con Holman         1.0./0.0.         13/847/21         Date         Time         Dept         Easing         Stat.         6/13/92          9.0         8.0/         0 hr           Rep.         1Mokee. P. Crowell         Hammer Wt.         1400 lbs.         6/13/92          9.0         8.0/         0 hr           Start         6/13/92         End 6/13/92         Hammer Wt.         1400 lbs.         6/13/92          9.0         8.0/         0 hr           Start         6/13/92         Datum         Other          9.0         8.0/         0 hr           See plan          Datum         Other          9.0         8.0/         0 hr           See plan           0.6/0.6         1500 ml 21:5000, fine to coarse GRAVEL, trace         10.087/04         Field         0.3/            0.3/                          <	2 T	04 Sp rumbu 203)	ill, C 268-0	Hill Ro onnecti 808	ad cut 06611			Wilton, Co	nnecticut				ł	CHKD. BY:	50642 JMB
man       Ron Holman       1.0./0.0.       1 3/8*/2*       Date       Time       Depth       Casing Stab. T         Rep.       6/13/92       End 6/13/92       Hammer Ht.       140 lbs.       6/13/92       9.0'       8.0'       0 hr         Start       6/13/92       End 6/13/92       Hammer Ht.       140 lbs.       6/13/92       9.0'       8.0'       0 hr         Start       Datum       Other       30 in.        9.0'       8.0'       0 hr         Start       Datum       Other       Start        9.0'       8.0'       0 hr         Start       See plan           9.0'       8.0'       0 hr         Start       Beptin       Blows/6'       Field       DESCRIPTION & CLASSIFICATION       Stratum       R       Equipment         Start       24/16       2.0-4.0       16-20-17-17       0.6/0.6       Dense, brown, fine to ccarse SAND       Start       0.3'        Start       FINE TO       CLASSIFICATION       CASSIF       Start        0.4/12         None	Boi	ring	Co.	GZADr	illing	т	уре	CASING 2%" HSA	<u>SAMPLER</u> Split Spoon		GROUN	DWATER	RE	ADINGS	
Rep.       L. MCKEe, P. Crowell       Hammer Wt.       140 lbs.       6/13/92        9.0'       8.0'       0 hr         Start	Foi	reman		Ron Ho	lman	I	.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab.
Start	GZ/	A Rep		L. McK	ee, P. Cro	well H	ammer Wt.		140 lbs.	6/13/92		9.0'		8.0'	0 hr
Lev.       Datum       Other         ion       See plan       SAMPLE       SAMPLE         is       Sample Information       Field       DESCRIPTION & CLASSFICATION       Stratum       R         is       Depth       Blows/6"       Testing       DESCRIPTION & CLASSFICATION       Stratum       R         is       2       1       1       Stratum       Stratum       R       Equipment         is       2       1       1       Stratum       Stratum       None       None         is       2       1       1       Stratum       Stratum       Stratum       None         is       1       2       1       1       Stratum       Stratum       Stratum       Stratum       None         is       2       1       1       1       Stratum	Dat	te St	art	6/13/	92 End	6/13/92 H	ammer Fal		30 in.						
See plan       Sample Information       Equipment       Equipment         8       Sample Information       Field       DESCRIPTION & CLASSIFICATION       Stratum       Equipment         8       5-1       24/16       0-2.0       3-6-8-12       0.6/0.6       DESCRIPTION & CLASSIFICATION       Stratum       Equipment         9       -	S.	.Elev			Datum	0	ther								
Sample Information         SAMPLE         SAMPLE         SAMPLE         Stratum         Equipment Installed           No.         Pen./         Depth Rec.         Blows/6"         Field Testing (ppm)         DESCRIPTION & CLASSIFICATION         Stratum         Equipment Installed           S-1         24/16         0.3 - 6-8-12         0.6/0.6         Top 4": Brown to black TOPSDIL. Bottom 2011 Brown, fine to coarse SAMD and fine to coarse GANVEL, trace         TOPSDIL         0.3'           S-2         24/16         2.0 -4.0         16-20-17-17         0.6/0.6         Dense, brown, fine to coarse GANVEL, trace         0.3'           S-3         24/18         4.0-6.0         23-22-29-30         0.6/0.6         Silt         Dense, brown, fine to coarse GANVEL, trace         FINE TO COARSE           S-3         24/18         4.0-6.0         23-22-29-30         0.6/0.6         Silt         Silt         Fine to coarse GANVEL, trace         Silt         Fine to coarse GANVEL, trace         Silt           S-4         24/16         6.0-8.0         44-37-54-50         0.6/0.6         Yery dense, brown, fine to coarse GANVEL, trace         B.0' FINE SAND         B.5'         Fine TO COARSE         SAND         GANVEL         S.5'         SAND, trace Silt         B.0', FINE SAND         B.	.00	catio	n	See pl	an										
No.         Pen./ Rec.         Depth (ft.)         Blows/6"         Field Testing (ppm)         DESCRIPTION S LASSIFICATION         Straum Description K         Straum Description K           5-1         24/16         0-2.0         3-6-8-12         0.6/0.6         Top A": prown file to coarse GRAVEL, Top A": prown file to coarse GRAVEL, title Sit.         TOPSOIL         0.3'           5-2         24/16         2.0-4.0         16-20-17-17         0.6/0.6           5-3         24/18         4.0-6.0         23-22-29-30         0.6/0.6           5-4         24/16         6.0-8.0         44-37-54-50         0.6/0.6           5-5         24/18         8.0-10.0         21-13-12-12         0.2/0.6           5-5         24/18         8.0-10.0         21-13-12-12         0.2/0.6           5-5         24/18         8.0-10.0         21-13-12-12         0.2/0.6           5-5         24/18         8.0-10.0         21-13-12-12         0.2/0.6           5-1         24/16         6.0-8.0         44-37-54-50         0.5/0.6           5-5         24/18         8.0-10.0         21-13-12-12         0.2/0.6           10.0/2         21-13-12-12         0.2/0.6         50-57           20.1         10.0/2         50-57 </td <td></td> <td>СВ</td> <td></td> <td>S</td> <td>ample Infor</td> <td>rmation</td> <td></td> <td>a contraction of the second</td> <td></td> <td></td> <td></td> <td>1000</td> <td>R</td> <td>Equ</td> <td>ipment</td>		СВ		S	ample Infor	rmation		a contraction of the second				1000	R	Equ	ipment
S-1       24/16       0-2.0       3-6-8-12       0.600.6       Top 4": Brown to black TOPSOIL. Bottom 12": Brown fire to coarse settom 12": Brown fire to coarse SAND and fire to coarse GRAVEL, trace sitt.       0.3"         S-2       24/16       20-4.0       16-20-17-17       0.6/0.6         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         SAND       A       A       A       Bottom 12": Brown, fine to coarse SAND       B.0' FINE SAND S.5' IE         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Bottom 12": Brown, fine to c		SNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIF	TION & CLASSIF	ICATION	Stra Descri	tum ption	<b>H</b> MKS	Ins	talled
Bottom 121: Brown, fine to coarse GRAVEL,         S-2       24/16       2.0-4.0       16-20-17-17       0.6/0.6         Bottom 121: Brown, fine to coarse GRAVEL,       111112       11112       11112         S-2       24/16       2.0-4.0       16-20-17-17       0.6/0.6       Dense, brown, fine to coarse GRAVEL, trace       FINE TO COARSE SAND and fine to coarse GRAVEL, trace         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Dense, brown, fine to coarse GRAVEL, trace       FINE TO COARSE SAND and fine to coarse GRAVEL, trace         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Dense, brown, fine to coarse GRAVEL, trace       SND         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Dense, brown, fine to coarse GRAVEL, trace       SND         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.       S.0' FINE SAND         S-4       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Top 6'': Grey, fine SAND, some fine to coarse GRAVEL, trace Silt.       S.5'       FINE TO COARSE SAND         SAND       SAND       SAND, trace Silt.       S.5'       FINE TO COARSE SAND       SAND         SAND       SAND       SAND, trace Silt.			s-1	24/16	0-2.0	3-6-8-12	0.6/0.6	Top 4": Brow	n to black TOP	SOIL.	TOPS	OIL	1	1.0	
Image: S-2       24/16       2.0-4.0       16-20-17-17       0.6/0.6       Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt.         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt.         S-3       24/16       6.0-8.0       23-22-29-30       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/18       8.0-10.0       21-13-12-12       0.2/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         SAND       And       SAND       SAND       8.5'         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         SAND       SAND       SAND       SAND         SAND       SAND       SAND       8.0'         Sub       Unit Silt       Silt								Bottom 12": SAND and fir	Brown, fine to e to coarse GR	AVEL,	0.3'		11		
S-2       24/16       2.0-4.0       16-20-17-17       0.6/0.6         a	1							little Silt.		1919-1919	104764				
S-2       24/16       2.0-4.0       16-20-17-17       0.6/0.6       and fine to coarse GRAVEL, trace         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Sitt.         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Sitt.         S-3       24/16       6.0-8.0       23-22-29-30       0.6/0.6       Sitt.       Sitt.         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.       8.0' FINE SAND         SAD       0.4/0.6       SAND       Tace Silt.       SAND, trace Silt.       8.5'         SAD       0.4/0.6       SAD, trace Silt.       SAD, trace Silt.       8.0' FINE SAND         SAD       SAD       SAD       SAD       SAD       8.0' FINE SAND         SAD       SAD       SAD       SAD       SAD       8.0' FINE SAND         SAD       SAD       SAD       SAD       SAD       8.0' FINE SAND	2														
a       a	2		s-2	24/16	2.0-4.0	16-20-17-17	0.6/0.6	Dense, brown	, fine to coar	se SAND	1				
s-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       pense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt.       FINE TO COARSE SAND and fine to coarse GRAVEL, trace Silt.         s-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.       FINE TO COARSE SAND and fine to coarse GRAVEL, trace Silt.         s-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.       SAND and fine to coarse GRAVEL, trace Silt.         s-4       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.       8.0' FINE SAND         s-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       SAND, trace Silt.       8.0' FINE SAND       8.5'         s-1       0.4/0.6       SAND, trace Silt.       3       10.0'       8.5'       5AND         s-1       0.2       0.2       0.2       0.2       0.2       0.2       0.2         s-2       0.2       0.2       0.2       0.2       0.2       0.2       0.2       0.2         s-2       0.2       0.2       0.2       0.2       0.2       0.2       0.2         s-3       0.2	z							Silt.	coarse GRAVEL,	trace	1				
S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6         S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6         S-4       S44       Silt.       Dense, brown, fine to coarse GRAVEL, trace       SAND         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         SAND, trace Silt.       Top 6": Grey, fine SAND, some fine to coarse SAND, trace Silt.       8.0' FINE SAND         2       0.4/0.6       SAND, trace Silt.       2         3       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND         2       2       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND         3       2       2       0.6/0.6       3       3         2       2       2       0.6/0.6       3       3         3       2       2       2       2       3         4       4       4       4       4       4       4         4       4 <td>2</td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>TO</td> <td>  </td> <td></td> <td></td>	2					-						TO			
S-3       24/18       4.0-6.0       23-22-29-30       0.6/0.6       Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace       AND         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace       Sitt.         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace       Sitt.         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Top 6": Grey, fine SAND, some fine to coarse GRAVEL, trace Silt.       8.0' FINE SAND       8.5'         SAND       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND       8.5'       8.5'         SAND       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND       8.5'       8.5'       8.5'         SAND       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND       8.5'       8.5'       8.0' FINE SAND       8.5'         SAND       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND       8.0'       8.0'       8.0'       8.5'       8.0'       8.0'       8.5'       8.0'       8.5'       8.0'       8.5'       8.0'       8.0'       8.0'       8.0'       8.5'       8.0'       8.0'       8.5'       8.0'       8.0'	4										COAR	SE			
Image: Single interviewed	-		s-3	24/18	4.0-6.0	23-22-29-30	0.6/0.6	Dense, brown	, fine to coar	se SAND	AND	)			
S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         SAND and fine to coarse GRAVEL, trace Silt.       Top 6": Grey, fine SAND, some fine to coarse Gravel, little Silt.       8.0' FINE SAND         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         O.4/0.6       SAND, trace Gravel, little Silt.       8.5'       Fine TO COARSE SAND         SAND       SAND, trace Silt.       8.5'       Fine TO COARSE SAND         SAND       SAND       SAND, trace Silt.       8.0' FINE SAND         SAND       SAND       SAND       SAND	5							Silt.	coarse GRAVEL,	crace	GRAV	eL			
S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         Top 6": Grey, fine SAND, some fine to coarse Gravel, little Silt.       8.0' FINE SAND         SAND, trace Silt.       SAND, trace Silt.       8.0' FINE SAND         SAND       SAND, trace Silt.       8.0' EINE SAND         SAND       SAND, trace Silt.       8.0' EINE SAND         SAND       SAND       SAND, trace Silt.	1										1				
S-4       24/16       6.0-8.0       44-37-54-50       0.6/0.6       Very dense, brown, fine to coarse GRAVEL, trace Silt.         SAND and fine to coarse GRAVEL, trace Silt.       Image: Sand fine to coarse GRAVEL, trace Silt.       Image: Sand fine to coarse GRAVEL, trace Silt.         S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         Month of the to coarse Gravel, Little Silt.       Image: Sand fine to coarse Gravel, Little Silt.       8.0' FINE SAND         Image: Sand fine to coarse Gravel, Little Silt.       Solve fine to coarse Gravel, Little Silt.       8.5'         Image: Sand fine to coarse Gravel, Little Silt.       Sand fine to coarse Gravel, Little Silt.       8.5'         Image: Sand fine to coarse Gravel, Little Silt.       Sand fine to coarse Gravel, Little Silt.       8.5'         Image: Sand fine to coarse Gravel, Little Silt.       Sand fine to coarse Gravel, Little Silt.       8.0' FINE Sand Coarse Gravel, Little Silt.         Image: Image: Sand fine to coarse Gravel, Little Silt.       Image:	6														
S-5     24/18     8.0-10.0     21-13-12-12     0.2/0.6       0.4/0.6     0.4/0.6     Bottom 12*     SAND, some fine to coarse Gravel, little Silt.       1     0.4/0.6       2     0.4/0.6       1     0.4/0.6       2     0.4/0.6       1     0.4/0.6       2     0.4/0.6       1     0.4/0.6       2     0.4/0.6       1     0.4/0.6       1     0.4/0.6       1     0.4/0.6       2     0.4/0.6       10.0'       2     0.4/0.6       2     0.4/0.6       10.0'       2     0.4/0.6       2     0.4/0.6       2     0.4/0.6       2     0.4/0.6       3     10.0'       2     0.4/0.6       10.0'     10.0'       2     0.4/0.6       2     0.4/0.6       3     0.4/0.6       3     0.4/0.6       4     0.4/0.6       5     0.4/0.6       5     0.4/0.6       10.0'     10.0'       2     0.4/0.6       10.0'     10.0'       10.0'     10.0'       10.0'     10.0'       10.0'	-	-	s-4	24/16	6.0-8.0	44-37-54-50	0.6/0.6	Very dense, SAND and fin	brown, fine to	coarse					
S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Top 6": Grey, fine SAND, some fine to coarse Gravel, little Silt.       8.0' FINE SAND       2	7							trace Silt.							
S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6         0.4/0.6       0.4/0.6       0.4/0.6       8.5'       8.0' FINE SAND         0.1       0.4/0.6       SAND, trace Silt.       8.0' FINE SAND         0.1       0.4/0.6       0.4/0.6       8.5'       5'         0.1       0.4/0.6       0.4/0.6       8.0' FINE SAND       8.5'         0.1       0.1       0.4/0.6       8.0' FINE SAND       8.0' FINE SAND         1       1       1       1       1       1         1       1       1       1       1       1         1       1       1       1       1       1       1         1       1       1       1       1       1       1         1       1       1       1       1       1       1         1       1       1       1       1       1       1         1       1       1       1       1       1       1       1         1       1       1       1       1       1       1       1       1         1       1       1       1       1       1       1															
S-5       24/18       8.0-10.0       21-13-12-12       0.2/0.6       Top 6": Grey, fine SAND, some fine to coarse Gravel, little Silt.       8.0' FINE SAND       2         Image: Solution of the sol	8	-					-		- 22	12				5	
0.4/0.6     Bottom 12": Brown, fine to coarse     8.5'       SAND, trace Silt.     FINE TO COARSE SAND			S-5	24/18	8.0-10.0	21-13-12-12	0.2/0.6	Top 6": Grey to coarse Gr	, fine SAND, s avel, little S	ome fine ilt.	8.0' FIN	E SAND	2		
COARSE     3       Image: Sand     10.0'       Image: Sand     10.0' </td <td>9</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.4/0.6</td> <td>SAND, trace</td> <td>Brown, fine to Silt.</td> <td>coarse</td> <td>8.5' FINE</td> <td>то</td> <td></td> <td></td> <td></td>	9						0.4/0.6	SAND, trace	Brown, fine to Silt.	coarse	8.5' FINE	то			
Image: 10.0'     3       Image: 10.0'     5.0.8.       Image: 10.0'     5.0.8.	$\mathbf{I}$						-				COAR	SE D			
	0										10.01		3		
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	t														
. Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101	2 -	1.	Sọil s	şamples	field scre	eened for vola	tile orga	nic compounds	with an 11.7	eV portable	HNu, Mode	L PI-10	01		
	ra Ve	atifi e bee	cation n made	n lines e at ti	represent mes and und	approximate b	oundaries stated.	between soi Fluctuation	types, trans	itions may be er may occur	e gradual due to f	. Wat	er	level rea	dings
ification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings	05	se pr	esent	at the	time measu	urements were	made.	. tastaat ron	an groundwat	er may occur		Γ	BO	RING NO	B-9
ification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than present at the time measurements were made.	_												50	no.	

SE 2T	04 S	pring	Hill R	entists oad icut 0661	1		141 Dani	oury Road					BORING NO PAGE 1 FILE NO.	0- <u>B-10</u> 0F_1 50642
Ċ	203)	268-0	808				Wilton, Co	onnecticut					CHKD. BY:	JMB
0	ring	Co.	GZA D	<u>rilling</u>		Туре	CASING 2%" HSA	SAMPLER Split Spoon		GROUN	IDWATER	RE	EADINGS	
7	Renal	1		olman Koo P Cr		I.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. Ti
a1	te St	art	6/13	/92 End	6/13/02	Hammer Wt.	·	<u>140 lbs.</u>	6/13/92		6.5	'	4.0'	0 hrs
s.	Elev	<i>.</i>		Datum	0/10/92	Other		<u>30 in.</u>						
00	atio	n	See pl	lan –		other			*					
1	CB		S	ample Info	ormation			Parata and Parata and				P	Eau	
	SNGS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSIF	ICATION	Stra Descri	tum otion	NX KIN	Ins	talled
		s-1	24/7	0-2.0	4-7-3-3	0.6/0.6	Top 4": Brow	n to black TOP	SOIL.	TOPS	DIL	1		
1		-					SAND and fir	ne to coarse GR/	coarse AVEL,	0.31				
2	100	S-1A	24/3	2 0-4 0	7-8-7-7	0.610.6								
ł				2.0 4.0	1-0-1-1	0.6/0.6	some fine to	, brown, fine s coarse Gravel,	SAND, little					
İ							Sitt.			FIN	Ę			
										(ORGAN	ICS			
L	_	s-2	24/2	4.0-6.0	1-3-4-7	0.8/0.6	Loose, brown	to black, fine	SAND,	TROM 4	0.7			
ŀ	_						little fine Silt.	Gravel, little	organic					
ŀ	_													
┝		. 7	24.440						_					
F	-	5-3	24/10	6.0-8.0	14-17-14-27	0.6/0.6	Dense, brown, and fine to d	, fine to coars coarse GRAVEL.	e SAND some	6.0'		2		
ŀ	-						Silt.	TTER 194. ANNO200111	2862281	FINE	TO E			
ŀ	-									SAND				
									ŀ	8.0/		3	3	
				-						E.O.B	.			
-	-													
-	-													
-	-	-												
-	-	-												
-	-	-												
	-													
_														
NA <sup>1</sup>		1		_										
1	S P P S B	oil sa hotoic pm = p ample oring	ended a	field scree on detecto er million approximat at approxim	ened for vola r. 1/0.8 = m tely 6.5 feet mately 8 feet	tile organ eter respo below gra below gra	nic compounds onse of sample de. de. E.O.B. =	with an 11.7 e e/meter reponse	V portable H of backgrou	Nu Model Ind condi	PI-101 tions.			
at	ific	ation made	lines at time	represent a	approximate b	oundaries	between soil	types, transit	ions may be	gradual.	Water	- 10	evel read	ings
se	pre	sent a	t the	time measur	rements were i	made.	ructuations	of groundwater	may occur d	ue to fac	tors o	othe	er than	
											E	SOR	ING NO.	3-10

GE	ZA GE	OENVI	RONMEN nd Sci	TAL, INC. entists			141 Danbury Road					BORING NO	. <u>B-11</u>
2	04 Sp rumbu 203)	oring ull C 268-0	Hill Ro connect 808	oad icut 0661	1		Wilton, Connecticut	-				PAGE 1 FILE NO. CHKD. BY:	OF 1 50642 JMB
Bo	ring	co.	GZA D	rilling		Туре	CASING SAMPLER		GROUN	DWATER	RE	ADINGS	
Foi	remar	1	Ron He	olman		I.D./O.D.	1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab.
GZ/	Rep		L. Mcl	Kee, P. Cr	owell	Hammer Wt.	140 lbs.	6/13/92		10.0	,	8.0'	0 hr
Dat	e St	art	6/13/	/92 End	6/13/92	Hammer Fal	l 30 in.						
GS.	Elev			Datum_		Other							
Loc	atio	n	See pl	lan									
D	СВ		S	ample Info	ormation	Contraction of the					R	Equ	ioment
	ASWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	SAMPLE DESCRIPTION & CLASSIF	ICATION	Stra Descri	tum ption	EMK	Ins	talled
-		s-1	24/12	0.3-2.3	16-13-7-5	0.6/0.6	Medium dense brown fine (	CAND	4000	AL 7	5		ione
	-						some fine Gravel, trace Sil	lt.	ASPH		1'		
1							spoon).	OT	0.37				
						-			1				
2													
ł	_												
3	_								FINE	то			
ł		-							COAR	SE			
4	-	0.2	24.72	1010	17 44 64 45				AND GRAVI	EL			
ł	_	S-2	24/2	4.0-6.0	17-14-21-19	0.4/0.6	Dense, brown, coarse GRAVEL	•	(ORGAI	VIC			
5	-		-						AT 2	')			
ł	-	-											
s	_												
F	_	s-3	24/14	6.0-8.0	22-31-30-27	0.6/0.6	Very dense, brown, fine to	coarse					
7	_						trace Silt.	v,					
+	_												
₃┝													
F	-	s-4	24/16	8.0-10.0	42-45-30-20	0.4/0.6	Top 8": Grey, fine to coarse	e			2		
,	-						Silt.	fina					
L	_						to coarse SAND, some fine G	ravel,					
							tittle sitt.						
L	_								10.0'		5		
			-	-					E.O.B	•			
L													
L													
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L				-	_	_							
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Ľ													
					-								
1	. s	oil sa	amples	field scre	ened for vola	tile organ	ic compounds with an 11.7 e	V portable H	Nu Model	PI-10	1		
NN		ample oring	onizati parts p wet at ended	on detecto per millior approxima at approxi	or. 1/0.8 = m h. htely 10 feet mately 10 fee	neter respo below grac t below gr	onse of sample/meter reponse e. ade. E.O.B. = End of Borin	e of backgrou g.	und condi	tions.			
at /e	ific	ation made	lines at tim	represent	approximate b	oundaries	between soil types, transit	ions may be	gradual.	Wate	r l	evel read	ings
ose	pre	sent a	at the	time measu	rements were	made.	rectuations of groundwater	may occur o	que to fa	ctors	oth	er than	
											BOR	ING NO.	B-11

#### TABLE 1 GROUNDWATER ELEVATION DATA: 11/2/93 141 DANBURY ROAD WILTON, CONNECTICUT

LOCATION	REFERENCE ELEVATION	DEPTH TO WATER (FT)	WATER TABLE ELEVATION
MW-1	00.14	12.60	96 54
MW-2	100.57	14.33	86.24
MW-3	98.56	12.18	86.38
MW-4	96.24	10.51	85.73
MW-5	94.53	9.24	85.29
MW-6	96.43	11.35	85.08
MW-7	94.73	9.75	84.98
MW-8	88.89	4.00	84.89

NOTES:

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1. Reference elevation: are top of PVC monitor wells based on relative

difference to an arbitrary benchmark established on center of a manhole cover along the eastern property line which was assumed to be 100 feet above mean sea level.

# **Tighe&Bond**

**APPENDIX C** 





Name: EX-WS-01

Location: Southern Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	1.932	98	189.314
Landscaped and Lawns	0.872	69	60.183
			249.497

 Total Area:
 2.804
 CN:
 89

Time of Concentration:

	Sheet-Flow Travel Time											
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)							
A-B	0.24	3.54	100	0.015	15.2							

	Shallow Concentrated Flow Travel Time												
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)								
B-C	Paved	580	0.020	2.87	3.4								

Total Tc (min) = 18.6

Name: EX-WS-02

Location: No

Northern Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.059	98	5.739
Landscaped and Lawns	1.040	69	71.728
			77.467

Total Area: 1.098 CN: 71

Time of Concentration:

	Sheet-Flow Travel Time												
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)								
A-B	0.24	3.54	130	0.035	13.4								

Shallow Concentrated Flow Travel Time								
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)			
B-C	Unpaved	410	0.020	2.28	3.0			

Total Tc (min) = \_\_\_\_\_16.4

References: NRCS Technical Release 55 ConnDOT Drainage Manual, Chapter 6



Name: EX-RF-01

Location: Existing Building

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.775	98	75.932
Landscaped and Lawns	0.000	69	0.000
			75.932
Total Area:	0.775	CN:	98

Time of Concentration:

Sheet-Flow Travel Time							
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)		
A-B	0.015	3.54	60	0.015	1.1		

Total Tc (min) = <u>1.1</u> Minimum Tc = <u>5.0</u>

References: NRCS Technical Release 55 ConnDOT Drainage Manual, Chapter 6



#### Legend

<u>Hyd.</u>	<u>Origin</u>	<b>Description</b>
1	SCS Runoff	EX-WS-01
2	SCS Runoff	EX-WS-02

3 SCS Runoff EX-RF-01

4 Combine TOTAL - EXISTING

# Hydrograph Return Period Recap Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd.	Hydrograph	Inflow	Peak Outflow (cfs)						Hydrograph Description		
140.	(origin)	liyu(3)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			5.474			9.316	11.72	13.50	15.39	EX-WS-01
2	SCS Runoff			0.975			2.287	3.202	3.910	4.680	EX-WS-02
3	SCS Runoff			2.573			3.949	4.812	5.454	6.139	EX-RF-01
4	Combine	1, 2, 3		7.662			13.50	17.25	20.05	23.05	TOTAL - EXISTING
<u> </u>		L		L	1						

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	5.474	2	732	24,369				EX-WS-01
2	SCS Runoff	0.975	2	732	4,233				EX-WS-02
3	SCS Runoff	2.573	2	724	8,720				EX-RF-01
4	Combine	7.662	2	730	37,453	1, 2, 3			TOTAL - EXISTING
FO	73-02 Hvdroc	Tranhs - F			Return P	eriod: 2 Ye	ar	Monday 05	/ 24 / 2021
1.0		,							. = =

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

EX-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 5.474 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 24,369 cuft
Drainage area	= 2.804 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 18.60 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 2

EX-WS-02

Hydrograph type	= SCS Runoff	Peak discharge	= 0.975 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 4,233 cuft
Drainage area	= 1.098 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 16.40 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 3

EX-RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.573 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 8,720 cuft
Drainage area	= 0.775 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 4

TOTAL - EXISTING

= Combine	Peak discharge	= 7.662 cfs
= 2 yrs	Time to peak	= 730 min
= 2 min	Hyd. volume	= 37,453 cuft
= 1, 2, 3	Contrib. drain. area	= 4.677 ac
	= Combine = 2 yrs = 2 min = 1, 2, 3	= CombinePeak discharge= 2 yrsTime to peak= 2 minHyd. volume= 1, 2, 3Contrib. drain. area



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# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	9.316	2	732	42,301				EX-WS-01
2	SCS Runoff	2.287	2	732	9,417				EX-WS-02
3	SCS Runoff	3.949	2	724	13,616				EX-RF-01
4	Combine	13.50	2	730	65,561	1, 2, 3			TOTAL - EXISTING
F01	I73-02 Hydrog	ıraphs - E	Existing.	]pw	Return P	eriod: 10 Y	ear	Monday, 05	5 / 24 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

EX-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 9.316 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 42,301 cuft
Drainage area	= 2.804 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 18.60 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 2

EX-WS-02

Hydrograph type	= SCS Runoff	Peak discharge	= 2.287 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 9,417 cuft
Drainage area	= 1.098 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 16.40 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Monday, 05 / 24 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 3

EX-RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 3.949 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 13,616 cuft
Drainage area	= 0.775 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Monday, 05 / 24 / 2021
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 4

TOTAL - EXISTING

= Combine	Peak discharge	= 13.50 cfs
= 10 yrs	Time to peak	= 730 min
= 2 min	Hyd. volume	= 65,561 cuft
= 1, 2, 3	Contrib. drain. area	= 4.677 ac
	= Combine = 10 yrs = 2 min = 1, 2, 3	= CombinePeak discharge= 10 yrsTime to peak= 2 minHyd. volume= 1, 2, 3Contrib. drain. area



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	11.72	2	732	53,834				EX-WS-01
2	SCS Runoff	3.202	2	730	13,075				EX-WS-02
3	SCS Runoff	4.812	2	724	16,698				EX-RF-01
4	Combine	17.25	2	730	83,894	1, 2, 3			TOTAL - EXISTING
	73-02 Hvdroc				Return D	eriod: 25 V		Monday 05	- 10 I / 24 / 2021
		jiapris - E	sisting.	Jhm	Return P	enou: 25 Y	eal	wonday, 05	0 / 24 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

EX-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 11.72 cfs
Storm frequency	= 25 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 53,834 cuft
Drainage area	= 2.804 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 18.60 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 2

EX-WS-02

Hydrograph type	= SCS Runoff	Peak discharge	= 3.202 cfs
Storm frequency	= 25 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 13,075 cuft
Drainage area	= 1.098 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 16.40 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 3

EX-RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 4.812 cfs
Storm frequency	= 25 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 16,698 cuft
Drainage area	= 0.775 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type =	= Combine	Peak discharge	= 17.25 cfs
Storm frequency =	= 25 yrs	Time to peak	= 730 min
Time interval =	= 2 min	Hyd. volume	= 83,894 cuft
Inflow hyds.	= 1, 2, 3	Contrib. drain. area	= 4.677 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	13.50	2	732	62,477				EX-WS-01
2	SCS Runoff	3.910	2	730	15,920				EX-WS-02
3	SCS Runoff	5.454	2	724	18,991				EX-RF-01
4	Combine	20.05	2	730	97,722	1, 2, 3			TOTAL - EXISTING
	Combine	20.05	2	730	91,122	1, 2, 3			
<b>F01</b>	73-02 Hydrog	graphs - E	Existing.q	gpw	Return P	eriod: 50 Y	ear	Monday, 05	6 / 24 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

EX-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 13.50 cfs
Storm frequency	= 50 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 62,477 cuft
Drainage area	= 2.804 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 18.60 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 2

EX-WS-02

Hydrograph type	= SCS Runoff	Peak discharge	= 3.910 cfs
Storm frequency	= 50 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 15,920 cuft
Drainage area	= 1.098 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 16.40 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 3

EX-RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 5.454 cfs
Storm frequency	= 50 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 18,991 cuft
Drainage area	= 0.775 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type	= Combine	Peak discharge	= 20.05 cfs
Storm frequency	= 50 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 97,722 cuft
Inflow hyds.	= 1, 2, 3	Contrib. drain. area	= 4.677 ac



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# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	15.39	2	732	71,759				EX-WS-01
2	SCS Runoff	4.680	2	730	19,050				EX-WS-02
3	SCS Runoff	6.139	2	724	21,442				EX-RF-01
4	Combine	23.05	2	730	112,636	1, 2, 3			TOTAL - EXISTING
F01	73-02 Hydrog	graphs - E	Existing.	gpw	Return P	eriod: 100	Year	Monday, 05	/ 24 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

EX-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 15.39 cfs
Storm frequency	= 100 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 71,759 cuft
Drainage area	= 2.804 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 18.60 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 2

EX-WS-02

Hydrograph type	= SCS Runoff	Peak discharge	= 4.680 cfs
Storm frequency	= 100 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 19,050 cuft
Drainage area	= 1.098 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 16.40 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 3

EX-RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 6.139 cfs
Storm frequency	= 100 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 21,442 cuft
Drainage area	= 0.775 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 4

TOTAL - EXISTING

Hydrograph type =	= Combine	Peak discharge :	= 23.05 cfs
Storm frequency =	= 100 yrs	Time to peak =	= 730 min
Time interval	= 2 min	Hyd. volume :	= 112,636 cuft
Inflow hyds.	= 1, 2, 3	Contrib. drain. area	= 4.677 ac



# **Tighe&Bond**

APPENDIX D





Location: Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.007	98	0.720
Landscaped and Lawns	0.187	69	12.880
			13.600
Total Area:	0.194	CN:	70

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	130	0.030	14.2

Total Tc (min) = 14.2

Name: CB-01A

Location: Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.024	98	2.362
Landscaped and Lawns	0.080	69	5.512
			7.875
Total Area:	0.104	CN:	76

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min)					
A-B	0.24	3.54	50	0.020	7.8

Total Tc (min) = 7.8



Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.043	98	4.207
Landscaped and Lawns	0.011	69	0.775
			4.982
Total Area:	0.054	CN:	92

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (m					
A-B	0.015	3.54	98	0.050	1.0

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0

Name: CB-03

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.051	98	5.035
Landscaped and Lawns	0.023	69	1.560
			6.595
Total Area:	0.074	CN:	89

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft)				Slope (ft/ft)	Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	60	0.033	0.8

Total Tc (min) = 4.5 Minimum Tc = 5.0



Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.045	98	4.439
Landscaped and Lawns	0.011	69	0.767
			5.205
Total Area:	0.056	CN:	92

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (m					Time (min)	
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	55	0.045	0.7	

 Total Tc (min) =
 4.4

 Minimum Tc =
 5.0

Name: CB-05

Location:

Proposed Catch Basin - Driveway

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.075	98	7.323
Landscaped and Lawns	0.041	69	2.827
			10.150
Total Aroa-	0 116	CN-	88
Total Area.	0.110	CN.	00

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (mir					Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	65	0.040	0.8

Total Tc (min) = 4.5 Minimum Tc = 5.0



Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.048	98	4.707
Landscaped and Lawns	0.014	69	0.965
			5.671
Total Area:	0.062	CN:	91

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (m					Time (min)
A-B	0.24	3.54	22	0.020	4.0
B-C	0.015	3.54	58	0.025	0.9

 Total Tc (min) =
 4.9

 Minimum Tc =
 5.0

Name: CB-07

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.080	98	7.879
Landscaped and Lawns	0.019	69	1.296
			9.174
Total Area	a: 0.099	CN:	93

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (m					Time (min)
A-B	0.24	3.54	15	0.020	3.0
B-C	0.015	3.54	115	0.035	1.3

Total Tc (min) = 4.3 Minimum Tc = 5.0



Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.095	98	9.280
Landscaped and Lawns	0.022	69	1.551
			10.831
Total Area:	0.117	CN:	92

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (mi					Time (min)
A-B	0.24	3.54	30	0.040	3.9
B-C	0.015	3.54	140	0.035	1.5

Total Tc (min) = 5.5

Name: CB-09

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.117	98	11.440
Landscaped and Lawns	0.020	69	1.405
			12.845
	0.407	0.1	
Total Area:	0.137	CN:	94

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (mi					Time (min)	
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	120	1.000	0.4	

 Total Tc (min) =
 4.1

 Minimum Tc =
 5.0



#### CB-10 Name:

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.103	98	10.095
Landscaped and Lawns	0.031	69	2.156
			12.251
Total Area	0 134	CN.	91
Total Area.	0.134	CN.	31

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min)						
A-B	0.24	3.54	30	0.040	3.9	
B-C	0.015	3.54	135	1.000	0.4	

 Total Tc (min) =
 4.3

 Minimum Tc =
 5.0

Name:

CB-11

Location: Proposed Yard Drain - Southeast Corner Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.000	98	0.000
Landscaped and Lawns	0.227	69	15.642
			15.642
Total Area:	0.227	CN:	69

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)				
A-B	0.24	3.54	130	0.050	11.6

Total Tc (min) = 11.6



#### Name: PP-01

Location: Proposed Porous Pavement - Southwest Parking Area

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.331	98	32.415
Landscaped and Lawns	0.018	69	1.248
			33.663
Total Area:	0.349	CN:	96

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)						
A-B	0.24	3.54	30	0.035	4.1	
B-C	0.015	3.54	100	0.020	1.5	

Total Tc (min) = 5.6

Name: PP-02

Location: Proposed Porous Pavement - Northwest Parking Area

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.400	98	39.247
Landscaped and Lawns	0.068	69	4.717
			43.964
Total Area:	0.469	CN:	94
Total Area:	0.469	CN	:

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min						
A-B	0.24	3.54	40	0.040	4.9	
B-C	0.015	3.54	60	0.016	1.1	

Total Tc (min) = 6.0



#### Name: RF-01

Location: Proposed Building - North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.571	98	55.997
Landscaped and Lawns	0.000	69	0.000
			55.997

Total Area: 0.571 CN: 98

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)					Time (min)
A-B	0.015	3.54	50	0.015	1.0

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0

Name: RF-02

Location: Proposed Building - South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.585	98	57.365
Landscaped and Lawns	0.000	69	0.000
			57.365
Total Area:	0.585	CN:	98

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)					Time (min)
A-B	0.015	3.54	50	0.015	1.0

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0



#### Name: RF-03

Location: Proposed Building - Northwest

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.138	98	13.485
Landscaped and Lawns	0.000	69	0.000
			13.485
Total Area:	0.138	CN:	98

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.015	3.54	50	0.015	1.0	

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0

Name: RF-04

Location: Proposed Building - Southwest

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.127	98	12.432
Landscaped and Lawns	0.000	69	0.000
			12.432
Total Area:	0.127	CN:	98

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.015	3.54	50	0.015	1.0	

Total Tc (min) = 1.0 Minimum Tc = 5.0



Name: PR-WS-01

Location: Site - West

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.065	98	6.385
Landscaped and Lawns	0.973	69	67.106
			73.490
Total Area:	1.038	CN:	71

Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	130	0.008	24.1

Shallow Concentrated Flow Travel Time								
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)			
B-C	Unpaved	240	0.013	1.80	2.2			
C-D	Paved	165	0.013	2.27	1.2			

Total Tc (min) = 27.6

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## Hydrograph Return Period Recap Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd.	. Hydrograph Inflow Peak Outflow (cfs)					Hydrograph					
No.	type (origin)	type hyd(s) origin)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			0.161			0.389	0.548	0.672	0.807	CB-01
2	SCS Runoff			0.150			0.317	0.428	0.513	0.604	CB-01A
3	SCS Runoff			0.159			0.259	0.321	0.366	0.415	CB-02
4	SCS Runoff			0.199			0.337	0.423	0.487	0.554	CB-03
5	SCS Runoff			0.165			0.268	0.332	0.380	0.431	CB-04
6	SCS Runoff			0.302			0.518	0.653	0.753	0.860	CB-05
7	SCS Runoff			0.177			0.292	0.364	0.417	0.473	CB-06
8	SCS Runoff			0.299			0.481	0.594	0.678	0.767	CB-07
9	SCS Runoff			0.344			0.560	0.695	0.794	0.900	CB-08
10	SCS Runoff			0.424			0.674	0.830	0.945	1.068	СВ-09
11	SCS Runoff			0.383			0.632	0.786	0.901	1.022	CB-10
12	SCS Runoff			0.198			0.490	0.697	0.858	1.034	CB-11
13	SCS Runoff			1.126			1.754	2.146	2.437	2.747	PP-01
14	SCS Runoff			1.452			2.308	2.841	3.235	3.655	PP-02
15	SCS Runoff			1.896			2.910	3.546	4.018	4.523	RF-01
16	SCS Runoff			1.942			2.981	3.633	4.117	4.634	RF-02
17	SCS Runoff			0.458			0.703	0.857	0.971	1.093	RF-03
18	SCS Runoff			0.422			0.647	0.789	0.894	1.006	RF-04
19	SCS Runoff			0.734			1.726	2.421	2.955	3.537	PR-WS-01
20	Combine	1, 2, 3,		0.703			1.351	1.778	2.102	2.450	COMBINE-1
21	Combine	5, 7, 8, 9,		2.910			4.708	5.855	6.713	7.633	COMBINE-2
22	Combine	12, 16, 20, 21		3.612			6.059	7.634	8.815	10.08	TO SOUTH INFIL SYS
23	Combine	4, 5, 10,		3.067			4.821	5.917	6.730	7.597	TO NORTH INFIL SYS
24	Reservoir	11, 15,		0.000			0.053	0.188	0.278	0.330	SOUTH POR PVMT
25	Reservoir	14		0.000			0.000	0.050	0.140	0.237	NORTH POR PVMT
26	Reservoir	22		0.013			1.750	3.418	4.661	6.520	SOUTH INFIL SYS
27	Reservoir	23		0.292			1.863	3.033	4.540	5.682	NORTH INFIL SYS
28	Combine	17, 18,		0.880			1.350	1.646	1.865	2.099	COMBINE-3
29	Combine	24, 25, 26,		0.880			3.943	7.202	10.05	13.89	SYSTEM OUTLET
30	Combine	19, 29		1.185			5.658	9.362	12.19	16.34	TOTAL SITE
Pro	i file: F0173.	-02 Hydroy	graphs -	Pronose	ad apw				 Т.,	esday 0	5 / 25 / 2021

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.161	2	732	709				CB-01
2	SCS Runoff	0.150	2	726	526				CB-01A
3	SCS Runoff	0.159	2	724	492				CB-02
4	SCS Runoff	0.199	2	724	603				CB-03
5	SCS Runoff	0.165	2	724	510				CB-04
6	SCS Runoff	0.302	2	724	910				CB-05
7	SCS Runoff	0.177	2	724	544				CB-06
8	SCS Runoff	0.299	2	724	934				CB-07
9	SCS Runoff	0.344	2	724	1,065				CB-08
10	SCS Runoff	0.424	2	724	1,340				CB-09
11	SCS Runoff	0.383	2	724	1,176				CB-10
12	SCS Runoff	0.198	2	730	831				CB-11
13	SCS Runoff	1.126	2	724	3,664				PP-01
14	SCS Runoff	1.452	2	724	4,588				PP-02
15	SCS Runoff	1.896	2	724	6,425				RF-01
16	SCS Runoff	1.942	2	724	6,582				RF-02
17	SCS Runoff	0.458	2	724	1,553				RF-03
18	SCS Runoff	0.422	2	724	1,429				RF-04
19	SCS Runoff	0.734	2	742	4,104				PR-WS-01
20	Combine	0.703	2	724	2,637	1, 2, 3,			COMBINE-1
21	Combine	2.910	2	724	9,957	0, 7, 8, 9,			COMBINE-2
22	Combine	3.612	2	724	12,594	20, 21			TO SOUTH INFIL SYS
23	Combine	3.067	2	724	10,054	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.000	2	690	0	13	141.89	1,113	SOUTH POR PVMT
25	Reservoir	0.000	2	736	0	14	141.31	1,422	NORTH POR PVMT
26	Reservoir	0.013	2	802	50	22	143.05	5,211	SOUTH INFIL SYS
27	Reservoir	0.292	2	752	960	23	143.25	4,072	NORTH INFIL SYS
28	Combine	0.880	2	724	2,982	17, 18,			COMBINE-3
29	Combine	0.880	2	724	3,992	24, 25, 26,			SYSTEM OUTLET
30	Combine	1.185	2	744	8,096	19, 29			TOTAL SITE
F01	73-02 Hvdroo	Iraphs - F	Proposed	.apw	Return P	eriod: 2 Ye	ar	Tuesday, 0!	5 / 25 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

CB-01

Hydrograph type	= SCS Runoff	Peak discharge	= 0.161 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.20 hrs
Time interval	= 2 min	Hyd. volume	= 709 cuft
Drainage area	= 0.194 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.20 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 2

CB-01A

Hydrograph type	= SCS Runoff	Peak discharge	= 0.150 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 526 cuft
Drainage area	= 0.104 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 7.80 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Tuesday, 05 / 25 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.159 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 492 cuft
Drainage area	= 0.054 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 4

Hydrograph type =	SCS Runoff	Peak discharge	= 0.199 cfs
Storm frequency =	= 2 yrs	Time to peak	= 12.07 hrs
Time interval =	= 2 min	Hyd. volume	= 603 cuft
Drainage area =	= 0.074 ac	Curve number	= 89
Basin Slope =	= 0.0 %	Hydraulic length	= 0 ft
Tc method =	= User	Time of conc. (Tc)	= 5.00 min
Total precip. =	= 3.54 in	Distribution	= Type III
Storm duration =	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 5

CB-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.165 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 510 cuft
Drainage area	= 0.056 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484


Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 6

CB-05

Hydrograph type	= SCS Runoff	Peak discharge	= 0.302 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 910 cuft
Drainage area	= 0.116 ac	Curve number	= 88
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 7

Hydrograph type	= SCS Runoff	Peak discharge	= 0.177 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 544 cuft
Drainage area	= 0.062 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Tuesday, 05 / 25 / 2021

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 8

Hydrograph type	= SCS Runoff	Peak discharge	= 0.299 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 934 cuft
Drainage area	= 0.099 ac	Curve number	= 93
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 9

Hydrograph type	= SCS Runoff	Peak discharge	= 0.344 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,065 cuft
Drainage area	= 0.117 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.50 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 10

CB-09

Hydrograph type	= SCS Runoff	Peak discharge	= 0.424 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,340 cuft
Drainage area	= 0.137 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 11

Hydrograph type	= SCS Runoff	Peak discharge	= 0.383 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,176 cuft
Drainage area	= 0.134 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 12

Hydrograph type	= SCS Runoff	Peak discharge	= 0.198 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 831 cuft
Drainage area	= 0.227 ac	Curve number	= 69
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 11.60 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 13

PP-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.126 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,664 cuft
Drainage area	= 0.349 ac	Curve number	= 96
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.60 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 14

PP-02

Hydrograph type	= SCS Runoff	Peak discharge	= 1.452 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 4,588 cuft
Drainage area	= 0.469 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 15

RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.896 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 6,425 cuft
Drainage area	= 0.571 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 16

RF-02

Hydrograph type	= SCS Runoff	Peak discharge	= 1.942 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 6,582 cuft
Drainage area	= 0.585 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 17

RF-03

Hydrograph type	= SCS Runoff	Peak discharge	= 0.458 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,553 cuft
Drainage area	= 0.138 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 18

RF-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.422 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,429 cuft
Drainage area	= 0.127 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 19

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 0.734 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 4,104 cuft
Drainage area	= 1.038 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 27.60 min
Total precip.	= 3.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 20

COMBINE-1

Hydrograph type	= Combine	Peak discharge	= 0.703 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,637 cuft
Inflow hyds.	= 1, 2, 3, 6	Contrib. drain. area	= 0.468 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 21

COMBINE-2

Hydrograph type =	= Combine	Peak discharge	= 2.910 cfs
Storm frequency =	= 2 yrs	Time to peak	= 12.07 hrs
Time interval :	= 2 min	Hyd. volume	= 9,957 cuft
Inflow hyds.	= 7, 8, 9, 12, 16	Contrib. drain. area	= 1.090 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type =	Combine	Peak discharge	= 3.612 cfs
Storm frequency =	2 yrs	Time to peak	= 12.07 hrs
Time interval =	2 min	Hyd. volume	= 12,594 cuft
Inflow hyds. =	20, 21	Contrib. drain. area	= 0.000 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 3.067 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 10,054 cuft
Inflow hyds.	= 4, 5, 10, 11, 15	Contrib. drain. area	= 0.972 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 24

SOUTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.50 hrs
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 13 - PP-01	Max. Elevation	= 141.89 ft
Reservoir name	= SOUTH POROUS PVMT	Max. Storage	= 1,113 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



## **Pond Report**

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### Pond No. 3 - SOUTH POROUS PVMT

### **Pond Data**

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 141.50 ft. Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.50	9,428	0	0
0.50	142.00	9,428	1,414	1,414
1.00	142.50	9,428	1,414	2,828

#### + / Orifi C+

Culvert / Orifice Structures			Weir Structures						
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 6.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 6.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 142.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 10.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

### Stage (ft)

Stage / Discharge



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## Hyd. No. 25

NORTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.27 hrs
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 14 - PP-02	Max. Elevation	= 141.31 ft
Reservoir name	= NORTH POROUS PVMT	Max. Storage	= 1,422 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



## **Pond Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

### Pond No. 4 - NORTH POROUS PVMT

### **Pond Data**

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 141.00 ft. Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	15,420	0	0
0.50	141.50	15,420	2,313	2,313
1.00	142.00	15,420	2,313	4,626

### vort / Orifico Structuros

Culvert / Orifice Structures			Weir Structures						
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 6.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 6.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 141.50	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 10.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

### Stage / Discharge Stage (ft) Elev (ft) 1.00 142.00 0.90 141.90 0.80 141.80 0.70 141.70 0.60 141.60 0.50 141.50 0.40 141.40 0.30 141.30 0.20 141.20 0.10 141.10 0.00 141.00 0.00 0.50 1.00 1.50 2.00 Discharge (cfs) Total Q

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## Hyd. No. 26

SOUTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 0.013 cfs
Storm frequency	= 2 yrs	Time to peak	= 13.37 hrs
Time interval	= 2 min	Hyd. volume	= 50 cuft
Inflow hyd. No.	= 22 - TO SOUTH INFIL SYS	Max. Elevation	= 143.05 ft
Reservoir name	= SOUTH INFIL SYS	Max. Storage	= 5,211 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## **Pond Report**

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### Pond No. 1 - SOUTH INFIL SYS

### **Pond Data**

**UG Chambers -**Invert elev. = 142.00 ft, Rise x Span =  $2.00 \times 7.00$  ft, Barrel Len = 170.00 ft, No. Barrels = 3, Slope = 0.00%, Headers = Yes **Encasement -**Invert elev. = 141.00 ft, Width = 7.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	n/a	0	0
0.40	141.40	n/a	464	464
0.80	141.80	n/a	464	928
1.20	142.20	n/a	1,005	1,932
1.60	142.60	n/a	1,546	3,478
2.00	143.00	n/a	1,546	5,024
2.40	143.40	n/a	1,546	6,570
2.80	143.80	n/a	1,546	8,116
3.20	144.20	n/a	1,005	9,121
3.60	144.60	n/a	464	9,584
4.00	145.00	n/a	464	10,048

### **Culvert / Orifice Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	0.00	0.00	Crest Len (ft)	Inactive	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 143.00	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 38.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a	-				
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by	y Wet area)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00	. *		

**Weir Structures** 

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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## Hyd. No. 27

NORTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 0.292 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.53 hrs
Time interval	= 2 min	Hyd. volume	= 960 cuft
Inflow hyd. No.	= 23 - TO NORTH INFIL SYS	Max. Elevation	= 143.25 ft
Reservoir name	= NORTH INFIL SYS	Max. Storage	= 4,072 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



## **Pond Report**

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### Pond No. 2 - NORTH INFIL SYS

### **Pond Data**

**UG Chambers -**Invert elev. = 142.00 ft, Rise x Span =  $2.00 \times 7.00 \text{ ft}$ , Barrel Len = 80.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = Yes **Encasement -**Invert elev. = 141.00 ft, Width = 7.00 ft, Height = 4.00 ft, Voids = 30.00%

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	n/a	0	0
0.40	141.40	n/a	316	316
0.80	141.80	n/a	316	632
1.20	142.20	n/a	684	1,316
1.60	142.60	n/a	1,053	2,369
2.00	143.00	n/a	1,053	3,422
2.40	143.40	n/a	1,053	4,475
2.80	143.80	n/a	1,053	5,528
3.20	144.20	n/a	684	6,213
3.60	144.60	n/a	316	6,528
4.00	145.00	n/a	316	6,844

### **Culvert / Orifice Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	0.00	0.00	Crest Len (ft)	Inactive	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 143.00	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 50.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a	-				
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by	/Wet area)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

**Weir Structures** 

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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## Hyd. No. 28

COMBINE-3

80 cts
07 hrs
82 cuft
65 ac



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## Hyd. No. 29

## SYSTEM OUTLET

Hydrograph type	= Combine	Peak discharge	= 0.880 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,992 cuft
Inflow hyds.	= 24, 25, 26, 27, 28	Contrib. drain. area	= 0.000 ac



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## Hyd. No. 30

TOTAL SITE

Hydrograph type	= Combine	Peak discharge	= 1.185 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 8,096 cuft
Inflow hyds.	= 19, 29	Contrib. drain. area	= 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.389	2	732	1,605				CB-01
2	SCS Runoff	0.317	2	726	1,083				CB-01A
3	SCS Runoff	0.259	2	724	823				CB-02
4	SCS Runoff	0.337	2	724	1,047				CB-03
5	SCS Runoff	0.268	2	724	854				CB-04
6	SCS Runoff	0.518	2	724	1,599				CB-05
7	SCS Runoff	0.292	2	724	922				CB-06
8	SCS Runoff	0.481	2	724	1,547				CB-07
9	SCS Runoff	0.560	2	724	1,784				CB-08
10	SCS Runoff	0.674	2	724	2,193				СВ-09
11	SCS Runoff	0.632	2	724	1,993				CB-10
12	SCS Runoff	0.490	2	730	1,914				CB-11
13	SCS Runoff	1.754	2	724	5,856				PP-01
14	SCS Runoff	2.308	2	724	7,506				PP-02
15	SCS Runoff	2.910	2	724	10,032				RF-01
16	SCS Runoff	2.981	2	724	10,278				RF-02
17	SCS Runoff	0.703	2	724	2,425				RF-03
18	SCS Runoff	0.647	2	724	2,231				RF-04
19	SCS Runoff	1.726	2	740	9,131				PR-WS-01
20	Combine	1.351	2	724	5,110	1, 2, 3,			COMBINE-1
21	Combine	4.708	2	724	16,445	6, 7, 8, 9,			COMBINE-2
22	Combine	6.059	2	724	21,556	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	4.821	2	724	16,118	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.053	2	742	79	11, 15,	142.13	1,789	SOUTH POR PVMT
25	Reservoir	0.000	2	780	0	14	141.49	2,281	NORTH POR PVMT
26	Reservoir	1.750	2	744	5,699	22	143.65	7,518	SOUTH INFIL SYS
27	Reservoir	1.863	2	734	5,078	23	143.73	5,328	NORTH INFIL SYS
28	Combine	1.350	2	724	4,656	17, 18,			COMBINE-3
29	Combine	3.943	2	738	15,512	24, 25, 26,			SYSTEM OUTLET
30	Combine	5.658	2	740	24,643	27, 28 19, 29			TOTAL SITE
F01	73-02 Hvdroc	graphs - F	Proposed	l.gpw	Return P	eriod: 10 Y	/ /ear	Tuesday, 0	5 / 25 / 2021
F0173-02 Hydrographs - Proposed.gpw				Return P	eriod: 10 Y	rear	I uesday, 0	5 / 25 / 2021	

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.389 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.20 hrs
Time interval	= 2 min	Hyd. volume	= 1,605 cuft
Drainage area	= 0.194 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.20 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 2

CB-01A

Hydrograph type	= SCS Runoff	Peak discharge	= 0.317 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 1,083 cuft
Drainage area	= 0.104 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 7.80 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.259 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 823 cuft
Drainage area	= 0.054 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 4

Hydrograph type	= SCS Runoff	Peak discharge	= 0.337 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,047 cuft
Drainage area	= 0.074 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 5

Hydrograph type	= SCS Runoff	Peak discharge	= 0.268 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 854 cuft
Drainage area	= 0.056 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 6

CB-05

Hydrograph type	= SCS Runoff	Peak discharge	= 0.518 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,599 cuft
Drainage area	= 0.116 ac	Curve number	= 88
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484


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#### Hyd. No. 7

Hydrograph type	= SCS Runoff	Peak discharge	= 0.292 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 922 cuft
Drainage area	= 0.062 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 8

Hydrograph type	= SCS Runoff	Peak discharge	= 0.481 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,547 cuft
Drainage area	= 0.099 ac	Curve number	= 93
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 9

Hydrograph type	= SCS Runoff	Peak discharge	= 0.560 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,784 cuft
Drainage area	= 0.117 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.50 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 10

CB-09

Hydrograph type	= SCS Runoff	Peak discharge	= 0.674 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,193 cuft
Drainage area	= 0.137 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 11

Hydrograph type	= SCS Runoff	Peak discharge	= 0.632 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,993 cuft
Drainage area	= 0.134 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 12

Hydrograph type	= SCS Runoff	Peak discharge	= 0.490 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 1,914 cuft
Drainage area	= 0.227 ac	Curve number	= 69
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 11.60 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 13

PP-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.754 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 5,856 cuft
Drainage area	= 0.349 ac	Curve number	= 96
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.60 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 14

PP-02

Hydrograph type	= SCS Runoff	Peak discharge	= 2.308 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 7,506 cuft
Drainage area	= 0.469 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 15

RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.910 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 10,032 cuft
Drainage area	= 0.571 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 16

RF-02

Hydrograph type	= SCS Runoff	Peak discharge	= 2.981 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 10,278 cuft
Drainage area	= 0.585 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 17

RF-03

Hydrograph type	= SCS Runoff	Peak discharge	= 0.703 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,425 cuft
Drainage area	= 0.138 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 18

RF-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.647 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,231 cuft
Drainage area	= 0.127 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 19

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.726 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.33 hrs
Time interval	= 2 min	Hyd. volume	= 9,131 cuft
Drainage area	= 1.038 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 27.60 min
Total precip.	= 5.40 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 20

COMBINE-1

Hydrograph type	= Combine	Peak discharge	= 1.351 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 5,110 cuft
Inflow hyds.	= 1, 2, 3, 6	Contrib. drain. area	= 0.468 ac



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#### Hyd. No. 21

COMBINE-2

Hydrograph type	= Combine	Peak discharge	= 4.708 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 16,445 cuft
Inflow hyds.	= 7, 8, 9, 12, 16	Contrib. drain. area	= 1.090 ac



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#### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type Storm frequency	= Combine = 10 yrs	Peak discharge Time to peak	= 6.059 cfs = 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 21,556 cuft
Inflow hyds.	= 20, 21	Contrib. drain. area	= 0.000 ac



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#### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 4.821 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 16,118 cuft
Inflow hyds.	= 4, 5, 10, 11, 15	Contrib. drain. area	= 0.972 ac



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### Hyd. No. 24

SOUTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.053 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 79 cuft
Inflow hyd. No.	= 13 - PP-01	Max. Elevation	= 142.13 ft
Reservoir name	= SOUTH POROUS PVMT	Max. Storage	= 1,789 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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### Hyd. No. 25

NORTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 10 yrs	Time to peak	= 13.00 hrs
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 14 - PP-02	Max. Elevation	= 141.49 ft
Reservoir name	= NORTH POROUS PVMT	Max. Storage	= 2,281 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Hyd. No. 26

SOUTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 1.750 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 5,699 cuft
Inflow hyd. No.	= 22 - TO SOUTH INFIL SYS	Max. Elevation	= 143.65 ft
Reservoir name	= SOUTH INFIL SYS	Max. Storage	= 7,518 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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Tuesday, 05 / 25 / 2021

#### Hyd. No. 27

NORTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 1.863 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.23 hrs
Time interval	= 2 min	Hyd. volume	= 5,078 cuft
Inflow hyd. No.	= 23 - TO NORTH INFIL SYS	Max. Elevation	= 143.73 ft
Reservoir name	= NORTH INFIL SYS	Max. Storage	= 5,328 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Hyd. No. 28

COMBINE-3

= Combine	Peak discharge	= 1.350 cfs
= 10 yrs	Time to peak	= 12.07 hrs
= 2 min	Hyd. volume	= 4,656 cuft
= 17, 18	Contrib. drain. area	= 0.265 ac
	= Combine = 10 yrs = 2 min = 17, 18	= CombinePeak discharge= 10 yrsTime to peak= 2 minHyd. volume= 17, 18Contrib. drain. area



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#### Hyd. No. 29

#### SYSTEM OUTLET

Hydrograph type	= Combine	Peak discharge	= 3.943 cfs
Storm frequency	= 10 vrs	Time to peak	= 12.30 hrs
Time interval	= 2 min	Hyd. volume	= 15,512 cuft
Inflow hyds.	= 24, 25, 26, 27, 28	Contrib. drain. area	= 0.000 ac



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#### Hyd. No. 30

TOTAL SITE

Hydrograph type Storm frequency Time interval	= Combine = 10 yrs = 2 min = 19 29	Peak discharge Time to peak Hyd. volume Contrib. drain, area	= 5.658 cfs = 12.33 hrs = 24,643 cuft = 1.038 ac
Inflow hyds.	= 19, 29	Contrib. drain. area	= 1.038 ac



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# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.548	2	730	2,241				CB-01
2	SCS Runoff	0.428	2	726	1,464				CB-01A
3	SCS Runoff	0.321	2	724	1,035				CB-02
4	SCS Runoff	0.423	2	724	1,332				CB-03
5	SCS Runoff	0.332	2	724	1,073				CB-04
6	SCS Runoff	0.653	2	724	2,043				CB-05
7	SCS Runoff	0.364	2	724	1,164				CB-06
8	SCS Runoff	0.594	2	724	1,936				CB-07
9	SCS Runoff	0.695	2	724	2,242				CB-08
10	SCS Runoff	0.830	2	724	2,733				CB-09
11	SCS Runoff	0.786	2	724	2,515				CB-10
12	SCS Runoff	0.697	2	728	2,689				CB-11
13	SCS Runoff	2.146	2	724	7,239				PP-01
14	SCS Runoff	2.841	2	724	9,355				PP-02
15	SCS Runoff	3.546	2	724	12,303				RF-01
16	SCS Runoff	3.633	2	724	12,605				RF-02
17	SCS Runoff	0.857	2	724	2,973				RF-03
18	SCS Runoff	0.789	2	724	2,736				RF-04
19	SCS Runoff	2.421	2	740	12,677				PR-WS-01
20	Combine	1.778	2	724	6,783	1, 2, 3,			COMBINE-1
21	Combine	5.855	2	724	20,635	0, 7, 8, 9,			COMBINE-2
22	Combine	7.634	2	724	27,418	20, 21			TO SOUTH INFIL SYS
23	Combine	5.917	2	724	19,956	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.188	2	742	389	13	142.27	2,190	SOUTH POR PVMT
25	Reservoir	0.050	2	744	73	14	141.63	2,905	NORTH POR PVMT
26	Reservoir	3.418	2	736	10,013	22	143.97	8,545	SOUTH INFIL SYS
27	Reservoir	3.033	2	730	7,914	23	144.15	6,117	NORTH INFIL SYS
28	Combine	1.646	2	724	5,710	17, 18,			COMBINE-3
29	Combine	7.202	2	732	24,099	24, 25, 26,			SYSTEM OUTLET
30	Combine	9.362	2	736	36,776	19, 29			TOTAL SITE
	72.02 44/45-5	roopho 5			Poture D	oriod: 25 M		Tuesday 0	- / 25 / 2024
F0173-02 Hydrographs - Proposed.gpw Ret			Return P	eriod: 25 Y	ear	Tuesday, 0	o / 25 / 2021		

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.548 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 2,241 cuft
Drainage area	= 0.194 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.20 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 2

CB-01A

Hydrograph type	= SCS Runoff	Peak discharge	= 0.428 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 1,464 cuft
Drainage area	= 0.104 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 7.80 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.321 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,035 cuft
Drainage area	= 0.054 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 4

Hydrograph type	= SCS Runoff	Peak discharge	= 0.423 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,332 cuft
Drainage area	= 0.074 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 5

Hydrograph type	= SCS Runoff	Peak discharge	= 0.332 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,073 cuft
Drainage area	= 0.056 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 6

Hydrograph type	= SCS Runoff	Peak discharge	= 0.653 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,043 cuft
Drainage area	= 0.116 ac	Curve number	= 88
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 7

Hydrograph type	= SCS Runoff	Peak discharge	= 0.364 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,164 cuft
Drainage area	= 0.062 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 8

Hydrograph type	= SCS Runoff	Peak discharge	= 0.594 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,936 cuft
Drainage area	= 0.099 ac	Curve number	= 93
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 9

Hydrograph type	= SCS Runoff	Peak discharge	= 0.695 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,242 cuft
Drainage area	= 0.117 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.50 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 10

CB-09

Hydrograph type	= SCS Runoff	Peak discharge	= 0.830 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,733 cuft
Drainage area	= 0.137 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 11

Hydrograph type	= SCS Runoff	Peak discharge	= 0.786 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,515 cuft
Drainage area	= 0.134 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484


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## Hyd. No. 12

Hydrograph type	= SCS Runoff	Peak discharge	= 0.697 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 2,689 cuft
Drainage area	= 0.227 ac	Curve number	= 69
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 11.60 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 13

PP-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.146 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 7,239 cuft
Drainage area	= 0.349 ac	Curve number	= 96
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.60 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 14

PP-02

Hydrograph type	= SCS Runoff	Peak discharge	= 2.841 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 9,355 cuft
Drainage area	= 0.469 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 15

RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 3.546 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 12,303 cuft
Drainage area	= 0.571 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 16

RF-02

Hydrograph type	= SCS Runoff	Peak discharge	= 3.633 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 12,605 cuft
Drainage area	= 0.585 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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### Hyd. No. 17

RF-03

Hydrograph type	= SCS Runoff	Peak discharge	= 0.857 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,973 cuft
Drainage area	= 0.138 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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### Hyd. No. 18

RF-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.789 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,736 cuft
Drainage area	= 0.127 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 19

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.421 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.33 hrs
Time interval	= 2 min	Hyd. volume	= 12,677 cuft
Drainage area	= 1.038 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 27.60 min
Total precip.	= 6.57 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 20

COMBINE-1

Hydrograph type	= Combine	Peak discharge	= 1.778 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 6,783 cuft
Inflow hyds.	= 1, 2, 3, 6	Contrib. drain. area	= 0.468 ac



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### Hyd. No. 21

COMBINE-2

Hydrograph type	= Combine	Peak discharge	= 5.855 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 20,635 cuft
Inflow hyds.	= 7, 8, 9, 12, 16	Contrib. drain. area	= 1.090 ac



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## Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 7.634 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 27,418 cuft
Inflow hyds.	= 20, 21	Contrib. drain. area	= 0.000 ac



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## Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 5.917 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 19,956 cuft
Inflow hyds.	= 4, 5, 10, 11, 15	Contrib. drain. area	= 0.972 ac



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## Hyd. No. 24

SOUTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.188 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 389 cuft
Inflow hyd. No.	= 13 - PP-01	Max. Elevation	= 142.27 ft
Reservoir name	= SOUTH POROUS PVMT	Max. Storage	= 2,190 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 25

NORTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.050 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 73 cuft
Inflow hyd. No.	= 14 - PP-02	Max. Elevation	= 141.63 ft
Reservoir name	= NORTH POROUS PVMT	Max. Storage	= 2,905 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 26

SOUTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 3.418 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.27 hrs
Time interval	= 2 min	Hyd. volume	= 10,013 cuft
Inflow hyd. No.	= 22 - TO SOUTH INFIL SYS	Max. Elevation	= 143.97 ft
Reservoir name	= SOUTH INFIL SYS	Max. Storage	= 8,545 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 27

NORTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 3.033 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 7,914 cuft
Inflow hyd. No.	= 23 - TO NORTH INFIL SYS	Max. Elevation	= 144.15 ft
Reservoir name	= NORTH INFIL SYS	Max. Storage	= 6,117 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 28

COMBINE-3

= Combine	Peak discharge	= 1.646 cfs
= 25 yrs	Time to peak	= 12.07 hrs
= 2 min	Hyd. volume	= 5,710 cuft
= 17, 18	Contrib. drain. area	= 0.265 ac
	= Combine = 25 yrs = 2 min = 17, 18	= CombinePeak discharge= 25 yrsTime to peak= 2 minHyd. volume= 17, 18Contrib. drain. area



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### Hyd. No. 29

## SYSTEM OUTLET

Hydrograph type	= Combine	Peak discharge	= 7.202 cfs
Storm frequency	= 25 yrs	Time to peak	= 12.20 hrs
Time interval	= 2 min	Hyd. volume	= 24,099 cuft
Inflow hyds.	= 24, 25, 26, 27, 28	Contrib. drain. area	= 0.000 ac



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## Hyd. No. 30

TOTAL SITE

Hydrograph type Storm frequency	= Combine = 25 yrs	Peak discharge Time to peak	= 9.362 cfs = 12.27 hrs
Time interval	= 2 min	Hyd. volume	= 36,776 cuft
Inflow hyds.	= 19, 29	Contrib. drain. area	= 1.038 ac



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# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.672	2	730	2,738				CB-01
2	SCS Runoff	0.513	2	726	1,756				CB-01A
3	SCS Runoff	0.366	2	724	1,193				CB-02
4	SCS Runoff	0.487	2	724	1,546				CB-03
5	SCS Runoff	0.380	2	724	1,237				CB-04
6	SCS Runoff	0.753	2	724	2,377				CB-05
7	SCS Runoff	0.417	2	724	1,344				CB-06
8	SCS Runoff	0.678	2	724	2,226				CB-07
9	SCS Runoff	0.794	2	724	2,584				CB-08
10	SCS Runoff	0.945	2	724	3,136				CB-09
11	SCS Runoff	0.901	2	724	2,906				CB-10
12	SCS Runoff	0.858	2	728	3,295				CB-11
13	SCS Runoff	2.437	2	724	8,269				PP-01
14	SCS Runoff	3.235	2	724	10,734				PP-02
15	SCS Runoff	4.018	2	724	13,992				RF-01
16	SCS Runoff	4.117	2	724	14,335				RF-02
17	SCS Runoff	0.971	2	724	3,382				RF-03
18	SCS Runoff	0.894	2	724	3,112				RF-04
19	SCS Runoff	2.955	2	740	15,436				PR-WS-01
20	Combine	2.102	2	724	8,063	1, 2, 3,			COMBINE-1
21	Combine	6.713	2	724	23,785	5, 7, 8, 9,			COMBINE-2
22	Combine	8.815	2	724	31,848	20, 21			TO SOUTH INFIL SYS
23	Combine	6.730	2	724	22,816	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.278	2	742	694	13	142.38	2,484	SOUTH POR PVMT
25	Reservoir	0.140	2	744	271	14	141.73	3,359	NORTH POR PVMT
26	Reservoir	4.661	2	732	13,406	22	144.41	9,355	SOUTH INFIL SYS
27	Reservoir	4.540	2	728	10,110	23	144.57	6,500	NORTH INFIL SYS
28	Combine	1.865	2	724	6,494	17, 18,			COMBINE-3
29	Combine	10.05	2	728	30,974	24, 25, 26,			SYSTEM OUTLET
30	Combine	12.19	2	730	46,410	19, 29			TOTAL SITE
F01	73-02 Hvdroc	graphs - F	Proposed	.apw	Return P	eriod: 50 Y	/ /ear	Tuesday. 0	5 / 25 / 2021
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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 1

CB-01

Hydrograph type	= SCS Runoff	Peak discharge	= 0.672 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 2,738 cuft
Drainage area	= 0.194 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.20 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 2

CB-01A

Hydrograph type	= SCS Runoff	Peak discharge	= 0.513 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 1,756 cuft
Drainage area	= 0.104 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 7.80 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.366 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,193 cuft
Drainage area	= 0.054 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 4

Hydrograph type	= SCS Runoff	Peak discharge	= 0.487 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,546 cuft
Drainage area	= 0.074 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 5

CB-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.380 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,237 cuft
Drainage area	= 0.056 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 6

CB-05

Hydrograph type	= SCS Runoff	Peak discharge	= 0.753 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,377 cuft
Drainage area	= 0.116 ac	Curve number	= 88
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 7

Hydrograph type	= SCS Runoff	Peak discharge	= 0.417 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,344 cuft
Drainage area	= 0.062 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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## Hyd. No. 8

Hydrograph type	= SCS Runoff	Peak discharge	= 0.678 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,226 cuft
Drainage area	= 0.099 ac	Curve number	= 93
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 9

CB-08

Hydrograph type	= SCS Runoff	Peak discharge	= 0.794 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,584 cuft
Drainage area	= 0.117 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.50 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 10

CB-09

Hydrograph type	= SCS Runoff	Peak discharge	= 0.945 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,136 cuft
Drainage area	= 0.137 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 11

Hydrograph type	= SCS Runoff	Peak discharge	= 0.901 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,906 cuft
Drainage area	= 0.134 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 12

Hydrograph type	= SCS Runoff	Peak discharge	= 0.858 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 3,295 cuft
Drainage area	= 0.227 ac	Curve number	= 69
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 11.60 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 13

PP-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.437 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 8,269 cuft
Drainage area	= 0.349 ac	Curve number	= 96
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.60 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 14

PP-02

Hydrograph type	= SCS Runoff	Peak discharge	= 3.235 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 10,734 cuft
Drainage area	= 0.469 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 15

RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 4.018 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 13,992 cuft
Drainage area	= 0.571 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

## Hyd. No. 16

RF-02

Hydrograph type	= SCS Runoff	Peak discharge	= 4.117 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 14,335 cuft
Drainage area	= 0.585 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 17

RF-03

Hydrograph type	= SCS Runoff	Peak discharge	= 0.971 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,382 cuft
Drainage area	= 0.138 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 18

RF-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.894 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,112 cuft
Drainage area	= 0.127 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 19

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.955 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.33 hrs
Time interval	= 2 min	Hyd. volume	= 15,436 cuft
Drainage area	= 1.038 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 27.60 min
Total precip.	= 7.44 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 20

COMBINE-1

Hydrograph type	= Combine	Peak discharge	= 2.102 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 8,063 cuft
Inflow hyds.	= 1, 2, 3, 6	Contrib. drain. area	= 0.468 ac



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#### Hyd. No. 21

COMBINE-2

Hydrograph type	= Combine	Peak discharge	= 6.713 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 23,785 cuft
Inflow hyds.	= 7, 8, 9, 12, 16	Contrib. drain. area	= 1.090 ac



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### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 8.815 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 31,848 cuft
Inflow hyds.	= 20, 21	Contrib. drain. area	= 0.000 ac



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#### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 6.730 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 22,816 cuft
Inflow hyds.	= 4, 5, 10, 11, 15	Contrib. drain. area	= 0.972 ac



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#### Hyd. No. 24

SOUTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.278 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 694 cuft
Inflow hyd. No.	= 13 - PP-01	Max. Elevation	= 142.38 ft
Reservoir name	= SOUTH POROUS PVMT	Max. Storage	= 2,484 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Hyd. No. 25

NORTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.140 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 271 cuft
Inflow hyd. No.	= 14 - PP-02	Max. Elevation	= 141.73 ft
Reservoir name	= NORTH POROUS PVMT	Max. Storage	= 3,359 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 26

SOUTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 4.661 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.20 hrs
Time interval	= 2 min	Hyd. volume	= 13,406 cuft
Inflow hyd. No.	= 22 - TO SOUTH INFIL SYS	Max. Elevation	= 144.41 ft
Reservoir name	= SOUTH INFIL SYS	Max. Storage	= 9,355 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 27

NORTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 4.540 cfs
Storm frequency	= 50 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 10,110 cuft
Inflow hyd. No.	= 23 - TO NORTH INFIL SYS	Max. Elevation	= 144.57 ft
Reservoir name	= NORTH INFIL SYS	Max. Storage	= 6,500 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 28

COMBINE-3

- Combine	Peak discharge	= 1.865 cfs
= 50 yrs	Time to peak	= 12.07 hrs
= 2 min	Hyd. volume	= 6,494 cuft
= 17, 18	Contrib. drain. area	= 0.265 ac
	= Combine = 50 yrs = 2 min = 17, 18	CombinePeak discharge50 yrsTime to peak2 minHyd. volume17, 18Contrib. drain. area



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 29

### SYSTEM OUTLET

Hydrograph type	= Combine	Peak discharge	= 10.05 cfs
Storm frequency	= 50 vrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 30,974 cuft
Inflow hyds.	= 24, 25, 26, 27, 28	Contrib. drain. area	= 0.000 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 30

TOTAL SITE

Hydrograph type Storm frequency	= Combine = 50 vrs	Peak discharge Time to peak	= 12.19 cfs = 12.17 hrs
Time interval	$= 2 \min_{x \in A} \frac{1}{2} \sum_{x \in$	Hyd. volume	= 46,410 cuft
Inflow hyds.	= 19, 29	Contrib. drain. area	= 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.807	2	730	3,285				CB-01
2	SCS Runoff	0.604	2	726	2,075				CB-01A
3	SCS Runoff	0.415	2	724	1,362				CB-02
4	SCS Runoff	0.554	2	724	1,775				CB-03
5	SCS Runoff	0.431	2	724	1,412				CB-04
6	SCS Runoff	0.860	2	724	2,736				CB-05
7	SCS Runoff	0.473	2	724	1,538				CB-06
8	SCS Runoff	0.767	2	724	2,537				CB-07
9	SCS Runoff	0.900	2	724	2,950				CB-08
10	SCS Runoff	1.068	2	724	3,567				CB-09
11	SCS Runoff	1.022	2	724	3,324				CB-10
12	SCS Runoff	1.034	2	728	3,965				CB-11
13	SCS Runoff	2.747	2	724	9,371				PP-01
14	SCS Runoff	3.655	2	724	12,210				PP-02
15	SCS Runoff	4.523	2	724	15,798				RF-01
16	SCS Runoff	4.634	2	724	16,185				RF-02
17	SCS Runoff	1.093	2	724	3,818				RF-03
18	SCS Runoff	1.006	2	724	3,514				RF-04
19	SCS Runoff	3.537	2	740	18,471				PR-WS-01
20	Combine	2.450	2	724	9,457	1, 2, 3,			COMBINE-1
21	Combine	7.633	2	724	27,176	6, 7, 8, 9,			COMBINE-2
22	Combine	10.08	2	724	36,633	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	7.597	2	724	25,877	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.330	2	742	1,045	11, 15, 13	142.50	2,824	SOUTH POR PVMT
25	Reservoir	0.237	2	744	582	14	141.83	3,832	NORTH POR PVMT
26	Reservoir	6.520	2	730	17,173	22	144.92	9,945	SOUTH INFIL SYS
27	Reservoir	5.682	2	728	12,524	23	144.93	6,752	NORTH INFIL SYS
28	Combine	2.099	2	724	7,332	17, 18,			COMBINE-3
29	Combine	13.89	2	728	38,655	24, 25, 26,			SYSTEM OUTLET
30	Combine	16.34	2	728	57,126	27, 28 19, 29			TOTAL SITE
F01	73-02 Hvdroc	Jraphs - F	Proposed	Lapw	Return P	eriod: 100	Year	Tuesday 0	5/25/2021
			.000000			5.164. 100		1 400449, 0	

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#### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.807 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 3,285 cuft
Drainage area	= 0.194 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.20 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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### Hyd. No. 2

CB-01A

Hydrograph type	= SCS Runoff	Peak discharge	= 0.604 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.10 hrs
Time interval	= 2 min	Hyd. volume	= 2,075 cuft
Drainage area	= 0.104 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 7.80 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.415 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,362 cuft
Drainage area	= 0.054 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 4

Hydrograph type	= SCS Runoff	Peak discharge	= 0.554 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,775 cuft
Drainage area	= 0.074 ac	Curve number	= 89
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 5

CB-04

Hydrograph type	= SCS Runoff	Peak discharge	= 0.431 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 1,412 cuft
Drainage area	= 0.056 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 6

CB-05

Hydrograph type	= SCS Runoff	Peak discharge	= 0.860 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,736 cuft
Drainage area	= 0.116 ac	Curve number	= 88
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 7

Hydrograph type =	SCS Runoff	Peak discharge	= 0.473 cfs
Storm frequency =	= 100 yrs	Time to peak	= 12.07 hrs
Time interval =	= 2 min	Hyd. volume	= 1,538 cuft
Drainage area =	= 0.062 ac	Curve number	= 91
Basin Slope =	= 0.0 %	Hydraulic length	= 0 ft
Tc method =	= User	Time of conc. (Tc)	= 5.00 min
Total precip. =	= 8.37 in	Distribution	= Type III
Storm duration =	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 8

Hydrograph type	= SCS Runoff	Peak discharge	= 0.767 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,537 cuft
Drainage area	= 0.099 ac	Curve number	= 93
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 9

Hydrograph type	= SCS Runoff	Peak discharge	= 0.900 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 2,950 cuft
Drainage area	= 0.117 ac	Curve number	= 92
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.50 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 10

CB-09

Hydrograph type	= SCS Runoff	Peak discharge	= 1.068 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,567 cuft
Drainage area	= 0.137 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 11

CB-10

Hydrograph type	= SCS Runoff	Peak discharge	= 1.022 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,324 cuft
Drainage area	= 0.134 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 12

Hydrograph type	= SCS Runoff	Peak discharge	= 1.034 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 3,965 cuft
Drainage area	= 0.227 ac	Curve number	= 69
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 11.60 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 13

PP-01

Hydrograph type	= SCS Runoff	Peak discharge	= 2.747 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 9,371 cuft
Drainage area	= 0.349 ac	Curve number	= 96
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.60 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

#### Hyd. No. 14

PP-02

Hydrograph type	= SCS Runoff	Peak discharge	= 3.655 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 12,210 cuft
Drainage area	= 0.469 ac	Curve number	= 94
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 15

RF-01

Hydrograph type	= SCS Runoff	Peak discharge	= 4.523 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 15,798 cuft
Drainage area	= 0.571 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 16

RF-02

Hydrograph type	= SCS Runoff	Peak discharge	= 4.634 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 16,185 cuft
Drainage area	= 0.585 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 17

RF-03

Hydrograph type	= SCS Runoff	Peak discharge	= 1.093 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,818 cuft
Drainage area	= 0.138 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 18

RF-04

Hydrograph type	= SCS Runoff	Peak discharge	= 1.006 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 3,514 cuft
Drainage area	= 0.127 ac	Curve number	= 98
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 19

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 3.537 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.33 hrs
Time interval	= 2 min	Hyd. volume	= 18,471 cuft
Drainage area	= 1.038 ac	Curve number	= 71
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 27.60 min
Total precip.	= 8.37 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 20

COMBINE-1

Hydrograph type	= Combine	Peak discharge	= 2.450 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 9,457 cuft
Inflow hyds.	= 1, 2, 3, 6	Contrib. drain. area	= 0.468 ac



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#### Hyd. No. 21

COMBINE-2

Hydrograph type	= Combine	Peak discharge	= 7.633 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 27,176 cuft
Inflow hyds.	= 7, 8, 9, 12, 16	Contrib. drain. area	= 1.090 ac


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## Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 10.08 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 36,633 cuft
Inflow hyds.	= 20, 21	Contrib. drain. area	= 0.000 ac



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## Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type	= Combine	Peak discharge	= 7.597 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 25,877 cuft
Inflow hyds.	= 4, 5, 10, 11, 15	Contrib. drain. area	= 0.972 ac



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## Hyd. No. 24

SOUTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.330 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.37 hrs
Time interval	= 2 min	Hyd. volume	= 1,045 cuft
Inflow hyd. No.	= 13 - PP-01	Max. Elevation	= 142.50 ft
Reservoir name	= SOUTH POROUS PVMT	Max. Storage	= 2,824 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 25

NORTH POR PVMT

Hydrograph type	= Reservoir	Peak discharge	= 0.237 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.40 hrs
Time interval	= 2 min	Hyd. volume	= 582 cuft
Inflow hyd. No.	= 14 - PP-02	Max. Elevation	= 141.83 ft
Reservoir name	= NORTH POROUS PVMT	Max. Storage	= 3,832 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 26

SOUTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 6.520 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 17,173 cuft
Inflow hyd. No.	= 22 - TO SOUTH INFIL SYS	Max. Elevation	= 144.92 ft
Reservoir name	= SOUTH INFIL SYS	Max. Storage	= 9,945 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 27

NORTH INFIL SYS

Hydrograph type	= Reservoir	Peak discharge	= 5.682 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 12,524 cuft
Inflow hyd. No.	= 23 - TO NORTH INFIL SYS	Max. Elevation	= 144.93 ft
Reservoir name	= NORTH INFIL SYS	Max. Storage	= 6,752 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 28

COMBINE-3

Hydrograph type	= Combine	Peak discharge	= 2.099 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.07 hrs
Time interval	= 2 min	Hyd. volume	= 7,332 cuft
Inflow hyds.	= 17, 18	Contrib. drain. area	= 0.265 ac



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## Hyd. No. 29

### SYSTEM OUTLET

Hydrograph type	= Combine	Peak discharge	= 13.89 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 38,655 cuft
Inflow hyds.	= 24, 25, 26, 27, 28	Contrib. drain. area	= 0.000 ac



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## Hyd. No. 30

TOTAL SITE

Peak discharge = Fime to peak =	= 16.34 cfs = 12.13 hrs
-lyd. volume =	= 57,126 cuft
Contrib. drain. area =	= 1.038 ac
- -	Peak discharge = Time to peak = Hyd. volume = Contrib. drain. area =



# **Tighe&Bond**

**APPENDIX E** 



#### **Required Water Quality Volume (WQV)**

#### 141 Danbury Road

Site Area in Acres, A	=	4.692	ac
Impervious Area in Acres	=	2.905	ac
Percent Impervious Cover, I	=	62	%
Volumetric Runoff Coefficient, R			
R = 0.05 + 0.009(I)	=	0.607	

#### Water Quality Volume (WQV)

WOV = (1'')(R)(A)	= 0.237	ac∙ft
$WQV \equiv \frac{12}{12}$	= 10,342	cf

#### **Provided Water Quality Volume**

North Infiltration System	=	2,912	cf
South Infiltration System	=	4,641	cf
North Porous Pavement System	=	2,313	cf
South Porous Pavement System	=	1,414	cf

= 11,280 cf





Project Name: 141 Danbury Road Project Number: **F0173-002** Project Location: Wilton, CT Description: Stormwater BMP Pollutant Removal Estimate Prepared By: ACF Date: May 12 2021

#### Water Quality Area 1

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.067	0.014	3.561	0.005	0.001	0.005
Proposed, Post Treatment	lb/yr/1-in	0.040	0.003	0.360	0.002	0.000	0.000
Reduction, Pre to Post Treat		40%	78%	90%	64%	70%	90%

#### Water Quality Area 2

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.187	0.038	9.937	0.014	0.003	0.013
Proposed, Post Treatment	lb/yr/1-in	0.111	0.008	1.006	0.005	0.001	0.001
Reduction, Pre to Post Treat		40%	78%	90%	64%	70%	90%

#### Water Quality Area 3

		Pollutant						
Item	Units	TKN	Р	TSS	Pb	Cu	Zn	
Proposed, Pre Treatment	lb/yr/1-in	0.037	0.007	1.962	0.003	0.001	0.003	
Proposed, Post Treatment	lb/yr/1-in	0.027	0.005	1.079	0.002	0.000	0.002	
Reduction, Pre to Post Treat		27%	33%	45%	32%	32%	32%	

#### Water Quality Area 4

		Pollutant						
Item	Units	TKN	Ρ	TSS	Pb	Cu	Zn	
Proposed, Pre Treatment	lb/yr/1-in	0.038	0.008	2.010	0.003	0.001	0.003	
Proposed, Post Treatment	lb/yr/1-in	0.028	0.005	1.105	0.002	0.000	0.002	
Reduction, Pre to Post Treat		27%	33%	45%	32%	32%	32%	

#### Water Quality Area 5

		Pollutant						
Item	Units	TKN	Ρ	TSS	Pb	Cu	Zn	
Proposed, Pre Treatment	lb/yr/1-in	0.091	0.018	4.833	0.007	0.002	0.006	
Proposed, Post Treatment	lb/yr/1-in	0.055	0.011	0.967	0.003	0.001	0.003	
Reduction, Pre to Post Treat		40%	40%	80%	60%	60%	60%	

#### Water Quality Area 6

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Proposed, Post Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Reduction, Pre to Post Treat							

#### Water Quality Area 7

		Pollutant						
Item	Units	TKN	Ρ	TSS	Pb	Cu	Zn	
Proposed, Pre Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000	
Proposed, Post Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000	
Reduction, Pre to Post Treat								

#### Water Quality Area 8

		Pollutant						
Item	Units	TKN	Р	TSS	Pb	Cu	Zn	
Proposed, Pre Treatment	lb/yr/1-in	0.060	0.012	3.178	0.005	0.001	0.004	
Proposed, Post Treatment	lb/yr/1-in	0.036	0.007	0.636	0.002	0.000	0.002	
Reduction, Pre to Post Treat		40%	40%	80%	60%	60%	60%	

#### **Total Site**

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.479	0.097	25.480	0.036	0.008	0.034
Proposed, Post Treatment	lb/yr/1-in	0.296	0.040	5.152	0.015	0.003	0.010
Reduction. Pre to Post Treat		38%	59%	80%	58%	61%	72%

#### **Loading Calculation**

Location:	Area 1		Со	ndition: <b>F</b>	Proposed
Rainfall: Impervious Fraction:	1 0.32	inches	Total Area =	0.4017	acres
Pollutant	<u>Resid</u>	<u>dential</u>		Weig	<u>ghted</u>
	A	EMC		EMC	L (lba().m)
	(acres)	(mg/L)		(mg/L)	(IDS/YF)
Total Nitrogen (N)	0.402	1.900		1.900	0.067
Total Phosphorus (P)	0.402	0.383		0.383	0.014
Total Suspended Solids	0.402	101.0		101.0	3.6
Lead	0.402	0.144		0.144	0.005
Copper	0.402	0.033		0.033	0.001
Zinc	0.402	0.135		0.135	0.005
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
	Pollution	Loading	(lbs/vear)		
EMC	Mean Ev	ent Mean	Concentration (mg/L)		
I	Fraction	of Imperv	vious Acres (acres)		
Р	Annual R	ainfall (in	)		
А	Watersh	ed Area (a	acres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Total Area = 0.4017 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (Ibs)	Lout (Ibs)					
Total Nitrogen (N)	0.067	0.067	0	0.00	0.067					
Total Phosphorus (P)	0.014	0.014	0	0.00	0.014					
Total Suspended Solids	3.561	3.6	20	0.71	2.8					
Lead	0.005	0.005	0	0.00	0.005					
Copper	0.001	0.001	0	0.00	0.001					
Zinc	0.005	0.005	0	0.00	0.005					
Lin 1	Pollutant Load Ar	ea 1								
Sum L	Sum of Pollutant	Load to this	BMP							
RR	Removal rate in p	Removal rate in percentage								
Lout	Pollutant Load ou	it of BMP								

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Total Area = 0.4017 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.067	0.067	18.3	0.01	0.055
Total Phosphorus (P)	0.014	0.014	66.9	0.01	0.004
Total Suspended Solids	2.849	2.8	77	2.19	0.7
Lead	0.005	0.005	46.5	0.00	0.003
Copper	0.001	0.001	56.2	0.00	0.001
Zinc	0.005	0.005	85.3	0.00	0.001
Lin 1	Pollutant Load Out	of Deep S	ump Cat	ch Basins E	3MP
Sum L	Sum of Pollutant Lo	oad to this	BMP		
RR	Removal rate in pe	rcentage			
Lout	Pollutant Load out	of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location:	Area 1
Rainfall:	1 inches
Impervious Fraction:	0.32
BMP:	Infiltration System

Total Area = 0.4017 acres

Pollutant	Lin 1 (Ibs)	Sum L (Ibs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.055	0.055	27	0.01	0.040
Total Phosphorus (P)	0.004	0.004	33	0.00	0.003
Total Suspended Solids	0.655	0.7	45	0.29	0.4
Lead	0.003	0.003	32	0.00	0.002
Copper	0.001	0.001	32	0.00	0.000
Zinc	0.001	0.001	32	0.00	0.000
Lin 1	Pollutant Load ou	t from WQS			
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in p	percentage			
Lout	Pollutant Load ou	t of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location:	Area 2	inches	Co	ondition: <b>P</b>	roposed
Impervious Fraction:	0.37	inches	Total Area =	1.01338	acres
Pollutant	Resid	dential		Weig	<u>ihted</u>
	A	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	1.013	1.900		1.900	0.187
Total Phosphorus (P)	1.013	0.383		0.383	0.038
Total Suspended Solids	1.013	101.0		101.0	9.9
Lead	1.013	0.144		0.144	0.014
Copper	1.013	0.033		0.033	0.003
Zinc	1.013	0.135		0.135	0.013
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (	lbs/year)		
EMC	Mean Ev	ent Mean (	Concentration (mg/L)		
I	Fraction	of Imperv	ious Acres (acres)		
Р	Annual R	ainfall (in)			
A	Watershe	<u>ed Area (a</u>	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Total Area = 1.0134 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (Ibs)	Lout (Ibs)	
Total Nitrogen (N)	0.187	0.187	0	0.00	0.187	
Total Phosphorus (P)	0.038	0.038	0	0.00	0.038	
Total Suspended Solids	9.937	9.9	20	1.99	7.9	
Lead	0.014	0.014	0	0.00	0.014	
Copper	0.003	0.003	0	0.00	0.003	
Zinc	0.013	0.013	0	0.00	0.013	
Lin 1	Pollutant Load A	rea 1				
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in	Removal rate in percentage				
Lout	Pollutant Load o	ut of BMP				

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Area 2	
1 inches	
0.37	
Water Quality Structure	2
	Area 2 1 inches 0.37 Water Quality Structure

Total Area = 1.0134 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.187	0.187	18.3	0.03	0.153
Total Phosphorus (P)	0.038	0.038	66.9	0.03	0.012
Total Suspended Solids	7.949	7.9	77	6.12	1.8
Lead	0.014	0.014	46.5	0.01	0.008
Copper	0.003	0.003	56.2	0.00	0.001
Zinc	0.013	0.013	85.3	0.01	0.002
Lin 1	Pollutant Load Out	t of Deep S	ump Cat	ch Basins E	3MP
Sum L	Sum of Pollutant Load to this BMP				
KR Lout	Removal rate in pe Pollutant Load out	ercentage of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location:	Area 2
Rainfall:	1 inches
Impervious Fraction:	0.37
BMP:	Infiltration System

Total Area = 1.0134 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)	
Total Nitrogen (N)	0.153	0.153	27	0.04	0.111	
Total Phosphorus (P)	0.012	0.012	33	0.00	0.008	
Total Suspended Solids	1.828	1.8	45	0.82	1.0	
Lead	0.008	0.008	32	0.00	0.005	
Copper	0.001	0.001	32	0.00	0.001	
Zinc	0.002	0.002	32	0.00	0.001	
Lin 1	Pollutant Load ou	It from WQS				
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in p	Removal rate in percentage				
Lout	Pollutant Load ou	it of BMP				

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location:	Area 3	inches	C	ondition: <b>F</b>	roposed
Impervious Fraction:	0.00	inches	Total Area =	0.57139	acres
Pollutant	Resid	dential		<u>Weic</u>	<u>ihted</u>
	A	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.571	1.900		1.900	0.037
Total Phosphorus (P)	0.571	0.383		0.383	0.007
Total Suspended Solids	0.571	101.0		101.0	2.0
Lead	0.571	0.144		0.144	0.003
Copper	0.571	0.033		0.033	0.001
Zinc	0.571	0.135		0.135	0.003
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (	lbs/year)		
EMC	Mean Eve	ent Mean (	Concentration (mg/L)		
I	Fraction	of Imperv	ious Acres (acres)		
Р	Annual R	ainfall (in)			
A	Watershe	<u>ed Area (a</u>	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location:	Area 3
Rainfall:	1 inches
Impervious Fraction:	0.00
BMP:	Infiltration System

Total Area = 0.5714 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)	
Total Nitrogen (N)	0.037	0.037	27	0.01	0.027	
Total Phosphorus (P)	0.007	0.007	33	0.00	0.005	
Total Suspended Solids	1.962	2.0	45	0.88	1.1	
Lead	0.003	0.003	32	0.00	0.002	
Copper	0.001	0.001	32	0.00	0.000	
Zinc	0.003	0.003	32	0.00	0.002	
Lin 1	Pollutant Load out	from WQS				
Sum L	Sum of Pollutant L	oad to this	BMP			
RR	Removal rate in pe	Removal rate in percentage				
Lout	Pollutant Load out	of BMP				

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location:	Area 4	inchoc	Co	ondition: <b>F</b>	Proposed
Impervious Fraction:	0.00	inches	Total Area =	0.58535	acres
Pollutant	Resid	dential		<u>Weic</u>	<u>ahted</u>
	А	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.585	1.900		1.900	0.038
Total Phosphorus (P)	0.585	0.383		0.383	0.008
Total Suspended Solids	0.585	101.0		101.0	2.0
Lead	0.585	0.144		0.144	0.003
Copper	0.585	0.033		0.033	0.001
Zinc	0.585	0.135		0.135	0.003
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (	bs/year)		
EMC	Mean Ev	ent Mean (	Concentration (mg/L)		
I	Fraction	of Imperv	ious Acres (acres)		
Р	Annual R	ainfall (in)			
А	Watershe	ed Area (a	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location:	Area 4
Rainfall:	1 inches
Impervious Fraction:	0.00
BMP:	Infiltration System

Total Area = 0.5854 acres

Pollutant	Lin 1 (Ibs)	Sum L (Ibs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.038	0.038	27	0.01	0.028
Total Phosphorus (P)	0.008	0.008	33	0.00	0.005
Total Suspended Solids	2.010	2.0	45	0.90	1.1
Lead	0.003	0.003	32	0.00	0.002
Copper	0.001	0.001	32	0.00	0.000
Zinc	0.003	0.003	32	0.00	0.002
Lin 1	Pollutant Load ou	t from WQS			
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in p	ercentage			
Lout	Pollutant Load out	t of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location:	Area 5	inchoo	Co	ondition: <b>F</b>	roposed
Impervious Fraction:	0.40	inches	Total Area =	0.46886	acres
Pollutant	Resid	<u>lential</u>		<u>Weic</u>	<u>ihted</u>
	A	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(IDS/Yr)
Total Nitrogen (N)	0.469	1.900		1.900	0.091
Total Phosphorus (P)	0.469	0.383		0.383	0.018
Total Suspended Solids	0.469	101.0		101.0	4.8
Lead	0.469	0.144		0.144	0.007
Copper	0.469	0.033		0.033	0.002
Zinc	0.469	0.135		0.135	0.006
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (	lbs/year)		
EMC	Mean Eve	ent Mean	Concentration (mg/L)		
I	Fraction	of Imperv	ious Acres (acres)		
Р	Annual R	ainfall (in)			
A	Watershe	ed Area (a	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location:	Area 5
Rainfall:	1 inches
Impervious Fraction:	0.40
BMP:	Porous Pavement

Total Area = 0.4689 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.091	0.091	40	0.04	0.055
Total Phosphorus (P)	0.018	0.018	40	0.01	0.011
Total Suspended Solids	4.833	4.8	80	3.87	1.0
Lead	0.007	0.007	60	0.00	0.003
Copper	0.002	0.002	60	0.00	0.001
Zinc	0.006	0.006	60	0.00	0.003
Lin 1	Pollutant Load ou	ut from WQS			
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in percentage				
Lout	Pollutant Load ou	ut of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location:	Area 8	inches	Co	ondition: <b>F</b>	roposed
Rainfail: Impervious Fraction:	1 0.33	Inches	Total Area =	0.34885	acres
Pollutant	Resid	dential		<u>Weic</u>	<u>ihted</u>
	A	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.349	1.900		1.900	0.060
Total Phosphorus (P)	0.349	0.383		0.383	0.012
Total Suspended Solids	0.349	101.0		101.0	3.2
Lead	0.349	0.144		0.144	0.005
Copper	0.349	0.033		0.033	0.001
Zinc	0.349	0.135		0.135	0.004
	L = 0.22	66 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (	lbs/year)		
EMC	Mean Ev	ent Mean	Concentration (mg/L)		
I	Fraction	of Imperv	ious Acres (acres)		
Р	Annual R	ainfall (in)	)		
А	Watershe	ed Area (a	icres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location:	Area 8
Rainfall:	1 inches
Impervious Fraction:	0.33
BMP:	Porous Pavement

Total Area = 0.3489 acres

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (-)	Lremoved (Ibs)	Lout (Ibs)
Total Nitrogen (N)	0.060	0.060	40	0.02	0.036
Total Phosphorus (P)	0.012	0.012	40	0.00	0.007
Total Suspended Solids	3.178	3.2	80	2.54	0.6
Lead	0.005	0.005	60	0.00	0.002
Copper	0.001	0.001	60	0.00	0.000
Zinc	0.004	0.004	60	0.00	0.002
Lin 1	Pollutant Load o	ut from WQS			
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in percentage				
Lout	Pollutant Load o	ut of BMP			

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

# **Tighe&Bond**

**APPENDIX F** 



Location: Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.007	0.95	0.007
Landscaped and Lawns	0.187	0.30	0.056
			0.063
Total Area:	0.194	C:	0.32

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)						
A-B	0.24	3.54	130	0.030	14.2	

Total Tc (min) = 14.2

Name: CB-01A

Location: Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.024	0.95	0.023
Landscaped and Lawns	0.080	0.30	0.024
			0.047
Total Area:	0.104	C:	0.45

Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)					
A-B	0.24	3.54	50	0.020	7.8	

Total Tc (min) = 7.8



Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.047	0.95	0.045
Landscaped and Lawns	0.001	0.30	0.000
			0.045
Total Area:	0.048	C:	0.94

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)					Time (min)
A-B	0.015	3.54	23	0.050	0.3

 Total Tc (min) =
 0.3

 Minimum Tc =
 5.0

Name: CB-03

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.051	0.95	0.049
Landscaped and Lawns	0.023	0.30	0.007
			0.056
Total Area:	0.074	C:	0.75

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (mir						
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	60	0.033	0.8	

 Total Tc (min) =
 4.5

 Minimum Tc =
 5.0



Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.045	0.95	0.043
Landscaped and Lawns	0.011	0.30	0.003
			0.046
Total Area:	0.056	C:	0.82

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min						
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	55	0.045	0.7	

 Total Tc (min) =
 4.4

 Minimum Tc =
 5.0

Name: CB-05

Location:

Proposed Catch Basin - Driveway

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.101	0.95	0.096
Landscaped and Lawns	0.061	0.30	0.018
			0.114
Total Area:	0.162	C:	0.70

Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min)						
A-B	0.24	3.54	30	0.020	5.2	
B-C	0.015	3.54	90	0.040	1.0	

Total Tc (min) = <u>6.2</u>



Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.048	0.95	0.046
Landscaped and Lawns	0.014	0.30	0.004
			0.050
Total Area:	0.062	C:	0.80

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min						
A-B	0.24	3.54	22	0.020	4.0	
B-C	0.015	3.54	58	0.025	0.9	

 Total Tc (min) =
 4.9

 Minimum Tc =
 5.0

Name: CB-07

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.080	0.95	0.076
Landscaped and Lawns	0.019	0.30	0.006
			0.082
Total Area:	0.099	C:	0.83

Time of Concentration:

Sheet-Flow Travel Time						
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (min)						
A-B	0.24	3.54	15	0.020	3.0	
B-C	0.015	3.54	115	0.035	1.3	

Total Tc (min) = 4.3 Minimum Tc = 5.0



Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.095	0.95	0.090
Landscaped and Lawns	0.022	0.30	0.007
			0.097
Total Area:	0.117	C:	0.83

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	30	0.040	3.9
B-C	0.015	3.54	140	0.035	1.5

Total Tc (min) = 5.5

Name: CB-09

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.117	0.95	0.111
Landscaped and Lawns	0.020	0.30	0.006
			0.117
Total Area:	0.137	C:	0.85

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	120	1.000	0.4

 Total Tc (min) =
 4.1

 Minimum Tc =
 5.0


### Name: CB-10

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.103	0.95	0.098
Landscaped and Lawns	0.031	0.30	0.009
			0.107
Total Area:	0.134	C:	0.80

### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	30	0.040	3.9	
B-C	0.015	3.54	135	1.000	0.4	

 Total Tc (min) =
 4.3

 Minimum Tc =
 5.0

Name: CB-11

Location: Proposed Yard Drain - Southeast Corner Site

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.000	0.95	0.000
Landscaped and Lawns	0.227	0.30	0.068
			0.068
Total Area:	0.227	C:	0.30

Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) Time (m				Time (min)	
A-B	0.24	3.54	130	0.050	11.6	

Total Tc (min) = 11.6



### Name: RF-01

Location: Proposed Building - North

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.571	0.95	0.543
Landscaped and Lawns	0.000	0.30	0.000
			0.543
Total Area:	0.571	C:	0.95

### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0

Name: RF-02

Location: Proposed Building - South

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.585	0.95	0.556
Landscaped and Lawns	0.000	0.30	0.000
			0.556
Total Area:	0.585	C:	0.95

### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P2 (in) Flow Length (ft) Slope (ft/ft) 1					Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = 1.0 Minimum Tc = 5.0



### Name: RF-03

Location: Proposed Building - Northwest

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.138	0.95	0.131
Landscaped and Lawns	0.000	0.30	0.000
			0.131
Total Area:	0.138	C:	0.95

### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

 Total Tc (min) =
 1.0

 Minimum Tc =
 5.0

Name: RF-04

Location: Proposed Building - Southwest

Cover Type	Area (ac)	С	A x C
Pavement / Impervious	0.127	0.95	0.121
Landscaped and Lawns	0.000	0.30	0.000
			0.121
Total Area:	0.127	C:	0.95

### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = 1.0 Minimum Tc = 5.0

# Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Station Len Drng Area Rnoff Area x C Tc Rain Total Cap Vel		Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID												
Line	То	_	Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	fuli		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	End 1 2 3 2 1 1 7 End 9 10 11 12 13 14 15 16 13 End 19 20 21 22	76.000 178.000 192.000 52.600 37.000 58.500 5.000 30.400 96.000 87.000 53.300 97.600 23.900 66.300 66.300 66.000 53.000 27.400 105.100 167.900 96.700	0.00 0.00 0.00 0.00 0.00 0.26 0.00 0.12 0.10 0.06 0.00 0.12 0.10 0.23 0.00 0.13 0.14 0.07 0.06	0.26 0.00 0.00 0.00 0.00 0.26 0.00 1.01 1.01 0.89 0.79 0.73 0.50 0.34 0.29 0.10 0.23 0.40 0.27 0.13 0.06	0.00 0.00 0.00 0.00 0.00 0.00 0.95 0.00 0.83 0.83 0.83 0.80 0.70 0.94 0.32 0.45 0.30 0.00 0.88 0.75 0.82	0.00 0.00 0.00 0.00 0.00 0.25 0.00 0.10 0.08 0.05 0.00 0.11 0.05 0.06 0.05 0.07 0.00 0.12 0.05	0.25 0.00 0.00 0.00 0.25 0.00 0.57 0.57 0.57 0.47 0.33 0.27 0.15 0.11 0.05 0.07 0.32 0.32 0.32 0.10 0.05	0.0 0.0 0.0 0.0 5.0 0.0 5.0 5.0 5.0 5.0	16.9 1.3 0.2 0.0 0.0 15.3 0.0 16.6 16.4 15.9 15.6 15.3 14.9 15.6 15.3 14.7 14.2 7.8 11.6 7.6 7.5 7.0 5.8 5.0	4.7 0.0 0.0 0.0 4.9 0.0 4.7 4.7 4.8 4.9 5.0 5.1 5.2 7.0 5.8 7.1 7.2 7.4 8.0 8.6	7.79 6.40 3.00 3.40 1.27 0.05 2.68 2.69 2.26 1.88 1.65 1.34 0.77 0.56 0.33 0.39 2.29 2.30 1.61 0.79 0.39	8.04 11.05 9.85 9.65 7.00 2.80 3.32 3.33 3.34 2.38 2.39 1.69 0.00 3.38 6.36 6.09 4.71	4.41 4.20 2.88 4.43 5.07 0.25 0.06 3.41 3.43 3.02 4.16 3.62 3.98 2.49 2.05 2.04 1.55 2.91 3.64 3.36 2.41 1.96	18 18 18 15 15 12 12 12 12 12 12 12 12 12 10 10 10 10 12 12 12 12	0.50 0.94 0.75 1.90 1.00 13.30 0.50 0.50 0.50 0.50 0.74 0.75 0.75 0.79 1.00 1.01 1.02 0.51 0.00 0.77 2.72 2.50 1.49	138.50 138.88 140.56 142.00 142.63 138.88 139.23 142.00 143.00 143.16 144.38 145.03 146.39 147.36 147.36 147.36 147.36 148.03 145.43 142.00 143.21 146.07 150.26	138.88 140.56 142.00 143.00 143.00 140.21 139.23 139.52 142.00 143.16 143.87 145.03 145.43 145.43 145.70 148.03 148.70 145.70 142.00 143.21 146.07 150.26 151.70	140.44 141.10 141.97 142.66 143.24 141.10 141.11 143.84 144.04 144.43 144.92 145.61 146.80 147.85 147.97 148.36 145.98 143.79 143.94 143.86 146.61 150.63	140.80 141.62 142.66 143.70 143.74 141.10 141.11 143.86 144.16 144.72 145.61 145.98 147.85 147.97 148.36 148.36 148.95 146.02 143.81 143.86 146.63 151.96	141.50 142.82 145.79 145.79 142.82 142.82 143.80 146.33 146.33 146.33 146.10 148.30 151.60 152.50 150.70 152.50 146.50 146.50 146.50 146.30 149.70 154.70	142.82 145.79 145.97 146.50 146.33 144.30 143.90 146.33 146.10 148.30 151.60 151.60 152.50 150.70 150.70 150.70 146.50 146.30 149.70 154.70	
Proje	ect File:	F0173-	02 Storr	n Sewer	s Model.	stm										Number	r of lines: 2	23		Run Dat	e: 5/27/20	)21
NOT	ES:Inte	ensity = 3	8.51 / (	nlet time	e + 3.60)	^ 0.70; I	Return p	eriod =Y	′rs. 25;	c = cir	e = ellip	b = box										

# **Storm Sewer Tabulation**

# **Tighe&Bond**

**APPENDIX G** 

141 Danbury Road Residential Development Wilton, Connecticut

# **Maintenance and Inspection Plan**

May 2021

The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, roof leaders, piping, hydrodynamic separators, underground infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures</u>: The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator</u>: The Contech CDS units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand, and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration</u>: The underground infiltration system will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader</u>: The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plan species or tree saplings.

<u>Pavement:</u> Paved areas shall be swept periodically by the Owner to clean trash and other debris. The Owner will sweep paved areas on its property in the spring to remove winter accumulations of road sand.

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

## Drainage Structures Inspection

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

# Underground Infiltration

The underground infiltration system shall be inspected annually and will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

# **Pavement Inspection**

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

# **Tighe&Bond**

**APPENDIX H** 

Questions	concerning	the	VERTCON	process	may	be	mailed	to	NGS	
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Latitude:	41.179			
Longitude: 073	.417			
NGVD 29 height	:			
Datum shift(NAV	0 88 minus NGVD 29 <b>):</b>	-0.329 meter = -1.07 feet		

# TABLE 5 - SUMMARY OF DISCHARGES - continued

			PEAK DISC	HARGES (cfs)	
		10-	2-	1-	0.2-
	DRAINAGE	PERCENT-	PERCENT-	PERCENT-	PERCENT-
FLOODING SOURCE	AREA	ANNUAL-	ANNUAL-	ANNUAL-	ANNUAL-
AND LOCATION	(sq. miles)	<u>CHANCE</u>	<u>CHANCE</u>	<u>CHANCE</u>	<u>CHANCE</u>
NOROTON RIVER -					
continued					
At Jelliff Mill Road	4 38	520	890	1 080	1 900
Upstream of Mead Park	1.90	220	390	460	820
Upstream of Wahackne	1190	220	570	100	020
Road	0.79	90	160	200	340
Upstream of Greenley	0172	20	100	200	0.0
Road	0.43	50	90	110	190
NORTH FARRAR					
BROOK					
At the confluence with					
the Pequonnock River					
(Upper Reach)	0.46	100	245	350	780
At the Trumbull-Monroe					
corporate limits	0.03	10	25	35	80
NORWALK RIVER					
Upstream of confluence					
of Betts Pond Brook	57.6	4,100	9,500	14,000	16,250
Upstream of confluence					
of Silvermine River	32.8	2,600	6,300	9,100	20,000
At Kent Road	30.0	2,980	5,840	7,455	12,505
Downstream of					
confluence of					
Comstock Brook	25.7	2,680	5,280	6,735	11,295
Upstream of confluence					
of Comstock Brook	18.4	1,845	3,660	4,675	7,840
Downstream of					
confluence of Gilbert					
and Bennett Brooks	13.8	1,425	2,865	3,655	6,135
Upstream of confluence					
of Gilbert and Bennett					
Brooks	12.3	1,205	2,445	3,125	5,240
Downstream of the					
confluence of Cooper					
Pond Brook	11.13	1,010	2,085	2,665	4,475
Upstream of the					
confluence of Cooper	a =-				
Pond Brook	8.73	665	1,250	1,595	2,680

# Norwalk River Calibrated (Duplicate Effective) Model Output Table

HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	29920	10%	2980.00	147.00	152.32	152.32	153.29	0.004454	9.23	671.47	438.66	0.75
Reach-1	29920	2%	5840.00	147.00	153.56	153.56	154.60	0.004481	10.83	1400.71	673.09	0.79
Reach-1	29920	1%	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86	1676.50	693.44	0.83
Reach-1	29920	0.2%	12505.00	147.00	154.99	154.99	156.40	0.005722	14.14	2414.85	738.35	0.92
Reach-1	29760	10%	2980.00	142.20	148.53		149.01	0.001498	5.62	583.13	179.68	0.44
Reach-1	29760	2%	5840.00	142.20	151.31		151.93	0.001165	6.63	1125.96	211.79	0.42
Reach-1	29760	1%	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	29760	0.2%	12505.00	142.20	154.28		155.51	0.001589	9.59	1814.00	255.42	0.51
Reach-1	28240	10%	2980.00	138.00	145.34		146.30	0.002090	7.99	445.85	151.41	0.55
Reach-1	28240	2%	5840.00	138.00	146.52	146.52	148.75	0.004139	12.55	696.60	258.98	0.79
Reach-1	28240	1%	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	28240	0.2%	12505.00	138.00	149.76	149.76	151.98	0.003397	14.32	1979.91	552.23	0.76
Reach-1	27468	10%	2980.00	132.10	145.99		145.99	0.000005	0.60	9140.64	793.45	0.03
Reach-1	27468	2%	5840.00	132.10	146.99		146.99	0.000017	1.11	9943.03	813.12	0.05
Reach-1	27468	1%	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	27468	0.2%	12505.00	132.10	148.85		148.88	0.000052	2.13	11529.28	890.79	0.10
Reach-1	27110	10%	2980.00	136.60	145.97		145.99	0.000064	1.74	4765.52	962.48	0.10
Reach-1	27110	2%	5840.00	136.60	146.94		146.97	0.000148	2.83	5707.19	991.44	0.16
Reach-1	27110	1%	7455.00	136.60	147.46		147.51	0.000187	3.29	6234.70	1005.58	0.18
Reach-1	27110	0.2%	12505.00	136.60	148.74		148.82	0.000304	4.52	7518.38	1009.50	0.23
Reach-1	27025	10%	2980.00	135.50	145.63	141.84	145.90	0.000562	5.28	1759.35	880.05	0.30
Reach-1	27025	2%	5840.00	135.50	145.74	145.59	146.68	0.001965	9.96	1855.68	883.55	0.56
Reach-1	27025	1%	7455.00	135.50	146.24	146.03	147.20	0.002112	10.68	2304.78	899.67	0.59
Reach-1	27025	0.2%	12505.00	135.50	147.33	147.10	148.46	0.002654	12.81	3304.65	934.56	0.67
Reach-1	27020		Bridge									
Reach-1	27015	10%	2980.00	135.50	141.85	141.85	144.38	0.006857	13.22	278.63	62.97	0.97
Reach-1	27015	2%	5840.00	135.50	145.62	145.62	146.66	0.002172	10.38	1752.24	879.80	0.59
Reach-1	27015	1%	7455.00	135.50	146.08	146.08	147.18	0.002399	11.26	2163.67	894.64	0.63
Reach-1	27015	0.2%	12505.00	135.50	147.11	147.11	148.43	0.003090	13.64	3099.86	927.52	0.72
Reach-1	26680	10%	2980.00	134.00	140.31	140.08	141.21	0.004091	9.97	762.74	365.85	0.74
Reach-1	26680	2%	5840.00	134.00	142.16		142.88	0.003007	10.34	1642.26	560.63	0.67
Reach-1	26680	1%	7455.00	134.00	142.90		143.58	0.002777	10.58	2066.21	590.20	0.65
Reach-1	26680	0.2%	12505.00	134.00	145.35		145.79	0.001646	9.70	3857.15	759.13	0.52
Reach-1	26209	10%	2980.00	133.40	140.62		140.66	0.000240	1.93	2591.95	867.42	0.17
Reach-1	26209	2%	5840.00	133.40	142.35		142.41	0.000238	2.43	4170.98	944.15	0.18
Reach-1	26209	1%	7455.00	133.40	143.05		143.12	0.000251	2.70	4830.47	949.47	0.19
Reach-1	26209	0.2%	12505.00	133.40	145.37		145.47	0.000223	3.12	7059.39	967.22	0.19
Reach-1	26136	10%	2980.00	130.20	139.77	136.89	140.44	0.001214	7.36	865.42	504.59	0.44
Reach-1	26136	2%	5840.00	130.20	141.38	140.68	142.16	0.001499	9.14	1847.21	666.49	0.50
Reach-1	26136	1%	7455.00	130.20	142.12	141.28	142.88	0.001499	9.56	2353.38	704.50	0.50
Reach-1	26136	0.2%	12505.00	130.20	144.86	142.59	145.33	0.000938	8.76	4394.50	760.00	0.41
Deert d	06107.5		D.1									
Reach-1	26127.5		Bridge									
Deert d	06140	100/	0000.05	404.05	400.00	400.00	400.05	0.001015		4050.05	F 4 4 4 -	
Reach-1	20119	10%	2980.00	131.30	138.62	136.96	138.86	0.001012	5.17	1356.28	541.45	0.36
Reach-1	26119	2%	5840.00	131.30	141.25	138.61	141.42	0.000572	4.88	3054.77	719.80	0.28
Reach-1	20119	0.20/	1455.00	131.30	142.26	138.86	142.42	0.000529	5.03	3/91.17	742.95	0.28
Reach-1	20119	0.2%	12505.00	131.30	144.97	140.05	145.13	0.000437	5.35	5865.51	//8.00	0.26
Reach 1	26059	10%	2000 00	104.00	120 50		120 70	0.004000	E 00	1200.05	E04 00	0.07
Reach 1	20030	2%	2900.00	101.00	1/1 22		1.10.79	0.001092	0.03	3036 55	717 66	0.37
Reach-1	20050	2 /0	7455.00	131.30	141.22		141.30	0.000580	4.92	3020.33	717.00	0.29
Reach 1	20050	0.2%	19505 00	121.30	142.22		142.38	0.000539	5.00	5/04.00	770.00	0.28
Reduit-1	20030	0.2 /0	12005.00	131.30	144.94		145.10	0.000442	5.37	5045.13	110.00	0.26
Reach-1	25358	10%	2080 00	131 00	137 00		138 12	0 000730	/ 91	150/ 09	436 04	0.33
Reach-1	25358	2%	5840.00	131.00	1/0 85		1/0 00	0.000739	4.01	2885 25	162 20	0.00
Reach-1	25358	1%	7/55 00	131.00	140.00		140.99	0.000527	5.13	2000.00	400.00 501.77	0.29
Reach-1	25358	0.2%	12505.00	131.00	141.04		142.00	0.000548	0.09 6 / 0	5013 74	625.96	0.30
i teatil-1	20000	J.Z /0	12000.00	131.00	144.00		144.70	0.000543	0.46	5013.74	000:00	0.31
Reach-1	24597	10%	2080 00	127 00	137 64		137 70	0.000/15	2.74	008 33	167 01	0.22
Reach-1	24507	2%	58/0.00	127.00	1/1.04		1/1 60	0.000415	1 70	1/77 02	207.21	0.22
Reach 1	24507	1%	7455 00	127.90	140.33		140.00	0.000402	4.72	14/1.03	202.08	0.24
Reach-1	24597	0.2%	12505.00	127.90	141.20		141.08	0.000532	0.03 6 50	3250 65	401.39	0.20
Reduit-1	24391	0.2 /0	12005.00	127.90	145.91		144.30	0.000614	0.00	3239.05	5/0.34	0.29
Reach-1	24560	10%	2020 00	127.00	197 15	120 70	137 67	0.001050	E 70	515 00	160 / /	0.25
Reach 1	24560	2%	2900.00	107.00	140.00	132.19	140 50	0.001052	01.0	1076 45	100.44	0.35
rteach-1	24000	∠ 70	5840.00	127.90	140.28	135.20	140.58	0.000520	4.99	13/0.45	2/4.15	0.26

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	24560	1%	7455.00	127.90	141.24	136.38	141.56	0.000537	5.35	1773.46	485.12	0.26
Reach-1	24560	0.2%	12505.00	127.90	143.88	139.30	144.28	0.000619	6.52	3245.22	576.17	0.29
Decel 4	04540.5		Duidaa									
Reach-1	24542.5		Bridge									
Reach-1	24525	10%	2980.00	127 20	135 27	133 49	136.46	0.003361	9.08	507 48	212.95	0.60
Reach-1	24525	2%	5840.00	127.20	138.57	136.74	139.62	0.002188	9.45	1358.71	342.03	0.52
Reach-1	24525	1%	7455.00	127.20	139.76	137.71	140.91	0.002189	10.16	1844.44	449.44	0.53
Reach-1	24525	0.2%	12505.00	127.20	142.35	139.79	143.79	0.002461	12.32	3395.84	811.45	0.58
Reach-1	24457	10%	2980.00	127.20	133.42	133.42	136.00	0.007504	12.96	249.76	64.13	1.00
Reach-1	24457	2%	5840.00	127.20	136.74	136.74	139.26	0.004358	13.68	858.70	241.86	0.82
Reach-1	24457	1%	7455.00	127.20	137.78	137.78	140.54	0.004328	14.71	1121.20	262.63	0.84
Reach-1	24457	0.2%	12505.00	127.20	140.59	140.59	143.45	0.003743	16.22	2228.03	492.18	0.81
	04405	100/	0000.00	101.00	400.05	100.00	100.11	0.000004	7.40	447.00	70.00	0.55
Reach-1	24105	10%	2980.00	124.80	132.65	130.63	133.44	0.002381	7.13	417.66	78.83	0.55
Reach-1	24105	2%	5840.00	124.80	134.03	132.93	130.19	0.003492	10.03	582.32	262.38	0.69
Reach-1	24105	1%	12505.00	124.80	135.37	134.00	137.42	0.004065	0.47	3845.46	1520.09	0.75
Tteach-1	24103	0.270	12303.00	124.00	130.30	107.07	155.45	0.001714	3.41	3043.40	1320.03	0.52
Reach-1	23805	10%	2980.00	124.00	132.38		132.87	0.001170	6.13	997.32	331.23	0.41
Reach-1	23805	2%	5840.00	124.00	134.65		135.32	0.001300	7.78	1933.43	474.68	0.45
Reach-1	23805	1%	7455.00	124.00	135.65		136.39	0.001316	8.38	2427.76	508.37	0.46
Reach-1	23805	0.2%	12505.00	124.00	138.18		138.99	0.001278	9.55	4409.49	1582.59	0.47
Reach-1	23415	10%	2980.00	123.00	129.81	129.81	131.82	0.006096	11.90	404.45	161.55	0.89
Reach-1	23415	2%	5840.00	123.00	132.27	132.27	134.30	0.004596	13.19	1159.47	343.43	0.82
Reach-1	23415	1%	7455.00	123.00	133.11	133.11	135.33	0.004719	14.27	1451.84	358.59	0.84
Reach-1	23415	0.2%	12505.00	123.00	135.13	135.13	137.89	0.005069	16.96	2245.13	422.31	0.91
	00474	4000	0000.00	100.00	100.75		100.10	0.00000.4	0.07	155 70	101.00	0.57
Reach-1	23171	10%	2980.00	120.30	128.75	100.10	129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2 70	7455.00	120.30	129.79	129.12	131.57	0.003575	0.01	012.49	264.15	0.67
Reach-1	23171	0.2%	12505.00	120.30	131.12	130.65	135.49	0.003907	7.84	1880.08	204.13	0.07
Tteach-1	20171	0.270	12303.00	120.50	104.00		133.10	0.001732	7.04	1000.00	555.25	0.44
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	1%	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	23036	0.2%	12505.00	121.70	134.55		134.98	0.000237	3.32	2572.37	391.51	0.18
Reach-1	22916	10%	2980.00	121.00	128.01	126.93	128.88	0.002603	8.01	570.82	302.03	0.57
Reach-1	22916	2%	5840.00	121.00	130.41		130.84	0.000999	6.20	1483.60	430.42	0.38
Reach-1	22916	1%	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Decel 4	00705	400/	0000.00	444.00	400.40		400.50	0.000140	0.50	4 400 00	004.00	0.42
Reach-1	22/65	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	2 70	7455.00	114.20	131.64		130.70	0.000299	3.90	2020.14	511 01	0.19
Reach-1	22765	0.2%	12505.00	114.20	134.64		134.84	0.000301	4.13	4324 67	669.64	0.13
	22100	0.270	12000.00	114.20	104.04		104.04	0.000240	4.22	4024.01	000.04	0.17
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27		130.51	0.001575	4.56	1791.09	483.52	0.26
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
Reach-1	22140	10%	2980.00	117.00	124.05	124.05	126.26	0.006734	12.84	391.36	132.65	0.95
Reach-1	22140	2%	5840.00	117.00	126.77	126.77	129.42	0.005440	14.96	889.23	205.48	0.91
Reach-1	22140	1%	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
Deach 1	01005	100/	2080.00	115.00	101.00	101 75	100.65	0.007091	11 17	214 54	94.01	0.07
Reach-1	21025	20%	2960.00	115.90	121.00	121.75	123.03	0.007961	12.42	514.54 604.09	170.14	0.97
Reach-1	21025	2 70	7455.00	115.90	124.12	124.12	120.73	0.006551	13.42	947.00	220.00	0.94
Reach-1	21825	0.2%	12505.00	115.90	131.24	123.20	132.45	0.001436	10.39	3430.35	1045.30	0.50
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.97	0.002174	7.62	390.83	103.38	0.55
Reach-1	21770	2%	5840.00	115.40	124.17	122.36	126.07	0.003067	11.07	527.79	119.93	0.68
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Reach-1	21757.5		Bridge									
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach-1	21745	1%	7455.00	115.40	124.48	123.47	127.36	0.004410	13.60	547.97	122.37	0.83
Reach-1	21745	0.2%	12505.00	115.40	126.94	126.53	131.79	0.005288	17.67	707.72	141.67	0.94

HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1 (Continued)

### HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21695	10%	2980.00	114.20	121.74	120.15	122.74	0.003025	8.01	371.94	69.60	0.61
Reach-1	21695	2%	5840.00	114.20	123.69	122.46	125.72	0.004430	11.42	511.32	74.77	0.76
Reach-1	21695	1%	7455.00	114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1	21695	0.2%	12505.00	114.20	127.45	127.45	130.78	0.004531	14.98	1124.07	292.57	0.82
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

## Norwalk River Existing Conditions (Corrected Effective) Model Output Table

HEC-RAS Plan: EXIST River: RIVER-1 Reach: Reach-1 Min Ch El W.S. Elev Crit W.S. Vel Chnl Froude # Chl Reach River Sta Profile Q Total E.G. Elev E.G. Slope Flow Area Top Width (ft/ft) (ft/s) (cfs) (ft) (ft) (sq ft) (ft) (ft) (ft) 29920 10% 152.32 0.004454 671.47 438.66 0.75 Reach-1 147.00 152.32 153.29 9.23 2980.00 147.00 153.56 10.83 1400.71 0.79 Reach-1 29920 5840.00 153.56 154.60 0.004481 673.09 2% 29920 1% 147.00 153.96 153.96 0.004919 11.86 1676.50 693.44 0.83 Reach-1 7455.00 155.12 147.00 Reach-1 29920 0.2% 12505.00 154.99 154.99 156.40 0.005722 14.14 2414.85 738.35 0.92 Reach-1 29760 10% 2980.00 142 20 148 53 149 01 0.001498 5.62 583.07 179 68 0 44 Reach-1 29760 2% 5840.00 142 20 151.31 151.93 0.001165 6.63 1125.96 211 79 0.42 29760 1% 7455.00 142.20 152.19 152.97 0.001276 7.45 1317.25 222.00 0.44 Reach-1 Reach-1 29760 0.2% 12505.00 142.20 154.28 155.51 0.001589 9.59 1814.00 255.42 0.51 Reach-1 28240 10% 2980.00 138.00 145.39 146.32 0.002036 7.92 452.97 156.57 0.54 28240 5840.00 138.00 146.52 146.52 148.75 0.004139 12.55 696.60 258.98 0.79 Reach-1 2% 1% 147.71 147.71 28240 7455.00 138.00 0.003506 12.69 1059.97 366.77 0.75 Reach-1 149.80 28240 0.2% 138.00 149.76 149.76 151.98 0.003397 14.32 1979.9 552.23 0.76 Reach-1 12505.00 Reach-1 28020 10% 2980.00 136.33 146.00 146.01 0.000055 1.53 4394.50 676.05 0.09 Reach-1 28020 2% 5840.00 136.33 147.00 147.03 0.000131 2.54 5105.56 745.73 0.14 Reach-1 28020 1% 7455.00 136.33 147.55 147.59 0.000166 2.97 5519.40 766.71 0.16 0.2% 12505.00 136.33 148.88 148.97 0.000263 4.06 6569.85 803.73 0.21 Reach-1 28020 27930 146.00 721.01 0.08 Reach-1 10% 2980.00 135.65 146.01 0.000046 1.46 4590.19 Reach-1 27930 2% 5840.00 135.65 146.99 147.02 0.000106 2.38 5340.23 774.68 0.13 Reach-1 27930 1% 7455.00 135.65 147.54 147.58 0.000132 2.76 5765.37 785.36 0.15 0.2% 27930 135.65 148.86 3.72 6803.94 788.32 0.19 Reach-1 12505.00 148.95 0.000207 0.08 Reach-1 27830 10% 134.60 145.99 1.37 4836.61 785.83 2980.00 146.00 0.000037 Reach-1 27830 2% 5840.00 134.60 146.98 147.01 0.000084 2.20 5662.42 869.13 0.12 Reach-1 27830 1% 7455.00 134.60 147.53 147.57 0.000104 2.52 6148.13 920.10 0.13 Reach-1 27830 0.2% 12505.00 134.60 148.85 148.92 0.000153 3.29 7437.92 1023.96 0.16 Reach-1 27790 10% 2980.00 134.60 145.99 146.00 0.000035 1.33 4920.80 803.92 0.08 146.98 Reach-1 27790 2% 5840.00 134.60 147.01 0.000079 2.13 5783.83 928.44 0.11 Reach-1 27790 1% 7455.00 134.60 147.53 147.56 0.000097 2.43 6299.40 970.45 0.13 27790 0.2% 12505.00 134.60 148.85 148.92 0.000139 7665.44 1110.26 0.16 Reach-1 3.14 Reach-1 27468 132.10 145.99 9140.64 793.45 0.03 10% 2980.00 145.99 0.000005 0.60 0.05 132.10 1.11 Reach-1 27468 2% 5840.00 146.99 146.99 0.000017 9943.03 813.12 Reach-1 27468 1% 7455.00 132.10 147.53 147.54 0.000024 1.37 10389.13 832.33 0.06 Reach-1 27468 0.2% 12505.00 132.10 148.85 148.88 0.000052 2.13 11529.28 890.79 0.10 Reach-1 27110 10% 2980.00 136.60 145.97 145.99 0.000064 1.74 4765.52 962.48 0.10 Reach-1 27110 2% 5840.00 136.60 146.94 146.97 0.000148 2.83 5707.19 991.44 0.16 Reach-1 27110 1% 7455.00 136.60 147.46 147.51 0.000187 3.29 6234.70 1005.58 0.18 27110 0.2% 12505.00 136.60 148.74 148.82 0.000304 4.52 7518.38 1009.50 0.23 Reach-1 Reach-1 27025 10% 135.50 145.63 141.84 145.90 0.000562 5.28 1759.35 880.05 0.30 2980.00 135.50 145.74 0.001965 9.96 1855.68 0.56 Reach-1 27025 2% 5840.00 145.59 146.68 883.55 1% 10.68 0.59 Reach-1 27025 7455.00 135.50 146.24 146.03 147.20 0.002112 2304.78 899.67 Reach-1 27025 0.2% 12505.00 135.50 147.33 147.10 148.46 0.002654 12.81 3304.65 934.56 0.67 Reach-1 27020 Bridge Reach-1 27015 10% 2980.00 135.50 141.85 141.85 144.38 0.006857 13.22 278.63 62.97 0.97 135.50 0.002172 0.59 Reach-1 27015 2% 5840.00 145.62 145.62 146.66 10.38 1752.24 879.80 27015 1% 7455.00 135.50 146.08 146.08 147.18 0.002399 11.26 2163.67 894.64 0.63 Reach-1 147.11 27015 0.2% 147.11 148.43 0.003090 13.64 3099.86 927.52 0.72 Reach-1 12505.00 135.50 26680 140.08 0.76 Reach-1 10% 134.00 140.25 141.20 0.004316 10.17 742.52 359.88 2980.00 Reach-1 26680 2% 5840.00 134.00 142.16 142.88 0.003007 10.34 1642.30 560.63 0.67 0.002787 Reach-1 26680 1% 7455.00 134.00 142.89 143.57 10.60 2063.23 590.00 0.65 Reach-1 26680 0.2% 12505.00 134.00 145.43 145.86 0.001574 9.53 3920.70 759.51 0.51 26209 10% 133.40 140.59 140.63 0.000247 1.94 2566.09 865.64 0.17 Reach-1 2980.00 2% 5840.00 133.40 142.35 142.41 0.000238 2.43 4171.02 944.15 0.18 Reach-1 26209 1% Reach-1 26209 7455.00 133.40 143.04 143.12 0.000252 2.70 4826.43 949.44 0.19 26209 0.2% 12505.00 133.40 145.45 145.54 0.000216 3.09 7137.65 967.83 0.18 Reach-1 Reach-1 26136 10% 130.20 139.70 136.89 140.40 0.001266 7.48 832.78 483.49 0.44 2980.00 26136 5840.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.50 Reach-1 2% 1% 0.001511 Reach-1 26136 7455.00 130.20 142.10 141.28 142.87 9.59 2344.50 703.85 0.51 Reach-1 26136 0.2% 12505.00 130.20 144.97 142.59 145.41 0.000893 8.59 4476.35 760.00 0.40 Reach-1 26127.5 Bridge Reach-1 26119 10% 2980.00 131.30 137.79 136.96 139.43 0.004828 10.33 444.27 0.76 305.18 Reach-1 26119 2% 5840.00 131.30 141.23 138.61 141.40 0.000580 4.90 3038.66 718.58 0.29

HEC-RAS P	lan: EXIST Ri	ver: RIVER-1	Reach: Reach-	1 (Continued)								
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	26119	1%	7455.00	131.30	142.25	138.86	142.41	0.000532	5.04	3781.94	742.73	0.28
Reach-1	20119	0.2%	12505.00	131.30	145.07	140.05	145.23	0.000420	5.27	5944.93	778.00	0.26
Reach-1	26058	10%	2980.00	131.30	138.31		138.63	0.001328	5.74	1195.20	506.31	0.41
Reach-1	26058	2%	5840.00	131.30	141.19		141.36	0.000594	4.95	3010.05	716.41	0.29
Reach-1	26058	1%	7455.00	131.30	142.21		142.37	0.000543	5.08	3755.15	742.11	0.28
Reach-1	26058	0.2%	12505.00	131.30	145.04		145.20	0.000425	5.29	5923.49	778.00	0.26
Reach-1	25358	10%	2980.00	131.00	137.60		137.79	0.000999	5.37	1424.10	432.76	0.38
Reach-1	25358	2%	5840.00	131.00	140.82		140.96	0.000534	5.16	2872.39	468.02	0.29
Reach-1	25358	0.2%	12505.00	131.00	141.03		141.99	0.000552	0.01 6.30	5088 72	636 70	0.30
	20000	0.270	12000.00	101.00	144.00		144.07	0.000022	0.00	0000.12	000.70	0.01
Reach-1	25340	10%	2980.00	128.10	137.58		137.77	0.000473	4.58	1994.04	375.83	0.27
Reach-1	25340	2%	5840.00	128.10	140.68		140.94	0.000504	5.76	3250.24	506.40	0.29
Reach-1	25340	1%	7455.00	128.10	141.64		141.96	0.000587	6.55	3740.65	512.66	0.32
Reach-1	25340	0.2%	12505.00	128.10	144.36		144.83	0.000718	8.22	5237.84	696.11	0.37
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Reach-1	25334	10%	2980.00	130.31	137.63		137.75	0.000522	3.87	15/2.58	347.27	0.27
Reach-1	25334	270	7455.00	130.31	140.75		140.90	0.000405	4.43	2/ 15./0	411.00	0.25
Reach-1	25334	0.2%	12505.00	130.31	144.51		144.76	0.000444	4.30 6.04	4441.00	475 13	0.27
	20001	0.270	12000.00					0.000100	0.01			0.20
Reach-1	24975	10%	2980.00	129.20	135.57	135.57	137.16	0.005532	10.62	402.65	172.24	0.83
Reach-1	24975	2%	5840.00	129.20	139.83		140.59	0.001521	8.36	1283.40	362.15	0.48
Reach-1	24975	1%	7455.00	129.20	140.90		141.61	0.001359	8.49	1683.39	414.42	0.46
Reach-1	24975	0.2%	12505.00	129.20	144.14		144.54	0.000656	7.07	3094.75	445.51	0.34
	0.4000	4000	0000.00	407.00	105 50		400.00	0.000404	7 70		155.00	0.55
Reach-1	24922	10%	2980.00	127.89	135.50		136.32	0.002194	7.76	1421.07	274 77	0.55
Reach-1	24922	1%	7455.00	127.69	139.90		140.47	0.000917	7.14	1431.97	441 04	0.38
Reach-1	24922	0.2%	12505.00	127.89	144.18		144.49	0.000415	6.01	3438.02	506.44	0.27
Reach-1	24677	10%	2980.00	127.87	135.59		135.88	0.000688	4.52	855.68	167.98	0.31
Reach-1	24677	2%	5840.00	127.87	139.95		140.24	0.000405	4.83	1817.72	331.75	0.25
Reach-1	24677	1%	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24677	0.2%	12505.00	127.87	143.91		144.36	0.000485	6.46	3377.85	405.00	0.29
Reach-1	24620	10%	2080.00	128.00	13/ /1	133.07	135.60	0.005035	0.23	402.42	166 53	0.77
Reach-1	24620	2%	5840.00	120.90	139.56	155.57	140 17	0.003035	6.96	1443.21	273.89	0.17
Reach-1	24620	1%	7455.00	128.90	140.48		141.22	0.001143	7.78	1737.87	369.05	0.42
Reach-1	24620	0.2%	12505.00	128.90	143.60		144.30	0.000901	8.22	3001.58	410.00	0.39
Reach-1	24597	10%	2980.00	127.30	134.90		135.41	0.001279	5.88	709.79	201.22	0.40
Reach-1	24597	2%	5840.00	127.30	139.69		140.09	0.000572	5.66	1863.48	322.73	0.30
Reach-1	24597	1%	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-i	24397	0.2%	12505.00	127.30	143.74		144.22	0.000567	0.91	3499.24	421.00	0.31
Reach-1	24570	10%	2980.00	127.60	134.33	132.31	135.31	0.002228	7.94	375.39	104.89	0.56
Reach-1	24570	2%	5840.00	127.60	138.87	134.73	140.00	0.001290	8.69	958.27	316.33	0.47
Reach-1	24570	1%	7455.00	127.60	139.43	135.90	140.99	0.001698	10.31	1145.22	348.43	0.54
Reach-1	24570	0.2%	12505.00	127.60	142.91	140.91	144.13	0.001176	10.26	3114.93	807.05	0.47
Reach-1	24542.5		Bridge									
Reach-1	24540	10%	2980.00	127 60	134 18		135 21	0.002423	8 14	366.09	101 22	0.58
Reach-1	24540	2%	5840.00	127.60	137.37	134.72	139.01	0.002223	10.32	679.47	187.99	0.60
Reach-1	24540	1%	7455.00	127.60	138.19	135.88	140.32	0.002630	11.88	844.91	232.45	0.66
Reach-1	24540	0.2%	12505.00	127.60	142.97	140.68	144.09	0.001107	9.98	3240.15	809.73	0.46
Reach-1	24485	10%	2980.00	126.30	133.05		134.80	0.004960	10.97	339.74	65.99	0.79
Reach-1	24485	2%	5840.00	126.30	135.42	135.42	138.41	0.006522	14.55	576.27	136.90	0.94
Reach-1	24485	1%	7455.00	126.30	136.91	136.91	139.86	0.005771	14.75	837.67	207.98	0.90
Reduit-1	24403	0.276	12303.00	120.30	138.57	139.37	143.21	0.003430	17.09	147 3.02	230.14	0.92
Reach-1	24430	10%	2980.00	126.60	133.65		134.19	0.004131	5.91	504.51	89,39	0.44
Reach-1	24430	2%	5840.00	126.60	136.49		137.13	0.003507	6.76	1121.38	251.35	0.41
Reach-1	24430	1%	7455.00	126.60	137.85		138.46	0.002969	6.88	1464.10	254.64	0.39
Reach-1	24430	0.2%	12505.00	126.60	140.49		141.28	0.002984	8.11	2145.07	261.05	0.41
Reach-1	24401	10%	2980.00	124.66	133.66		134.04	0.003118	4.88	610.18	102.03	0.35
Reach-1	24401	2%	5840.00	124.66	136.40		137.02	0.003389	6.39	985.38	198.56	0.39
Reach-1	24401	0.2%	12505.00	124.66	137.67		138.37	0.003234	5.86 • ^7	20/0 12	257.49	0.39
	24701	0.2 /0	12000.00	124.00	140.01		171.10	0.003240	0.07	2048.10	332.03	0.41
Reach-1	24381	10%	2980.00	124.66	133.34		133.96	0.001781	7.05	527.73	91.46	0.49

HEC-RAS P	Plan: EXIST Ri	ver: RIVER-1	Reach: Reach-	1 (Continued)								
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	24381	2%	5840.00	124.66	135.78		136.91	0.002413	9.59	770.10	118.58	0.59
Reach-1	24381	1%	7455.00	124.66	136.85	407.40	138.24	0.002563	10.71	931.57	185.57	0.62
Reach-1	24381	0.2%	12505.00	124.00	139.22	137.40	141.03	0.002745	12.89	1531.13	330.29	0.00
Reach-1	24180	10%	2980.00	124 70	133.06		133 61	0.001495	5 98	502.38	92 91	0.44
Reach-1	24180	2%	5840.00	124.70	135.48		136.44	0.001803	7.95	844.89	259.49	0.51
Reach-1	24180	1%	7455.00	124.70	136.78	133.49	137.70	0.001560	8.02	1209.32	290.98	0.48
Reach-1	24180	0.2%	12505.00	124.70	139.53	136.93	140.38	0.001281	8.35	2316.16	451.50	0.45
Reach-1	24105	10%	2980.00	124.80	132.53		133.42	0.003018	7.59	392.78	80.10	0.60
Reach-1	24105	2%	5840.00	124.80	134.54	101.01	136.18	0.004147	10.27	570.55	100.04	0.73
Reach-1	24105	1%	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reduit-1	24103	0.2 /0	12303.00	124.00	137.04	137.23	140.07	0.003809	12.93	1090.93	201.02	0.70
Reach-1	23805	10%	2980.00	124.00	132.40		132.79	0.001004	5.69	1165.28	312.50	0.38
Reach-1	23805	2%	5840.00	124.00	134.69		135.27	0.001156	7.36	2038.14	469.70	0.42
Reach-1	23805	1%	7455.00	124.00	135.70		136.34	0.001191	7.99	2548.56	544.98	0.44
Reach-1	23805	0.2%	12505.00	124.00	138.21		138.97	0.001211	9.31	4063.59	641.58	0.46
Reach-1	23415	10%	2980.00	123.00	129.81	129.81	131.82	0.006096	11.90	404.45	161.55	0.89
Reach-1	23415	2%	5840.00	123.00	132.27	132.27	134.30	0.004596	13.19	1159.47	343.43	0.82
Reach-1	23415	0.2%	12505.00	123.00	133.11	133.11	135.33	0.004719	14.27	22/5 12	358.59	0.84
i teach-i	20410	0.270	12000.00	123.00	130.13	133.13	137.09	0.000009	10.90	2240.10	422.31	0.91
Reach-1	23171	10%	2980.00	120.30	128.75		129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2%	5840.00	120.30	129.79	129.12	131.57	0.005575	10.79	599.24	177.93	0.81
Reach-1	23171	1%	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23171	0.2%	12505.00	120.30	134.35		135.16	0.001732	7.84	1880.08	333.29	0.44
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	0.2%	12505.00	121.70	131.02		134.08	0.000479	3.90	2572 37	341.41	0.25
I teach-i	23030	0.270	12303.00	121.70	134.33		134.30	0.000237	5.52	2012.01	591.51	0.10
Reach-1	22916	10%	2980.00	121.00	128.01	126.93	128.88	0.002603	8.01	570.82	302.03	0.57
Reach-1	22916	2%	5840.00	121.00	130.41		130.84	0.000999	6.20	1483.60	430.42	0.38
Reach-1	22916	1%	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Reach-1	22765	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	10/	5840.00	114.20	130.48		130.70	0.000299	3.96	2020.14	395.39	0.19
Reach-1	22765	0.2%	12505.00	114.20	131.04		134.84	0.000301	4.19	4324.67	669.64	0.19
	22100	0.270	12000.00	114.20	104.04		104.04	0.000240	7.22	4024.01	000.04	0.17
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27		130.51	0.001575	4.56	1791.09	483.52	0.26
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
		400/		117.00	101.05	404.05	100.00	0.00070.4	10.01	004.00	100.05	0.05
Reach-1	22140	10%	2980.00	117.00	124.05	124.05	120.20	0.006734	12.84	391.30	132.05	0.95
Reach-1	22140	1%	7455.00	117.00	120.77	120.77	129.42	0.005382	14.90	1119.61	203.48	0.91
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
Reach-1	21825	10%	2980.00	115.90	121.80	121.75	123.65	0.007981	11.17	314.54	84.21	0.97
Reach-1	21825	2%	5840.00	115.90	124.12	124.12	126.73	0.006551	13.42	604.08	179.14	0.94
Reach-1	21825	1%	7455.00	115.90	125.26	125.26	128.03	0.005781	14.07	847.23	239.90	0.91
Reach-1	21825	0.2%	12505.00	115.90	131.24	127.79	132.45	0.001436	10.39	3430.35	1045.30	0.50
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.07	0.002174	7.62	300.83	103 38	0.55
Reach-1	21770	2%	5840.00	115.40	122.00	120.00	122.97	0.002174	11.02	527 79	119.38	0.55
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Reach-1	21757.5		Bridge									
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach 1	21745	0.2%	12505.00	115.40	124.48	123.47	127.36	0.005299	13.60	547.97	122.37	0.83
inteach-1	21/45	0.2 /0	12505.00	115.40	120.94	120.53	131.79	0.005288	10.11	101.12	141.07	0.94
Reach-1	21695	10%	2980.00	114 20	121 74	120 15	122 74	0.003025	8.01	371.94	69 60	0.61
Reach-1	21695	2%	5840.00	114.20	123.69	122.46	125.72	0.004430	11.42	511.32	74.77	0.76
Reach-1	21695	1%	7455.00	114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1	21695	0.2%	12505.00	114.20	127.45	127.45	130.78	0.004531	14.98	1124.07	292.57	0.82

HEC-RAS Plan: EXIST River: RIVER-1 Reach: Reach-1 (Continued)

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Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

# Norwalk River Proposed Conditions Model Output Table

HEC-RAS PI	lan: PROPOSE	D River: RIVE	ER-1 Reach: F	Reach-1								
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	29920	10%	2980.00	147.00	152.32	152.32	153.29	0.004454	9.23	671.47	438.66	0.75
Reach-1	29920	2%	5840.00	147.00	153.56	153.56	154.60	0.004481	10.83	1400.71	673.09	0.79
Reach-1	29920	1%	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86	1676.50	693.44	0.83
Reach-1	29920	0.2%	12505.00	147.00	154.99	154.99	156.40	0.005722	14.14	2414.85	738.35	0.92
Reach-1	29760	10%	2980.00	142.20	148.53		149.01	0.001498	5.62	583.07	179.68	0.44
Reach-1	29760	2%	5840.00	142.20	151.31		151.93	0.001165	6.63	1125.96	211.79	0.42
Reach-1	29760	1%	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	29760	0.2%	12505.00	142.20	154.28		155.51	0.001589	9.59	1814.00	255.42	0.51
Reach-1	28240	10%	2980.00	138.00	145.39		146.33	0.002035	7.92	453.14	156.69	0.54
Reach-1	28240	2%	5840.00	138.00	146.52	146.52	148.75	0.004139	12.55	696.60	258.98	0.79
Reach-1	28240	1%	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	28240	0.2%	12505.00	138.00	149.76	149.76	151.98	0.003397	14.32	1979.91	552.23	0.76
Reach-1	28020	10%	2980.00	136.33	146.00		146.01	0.000055	1.53	4419.69	705.50	0.09
Reach-1	28020	2%	5840.00	136.33	147.00		147.04	0.000130	2.53	5181.72	802.47	0.14
Reach-1	28020	1%	7455.00	136.33	147.55		147.59	0.000163	2.94	5632.11	838.83	0.16
Reach-1	28020	0.2%	12505.00	136.33	148.89		148.97	0.000246	3.92	6797.17	892.67	0.20
Reach-1	27930	10%	2980.00	135.65	146.00		146.01	0.000049	1.51	4606.87	734.08	0.09
Reach-1	27930	2%	5840.00	135.65	146.99		147.02	0.000116	2.50	5386.72	818.88	0.14
Reach-1	27930	1%	7455.00	135.65	147.54		147.58	0.000146	2.90	5847.71	863.80	0.16
Reach-1	27930	0.2%	12505.00	135.65	148.87		148.94	0.000221	3.85	7100.18	1055.04	0.20
Reach-1	27830	10%	2980.00	134.60	145.99		146.00	0.000041	1.44	4845.93	788.10	0.08
Reach-1	27830	2%	5840.00	134.60	146.99		147.01	0.000096	2.34	5676.92	876.39	0.13
Reach-1	27830	1%	7455.00	134.60	147.53		147.57	0.000120	2.70	6166.04	914.94	0.14
Reach-1	27830	0.2%	12505.00	134.60	148.86		148.92	0.000180	3.57	7478.45	1102.15	0.18
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Reach-1	27790	10%	2980.00	134.60	145.99		146.00	0.000039	1.40	4934.34	818.72	0.08
Reach-1	27790	2%	5840.00	134.60	146.98		147.01	0.000089	2.25	5799.61	916.21	0.12
Reach-1	27790	1%	7455.00	134.60	147.53		147.56	0.000109	2.58	6306.18	946.93	0.14
Reach-1	27790	0.2%	12505.00	134.60	148.85		148.92	0.000161	3.38	7600.04	999.96	0.17
Deerb 4	07400	100/	0000.00	100.40	445.00		115.00	0.000005	0.00	0140.04	700.45	0.00
Reach-1	27468	10%	2980.00	132.10	145.99		145.99	0.000005	0.60	9140.64	793.45	0.03
Reach-1	27468	2%	5840.00	132.10	146.99		146.99	0.000017	1.11	9943.03	813.12	0.05
Reach-1	27468	1%	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	2/408	0.2%	12505.00	132.10	148.85		148.88	0.000052	2.13	11529.28	890.79	0.10
Deerb 4	07440	100/	0000.00	400.00	445.07		115.00	0.000001	4 74	4705 50	000.40	0.40
Reach-1	27110	10%	2980.00	136.60	145.97		145.99	0.000064	1.74	4765.52	962.48	0.10
Reach-1	27110	270	7455.00	130.00	140.94		140.97	0.000146	2.03	6224.70	991.44 1005.58	0.10
Reach-1	27110	0.2%	12505.00	130.00	147.40		147.51	0.000167	3.29	7519.29	1005.56	0.10
Reach-1	27110	0.270	12303.00	130.00	140.74		140.02	0.000304	4.52	7510.50	1009.50	0.23
Roach 1	27025	10%	2080.00	125 50	145.62	141.94	145.00	0.000562	5.29	1750.25	990.05	0.20
Reach-1	27025	20%	2980.00	135.50	145.03	141.04	145.90	0.000302	0.06	1955.69	880.03	0.50
Reach-1	27025	1%	7455.00	135.50	145.74	145.59	140.08	0.001903	10.68	2304 78	800.67	0.50
Reach-1	27025	0.2%	12505.00	135.50	140.24	140.05	147.20	0.002112	12.81	3304.65	033.07	0.53
Reach-1	21025	0.270	12303.00	133.50	147.55	147.10	140.40	0.002034	12.01	3304.03	334.30	0.07
Reach-1	27020		Bridge									
INeach-1	21020		Diluge									
Reach-1	27015	10%	2980.00	135 50	141 85	141 85	144.38	0.006857	13.22	278 63	62.97	0.97
Reach-1	27015	2%	5840.00	135.50	145.62	145.62	146.66	0.002172	10.38	1752.24	879.80	0.59
Reach-1	27015	1%	7455.00	135.50	146.08	146.08	147 18	0.002399	11.26	2163.67	894 64	0.63
Reach-1	27015	0.2%	12505.00	135.50	147.11	147.11	148.43	0.003090	13.64	3099.86	927.52	0.72
Reach-1	26680	10%	2980.00	134.00	140 25	140.08	141 20	0.004316	10 17	742 52	359.88	0.76
Reach-1	26680	2%	5840.00	134.00	142 16	110.00	142.88	0.003007	10.34	1642.30	560.63	0.67
Reach-1	26680	1%	7455.00	134.00	142.10		143.57	0.002787	10.64	2063.23	590.00	0.65
Reach-1	26680	0.2%	12505.00	134.00	145.43		145.86	0.001574	9.53	3920.70	759.51	0.51
Reach-1	26209	10%	2980.00	133.40	140.59		140.63	0.000247	1.94	2566.09	865.64	0.17
Reach-1	26209	2%	5840.00	133.40	142.35		142.00	0.000238	2 43	4171.02	944 15	0.17
Reach-1	26209	1%	7455.00	133.40	143.04		143.12	0.000258	2.43	4826.43	949.13	0.10
Reach-1	26209	0.2%	12505.00	133.40	145.04		145.12	0.000232	3 00	7137 65	967.83	0.19
			.2000.00	100.40	1-10.40		140.04	0.000210	0.00	. 107.00	007.00	0.10
Reach-1	26136	10%	2980.00	130.20	130 70	136.80	140 40	0.001266	7 4 9	832 78	483.40	0.44
Reach-1	26136	2%	5840.00	130.20	141.38	140 68	140.40	0.001200	9 14	1847.30	666.49	0.44
Reach-1	26136	1%	7455.00	130.20	142 10	141 28	142.10	0.001511	9.50	2344 50	703.85	0.50
Reach-1	26136	0.2%	12505.00	130.20	144 97	142.59	145 41	0.000893	8.59	4476.35	760.00	0.01
	20.00	5.2.70	12000.00	100.20	1-14.07	142.00	140.41	0.000000	0.08	++10.00	100.00	0.40
Reach-1	26127.5		Bridge									
			Linago									
Reach-1	26119	10%	2980.00	131.30	137.79	136.96	139.43	0,004828	10.33	305.18	444.27	0.76
Reach-1	26119	2%	5840.00	131.30	141 23	138.61	141 40	0.000580	4 90	3038.66	718 58	0.29

HEC-RAS P	lan: PROPOSI	ED River: RIV	ER-1 Reach: F	Reach-1 (Contir	nued)							
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
	00110	40/	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	26119	1%	12505.00	131.30	142.25	138.86	142.41	0.000532	5.04	3781.94	742.73	0.28
Reduit-1	20119	0.2 /0	12303.00	131.30	143.07	140.05	140.20	0.000420	J.21	3944.93	778.00	0.20
Reach-1	26058	10%	2980.00	131.30	138.31		138.63	0.001328	5.74	1195.20	506.31	0.41
Reach-1	26058	2%	5840.00	131.30	141.19		141.36	0.000594	4.95	3010.05	716.41	0.29
Reach-1	26058	1%	7455.00	131.30	142.21		142.37	0.000543	5.08	3755.15	742.11	0.28
Reach-1	26058	0.2%	12505.00	131.30	145.04		145.20	0.000425	5.29	5923.49	778.00	0.26
Reach-1	25358	10%	2980.00	131.00	137.60		137.79	0.000999	5.37	1424.10	432.76	0.38
Reach-1	25358	2%	5840.00	131.00	140.82		140.96	0.000534	5.16	2872.39	468.02	0.29
Reach-1	25358	0.2%	12505.00	131.00	141.63		141.99	0.000552	5.01	5088.72	636 70	0.30
Reduit-1	2000	0.276	12303.00	131.00	144.00		144.07	0.000322	0.39	5066.72	030.70	0.31
Reach-1	25340	10%	2980.00	128.10	137.58		137.77	0.000473	4.58	1994.04	375.83	0.27
Reach-1	25340	2%	5840.00	128.10	140.68		140.94	0.000504	5.76	3250.24	506.40	0.29
Reach-1	25340	1%	7455.00	128.10	141.64		141.96	0.000587	6.55	3740.65	512.66	0.32
Reach-1	25340	0.2%	12505.00	128.10	144.36		144.83	0.000718	8.22	5237.84	696.11	0.37
Reach-1	25334	10%	2980.00	130.31	137.63		137.75	0.000522	3.87	1572.58	347.27	0.27
Reach-1	25334	2%	5840.00	130.31	140.75		140.90	0.000405	4.43	2715.70	411.08	0.25
Reach-1	25334	1%	7455.00	130.31	141.74		141.92	0.000444	4.96	3149.10	457.22	0.27
Reach-i	20004	0.2%	12505.00	130.31	144.51		144.70	0.000483	0.04	4441.00	475.15	0.29
Reach-1	24975	10%	2980.00	129 20	135.57	135.57	137 16	0.005532	10 62	402 65	172 24	0.83
Reach-1	24975	2%	5840.00	129.20	139.83	100.01	140.59	0.001521	8.36	1283.40	362.15	0.48
Reach-1	24975	1%	7455.00	129.20	140.90		141.61	0.001359	8.49	1683.39	414.42	0.46
Reach-1	24975	0.2%	12505.00	129.20	144.14		144.54	0.000656	7.07	3094.75	445.51	0.34
Reach-1	24922	10%	2980.00	127.89	135.50		136.32	0.002194	7.76	556.72	155.93	0.55
Reach-1	24922	2%	5840.00	127.89	139.90		140.47	0.000917	7.14	1431.97	374.77	0.38
Reach-1	24922	1%	7455.00	127.89	140.97		141.50	0.000829	7.23	1850.23	441.04	0.37
Reach-1	24922	0.2%	12505.00	127.89	144.18		144.49	0.000415	6.01	3438.02	506.44	0.27
Reach-1	24677	10%	2980.00	127.87	135 50		135.88	0.000688	4 52	855.68	167.08	0.31
Reach-1	24677	2%	5840.00	127.87	139.95		140.24	0.000405	4.83	1817.72	331.75	0.25
Reach-1	24677	1%	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24677	0.2%	12505.00	127.87	143.91		144.36	0.000485	6.46	3377.85	405.00	0.29
Reach-1	24620	10%	2980.00	128.90	134.41	133.97	135.69	0.005035	9.23	402.42	166.53	0.77
Reach-1	24620	2%	5840.00	128.90	139.56		140.17	0.001035	6.96	1443.21	273.89	0.40
Reach-1	24620	1%	7455.00	128.90	140.48		141.22	0.001143	7.78	1737.87	369.05	0.42
Reach-1	24620	0.2%	12505.00	128.90	143.60		144.30	0.000901	8.22	3001.58	410.00	0.39
Reach-1	24597	10%	2980.00	127 30	134.90		135.41	0.001279	5.88	709 79	201 22	0.40
Reach-1	24597	2%	5840.00	127.30	139.69		140.09	0.000572	5.66	1863.48	322.73	0.30
Reach-1	24597	1%	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-1	24597	0.2%	12505.00	127.30	143.74		144.22	0.000567	6.91	3499.24	421.00	0.31
Reach-1	24570	10%	2980.00	127.60	134.33	132.31	135.31	0.002228	7.94	375.39	104.89	0.56
Reach-1	24570	2%	5840.00	127.60	138.87	134.73	140.00	0.001290	8.69	958.27	316.33	0.47
Reach-1	24570	1%	7455.00	127.60	139.43	135.90	140.99	0.001698	10.31	1145.22	348.43	0.54
Reach-1	24570	0.2%	12505.00	127.60	142.91	140.91	144.13	0.001176	10.26	3114.93	807.05	0.47
Reach-1	24542 5		Bridge									
- todon i	2.10.12.0	-	Dilago									
Reach-1	24540	10%	2980.00	127.60	134.18		135.21	0.002423	8.14	366.09	101.22	0.58
Reach-1	24540	2%	5840.00	127.60	137.37	134.72	139.01	0.002223	10.32	679.47	187.99	0.60
Reach-1	24540	1%	7455.00	127.60	138.19	135.88	140.32	0.002630	11.88	844.91	232.45	0.66
Reach-1	24540	0.2%	12505.00	127.60	142.97	140.68	144.09	0.001107	9.98	3240.15	809.73	0.46
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Reach-1	24485	10%	2980.00	126.30	133.05	105.10	134.80	0.004960	10.97	339.74	65.99	0.79
Reach-1	24485	2%	5840.00	126.30	135.42	135.42	138.41	0.006522	14.55	5/6.2/	136.90	0.94
Reach-1	24485	0.2%	12505.00	120.30	139.57	139.57	143 21	0.005456	14.75	1473.62	250.14	0.90
T COUDIT-T	24400	0.270	12000.00	120.00	100.07	100.07	140.21	0.000400	17.00	1470.02	200.14	0.02
Reach-1	24430	10%	2980.00	126.60	133.65		134.19	0.004131	5.91	504.51	89.39	0.44
Reach-1	24430	2%	5840.00	126.60	136.49		137.13	0.003507	6.76	1121.38	251.35	0.41
Reach-1	24430	1%	7455.00	126.60	137.85		138.46	0.002969	6.88	1464.10	254.64	0.39
Reach-1	24430	0.2%	12505.00	126.60	140.49		141.28	0.002984	8.11	2145.07	261.05	0.41
Reach-1	24401	10%	2980.00	124.66	133.66		134.04	0.003118	4.88	610.18	102.03	0.35
Reach-1	24401	2%	5840.00	124.66	136.40		137.02	0.003389	6.39	985.38	198.56	0.39
Reach-1	24401	1%	/455.00	124.66	137.67		138.37	0.003234	6.86	12/8.84	257.49	0.39
Reault-1	24401	0.270	12000.00	124.00	140.31		141.18	0.003245	0.07	2049.10	აა∠.ძა	0.41
Reach-1	24381	10%	2980.00	124.66	133.34		133.96	0.001781	7.05	527.73	91.46	0.49
					. 50.04		. 20.00				50	0.70

HEC-RAS P	lan: PROPOSE	D River: RIVI	ER-1 Reach: F	Reach-1 (Contir	nued)							
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
Deech 1	04004	20/	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.50
Reach-1	24361	1%	7455.00	124.66	135.76		138.24	0.002413	9.59	931.57	185.57	0.59
Reach-1	24381	0.2%	12505.00	124.66	139.22	137.46	141.03	0.002745	12.89	1531.13	330.29	0.66
Reach-1	24180	10%	2980.00	124.70	133.06		133.61	0.001495	5.98	502.38	92.91	0.44
Reach-1	24180	2%	5840.00	124.70	135.48	122.40	136.44	0.001803	7.95	1200.22	259.49	0.51
Reach-1	24180	1%	12505.00	124.70	130.78	133.49	137.70	0.001560	8.02	2316.16	290.98	0.48
Tteach-1	24100	0.270	12303.00	124.70	155.55	130.33	140.50	0.001201	0.55	2010.10	401.00	0.43
Reach-1	24105	10%	2980.00	124.80	132.53		133.42	0.003018	7.59	392.78	80.10	0.60
Reach-1	24105	2%	5840.00	124.80	134.54		136.18	0.004147	10.27	570.55	100.04	0.73
Reach-1	24105	1%	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reach-1	24105	0.2%	12505.00	124.80	137.64	137.25	140.07	0.003869	12.93	1098.93	201.62	0.76
Reach-1	23805	10%	2980.00	124.00	132.40		132,79	0.001004	5.69	1165.28	312.50	0.38
Reach-1	23805	2%	5840.00	124.00	134.69		135.27	0.001156	7.36	2038.14	469.70	0.42
Reach-1	23805	1%	7455.00	124.00	135.70		136.34	0.001191	7.99	2548.56	544.98	0.44
Reach-1	23805	0.2%	12505.00	124.00	138.21		138.97	0.001211	9.31	4063.59	641.58	0.46
				(								
Reach-1	23415	10%	2980.00	123.00	129.81	129.81	131.82	0.006096	11.90	404.45	161.55	0.89
Reach-1	23415	1%	7455.00	123.00	132.27	132.27	134.30	0.004596	13.19	1451.84	358 59	0.84
Reach-1	23415	0.2%	12505.00	123.00	135.13	135.13	137.89	0.005069	16.96	2245.13	422.31	0.91
Reach-1	23171	10%	2980.00	120.30	128.75		129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2%	5840.00	120.30	129.79	129.12	131.57	0.005575	10.79	599.24	177.93	0.81
Reach-1	23171	1%	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23171	0.2 /0	12303.00	120.30	104.00		133.10	0.001732	7.04	1000.00	333.29	0.44
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	1%	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	23036	0.2%	12505.00	121.70	134.55		134.98	0.000237	3.32	2572.37	391.51	0.18
Peach 1	22016	10%	2080.00	121.00	129.01	126.02	120.00	0.002602	9.01	570.92	202.02	0.57
Reach-1	22910	2%	5840.00	121.00	130.41	120.93	120.00	0.002003	6.20	1483.60	430 42	0.37
Reach-1	22916	1%	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Reach-1	22765	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	2%	5840.00	114.20	130.48		130.70	0.000299	3.96	2020.14	395.39	0.19
Reach-1	22765	1%	12505.00	114.20	131.04		131.87	0.000301	4.19	2548.37	511.91	0.19
Tteach-1	22105	0.270	12303.00	114.20	134.04		134.04	0.000240	4.22	4324.07	003.04	0.17
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27		130.51	0.001575	4.56	1791.09	483.52	0.26
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
Reach-1	22140	10%	2980.00	117.00	124 05	124.05	126 26	0.006734	12 84	391.36	132 65	0.95
Reach-1	22140	2%	5840.00	117.00	124.00	124.00	120.20	0.005440	14.96	889.23	205.48	0.91
Reach-1	22140	1%	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
Reach-1	21825	10%	2980.00	115.90	121.80	121.75	123.65	0.007981	11.17	314.54	84.21	0.97
Reach-1	21825	1%	7455.00	115.90	124.12	124.12	120.73	0.006551	13.42	847.23	239.90	0.94
Reach-1	21825	0.2%	12505.00	115.90	131.24	127.79	132.45	0.001436	10.39	3430.35	1045.30	0.50
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.97	0.002174	7.62	390.83	103.38	0.55
Reach-1	21770	2%	5840.00	115.40	124.17	122.36	126.07	0.003067	11.07	527.79	119.93	0.68
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Reach-1	21757.5		Bridge									
			Dilago									
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach-1	21745	1%	7455.00	115.40	124.48	123.47	127.36	0.004410	13.60	547.97	122.37	0.83
Reach-1	21745	0.2%	12505.00	115.40	126.94	126.53	131.79	0.005288	17.67	707.72	141.67	0.94
Reach 1	21605	10%	2000.00	114.00	101 74	100.15	100 74	0.002025	0.04	271.04	60.60	0.61
Reach-1	21695	2%	2960.00	114.20	121.74	120.15	122.74	0.003025	8.01 11.42	511.94	09.00 74 77	0.01
Reach-1	21695	1%	7455.00	114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1	21695	0.2%	12505.00	114.20	127.45	127.45	130.78	0.004531	14.98	1124.07	292.57	0.82

### HEC-RAS Plan: PROPOSED River: RIVER-1 Reach: Reach-1 (Continued)

					,							
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

# **Tighe&Bond**

**APPENDIX I** 



Project Name: 141 Danbury Road Project Number: F0173-02 Project Location: Wilton, CT Description: Riprap Apron Calculation Prepared By: TAS Date: May 24, 2021

## **Riprap Apron**

Invert Elevation =	138.50	ft
Tailwater Elevation =	140.44	ft
Tailwater Depth (TW) =	1.94	ft
Inside Pipe Diameter $(S_p) =$	2.00	ft
Pipe Discharge (Q) =	10.21	cfs
Outlet Velocity $(V) =$	4.41	ft/s

### **Apron Type**

Type A Riprap Apron (Minimum Tailwater Condition) TW <  $0.5R_p$ Type B Riprap Apron (Maximum Tailwater Condition) TW  $\ge 0.5R_p$ TW =  $1.94 > 0.5R_p$ 



### **Apron Length**

Type B Riprap Apron (Maximum Tailwater Condition) TW  $\geq$  0.5R $_p$   $L_a = ~(3.0(Q\text{-}5)/\text{Sp}^{1.5}) + 10.0$ 

|--|

### **Apron Width**

Type B Riprap Apron (Maximum Tailwater Condition) TW ≥ 0.5R<sub>p</sub>

 $W_1 = 3*S_p$  $W_2 = 3*S_p+0.4L_a$ 

 $W_1 = 6.00 \text{ ft}$  $W_2 = 12.21 \text{ ft}$ 

### **Riprap Specification**

Outlet Velocity (V)=	0-8 ft/s	Modified	
Outlet Velocity (V)=	8-10 ft/s	Intermediate	
Outlet Velocity (V)=	10-14 ft/s	Standard	
Outlet Velocity (V)=	4.410 ft/s	Use Modified Riprap	

Outlet protection has been designed in accordance with the Section 11.13 of the ConnDOT Drainage Manual



Project Name: **141 Danbury Road** Project Number: **F0173-02** Project Location: **Wilton, CT** Description: **Temporary Sediment Trap Sizing Calculation** Prepared By: **TAS** Date: **May 20, 2021** 

# **Temporary Sediment Trap 01**

# Sediment Storage Volume

Drainage Area	=	2.4	acres
Initial Storage Volume	=	134	cy/ac
Required Storage	=	322	су
	=	8,683	cf
Min Wet Storage (1/2 Required Storage)	=	4,342	cf

## Wet Storage Volume

## $V_w = 0.85 * A_w * D_w$

V <sub>w</sub> , Wet Storage Volume	=	7064	cf
D <sub>w</sub> , Maximum Depth (Low Point in Trap to Base of Outlet)	=	3	ft
A <sub>w</sub> , Surface Area of the Flooded Area at	_	2770	of
the Base of the Outlet	=	2770	SI

# **Dry Storage Volume**

$$V_d = [(A_w + A_d) / 2] * D_d$$

V <sub>d</sub> , Dry Storage Volume	=	3004	cf
$D_d,$ Depth (Base to the top of the Outlet)	=	1	ft
the Top of the Outlet	=	3237	SI
$A_d$ , Surface Area of the Flooded Area at	_	7777	cf
the Base of the Outlet	-	2770	51
$A_w$ , Surface Area of the Flooded Area at	_	7770	cf

### **Provided Storage Volume**

Total Provided Storage	=	10067 373	cf cy
	=	111	су
Dry Storage	=	3004	cf
	=	262	су
Wet Storage	=	7064	cf

Calculated in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control Section 5-11

# **Tighe&Bond**

**APPENDIX J** 



### 141 Danbury Road

### **Total Bedrooms**

			Bedrooms
1 Bedroom Units =	44	x 1	44
2 Bedroom Units =	114	x 2	228
3 Bedroom Units =	15	х З	45

Total Residential Units = 173

317 Total Bedrooms

### Average Daily & Peak Flow

317	Units		
150	GPD per Bedr	oom	
	Average Flow =	317	x 150
	Average Flow =	47,550	GPD
	-		_
Pe	eak Flow Factor =	4	
	Peak Flow = $\_$	190,200	_GPD
	=_	132	

### Sanitary Sewer Lateral Capactity

6" PVC Gravity Lateral

Canacity	1.49 x R <sup>2/3</sup> x S <sup>1/2</sup> x A		
	n		
	R =	0.125	
	S = 2% =	0.020	
	A =	0.196	
	n =	0.010	

Capacity = <u>668,400</u> GPD



а**н** 

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May 19, 2021

Mr. Michael Wrinn Town Planner Planning and Zoning Department Town of Wilton Town Annex 238 Danbury Road Wilton, CT 06897

# RE: 141 Danbury Road, Wilton, CT (the "Property") Letter of Authority

Dear Mr. Wrinn:

FDSPIN 141 DR LLC is the contract purchaser of the property located at 141 Danbury Road, Wilton, CT (the "Property"), I hereby authorize the attorneys of Carmody Torrance Sandak & Hennessey, LLP, with offices located at 707 Summer Street, Stamford, Connecticut 06901, to act as agent for FDSPIN 141 DR LLC in connection with the enclosed land use applications. Thank you for your acknowledgement of said authority.

Sincerely,

FDSPIN 141 DR LLC

By: hull 5, Fuller

Samuel B. Fuller Duly Authorized

# Project Narrative

# I. Background

FDSPIN 141 DR LLC (the "**Applicant**") is the contract purchaser of the property located at 141 Danbury Road, Wilton, Connecticut (the "**Property**"). The Property consists of approximately 4.28+/- acres on the westerly side of Danbury Road and is designated as Tax Lot 2 on Map 70 in a DE-5 Design Enterprise District. The Property is adjacent to the Norwalk River. The Applicant seeks to redevelop the Property with a multifamily residential building and associated landscape and site improvements. Because these site enhancements will partially take place in the regulated area, the Applicant is seeking approval of an Application for a Significant Regulated Activity from the Inland Wetlands Commission (the "**Commission**").

The Property is currently improved with a warehouse style office building and a large surface parking lot extending up to the river's edge. These impervious improvements currently cover 63% of the Property, and stormwater currently sheet flows over the site directly into the river without any water quality treatment. The width of the riparian buffer adjacent to the river varies from 0' to 35'+/- across the westerly portion of the Property. The Property, and existing improvements located thereon, are depicted in the aerial photograph below.<sup>1</sup>



II. Proposal

<sup>&</sup>lt;sup>1</sup> Aerial photograph of the Property obtained from the Wilton GIS website.

The enclosed application is in furtherance of the redevelopment of the Property that, if approved, will allow the Applicant to replace the existing structure and parking with a new multi-family residential building accompanied by dense landscaping throughout the Property, including the westerly portion of the site along the Norwalk River.



As seen in the above rendered Landscape Plan, the Applicant proposes transforming 85% of the area within the Regulated Area (approximately 25,020+/- sf) from a paved parking area to a private landscaped, recreational area. This passive, recreational space will consist of native trees, shrubs and perennials. Because much of the site is in the Flood Zone, the building will be raised with parking beneath it. Aside from building columns (approximately 315+/- sf), the building itself is located entirely outside of the Regulated Area and site improvements are no closer than 66' to the Norwalk River. Although not visible in the image above, porous pavers will be utilized on all parking surfaces within 200' of the Norwalk River, further facilitating the reduction of runoff by infiltrating rainwater and melting snow. Material excavated onsite will be utilized as fill, and additional pavement subbase will be incorporated on an as-needed basis.

Work within the Regulated Area is intended to restore and enhance the natural characteristics of the Property and significantly improve water quality on the site, and to provide outdoor, passive recreation space for the residents. While no adverse impacts are anticipated, Best Management Practices (BMPs) as described in the enclosed Engineering Report and plans are incorporated to avoid and minimize potential adverse environmental impacts.

# III. Compliance with Standards & Criteria For Decision

The proposal is compliant with the standards of Section 10.3 of the Inland Wetlands and Watercourses Regulations for the Town of Wilton (the "Regulations") as follows:

In carrying out the purposes and policies of sections 22a-36 to 22a-45, inclusive, of the Connecticut General Statutes, including matters relating to regulating, licensing and enforcing of the provisions thereof, the Commission shall consider all relevant facts and circumstances in making its decision on any application for a permit, including but not limited to the following:

> a) Impacts of the proposed regulated activity on wetlands or watercourses outside the area for which the activity is proposed and future activities associated with, or reasonably related to, the proposed regulated activity which are made inevitable by the proposed regulated activity and which may have an impact on wetlands or watercourses.

All of the work proposed within the Regulated Area is intended to restore and expand the function of the Norwalk River's riparian buffer, improve water quality and provide wildlife habitat, while simultaneously providing recreation space for residents. As such, no impacts on wetlands or watercourses outside the area for which the activity is proposed are anticipated. Similarly, future activities associated with, or reasonably related to the proposed regulated activity will be primarily comprised of Wilton residents enjoying the landscaped areas proposed by the Applicant. No direct disturbance is proposed. Therefore, no adverse impact on wetlands or watercourses are anticipated. In fact, improvements to the river buffer, and proposed stormwater treatment measures described in the enclosed Engineering Report, will dramatically improve water quality on the Property.

b) The applicant's purpose for, and any feasible and prudent alternatives to, the proposed regulated activity which alternatives would cause less or no environmental impact to wetlands and watercourses. This consideration should include, but is not limited to, the alternative of requiring actions of a different nature which would provide similar benefits with different environmental impacts, such as using a different location for the activity.

Pursuant to the Connecticut General Statutes, a "feasible" and "prudent" alternative includes one able to be "constructed or implemented consistent with sound engineering principles" which is "economically and otherwise reasonable in light of the social benefits to be derived from the proposed regulated activity provided cost may be considered in deciding what is prudent and further provided a mere showing of expense will not necessarily mean an alternative is imprudent."<sup>2</sup>

After considering several different development proposals, the Applicant is confident that the current proposal is the most feasible and prudent alternative for the Property. As shown on the submitted alternatives, other development scenarios would have produced a shorter

<sup>&</sup>lt;sup>2</sup> Conn. Gen. Stat. Sec. 22a-38(17) – Conn. Gen. Stat. Sec. 22a-38(18).

building; however, in order to ensure the project remained economically viable, those proposals also would have located the building and associated parking areas closer to the Norwalk River. These scenarios would encroach further into the Regulated Area than the proposed activity and would prohibit the significant investment in site landscaping currently proposed. Specifically, the March 2020 proposal would result in a building approximately 38' away from the edge of the Norwalk River, and a parking area located approximately 24' away from the edge of the Norwalk River. Similarly, the January 2021 proposal would result in a building approximately 40' away from the river's edge, and a surface parking area approximately 7'6" away from the river's edge. The current proposal, which locates the building no closer than 88' to the Norwalk River is far superior in terms of environmental impact.

In addition to setting the building back, the current proposal also incorporates:

- Catch Basins and yard drains fitted with 24" sumps to collect sediment and prevent discharge of oil and other pollutants into the storm drainage system;
- Hydrodynamic Separators to prevent the transport of oils and sediment further downstream, including Contech CDS units sized in accordance with the 2004 CTDEEP Stormwater Quality Manual; and
- Concrete chambers surrounded by stone and filter fabric designed to attenuate peak flows, serve as a primary treatment practice and promote groundwater discharge.

At the same time, the proposal will result in several important social benefits for the Town of Wilton (the "Town"). As noted in the 2019 Plan of Conservation and Development (the "**POCD**"), the "relatively high price of housing coupled with an available housing stock of detached single-family homes has more recently contributed to lower in-migration of younger working-age people and has increased the out-migration of empty-nesters and retirees."<sup>3</sup> Trends of increasing housing costs and decreasing housing supply have only been exacerbated by the COVID-19 Pandemic. At the same time, "the community has increasingly expressed interest in increasing housing type variety and price points in design and location appropriate ways" to increase the Town's overall housing stock and to attract and meet "the needs of occupants at different life and employment stages."<sup>4</sup> Moreover, the proposal would include an affordability component with 10% of the units available at prices affordable to families earning less than 80% of Area Median Income. With limited sites that are appropriate for multifamily residential development, the redevelopment of the Property for this purpose is necessary to achieve the Town's housing and economic development goals. For these reasons, the proposal is responsive to these trends and the vision identified in the POCD.

<sup>&</sup>lt;sup>3</sup> POCD, pg. 8.

<sup>&</sup>lt;sup>4</sup> Id.
In addition to increasing housing type, the proposal will result in the conversion of a paved parking area to a private park available for outdoor, recreational use. The replacement of impervious surface with a landscaped area planted with native species will enhance the environmental characteristics of the Property.

c) The relationship between the short-term and long-term impacts of the proposed regulated activity on wetlands or watercourses and the maintenance and enhancement of long-term productivity of such wetlands or watercourses.

No impacts on the wetlands or watercourses are anticipated. However, to mitigate any potential short-term impacts associated with site disturbance and construction, sediment and erosion controls will be implemented such as: silt fencing to trap sediments within stormwater runoff; anti-tracking pads to remove sediments from vehicles entering the Property; and watering of the Property as needed to prevent dust.

BMPs proposed to avoid long-term impacts include: catch basins fitted with sumps to trap sediments from roadway stormwater runoff; swirl concentrators designed to maintain water quality by trapping sediments, litter, oils and grease; and underground infiltration galleries to store and treat runoff.

d) Irreversible and irretrievable loss of wetland or watercourse resources which would be caused by the proposed regulated activity, including consideration of the extent to which the proposed regulated activity would foreclose a future ability to protect, enhance or restore such resources. This requires recognition that the inland wetlands and watercourses of the State of Connecticut are an indispensable, irreplaceable and fragile natural resource, and that these areas may be irreversibly destroyed by deposition, filling, and removal of material, by the diversion, obstruction or change of water flow including low flows, and by the erection of structures and other uses.

No deposition, filling, removal of material, diversion, obstruction or change of water flow is proposed in connection with the proposed redevelopment. The proposal will not result in the irreversible or irretrievable loss of wetland or watercourse resources. Rather, the proposal will better protect, enhance and restore these resources as compared to the existing impervious parking lot located within the Regulated Area. For example, the proposal will increase the width of the riparian buffer along the Norwalk River from 0' - 35'+/- to 60' - 100'+/-. This buffer will include 49 shade and understory trees, over 375 shrubs and over 500 perennials known to benefit pollinators.

e) The character and degree of injury to, or interference with, safety, health, or the reasonable use of property, including abutting or downstream

property, which would be caused or threatened by the proposed regulated activity, or the creation of conditions which may do so. This includes recognition of potential damage from erosion, turbidity, or siltation, loss of fish and wildlife and their habitat, loss of unique habitat having demonstrable natural, scientific or educational value, loss or diminution of beneficial aquatic organisms and wetland plants, the dangers of flooding and pollution, and the destruction of the economic, aesthetic, recreational and other public and private uses and values of wetlands and watercourses to the community.

The proposal will not injure or interfere with the safety, health or reasonable use of the Property or abutting/downstream properties. In fact, building multifamily housing on the Property will facilitate the preservation of open space in other areas of Town that are better suited for passive, green space than multifamily residential use. BMPs employed during and after construction will protect the wetlands and watercourses on and adjacent to the Property. Currently, the Property provides little to no wildlife habitat due to existing improvements adjoining the Norwalk River and lacks water quality improvements. Modern stormwater systems and the planting of native species will protect against erosion, turbidity, and adverse impacts to wildlife and their habitat. Furthermore, replacing a parking lot with significant landscaping will increase the aesthetic and recreational value of the Property.

f) The environmental impact of the proposed regulated activity on the inland wetland or watercourse including the effects on the inland wetland's and watercourse's capacity to support desirable biological life, to prevent flooding, to supply and protect surface and ground waters, to control sediment, to facilitate drainage, to control pollution, to support recreational activities, and to promote public health and safety. Measures which would mitigate the impact of any aspect of the proposed regulated activity. Mitigation measures which may be considered as a condition of issuing a permit for such activity include but are not limited to, measures to (a) prevent or minimize pollution or other environmental damage, (b) maintain or enhance existing environmental quality, or (c) in the following order of priority: 1. restore, 2. enhance, and 3. create productive wetland or watercourse resources. Appropriate mitigation measures are those which could be feasibly carried out by the applicant and would protect the wetland's or watercourse's natural capacity to support fish and wildlife, to prevent flooding, to supply and protect surface and ground waters, including public water supplies to control sedimentation, to prevent erosion, to assimilate wastes, to facilitate drainage, to control pollution, to support recreational activities and open space, and to promote public health and safety.

Replacement of a surface parking lot with enhanced landscaping and updated water quality improvements will enhance the wetland and watercourse's ability to support desirable biological life, prevent flooding, supply and protect surface water and ground waters, control sediment, facilitate drainage, support recreational activities and promote public health and safety. These features will restore and enhance the productive wetland and watercourse resources on and near the Property.

## IV. Feasible & Prudent Alternative Analysis

As stated in the Applicant's response to Section 10.3(b) above, the current proposal is the feasible and prudent alternative for the site. Other proposals would have located a building and/or parking areas closer to the Norwalk River with greater impact on the Regulated Area. This proposal appropriately sets the building and impervious improvements back from the Regulated Area, provides a robust landscaped recreational area and restores and enhances the natural environment. At the same time, the proposal will facilitate the Town's ability to respond to trends impacting housing cost and supply.



\*NOTE: REFER TO CIVIL FOR SITE PLAN AND CIVIL INFORMATION. LANDSCAPE SHOWN FOR ILLUSTRATIVE PURPOSES ONLY. REFER TO LANDSCAPE FOR TREES AND LANDSCAPE INFORMATION.



## ILLUSTRATIVE SITE PLAN - 141 DANBURY ROAD

## SITE ANALYSIS

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BUILDING **3 STORIES OVER PODIUM** (APPROXIMATELY 45' HIGH)

65,888 X 3

= 197,664 GSF TOTAL

UNITS: 188

PARKING PROVISION: +/- 432 PARKING SPACES \*

200 ON PODIUM 232 ON SURFACE

\*LOSS FOR EGRESS AND UTILITY AREAS NEEDS TO BE ANALYZED.

**141 DANBURY ROAD** 

JAN 21, 2021 FUL.003

A.01

WILTON, CT FULLER DEVELOPMENT

SCALE: 1"=50' (@ 22"x34")





	COMMON NAME	SIZE	ROOT	REMARKS
	RED MAPLE	3-3.5" CAL	B&B	
	RIVER BIRCH	8-9' HT.	B&B	3 STEMS
S'SHADEMASTER'	SHADEMASTER LOCUST	3-3.5" CAL.	B&B	FULL
	BLACK GUM	2-2.5" CAL.	B&B	
S	AMERICAN SYCAMORE	335" CAL,	B&B	FULL
	SWAMP WHITE OAK	2-2.5" CAL.	B&B	FULL
	PIN OAK	2-2.5" CAL.	B&B	FULL
OND'	REDMOND LINDEN	3-3.5" CAL.	B&B	FULL
SISI	SHADBLOW	7-8' HT.	B&B	
I BRULLANCE'	AUTUMN BRILLANCE SHAD	8-10' HT.	B&B	TRISTEM
	PAGODA DOGWOOD	6-8' HT	B7b	
	FLOWERING DOGWOOD	2-2.5' HT.	B&B	WHITE
1G'	WINTER KING HAWTHORN	2-2.5" CAL.	B&B	FULL
	ADIRONDACK CRAB APPLE	2-2.5" CAL.	B&B	
M	SOURWOOD	2-2.5" CAL.	B&B	
	AMERICAN HOLLY	7-8' HT.	B&B	25% MALES
	WHTIE SPRUCE	8-10' HT.	B&B	
	WHITE PINE	10-12' HT.	B&B	FULL
GRA'	DARK ARBORVITEA	7-8' HT.	B&B	
	GREEN GIANT	8-10'	B&B	
	•			