

McChord Engineering Associates, Inc.

Civil Engineers and Land Planners

1 Grumman Hill Rd, Wilton, CT 06897 Tel: (203) 834-0569 Fax: (203) 834-2789

June 16, 2020

Michael Conklin Director of Environmental Affairs Town Hall Annex 238 Danbury Road Wilton, CT 06897

Re: E

Engineering Summary Proposed Culvert Repair 68 McFadden Drive, Wilton, CT Map 85, Lot 13

Dear Mr. Conklin:

McChord Engineering Associates, Inc. has been commissioned to prepare a design for the repair of the culvert crossing at 68 McFadden Drive. The culvert is located within a right-of-way on 68 McFadden drive. It provides a stream crossing for a shared driveway that serves four houses at 58, 62, 64 and 66 McFadden Drive. This office has inspected the existing culvert, reviewed the contributing watershed, prepared a hydraulic analysis of the culvert pipes and created a repair plan. The following is an engineering summary of the existing conditions, proposed repair and potential impacts.

The existing culvert crossing consists of two asphalt lined corrugated pipe arches. The north pipe arch is approximately 65" wide x 40" tall and the south pipe arch is approximately 54" wide x 40" tall. Stone headwalls and wing walls support the banks on the upstream and downstream sides. The asphalt driveway is approximately 14' wide with the edges of the driveway at the headwalls. It is assumed that the culvert was constructed in the mid-1960's when this neighborhood was developed. Just downstream of the driveway culvert is another inlet from a 24" RCP that passes under McFadden Drive. The stream itself is approximately 12' wide, with a stony bottom and steep vegetated banks. The existing conditions are shown on the "Improvement Location Map, 68 McFadden Drive" prepared for JoAnne F. Pica by Stalker Land Surveying, Inc, dated July 18, 2019.

Our inspection of the driveway culvert revealed that the south pipe arch is severely degraded. The entire flow line of the culvert has rusted out the culvert has begun to settle. The settling has opened up a large pothole in the driveway and a number of cracks have formed in the stone headwalls. The north pipe arch was generally intact, but moderate deflection was

Michael Conklin June 16, 2020 Page 2/3

noted and the asphalt lining was very worn. Some scouring was observed on the downstream outlet but otherwise no significant erosion was noted. The attached pictures highlight the conditions of the existing culvert.

The south pipe arch is too degraded to attempt to reline. The existing conditions are also not conducive to sleeve a new pipe through the old pipes. Therefore the best option is to replace the pipe arch completely. Due to the amount of effort involved to replace the pipes, both pipes should be replaced at the same time. Two 48" diameter HDPE pipes are proposed to replace the two pipe arches. The HDPE is more readily available and easier to work with than other pipe materials, and the 48" circular pipe will have a very similar hydraulic capacity to the pipe arches being replaced. The stone headwalls will be dismantled and rebuilt.

The watershed upstream of the culvert crossing totals approximately 211 acres. It consists primarily of single family residences in the 1-acre and 2-acre zone. It also encompasses a portion of the Miller-Driscoll school campus. The watershed map is attached. Approximately 400' upstream is a culvert crossing under McFadden Drive that consists of two 42" diameter reinforced concrete pipes. Approximately 150' downstream is another driveway culvert that appears to be of the same size and configuration as the subject culvert. The stream discharges to a pond approximately 400' downstream of the culvert crossing and the pond outlets to the Norwalk River. The culvert is also within FEMA Flood Zone A, which has no base flood elevation determined.

Culvert Studio v 2.0.0.19 software was used to model the culvert under existing and proposed conditions during a 25-year and a 100-year storm event. This software uses FHWA – HDS-5 methodology to compute the hydraulic grade line for the culvert. That rational method was used to determine peak flows to the culvert crossing. The 25-year peak flow is 217.7 cfs and the 100-year peak flow is 269.6 cfs. The analysis found that the proposed headwater and tailwater conditions will be very similar to the existing conditions. Detailed calculations are attached.

The "Culvert Repair Plan" prepared for Christopher J. Silver by this office details the proposed work. The new 48" HDPE pipes and rebuilt headwalls will be in the same location as what is being removed. The existing wing walls will be reused where possible to reduce the amount of disturbance. Rip-rap inlet and outlet protection will be added to the stream bed. The driveway elevation will be raised slightly at the culvert crossing and then blended back into the existing driveway grades. The goal of the plan is to minimize site disturbance and allow the culvert to be quickly replaced.

The "Culvert Repair Plan" shows silt fence to protect the stream and banks. It also includes a construction sequence outlining the critical steps of the repair. Work will be staged from the existing driveway which will protect the existing vegetation. It is anticipated that the material excavated can be reused for the bedding of the new culverts. Approximately 10 cubic yards of intermediated rip-rap is proposed for the inlet and outlet protection. Approximately 13

Michael Conklin June 16, 2020 Page 3/3

cubic yards of processed aggregate will be required to regrade the driveway. If there is any excess material, it will be removed from the site.

Construction of the project will be timed to work within good weather conditions. Temporary dewatering measures will be required to install the culverts and headwalls. Dewatering will be accomplished by installing a pump intake at the upstream end of the project and pumping to a filter sock at the downstream end. The filter sock will ensure clean water discharge. It is anticipated that the bulk of the repair can be completed within one week and will allow residents to regain vehicle access to their houses. The completed project, including paving and stabilization, is anticipated to take two weeks.

The proposed culvert repair is necessary and needs to happen quickly in order to maintain safe access to the four houses. The proposed culvert crossing will be very similar to the existing culvert crossing. There will be no negative impact to the existing flood zone or flood elevations. Proper implementation of the proposed construction sequence and erosion control measures will minimize potential impacts to the stream and downstream property owners during construction.

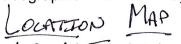
Sincerely,

Thomas Nelson, P.E. Project Manager

Attachements.

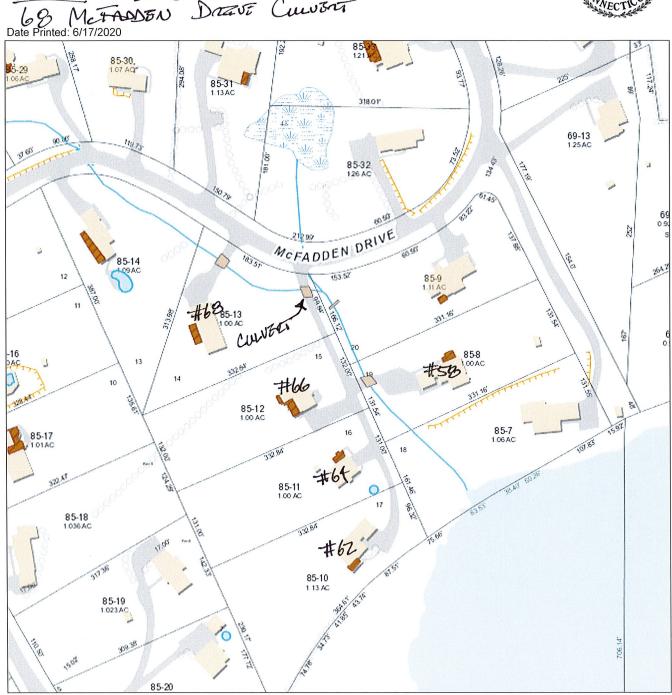
Town of Wilton

Geographic Information System (GIS)









MAP DISCLAIMER - NOTICE OF LIABILITY

This map is for assessment purposes only. It is not for legal description or conveyances. All information is subject to verification by any user. The Town of Wilton and its mapping contractors assume no legal responsibility for the information contained herein.

Zoning Effective: July 28, 2017 Planimetrics Updated: 2014

Approximate Scale: 1 inch = 150 feet





CHIVENT CROSSING FOR SHARES DRAVEWAY





68 McFADEN DRIVE

DOWNSTREAM HEADWALL



UPSTREAM HEADWALL - SOUTH CULVERT



Town of Wilton

Geographic Information System (GIS)

WATERSHED MAP



Cuevon



OLD FARM

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Zoning Effective: July 28, 2017 Planimetrics Updated: 2014

Approximate Scale: 1 inch = 800 feet





Culvert Studio v 2.0.0.19 06-17-2020

Existing - 68 McFadden

Culvert 1

CULVERT EMBANKMENT

Shape = Arch Pipe Top Width = 16.00 ft

Inlet Edge = Square Edge/ Hdwall Top Elevation = 99.40 ft

Material = Corrugated Steel Crest Length = 16.00 ft

Manning's n = 0.024

Rise

Span = 59 in Method = Rational Method

DISCHARGE

Invert Elev. Down = 93.30 ft Drainage Area = 211.00 ac

Length = 18.00 ft Runoff Coefficient = 0.33

Slope = 0.028 ft/ft Time of Concentration = 32.6 min

Slope = 0.028 ft/ft Time of Concentration
Invert Elev. Up = 93.80 ft

No. Barrels = 2 TAILWATER

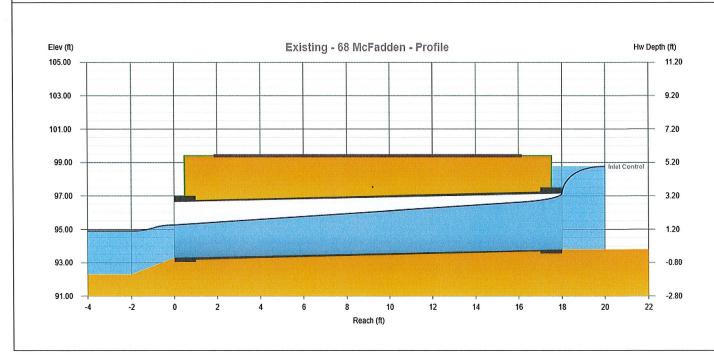
Plan Skew Angle = 20 degrees Tailwater Condition = Channel 1

CALCULATION SAMPLE, 25 - Year Event

= 40 in

| Discharge | | Velocity | | Depth | | HGL @ Hw/D = 1.49 | | | |
|-----------|---------|----------|--------|--------|------|-------------------|-------|-------|-------|
| Total | Culvert | Over Top | Down | Up | Down | Up | Down | Up | Hw |
| (cfs) | (cfs) | (cfs) | (ft/s) | (ft/s) | (in) | (in) | (ft) | (ft) | (ft) |
| 217.70 | 217.70 | 0.00 | 12.05 | 8.81 | 23.5 | 35.8 | 95.26 | 96.79 | 98.76 |

 $Notes: IDF\ Curves = Atlas14-IDF. idf;\ Tailwater = Channel\ 1,\ Id = Sample\ Channel,\ Velocity = 7.61\ ft/s,\ Tailwater\ Elev. = 94.90\ ft/s,\ Tailwater\ Elev. =$



Culvert Studio v 2.0.0.19 06-17-2020

Existing - 68 McFadden

Culvert 1

CULVERT EMBANKMENT

Shape = Arch Pipe Top Width = 16.00 ft

Inlet Edge = Square Edge/ Hdwall Top Elevation = 99.40 ft

Material = Corrugated Steel Crest Length = 16.00 ft

Manning's n = 0.024Rise = 40 in DISCHARGE

Span = 59 in Method = Rational Method

Invert Elev. Down = 93.30 ft Drainage Area = 211.00 ac

Length = 18.00 ft Runoff Coefficient = 0.33

Slope = 0.028 ft/ft Time of Concentration = 32.6 min

Invert Elev. Up = 93.80 ft

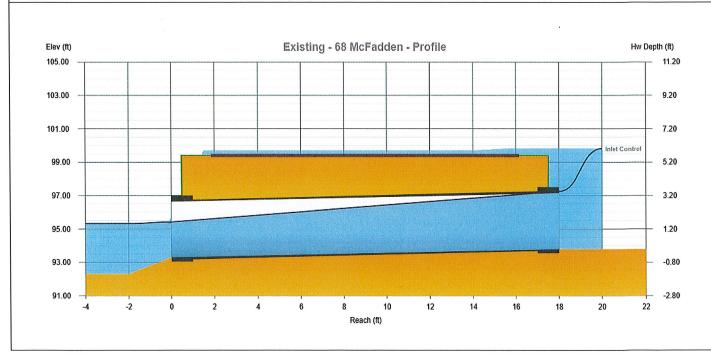
No. Barrels = 2 **TAILWATER**

Plan Skew Angle = 20 degrees Tailwater Condition = Channel 1

CALCULATION SAMPLE, 100 - Year Event

| | Discharge | | Velo | Velocity Depth | | pth | HG | L @ Hw/D = 1 | .81 |
|--------|-----------|----------|--------|----------------|------|------|-------|--------------|-------|
| Total | Culvert | Over Top | Down | Up | Down | Up | Down | Up | Hw |
| (cfs) | (cfs) | (cfs) | (ft/s) | (ft/s) | (in) | (in) | (ft) | (ft) | (ft) |
| 269.56 | 256.59 | 12.97 | 13.30 | 9.97 | 25.4 | 40.0 | 95.41 | 97.25 | 99.82 |

Notes:IDF Curves = Atlas14-IDF.idf; Tailwater = Channel 1, Id = Sample Channel, Velocity = 8.11 ft/s, Tailwater Elev. = 95.32 ft



Invert Elev. Up

Culvert Studio v 2.0.0.19 06-17-2020

Proposed - 68 McFadden

Culvert 2

CULVERT EMBANKMENT

Shape = Circular Top Width = 16.00 ft

Inlet Edge Top Elevation = 99.70 ft= Beveled

Crest Length Material = HDPE = 16.00 ftManning's n = 0.012

Rise = 48 in **DISCHARGE**

Span = 48 inMethod = Rational Method

Invert Elev. Down = 211.00 ac= 93.00 ftDrainage Area = 18.00 ftRunoff Coefficient = 0.33

Length

Time of Concentration = 32.6 min Slope = 0.028 ft/ft

No. Barrels = 2 **TAILWATER**

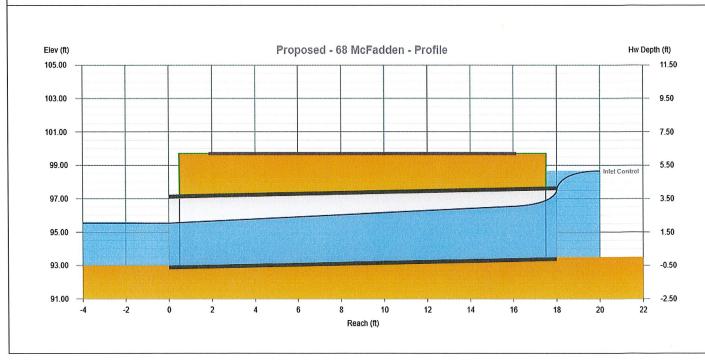
Plan Skew Angle **Tailwater Condition** = Channel 2 = 20 degrees

CALCULATION SAMPLE, 25 - Year Event

= 93.50 ft

| | Discharge | | Discharge Velocity | | Depth | | HGL @ Hw/D = 1.29 | | .29 |
|--------|-----------|----------|--------------------|--------|-------|------|-------------------|-------|-------|
| Total | Culvert | Over Top | Down | Up | Down | Up | Down | Up | Hw |
| (cfs) | (cfs) | (cfs) | (ft/s) | (ft/s) | (in) | (in) | (ft) | (ft) | (ft) |
| 217.70 | 217.70 | 0.00 | 12.98 | 10.22 | 30.4 | 37.9 | 95.53 | 96.66 | 98.66 |

Notes:IDF Curves = Atlas14-IDF.idf; Tailwater = Channel 2, Id = Sample Channel, Velocity = 7.61 ft/s, Tailwater Elev. = 95.60 ft



Culvert Studio v 2.0.0.19 06-17-2020

Proposed - 68 McFadden

Culvert 2

| CULVERT | EMBANKMENT |
|---------|------------|
| | |

Shape = Circular Top Width = 16.00 ft

Inlet Edge Top Elevation = 99.70 ftMaterial = HDPE Crest Length = 16.00 ft

Manning's n = 0.012

Rise

= Beveled

= 48 in

Span = 48 inMethod = Rational Method

DISCHARGE

Invert Elev. Down = 93.00 ftDrainage Area = 211.00 ac

Length = 18.00 ft**Runoff Coefficient** = 0.33

Time of Concentration = 32.6 min Slope = 0.028 ft/ft

Invert Elev. Up = 93.50 ft

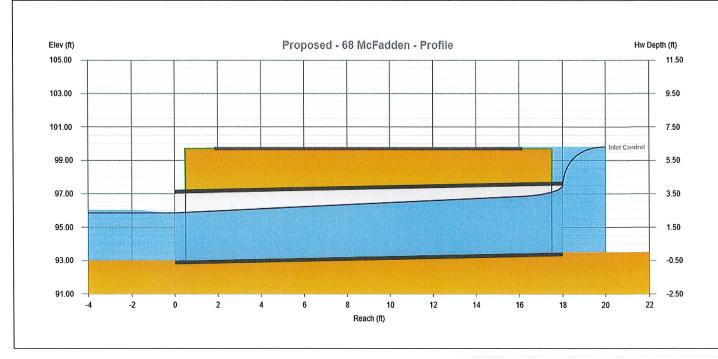
No. Barrels = 2 **TAILWATER**

Plan Skew Angle = Channel 2 = 20 degrees **Tailwater Condition**

CALCULATION SAMPLE, 100 - Year Event

| | Discharge | | Velocity | | De | Depth HGL @ | | L @ Hw/D = 1 | 1.58 |
|--------|-----------|----------|----------|--------|------|-------------|-------|--------------|-------|
| Total | Culvert | Over Top | Down | Up | Down | Up | Down | Up | Hw |
| (cfs) | (cfs) | (cfs) | (ft/s) | (ft/s) | (in) | (in) | (ft) | (ft) | (ft) |
| 269.56 | 267.90 | 1.66 | 13.98 | 11.59 | 34.2 | 41.5 | 95.85 | 96.96 | 99.81 |

Notes:IDF Curves = Atlas14-IDF.idf; Tailwater = Channel 2, Id = Sample Channel, Velocity = 8.11 ft/s, Tailwater Elev. = 96.02 ft



MCCHORD ENGINEERING ASSOCIATES, INC.



Executive Offices, Suite 202 78 Danbury Rd., Wilton, CT 06897 (203) 834-0569 FAX (203) 834-2789

| JOB: | 68 McFadden Drive, Wilton, CT | | | | | | |
|----------|-------------------------------|-------|---------|--|--|--|--|
| BY: | TSN | DATE: | 6/16/20 | | | | |
| CHECKED: | | DATE: | | | | | |
| | | | | | | | |

WORKSHEET: COMPOSITE C VALUE

Total Area (acres):

211.0000

Area No:

1

COVER CONDITIONS - CULVERT WATERSHED

| Cover Description | С | Area (ac) | CxA |
|------------------------------|---------|-----------|---------|
| Single Family, B-Group Soils | 0.35 | 103.4000 | 36.1900 |
| Single Family, C-Group Soils | 0.40 | 66.3000 | 26.5200 |
| Wooded, D-Group Soils | 0.18 | 41.3000 | 7.4340 |
| | | | |
| | | | |
| | Totals: | 211.0000 | 70.1440 |

C(Weighted) =

0.33

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| JOB: | 68 McFadden Drive, Wilton, CT | | | | | | |
|----------|-------------------------------|-------|---------|--|--|--|--|
| BY: | TSN | DATE: | 6/16/20 | | | | |
| CHECKED: | | DATE: | | | | | |
| PAGE | | _ | | | | | |

DRAINAGE COMPUTATIONS: RATIONAL METHOD

COMMON RUNOFF COEFFICIENTS

| Type of Drainage Area | Runoff Coefficient, C | |
|--|-----------------------|--|
| Categorized by Surface | | |
| Forested | 0.06 - 0.20 | |
| Asphalt | 0.70 - 0.95 | |
| Brick | 0.70 - 0.85 | |
| Concrete | 0.80 - 0.95 | |
| Shingle Roof | 0.70 - 0.95 | |
| Lawns, well-drained (sandy soil) | | |
| Up to 2% slope | 0.05 - 0.10 | |
| 2% to 7% slope | 0.10 - 0.15 | |
| Over 7% slope | 0.15 - 0.20 | |
| Lawns, poorly-drained (clay soil) | | |
| Up to 2% slope | 0.13 - 0.17 | |
| 2% to 7% slope | 0.18 - 0.22 | |
| Over 7% slope | 0.25 - 0.35 | |
| Driveways, walkways | 0.75 - 0.85 | |
| Categorized by Use | | |
| Farmland | 0.05 - 0.30 | |
| Pasture | 0.05 - 0.30 | |
| Unimproved | 0.10 - 0.30 | |
| Parks | 0.10 - 0.25 | |
| Cemeteries | 0.10 - 0.25 | |
| Railroad yards | 0.20 - 0.40 | |
| Playgrounds (except asphalt or concrete) | 0.20 - 0.35 | |
| Business districts | | |
| Neighborhood | 0.50 - 0.70 | |
| City (downtown) | 0.70 - 0.95 | |
| Residential | | |
| Single-family | 0.30 - 0.50 | |
| Multi-units, detached | 0.40 - 0.60 | |
| Multi-units, attached | 0.60 - 0.75 | |
| Suburban | 0.25 - 0.40 | |
| Apartments, condominiums | 0.50 - 0.70 | |
| Industrial | 3.00 3.70 | |
| Light areas | 0.50 - 0.80 | |
| Heavy areas | 0.60 - 0.90 | |

MCCHORD ENGINEERING ASSOCIATES, INC. CONSULTING CIVIL ENGINEERS



Executive Offices, Suite 202 78 Danbury Rd., Wilton, CT 06897 (203) 834-0569 FAX (203) 834-2789

| JOB: | 68 McFadden | Drive, | Wilton, | CT |
|------|-------------|--------|---------|----|
|------|-------------|--------|---------|----|

| BY: | TSN | DATE: | 6/16/20 | |
|----------|-----|-------|---------|--|
| CHECKED: | | DATE: | | |
| | | | | |

WORKSHEET: TIME OF CONCENTRATION (Tc)

Condition:

Existing

Area No:

Compute:

T_c through sub-area

Sheet Flow (Applicable to T_c only)

- 1. Surface description
- 2. Manning's roughness coefficient, n
- 3. Flow length, L (ft) [total <= 300 ft]
- 4. Two-year 24-hour rainfall, P2 (in)
- 5. Land slope, s (ft/ft)

6. Tt =
$$\frac{0.007 \text{ (nL)}^{0.8}}{P_2^{0.5} \text{s}^{0.4}}$$

Compute T_t (min)

Segment ID

BC

| Segment ID | AB | | |
|---------------------------|--------|--|------|
| | lawn | | |
| | 0.24 | | |
| | 150 | | |
| | 3.3 | | |
| | 0.0190 | | _ |
| pute T _t (min) | 19.8 | | 19.8 |

CD

Shallow Concentrated Flow

- 7. Surface description
- 8. Velocity Factor, Kv (ft/s)
- 9. Flow length, L (ft)
- 10. Watercourse slope, s (ft/ft)
- 11. Average velocity, V (ft/s)

12. Tt =
$$\frac{L}{3600 \text{ V}}$$

Compute T_t (min)

| | lawn | lawn | |
|----|--------|--------|---------|
| | 7.0 | 7.0 | |
| | 340 | 120 | |
| | 0.0240 | 0.1100 | |
| | 1.084 | 2.322 | |
| 1) | 5.2 | 0.9 | 6.1 |

Channel Flow

- 13. Cross sectional flow area, a (ft²)
- 14. Wetted perimeter, pw (ft)
- 15. Hydraulic radius, r = a/pw (ft)
- 16. Channel slope, s (ft/ft)
- 17. Manning's roughness coefficient, n
- 18. V = (1.486/n) r2/3s1/2 (ft/s)
- 19. Flow length, L (ft)

20. Tt =
$$\frac{L}{3600 \text{ V}}$$

Compute T_t (min)

| Segment ID | DE | EF | FG |
|---------------------------|--------|---------|---------|
| | 4.0000 | 20.0000 | 45.0000 |
| | 5.4800 | 13.6600 | 20.4800 |
| | 0.7299 | 1.4641 | 2.1973 |
| | 0.1200 | 0.0480 | 0.0330 |
| | 0.060 | 0.050 | 0.050 |
| | 6.955 | 8.396 | 9.125 |
| | 650 | 1450 | 1200 |
| pute T _t (min) | 1.6 | 2.9 | 2.2 |

21. Watershed or sub-area T_c or T_t (add T_t in steps 6, 12, and 20) (min)

32.6

6.7