INLAND WETLANDS COMMISSION Telephone (203) 563-0180 Fax (203) 563-0284



TOWN HALL 238 Danbury Road Wilton, Connecticut 06897

APPLICATION FOR A SIGNIFICANT REGULATED ACTIVITY

	·	
For Office Use Only:		
	WET#	
Filing Fee \$	Wilton Land Record Map#	
Date of Submission	Volume # Page #	
Date of Acceptance	Assessor's Map #Lot#	
APPLICAN	NT INFORMATION:	
Applicant Wilton Campus 1691, LLC (Nichola	Agent (if applicable) Sara Berryman, VHB	
Address 500 North Broadway, Suite 201	Address 100 Great Meadow Road, Suite 200	
Jericho, NY 11753	Wethersfield, CT 06109	
Telephone (917) 699-0960	Telephone 860-807-4336	
Email_nbrown@kimcorealty.com	Email_sberryman@vhb.com	
	T INFORMATION:	
Property Address 21-23 River Road		
Acres of altered Wetlands On-Site_0		
Linear Feet of Watercourse_+/- 530ft	Cu. Yds. of Material to be Deposited 980 CY	
Linear Feet of Open Water	Acres of altered upland buffer+/-0.93-acres	
Sq. Ft. of proposed and/or altered impervious coverage <u>+/-0.7-acres</u>	Sq. Ft. of disturbed land in regulated area Disturbances within regulated area are limited to only the 100' upland buffer. no direct wetland impacts are proposed.	
APPLICAT	ION REQUIREMENTS:	

Is The Site Within a Publ	lic Water Supply
Is The Site Within a Publ Watershed Boundary? N	NO YES*

Is The Site Within 500 Feet of a Town Boundary?

* If the answer is yes, then the applicant is responsible for notifying the appropriate water authority and/or adjoining community's Wetlands Department. Instructions for notification are available at the office of the commission.

Page 2 Application for a Significant Regulated Activity

Project Description and Purpose: <u>The proposal seeks to demolish a portion of the existing building that fronts River Rd</u> and proposed to construct two (2) new buildings, totaling +/-170 total residential units and approx. +/-12,000 SF of retail and restaurant space. The parking lot will be reconstructed to accommodate the two new buildings, as well as landscaping, utility, site lighting, and stormwater management improvements to support the use.

In addition, the applicant shall provide eleven (11) collated copies of the following information as well as an electronic submission via email to mike.conklin@wiltonct.org & elizabeth.larkin@wiltonct.org **

\checkmark	A.	Written consent from the owner authorizing the agent to act on his/her behalf
\checkmark	В.	A Location Map at a scale of $1'' = 800'$
\checkmark	· C.	A Site Plan showing existing and proposed features at a scale not to exceed 1" = 40' accurate to the level of a A-2 property and T-2 topographic surveys
\checkmark	D.	Sketch Plans depicting the alternatives considered see "Narrative"
\checkmark	E.	Engineering Reports and Analysis and additional drawing to fully describe the proposed project
\checkmark	F.	Sedimentation and Erosion Control Plan, including the Construction Sequence
\checkmark	G.	Names and addresses of adjoining property owners
\checkmark	H.	A narrative describing, in detail
		a. the proposed activity c. impacts b. the alternatives considered d. proposed mitigation measures
\checkmark	I.	Soils Report prepared by a Certified Soil Scientist and Wetlands Map prepared by a Registered Land Surveyor
\checkmark	J.	A Biological Evaluation prepared by a biologist or other qualified professional
\checkmark	K	Description of the chemical and physical characteristics of fill material to be used in the Regulated Area see "Narrative"
\checkmark	L.	Description and maps detailing the watershed of the Regulated Area
\checkmark	М.	Envelopes addressed to adjacent neighbors, the applicant, and/or agent, with <u>certified</u> postage and no return address
** 4	lintor	motorials shall be colleted and conject of documents more than two nages in length shall be double

**Application materials shall be collated and copies of documents more than two pages in length shall be double sided.

See Section 7 of the Wetlands and Watercourses Regulations of the Town of Wilton for a more detailed description of applications requirements.

The Applicant or his/her agent certifies that he is familiar with the information provided in this application and is aware of the penalties for obtaining a permit through deception, inaccurate or misleading information.

By signing this application, permission is hereby given to necessary and proper inspections of the subject property by the Commissioners and designated agents of the Commission or consultants to the Commission, at reasonable times, both before and after a final decision has been rendered.

Wilton Campus 1691, LLC by its Agent, Gregory and Adams, P.C. Applicant's Signature: Wilton Campus 1691, LLC by its Agent, Gregory and Adams, P.C. Agent's Signature (if applicable); Agent's	2027
Applicant's Signature: <u>(Li Ca Aey Ne a Cy Ke</u> Date: April 23,	2024
Wilton Campus 169. LLC by its Agent, Gregory and Adams, P.C.	
Agent's Signature (if applicable): (A start of the start	2024
Agent's Signature (in approvale),	
	2.53

GREGORY AND ADAMS, P.C.

PAUL H. BURNHAM SUSAN L. GOLDMAN J. VANCE HANCOCK DERREL M. MASON* MATTHEW C. MASON* JAMES D'ALTON MURPHY* KATHLEEN L. ROYLE * RALPH E. SLATER ROGER R. VALKENBURGH * ATTORNEYS AT LAW 190 Old Ridgefield Road Wilton, CT 06897 (203) 762-9000 FAX: (203) 834-1628

ESTABLISHED 1964

WWW.GREGORYANDADAMS.COM

J. CASEY HEALY OF COUNSEL

JULIAN A. GREGORY (1912 - 2002)

THOMAS T. ADAMS (1929 - 2015)

PLEASE REPLY TO SENDER: J. CASEY HEALY DIRECT DIAL: 203-571-6304 jhealy@gregoryandadams.com

April 23, 2024

By E-mail and Hand Delivery

Inland Wetlands Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897 Attn: Mr. Mike Conklin – Director of Environmental Affairs

> Re: Wilton Campus 1691, LLC – Application to Inland Wetlands Commission Premises: <u>15-21 River Road, Wilton, Connecticut</u>

Dear Mr. Chairman and Members of the Commission:

As attorney for Wilton Campus 1691, LLC ("WC1691"), we hereby submit materials prepared in support of its proposed redevelopment at the Premises, a small portion of which will occur in a regulated area (not in a wetlands or watershed). We enclose thirteen full-size and one reduced-size copies for the Commission of each the following in support of WC1691's application for significant regulated activity:

- 1. Authorization letter signed by WC1691 authorizing Gregory and Adams to act as its Agent in connection with all Wilton land use matters.
- 2. Assessor's Parcel Map.
- 3. Application for a Significant Regulated Activity.
- 4. Wetland Narrative & Application Material prepared by VHB dated April 18, 2024.
- 5. Site Civil Planset titled "Proposed Redevelopment, 21-23 River Road, Wilton, CT" prepared by VHB dated April 23, 2024.
- 6. Stormwater Management Report prepared by VHB dated April 2024.
- 7. Title Certification Letter prepared by Gregory and Adams, P.C.

* Also Admitted in New York

Inland Wetlands Commission April 23, 2024 Page 2 of 2

8. List of Project Professionals.

I also enclose:

- 1. Gregory and Adams' check in the amount of \$1,260.00 in payment of the application fee
- 2. Gregory and Adams' check in the amount of \$15.84 in payment of the certificate of mailing fee.
- 3. Envelopes addressed to owners of property adjoining the Premises.
- 4. Two envelopes addressed to Gregory and Adams, P.C.

We do not believe a third-party review of this application is required but recognize that this decision falls within the purview of the Commission. If the Commission desires to request a third-party review, Wilton Campus 1691 would like the opportunity to discuss the scope of the review with the Commission. Thank you.

We look forward to presenting the application to the Commission.

Respectfully submitted, Gregory and Adams, P.C.

1s 9. Casey Healy

By: _

J. Casey Healy

JCH/ko Enclosures By email only, with enclosures: cc: Nicholas Brown – Wilton Campus 1691, LLC Craig Flaherty – Redniss & Mead Matt Renauld – Mahan Rykiel Associates

Mark Grocki – VHB Ricky Long, Ahmed Aly and Brian O'Connor – Cube 3 Kathleen L. Royle, Esq.

GREGORY AND ADAMS, P.C.

PAUL H. BURNHAM SUSAN L. GOLDMAN J. VANCE HANCOCK DERREL M. MASON* MATTHEW C. MASON* JAMES D'ALTON MURPHY* KATHLEEN L. ROYLE * RALPH E. SLATER ROGER R. VALKENBURGH * ATTORNEYS AT LAW 190 Old Ridgefield Road Wilton, CT 06897 (203) 762-9000 FAX: (203) 834-1628

ESTABLISHED 1964

WWW.GREGORYANDADAMS.COM

J. CASEY HEALY OF COUNSEL

JULIAN A. GREGORY (1912 - 2002)

THOMAS T. ADAMS (1929 - 2015)

* Also Admitted in New York Also Admitted in Vermont PLEASE REPLY TO SENDER: J. CASEY HEALY DIRECT DIAL: 203-571-6304 jhealy@gregoryandadams.com

February 28, 2024

By E-Mail Only

Wilton Campus 1691, LLC c/o Mr. Nicholas Brown

Re: Wilton Campus 1691, LLC – Land Use Applications Premises: 15 and 21 River Road, Wilton, Connecticut

Dear Mr. Brown:

As you know, we are in the process of preparing land use applications to various Town of Wilton and State of Connecticut and other government agencies, if applicable. These agencies require written authorization from the applicant and owner authorizing Gregory and Adams, P.C to act as its agent in connection with any and all land use matters involving the subject Premises. Please sign a copy of this letter as applicant and owner and return it to me by email.

Very truly yours,

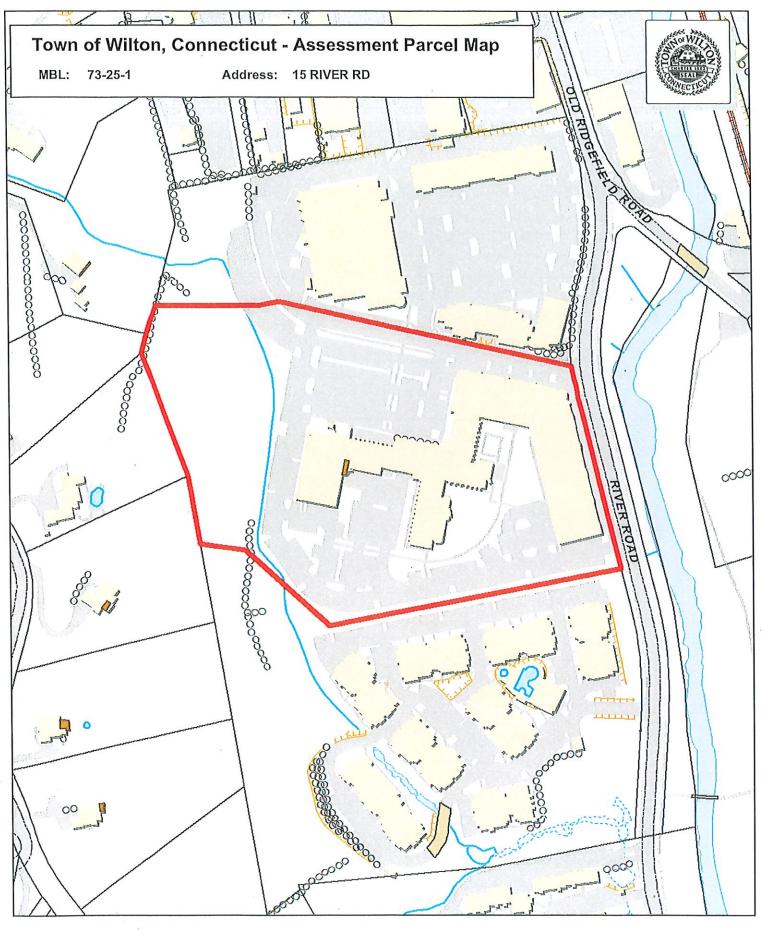
Isl J. Casey Healy J. Casey Healy

JD'AM/ko

The undersigned hereby authorizes Gregory and Adams, P.C. to act as its agent in connection with the above-referenced matters.

Wilton Campus 1691, LLC

By: _____ Nicholas Brown Vice President



W E

Approximate Scale: 1 inch = 200 feet Disclaimer: This map is for informational purposes only. All information is subject to verification by any user. The Town of Wilton and its mapping contractors assume no legal responsibility for the information contained herein.

Map Grand List Date: Oct 2017 110 220 330 Feet

0

GREGORY AND ADAMS, P.C.

PAUL H. BURNHAM SUSAN L. GOLDMAN J. VANCE HANCOCK DERREL M. MASON* MATTHEW C. MASON* JAMES D'ALTON MURPHY* KATHLEEN L. ROYLE * RALPH E. SLATER ROGER R. VALKENBURGH *

* Also Admitted in New York ② Also Admitted in Vermont ATTORNEYS AT LAW 190 Old Ridgefield Road Wilton, CT 06897 (203) 762-9000 FAX: (203) 834-1628

ESTABLISHED 1964

WWW.GREGORYANDADAMS.COM

J. CASEY HEALY OF COUNSEL

JULIAN A.GREGORY (1912 - 2002)

THOMAS T. ADAMS (1929 - 2015)

PLEASE REPLY TO SENDER: J. CASEY HEALY DIRECT DIAL: 203-571-6304 jhealy@gregoryandadams.com

April 16, 2024

By E-mail and Hand Delivery

Inland Wetlands Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897 Attn: Mr. Mike Conklin – Director of Environmental Affairs

> Re: Wilton Campus 1691, LLC – Application to Inland Wetlands Commission Premises: <u>15-21 River Road</u>, Wilton, Connecticut

Dear Mr. Chairman and Members of the Commission:

As attorneys for Wilton Campus 1691, LLC, we hereby certify that title to the above-referenced Premises is vested in Wilton Campus 1691, LLC by virtue of a Statutory Quit Claim Deed from Wilton Executive Campus, LLC to Wilton Campus 1691, LLC dated March 4, 2013 and recorded on March 6, 2013 in Volume 2311 of the Wilton Land Records at Page 53. A copy of the Deed is enclosed.

Respectfully submitted, Gregory and Adams, P.C.

Is J. Casey Healy

By:

J. Casey Healy

JCHko Enclosure

00129261 · VOL: 2311 FG: 53

STATUTORY QUITCLAIM DEED

KNOW ALL PERSONS BY THESE PRESENTS THAT:

WILTON EXECUTIVE CAMPUS, LLP, a Connecticut limited liability partnership having an address at c/o Sparrow Management LLC, 1300 Post Road East, Westport, Connecticut 06880 (the "Grantor"), for good and valuable consideration, grants to WILTON CAMPUS 1691, LLC, a Delaware limited liability company having an address at c/o Sparrow Management LLC, 1300 Post Road East, Westport, Connecticut 06880 (the "Grantee"), with QUITCLAIM COVENANTS, the following:

All that certain piece or parcel of land with the improvements thereon, located in the City of Wilton, County of Fairfield, and State of Connecticut, being bounded and described on Exhibit A attached hereto

IN WITNESS WHEREOF, the Grantor has executed this instrument as of the $\frac{4}{100}$ day of $\frac{1000}{1000}$, 2013.

Witnesses:

E. Claire Ingram

STATE OF CONNECTICUT

COUNTY OF FAIRFIELD

ss.: Town of Westport

The foregoing instrument was acknowledged before me this February 27, 2013 by Stephen J. . . . Saft, a managing partner of Wilton Executive Campus LLP, on behalf of the partnership:

Stephan B. Grozinger, Esq. . Commissioner of the Superior Court

No Conveyance Tax Collected Bettye Joan Rasosnetti Town Clerk of Wilton

Quitclaim Deed - Wilton Executive Campus

WILTON EXECUTIVE CAMPUS, LLP

By anaging partner

00129261 VOL: 2311 PG: 54

Exhibit A

Real property known as 15 River Road in the City of Wilton, County of Fairfield, State of Connecticut, described as follows:

All that certain tract, piece or parcel of land, together with the buildings and other improvements located thereon, situated, lying and being in the Town of Wilton, County of Fairfield and State of Connecticut, shown as Parcel "A" 12.1986 acres, and as more particularly delineated on a survey entitled "Improvement location Survey of Property in Wilton, Connecticut prepared for Wilton Campus Properties, LLC" dated February 11, 2000, prepared by Robert L. Liddel Jr. of the firm of Rocco V. D'Andrea, Inc., and filed in the Wilton Town Clerk's Office as Map No. 5214.

Together with the slope and drainage pipe rights and agreements benefiting the premises as set forth in the deed from Wilton Properties Associates to Julius Wile Sons & Co., Inc. dated April 26, 1977 and recorded April 26, 1977 in Volume 273 at Page 258 of the Wilton Land Records.

Together with the rights benefiting the premises granted in the Easement And Right-Of-Way from Albert J. Kleban, Trustee, to Nabisco, Inc. dated December 3, 1985 and recorded December 4, 1985 in Volume 520 at Page 147 of the Wilton Land Records.

Together with the drainage easement benefiting the premises as granted in the Drainage Easement Agreement between Wilton Shopping Center, Limited Partnership and Wilton Executive Campus Associates dated February 17, 1990 and recorded February 21, 1990 in Volume 710 at Page 211 of the Wilton Land Records.

Being the same premises as shown on prior maps recorded in the Wilton Town Clerk's Office as Maps No. 4409 and 5158.

Together with the easements set forth in the Reciprocal Access and Parking Easement Agreement by and between Wilton River Park 1688, LLC, Wilton Executive Campus, LP and Wilton River Park North, LLC recorded August 10, 2012 in Volume 2269, Page 106 of the Wilton Land Records.

Received For Record Mar 06,2013 AT 12:33P ATTEST: Bettye J. Rasosnetti Wilton Town Clerk

Wilton Campus 1691, LLC

Land Use Applications to Town of Wilton

Premises: 15-21 River Road, Wilton, CT

List of Project Professionals

1. Owner and Applicant	Wilton Campus 1691, LLC c/o Gregory and Adams, P.C. 190 Old Ridgefield Road Wilton, CT 06897
2. Surveyor	Jack W. Shoemaker Valley Land Services, Inc. 4383 Hecktown Road Bethlehem, PA 18020 610-365-2907
3. Land Use Consultant	Craig J. Flaherty Redniss & Mead 22 1 st Street Stamford, CT 06905 C.Flaherty@rednissmead.com 203-327-0500
4. Civil Engineer	Mark Grocki VHB 100 Great Meadow Road, Ste. 200 Wethersfield, CT 06109-2377 MGrocki@VHB.com 860-807-4369
5. Landscape Architect	Matt Renauld Mahan Rykiel Associates, Inc. 3300 Clipper Mill Road, Ste. 200 Baltimore, MD 21211 mrenauld@mahanrykiel.com 443-691-8857
6. Architect	Ricky Long Cube 3 160 State Street, Floor 6 Boston, MA 02109 rlong@cube3.com 978-989-9900

7. Attorneys

J. Casey Healy, Esq. Kathleen L. Royle, Esq. Gregory and Adams, P.C. 190 Old Ridgefield Road Wilton, CT 06897 jhealy@gregoryandadams.com kroyle@gregoryandadams.com 203.762.9000

Wilton Center Redevelopment

Wetland Narrative & Application Materials

PREPARED FOR

Wilton Campus 1691, LLC 500 North Broadway, Suite 201 Jericho, NY 11753

PREPARED BY



100 Great Meadow Road Suite 200 Wethersfield, CT, 06109

APRIL 18, 2024



Memorandum

To: Chairman Nick Lee Middlebury Inland Wetlands Commission Date: April 18, 2024

Project #: 20849.00

From: Sara Berryman, CSS Wetland Scientist Mark Grocki, PE Re: 21-23 River Rd Redevelopment Wilton, CT Narrative - IW Application

Dear Chairman Lee,

The following Narrative is to accompany the application to the Inland Wetlands Commission for proposed regulated activity within 100ft of a wetland or watercourse at 21-23 River Rd in Wilton, CT (aka Wilton Center, Map 73, Lots 25.1 and 25.4, see Figure 1).

Proposed Activity:

The Applicant, Wilton Campus 1691, LLC, is proposing to redevelop a portion of the site located at 21-23 River Road in Wilton, CT. The project will include the demolition of an existing building along River Road and construct of two (2) new buildings: Building A) a four-story, $\pm 50,000$ square foot (sf) building footprint with ± 100 multifamily residential apartment units on the second, third and fourth floors with $\pm 12,000$ sf of restaurant/retail use on the first floor; and Building B) a 5-story, $\pm 25,000$ sf footprint, stand-alone building with ± 70 multifamily residential apartment units at the rear of the site. The remaining building onsite will be retained with its existing use of office and retail space. Improved landscaping, utility infrastructure, parking, stormwater management system, and wetland mitigation measures will be proposed to support the redevelopment.

The project site is located within the Norwalk River Valley on the west side of River Road. The site is bounded by Wilton River Park Plaza to the north, River Road and Norwalk River to the east, the Avalon apartment complex to the south, and a dense wooded hillside to the west.

There are two separate wetland systems located on or adjacent to the project site. Wetlands associated with the Norwalk River are located on the eastern side of River Road. Though not directly within the limit of work, the 100ft upland review buffer of the Norwalk River extends into the proposed development. A second wetland system following a small watercourse is located at the toe of slope along the western edge of the currently developed site. Work is proposed within the 100' regulated area to this westerly system, predominately within already disturbed areas for existing impervious parking lots. The westerly wetland system itself will remain unaltered and be protected as there are no direct wetland impacts proposed.

A Wetland & Watercourse Delineation Report was prepared on October 4, 2023 by VHB (Attachment C) describing the wetland resources delineated within the project site. An additional Functions and Values report (Attachment D) was



compiled describing the minimal to no impact to the adjacent wetland systems. These reports are included under separate cover.

There are no direct wetland impacts proposed for the redevelopment of the property to either of the two wetland systems. The proposed regulated activity within 100ft of a wetland or watercourse includes the following:

- 1. Re-construction of parking fields currently located within the 100' upland review buffer to the wetlands.
- 2. Construction of Building B within 100' upland review buffer, which is predominately located within an alreadydisturbed areas (parking lot).
- 3. Stormwater management and water quality improvements, including an underground retention system, rain garden, hydrodynamic water quality units, catch basins, and closed pipe network, etc.
- 4. Landscaping and utility improvements.
- 5. Wetland Mitigation plantings and improvements (further described herein and within the attached reports).

Alternatives Considered (see Attachment G):

The proposed development has evolved significantly through various stages of conception and design, over several years to meet the unique demands and expectations of the Town of Wilton. Attached to this memo are several alternatives considered for the layout of the property. The current design has undergone numerous modifications and revisions to align with the Town's strategic plan for conservation and development, bringing mixed use residential and commercial to Wilton Center. Several alternative layout designs have been thoroughly assessed and subsequently discredited as they failed to meet the prerequisite standards set by the community's plan. These designs were found lacking in preserving the town's charm, ensuring sustainable development, or permitting designated green spaces, all of which are vital to Wilton's Plan of Conservation and Development and meeting the intent of the newly adopted Form-Based Zoning Code.

The "Preferred" site layout is the result of considerable hard work and meetings with local Town Staff, Planning & Zoning Commission meetings, etc. that would accommodate the Town of Wilton's vision for Wilton Center to promote a street-scape, mixed use retail/ residential development. The following describes various site plan iterations and reasons why rejected which guided the development to the preferred site layout:

- <u>Preferred Layout: Sheet C-2.0 Layout & Materials Plan by VHB:</u>
 - The preferred layout proposes many benefits with respect to site design, stormwater quality, and surrounding critical resource area protection. Stormwater quality measures and BMPs in the form of deep sump/ hooded catch basins, hydrodynamic water quality units, underground retention system to capture

100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377 P 860.807.4300

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\docs\Permits\Wilton IWWC\Narrative -Wilton, CT.docx



and infiltrate 1" volume from roof runoff, and a rain garden are all proposed to improve water quality at the site (further described in the Stormwater Management Report prepared by VHB, under separate cover). A Wetland Mitigation Plan as described herein (and within the site civil planset) is proposed to enhance the watercourse towards the western (rear) of the property.

- As storm intensities increase over the past several years, River Rd has been discovered to be within a FEMA 100yr special flood hazard area with Base Flood Elevations established. Through analysis of the projected 100yr flood event elevations onto the site, it was also discovered that the existing building along River Rd is at risk today of inundation from the 100yr flood event. Under the proposed plan, the proposed Building A is pulled further back and away from River Rd when compared to the existing building's location and the frontage sidewalk and parking has been graded appropriately. Therefore, the proposed building is now located outside of the projected 100yr flood event. This proposal allows for a better protected building from the 100yr flood inundation, thus providing for better life/health/safety measures while maintaining proper compensatory flood volume onsite.
- The improved underground retention system is designed to infiltrate the 1" storm volume from the two (2) new buildings' rooftops. This will also help relieve any taxing of stormwater runoff volume discharging into the Norwalk River, providing relief from potential future flooding from a 100yr storm event. Moreover, there is an existing detention/ retention system onsite today consisting of 36" perforated pipes, but recent geotechnical investigations reveal that this system may be at seasonal high groundwater, putting its effectiveness at risk. It was also discovered through the design process that this existing 36" pipe system is undersized for the 1" stormwater retention, therefore the new proposed underground system seeks to alleviate these concerns and adding more storage volume while maximizing separation from groundwater. Despite the existing 36" pipe's shortcomings, a large portion of it shall remain and will connect to the new underground chamber retention system because removal of the 36" pipes will unnecessarily disturb a large, mature vegetated buffer to the southerly abutting apartment complex and will serve to expand the volume of the overall proposed retention system. (further discussions of the proposed stormwater system is described in the submitted Stormwater Management Report by VHB).
- This current layout presents a well-balanced site by pulling the building frontage (i.e. Building A) further back from River Rd while still maintaining a desirable streetscape presence and meets the expectation of Planning & Zoning commission, POCD, and Form-Based Zoning Code.
- Specific to Building B (rear building), unlike previous Alternate Versions of the site layout (described below), Building B is pulled away from the westerly watercourse and wetland system, thus proposing no direct wetland impacts. The impervious limits for the proposal are also pulled further away in the southwest corner of the site when compared to existing conditions. The vast majority of this site plan is

100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377 P 860.807.4300



contained within existing limits of impervious area with only a small portion of Building B extending beyond the existing parking lot. To offset this impervious encroachment, a wetland mitigation plan with proposed plantings is proposed (further described below).

• Alternate Versions 1, 2, 3:

The alternate plans attached have evolved over several iterations. While these iterations may seem similar to the preferred site plan, there are specific differences which are undesirable from both layout and critical resource management and protection perspectives.

- The rear (South) Bldg B presents a more aggressive layout, extending beyond limits of existing pavement, encroaching very close to wetlands which may have resulted in watercourse diversion, Army Corps of Engineers permitting and/or direct wetland impacts by extending beyond the existing impervious limits. It was hopeful and later achieved by the Preferred Layout to pull the rear Building B away from the critical wetland resources at the rear of the property.
- Specific to Alternate Version 1: The front (East) Building A infringes more on the 100yr special flood hazard zone and FEMA floodplain as this front building is closer to Norwalk River which would be very difficult to properly provide compensatory flood storage when filling within the 100yr floodzone. Furthermore, there is either no or very minimal parking in front of Building A.
- Subsequent iterations in Versions 2 and 3 provide excessive greenspace between the building and River Road which have been rejected by Planning & Zoning due to lack of active streetscape on River Rd, advising the developer against adding greenspace between the building and River Road. This prohibition was later codified in the new Form Base Code limiting building setback, in order to create an active streetscape environment.
- No-Build Alternative:
 - A no-built alternative may also be considered but is outshined by the improvements and benefits of the proposed Preferred Layout alternative. If no improvements were made, the existing stormwater management system provides limited relief for the Norwalk River flooding concerns, likely due to the fact that the existing underground system was designed 20+ years ago with different/ lessened stormwater data when compared to current data, thus an undersized and underperforming stormwater management system would remain.

100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377 P 860.807.4300

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\docs\Permits\Wilton IWWC\Narrative -Wilton, CT.docx



- Through recent geotechnical investigations, the existing onsite retention system is found to be at seasonal high groundwater, putting it at risk for inadequate volume retention or infiltration/ water quality measures. The new, proposed retention system will not only be upsized from the current system, but is proposed with proper separation from seasonal high groundwater.
- There are currently no plans to improve or enhance the existing watercourse towards the rear (west) of the property, leaving it in an unattractive, unenhanced state. The proposed mitigation planting plan seeks to improve this critical habitat (see additional discussion below under "Proposed Mitigation Measures").
- Water quality measures do exist on site but are limited. There is an existing water quality unit onsite, but it is likely undersized when compared to current rainfall data and standards.
- As discussed above, River Rd is projected to be within the FEMA 100yr special flood hazard area. Through our analysis, it is found that the projection of the 100yr flood event has the potential to affect the existing building that fronts River Road today. Under the proposed improvements plan, the new Building A will be pulled further away and slightly raised from the potential 100yr floodwaters while still maintaining appropriate flood volume compensation onsite.

Impacts:

No direct impacts to the delineated resources areas are anticipated as a result of the project. Within the 100-ft upland review area of the delineated intermittent stream along the west edge of the property, a portion of the existing parking lot will be removed, and Building B with new parking areas will be constructed. Moreover, the proposed site improvements along River Rd are within 100ft to the Norwalk River. The resulting disturbance area from these 2 locations is approximately 0.93 acres of disturbance, again only contained within the 100-ft upland review area (with no direct wetland impacts). The majority of the upland review area adjacent to the rear westerly stream is already disturbed due to the existing development and parking lots. Only approximately 500 square feet of new disturbance (i.e. beyond the existing limits of impervious parking lot) within the upland review area is proposed, which is associated with Building B.

Proposed Mitigation Measures:

While no direct wetland impacts will occur to the delineated wetland resources, plantings are proposed along the intermittent stream in the western portion of the property as a way to enhance the stream habitat. Debris that has accumulated in the stream will also be removed and supplemental plantings will be placed along the stream within an

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\docs\Permits\Wilton IWWC\Narrative -Wilton, CT.docx 100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377 P 860.807.4300



approximate 20-ft area around the streambanks, providing habitat and food sources for wildlife and enhancing the visual quality of the area. Supplemental plantings will include the following:

- Common winterberry (*Ilex verticillata*) provides food sources for songbirds, showy berries in fall/winter.
- Gray dogwood (Cornus racemosa) provides food sources for pollinators, birds, and small mammals.
- Sensitive fern (Onoclea sensibilis) provides shelter for amphibians.
- Sheep laurel (Kalmia angustifolia) provides showy flowers, food source for pollinators.
- Spicebush (*Lindera benzoin*) provides food source for pollinators and birds.

In addition to the above-mentioned mitigation measures, an Erosion and Sedimentation Control plan has been engineered and submitted with the site civil planset for protection of these critical resource areas during construction activities. The Erosion and Sediment Control plan includes measures to prevent the migration of silt and sediment during the construction process. A doubled BMP measure consisting of silt fencing and straw bales will line the perimeter of the construction area closest to the wetland resources. All catch basins will be fitted with silt sacks and will be removed/ replaced once full. A stabilized construction entrance (stone tracking pad) will be installed at the primary entrance/ exit for construction vehicles at River Rd. the Contractor will be instructed to clean/wash tires upon exiting the construction area, refresh the tracking pad when necessary, and provide street sweeping as required for any additional sediment tracked onto roadways. It is important to note that the existing site today does not drain or discharge stormwater to the rear westerly watercourse, only to the Norwalk River, therefore the Contractor will be instructed to monitor the Norwalk River for sediment discharges after each rainfall event to ensure the protection of the watercourse. There will be a designated concrete washout area located onsite during construction, well away from any critical resource areas, as well as temporary sediment detention basins for dewatering, as needed.

A Soil and Groundwater Management Plan (SGWMP) for use and implementation during construction activities is recommended for the contractor to follow. A summary memorandum of the recommended SGWMP best management practices is included with this submission (Attachment F).

Fill Material: Chemical and Physical Characteristics

The anticipated fill material imported to support construction of the proposed development that will be located within 100' of a wetland or watercourse will primarily consist of the following:

• Process aggregate base material and bituminous asphalt pavement to support parking lots and drive aisles.

100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377 P 860.807.4300

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\docs\Permits\Wilton IWWC\Narrative -Wilton, CT.docx



- Concrete: for sidewalks, building foundations and slabs, pavers, etc., or for stormwater management systems such as underground detention chambers, manholes, catch basins, or for sanitary sewer structures such as manholes.
- Landscaping including loam and seed/sod (grass/ vegetation stabilization), mulch and shrubs/ trees.
- Materials for utilities include the following: PVC (sewer pipe), HDPE (storm), Copper (domestic water less than 2"), ductile iron (domestic water 2" and greater or fire protection), concrete (manhole structures), etc.
- Light pole foundations & conduits

Attachments:

- Figure 1 Site Location Map
- Attachment A Town of Wilton Application for a Significant Regulated Activity Form
- Attachment B VHB Site Civil Planset, "Proposed Redevelopment, 21-23 River Rd, Wilton, CT" (Under separate cover)
- Attachment C VHB Wetlands and Watercourse Delineation Report, dated October 4, 2023
 - Figure 1 USGS Site Location Map
 - Figure 2 Delineated Wetlands and Watercourses Sketch
 - Appendix A Site Photograph Log
- Attachment D VHB Wetland Functions & Values Report, dated April 19, 2024
 - Appendix A VHB Wetland and Watercourses Delineation Report (Referenced above)
 - Appendix B Wetland Functions/Value Evaluation Form
 - Appendix C CT DEEP NDDB Map (December 2023)
- Attachment E VHB Stormwater Management Report (Under separate cover)
- Attachment F VHB Soil and Groundwater Management Plan Summary, dated April 23, 2024
- Attachment G Alternative Plan Versions
- Attachment H Wilton Campus 1691 LLC Letter of Authorization to VHB
- Attachment I Abutters List

100 Great Meadow Road Suite 200 Wethersfield, CT 06109-2377

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\docs\Permits\Wilton IWWC\Narrative -Wilton, CT.docx



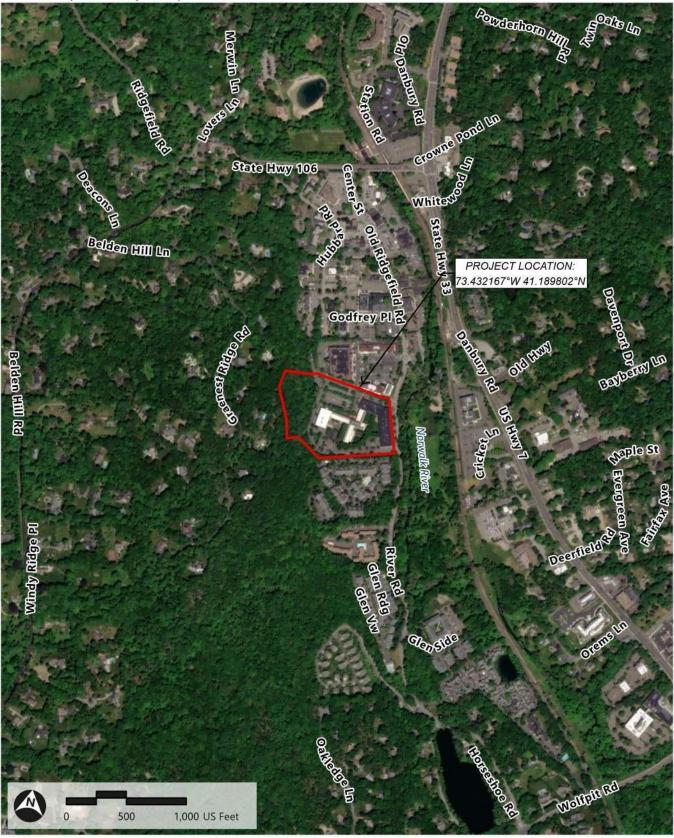
FIGURES

e Le state de la second	. • *	۰۰، ۲۰۰۰ ۱۰۰۰ - ۲۰۰۰
	•	······································
		······································
· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
		· · · · · · · · · · · · · · · · · · ·

Figure 1: USGS Site Location Map

Wilton Campus Development | Wilton, Connecticut





Project Location

ATTACHMENT A

TOWN OF WILTON APPLICATION FOR A SIGNIFICANT REGULATED ACTIVITY FORM

. 19.....

ATTACHMENT B

VHB SITE CIVIL PLANSET, "PROPOSED REDEVELOPMENT, 21-23 RIVER RD, WILTON, CT"

(Under separate cover)

ATTACHMENT C

VHB WETLANDS AND WATERCOURSES DELINEATION REPORT



October 4, 2023

Ref: 20849.00

Mr. Nicholas Brown 500 North Broadway, Suite 201 Jericho, New York 11753

Re: Wetland & Watercourse Delineation Report Wilton Campus Development, Wilton, Connecticut

Mr. Brown,

VHB completed an on-site investigation to determine the presence or absence of wetlands and/or watercourses at 15 River Road (Parcel ID Nos. 73-25-1 and 73-25-4) in the Town of Wilton, Connecticut (Figure 1) as requested and authorized. This investigation of the site involved a wetland/watercourse delineation that was completed by a qualified soil scientist and conducted in accordance with the principles and practices noted in the United States Department of Agriculture (USDA) Soil Survey Manual (1993). The soil classification system of the National Cooperative Soil Survey was used in this investigation to identify the soil map units present on the Project site. This report includes descriptions of site conditions, photographic documentation (Appendix A), and a Delineated Wetlands and Watercourse Sketch (Figure 2) displaying resources delineated within the Project site.

INVESTIGATION

The Project site was investigated on September 1, 2022. The weather during the time of delineation was sunny, with a temperature of 83°F. The state of Connecticut has been experiencing moderate, severe, and extreme drought conditions, which were ongoing during the September 2022 delineation effort. No significant rainfall event occurred within two days prior to the site visit. Soil types are identified by observing soil morphology (soil texture, color, structure, etc.). Soil morphology is evaluated through numerous test pits and/or hand borings (generally to a depth of at least two feet). If a wetland and/or watercourse were determined to be present, their boundaries are identified with flags and hung from vegetation or small wire stakes if in fields or grass communities. These flags are labeled "Wetland Delineation" and are generally spaced a maximum of approximately 50 feet apart. If both resources are within ±10-12 feet distance of each other, the most conservative of the two lines will be delineated. It is important to note that flagged wetland and watercourse boundaries are subject to change until verified by local, state, or federal regulatory agencies.

Engineers | Scientists | Planners | Designers

100 Great Meadow Road Wethersfield, Connecticut 06109 P 860.807.4300

F 860.372.4570



REGULATORY INFORMATION

Wetlands and watercourses are regulated by both state and federal law each with different definitions and regulatory requirements. Accordingly, the State may regulate waters that fall outside of federal jurisdiction; however, where federal jurisdiction exists concurrent State jurisdiction is almost always present.

State Regulation

Wetland determinations are based on the presence of poorly drained, very poorly drained, alluvial, or floodplain soils and submerged land. *Watercourses* are defined as "rivers, streams, brooks, waterways, lakes, ponds, marshes, swamps, bogs and all other bodies of water, natural or artificial, vernal or intermittent, public or private, which are contained within, flow through or border upon the state or any portion thereof." *Intermittent watercourse* determinations are made based on the presence of a defined permanent channel and bank, and two of the following characteristics: (1) evidence of scour or deposits of recent alluvium or detritus, (2) the presence of standing or flowing water for a duration longer than a particular storm incident, and (3) the presence of hydrophytic vegetation. (See Inland Wetlands and Watercourses Act §22a-38 CGS.)

WETLAND AND WATERCOURSE SITE DESCRIPTION

Wetland classifications used to identify the type of wetland(s) occurring on the Project site are based on guidance from the U.S. Fish and Wildlife Service (USFWS) (Cowardin et.al. 1979). These are further qualified with the Hydrogeomorphic Method of wetland classification (Brinson, 1993).

Wetland/Watercourse Description

As shown in Figure 1, the Project site is located within the Norwalk River valley, with a steep slope bounding the western edge of the site and the Norwalk River channel located ± 100 feet to the east of the site. The majority of the Project site is developed by commercial and office buildings with associated parking lots and driveways, and the surrounding parcels to the north and south are also similarly developed.

The Ordinary High-Water Line (OHW Line) of an intermittent stream was delineated along the toe of the slope and adjacent to onsite parking lots during the September 2022 delineation effort. The delineation relied on physical indications of the OHW Line including:

- Natural line impressed on the bank
- Changes in the character of the soil
- Destruction of terrestrial vegetation
- Presence of litter and debris
- Presence of a wrack line
- Leaf litter disturbed or washed away



- Scour
- Deposition
- Bed and banks
- Exposed root systems

Based on a review of historic aerial imagery, in the 1940s the stream onsite was a naturally flowing stream flowing north to south along the toe of the slope of the river valley, converging with a tributary of the Norwalk River \pm 750 feet south of the Project site. Until the 1970s, the Project site and surrounding area were either undeveloped or used for agricultural purposes. However, as the development of the area progressed through the 1990s, the once naturally flowing stream was diverted and occasionally culverted to support the development of the area. Currently, the stream is culverted (See Figure 2) until daylighting \pm 150 feet to the south of the northern Project site boundary. The stream then continues to flow naturally through the site and into the adjacent property to the south.

At the time of delineation, there was no flowing or standing water within the stream channel. Leaf litter, snags, and detritus covered the majority of the channel, but a natural, well-defined channel bank was present, and a sandy stream bottom was identified throughout its presence onsite. It is anticipated that in addition to human littering, stormwater sheet flow from the adjacent steep slope and upgradient areas likely pushed detritus and snags down the slope and into the stream channel.

Due to its location at the toe of a forested slope, canopy trees and saplings were the dominant vegetation onsite during the September 2022 delineation effort. Shrubs were limited to the western bank of the stream, and the eastern bank adjacent to the onsite parking lots consisted of a maintained lawn. As stated above, uplands onsite consisted of impervious parking lots, driveways, commercial and office buildings, and associated maintained lawn areas.

TREES & SAPLINGS				
Scientific	Common	Indicator	Upland	Wetland
Acer rubrum	Red Maple	FAC	Х	Х
Acer saccharinum	Sugar maple	FACW	Х	X
Fagus grandifolia	American beech	FACU	Х	-
Liriodendron tulipifera	Tulip poplar	FACU	Χ .	-
Platanus occidentalis	American sycamore	FACW	X	· · X
Populus deltoides	Eastern cottonwood	FAC	Χ	X
Quercus alba	White oak	FACU	Х	-
	SHRUBS			
Scientific	Common	Indicator	Upland	Wetland
Clethra alnifolia	Sweet pepperbush	FACU	Х	X
Euonymus atropurpureus	Burning bush	FACU	х	х

TABLE 1: Dominant Vegetation Within and Adjacent to Watercourse (Common (*Scientific*) names.)



Fallopia japonica*	Japanese knotweed	FACU	X	-	
Lindera benzoin	Northern spice bush	FACW	-	X	
	HERBS & VINES				
Scientific	Common	Indicator	Upland	Wetland	
Alliaria petiolate	Garlic mustard	FACU	X	-	
Rosa multiflora	Multiflora rose	FACU	-	X	
Smilax rotundifolia	Common greenbrier	FAC	Х	-	

*Denotes State non-native invasive species OBL-Obligate wetland species (99% or more found in wetlands) FACW-Facultative wetland species (67%-99% found in wetlands) FAC- Facultative species (34% -66% found in wetlands) UPL- Upland species NI- No Indicator

SOIL MAP TYPES

A brief description of each soil map unit identified on the Project site is presented below including information from the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) soil descriptions. For further information on these and other soils, please refer to the internet site at http://soils.usda.gov/technical/classification/osd/index.html).

Upland Soils

Canton Soil Series

The Canton series is a Typic Dystrudept consisting of very deep, well-drained soils formed in a loamy mantle and underlain by sandy till. The series is typically found on nearly level to very steep glaciated plains, hills, and ridges with slopes that range from 0 to 35 percent. Saturated hydraulic conductivity is high in the solum and high or very high in the substratum. Diagnostic horizons and features recognized in this pedon include an ochric epipedon in the zone from 0 to 2 inches (A and E horizons) and a cambic horizon in the zone from 2 to 22 inches (Bw1 and Bw2 horizons). There is a lithologic discontinuity showing an abrupt change in sand distribution at 22 inches (2C1 horizon).

Charlton Soils

The Charlton series is a Typic Dystrudept consisting of very deep, well-drained loamy soils formed in till. The series is typically found on nearly level to very steep soils on till plains and hills with slopes that range from 0 to 50 percent. Saturated hydraulic conductivity is moderately high or high. The diagnostic horizons and features recognized in this pedon include an ochric epipedon in the zone from 0 to 4 inches (Oe & A horizon) and a cambic horizon in the zone from 4 to 27 inches (Bw horizons). The particle-size class of this series is described as coarse-loamy with sizes in the control section from 10 to 40 inches.



REFERENCES

- 1. Brinson, M.M. 1993. *A Hydrogeomorphic Classification for Wetlands*. Tech. Rpt.WRP-DE-4, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.
- Cowardin, L.M., V. Carter, F.C. Golet and E.T. LaRoe, 1979. Classification of Wetlands and Deepwater Habitats of the United States. U.S. Fish and Wildlife Service. Washington, D.C. FWS/OBS-79/31.
- United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) soil descriptions. Internet site: <u>http://soils.usda.gov/technical/classification/osd/index.html</u>).

CLOSING

Thank you for the opportunity to work with you on this Project. Please contact Jeffrey Shamas at 860-807-4388 if you have any questions or require additional assistance.

Sincerely, Vanasse Hangen Brustlin, Inc.

Anna Loss Senior Environmental and Wetland Scientist aloss@vhb.com

Jeffrey R. Shamas, CE, CSS, ENV SP, SPWS Director of Environmental Services jshamas@vhb.com

Included in Report:

Figure 1 – USGS Site Location Map		
Figure 2 – Delineated Wetlands and Wate	ercourses Sketch	
Appendix A – Site Photograph Log		



APPENDIX A SITE PHOTOGRAPH LOG

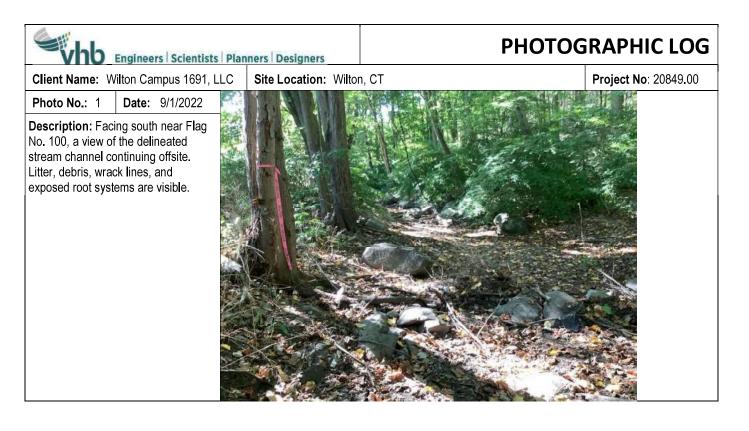
Figure 1: Site Photograph Log

Wilton Campus Development | Wilton, Connecticut

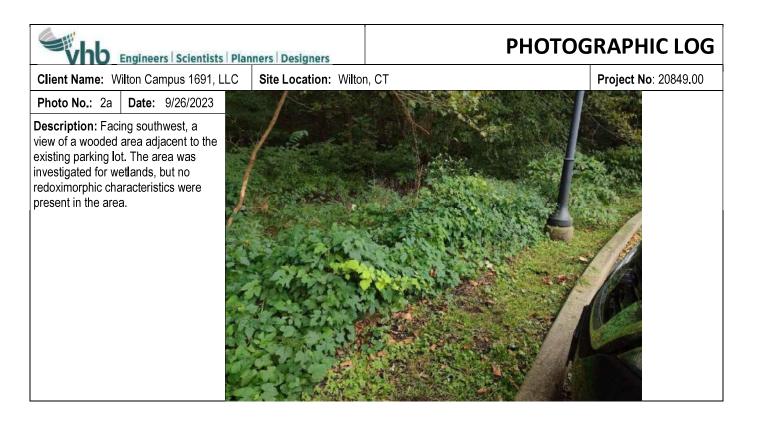




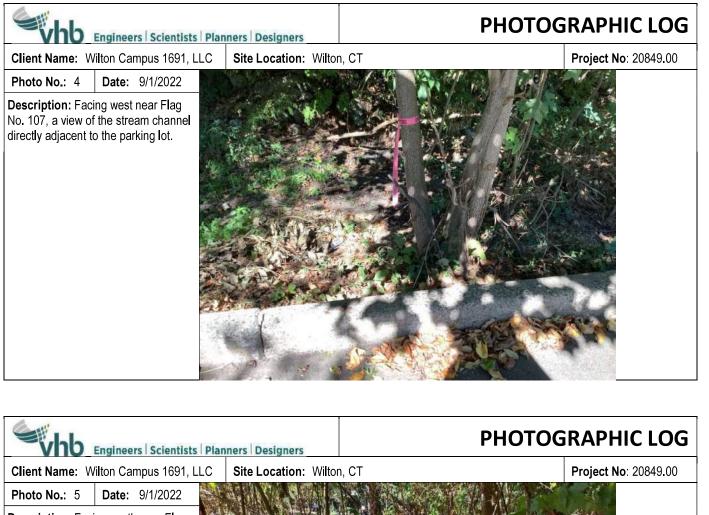
Path: \\vhb.com\gis\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\Project\Wilton Site.aprx (SPelletier, 9/29/



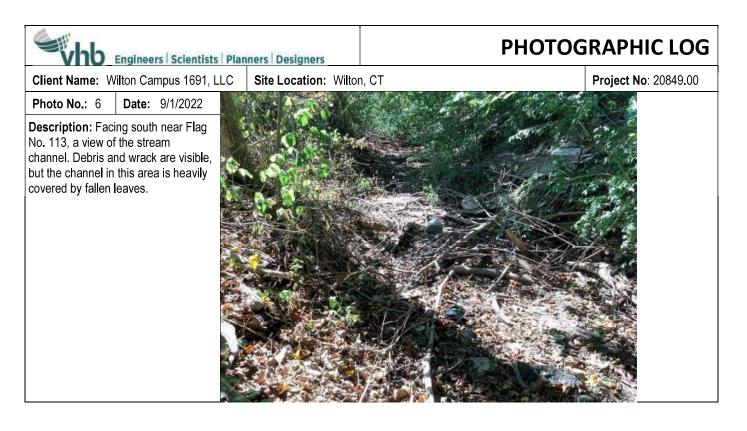
Engineers Scientists Plar	ners Designers	РНОТОС	RAPHIC LOG
Client Name: Wilton Campus 1691, LLC	Site Location: Wilton	n, CT	Project No: 20849.00
Photo No.: 2 Date: 9/1/2022			
Description: Facing north near Flag No. 101, no water is present within the stream channel. However, stained leaves, a well-defined channel, and a sandy stream bed were physical indicators used during the delineation effort.			



	nners Designers	РНОТОС	GRAPHIC LOG
Client Name: Wilton Campus 1691, LLC	Site Location: Wilto	n, CT	Project No: 20849.00
Photo No.: 3 Date: 9/1/2022			
Description: Facing north near Flag No. 104, snags are present throughout the stream channel onsite, but especially at this location. The steep slope is also visible in the background of the picture.			



Description: Facing south near Flag No. 111, the stream channel at this location is covered by fallen leaves and debris. While still defined, exposed roots and abrupt change in elevation beneath the fallen leaves were observed.



Engineers Scientists Planners Designers		PHOTOGRAPHIC LO	
Client Name: Wilton Campus 1691, LLC	Site Location: Wilto	n, CT	Project No: 20849.00
Photo No.: 7 Date: 9/1/2022			
Description: Facing north, the culvert that carries the stream from the north offsite.			

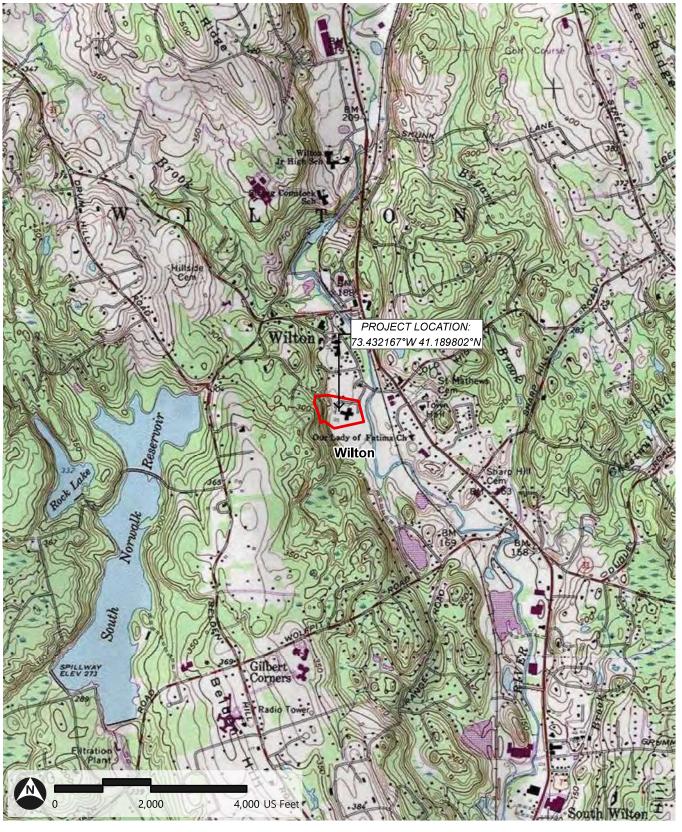


FIGURES

Figure 1: USGS Site Location Map

Wilton Campus Development | Wilton, Connecticut





Source: USGS, VHB

Project Location

Town Boundary

Figure 2: Delineated Wetlands and Watercourses Map



Wilton Campus Development | Wilton, Connecticut



ATTACHMENT D

VHB WETLAND FUNCTIONS & VALUES REPORT

Wilton Campus Development

15 River Road, Parcel Nos. 73-25-1 and 73-25-4, Wilton, Fairfield County, Connecticut

PREPARED FOR

Kimco Realty Corporation 500 North Broadway, Suite 201 Jericho, NY 11753

PREPARED BY



100 Great Meadow Road Suite 200 Wethersfield, Connecticut 06109-2377

April 2024

Table of Contents

1.	Introduction	1
2.	Site Description and Setting	
	2.1 - Current Landscape Ecological Setting	
3.	Wetland Function and Values Assessment	
4.	Proposed Activities and Potential Impacts	8
	4.1 – Proposed Activity Within Wetlands & Upland Review Area	
	4.2 – Potential Effects of Proposed Activity on Flora	
	4.3 – Potential Effects of Proposed Activity on Fauna	9
5.	References	10

Images

Image 1 – Wetland Functions and Values Categories	3
Image 2 – Project Location in HUC 12 Watershed	4

Appendices

Appendix A – VHB Wetland and Watercourses Delineation Report, dated Oct. 4, 2023
Appendix B – Wetland Function/Value Evaluation Form
Appendix C – CT DEEP NDDB Map (December 2023)



Introduction

This Wetland Function-Value Impact Report was prepared in support of a Town of Wilton Inland Wetland Commission submittal for the proposed redevelopment (herein referred to as the "Project") located at 15 River Road (Parcel Nos. 73-25-1 and 73-25-4) in Wilton, Fairfield County, Connecticut, (herein referred to as the "Site") (Figure 1). The proposed Project consists of the demolition of the existing building along River Road and construction of a four-story, \pm 50,000 square foot (sf) building that will include multi-family units on the second, third, and fourth floors, and 10,000 sf of restaurant/retail use on the first floor. Additionally, a four-story, \pm 23,000 sf stand-alone building with multi-family units will be constructed at the rear of the site. The remaining building onsite will be retained with its existing use of office and retail space. Improved landscaping, utility infrastructure, and parking is proposed to support the redevelopment.

The Site was originally investigated on September 1, 2022, during which time a state and federal wetland and watercourse delineation based on criteria used in the State of Connecticut Inland Wetlands and Watercourse Act was completed. Results of that site visit are documented in a Wetland and Watercourse Delineation Report, dated October 4, 2023 (Appendix A).

As shown in the accompanying Inland Wetland Commission submittal, the Project proposes to disturb approximately 0.93 acres of the upland review area to a delineated intermittent stream on the property. The majority of this area is currently developed with existing parking lots and buildings; the Project proposes approximately 500 sf of new disturbance (beyond the existing limits of impervious parking lot). To the east of the property lies the Norwalk River. The Project proposes impacts to the upland review area of the Norwalk River as well. Therefore, the purpose of this report is to assess the current conditions of wetlands and upland review area resources onsite, their function and values, and the effects of the proposed Project on these resources.

Site Description and Setting

The 11.8-acre lot is located at 15 River Road in Wilton, Connecticut. The property is currently occupied by a large commercial, multi-use building and associated parking lots. The areas north and south of the Site are developed, with commercial use buildings to the north and condominiums to the south. West of the Site are wooded residential properties. To the east is River Road and the Norwalk River. (Figure 2). Topography onsite ranges from 172ft to 272ft (NAVD88). Steep slopes ranging from 178ft top 272ft are present along the west side of the property; however, no work is proposed within this area. The elevations within the proposed work area range from 172ft to 182ft, gently sloping downgradient from the west to the east.

The existing building and parking areas encompass the majority of the Site. An intermittent stream (Stream 1) was delineated along the west edge of the parking lot, continuing off property to the southwest. Based on a review of historic aerial imagery, the stream was naturally flowing north to south and converging with a tributary of the Norwalk River ± 750 feet south of the Site. Until the 1970s, the Site and surrounding area were either undeveloped or used for agriculture. Development of the Site progressed through the 1990s, at which point the once naturally flowing stream was diverted and occasionally culverted to support development in the area. Currently the stream is culverted until daylighting ± 150 feet to the south of the northern Site boundary, then continues flowing naturally into the adjacent property to the south.

2.1 - Current Landscape Ecological Setting

The Site is located in southwest Connecticut, just west of the Norwalk River. The surrounding ecological neighborhood is rural with residential and light commercial development, surrounded by forested areas.

Wetland Function and Values Assessment

Wetland classifications used to identify the type of wetland(s) occurring on the Site are based on guidance from the U.S. Fish and Wildlife Service (USFWS) (Cowardin et.al. 1979).

Biophysical elements such as a wetland's landscape position, geology, hydrology, substrate, and vegetation determine the wetland functions and to what capacity they are performed. Due to the differing biophysical characteristics between on-site wetlands, the functions the wetlands provide and the capacity to perform those functions vary. To better understand these differences, a description of the assessed wetland functional values was completed based on the United States Army Corps of Engineers (USACE) Highway Methodology Workbook (1993) and its supplement workbook. This method requires a description of each of the wetland communities as well as indicating the functions they provide. The thirteen (13) functions and values that have been recognized include:

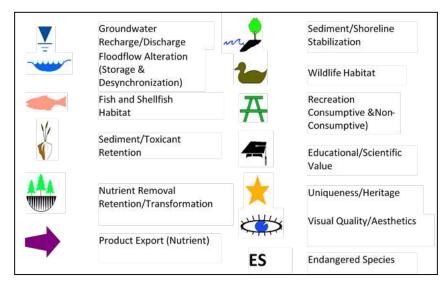


Image 1 - Wetland Function and Values Categories

Aquatic resource areas on the Site, further discussed and documented in the attached Wetland and Watercourse Delineation Report (dated October 4, 2023), consist of one intermittent stream. There is an established 100-ft upland review area regulated by the Town of Wilton.

Stream 1 is naturally occurring and located on the western side of the property. Stream 1 is an intermittent stream that originates from a culvert and flows from north to south along the western edge of the parking lot, before flowing offsite. The watercourse banks are primarily comprised of scrub-shrub vegetation, with sapling trees and a few mature canopy trees located sporadically throughout.

The Project is not proposing any impacts to the stream; however, impacts will occur in the upland areas directly abutting the stream. Therefore, a function-value assessment has been prepared below based on the USACE's 13 functions and values provided above. Please refer to Appendix B for a completed Wetland Function-Value Evaluation Form.

1. <u>Groundwater Recharge/Discharge</u> – This function considers the potential for a wetland to serve as a groundwater recharge and/or discharge area.

Stream 1 flows north to south from a culvert, continuing offsite to the southwest. It is anticipated that the stream captures stormwater sheet flow from the steep slope to the west. The adjacent parking lots are lined with a curb that would prevent regular stormwater flow from entering the stream; catch basins are also located throughout the parking lots and convey stormwater to the Norwalk River, not to Stream 1.

During the field delineation efforts, no flowing or standing water was observed in the stream, but during a subsequent site visit in February 2024, the stream was flowing with approximately 8 inches of water. Therefore, Stream 1 serves primarily as a groundwater discharge area.

 <u>Floodflow Alteration</u> – This function considers the effectiveness of the wetland in reducing flood damage by water retention for prolonged periods following precipitation events and the gradual release of floodwaters.

A FEMA-identified Flood Hazard Zone X (0.2% annual chance flood hazard) is identified along the Norwalk River to the east of the Site. The river is approximately 50-75 feet wide, with banks that rise approximately 3-4 feet, providing moderate flood water desynchronization for the area. The portion of the Site that is located within the Flood Hazard Zone X is currently developed with an existing building and parking spaces/sidewalks; the Project proposes demolishing the existing building and constructing a new building. As such, no change in the flood storage availability of the Norwalk River is anticipated.



Image 2 - Project Location in HUC 12 Watershed

No flood hazard zone is identified for Stream 1. According to aerial imagery and elevation contours, the stream is located east of a steep slope. It is expected that runoff from slope flows downgradient toward Stream 1. Stream 1 appears to have the capacity

to provide minimal flood water desynchronization (collection, storage, gradual release) during flooding events for its surrounding area. The stream collects and discharges excess water, but due to the defined channel and lack of substantial vegetated wetlands surrounding it, storage of excess water is not anticipated to occur.

As identified by the CTECO Advanced Viewer (See Image 2), the Site's HUC12 watershed (Norwalk River – Frontal Norwalk Harbor (011000060202)) is somewhat developed with moderate impervious cover present. Due to the size of the stream, the desynchronization provided would be small in relation to the size of the watershed.

 Fish and Shellfish Habitat – This function considers the effectiveness of seasonal or permanent watercourses associated with the wetland in question for fish and shellfish habitat.

Stream 1 flows from north to south and continues offsite. Stream 1 is approximately three feet in width at the widest part and approximately eight inches deep. The surrounding area is scrub-shrub/forested to the west of the stream; to the east of the stream is a paved parking lot and a large commercial, multi-use building. No fish/shellfish were observed during the site visits. Due to the narrow and shallow nature of the stream, is unlikely that the area is supportive of fish and/or shellfish habitat.

The Norwalk River is listed as an anadromous fish run for alewife and sea lamprey on the Connecticut Department of Energy and Environmental Protection's (CTDEEP) list of migratory fish runs; the river is also stocked with trout species by CTDEEP and recently underwent restoration work by Trout Unlimited. Currently, catch basins within the existing parking lots convey stormwater to the Norwalk River. The Project proposes stormwater management designs to control flows quality of stormwater that will ultimately be conveyed to the Norwalk River. As such, no impacts are anticipated to fish habitat/species within the Norwalk River as a result of the Project.

4. <u>Sediment/Toxicant/Pathogen Retention; Nutrient Removal; Product Transport</u> – This function reduces or prevents degradation of water quality, the effectiveness of the wetland as a trap for nutrients in runoff water from surrounding uplands or contiguous wetlands and the ability of the wetland to process these nutrients into other forms or trophic levels and the effectiveness of the wetland to produce food or usable products for humans or other living organisms.

Stream 1 is a small, intermittent stream that flows downstream on a slight grade, being fed by sheet flow from the adjacent steep slope to the west. It is anticipated that sediments/toxicants/pathogens are not retained onsite due to a lack of vegetated wetland in the area.

Toxicant/nutrient removal functions for Stream 1 are anticipated to be low. The banks of the stream are vegetated, but toxicants/nutrients are not expected to be held in the stream long term. In terms of product transport, the stream is not expected to be a stable source of production. Some vegetation is present along the banks (mostly scrubshrub and forested vegetation), however that vegetation is not overly diverse.

The Norwalk River is a much wider and faster flowing watercourse; the banks are vegetated, but due to the flow speed, sediments/toxicants/pathogens are not anticipated to be retained onsite. Toxicant and nutrient removal are also not expected to be held onsite long term. Product transport is expected to be higher for the Norwalk

River, as the vegetation along the banks is more diverse and there is a variety of fish and macroinvertebrates expected to be in the water.

5. <u>Sediment/Shoreline Stabilization</u> – This function considers the effectiveness of a wetland to stabilize streambanks and shorelines against erosion.

Stream 1 is a narrow, low flow watercourse that has a well-defined channel. The banks of the stream are vegetated with some low vegetation and shrubs/saplings, as well as a few more mature trees. While the vegetation may aid in stabilization, because there is not a vegetated wetland surrounding the stream, erosion and scouring may be possible in very heavy rainfall situations.

The Norwalk River is wider and faster flowing with vegetated banks. In the Project area, no vegetated wetlands are located along the river, therefore stabilization is not anticipated to be strong as erosion and scouring are likely during heavy rainfall/flooding events.

6. <u>Wildlife Habitat</u> – This function considers the effectiveness of the wetland to provide habitat for various types and populations of animals typically associated with wetlands and the wetland edge.

Stream 1's location being surrounded by residential and commercial development reduces connectivity from potential wildlife habitat nearby. While the area to the west is forested, there is a very steep, high slope that wildlife would need to navigate prior to reaching the stream. Vegetation along the stream includes some larger trees and shrubs and could provide some habitat and foraging material for avian and small mammal species, however it is unlikely that larger mammals traverse the area due the developed nature of the surrounding vicinity.

The Norwalk River is listed as an anadromous fish run for alewife and sea lamprey on the CTDEEP's list of migratory fish runs; the river is also stocked with trout species by CTDEEP and recently underwent restoration work by Trout Unlimited. The Project only proposes impacts in the upland review area of the river, where the area is currently already developed. The Project is not anticipated to add any impacts to the wildlife habitat of the Norwalk River.

7. <u>Recreation Consumption</u> – This value considers the suitability of the wetland and associated watercourses to provide recreational opportunities.

Stream 1 is situated behind and surrounded by residences/small businesses. Residential properties are located to the west of the stream and are forested in nature, but as they are private properties public access to the forested area is restricted. During site visits, people have been observed using the parking lots for walking.

The Norwalk River recently underwent trout habitat restoration work by Trout Unlimited and is utilized by fishermen for recreational fishing. On the east side of the Norwalk River is a town-owned park (Schneck's Island) that is used for walking. The Project only proposes impacts in the upland review area of the west side of the river, where the area is currently already developed; no impacts to recreation are anticipated.

8. <u>Educational/Scientific Value; Uniqueness/Heritage</u> – This value considers the suitability of the wetland as a site for an "outdoor classroom", as a location for scientific study or

research, and the effectiveness of the wetland or its associated waterbodies to provide certain special cultural resource values.

The stream and the Norwalk River are surrounded by developed, residential/commercial properties and are accessible to the public via the adjacent parking lots/sidewalks. There is no anticipated educational/scientific value to the stream, nor is Stream 1 considered unique or known to contain any remnants of historic or archeological value.

The Norwalk River does contain fish species and may provide some scientific or educational opportunities; however, the Project only proposes impacts to the alreadydeveloped upland review area and is not anticipated to impact any scientific/educational value of the Norwalk River.

 <u>Visual Quality and Aesthetics</u> – This value considers the visual and aesthetic quality or usefulness of the wetland.

Stream 1 is primarily obstructed from view by the surrounding residences and businesses. The Norwalk River is much more visible from the surrounding area of the Project; however, the Project only proposes impacts to the already-developed upland review area. No impacts to visual quality or aesthetics are anticipated.

10. <u>Endangered Species</u> – This value considers the suitability of the wetland to support threatened or endangered species.

Based on the most recent CTDEEP Natural Diversity Data Base (NDDB) mapping available (December 2023, Appendix C)), the Site is not located in or near NDDB polygon, and therefore a NDDB review request is not required. As no federal agency is involved with the Project, a review through the United States Fish and Wildlife Service's (USFWS) Information for Planning and Conservation (IPaC) system is also not required.

This stream is not anticipated to provide quality habitat for any endangered/protected species due to its small size and location within a developed, suburban downtown area with little to no connectivity to regional waterways and/or forests. The Norwalk River does contain fish species, including anadromous species, however no endangered species are anticipated in the river. Furthermore, the Project impacts are limited to the upland review area of the river and are not expected to negatively impact species within the river.

Proposed Activities and Potential Impacts

The Project proposes to redevelop a portion of the Site for a multi-use building (Building A) and a residential building (Building B), and associated parking lots.

4.1 – Proposed Activity Within Wetlands & Upland Review Area

The proposed Project will not include any direct impacts to Stream 1. Impacts will occur within the 100-foot upland review area surrounding the stream, due to the clearing of the parking lot area for construction of Building B.

The stream currently does not receive water from the parking lot, unless during flooding conditions, due to the curb height. During the winter, snow from the parking lot is sometimes plowed and piled in the grassy areas between the parking lot and the stream, therefore snowmelt may add to the stream's flow during the winter season.

Currently, catch basins are located throughout the parking lots that convey stormwater to the Norwalk River. Based upon the proposed construction of Building B and redevelopment of the project Site, stormwater from the building and surrounding areas will continue to be conveyed to the Norwalk River, therefore no anticipated additional stormwater will be conveyed to Stream 1. A stormwater management report has been prepared by VHB and is part of the IWW Application for this project, which contains more detailed information on how the stormwater quality and quantity will be managed. The design of the stormwater management measures is intended to control the stormwater flows and quality as to not impact the Norwalk River or its trout stream habitat.

Required permits from local, state, and federal agencies for these disturbances will be procured prior to the start of construction.

4.2 – Potential Effects of Proposed Activity on Flora

The majority of the vegetation within the stream area is red maple (*Acer rubrum*) and sugar maple (*Acer saccharinum*), northern spice bush (*Lindera benzoin*), and multifloral rose (*Rosa multiflora*). The proposed work would require some vegetation clearing in the upland review

area, including removal of a medium-sized tree. Plantings in the area have been proposed in an effort to restore and enhance the impacted upland review area surrounding the stream. Overall, the proposed Project is anticipated to have negligible impacts on Stream 1. Additionally, there are no proposed impacts on the flora to the Norwalk River is anticipated with this project.

4.3 – Potential Effects of Proposed Activity on Fauna

The proposed work is not anticipated to adversely impact fauna in the area as Stream 1 is not anticipated to provide quality wildlife habitat due to its proximity to residential and commercial development. Foraging material is available; however, due to development the area is not anticipated to act as a host to a sizable population of wildlife.

The proposed work in the upland review area of the Norwalk River will occur in an area that is currently developed with a building and parking spaces. The stormwater management plan intends to control stormwater flows/quality to alleviate impacts to the Norwalk River and species that utilize it. The impact of the Project to fauna is anticipated to be negligible.

References

- Cowardin, L.M., V. Carter, F.C. Golet, E.T. LaRoe (1979). Classification of Wetlands and Deepwater Habitats of the United States. US Government Printing Office. Washington D.C. GPO 024-010-00524-6.103 pp.
- 2. USACOE (1993). The Highway Methodology Workbook Supplement. US Army Corps of Engineers New England Division. NEDEP. 32 pp.
- 3. United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) soil descriptions. Website:

http://soils.usda.gov/technical/classification/osd/index.html).



APPENDIX A

VHB WETLAND AND WATERCOURSES DELINEATION REPORT

(Referenced in Attachment C)



APPENDIX B

WETLAND FUNCTIONS/VALUES EVALUATION FORM

	Wet	Wetland Function-V	'alue	Function-Value Evaluation Form	
Total area of wetlandHuman made? No	Is wet	Is wetland part of a wildlife corridor? <u>No</u>	No	or a "habitat island"? $\frac{No}{L_s}$	Wetland I.D. Stream 1 Latitude Longitude
Adjacent land use Commercial, multi-use building and parking lots	and parkin		adway oi	Distance to nearest roadway or other development 3 ft Pr	by: SJB
Dominant wetland systems present R2UB2F		Contiguous undeveloped buffer zone present No	ped buff		Wetland Impact: Type_Upland review area only - permanentArrea
is the wetland a separate hydraulic system $\frac{2}{3}$ N/A	If	If not, where does the wetland lie in the drainage basin? <u>N/A</u>	in the dr		Evaluation based on:
How many tributaries contribute to the wetland? $\overline{0}$		_Wildlife & vegetation diversi	ty/abunda	list)	Office × Field × Corps manual wetland delineation
Function/Value	Suitability Y / N	ty Rationale (Reference #)*	Principal Function	(s)/Value(s) Con	~
Groundwater Recharge/Discharge	А	4, 7, 10, 15	×	Stream collects rainwater/sheet flow from adjacent ar	Stream collects rainwater/sheet flow from adjacent areas but does not hold it for extended amounts of time.
Floodflow Alteration	Х	9, 11, 13	×	Stream collects rainwater/sheet flow fr	Stream collects rainwater/sheet flow from adjacent areas and conveys offsite.
-Fish and Shellfish Habitat	Ν	8, 17		Stream is intermittent, no fish observed during	h observed during site visits.
Sediment/Toxicant Retention	Z	4		No vegetated wetland is presen	No vegetated wetland is present, therefore retention is minimal.
Nutrient Removal	Z	൭		No vegetated wetland is preser	No vegetated wetland is present, therefore removal is minimal.
Production Export	Х	2, 4		Some vegetation is present along th	Some vegetation is present along the banks, but is not dense or diverse.
Sediment/Shoreline Stabilization	Z			No vegetated wetland is	is present.
👟 Wildlife Habitat	Х	7, 17		West of the stream is a large wooded area that could host wildlife, bu	West of the stream is a large wooded area that could host wildlife, but the site is not anticipated to host wildlife due to its developed nature.
Recreation	Х	10, 11, 12		Adjacent parking lots are currently used by the public for we	Adjacent parking lots are currently used by the public for walking, however the area is not a designated recreation area.
Educational/Scientific Value	N			The area does not hold any signifi	The area does not hold any significant educational or scientific value.
★ Uniqueness/Heritage	N	6		Parking lots are adjacent to the stream, however	Parking lots are adjacent to the stream, however the area is not an established recreational area.
Visual Quality/Aesthetics	N			Stream is hidden by residential/commercial buildings	mmercial buildings and parking lots
ES Endangered Species Habitat	Ν			No NNDB area nearby	
Other					
Notae:				* Refer to backu	* Refer to backup list of numbered considerations.

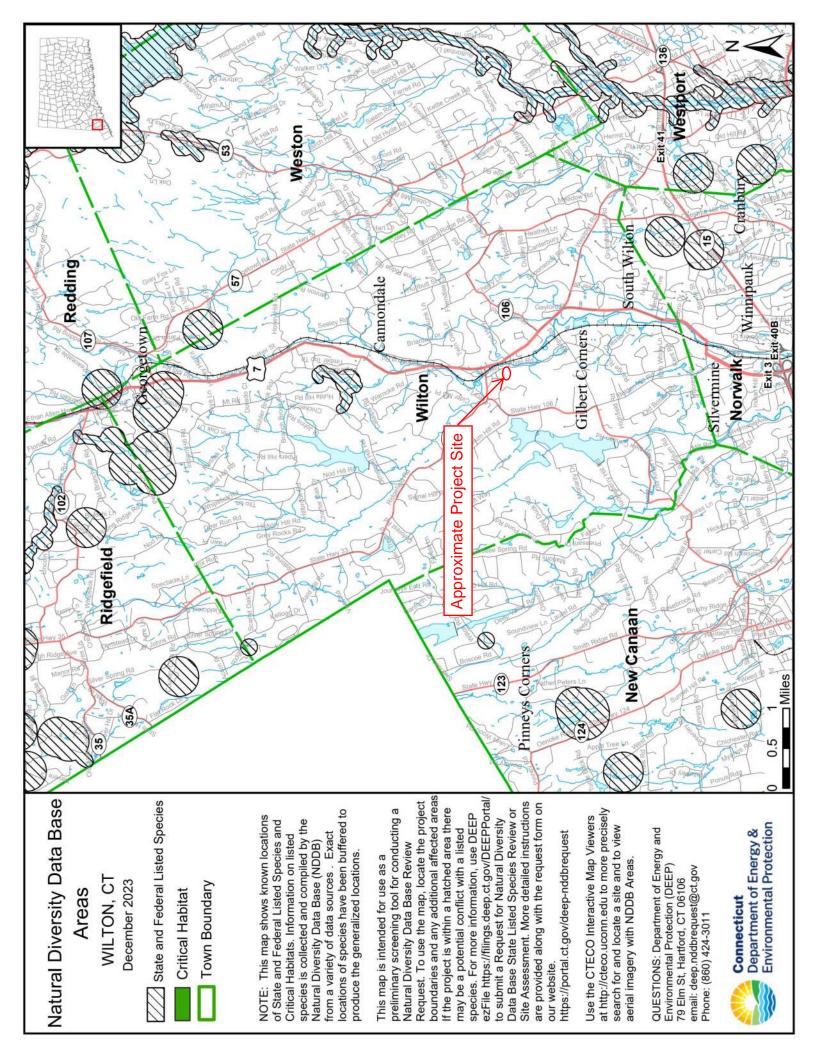
Notes:



APPENDIX C

CT DEEP NDDB MAP

• • •



ATTACHMENT E

VHB STORMWATER MANAGEMENT

REPORT

(Under separate cover)

ATTACHMENT F

VHB SOIL AND GROUNDWATER MANAGEMENT PLAN SUMMARY

ang kanala sa kanala sa
and the second
and a second second Second second
and the second
and the second
a faith and a star



April 23, 2024

Ref: 20849.00

Nicholas Brown 500 North Broadway, Suite 201 Jericho, New York 11753

Re: Soil and Groundwater Management Recommendations Memo

Dear Mr. Brown:

Vanasse Hangen Brustlin, Inc. (VHB) has prepared this Soil and Groundwater Management Recommendations Letter for Wilton Campus 1691, LLC (Client) to highlight best practices for soil and groundwater management on-site during redevelopment activities at 11, 15, and 21 River, the Wilton Campus (site). The client has a proposed redevelopment plan that includes various construction activities such as building demolition, building construction, grading, utility trenching, paving, and other activities. Specific activities that disturb subsurface soils and/or groundwater would benefit from a soil and groundwater management plan.

Background Information

The site was enrolled into the Connecticut Department of Energy and Environmental Protection (CTDEEP) Property Transfer Program in March 2013 act due to previous on-site activities that qualified the site as an "establishment". In April 2020, an Interim LEP Verification was completed for the site and in July 2021, a Final LEP Verification was completed by GZA GeoEnvironmental, Inc. (GZA). On October 5, 2021, CTDEEP issued a Letter of No-Audit for the verification.

During previous investigations by GZA, the site was identified in a Class GA groundwater area with groundwater fluctuating seasonally between 6 to 12 feet below grade at the site. Groundwater investigations identified impacts that included low concentrations of certain pesticides . Soil investigations identified impacts that included low concentrations of ETPH, VOCs, PAHs, metals, and pesticides.

GZA performed soil excavations to specific areas on-site where contaminant concentrations exceeded the applicable CTDEEP Remediation Standard Regulations (RSR) criteria. Confirmation soil samples collected confirmed that the remaining contaminant concentrations in soils were compliant with the RSR criteria. GZA recommended natural attenuation groundwater monitoring be performed to demonstrate RSR compliance for groundwater overtime.

Soil and Groundwater Management Recommendations

Based on the information contained in the GZA reports, there are areas of soil and groundwater contamination that remain at the site may be disturbed during construction activities proposed by the Client. Therefore, VHB recommends that a Soil and Groundwater Management Plan (SGWMP) be prepared and implemented in conjunction with construction activities. The SGWMP should be specific to the site and implement best management practices including, but not limited to:

Nicholas Brown Ref: 20849.00 April 23, 2024 Page 2



- > All soil stockpiles and equipment/materials storage areas are recommended be located outside of floodplain areas. Temporary stockpiles should be constructed with 6 mil polyethylene plastic placed on the ground and any soil stockpile should be covered with 6 mil polyethylene plastic.
- > If grossly contaminated soils are identified via odor or/and sheen/appearance, soil segregation may be recommended.
- > If excess soils generated are slated for off-site disposal, proper waste characterization sampling should be conducted to determine potential disposal requirements.
- > Any on-site reuse of soils should conducted in such a manner that placement of soils is not in a floodplain, subject to erosion, and in some cases cannot be placed below the groundwater table or used as surface cover based on contaminant concentrations.
- If groundwater dewatering is needed during construction activities, a groundwater discharge permit would likely needed with groundwater sampling to determine discharge is suitable for either discharge to an existing sewer/storm drain or to nearby surface water.
- > A site-specific health and safety plan is recommended prior to construction activities to promote worker safety.
- > Dust monitoring and/or dust suppression controls maybe required during demolition, excavation, or construction activities.
- > Erosion and sediment controls will be required to mitigate the effects of run-on and run-off from the site.
- > Processes to follow if unknown environmental issues are encountered.

Conclusions

Documented soil and groundwater contamination exists at the site. The remaining impacted soil is in compliance with CTDEEP RSRs but due to contaminant concentrations will require proper management and/or off-site disposal during construction activities. Groundwater contains pesticide concentrations that would require proper management and disposal if dewatering is needed during excavation activities for the project.

Based on this information, VHB recommends a site specific SGWMP be prepared for the project that contains (at a minimum) the recommended activities outlined above.

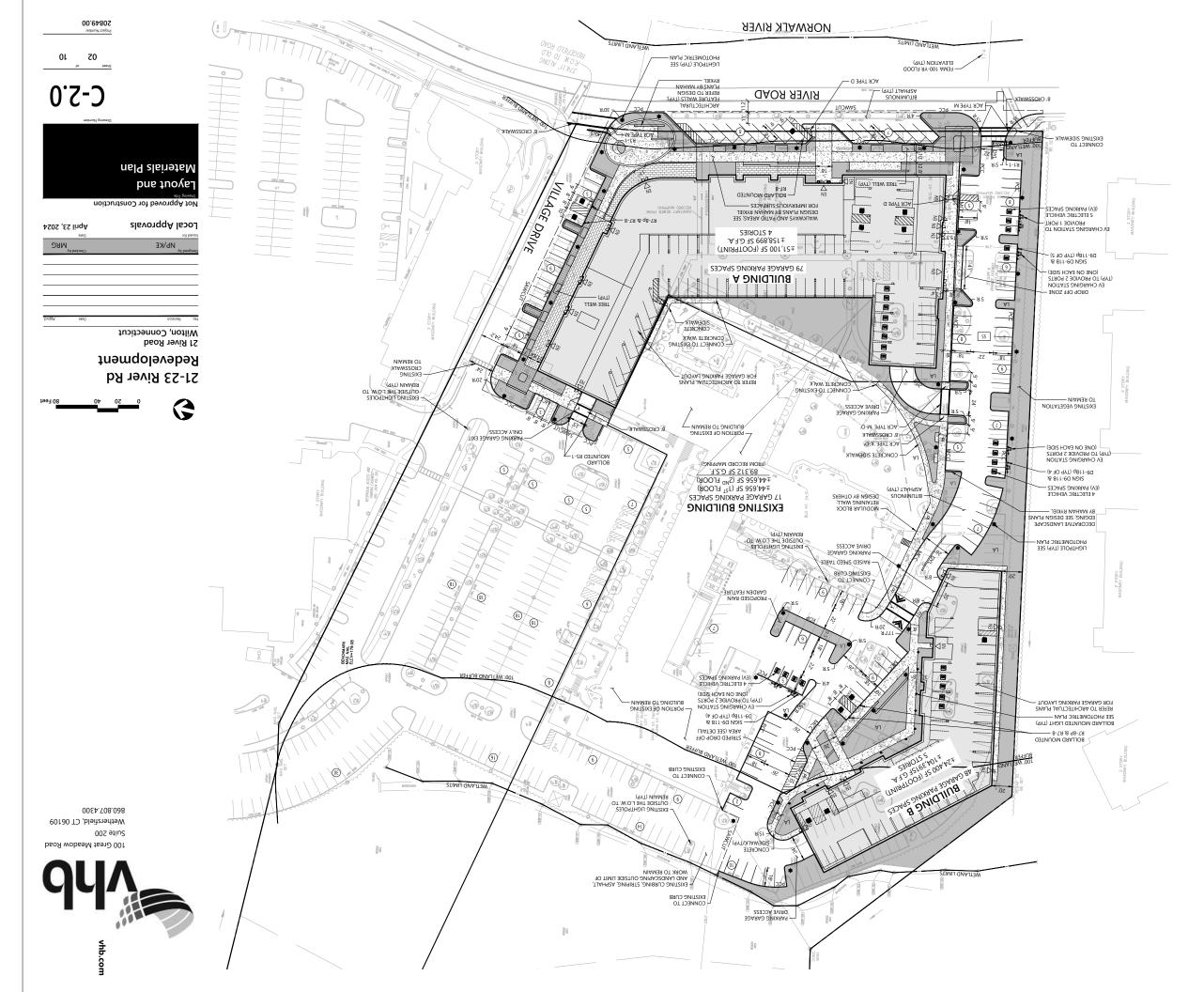
If you have any questions, please contact Amy Vaillancourt at <u>availlancourt@vhb.com</u> or at 860-807-4327.

Sincerely,

Any Vuillancent

Amy Vaillancourt, LEP Director of Environmental Services

ATTACHMENT G ALTERNATE VERSIONS









Parking

•

•

•

•

South Building

- •
- JinU\Z.1 :is9A

55 Covered Stalls

- Office/Retail: Prior ratio
- AZ X1/E @ baniatniam

2.3K SF Retail •

63 Units

- 6.5K SF Amenity/Lobby •
- - - 66 Covered Stalls
 - - 95 Units

 - •

 - gnibling tsea
 - 189K sf to 117K SF •
 - Demolish 72K SF • :list9A\90iffO

(λεβείον τ) **REDEVELOPMENT PLAN WILTON CAMPUS**



e3 Units South Building

....



Parking

•

- JinU\Z.1 :is9A
- Office/Retail: Prior ratio •
- TK ST @ benietniem

2.3K SF Retail • 6.5K SF Amenity/Lobby

95 Units

South Building

•

•

•

Baibling fast

- 63 Units •
- 55 Covered Stalls

 - •

6

- (VERSION 2)
- 189K sf to 117K SF

66 Covered Stalls

- •
- Demolish 72K SF •
- :list9A\92iffO
- **REDEVELOPMENT PLAN WILTON CAMPUS**



e3 Units gnibling dtuo2

....



Parking

•

•

•

•

South Building

- JinU\Z.1 :is9A

55 Covered Stalls

- Office/Retail: Prior ratio
- TK ST @ benietniem

2.3K SF Retail •

stinU 88

- 6.5K SF Amenity/Lobby •
 - - 66 Covered Stalls
 - 92 Units
 - •
 - Bnibling fzb3
 - 189K sf to 117K SF •
 - Demolish 72K SF • :listəA\əɔiffO

(VERSION 3) **REDEVELOPMENT PLAN WILTON CAMPUS**



stinU 88 gnibling dtuo2

00

ATTACHMENT H WILTON CAMPUS 1691 LLC LETTER OF AUTHORIZATION TO VHB

Wilton Campus 1691, LLC

500 North Broadway, Suite 201

Jericho, NY 11753

April 11, 2024

Inland Wetlands Commission Wilton Town Hall 238 Danbury Road Wilton, CT 06897

Dear Chairman Lee and Members of the Inland Wetlands Commission,

I, Nicholas Brown, Vice president of Development for Kimco Realty, authorized vice president of Wilton Campus 1691, LLC, authorize VHB, Inc. to act as agent on behalf of Wilton Campus 1691, LLC during the Town of Wilton Inland Wetlands Commission entitlement process.

Nicholas Brown

ATTACHMENT I

ABUTTERS LIST

Map Block Lot	73-25-3		
Property Address	25 River Road		
Owner	Avalonbay Communities Inc		
Co-Owner			
Mailing Address	P.O. Box 4697		
	Logan, UT 84323		

Map Block Lot	87-4
Property Address	76 Graenest Ridge Road
Owner	Bridge Jordan E & Jamie N
Co-Owner	
Mailing Address	76 Graenest Ridge Road
	Wilton, CT 06897

Map Block Lot	87-3		
Property Address	66 Graenest Ridge Road		
Owner	Stenzler Michael E & Caroline P		
Co-Owner			
Mailing Address	66 Graenest Ridge Road		
	Wilton, CT 06897		

Map Block Lot	87-2
Property Address	58 Graenest Ridge Road
Owner	Boland Amy L & Andrew E
Co-Owner	
Mailing Address	58 Graenest Ridge Road
	Wilton, CT 06897

Map Block Lot	73-48
Property Address	40 Graenest Ridge Road
Owner	Zheng Min &
Co-Owner	Ye Liyun
Mailing Address	40 Graenest Ridge Road
	Wilton, CT 06897

Map Block Lot	73-25
Property Address	5 River Road
Owner	Wilton River Park 1688 LLC
Co-Owner	C/O KRC Acquisition Corp
Mailing Address	500 North Broadway, Suite 201
	Jericho, NY 11753

Site Plans

Issued for Date Issued Latest Issue

Local Approvals April 23, 2024 April 23, 2024

Proposed ReDevelopment

21-23 River Road Wilton, Connecticut



Owner

Wilton Campus 1691, LLC 500 North Broadway, Suite 201 Jericho, NY 11753

Applicant

Wilton Campus 1691, LLC 500 North Broadway, Suite 201 Jericho, NY 11753

Map Block Lot: Map 73/ Lots 25.1 & 25.4



Sheet Index		Reference Drawings			
No.	Drawing Title	Latest Issue	No.	Drawing Title	Latest Issu
C-1.0	Legend, Abbreviations and General Notes	April 23, 2024	Sheets 1-3 of 3	Boundary & Topographic Survey	October 4, 202
C-2.0	Layout and Materials Plan	April 23, 2024	Lighting Plans		
C-2.1	Overall Parking Plan	April 23, 2024			
C-2.2	Bulk Zoning Summary Plan	April 23, 2024	SL200	Photometric Plan	April 16, 20
2-3.0	Grading and Drainage Plan	April 23, 2024	SL201	Proposed Landscape Lighting Plan	April 16, 20
2-4.0	Utility Plan	April 23, 2024	SL202	Proposed Building Mount Plan (Level 1)	April 16, 20
2-5.0	Erosion and Sedimentation Control Plan	April 23, 2024	SL203	Proposed Building Mount Plan (Level 2)	April 16, 20
			SL204	Proposed Building Mount Plan (Level 3)	April 16, 20
-6.0	Site Details 1	April 23, 2024	SL205	Proposed Building Mount Plan (Level 4)	April 16, 20
-6.1	Site Details 2	April 23, 2024	SL206	Proposed Building Mount Plan (Level 5)	April 16, 20
-6.2	Site Details 3	April 23, 2024	SL207	Proposed Schedules	April 16, 20
-6.3	Site Details 4	April 23, 2024	Landscape Plan	S	
			L1.00	Overall Site Rendering	April 23, 20
			L1.01	Building A Rendering Plan	April 23, 20
			L1.02	Building B Rendering Plan	April 23, 20
			L2.00	Overall Planting Plan	April 23, 20
			L2.01	Building A Planting Plan	April 23, 20
			L2.02	Building B Planting Plan	April 23, 20
					•

L2.03

L2.04



100 Great Meadow Road Suite 200 Wethersfield, CT 06109 860.807.4300

Plant Schedule

Mitigation Planting Plan

April 23, 2024 April 23, 2024 April 23, 2024

Survey:

Valley Land Services, LLC Jack Shoemaker 4383 Hecktown Road Behlehem, PA 18020 Ph: 610.365.2907

Geotechnical:

GEI Matt Glunt, PE 455 Winding Brook Dr Suite 201 Glastonbury, CT 06033 Ph: 860.368.5301

Site Lighting:

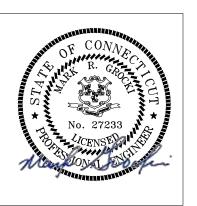
On-Site Lighting Marshall Tromborg 111 Highway 25 North Suite 201 Buffalo, MN 55313 Ph: 763.682.7114

Architect:

Cube3 Ricky Long 160 State St Floor 6 Boston, MA 02109 Ph: 617.896.6676

Landscape Architect:

Mahan Rykiel Assoc. Matt Renauld 3300 Clipper Mill Rd Suite 200 Baltimore, MD 21211 Ph: 410.900.1634



Legend

Exist.	Prop.		Exist.	Prop.	
		PROPERTY LINE			CONCRETE
		PROJECT LIMIT LINE	<u> </u>		HEAVY DUTY PAVEMENT
					BUILDINGS
		RIGHT-OF-WAY/PROPERTY LINE			
		EASEMENT			RIPRAP
·		BUILDING SETBACK			CONSTRUCTION EXIT
10+00	10+00	PARKING SETBACK	27.35 TC×	27.35 TC ×	TOP OF CURB ELEVATION
10+00	10+00	BASELINE	26.85 BC×	26.85 BC×	
		CONSTRUCTION LAYOUT	20.03 BC X	20.03 BC X	BOTTOM OF CURB ELEVATION
		ZONING LINE	132.75 ×	132.75 ×	SPOT ELEVATION
		TOWN LINE	45.0 TW 38.5 BW	45.0 TW 38.5 BW	TOP & BOTTOM OF WALL ELEVATION
			- 🔶	\bullet	BORING LOCATION
	·	LIMIT OF DISTURBANCE			TEST PIT LOCATION
∆		WETLAND LINE WITH FLAG	€ ^{MW}	^{MW}	MONITORING WELL
	·	FLOODPLAIN			
			UD	UD	UNDERDRAIN
BLSF		BORDERING LAND SUBJECT TO FLOODING	12"D	12″D→	DRAIN
BZ		WETLAND BUFFER ZONE		6″RD►	ROOF DRAIN
NDZ		NO DISTURB ZONE	1 <u>2</u> "S	1 <u>2"</u> S	SEWER
			FM	FM	FORCE MAIN
200'RA		200' RIVERFRONT AREA	OLIW		
		GRAVEL ROAD	- OHW	OHW	OVERHEAD WIRE
EOP			6"W	——6"W——	WATER
	BB	EDGE OF PAVEMENT	4"FP	4"FP	FIRE PROTECTION
<u></u>		BITUMINOUS BERM		2"DW	DOMESTIC WATER
BC	BC	BITUMINOUS CURB	3"G	G	GAS
CC	<u> </u>	CONCRETE CURB	——————————————————————————————————————	———E———	ELECTRIC
	CG	CURB AND GUTTER	STM	STM	STEAM
CC	ECC	EXTRUDED CONCRETE CURB	T	T	TELEPHONE
CC	MCC	MONOLITHIC CONCRETE CURB	FA	FA	
CC	PCC				FIRE ALARM
		PRECAST CONC. CURB	CATV	CATV	CABLE TV
<u>SGE</u>	SGE	SLOPED GRAN. EDGING			CATCH BASIN CONCENTRIC
VGC	VGC	VERT. GRAN. CURB			CATCH BASIN ECCENTRIC
		LIMIT OF CURB TYPE		<u> </u>	
		SAWCUT			DOUBLE CATCH BASIN CONCENTRIC
	.		_		DOUBLE CATCH BASIN ECCENTRIC
		BUILDING		===	GUTTER INLET
		BUILDING ENTRANCE	D	$igodoldsymbol{igo$	DRAIN MANHOLE CONCENTRIC
	Ξ		D	\odot	DRAIN MANHOLE ECCENTRIC
		LOADING DOCK	=TD=		TRENCH DRAIN
۰	•	BOLLARD	L	Ľ	PLUG OR CAP
D	D	DUMPSTER PAD	co	co	CLEANOUT
-0-	-	SIGN			
	T	DOUBLE SIGN			FLARED END SECTION
				\sim	HEADWALL
<u> </u>	I	STEEL GUARDRAIL	S	ullet	SEWER MANHOLE CONCENTRIC
	.	WOOD GUARDRAIL	S	$\overline{\bullet}$	SEWER MANHOLE ECCENTRIC
				-	Sewer MANHOLE ECCENTRIC
		PATH	CS	© ©	CURB STOP & BOX
\sim	\sim	TREE LINE	WV	₩V ●	WATER VALVE & BOX
			TSV	TSV	TAPPING SLEEVE, VALVE & BOX
<u> </u>	-x x	WIRE FENCE		•> •	
-00	• •	FENCE	HYD	HYD	FIRE DEPARTMENT CONNECTION
-00		STOCKADE FENCE	«©» WM	© _WM	FIRE HYDRANT
	$\infty \infty \infty \infty$	STONE WALL	•	⊡ PIV	WATER METER
		RETAINING WALL	PIV	e الا	POST INDICATOR VALVE
		STREAM / POND / WATER COURSE	\bigcirc	\bigcirc	WATER WELL
		DETENTION BASIN	GG	GG	GAS GATE
	• •]• •]• •]• •]• •]• •]	HAY BALES	GM	O GM ⊡	
					GAS METER
X	X		E	● ^{EMH}	ELECTRIC MANHOLE
<	< ·	SILT SOCK / STRAW WATTLE	EM 	EM	ELECTRIC METER
4	4	MINOR CONTOUR	¢	*	
— — 20— —	20	MAJOR CONTOUR			LIGHT POLE
	_~		Ū	● ^{™H}	TELEPHONE MANHOLE
(10)	(10)	PARKING COUNT	T	T	TRANSFORMER PAD
	(C10)	COMPACT PARKING STALLS		—	
DYL	DYL		-0-	•	UTILITY POLE
	SL	DOUBLE YELLOW LINE	0-	•-	GUY POLE
SL	JL	STOP LINE	Ţ	Ť	GUY WIRE & ANCHOR
		CROSSWALK	HH ⊡	HH ⊡	HAND HOLE
		ACCESSIBLE CURB RAMP	PB ⊡	PB ⊡	
/ N			L*1	Ľ	PULL BOX
A_A E	ٹے	ACCESSIBLE PARKING			

Abbreviations

C	1
Genera	
ABAN	ABANDON
ACR	ACCESSIBLE CURB RAMP
ADJ	ADJUST
APPROX	APPROXIMATE
BIT	BITUMINOUS
BS	BOTTOM OF SLOPE
BWLL	BROKEN WHITE LANE LINE
CONC	CONCRETE
DYCL	DOUBLE YELLOW CENTER LINE
EL	ELEVATION
ELEV	ELEVATION
EX	EXISTING
FDN	FOUNDATION
FFE	FIRST FLOOR ELEVATION
GRAN	GRANITE
GTD	GRADE TO DRAIN
LA	LANDSCAPE AREA
LOD	
MAX	MAXIMUM
MIN	MAXIMUM
NIC	NOT IN CONTRACT
NTS	
PERF	PERFORATED
PROP	PROPOSED
REM	REMOVE
RET	RETAIN
R&D	REMOVE AND DISPOSE
R&R	REMOVE AND RESET
SWEL	SOLID WHITE EDGE LINE
SWLL	SOLID WHITE LANE LINE
TS	TOP OF SLOPE
TYP	TYPICAL
Utility	
СВ	CATCH BASIN
СМР	CORRUGATED METAL PIPE
СМР СО	CORRUGATED METAL PIPE
СО	CLEANOUT
CO DCB	CLEANOUT DOUBLE CATCH BASIN
CO DCB DMH	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE
CO DCB DMH CIP	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE
CO DCB DMH CIP COND	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT
CO DCB DMH CIP COND DIP	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE
CO DCB DMH CIP COND DIP FES	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION
CO DCB DMH CIP COND DIP FES FM	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN
CO DCB DMH CIP COND DIP FES FM F&G	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE
CO DCB DMH CIP COND DIP FES FM F&G F&C	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND COVER
CO DCB DMH CIP COND DIP FES FM F&G F&C GI	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND COVER GUTTER INLET
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH HW	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH HW HW	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH HW	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH HW HW	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL
CO DCB DMH CIP COND DIP FES FM F&G F&C GI GT HDPE HH HW HYD INV	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION
 CO DCB DMH CIP COND DIP FES FM F&G F&G GI GT HDPE HH HW HYD INV I= 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION
CO DCB DMH CIP COND DIP FES FM F&C GI 6T HDPE HH HW HYD INV I= LP	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION LIGHT POLE
 CO DCB DMH CIP COND DIP FES FM F&C GI GT HDPE HH HW HYD INV I= LP MES 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION LIGHT POLE METAL END SECTION
 CO DCB DMH CIP COND DIP FES FM F&G GI GT HDPE HH HW HYD INV I= LP MES PIV 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION LIGHT POLE METAL END SECTION POST INDICATOR VALVE
 CO DCB DMH CIP COND DIP FES FM F&C GI GT HDPE HH HW HYD INV I= LP MES PIV PWW 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE RRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE
 CO DCB DMH CIP COND DIP FES FM F&C GI GT HDPE HH HW HYD INV I LP MES PIV PWW PVC 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE RRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE
 CO DCB DMH CIP COND DIP FES FM F&C GI GT HDPE HH HW HYD INV II LP MES PIV PWW PVC RCP 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION IGHT POLE METAL END SECTION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE REINFORCED CONCRETE PIPE
 CO DCB DMH CIP COND DIP FES FM F&G GI GT HDPE HH HW HYD INV I LP MES PIV PWW PVC RCP R= 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION LIGHT POLE METAL END SECTION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE REINFORCED CONCRETE PIPE
 CO DCB DMH CIP COND DIP F8C FM F&C GI F&C GI HDPE HH HV HDPE INV I INV I INV I INV I RES PIVC RCP RIM= 	CLEANOUT DOUBLE CATCH BASIN DRAIN MANHOLE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FORCE MAIN FRAME AND GRATE RAME AND GRATE GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION INVERT ELEVATION IGHT POLE METAL END SECTION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE REINFORCED CONCRETE PIPE
 CO DCB DMH CIP COND DIP F8C FM F&C GI F&C GI HDPE HH HV HDPE HH HW HDPE INV I INV I INV I RES PIV PWW PVC RCP R RIM= SMH 	CLEANOUTDOUBLE CATCH BASINDRAIN MANHOLECAST IRON PIPECONDUITDUCTILE IRON PIPEFLARED END SECTIONFORCE MAINFRAME AND GRATEFRAME AND COVERGUTTER INLETGREASE TRAPHIGH DENSITY POLYETHYLENE PIPEHANDHOLEHEADWALLHYDRANTINVERT ELEVATIONINVERT ELEVATIONPOST INDICATOR VALVEPAVED WATER WAYPOLYVINYLCHLORIDE PIPERIINFORCED CONCRETE PIPERIM ELEVATIONRIM ELEV
 CO DCB DMH CIP COND DIP F8C FM F&C GI F&C GI F&C GI HDPE HH HV HDPE HH HV HDPE INV I INV I I V PWW PVC RCP R RIM SMH TSV 	CLEANOUT DOUBLE CATCH BASIN CATCH BASIN CASI IRON PIPE CAST IRON PIPE CONDUIT DUCTILE IRON PIPE FLARED END SECTION FRAME AND GRATE FRAME AND GRATE FRAME AND COVER GUTTER INLET GREASE TRAP HIGH DENSITY POLYETHYLENE PIPE HANDHOLE HEADWALL HYDRANT INVERT ELEVATION INVERT ELEVATION LIGHT POLE METAL END SECTION POST INDICATOR VALVE PAVED WATER WAY POLYVINYLCHLORIDE PIPE RIINFORCED CONCRETE PIPE

Notes

	neral	Lay	out and Ma
1.	CONTRACTOR SHALL NOTIFY "CALL BEFORE YOU DIG, INC." (811 OR 1-800-922-4455) AT LEAST 72 HOURS BEFORE EXCAVATING.	1.	DIMENSIONS AF
2.	CONTRACTOR SHALL BE RESPONSIBLE FOR SITE SECURITY AND JOB SAFETY. CONSTRUCTION ACTIVITIES SHALL BE IN ACCORDANCE WITH OSHA STANDARDS AND LOCAL REQUIREMENTS.		CURB RADII ARE
3.	ACCESSIBLE ROUTES, PARKING SPACES, RAMPS, SIDEWALKS AND WALKWAYS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE FEDERAL AMERICANS WITH DISABILITIES ACT AND WITH STATE AND LOCAL LAWS AND REGULATIONS (WHICHEVER ARE MORE STRINGENT).		CURBING SHALL PLANS. SEE ARCHITECTU
4.	AREAS DISTURBED DURING CONSTRUCTION AND NOT RESTORED WITH IMPERVIOUS SURFACES (BUILDINGS, PAVEMENTS, WALKS, ETC.) SHALL RECEIVE 6 INCHES LOAM AND SEED.	-	THE BUILDING, I PENETRATIONS,
5.	WITHIN THE LIMITS OF THE BUILDING FOOTPRINT, THE SITE CONTRACTOR SHALL PERFORM EARTHWORK OPERATIONS REQUIRED UP TO SUBGRADE ELEVATIONS.	5.	PROPOSED BOU CONSTRUCTION
6.	WORK WITHIN THE LOCAL RIGHTS-OF-WAY SHALL CONFORM TO LOCAL MUNICIPAL STANDARDS. WORK WITHIN STATE RIGHTS-OF-WAY SHALL CONFORM TO THE LATEST EDITION OF THE STATE HIGHWAY DEPARTMENTS STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES.	6.	PRIOR TO START INTERFACE WITH DRAINAGE OUTI
7.	UPON AWARD OF CONTRACT, CONTRACTOR SHALL MAKE NECESSARY CONSTRUCTION NOTIFICATIONS AND APPLY FOR AND OBTAIN NECESSARY PERMITS, PAY FEES, AND POST BONDS ASSOCIATED WITH	De	molition
	THE WORK INDICATED ON THE DRAWINGS, IN THE SPECIFICATIONS, AND FOST BONDS ASSOCIATED WITH THE WORK INDICATED ON THE DRAWINGS, IN THE SPECIFICATIONS, AND IN THE CONTRACT DOCUMENTS. DO NOT CLOSE OR OBSTRUCT ROADWAYS, SIDEWALKS, AND FIRE HYDRANTS, WITHOUT APPROPRIATE PERMITS.	1.	CONTRACTOR S LIMIT OF WORK POLES, SIGNS, E EXISTING UTILITI
8.	TRAFFIC SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES.		FEET BEYOND TH SPECIFICALLY NO
9.	AREAS OUTSIDE THE LIMITS OF PROPOSED WORK DISTURBED BY THE CONTRACTOR'S OPERATIONS SHALL BE RESTORED BY THE CONTRACTOR TO THEIR ORIGINAL CONDITION AT THE CONTRACTOR'S EXPENSE.	2.	EXISTING UTILITI LOCAL, STATE AI CONTRACTOR S REPRESENTATIVI
10.	IN THE EVENT THAT SUSPECTED CONTAMINATED SOIL, GROUNDWATER, AND OTHER MEDIA ARE ENCOUNTERED DURING EXCAVATION AND CONSTRUCTION ACTIVITIES BASED ON VISUAL, OLFACTORY, OR OTHER EVIDENCE, THE CONTRACTOR SHALL STOP WORK IN THE VICINITY OF THE SUSPECT MATERIAL TO AVOID FURTHER SPREADING OF THE MATERIAL, AND SHALL NOTIFY THE OWNER	3.	CONTRACTOR S STATE AND LOC
11	IMMEDIATELY SO THAT THE APPROPRIATE TESTING AND SUBSEQUENT ACTION CAN BE TAKEN.	4	THE DEMOLITIO BIDDING AND CO OF DEMOLITION
	RESPONSIBLE FOR CLEANUP, REPAIRS AND CORRECTIVE ACTION IF SUCH OCCURS.		DEMOLITION BE CLAIMS AND SE
12.	DAMAGE RESULTING FROM CONSTRUCTION LOADS SHALL BE REPAIRED BY THE CONTRACTOR AT NO ADDITIONAL COST TO OWNER.		LATENT SITE CO WORK.
13.	CONTRACTOR SHALL CONTROL STORMWATER RUNOFF DURING CONSTRUCTION TO PREVENT ADVERSE IMPACTS TO OFF SITE AREAS, AND SHALL BE RESPONSIBLE TO REPAIR RESULTING DAMAGES, IF ANY, AT NO COST TO OWNER.	5.	UNLESS OTHERV HAS NOT PREPA DISCOVERY, REM POLLUTANTS AT
14.	THIS PROJECT DISTURBS MORE THAN FIVE ACRES OF LAND AND REQUIRES A CTDEEP PERMIT FOR THE GENERAL PERMIT OF DISCHARGE OF STORMWATER AND DEWATERING WASTEWATER FROM CONSTRUCTION ACTIVITIES. THE CONTRACTOR IS RESPONSIBLE TO FOLLOW THE STORMWATER POLLUTION PREVENTION PLAN (SWPPP) AND REQUIREMENTS AS OUTLINED IN THE PERMIT.		LOSS, DAMAGE, MATERIAL AND CLAIMS MADE II ADMINISTRATIV INVOLVING THE
Uti	lities		OR OTHER HAZA
1.	THE LOCATIONS, SIZES, AND TYPES OF EXISTING UTILITIES ARE SHOWN AS AN APPROXIMATE REPRESENTATION ONLY. THE OWNER OR ITS REPRESENTATIVE(S) HAVE NOT INDEPENDENTLY VERIFIED THIS INFORMATION AS SHOWN ON THE PLANS. THE UTILITY INFORMATION SHOWN DOES NOT GUARANTEE THE ACTUAL EXISTENCE, SERVICEABILITY, OR OTHER DATA CONCERNING THE UTILITIES, NOR DOES IT GUARANTEE AGAINST THE POSSIBILITY THAT ADDITIONAL UTILITIES MAY BE PRESENT		PRIOR TO START AGENCIES AND IDENTIFIED IN FE
	THAT ARE NOT SHOWN ON THE PLANS. PRIOR TO ORDERING MATERIALS AND BEGINNING CONSTRUCTION, THE CONTRACTOR SHALL VERIFY AND DETERMINE THE EXACT LOCATIONS, SIZES, AND ELEVATIONS OF THE POINTS OF CONNECTIONS TO EXISTING UTILITIES AND, SHALL CONFIRM THAT THERE ARE NO INTERFERENCES WITH EXISTING UTILITIES AND THE PROPOSED UTILITY ROUTES, INCLUDING ROUTES WITHIN THE PUBLIC RIGHTS OF WAY.	2.	CONTRACTOR S (MINIMUM) OR A CONTRACTOR S OF INSPECTION. ENCUMBER OTH
2.	WHERE AN EXISTING UTILITY IS FOUND TO CONFLICT WITH THE PROPOSED WORK, OR EXISTING CONDITIONS DIFFER FROM THOSE SHOWN SUCH THAT THE WORK CANNOT BE COMPLETED AS INTENDED, THE LOCATION, ELEVATION, AND SIZE OF THE UTILITY SHALL BE ACCURATELY DETERMINED WITHOUT DELAY BY THE CONTRACTOR, AND THE INFORMATION FURNISHED IN WRITING TO THE OWNER'S REPRESENTATIVE FOR THE RESOLUTION OF THE CONFLICT AND CONTRACTOR'S FAILURE TO NOTIFY PRIOR TO PERFORMING ADDITIONAL WORK RELEASES OWNER FROM OBLIGATIONS FOR		CONTRACTOR S SEDIMENTATION SEDIMENTATION
3.	ADDITIONAL PAYMENTS WHICH OTHERWISE MAY BE WARRANTED TO RESOLVE THE CONFLICT. SET CATCH BASIN RIMS, AND INVERTS OF SEWERS, DRAINS, AND DITCHES IN ACCORDANCE WITH	4.	EXPOSED FOR A TO PREVENT ERG
4	ELEVATIONS ON THE GRADING AND UTILITY PLANS.	5.	UPON COMPLET
4.	RIM ELEVATIONS FOR DRAIN AND SEWER MANHOLES, WATER VALVE COVERS, GAS GATES, ELECTRIC AND TELEPHONE PULL BOXES, AND MANHOLES, AND OTHER SUCH ITEMS, ARE APPROXIMATE AND SHALL BE SET/RESET AS FOLLOWS:	Exi	AND DEBRIS FRO
	A. PAVEMENTS AND CONCRETE SURFACES: FLUSH B. ALL SURFACES ALONG ACCESSIBLE ROUTES: FLUSH	1.	BASE PLAN: THE
	C. LANDSCAPE, LOAM AND SEED, AND OTHER EARTH SURFACE AREAS: ONE INCH ABOVE		PHYSICAL FEATU VALLEY LAND SE
5.	SURROUNDING AREA AND TAPER EARTH TO THE RIM ELEVATION. THE LOCATION, SIZE, DEPTH, AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE INSTALLED ACCORDING TO THE REQUIREMENTS PROVIDED BY, AND APPROVED BY,		A. DELINEA ON SEPT 2023.
	THE RESPECTIVE UTILITY COMPANY (GAS, TELEPHONE, ELECTRIC, FIRE ALARM, ETC.). FINAL DESIGN LOADS AND LOCATIONS TO BE COORDINATED WITH OWNER AND ARCHITECT.		B. FLAGS M
6.	CONTRACTOR SHALL MAKE ARRANGEMENTS FOR AND SHALL BE RESPONSIBLE FOR PAYING FEES FOR POLE RELOCATION AND FOR THE ALTERATION AND ADJUSTMENT OF GAS, ELECTRIC, TELEPHONE, FIRE ALARM, AND ANY OTHER PRIVATE UTILITIES, WHETHER WORK IS PERFORMED BY CONTRACTOR OR BY THE UTILITIES COMPANY.	2. 3.	TOPOGRAPHY: GEOTECHNICAL OBTAINED BY G
7.	UTILITY PIPE MATERIALS SHALL BE AS FOLLOWS, UNLESS OTHERWISE NOTED ON THE PLAN:	Do	cument Use
	A. WATER PIPES SHALL BE DUCTILE IRON, CLASS 52, MANUFACTURED AND INSTALLED IN ACCORDANCE WITH AWWA C151, AWWA C111, AWWA C104, AND AWWA C600, LATEST REVISIONS FOR GREATER THAN 2 INCH DIAMETER AND TYPE K COPPER MANUFACTURED AND INSTALLED IN CONFORMANCE WITH ASTM 888, IN ACCORDANCE WITH AWWA C800, LATEST REVISION FOR 2 INCH DIAMETER AND LESS.	1.	THESE PLANS AI SERVICE, AND SI WHICH IT WAS (USE, REUSE, MO DOCUMENT SHA
	B. SANITARY SEWER PIPES SHALL BE POLYVINYL CHLORIDE (PVC) SDR 35 SEWER PIPE	2.	CONTRACTOR S
	C. STORM DRAINAGE PIPES SHALL BE HIGH DENSITY POLYETHYLENE (HDPE) SMOOTH INTERIOR.		DATA FILES THA FEATURES IN AC SUPPLIED AS PA
8.	CONTRACTOR SHALL COORDINATE WITH ELECTRICAL CONTRACTOR AND SHALL FURNISH EXCAVATION, INSTALLATION, AND BACKFILL OF ELECTRICAL FURNISHED SITEWORK RELATED ITEMS SUCH AS PULL BOXES, CONDUITS, DUCT BANKS, LIGHT POLE BASES, AND CONCRETE PADS. SITE CONTRACTOR SHALL FURNISH CONCRETE ENCASEMENT OF DUCT BANKS IF REQUIRED BY THE UTILITY COMPANY AND AS INDICATED ON THE DRAWINGS.	3.	SYMBOLS AND I NECESSARILY SC CONTRACTOR S DRAWINGS AND
9.	CONTRACTOR SHALL EXCAVATE AND BACKFILL TRENCHES FOR GAS IN ACCORDANCE WITH GAS COMPANY'S REQUIREMENTS.		FEATURES.
10.	ALL DRAINAGE AND SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN.) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS AND LOCAL MUNICIPAL STANDARDS. FOR MANHOLES THAT ARE 20 FEET IN DEPTH AND GREATER, THE MINIMUM		

Layout and Materials

NSIONS ARE FROM THE FACE OF CURB, FACE OF BUILDING, FACE OF WALL, AND CENTER LINE OF MENT MARKINGS, UNLESS OTHERWISE NOTED.

3 RADII ARE 3 FEET UNLESS OTHERWISE NOTED.

BING SHALL BE CONCRETE CURB (CC) WITHIN THE SITE UNLESS OTHERWISE INDICATED ON THE

RCHITECTURAL DRAWINGS FOR EXACT BUILDING DIMENSIONS AND DETAILS CONTIGUOUS TO BUILDING, INCLUDING SIDEWALKS, RAMPS, BUILDING ENTRANCES, STAIRWAYS, UTILITY TRATIONS, CONCRETE DOOR PADS, COMPACTOR PAD, LOADING DOCKS, BOLLARDS, ETC.

POSED BOUNDS AND ANY EXISTING PROPERTY LINE MONUMENTATION DISTURBED DURING STRUCTION SHALL BE SET OR RESET BY A PROFESSIONAL LAND SURVEYOR.

R TO START OF CONSTRUCTION, CONTRACTOR SHALL VERIFY EXISTING PAVEMENT ELEVATIONS AT RFACE WITH PROPOSED PAVEMENTS, AND EXISTING GROUND ELEVATIONS ADJACENT TO NAGE OUTLETS TO ASSURE PROPER TRANSITIONS BETWEEN EXISTING AND PROPOSED FACILITIES.

ition

TRACTOR SHALL REMOVE AND DISPOSE OF EXISTING MANMADE SURFACE FEATURES WITHIN THE OF WORK INCLUDING BUILDINGS, STRUCTURES, PAVEMENTS, SLABS, CURBING, FENCES, UTILITY 5, SIGNS, ETC. UNLESS INDICATED OTHERWISE ON THE DRAWINGS. REMOVE AND DISPOSE OF ING UTILITIES, FOUNDATIONS AND UNSUITABLE MATERIAL BENEATH AND FOR A DISTANCE OF 10 BEYOND THE PROPOSED BUILDING FOOTPRINT INCLUDING EXTERIOR COLUMNS, UNLESS IFICALLY NOTED OTHERWISE, SEE PLAN SHEETS FOR SPECIFICS.

ING UTILITIES SHALL BE TERMINATED, UNLESS OTHERWISE NOTED, IN CONFORMANCE WITH L, STATE AND INDIVIDUAL UTILITY COMPANY STANDARD SPECIFICATIONS AND DETAILS. THE TRACTOR SHALL COORDINATE UTILITY SERVICE DISCONNECTS WITH THE UTILITY ESENTATIVES.

TRACTOR SHALL DISPOSE OF DEMOLITION DEBRIS IN ACCORDANCE WITH APPLICABLE FEDERAL, E AND LOCAL REGULATIONS, ORDINANCES AND STATUTES.

DEMOLITION LIMITS DEPICTED IN THE PLANS IS INTENDED TO AID THE CONTRACTOR DURING THE ING AND CONSTRUCTION PROCESS AND IS NOT INTENDED TO DEPICT EACH AND EVERY ELEMENT EMOLITION. THE CONTRACTOR IS RESPONSIBLE FOR IDENTIFYING THE DETAILED SCOPE OF OLITION BEFORE SUBMITTING ITS BID/PROPOSAL TO PERFORM THE WORK AND SHALL MAKE NO MS AND SEEK NO ADDITIONAL COMPENSATION FOR CHANGED CONDITIONS OR UNFORESEEN OR NT SITE CONDITIONS RELATED TO ANY CONDITIONS DISCOVERED DURING EXECUTION OF THE

SS OTHERWISE SPECIFICALLY PROVIDED ON THE PLANS OR IN THE SPECIFICATIONS, THE ENGINEER NOT PREPARED DESIGNS FOR AND SHALL HAVE NO RESPONSIBILITY FOR THE PRESENCE, OVERY, REMOVAL, ABATEMENT OR DISPOSAL OF HAZARDOUS MATERIALS, TOXIC WASTES OR UTANTS AT THE PROJECT SITE. THE ENGINEER SHALL NOT BE RESPONSIBLE FOR ANY CLAIMS OF , DAMAGE, EXPENSE, DELAY, INJURY OR DEATH ARISING FROM THE PRESENCE OF HAZARDOUS ERIAL AND CONTRACTOR SHALL INDEMNIFY AND HOLD HARMLESS THE ENGINEER FROM ANY MS MADE IN CONNECTION THEREWITH. MOREOVER, THE ENGINEER SHALL HAVE NO INISTRATIVE OBLIGATIONS OF ANY TYPE WITH REGARD TO ANY CONTRACTOR AMENDMENT LVING THE ISSUES OF PRESENCE, DISCOVERY, REMOVAL, ABATEMENT OR DISPOSAL OF ASBESTOS THER HAZARDOUS MATERIALS.

n Control

R TO STARTING ANY OTHER WORK ON THE SITE, THE CONTRACTOR SHALL NOTIFY APPROPRIATE NCIES AND SHALL INSTALL EROSION CONTROL MEASURES AS SHOWN ON THE PLANS AND AS TIFIED IN FEDERAL, STATE, AND LOCAL APPROVAL DOCUMENTS PERTAINING TO THIS PROJECT.

RACTOR SHALL INSPECT AND MAINTAIN EROSION CONTROL MEASURES ON A WEEKLY BASIS IMUM) OR AS REQUIRED PER THE STORMWATER POLLUTION PREVENTION PLAN (SWPPP). THE RACTOR SHALL ADDRESS DEFICIENCIES AND MAINTENANCE ITEMS WITHIN TWENTY-FOUR HOURS ISPECTION. CONTRACTOR SHALL PROPERLY DISPOSE OF SEDIMENT SUCH THAT IT DOES NOT MBER OTHER DRAINAGE STRUCTURES AND PROTECTED AREAS.

RACTOR SHALL BE FULLY RESPONSIBLE TO CONTROL CONSTRUCTION SUCH THAT IENTATION SHALL NOT AFFECT REGULATORY PROTECTED AREAS, WHETHER SUCH IENTATION IS CAUSED BY WATER, WIND, OR DIRECT DEPOSIT.

TRACTOR SHALL PERFORM CONSTRUCTION SEQUENCING SUCH THAT EARTH MATERIALS ARE SED FOR A MINIMUM OF TIME BEFORE THEY ARE COVERED, SEEDED, OR OTHERWISE STABILIZED REVENT EROSION.

N COMPLETION OF CONSTRUCTION AND ESTABLISHMENT OF PERMANENT GROUND COVER, TRACTOR SHALL REMOVE AND DISPOSE OF EROSION CONTROL MEASURES AND CLEAN SEDIMENT DEBRIS FROM ENTIRE DRAINAGE AND SEWER SYSTEMS.

g Conditions Information

PLAN: THE PROPERTY LINES SHOWN WERE DETERMINED BY AN ACTUAL FIELD SURVEY DUCTED BY VALLEY LAND SERVICES, LLC, AND FROM PLANS OF RECORD. THE TOPOGRAPHY AND ICAL FEATURES ARE BASED ON AN ACTUAL FIELD SURVEY PERFORMED ON THE GROUND BY EY LAND SERVICES, LLC, DURING JULY, 2022.

- DELINEATION OF THE WETLANDS AND PLACEMENT OF THE FLAGS WAS PERFORMED BY: VHB ON SEPTEMBER 1, 2022 AS DOCUMENTED IN THE REPORT PREPARED BY VHB DATED OCTOBER 4,
- FLAGS MARKING THE WETLANDS WERE LOCATED BY: VHB

OGRAPHY: ELEVATIONS ARE BASED ON NAVD88.

FECHNICAL DATA INCLUDING TEST PIT AND BORING LOCATIONS AND ELEVATIONS WERE AINED BY GEI GEOTECHNICAL ENGINEERS.

ent Use

E PLANS AND CORRESPONDING CADD DOCUMENTS ARE INSTRUMENTS OF PROFESSIONAL ICE, AND SHALL NOT BE USED, IN WHOLE OR IN PART, FOR ANY PURPOSE OTHER THAN FOR CH IT WAS CREATED WITHOUT THE EXPRESSED, WRITTEN CONSENT OF VHB. ANY UNAUTHORIZED REUSE, MODIFICATION OR ALTERATION, INCLUDING AUTOMATED CONVERSION OF THIS JMENT SHALL BE AT THE USER'S SOLE RISK WITHOUT LIABILITY OR LEGAL EXPOSURE TO VHB.

TRACTOR SHALL NOT RELY SOLELY ON ELECTRONIC VERSIONS OF PLANS, SPECIFICATIONS, AND A FILES THAT ARE OBTAINED FROM THE DESIGNERS, BUT SHALL VERIFY LOCATION OF PROJECT URES IN ACCORDANCE WITH THE PAPER COPIES OF THE PLANS AND SPECIFICATIONS THAT ARE LIED AS PART OF THE CONTRACT DOCUMENTS.

BOLS AND LEGENDS OF PROJECT FEATURES ARE GRAPHIC REPRESENTATIONS AND ARE NOT SSARILY SCALED TO THEIR ACTUAL DIMENSIONS OR LOCATIONS ON THE DRAWINGS. THE TRACTOR SHALL REFER TO THE DETAIL SHEET DIMENSIONS, MANUFACTURERS' LITERATURE, SHOP NINGS AND FIELD MEASUREMENTS OF SUPPLIED PRODUCTS FOR LAYOUT OF THE PROJECT



100 Great Meadow Road Suite 200 Wethersfield, CT 06109 860.807.4300

21-23 River Rd Redevelopment

21 River Road Wilton, Connecticut

No.	Revision	Date	Appvd.
Design	ed by	Checked by	
	NP/KE	· · · · · · · · · · · · · · · · · · ·	MRG

Local Approvals

Issued for

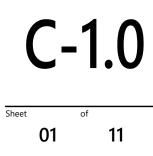
Date April 23, 2024

Not Approved for Construction

Legend, Abbreviations and General Notes

Drawing Number





Project Number 20849.00 Legend

M.U.T.C.D.	Specif	ication	Decc	
Number	Width	Height	Desc.	
R1-1	30"	30"	STOP	
R5-1	30"	30"	DO NOT ENTER	
R7-8	12"	18"	RESERVED PARKING E	
R7-8P	12"	6"	VAN ACCESSIBLE	
W11-2	30"	30"	$\langle \hat{\mathbf{x}} \rangle$	
W16-7P	24"	12"		

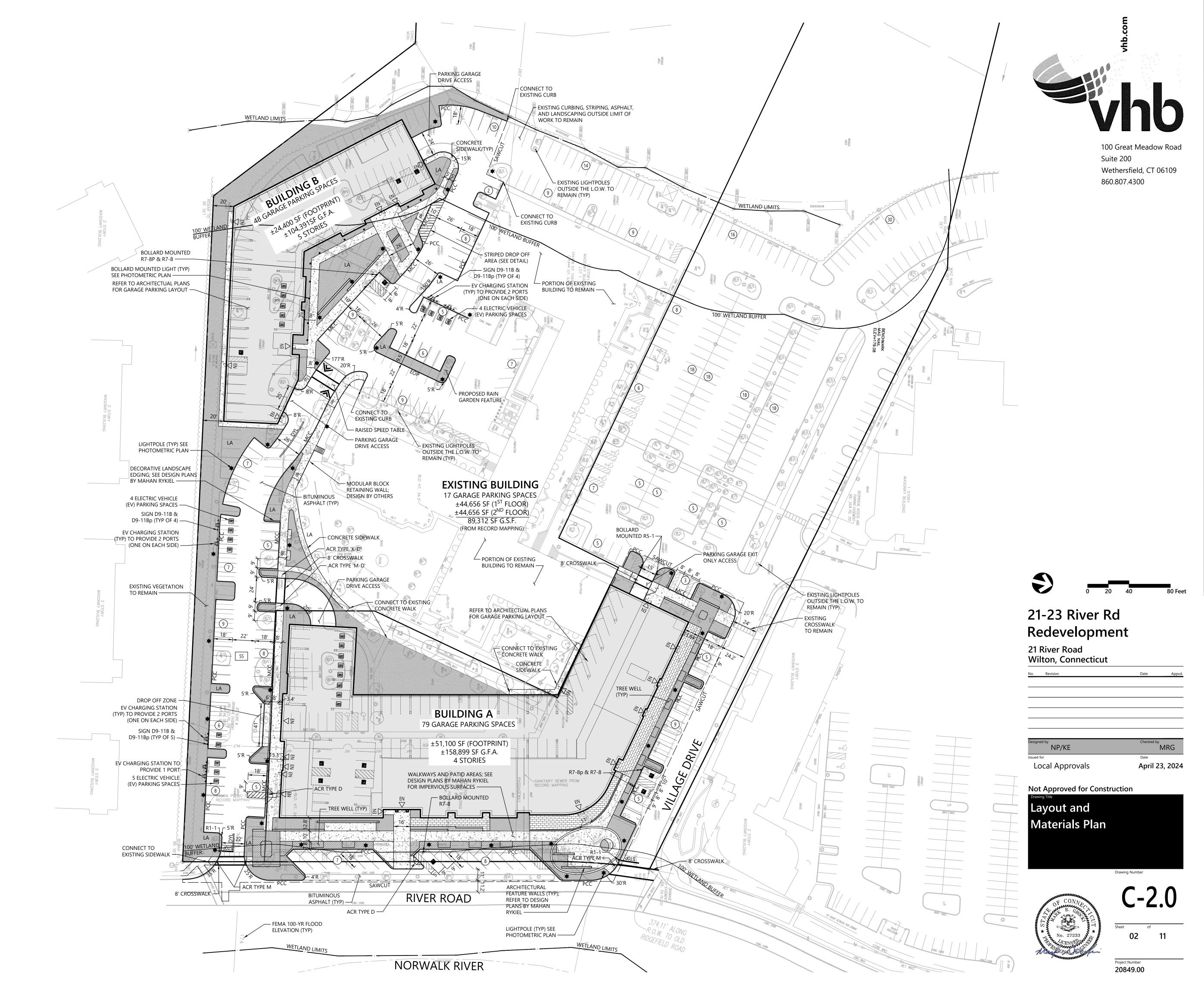
Hardscape

Landscape

Concrete

NOTE: REFER TO LANDSCAPE PLAN BY MAHAN RYKIEL FOR FINAL SURFACE TREATMENT AND DETAILS.

Proposed Building



Parking Summary Chart*

	Spac	es
Description	Required **	Provided
STANDARD SPACES	721	825
STANDARD ACCESSIBLE SPACES ***	15	30
VAN ACCESSIBLE SPACES ***	3	3
TOTAL SPACES	739	858
* PARKING REOUIREMENT IS REFLECTIVE C		5 25, 25,1 AND 25,4

** BASED ON THE NEW FORM-BASED CODE, SEC. E.6 PARKING STANDARDS (a)[3]: "...ALLOWS UP TO A 30% REDUCTION IN THE REQUIRED PARKING FOR THE JOINT

USE OF PARKING SPACES BY 2 OR MORE ESTABLISHMENTS..."

TOTAL SPACES REQ'D: 1,055 PARKING SPACES REQ'D (SEE PARKING REQUIREMENT CALCULATION IN SPREADSHEET BELOW) 1,055 x 0.7 = 739 SPACES.

*** ADA REQ'D, BASED OFF 858 PROVIDED * 2% = 18 TOTAL, INCL. 1 VAN FOR EVERY 6.

IDARKING RECHIREMENT C	ALCULATION SPREADSHEET:
	ALCOLATION STREADSTILLT.

LOADING REQUIREMENT FOR <u>ONLY LOTS 25.1 & 25.4</u> (EXCLUDING LOT 25 I.E. STOP & SHOP PLAZA): RETAIL & RESTAURANT:

3,000 TO 12,500 SF GFA = 1 12,501 TO 30,000 SF GFA = 2 OVER 30,000 SF = 3 + 1 PER ADD'L 20,000 SF GFA

TOTAL RETAIL/ RESTAURANT PROPOSED = ±12,000 SF TOTAL EXISTING RETAIL/ REST TO REMAIN = 0 SF GRAND TOTAL RETAIL / RESTAURANT= 12,000 SF

TOTAL LOADING RETAIL/ REST. = 1 SPACE

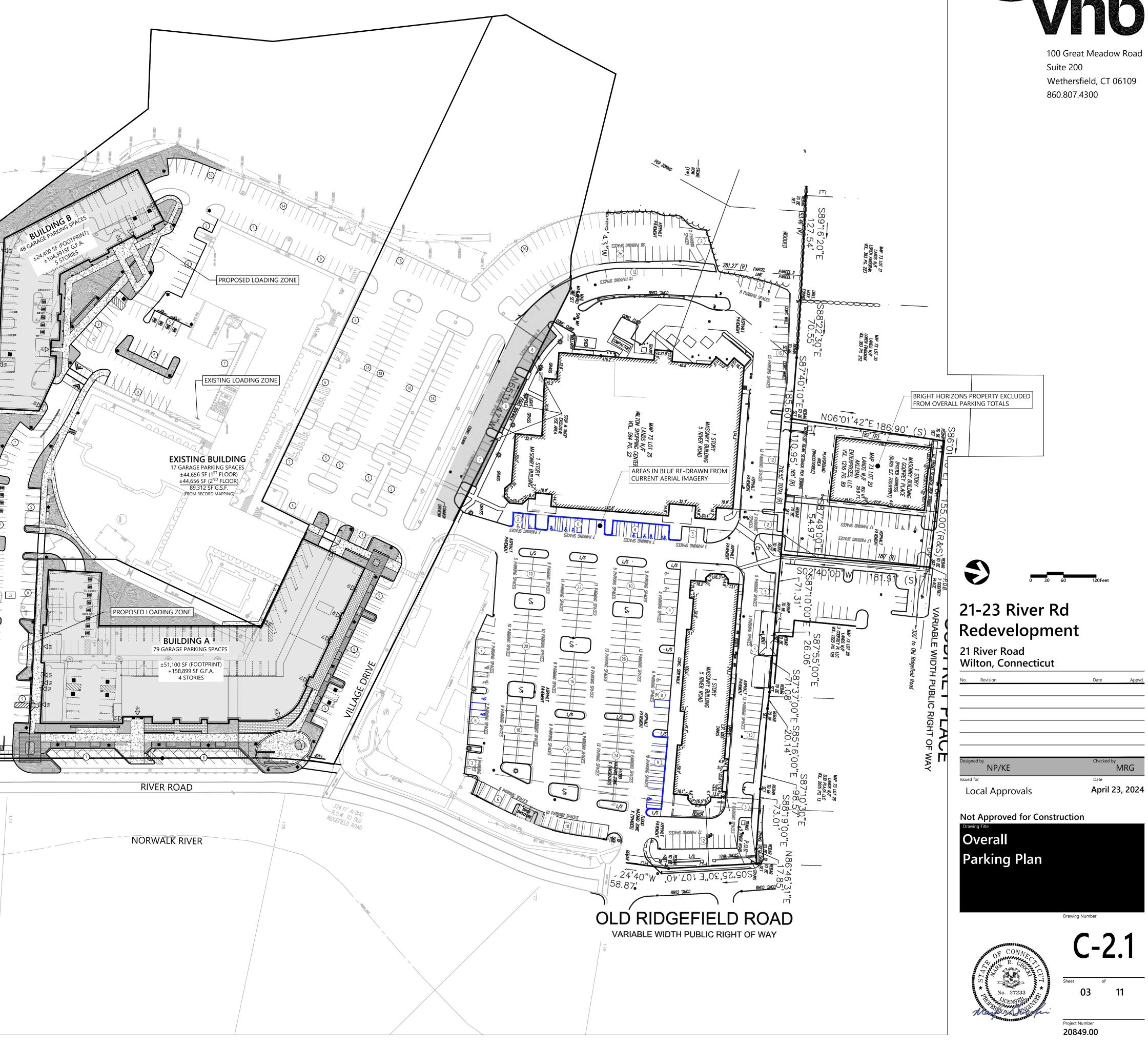
OFFICE UP TO 40,000 SF GFA = 1 UNLESS WAIVED BY COMMISSION 40,001 TO 125,000 SF GFA = 1

TOTAL OFFICE TO REMAIN = 117,296 SF TOTAL LOADING OFFICE = 1 SPACE

GRAND TOTAL LOADING REQUIRED = 2 SPACES GRAND TOTAL LOADING PROVIDED = 3 SPACES

ILTON R	IVER PARK (MAP 73, LOT 25)	Suite GLA		Parking/SF	Spots Requ
1	Stop & Shop	46764	Retail	3/1000	141
	The Vital Stretch	1383	Medical	4/1000	6
	Craft 14 Kitchen & Bar	2232	Restaurant	8/1000	18
	Ancona's Wines & Liquors	2153	Retail	3/1000	7
	CT Fitness Lab	3201	Retail	3/1000	10
	Tim La Bant Restaurant	1219	Restaurant	8/1000	10
	Happy Wok	1174	Restaurant	8/1000	10
	Great Clips	921	Retail	3/1000	3
	Cactus Rose Cantina Shaolin Studios	2584	Restaurant	8/1000	21
	Campus Jewelers	1322 955	Retail Retail	3/1000 3/1000	4
	Assumed Office	1384	Office	3/1000	3
	Assumed Office	794	Office	3/1000	3
	Sola Salon Studios	4100	Retail	3/1000	13
_	Fit Body Boot Camp	2112	Retail	8/1000	15
	Wilton Reflexology	916	Medical	4/1000	4
	Kumon Math & Reading Center	1101	Retail	3/1000	4
	Happy Hands Art & Pottery	1115	Retail	3/1000	4
	Town Green Cleaners	931	Retail	3/1000	3
	The UPS Store	1308	Retail	3/1000	4
23	Sweet Pierre's	449	Retail	3/1000	2
	Press Burger	1670	Restaurant	8/1000	14
	Sobol	903	Restaurant	8/1000	8
26	Your CBD Store	990	Retail	3/1000	3
27	Assumed Office	1505	Office	3/1000	5
	Assumed Office	376	Office	3/1000	2
29	Vision Search Partners	1237	Office	3/1000	4
	Baywater Associates	226	Office	3/1000	1
	Assumed Office	1771	Office	3/1000	6
32	Sweet Pierre's	444	Retail	3/1000	2
				TOTAL:	327
ILTON C	AMPUS (MAP 73, LOTS 25.4 & 25.1)				
	PROPOSED RESTAURANTS (BLDG A)	12,000	Restaurant	8/1000	96
	BLDG A RESIDENTIAL		Dwelling	1.55/Unit	155
4	BLDG B RESIDENTIAL	72 Units	Dwelling Office	1.55/Unit	112
	Assumed Office	1000 500	Office	3/1000 3/1000	3 2
	Blue Buffalo Storage Assumed Office	2699	Office	3/1000	2
	Blue Buffalo Storage	2033	Office	3/1000	7
	Assumed Office	3083	Office	3/1000	10
	Assumed Office	10906	Office	3/1000	33
	Kimco	1652	Office	3/1000	5
	Assumed Office	3457	Office	3/1000	11
9	Assumed Office	5773	Office	3/1000	18
10	Assumed Office	3512	Office	3/1000	11
11	Assumed Office	1408	Office	3/1000	5
12	Assumed Office	2090	Office	3/1000	7
16	Regus	9288	Office	3/1000	28
17	Assumed Office	2545	Office	3/1000	8
	BCH America, Inc.	1116	Office	3/1000	4
	Casper Company, LLC	1274	Office	3/1000	4
	Stanwich Partners, LLC	500	Office	3/1000	2
	Assumed Office	2798	Office	3/1000	9
	Laser Body Renewal LLC	1545	Medical	4/1000	7
	Blue Buffalo Enterprises, Inc.	50804	Office	3/1000	153
	Assumed Office	6899	Office	3/1000	21
27		14248	Office	3/1000	X
	Starbucks Coffee	1886	Retail	3/1000	X
29		1366	Office	3/1000	X
30		552	Office	3/1000	×
31	Annual second	3134	Office	3/1000	X
	Snappy Gator	1058	Retail Office	3/1000	X
33 34		8981		3/1000	X
		2394	Office Office	3/1000	X
35		7499	Office	3/1000	X
36	Absolute Investment Advisors	18315 1142	Office	3/1000 3/1000	×
3/	Fairfield Chemical	11043	Office	3/1000	×
20	Assumed Office	1504	Office	3/1000	X 5
		500	Office	3/1000	2
39	Snappy Gator (Storage)	1 300		3/1000	1
<mark>39</mark> 41	Snappy Gator (Storage)	225			
<mark>39</mark> 41	Snappy Gator (Storage) Assumed Office	225	Office		728
<mark>39</mark> 41		225		TOTAL:	728
39 41 42	Assumed Office	225			728 1055
39 41 42	Assumed Office Proposed Use		GRAND TOT	TOTAL:	
39 41 42	Assumed Office	tion purpos	GRAND TOT	TOTAL:	

** Total square footage of all existing tenant space in Wilton Center = 188,914 SF (not reflective of proposed changes)





FORM-BASE CODE: Development Regulations, Section E.5.(B).				
		Requirement	Proposed*	
Property Area - Large Lot, Section B.(1	8)	1.5 Acres	Lot 25.1 = 5.44, Lot 25.4 = 6.76 Total Area Combined = 12.2ac	
Building Coverage, Section E.5.(B)[1]		65%	23%	
Lot Impervious Coverage, Section E.5.(b)[2]		80%	59.7%	
Building Setbacks, Section E.5.(b)[3]				
	Front	Per Build-To-Line	See Frontage Tables	
	Rear	20 Feet	>20 Feet	
	Side	None	None	
Gross Floor Area				
	Existing to Remain	Not Applicable	115,067 SF	
	Building A	Not Applicable	158,899 SF	
	Building B	Not Applicable	104,391 SF	
	Total	Not Applicable	378,357 SF	
Floor Area Ratio		Not Applicable	0.72	
Civic Space Area (SHOWN ON PLAN H	HATCHED:	0.5 Acres	0.53 Acres	
Civic Space Frontage Occupancy				
	Building A	60%	74.8%	
	Building B	60%	72.6%	

* THE PROPOSED INFORMATION PROVIDED IS BASED ON THE COMBINATION OF TWO (2) LOTS: 25.1 AND 25.4

FORM-BASE CODE: River Road, Public Right-Of-Way, Primary Mixed-Use Street Frontage (FR-1) These Standards Apply To The Easterly Face Of Building A Fronting On River Road

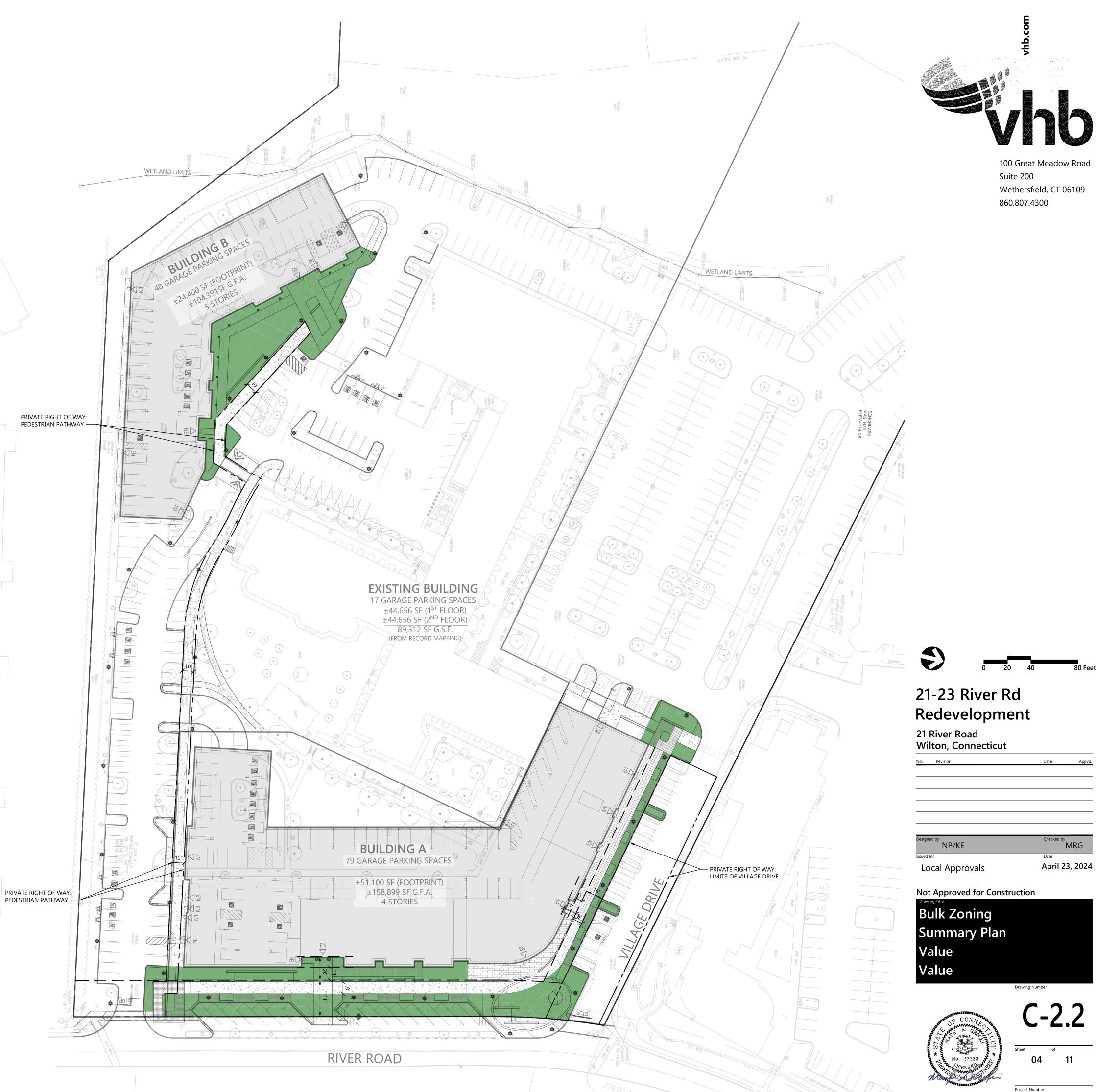
		· · · · ·		
Standard		Requirement	Proposed	Comments
Build-To-Line, Table E.2., Note 1		25'+	31'	Commission may increase to accommodate angled parking along frontage. Measured to Property Line.
Build-To-Zone, Table F.1., Note 6, WC-1 Store Professional	front Or WC-2	5'-20'	11' - 20'	Commission may increase to 20' on Large Lots. Per Section 29-6.G.1.C.(2): Commission may modify to Permit WC-1 or WC-2 Frontage Types
Sidewalks, Table E.2.		8'	10'	
Building Height, Table E.3. Including Ground L Retail/Commercial	evel			
	Minimum	2 Stories, 28 Feet	3 Stories, 41'-6"	
	Maximum	4 Stories, 54 Feet	4 Stories, 50'-4"	
	Bonus, Section E.5.(c)[1](i) < 25% of fourth story	5 Stories, 64 Feet	4 Stories + Lofts, 59'-10"	Commission may grant for a beneficial architectural feature that emphasizes a corner.
	Maximum in Build-to Zone	48 Feet	41'-6"	
Building Stepback for Large Lots, Section E.4.(b).a.	Average of 10'	Average of 10'	
Minimum Frontage Occupancy, Table F.4.		60%	68%	

FORM-BASE CODE: "Village Drive", Private Right-Of-Way, Mixed-Use Neighborhood Street Frontage (FR-3)

These Standards Apply To The Northerly Face Of Building A Fronting On The Shared Site Driveway, Given A Ceremonial Name Of "Village Drive"				
Standard		Requirement	Proposed	Comments
Build-To-Line, Table E.2.		15'	15'	Measured to curb line.
Build-To-Zone, Table F.1., Note 6, WC-1 Store Professional	front Or WC-2	5'-20'	5' - 11'	Commission may increase to 20' on Large Lots.
Sidewalks, Table E.2.		8'	8'	
Building Height, Table E.3. Including Ground L Retail/Commercial	evel			
	Minimum	2 Stories, 28 Feet	3 Stories, 40'-6"	
	Maximum	4 Stories, 54 Feet	4 Stories, 50'-4"	
	Bonus, Section E.5.(c)[1](i) < 25% of fourth story	5 Stories, 64 Feet	4 Stories + Loft, 59'-10"	Commission may grant for a beneficial architectural feature that emphasizes a corner.
	Maximum in Build-to Zone	48 Feet	40'-6"	
Building Stepback for Large Lots, Section E.4.(b).a.	Average of 10'	Average of 10'	
Minimum Frontage Occupancy, Table F.4.		50%	100%	

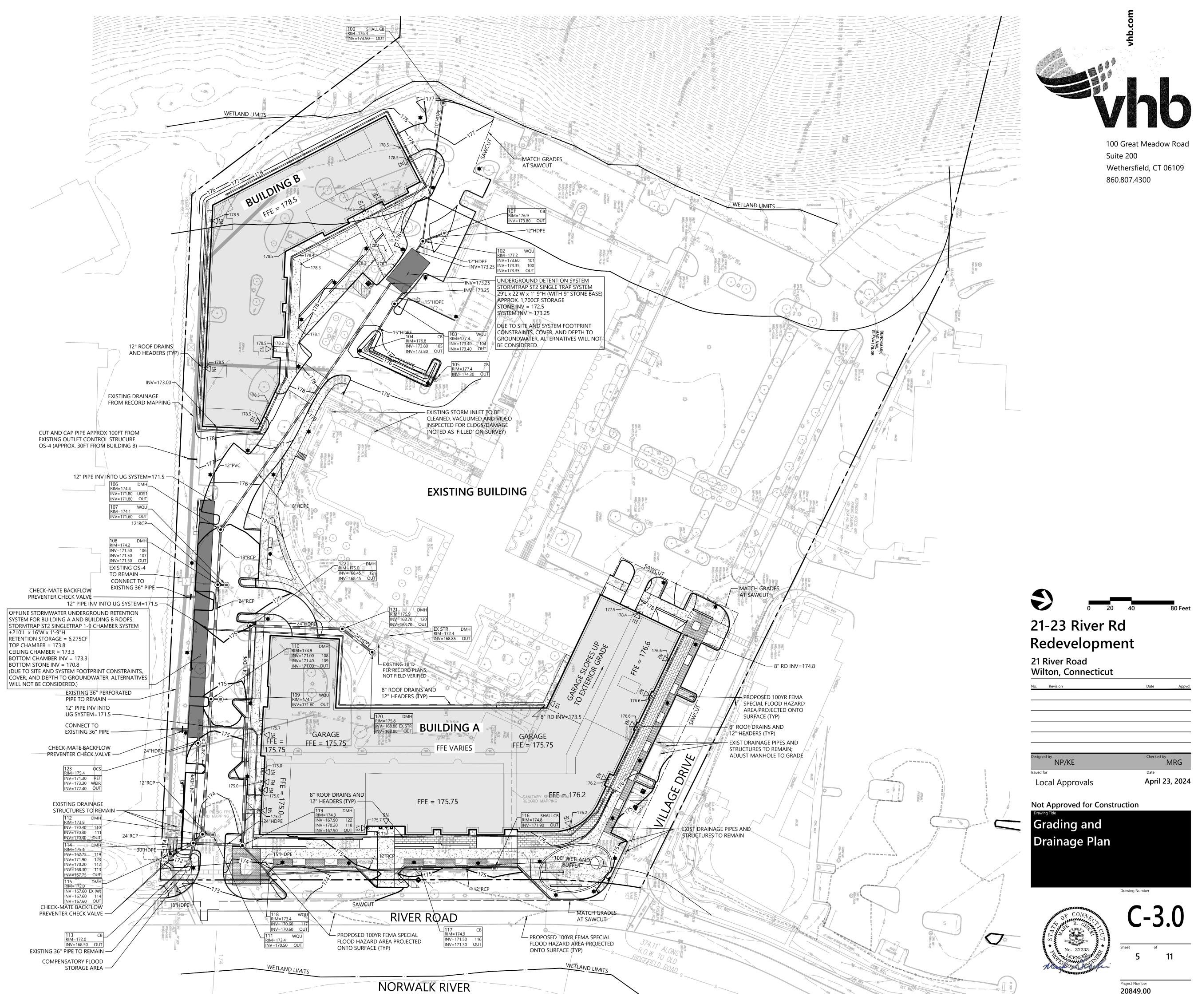
FORM-BASE CODE: Private Pedestrian Right-Of-Way: Pedestrian Pathway Street Frontage (FR-5)

Frontage (FK-5) These Standards Apply To The Northerly Face Of Building B Located In The Rear Of The Property.					
Standard		Requirement	Proposed	Comments	
Build-To-Line, Table E.2.		Not Applicable	Not Applicable		
Build-To-Zone, Table F.1., Easement, WC-10		Not Applicable	Not Applicable		
Sidewalks, Table E.2.		10'	10'		
Building Height, Table E.3. Including Ground Leve Retail/Commercial	el				
Ν	/inimum	2 Stories, 28 Feet	3 Stories, 33'-10"		
Ν	/laximum	4 Stories, 54 Feet	4 Stories, 44'-6"		
E	Conus, Section 5.(c)[1](ii) < 50% of fourth story	5 Stories, 64 Feet	5 Stories, 56'-8"	Commission may grant for a building 100 feet from a Street Frontage where a public benefit has been shown.	
1 1	Aaximum in Build-to Zone	48 Feet	33'-10"		
Building Stepback at 4th story for Large Lots, Sec	ction E.4.(b).a.	Average 10'	Average 10'		
Building Stepback at 5th story for Large Lots, Sec	ction E.4.(b).b.	At Least 10'	10'		
Minimum Frontage Occupancy, Table F.4.		None	Not Applicable		

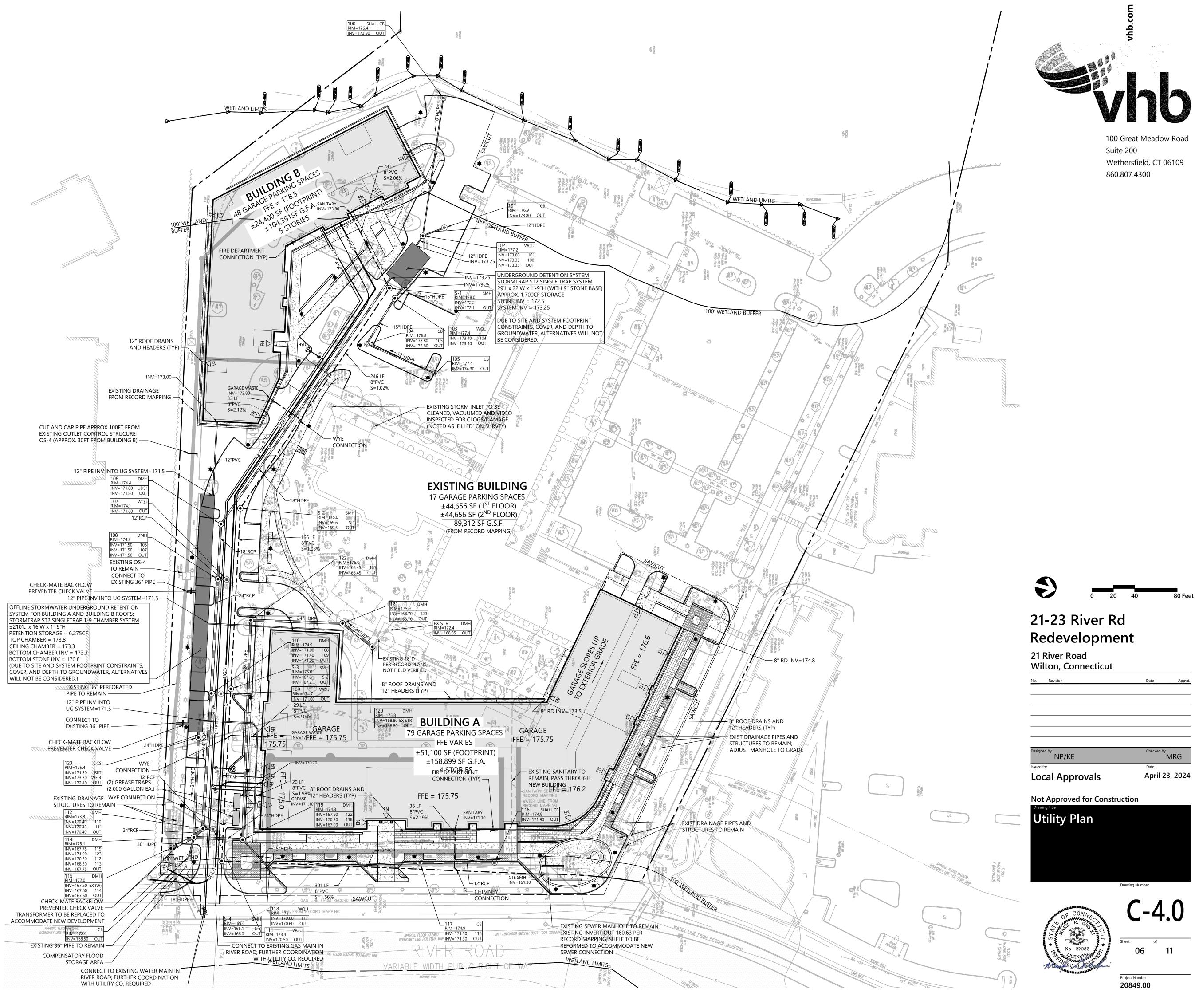


Project Number **20849.00**





No.	Revision	Date	Appvd
Designe		Checked by	
	NP/KE	IV	1RG
Issued fo	or	Date	
10	cal Approvals	April 23	, 2024



\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\cad\ld\Planset\04_20849.00UT.dwg



No.	Revision	Date	Appvd.
Design	NP/KE	Checked by	/IRG
ssued	for	Date	

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\cad\ld\Planset\05_20849.00ER.dwg

Site S&E Narrative:

UTILITIES

THE PROPOSED PROJECT CONSISTS OF DEMOLISHING A PORTION OF AN EXISTING BUILDING AND RECONSTRUCTING IN PLACE AND CONSTRUCTING ANOTHER SEPARATE BUILDING WITH ASSOCIATED PARKING, DRIVEWAYS AND UNDERGROUND

THE APPROXIMATELY 12 ACRE SITE WILL BE DEVELOPED IN A SINGLE PHASE PROJECT. APPROXIMATELY 5 ACRES WILL BE DISTURBED DURING CONSTRUCTION.

TO CONTROL SEDIMENT EROSION DURING EARTH FILLING OPERATIONS, THE CONTRACTOR SHALL EMPLOY TECHNIQUES OUTLINED IN THE CONSTRUCTION SEQUENCE AND EROSION CONTROL NOTES TO ENSURE THAT EROSION DOES NOT OCCUR AND THAT SEDIMENT IS NOT TRANSPORTED OFF. THE EARTHWORK IS PLANNED TO START SPRING 2025 AND BE COMPLETED SPRING 2026.

THE EROSION AND SEDIMENTATION CONTROLS SHALL BE EMPLOYED BY THE CONTRACTOR DURING THE EARTHWORK AND CONSTRUCTION PHASES OF THE PROJECT IN ACCORDANCE WITH THE CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL. REFER TO THE DRAINAGE/STORMWATER MANAGEMENT REPORT FOR MORE INFORMATION.

Temporary Erosion and Sedimentation Control Maintenance (throughout construction) THE SITE CONTRACTOR WILL BE RESPONSIBLE FOR IMPLEMENTING EACH CONTROL SHOWN ON THE SEDIMENTATION AND EROSION CONTROL PLAN.

THE SITE CONTRACTOR WILL INSPECT ALL SEDIMENT AND EROSION CONTROL STRUCTURES PERIODICALLY AND AFTER EACH RAINFALL EVENT. RECORDS OF THE INSPECTIONS WILL BE PREPARED AND MAINTAINED ON-SITE BY THE CONTRACTOR.

SILT SHALL BE REMOVED FROM BEHIND BARRIERS IF GREATER THAN 6-INCHES DEEP OR AS NEEDED.

DAMAGED OR DETERIORATED ITEMS WILL BE REPAIRED IMMEDIATELY AFTER IDENTIFICATION. THE UNDERSIDE OF HAY BALES SHOULD BE KEPT IN CLOSE CONTACT WITH THE EARTH AND RESET AS NECESSARY.

SEDIMENT THAT IS COLLECTED IN STRUCTURES SHALL BE DISPOSED OF PROPERLY AND COVERED IF STORED ON-SITE. INSPECT THE TEMPORARY SEDIMENT TRAP AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF A RAINFALL EVENT TO DETERMINE THE CONDITIONS OF THE BASINS DURING CONSTRUCTION. CLEAN OUT SEDIMENT BASINS WHEN ACCUMULATION REACHES 12". SEDIMENT LEVELS SHALL BE MARKED WITHIN THE SEDIMENT STORAGE AREA BY STAKES. DO NOT ALLOW ACCUMULATED SEDIMENTS TO FLUSH INTO WETLAND AREAS.

EROSION CONTROL STRUCTURES SHALL REMAIN IN PLACE UNTIL ALL DISTURBED EARTH HAS BEEN SECURELY STABILIZED. AFTER REMOVAL OF STRUCTURES, DISTURBED AREAS SHALL BE REGRADED AND STABILIZED AS SOON AS PRACTICAL.

MAINTAIN THE CONSTRUCTION ENTRANCE IN A CONDITION WHICH WILL PREVENT TRACKING AND WASHING OF SEDIMENTS ONTO PAVED SURFACES.

Construction Sequence

- 1. THE SITE CONTRACTOR SHALL BE FULLY RESPONSIBLE TO CONTROL CONSTRUCTION SUCH THAT SEDIMENTATION SHALL NOT AFFECT ROADS/HIGHWAYS AND THEIR DRAINAGE SYSTEM, NEIGHBORING PROPERTIES, AND REGULATORY PROTECTED AREAS, WHETHER SUCH SEDIMENTATION IS CAUSED BY WATER, WIND, OR DIRECT DEPOSIT. PRIOR TO CONSTRUCTION, THE APPLICANT SHALL PROVIDE THE TOWN OF WILTON WITH THE NAME OF CONTACT AND 24 HOUR CONTACT INFORMATION.
- 2. CONTRACTOR SHALL ADHERE TO CONNECTICUT GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
- 3. FLAG THE LIMITS OF CONSTRUCTION NECESSARY TO FACILITATE THE PRECONSTRUCTION MEETING. 4. HOLD PRECONSTRUCTION MEETING. (REMEMBER TO CALL BEFORE YOU DIG 1-800-922-4455).
- 5. NOTIFY THE TOWN OF WILTON AGENT, ZONING ENFORCEMENT OFFICER AND ENGINEERING DEPARTMENT, 48 HOURS PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION ACTIVITY. 6. INSTALL STABILIZED VEHICLE CONSTRUCTION EXIT.
- 7. PRIOR TO INSTALLING SURFACE WATER CONTROLS SUCH AS TEMPORARY DIVERSION SWALES, INSPECT EXISTING CONDITIONS TO ENSURE DISCHARGE LOCATIONS ARE STABLE. IF NOT STABLE, REVIEW DISCHARGE CONDITIONS WITH THE DESIGN ENGINEER AND IMPLEMENT ADDITIONAL STABILIZATION MEASURES PRIOR TO INSTALLING SURFACE WATER
- CONTROLS. 8. INSTALL EROSION AND SEDIMENT CONTROLS IN ACCORDANCE WITH THE E&S PLAN FOR THE SITE INCLUDING SILTFENCE BARRIERS AND SILT SAC.
- 9. COMPLETE CLEARING AND GRUBBING 10. ESTABLISH ROUGH GRADE ON THE SITE.

11. CONSTRUCT BUILDING AND UNDERGROUND UTILITIES. INSTALL SILT SAC SEDIMENT TRAPS IN ALL NEW CATCH BASINS. 12. INSTALL PAVEMENT BASE & FIRST COURSE OF BITUMINOUS CONCRETE. 13. INSTALL LANDSCAPING & LOAM AND SEED ALL DISTURBED AREAS.

- 14. AFTER SITE IS STABILIZED REMOVE TEMPORARY EROSION AND SEDIMENT CONTROLS.
- 15. LOAM AND SEED ALL DISTURBED AREAS. 16. WHEN ALL OTHER WORK HAS BEEN COMPLETED, REPAIR AND SWEEP ALL PAVED AREAS FOR THE FINAL COURSE OF PAVING. INSPECT THE DRAINAGE SYSTEM AND CLEAN AS NEEDED. 17. INSTALL FINAL COURSE OF PAVEMENT.

Erosion and Sedimentation Control Tecniques

THE FOLLOWING EROSION AND SEDIMENTATION CONTROLS SHALL BE EMPLOYED BY THE CONTRACTOR DURING THE EARTHWORK AND CONSTRUCTION PHASES OF THE PROJECT IN ACCORDANCE WITH THE CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION 2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL.

IN AREAS WHERE HIGH RUNOFF VELOCITIES OR HIGH SEDIMENT LOADS ARE EXPECTED, HAY BALE BARRIERS WILL BE BACKED UP WITH SILT FENCING. THIS SEMI-PERMEABLE BARRIER MADE OF A SYNTHETIC POROUS FABRIC WILL PROVIDE ADDITIONAL PROTECTION. THE SILT FENCES AND HAY BALE BARRIER WILL BE REPLACED AS DETERMINED BY PERIODIC FIELD INSPECTIONS.

STRAW BALE BARRIERS STRAW BALE BARRIERS WILL BE PLACED TO TRAP SEDIMENT TRANSPORTED BY RUNOFF BEFORE IT REACHES THE DRAINAGE SYSTEM OR LEAVES THE CONSTRUCTION SITE. BALES WILL BE SET AT LEAST FOUR INCHES INTO THE EXISTING GROUND TO MINIMIZE UNDERCUTTING BY RUNOFF.

CATCH BASIN PROTECTION NEWLY CONSTRUCTED AND EXISTING CATCH BASINS WILL BE PROTECTED WITH SILT SACKS THROUGHOUT CONSTRUCTION.

GRAVEL AND CONSTRUCTION ENTRANCE/EX MPORARY CRUSHED-STONE CONSTRUCTION ENTRANCE/EXIT WILL BE CONSTRUCTED. A CROSS SLOPE WILL BE PLACED IN THE ENTRANCE TO DIRECT RUNOFF TO THE SEDIMENT TRAP.

VEGETATIVE SLOPE STABILIZATION STABILIZATION OF OPEN SOIL SURFACES WILL BE IMPLEMENTED WITHIN 14 DAYS AFTER GRADING OR CONSTRUCTION ACTIVITIES HAVE TEMPORARILY OR PERMANENTLY CEASED, UNLESS THERE IS SUFFICIENT SNOW COVER TO PROHIBIT IMPLEMENTATION, VEGETATIVE SLOPE STABILIZATION WILL BE USED TO MINIMIZE EROSION ON SLOPES OF 3:1 OR FLATTER. ANNUAL GRASSES, SUCH AS ANNUAL RYE, WILL BE USED TO ENSURE RAPID GERMINATION AND PRODUCTION OF ROOTMASS. PERMANENT STABILIZATION WILL BE COMPLETED WITH THE PLANTING OF PERENNIAL GRASSES OR LEGUMES ESTABLISHMENT OF TEMPORARY AND PERMANENT VEGETATIVE COVER MAY BE ESTABLISHED BY HYDRO-SEEDING OR SODDING. A SUITABLE TOPSOIL, GOOD SEEDBED PREPARATION, AND ADEQUATE LIME, FERTILIZER AND WATER WILL BE PROVIDED FOR EFFECTIVE ESTABLISHMENT OF THESE VEGETATIVE STABILIZATION METHODS. MULCH WILL ALSO BE USED AFTER PERMANENT SEEDING TO PROTECT SOIL FROM THE IMPACT OF FALLING RAIN AND TO INCREASE THE CAPACITY OF THE SOIL TO ABSORB WATER.

STOCKPILE MANAGEMENT SIDESLOPES OF STOCKPILED MATERIAL SHALL BE NO STEEPER THAN 2:1. STOCKPILES NOT USED WITHIN 30 DAYS NEED TO BE SEEDED AND MULCHED IMMEDIATELY AFTER FORMATION OF THE STOCKPILE. HAYBALES AND SILT FENCE ARE TO BE PLACED AROUND THE STOCKPILE AREA APPROXIMATELY 10 FEET FROM THE TOW OF SLOPE.

DUST CONTROL PERIODICALLY MOISTEN EXPOSED SURFACES ON UNPAVED TRAVELWAYS TO KEEP THE TRAVELWAY DAMP AND REDUCE

Post Construction Stormwater Management

THE PROPERTY OWNER SHALL BE RESPONSIBLE FOR ENSURING THAT STORMWATER MANAGEMENT SYSTEMS BE INSPECTED AND MAINTAINED. THE FOLLOWING PLAN COMPONENTS SHALL BE ADHERED TO:

<u>SOURCE CONTROL</u> A COMPREHENSIVE SOURCE CONTROL PROGRAM WILL BE IMPLEMENTED AT THE SITE, WHICH INCLUDES REGULAR PAVEMENT SWEEPING AT A MINIMUM 2 TIMES PER YEAR, CATCH BASIN CLEANING, AND MAINTENANCE AND CLEARING OF LITTER FROM PARKING AREAS AND PERIMETER LANDSCAPED AREAS. CLEAN ALL CATCH BASINS AND STRUCTURES TWICE ANNUALLY TO REMOVE ACCUMULATED SAND, SEDIMENT, AND FLOATABLE PRODUCTS OR AS NEEDED BASED ON USE.

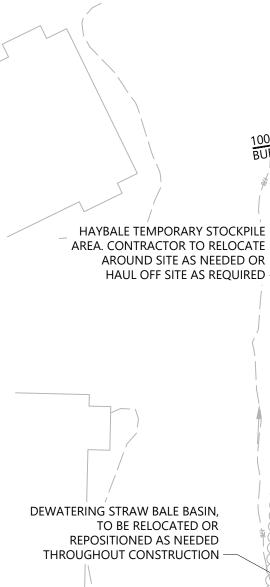
DEEP SUMP CATCH BASINS CATCH BASINS AT THE SITE ARE TO BE CONSTRUCTED WITH SUMPS (MINIMUM 4-FEET) TO TRAP DEBRIS AND SEDIMENTS. CATCH BASINS WILL BE CLEANED TWICE PER YEAR.

<u>SUBSURFACE STORAGE SYSTEM</u> THE SUBSURFACE STORAGE SYSTEM IS AN UNDERGROUND STORAGE SYSTEM TO BE USED FOR SURFACE AND ROOF RUNOFF. INSPECT THE UNDERGROUND STORAGE SYSTEM ANNUALLY, IN THE SPRING. NECESSARY REPAIRS WILL BE PERFORMED IMMEDIATELY UPON IDENTIFICATION. THE PROJECT IS REQUIRED TO STORE 1" OF RUNOFF FROM THE PROPOSED ROOFS AND THE PROJECT WILL PROVIDE 6,000 CF OF REQUIRED STORAGE.

SNOW SHELF INSPECT SNOW SHELVES ONCE ANNUALLY, IN THE SPRING, FOR ACCUMULATED SEDIMENT. NECESSARY SEDIMENT REMOVAL, EARTH REPAIR, AND/OR RESEEDING WILL BE PERFORMED IMMEDIATELY UPON IDENTIFICATION.

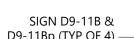
HYDRODYNAMIC SEPARATOR WATER QUALITY UNIT A HYDRODYNAMIC SEPARATOR WATER QUALITY UNIT WILL BE USED TO TREAT STORMWATER BEFORE IT REACHES THE DISCHARGE POINT. THIS ALLOWS SUSPENDED SEDIMENTS TO BE REMOVED AND REDUCES SEDIMENTATION ACCUMULATION. INSPECT THE WATER QUALITY UNIT FOR ACCUMULATED SEDIMENT AND DEBRIS. NECESSARY SEDIMENT AND/OR DEBRIS REMOVAL WILL BE PERFORMED IMMEDIATELY UPON IDENTIFICATION.

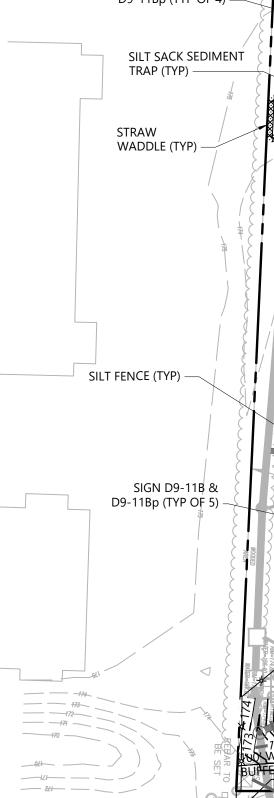
ALL E&S CONTROL MEASURES WILL BE INSPECTED WEEKLY AND AFTER RAINFALL OF 0.5 INCHES IN 24 HOURS.



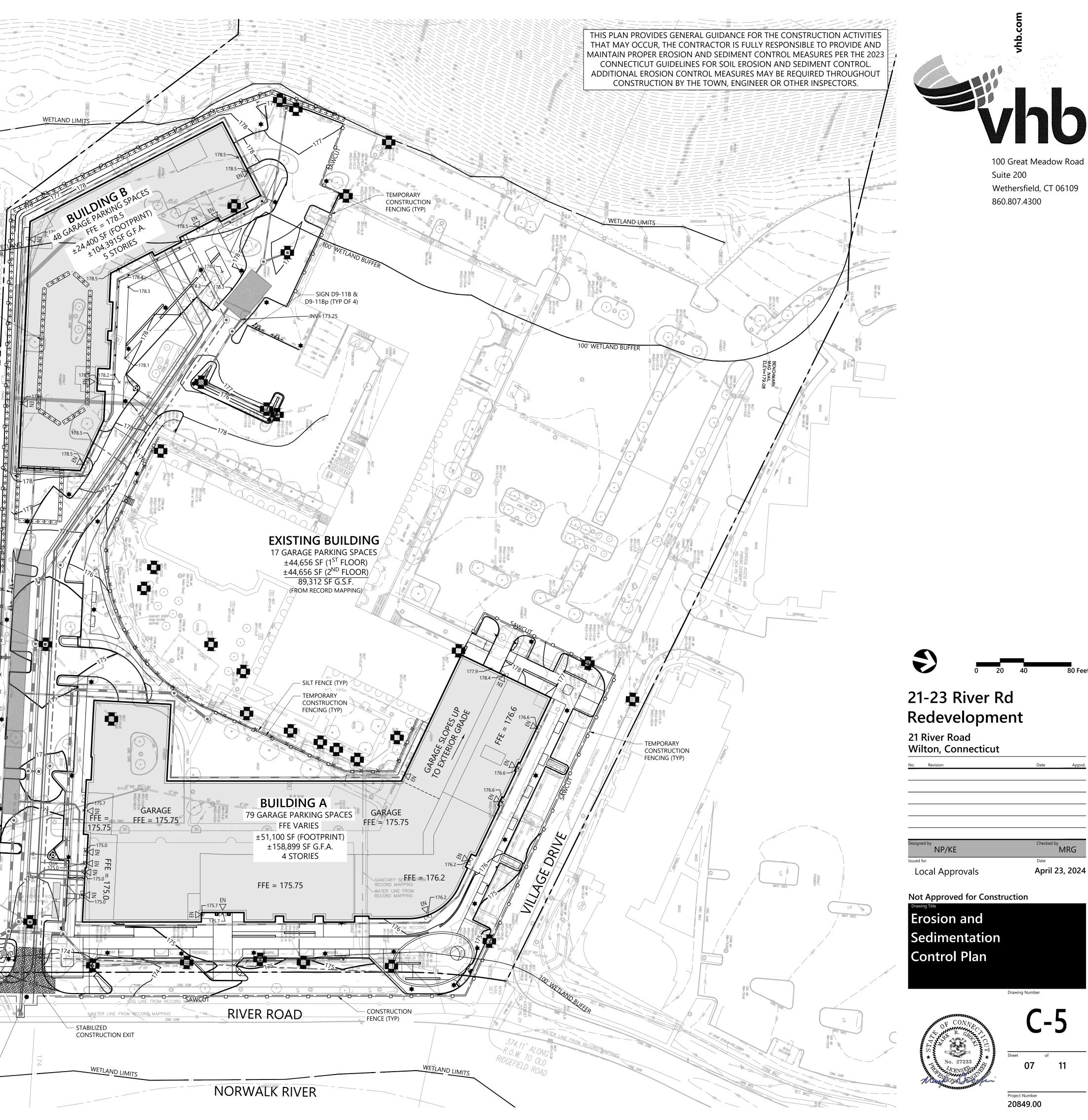
SILT FENCE AND

STRAW BALE -





PROVIDE STREET SWEEPING OR VACUUMING OF ANY TRANSPORTED SEDIMENT MATERIAL OFFSITE ONTO ROADWAYS AS NEEDED THROUGHOUT CONSTRUCTION -



Project Number 20849.00 11

hecked by

MRG



CATCH BASIN GRATE —

CATCH BASIN GRATE -

SILTSACK -

FLOW

NOTES

N.T.S.

WORK AREA

TOP OF

GROUND -

PLAN VIEW

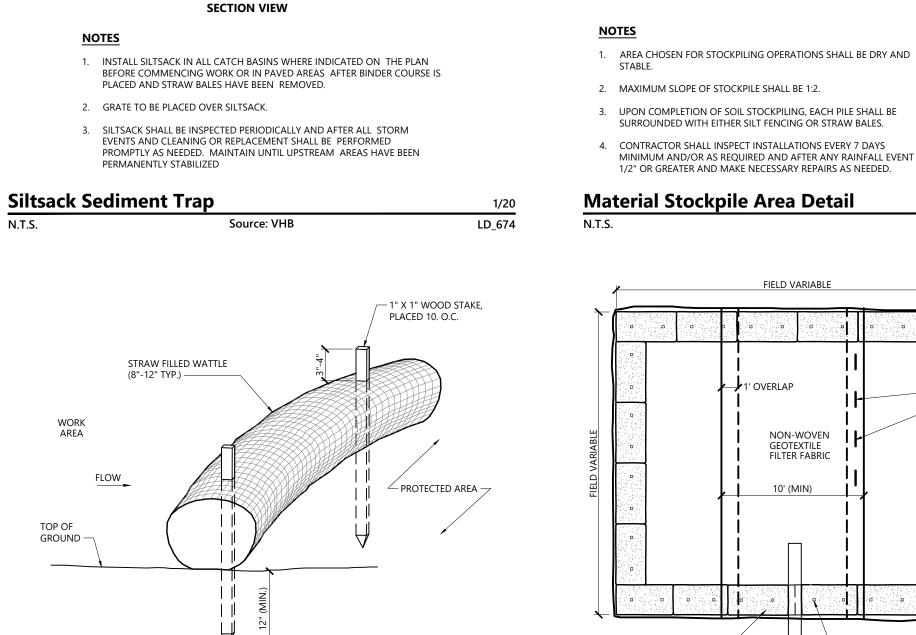
SILTSACK —

— 1" REBAR FOR

OVERFLOW PORT

EXPANSION RESTRAINT

BAG REMOVAL

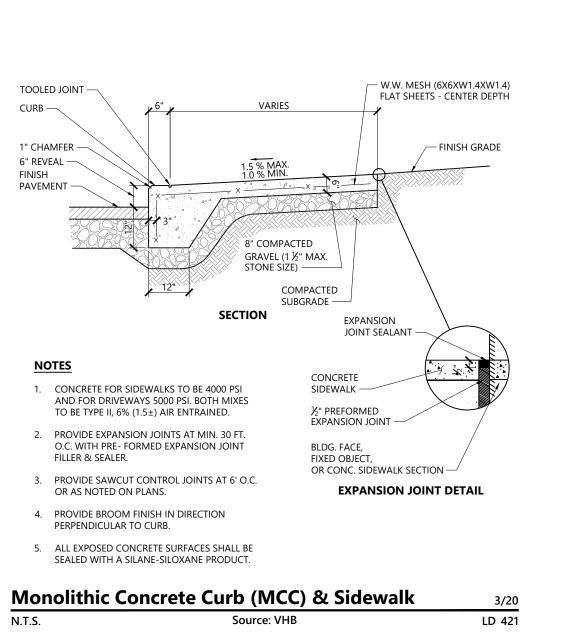


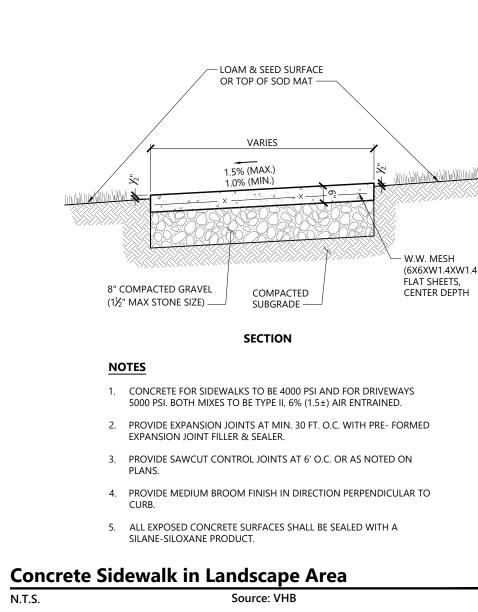
NOTES

FLOW

- 1. STRAW WATTLE SHALL BE AS MANUFACTURED BY EARTHSAVER OR APPROVED EQUAL.
- 2. STRAW WATTLES SHALL OVERLAP A MINIMUM OF 12 INCHES.
- 3. STRAW WATTLE SHALL BE INSPECTED PERIODICALLY AND AFTER ALL STORM EVENTS, AND REPAIR OR REPLACEMENT SHALL BE PERFORMED PROMPTLY AS NEEDED.
- 4. TEMPORARY STRAW WATTLES TO BE REMOVED BY CONTRACTOR. ALL OTHERS TO REMAIN IN PLACE UNLESS DIRECTED OTHERWISE BY ENGINEER.
- 5. IF NON BIODEGRADABLE NETTING IS USED THE NETTING SHALL BE COLLECTED AND DISPOSED OF OFFSITE.

Straw Wattle - Erosion Control Barrier 1/20 N.T.S. Source: VHB LD_659





2. THE BASIN TO BE SIZED TO PREVENT DISCHARGE WATER FROM

Source: VHB

OVERTOPPING BASIN.

Dewatering Straw Bale Basin

N.T.S.

- FIELD VARIABLE 1' OVERLAP NON-WOVEN GEOTEXTILE FILTER FABRIC 10' (MIN - WOODEN STAKES, STAKED BALES — 2 PER BALE DISCHARGE HOSE PLAN VIEW — FILTER FABRIC (MIRAFI 140N OR APPROVED EQUAL) - DISCHARGE HOSE SECURE HOSE DISCHARGE -CROSS-SECTION NOT 1. NUMBER OF BALES MAY VARY DEPENDING ON SITE CONDITIONS.
- 2. MAXIMUM SLOPE OF STOCKPILE SHALL BE 1:2. 3. UPON COMPLETION OF SOIL STOCKPILING, EACH PILE SHALL BE SURROUNDED WITH EITHER SILT FENCING OR STRAW BALES. 4. CONTRACTOR SHALL INSPECT INSTALLATIONS EVERY 7 DAYS

+-++

- STRAW BALES OR SILT FENCE

(SEE DETAIL THIS SHEET).

LOCATE 3' CLEAR FROM

BOTTOM OF STOCKPILE. -

IF STOCKPILE IS TO REMAIN

SHALL BE ENTIRELY

TEMPORARY VEGETATIVE MEASURES, OR MULCH. ---

STABILIZED WITH

2% N. PE

FOR MORE THAN 14 DAYS, IT

SLOP

SECURE FABRIC

WITH EROSION

CONTROL

- FII TER FABRIC

MIRAFI 140N (OR APPROVED

1/16

N.T.S.

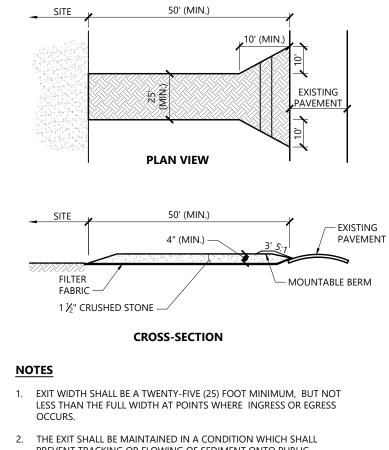
LD_690

EQUAL)

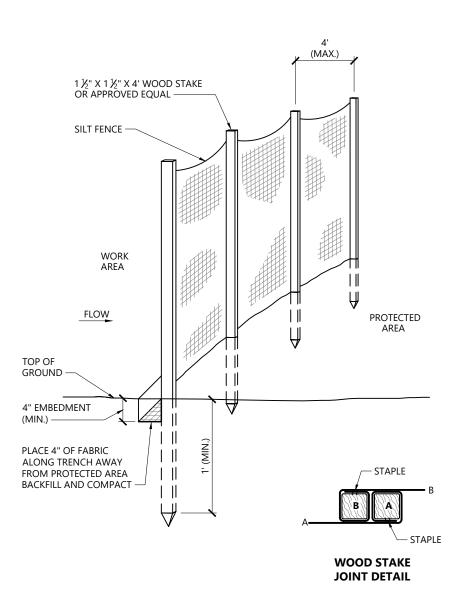
STAPLES

- MINIMUM AND/OR AS REQUIRED AND AFTER ANY RAINFALL EVENT OF 1/2" OR GREATER AND MAKE NECESSARY REPAIRS AS NEEDED.

Material Stockpile Area Detail



- PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY. BERM SHALL BE PERMITTED. PERIODIC INSPECTION AND MAINTENANCE SHALL BE PROVIDED AS NEEDED.
- 3. STABILIZED CONSTRUCTION EXIT SHALL BE REMOVED PRIOR TO FINAL FINISH MATERIALS BEING INSTALLED.

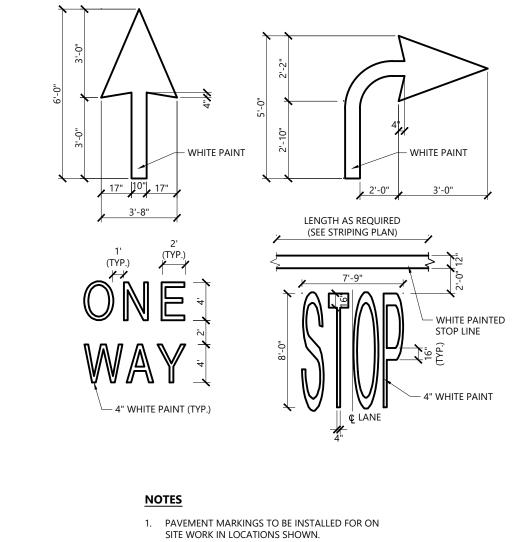


Source: VHB



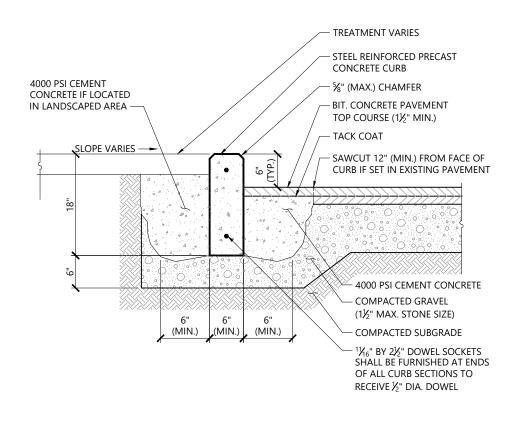


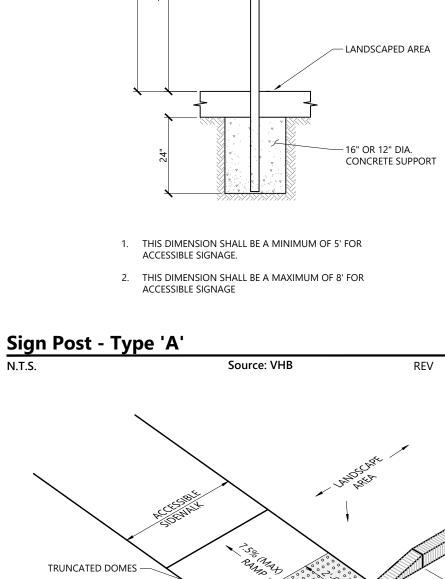


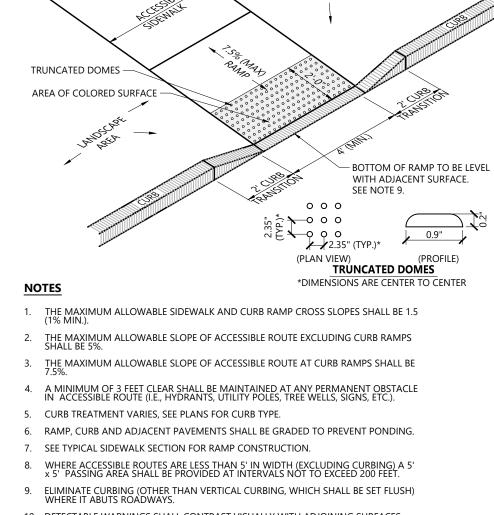




Source: VHB









Source: VHB

Accessible Curb Ramp (ACR) Type 'M-D'

3/21 LD_426 N.T.S.

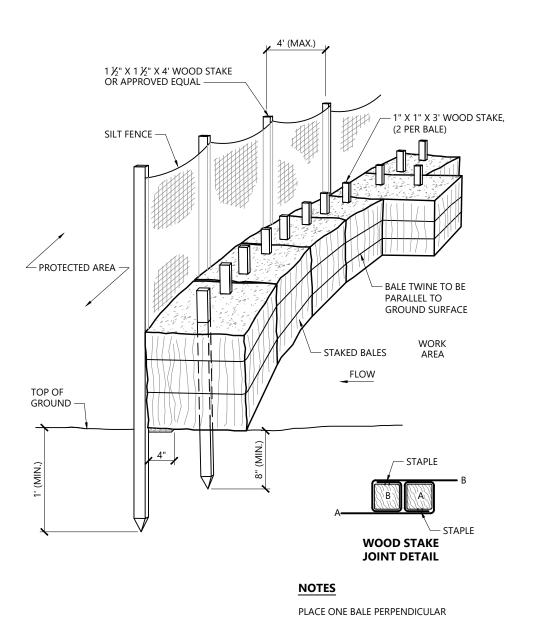
3/20 LD 404

N.T.S.

1/16

N.T.S.

LD_554





100 Great Meadow Road Suite 200 Wethersfield, CT 06109 860.807.4300



1/16

LD_650

3/19

LD_701

- CAP STEEL PIPE POST

- 2 ½" DIA. STEEL POST

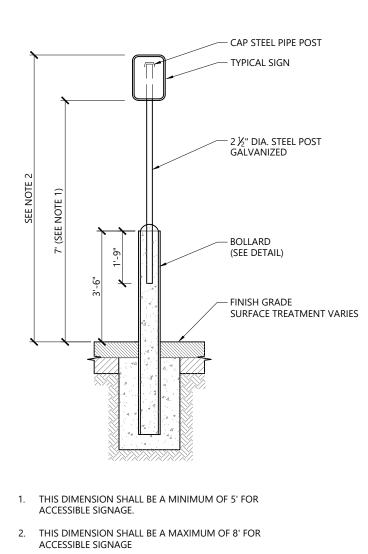
GALVANIZED

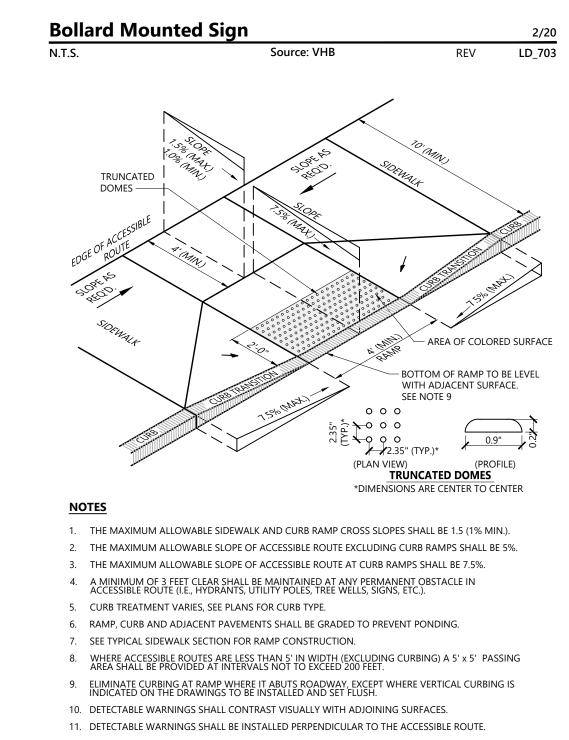
TYPICAL SIGN

ALONG BALE BARRIER (100' O.C.).

1/16

LD_657



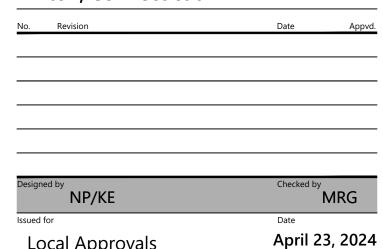


Accessible Curb Ramp (ACR) Type 'D-D'

Source: VHB

21-23 River Rd Redevelopment

21 River Road Wilton, Connecticut

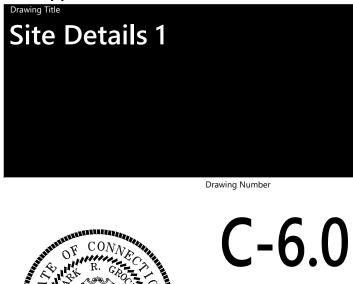


Local Approvals

12/20

LD 503

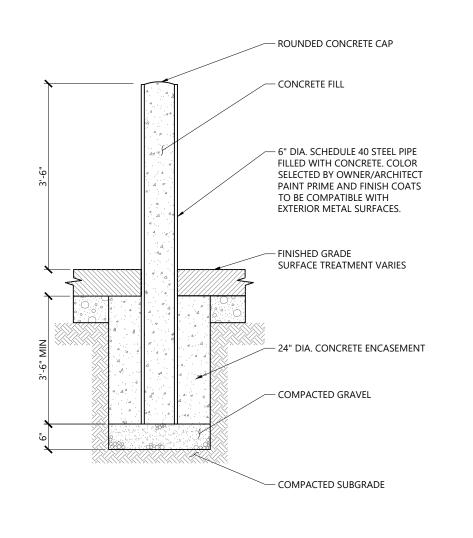
Not Approved for Construction



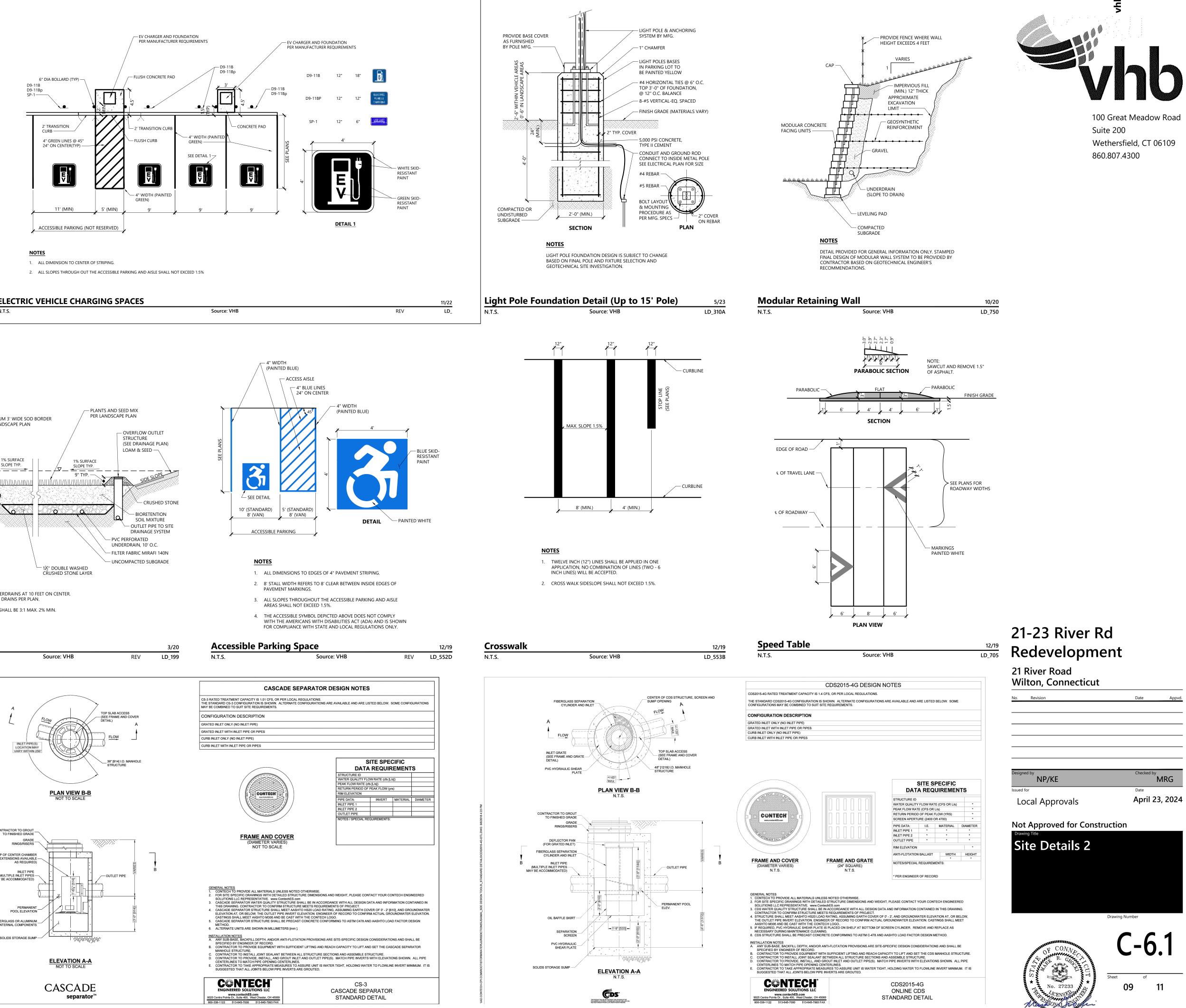
11 80

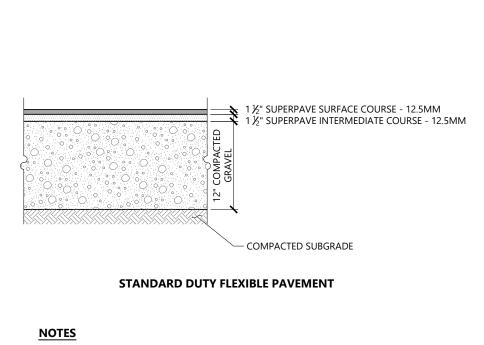
N.T.S.





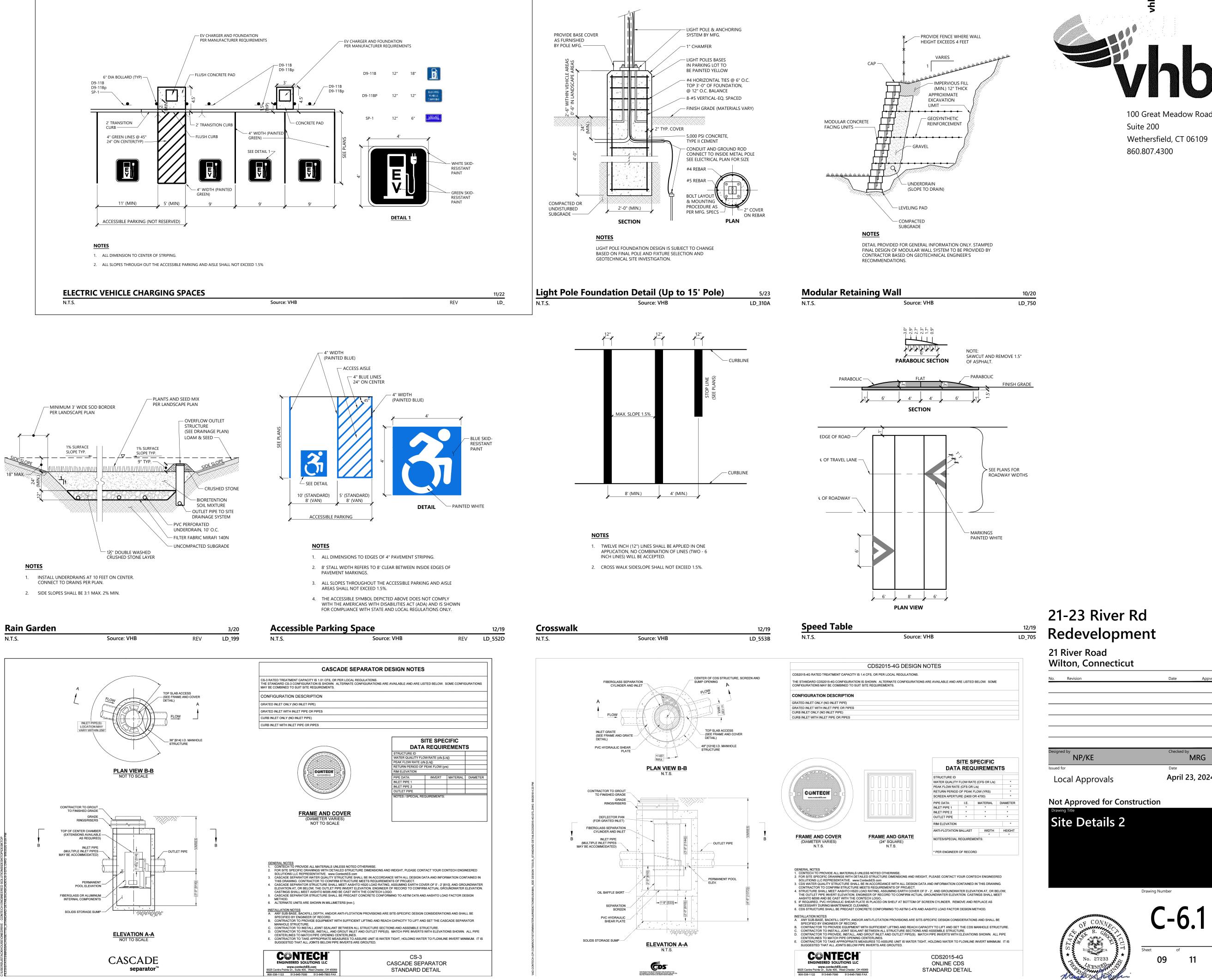


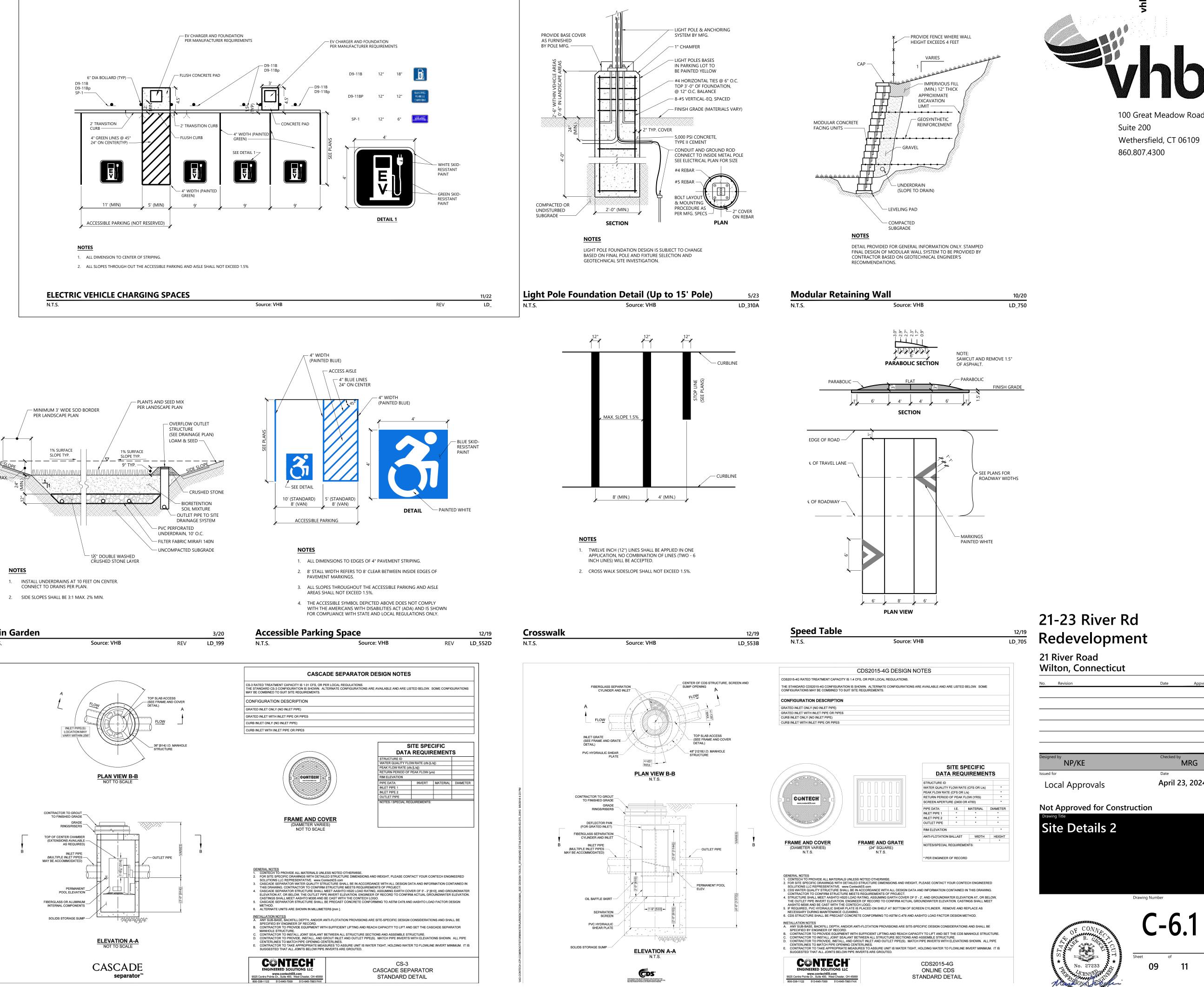




PAVEMENT SECTIONS ARE SUBJECT TO CHANGE AND WILL BE BASED ON THE RESULTS OF FURTHER GEOTECHNICAL INVESTIGATIONS.

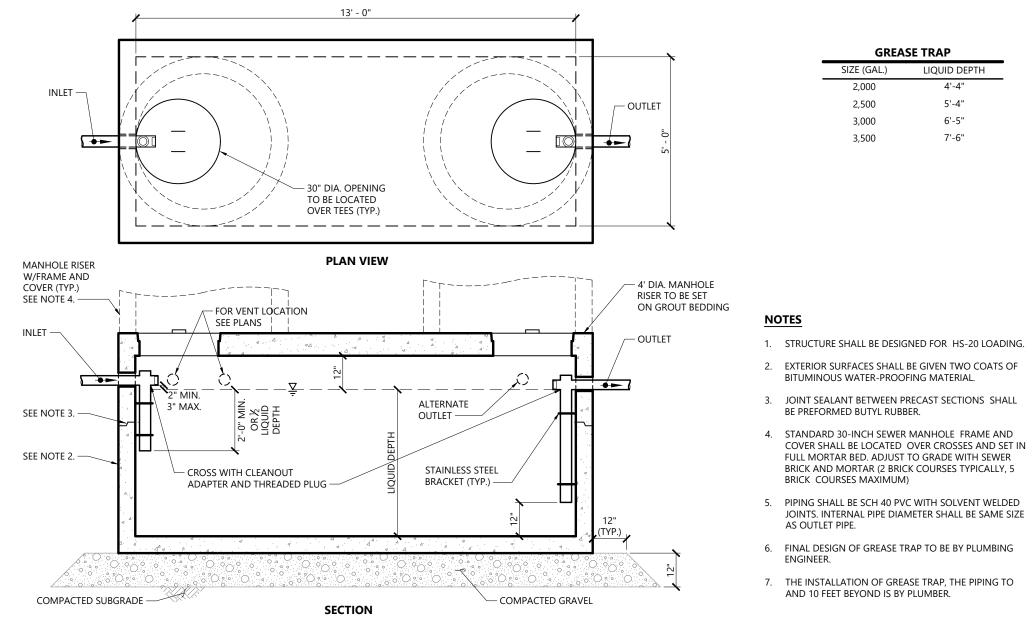
Bituminous Co	oncrete Pavement Sections		7/22
N.T.S.	Source: VHB	REV	LD_430





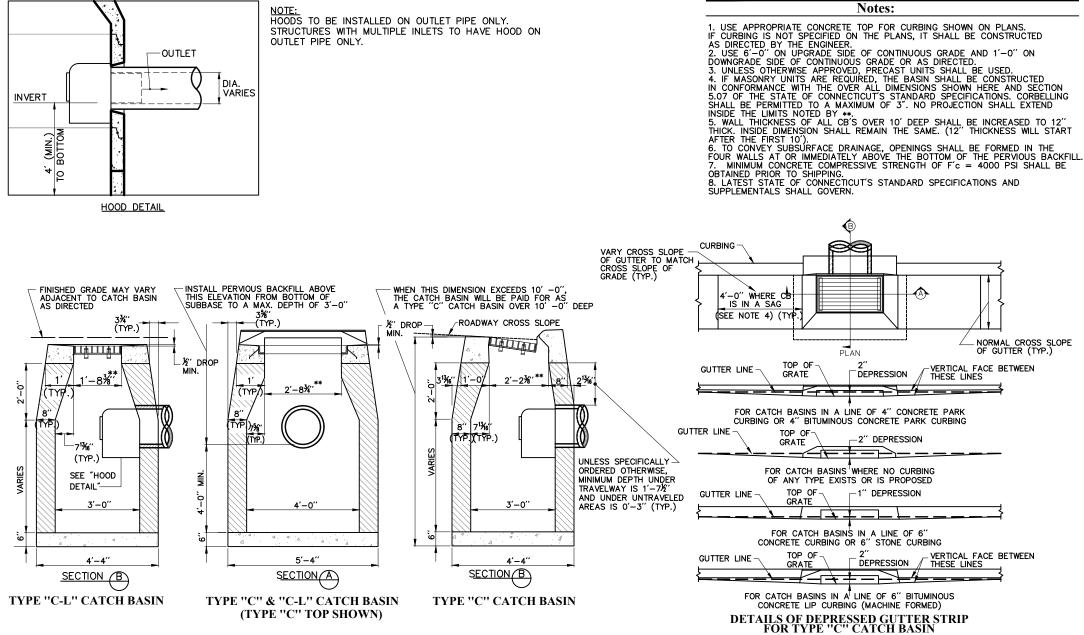
Project Number

20849.00



Source: VHB

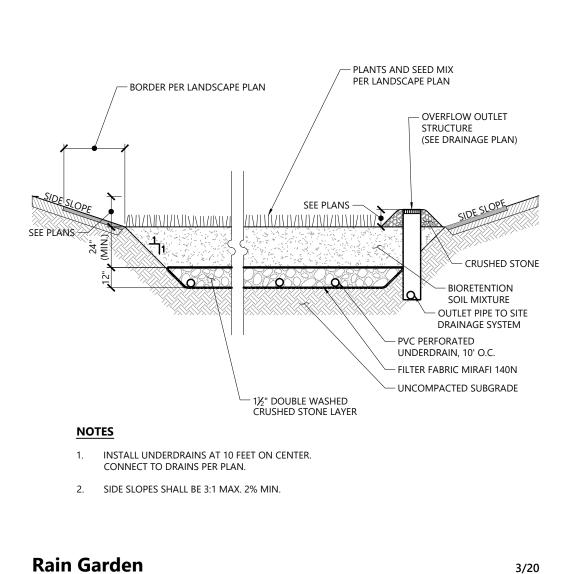




LD_199

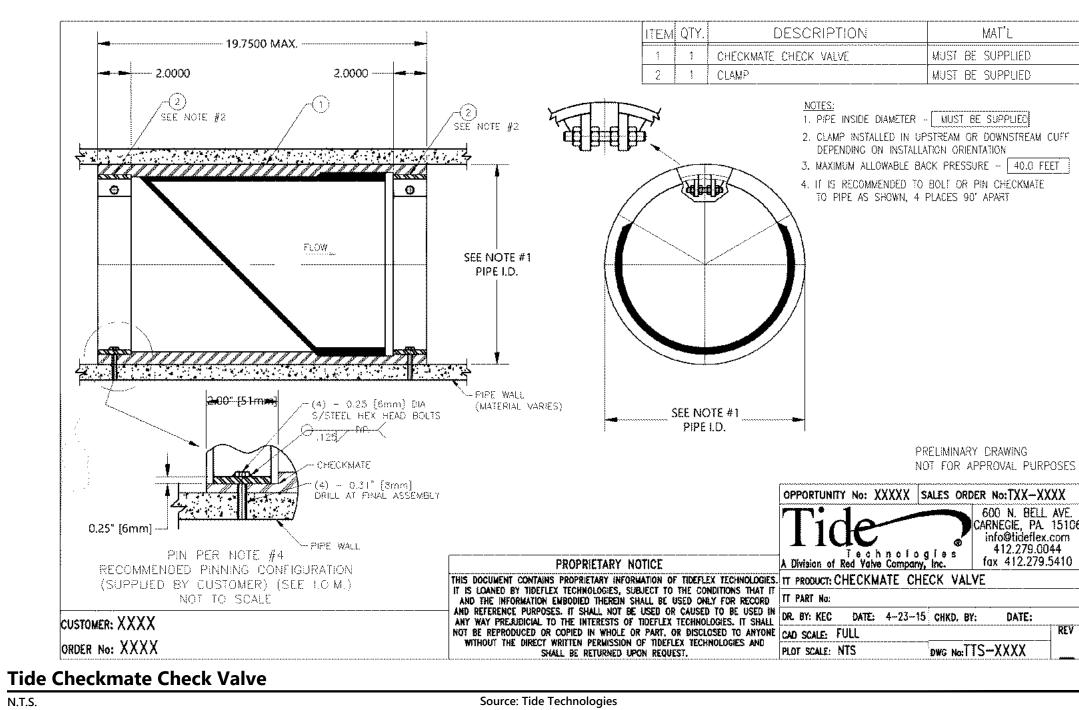
N.T.S.





Source: VHB

N.T.S.





PAVED AREA

SEE APPLICABLE

COMPACTED GRANULAR FILL —

SAWCUT -

 \leftarrow

¹⁹MN

ENGINEER.

SEE NOTE 4. —

COMPACTED GRAVEL -

1. ALL SECTIONS SHALL BE DESIGNED FOR HS-20 LOADING.

CONNECTIONS (NON-SHRINK GROUT).

2. PROVIDE DOGHOUSE OPENING FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE

3. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE PREFORMED BUTYL RUBBER.

4. CATCH BASIN FRAME AND GRATE (4"DEPTH) SHALL BE SET IN FULL MORTAR BED.

Source: VHB

5. ADJUST TO FINISH GRADE WITH CLAY BRICK AND MORTAR AS REQUIRED.

OF PIPE. TOP SLAB SHALL NOT REST DIRECTLY ON PIPE. GROUT ALL PIPE

NOTES

NOTE

Utility Trench

N.T.S.

(MIN.)

SPECIAL SECTION REQUIREMENTS.

WHERE UTILITY TRENCHES ARE CONSTRUCTED THROUGH

2. USE METALLIC TRACING/WARNING TAPE OVER ALL PIPES.

3. COMPACTED GRANULAR FILL MAY CONSIST OF GRAVEL,

Source: VHB

P00000

DETENTION BASIN BERMS OR OTHER SUCH SPECIAL SECTIONS, PLACE TRENCH BACKFILL WITH MATERIALS SIMILAR TO THE

CRUSHED STONE, SAND, OR OTHER MATERIAL AS APPROVED BY

PAVEMENT SECTION LANDSCAPED AREA

- COMMON FILL/

ORDINARY BORROW

- DEPTH AND SURFACE

HAND TAMPED HAUNCHING

11/19

1/16

LD_104

LD_300

- COMPACTED BEDDING

COMPACTED

SUBGRADE

- FINISH GRADE

SEE NOTE 3.

– DIA. VARIES

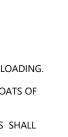
SEE NOTE 2.

- COMPACTED SUBGRADE

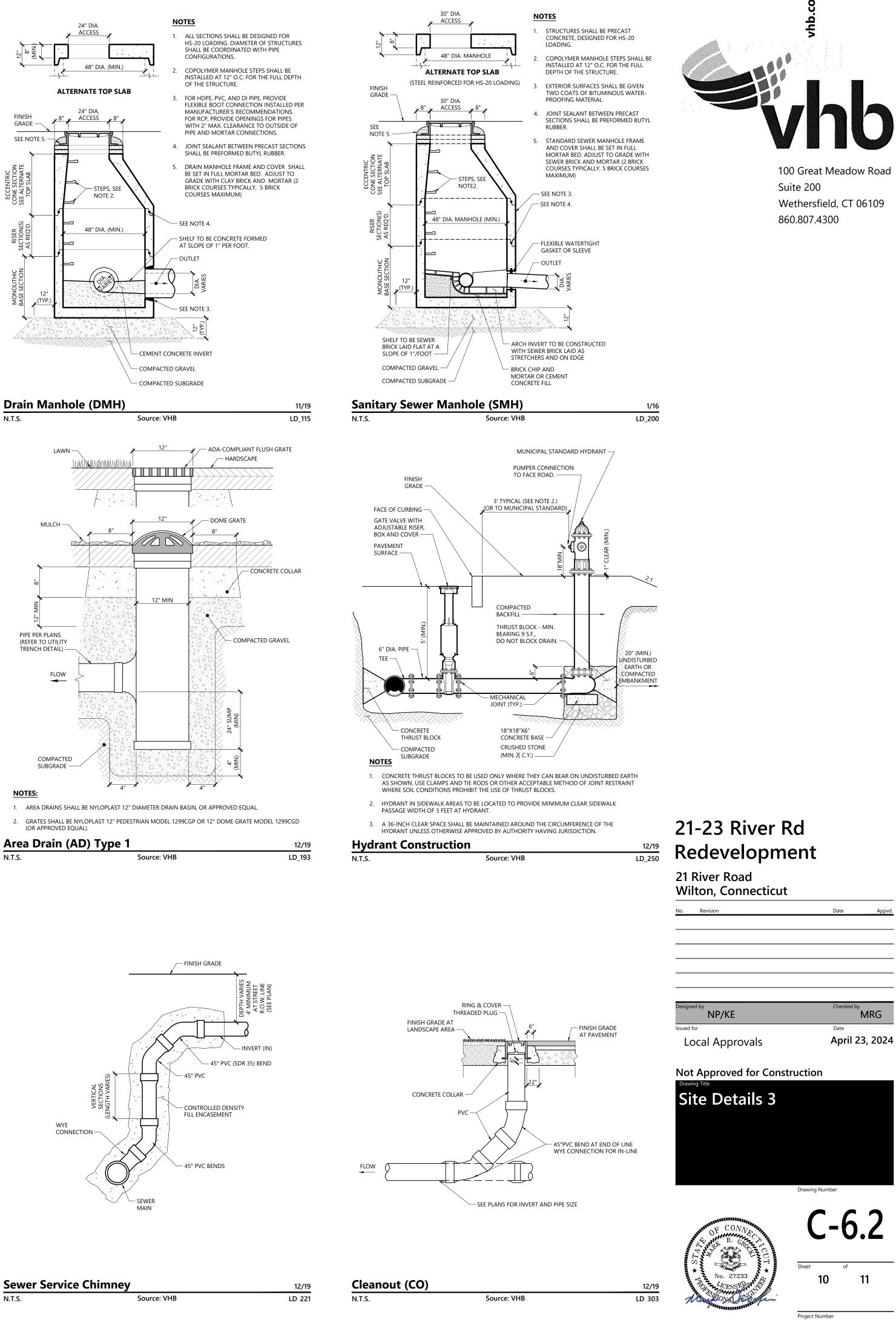
TOP OUTSIDE OF PIPE

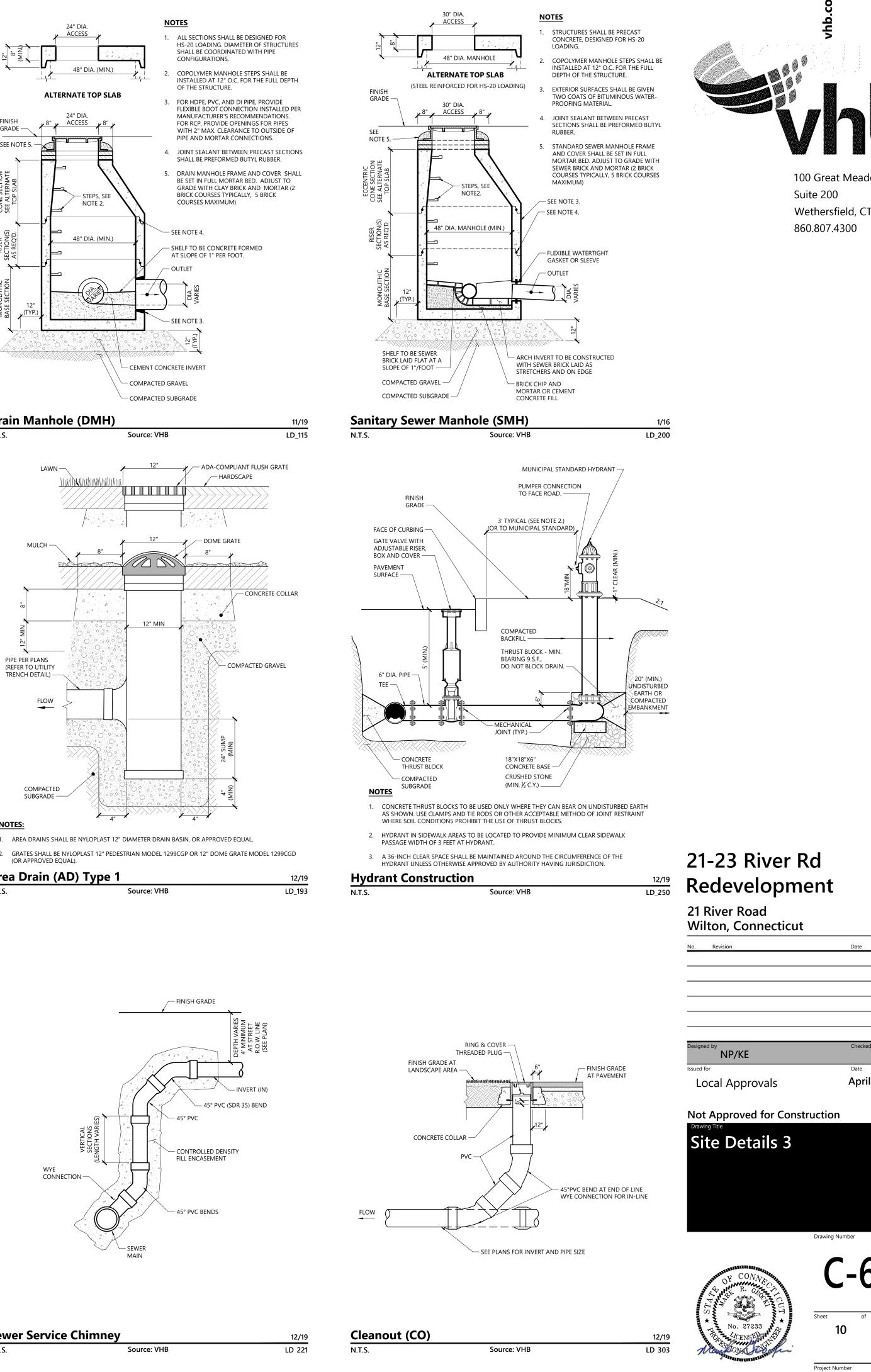
TREATMENT VARIES

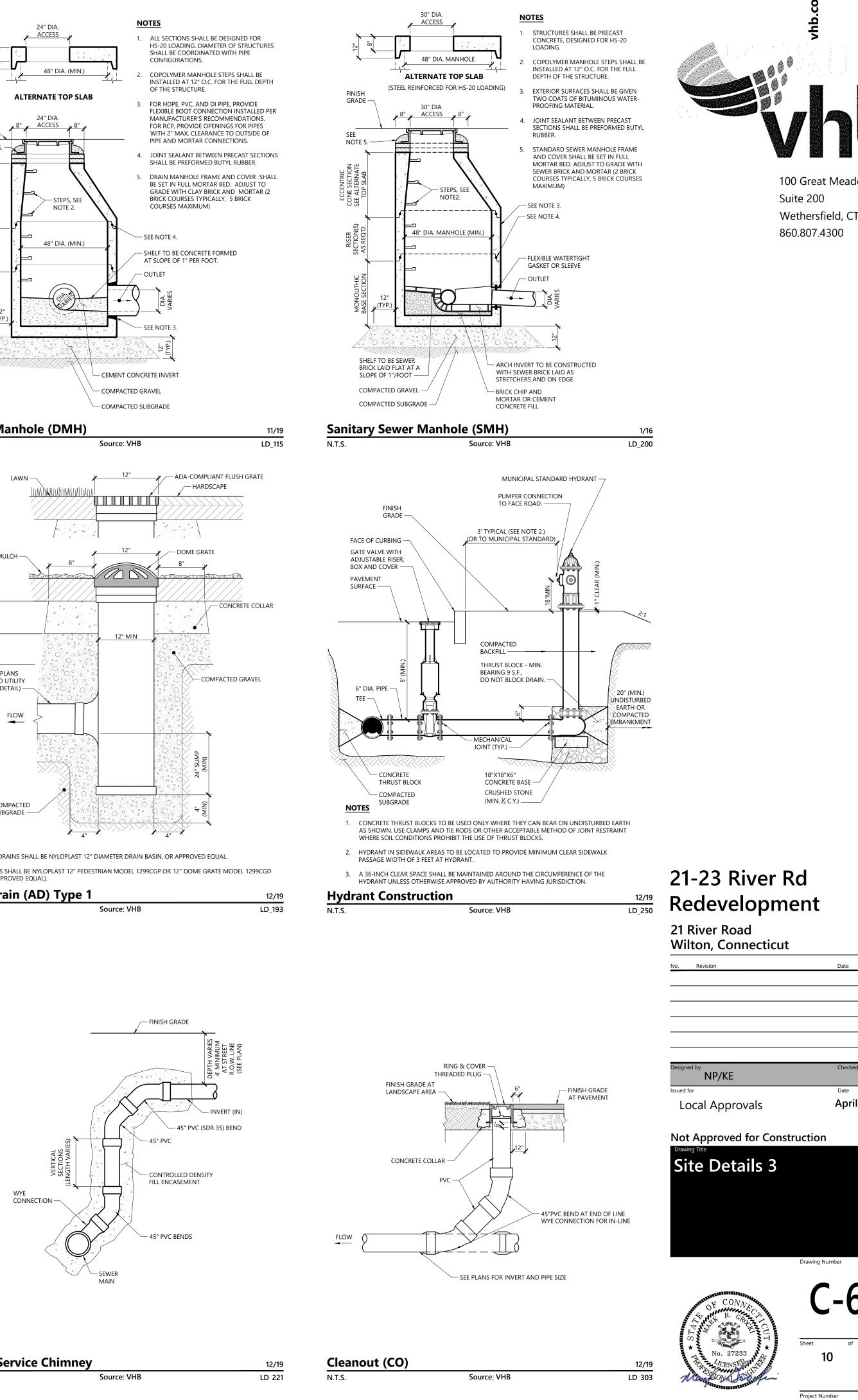
WARNING TAPE



- 12/19 LD_210
- MORMAL CROSS SLOPE OF GUTTER (TYP.)
- - Catch Basin (CB) Shallow Cover N.T.S. Source: BY OTHERS



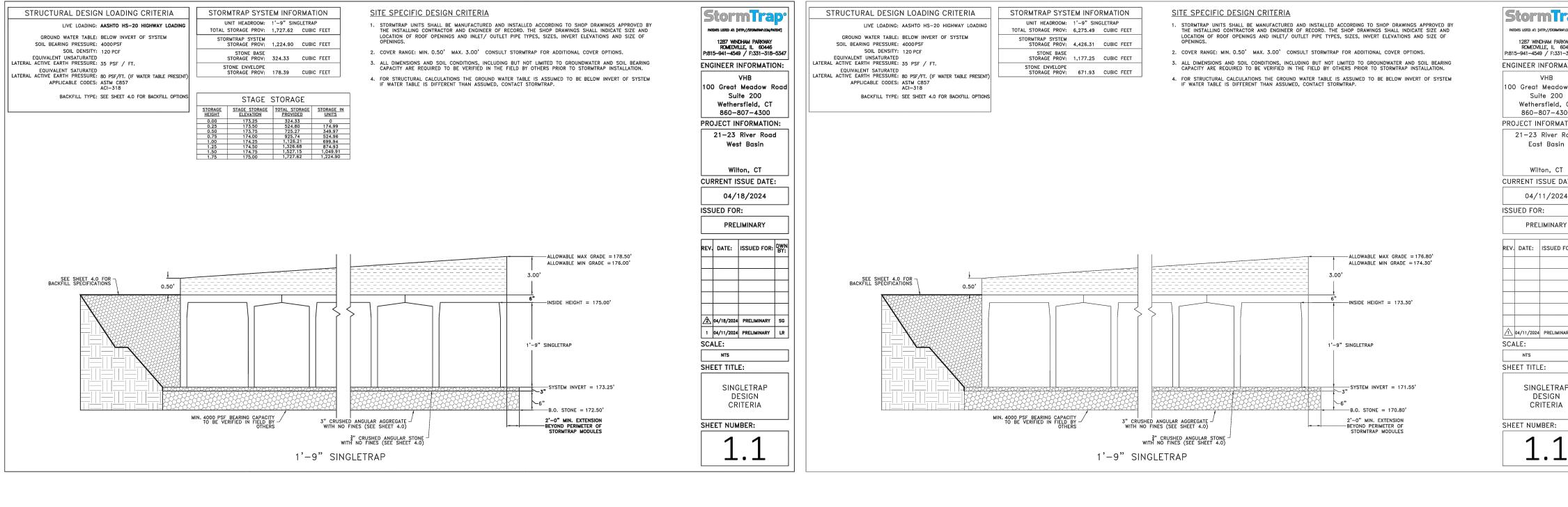


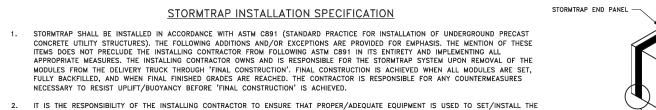


20849.00

MRG

\\vhb.com\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\cad\ld\Planset\06_20849.00DT.dwg

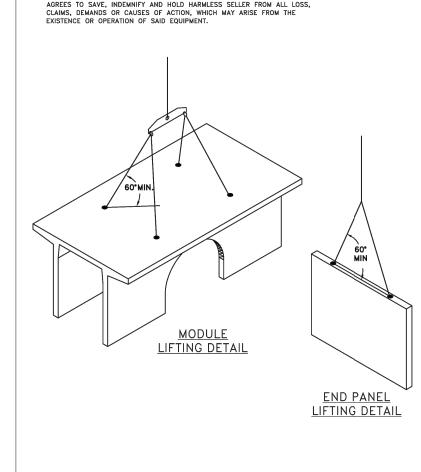




- 3. THE AGGREGATE FOUNDATION HAS BEEN DESIGNED BASED ON THE FOLLOWING ASSUMPTIONS. THESE ASSUMPTIONS WILL NEED TO BE VERIFIED BY A GEOTECHNICAL ENGINEER WHICH WILL NEED TO BE EMPLOYED BY THE OWNER.
- 3.1. A QUALIFIED GEOTECHNICAL ENGINEER WILL BE EMPLOYED, BY OWNER, TO PROVIDE ASSISTANCE IN EVALUATING THE EXISTING SOIL CONDITIONS BELOW THE PROPOSED ENGINEERED STONE FOUNDATION. IF A STONE FOUNDATION DESIGN IS TO BE USED, THE BEARING PRESSURE OF THE SOILS BELOW THE STONE WILL NEED TO MEET OR EXCEED ALLOWABLE CAPACITY. IF THIS IS NOT POSSIBLE, THE STONE FOUNDATION MAY NOT BE AN OPTION FOR THIS LOCATION.
- 3.2. A QUALIFIED GEOTECHNICAL ENGINEER WILL BE EMPLOYED, BY OWNER, TO EVALUATE A SOURCE OF STONE AGGREGATES THAT WILL BE PLACED ON PROPERLY COMPACTED SOILS (SEE SHEET 1.1 FOR SOIL BEARING CAPACITY REQUIREMENTS). THE AGGREGATE BASE COURSE (SEE NOTE 6) FOR WHICH THE STORMTRAP SYSTEM WILL BEAR DIRECTLY ON SHALL CONSIST OF A 3" THICK BED OF 3" DIAMETER ANGULAR STONE, WELL COMPACTED AND SEATED, WITH NO FINES. AND A 6" THICK BED OF 3" ANGULAR AGGREGATE (SEE SHEET 4.0 FOR FURTHER DESCRIPTION/EXPLANATION). PLEASE NOTE THAT THESE ARE ONLY MINIMUM RECOMMENDATIONS AND A QUALIFIED GEOTECHNICAL ENGINEER SHALL BE USED TO DETERMINE THE EXACT REQUIREMENTS FOR THE LOCATIONS THAT THE STORMTRAP SYSTEM IS TO BE LOCATED.
- 3.3. THE CONTRACTOR SHALL REMOVE ANY AND ALL EXPANDABLE OR COLLAPSIBLE SOILS AT THE DIRECTION OF A QUALIFIED GEOTECHNICAL
- 3.4. THE AGGREGATE FOUNDATION SHALL BE INSTALLED SUCH THAT THE AGGREGATE EXTENDS A MINIMUM OF 2'-O" PAST THE OUTSIDE OF THE SYSTEM (SEE DETAIL 1).
- 3.5. THE 🖁 AGGREGATE SHALL BE COMPACTED USING A VIBRATING ROLLER WITH ITS' FULL DYNAMIC FORCE APPLIED TO ACHIEVE A FLAT
- 3.6. DISK, DRY AND COMPACT THE TOP 8" OF THE SUBGRADE SOILS TO 95% OF THE STANDARD DRY DENSITY AND 110% OPTIMUM MOISTURE
- AGGREGATE SHALL BE GRADED WITHIN $+/-\frac{1}{2}$ of the grade shown on the plans
- 3.8. MINIMUM SOIL BEARING CAPACITY LISTED ON SHEET 1.1 SHALL BE VERIFIED IN FIELD BY OTHERS. 4. THE STORMTRAP MODULES SHALL BE PLACED SUCH THAT THE MAXIMUM SPACE BETWEEN ADJACENT MODULES DOES NOT EXCEED ⅔" (SEE DETAIL 2). IF THE SPACE EXCEEDS ≹", THE MODULES SHALL BE RESET WITH APPROPRIATE ADJUSTMENT MADE TO LINE AND GRADE TO BRING
- THE SPACE INTO SPECIFICATION. 5. STORMTRAP MODULES ARE NOT WATERTIGHT. IF A WATERTIGHT SOLUTION IS REQUIRED, CONTACT STORMTRAP FOR RECOMMENDATIONS. THE WATERTIGHT APPLICATION IS TO BE PROVIDED AND IMPLEMENTED BY THE CONTRACTOR. THE CONTRACTOR IS RESPONSIBLE TO ENSURE THAT THE SELECTED WATERTIGHT SOLUTION PERFORMS AS SPECIFIED BY THE MANUFACTURER.
- 6. ALL EXTERIOR ROOF AND EXTERIOR VERTICAL WALL JOINTS BETWEEN ADJACENT STORMTRAP MODULES SHALL BE SEALED WITH 8" WIDE PRE-FORMED, COLD-APPLIED, SELF-ADHERING ELASTONERIC RESIN, BONDED TO A WOVEN, HIGHLY PUNCTURE RESISTANT POLYMER WRAP, CONFORMING TO ASTM C891 AND SHALL BE INTEGRATED WITH PRIMER SEALANT AS APPROVED BY STORWTRAP (SEE DETAILS 2, 3, & 4). THE JOINT WRAP DOES NOT PROVIDE A WATERTIGHT SEAL. THE SOLE PURPOSE OF THE JOINT WRAP IS TO PROVIDE A SILT AND SOIL TIGHT SYSTEM. THE ADHESIVE EXTERIOR JOINT WRAP SHALL BE INSTALLED ACCORDING TO THE FOLLOWING INSTALLATION INSTRUCTIONS:
- 6.1. USE A BRUSH OR WET CLOTH TO THOROUGHLY CLEAN THE OUTSIDE SURFACE AT THE POINT WHERE THE JOINT WRAP IS TO BE APPLIED. 6.2. A RELEASE PAPER PROTECTS THE ADHESIVE SIDE OF THE JOINT WRAP. PLACE THE ADHESIVE TAPE (ADHESIVE SIDE DOWN) AROUND THE STRUCTURE, REMOVING THE RELEASE PAPER AS YOU GO. PRESS THE JOINT WRAP FIRMLY AGAINST THE STORMTRAP MODULE SURFACE WHEN APPLYING.
- 7. IF THE CONTRACTOR NEEDS TO CANCEL ANY SHIPMENTS, THEY MUST DO SO 48 HOURS PRIOR TO THEIR SCHEDULED ARRIVAL AT THE JOB SITE. IF CANCELED AFTER THAT TIME, PLEASE CONTACT THE PROJECT MANAGER.
- 8. IF THE STORMTRAP MODULE(S) IS DAMAGED IN ANY WAY PRIOR, DURING, OR AFTER INSTALL, STORMTRAP, MUST BE CONTACTED IMMEDIATELY
- TO ASSESS THE DAMAGE AND TO DETERMINE WHETHER OR NOT THE MODULE(S) WILL NEED TO BE REPLACED. IF ANY MODULE ARRIVES AT THE JOBSITE DAMAGE DO NOT UNLOAD IT; CONTACT STORMTRAP, IMMEDIATELY. ANY DAMAGE NOT REPORTED BEFORE THE TRUCK IS UNLOADED WILL BE THE CONTRACTOR'S RESPONSIBILITY. 9. STORMTRAP MODULES CANNOT BE ALTERED IN ANY WAY AFTER MANUFACTURING WITHOUT WRITTEN CONSENT FROM STORMTRAP.



- CHAINS/CABLES ARE SECURED PROPERLY TO THE LIFTING ANCHORS AND IN EQUAL TENSION WHEN LIFTING THE STORWTRAP MODULE.
- MINIMUM 7'-0" CHAIN/CABLE LENGTH TO BE USED TO LIFT STORMTRAP MODULES (SUPPLIED BY CONTRACTOR).
- CONTRACTOR TO ENSURE MINIMUM LIFTING ANGLE IS 60° FROM TOP SURFACE OF STORMTRAP MODULE. SEE DETAIL. IT IS UNDERSTOOD AND AGREED THAT AT ALL TIMES DURING WHICH HOISTING AND RIGGING EQUIPMENT IS BEING SUPPLIED TO THE PURCHASER, OPERATOR OF SUCH EQUIPMENT SHALL BE IN CHARGE OF HIS ENTIRE EQUIPMENT AND SHALL AT ALL TIMES BE THE JUDGE OF THE SAFETY AND PROPERTY OF ANY SUGGESTION TO HIM FROM THE SELLER, ITS AGENTS OR EMPLOYEES. PURCHASER AGREES TO SAVE, INDEMNIFY AND HOLD HARMLESS SELLER FROM ALL LOSS, CLAIMS, DEMANDS OR CAUSES OF ACTION, WHICH MAY ARISE FROM THE EXISTENCE OR OPERATION OF SAID EQUIPMENT.



- END PANEL ERECTION/INSTALLATION SPECIFICATION
- 1. END PANELS WILL BE SUPPLIED TO CLOSE OFF OPEN ENDS OF ROWS.

DETAIL 4

TOP OF STORMTRAP -

₹" GAP MAX. (SEE NOTE 4)

DETAIL 2

2. PANELS SHALL BE INSTALLED IN A TILT UP FASHION DIRECTLY ADJACENT TO OPEN END OF MODULE (REFER TO SHEET 2.0 FOR END PANEL LOCATIONS)

8" WIDE JOINT WRAP — (SEE NOTE 6)

STORMTRAP MODULE -

DETAIL 1

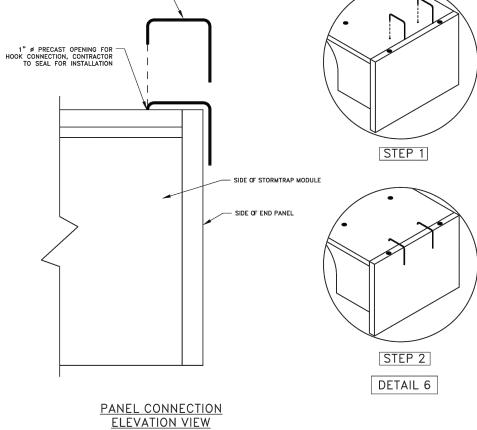
DETAIL 3

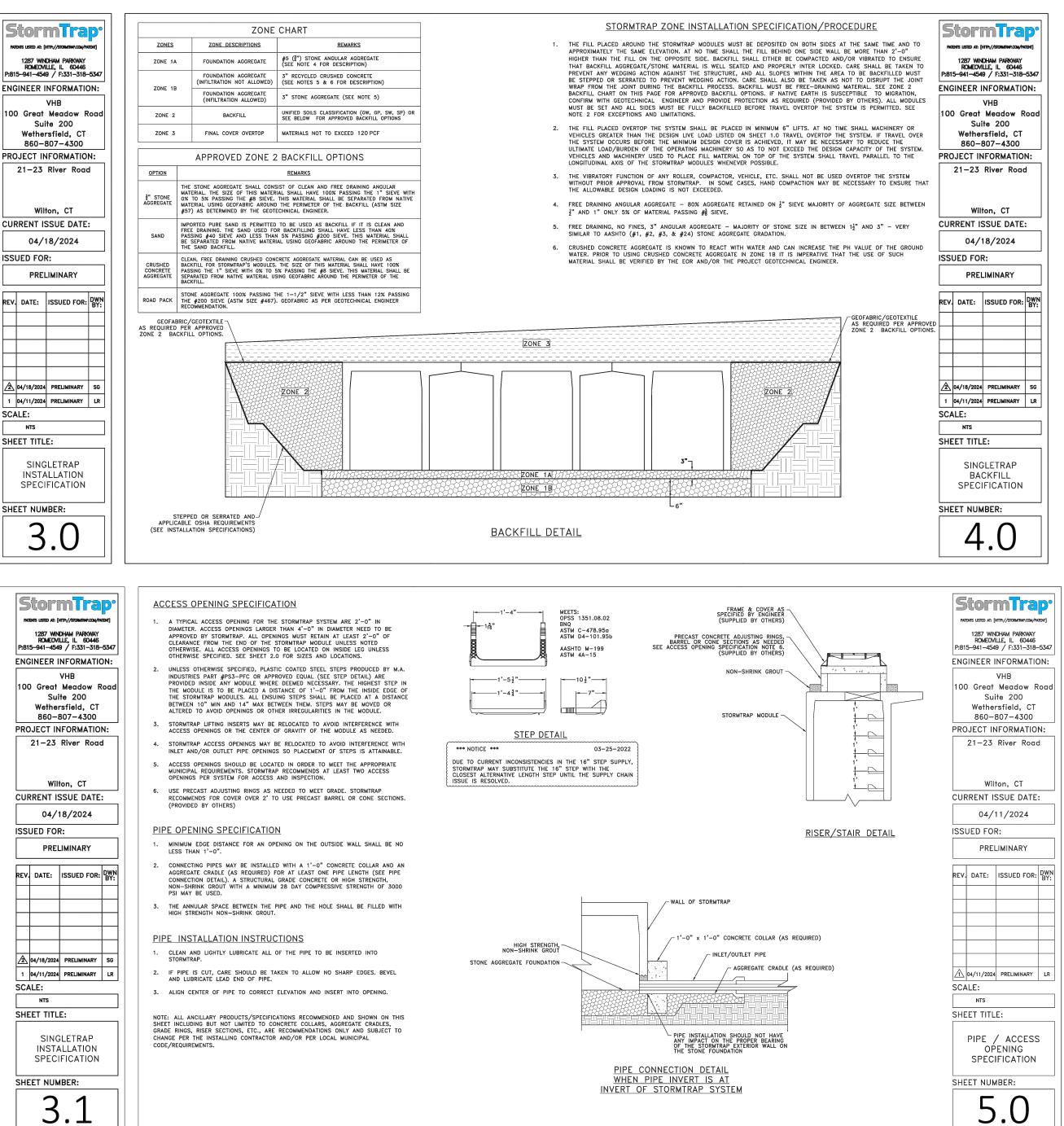
- EXTERIOR WALL OF STORMTRAP

GGREGATE BASE

2'-0" OVERHANG (SEE NOTE 3)

- CONNECTION HOOKS WILL BE SUPPLIED WITH END PANELS TO SECURELY CONNECT PANEL TO ADJACENT STORMTRAP MODULE (SEE PANEL CONNECTION ELEVATION VIEW).
- 4. ONCE CONNECTION HOOK IS ATTACHED, LIFTING CLUTCHES MAY BE REMOVED.
- 5. JOINT WRAP SHALL BE PLACED AROUND PERIMETER JOINT PANEL (SEE SHEET 3.0). CONNECTION HOOKS PROVIDED BY STORMTRAP AND INSTALLED BY CONTRACTOR (SEE DETAIL 6)





3.⊥

	mTrap [•]
ed at: [H	ITTP://STORMIRAP.COM/PATENT]
MEOVI	DHAM PARKWAY LLE, IL 60446 9 / F:331-318-5347
ER I	NFORMATION:
	VHB
	Meadow Road te 200
ther	sfield, CT
60-8	307-4300
t in	FORMATION:
23	River Road
Eas	t Basin
Wilt	on, CT
IT IS	SUE DATE:
4/1	1/2024
FOF	:
REL	IMINARY
Έ:	ISSUED FOR: DWN BY:

/2024	PRELIMINARY	LR	

S
TITLE:
INGLETRAP DESIGN CRITERIA
NUMBER:
1 1



100 Great Meadow Road Suite 200 Wethersfield, CT 06109 860.807.4300

21-23 River Rd Redevelopment

21 River Road Wilton, Connecticut

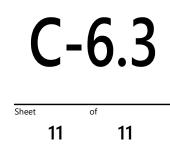
No.	Revision	Date	Appvd.
Design	ed by	Checked by	
	NP/KE	N	/IRG
ssued	for	Date	

Local Approvals

Not Approved for Construction

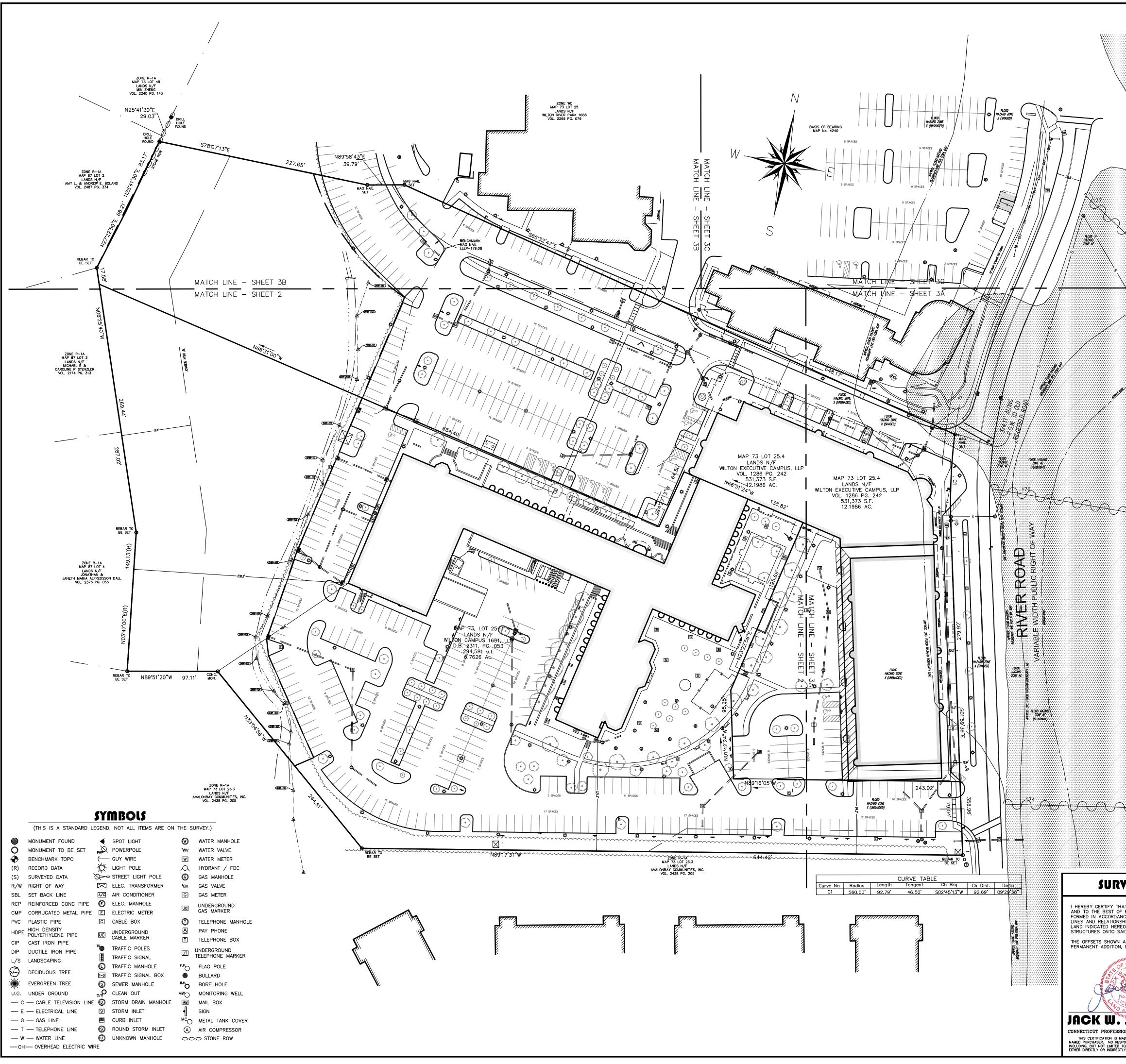
Site Details 4

Drawing Number

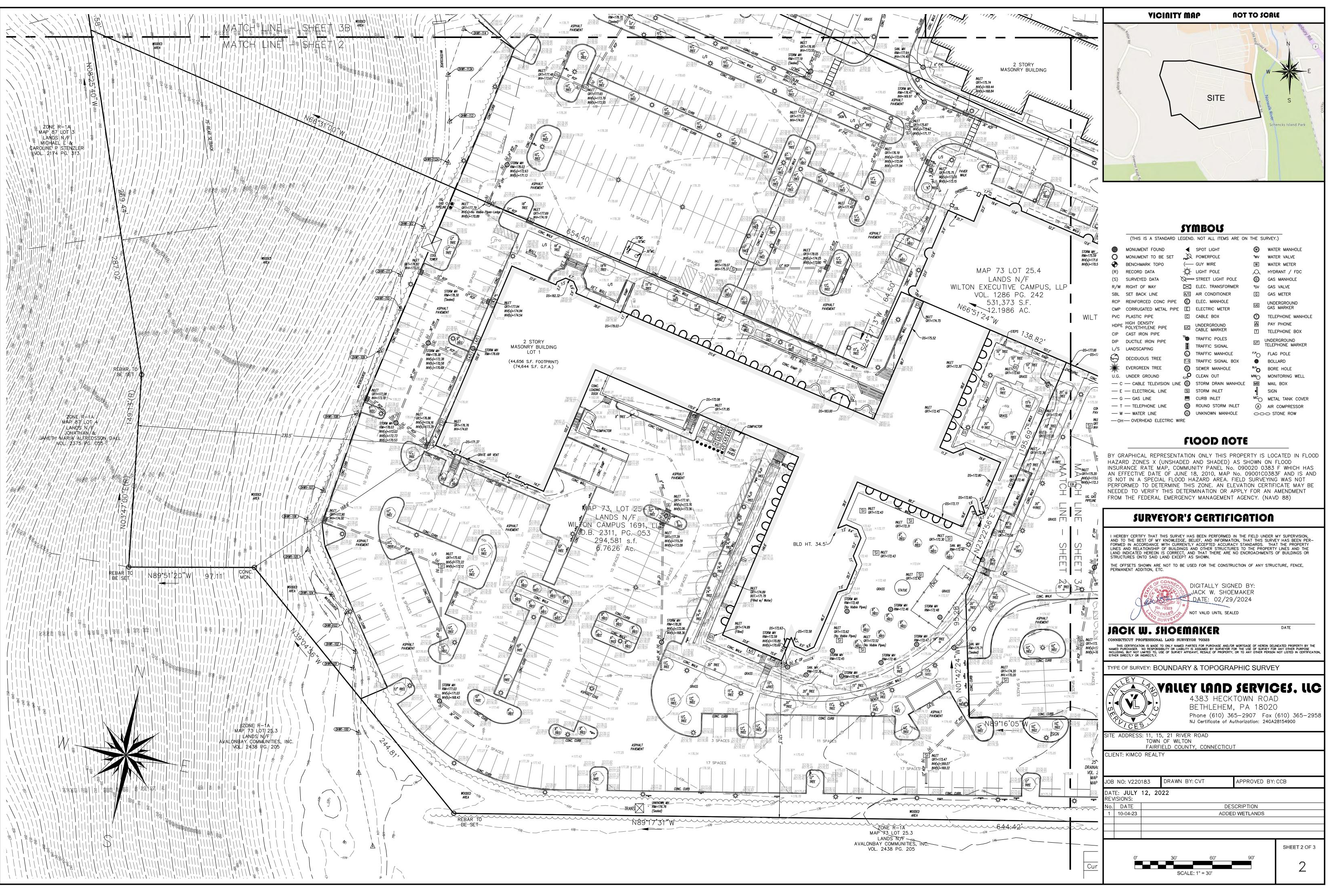


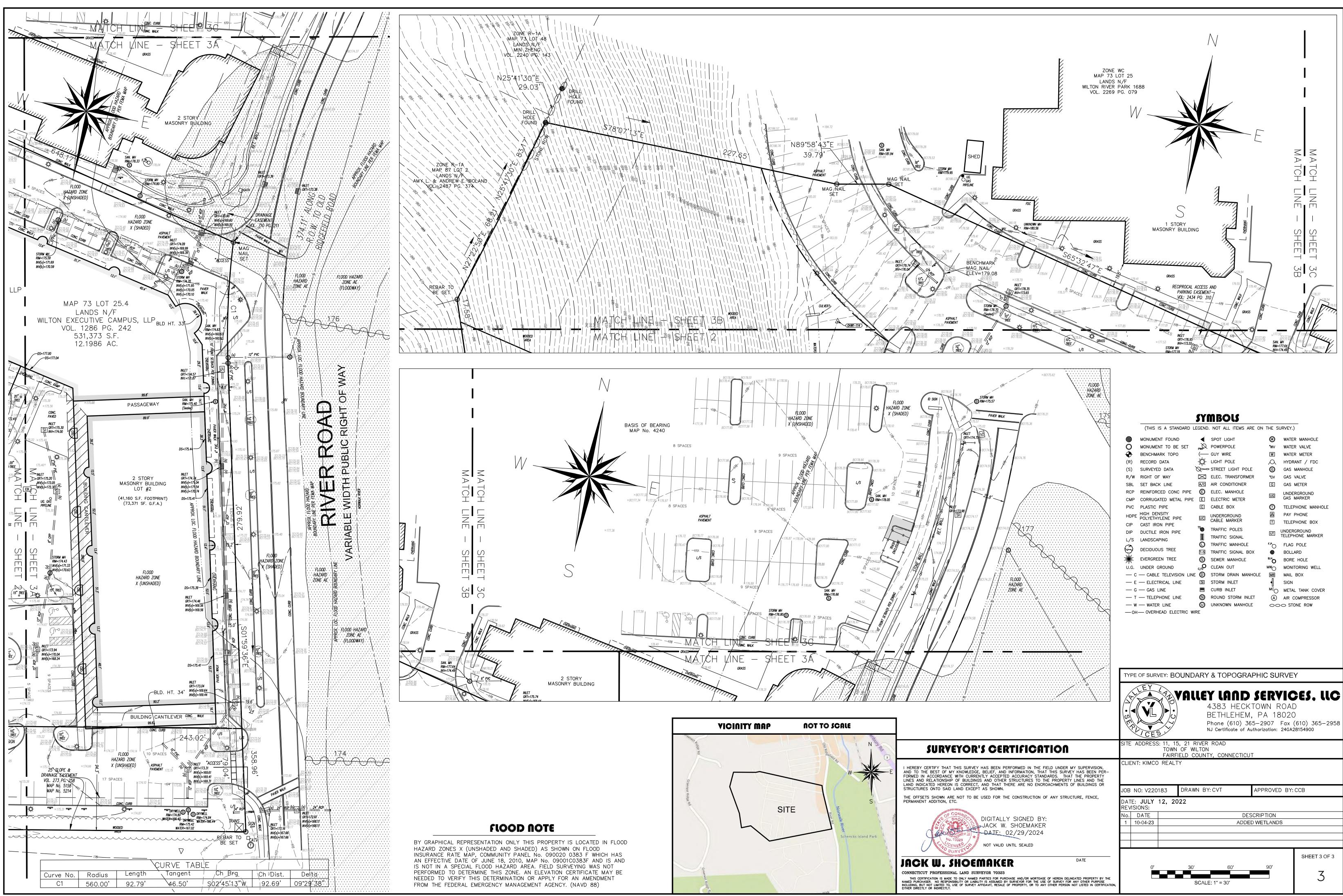
April 23, 2024

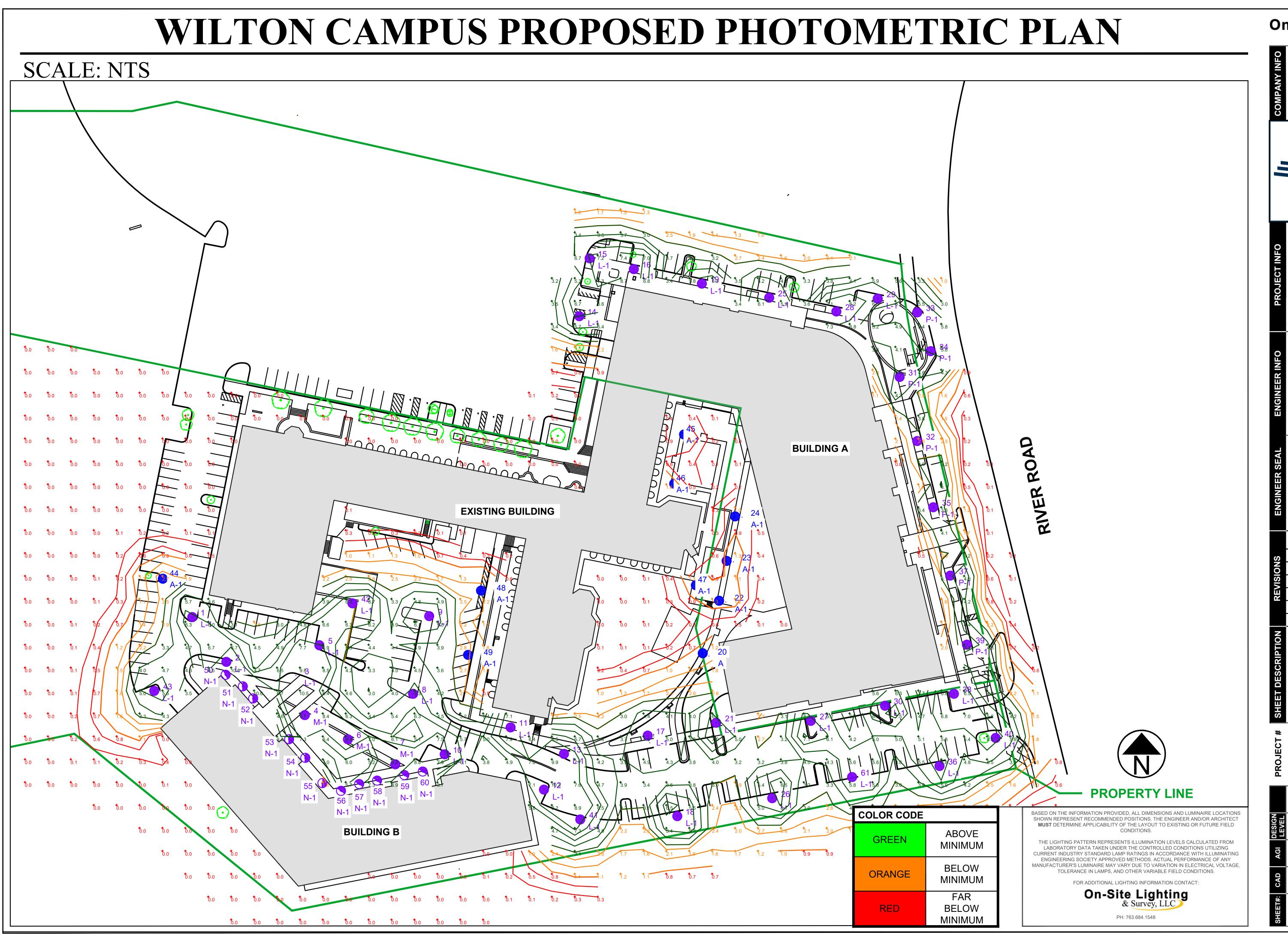
Project Number 20849.00



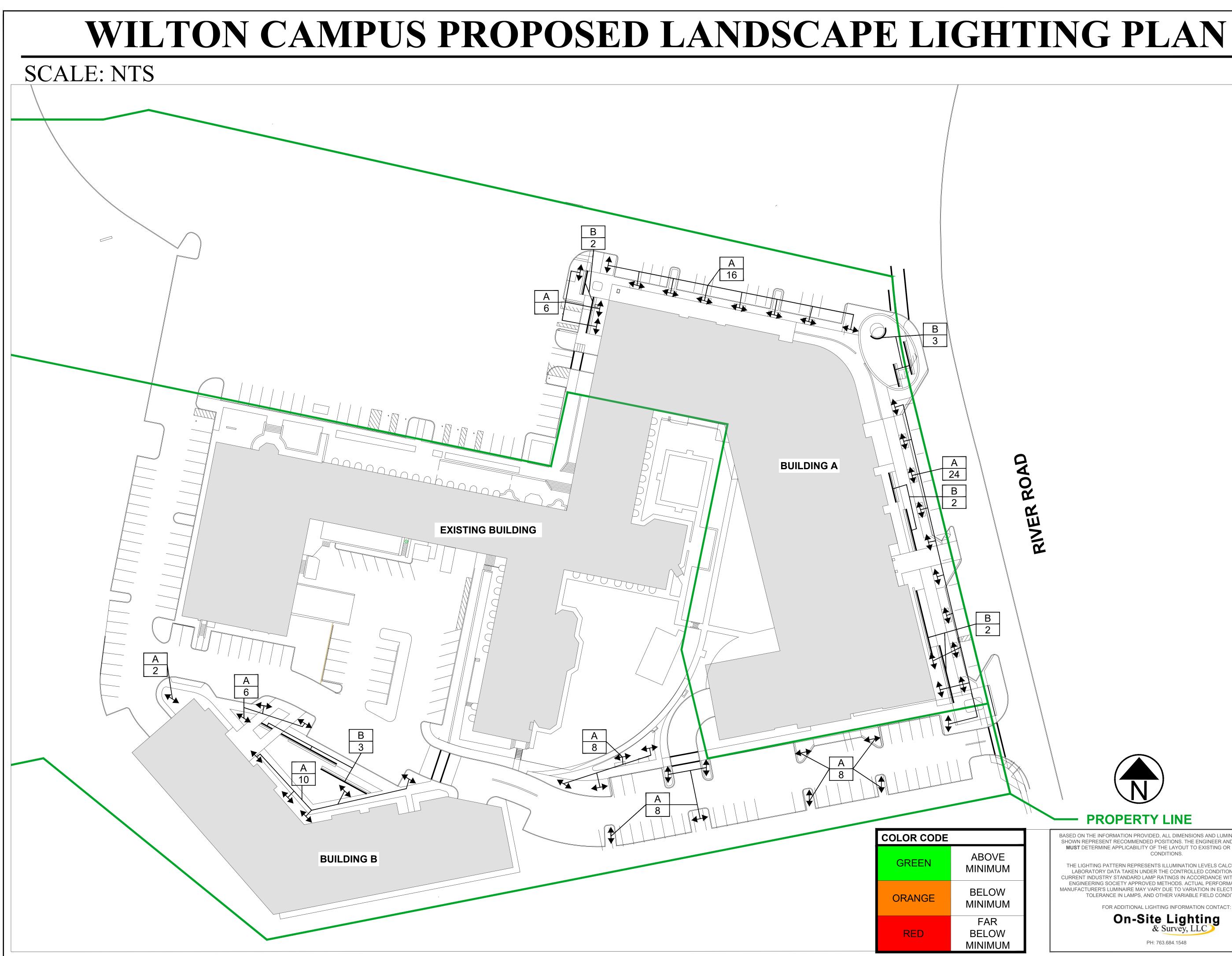
λ.,	VICINITY MAP NOT TO SCALE
	N MARINE O
9000 HACHOP 12040	W E
	SITE Sthencks Island Park
FLOOD HAZARD ZONE X (SHADED)	
S	SITE DATA1.PROPERTY IS KNOWN AS MAP #73, LOT 25.1 & MAP #73, LOT 25.4 IN THE
	 TOWN OF WILTON, FAIRFIELD COUNTY, CONNECTICUT. 2. LOT AREA 25.1 = 236,792 S.F. OR 5.4360 AC. LOT AREA 25.4 = 294,581 S.F. OR 6.7627 AC.
∇	 NO CHANGES IN STREET RIGHT OF WAY LINES EITHER COMPLETED OR PROPOSED KNOWN TO THIS SURVEYOR. NO OBSERVABLE EVIDENCE OF RECENT STREET OR SIDEWALK CONSTRUCTION OR REPAIRS. VERTICAL DATUM = NAVD 88. BENCHMARK – MAG NAIL, ELEV.=179.08
	5. LOCATION OF ALL UNDERGROUND UTILITIES ARE APPROXIMATE. ALL LOCATIONS AND SIZES ARE BASED ON UTILITY MARK-OUTS, ABOVE GROUND
	STRUCTURES THAT WERE VISIBLE & ACCESSIBLE IN THE FIELD, AND THE MAPS LISTED IN THE REFERENCES AVAILABLE AT THE TIME OF THE SURVEY. AVAILABLE AS-BUILT PLANS AND UTILITY MARK-OUT DOES NOT ENSURE MAPPING OF ALL UNDERGROUND UTILITIES AND STRUCTURES. BEFORE ANY EXCAVATION IS TO BEGIN, ALL UNDERGROUND UTILITIES SHOULD BE VERIFIED AS TO THEIR LOCATION, SIZE AND TYPE BY THE PROPER UTILITY COMPANIES.
	6. THIS PLAN WAS PREPARED WITHOUT THE BENEFIT OF A TITLE REPORT. THIS PROPERTY MAY BE SUBJECT TO RESTRICTIONS, COVENANTS AND/OR EASEMENTS, WRITTEN OR IMPLIED.
	7. THE EXISTENCE OF UNDERGROUND STORAGE TANKS, IF ANY, WAS NOT KNOWN AT THE TIME OF THIS SURVEY.
	 8. TOPOGRAPHIC INFORMATION SHOWN HEREON TAKEN FROM GROUND SURVEY PERFORMED BY VALLEY LAND SERVICES, LLC. DATE OF FIELD SURVEY = 7-5-2022. 9. THIS PLAN IS VALID ONLY WHEN SIGNED IN COLORED INK AND EMBOSSED
	WITH A RAISED IMPRESSION SEAL AND WAS PREPARED IN ACCORDANCE WITH THE MINIMUM STANDARD OF ACCURACY OF THE STATE IN WHICH THE PROJECT IS LOCATED.
	10. THE WORD "CERTIFY" OR "CERTIFICATE" AS SHOWN AND USED HEREON MEANS AN EXPRESSION OF PROFESSIONAL OPINION REGARDING THE FACTS OF THIS SURVEY AND DOES NOT CONSTITUTE A WARRANTY OR GUARANTEE, EXPRESSED OR IMPLIED.
	11. COPYRIGHT © 2022, VALLEY LAND SERVICES, LLC. ALL RIGHTS RESERVED. NO PART OF THIS DRAWING MAY BE REPRODUCED BY PHOTOCOPYING, RECORDING OR BY ANY OTHER MEANS, OR STORED, PROCESSED, OR TRANSMITTED IN OR BY ANY COMPUTER OR OTHER SYSTEMS WITHOUT THE PRIOR WRITTEN PERMISSION OF THE SURVEYOR. COPIES OF THIS PLAN WITHOUT A RAISED IMPRESSION SEAL ARE NOT VALID.
	12. PARKING PROVIDED – -REGULAR = 480 SPACES -UNDERGROUND = 17 SPACES -HANDICAP = 10 SPACES TOTAL SPACES PROVIDED = 507
	13. THIS SURVEY CONFORMS TO A CLASS A-2 SURVEY AND HAS BEEN PREPARED IN ACCORDANCE WITH THE "RECOMMENDED STANDARDS FOR SURVEYS AND MAPS IN THE STATE OF CONNECTICUT" AS ADOPTED BY THE CONNECTICUT ASSOCIATION OF LAND SURVEYORS, INC., ON OCTOBER 26, 2018.
	14. THE TYPE OF SURVEY PERFORMED IS A PROPERTY SURVEY.15. BOUNDARY DETERMINATION IS BASED UPON A DEPENDENT RESURVEY AND THIS SURVEY IS SUBJECT TO SUCH FACTS AS AN INDEPENDENT RESURVEY MAY DISCLOSE.
	16. WETLANDS AS SHOWN ARE BASED ON DATA SUPPLIED BY VHB ENGINEERS UTILIZING A TRIMBLE R1 MODEL 99133 GPS UNIT RECORDED ON $9-1-2022$.
	FLOOD NOTE
	BY GRAPHICAL REPRESENTATION ONLY THIS PROPERTY IS LOCATED IN FLOOD HAZARD ZONES X (UNSHADED AND SHADED) AS SHOWN ON FLOOD INSURANCE RATE MAP, COMMUNITY PANEL No. 090020 0383 F WHICH HAS AN EFFECTIVE DATE OF JUNE 18, 2010, MAP No. 09001C0383F AND IS AND IS NOT IN A SPECIAL FLOOD HAZARD AREA. FIELD SURVEYING WAS NOT PERFORMED TO DETERMINE THIS ZONE. AN ELEVATION CERTIFICATE MAY BE
	NEEDED TO VERIFY THIS DETERMINATION OR APPLY FOR AN AMENDMENT FROM THE FEDERAL EMERGENCY MANAGEMENT AGENCY. (NAVD 88)
	TYPE OF SURVEY: BOUNDARY & TOPOGRAPHIC SURVEY
	4383 HECKTOWN ROAD
	4303 HECKTOWN ROAD BETHLEHEM, PA 18020 Phone (610) 365–2907 Fax (610) 365–2958 NJ Certificate of Authorization: 24GA28154900
EYOR'S CERTIFICATION	SITE ADDRESS: 11, 15, 21 RIVER ROAD TOWN OF WILTON FAIRFIELD COUNTY, CONNECTICUT
T THIS SURVEY HAS BEEN PERFORMED IN THE FIELD UNDER MY SUPERVISION, MY KNOWLEDGE, BELIEF, AND INFORMATION, THAT THIS SURVEY HAS BEEN PER CE WITH CURRENTLY ACCEPTED ACCURACY STANDARDS. THAT THE PROPERTY HP OF BUILDINGS AND OTHER STRUCTURES TO THE PROPERTY LINES AND THE NUMBER OF DEPEND	CLIENT: KIMCO REALTY
ON IS CORRECT, AND THAT THERE ARE NO ENCROACHMENTS OF BUILDINGS OR D LAND EXCEPT AS SHOWN. ARE NOT TO BE USED FOR THE CONSTRUCTION OF ANY STRUCTURE, FENCE, ETC.	JOB NO: V220183 DRAWN BY: CVT APPROVED BY: CCB DATE: JULY 12, 2022 REVISIONS:
DIGITALLY SIGNED BY: JACK W. SHOEMAKER DATE: 02/29/2024	No. DATE DESCRIPTION 1 10-04-23 ADDED WETLANDS
NOT VALID UNTIL SEALED	
SHOEMAKER DATE	- SHEET 1 OF 3
	0' 50' 100' 150'

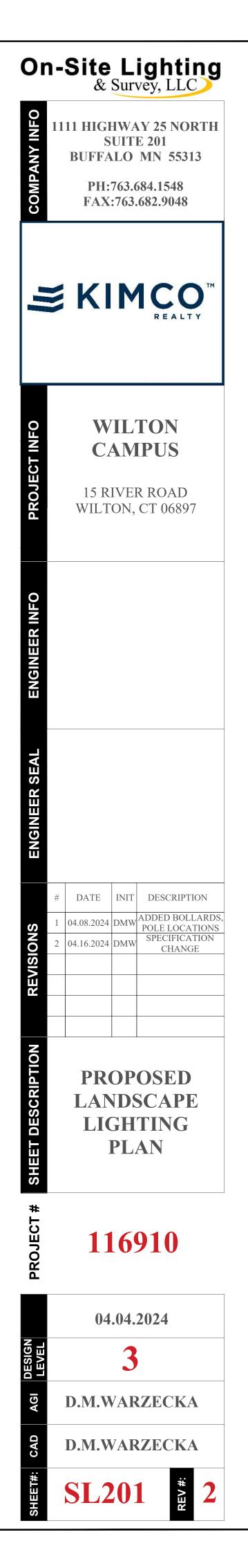






Or	-Site Lighting & Survey, LLC						
COMPANY INFO	1111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048						
11.	€ KIMCO REALTY						
PROJECT INFO	WILTON CAMPUS 15 RIVER ROAD WILTON, CT 06897						
ENGINEER INFO							
ENGINEER SEAL							
	 # DATE INIT DESCRIPTION 1 04.08.2024 DMW ADDED BOLLARDS, DOL 5 L OCATIONS 						
REVISIONS	1 04.03.2024 DMW POLE LOCATIONS 2 04.16.2024 DMW SPECIFICATION CHANGE						
REVI							
SHEET DESCRIPTION	PROPOSED PHOTOMETRIC PLAN						
PROJECT #	116910						
	04.04.2024						
DESIGN	3						
AGI	D.M.WARZECKA						
CAD	D.M.WARZECKA						
внеет#:	SL200 2						





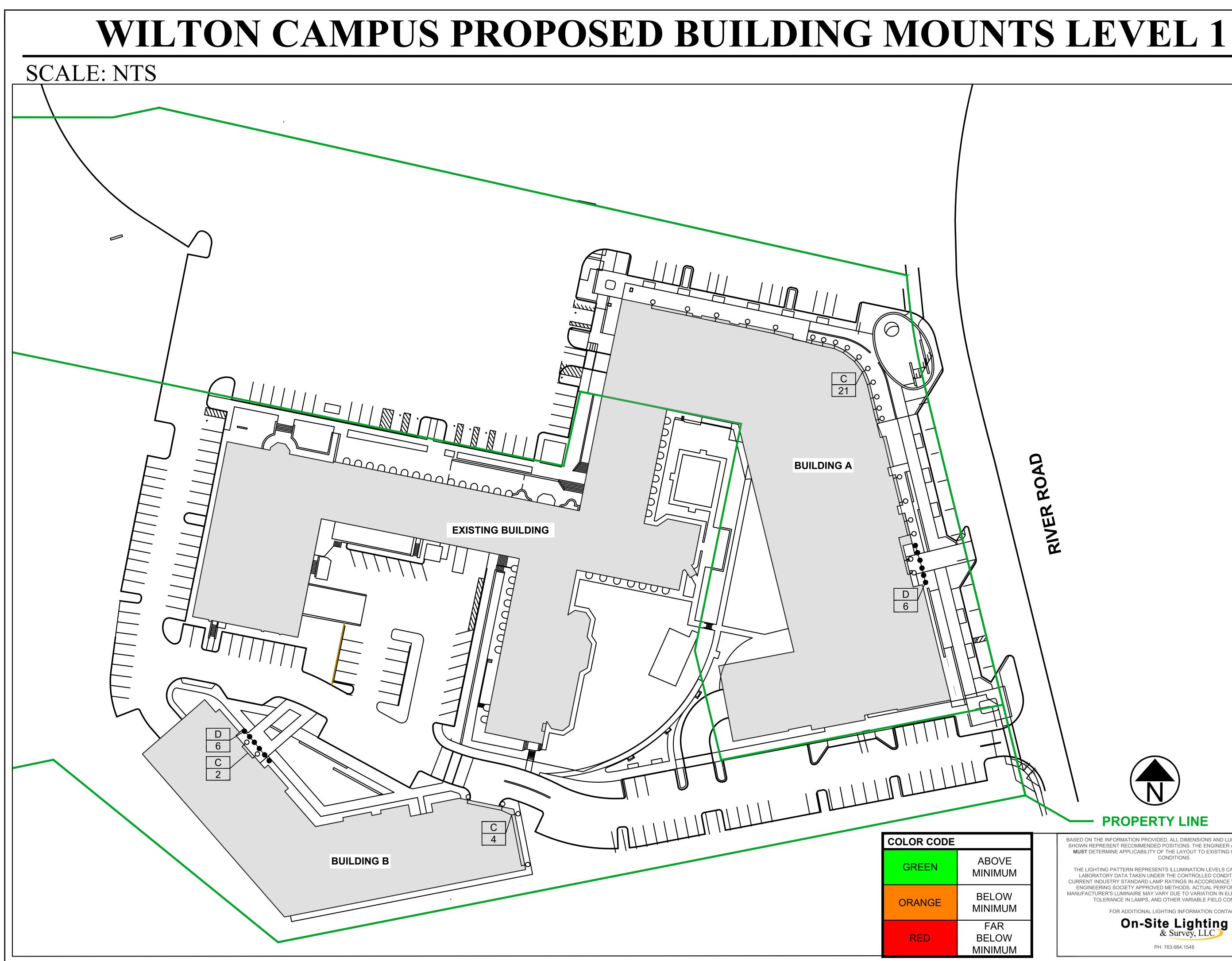


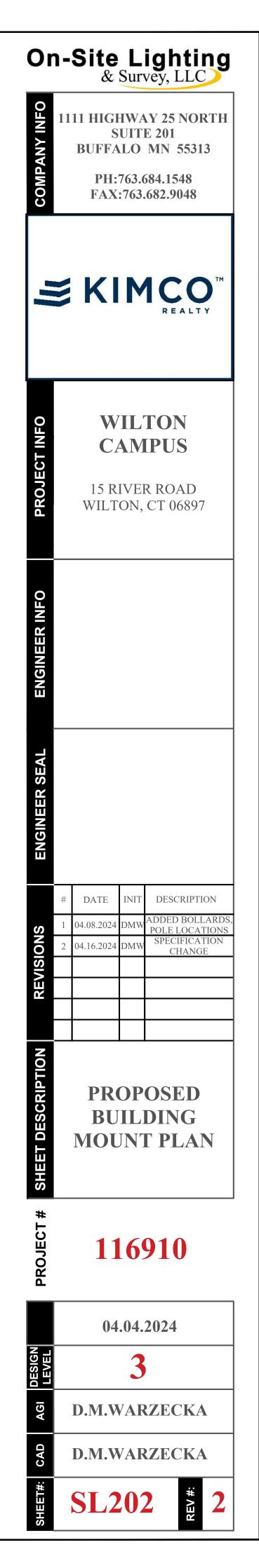
BASED ON THE INFORMATION PROVIDED, ALL DIMENSIONS AND LUMINAIRE LOCATIONS SHOWN REPRESENT RECOMMENDED POSITIONS. THE ENGINEER AND/OR ARCHITECT MUST DETERMINE APPLICABILITY OF THE LAYOUT TO EXISTING OR FUTURE FIELD CONDITIONS.

THE LIGHTING PATTERN REPRESENTS ILLUMINATION LEVELS CALCULATED FROM LABORATORY DATA TAKEN UNDER THE CONTROLLED CONDITIONS UTILIZING CURRENT INDUSTRY STANDARD LAMP RATINGS IN ACCORDANCE WITH ILLUMINATING ENGINEERING SOCIETY APPROVED METHODS. ACTUAL PERFORMANCE OF ANY MANUFACTURER'S LUMINAIRE MAY VARY DUE TO VARIATION IN ELECTRICAL VOLTAGE, TOLERANCE IN LAMPS, AND OTHER VARIABLE FIELD CONDITIONS.



PH: 763.684.1548





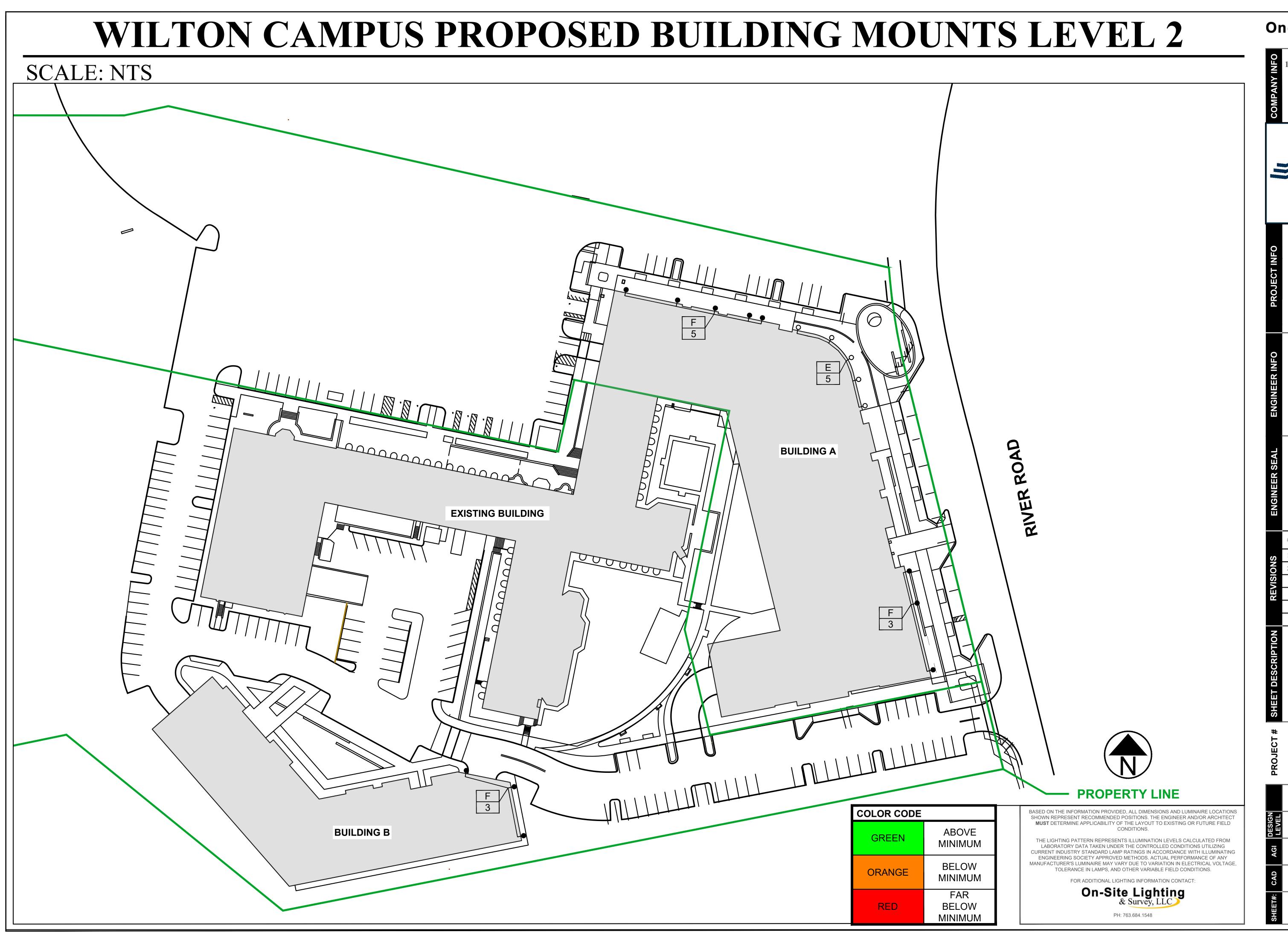


PROPERTY LINE

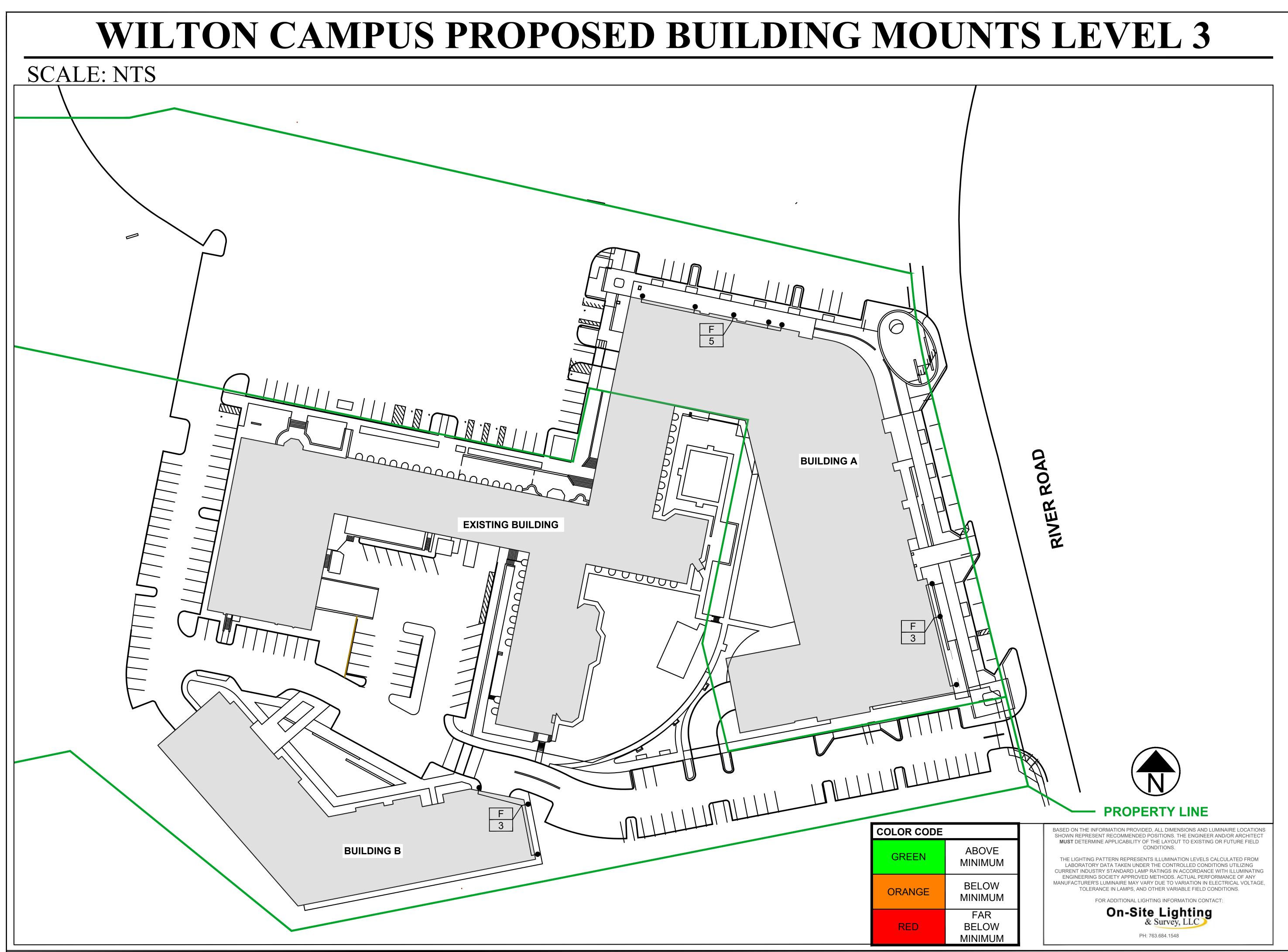
BASED ON THE INFORMATION PROVIDED, ALL DIMENSIONS AND LUMINAIRE LOCATIONS SHOWN REPRESENT RECOMMENDED POSITIONS. THE ENGINEER AND/OR ARCHITECT MUST DETERMINE APPLICABILITY OF THE LAYOUT TO EXISTING OR FUTURE FIELD CONDITIONS.

THE LIGHTING PATTERN REPRESENTS ILLUMINATION LEVELS CALCULATED FROM LABORATORY DATA TAKEN UNDER THE CONTROLLED CONDITIONS UTILIZING CURRENT INDUSTRY STANDARD LAMP RATINGS IN ACCORDANCE WITH ILLUMINATING ENGINEERING SOCIETY APPROVED METHODS. ACTUAL PERFORMANCE OF ANY MANUFACTURER'S LUMINAIRE MAY VARY DUE TO VARIATION IN ELECTRICAL VOLTAGE, TOLERANCE IN LAMPS, AND OTHER VARIABLE FIELD CONDITIONS.

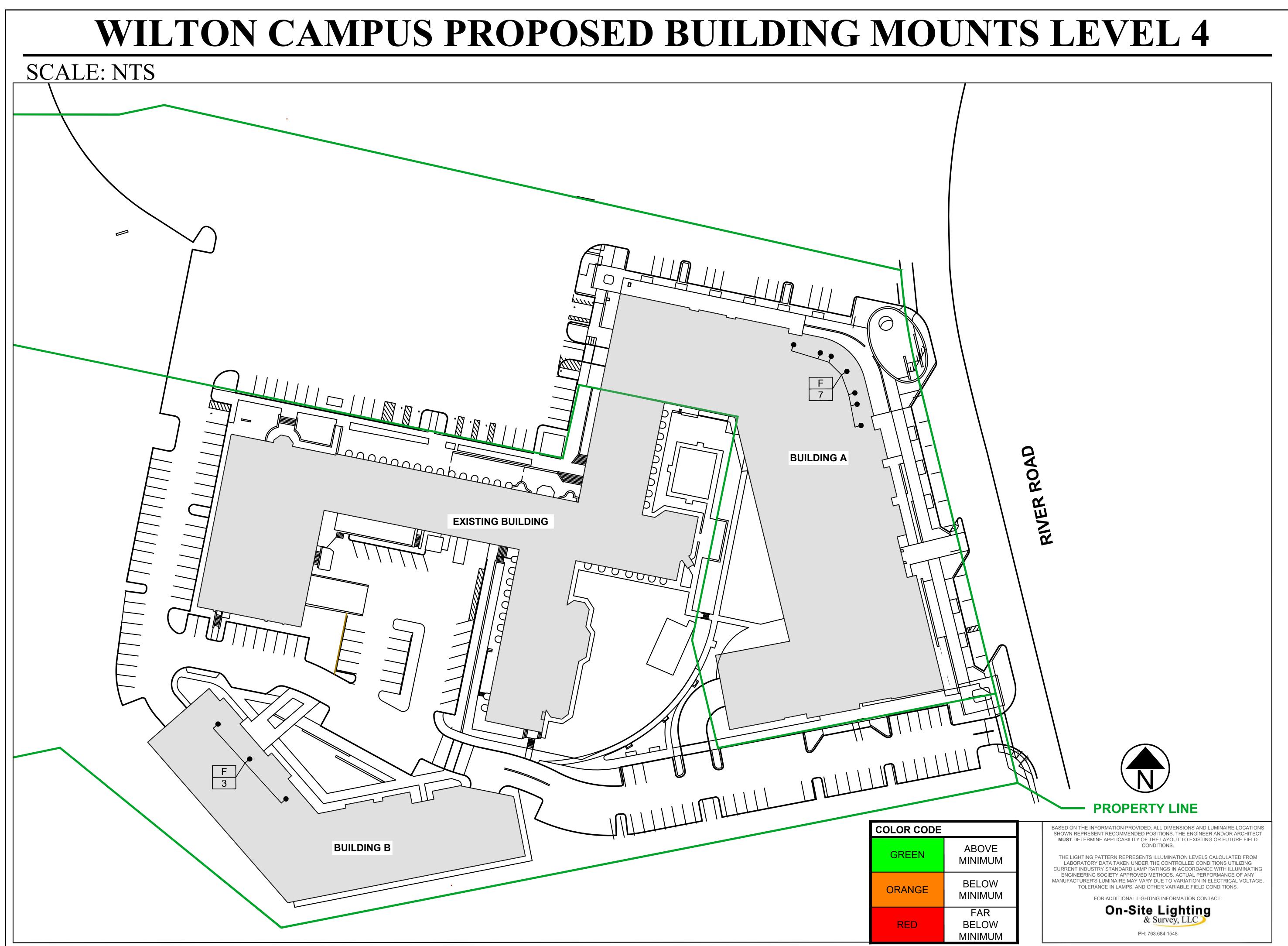




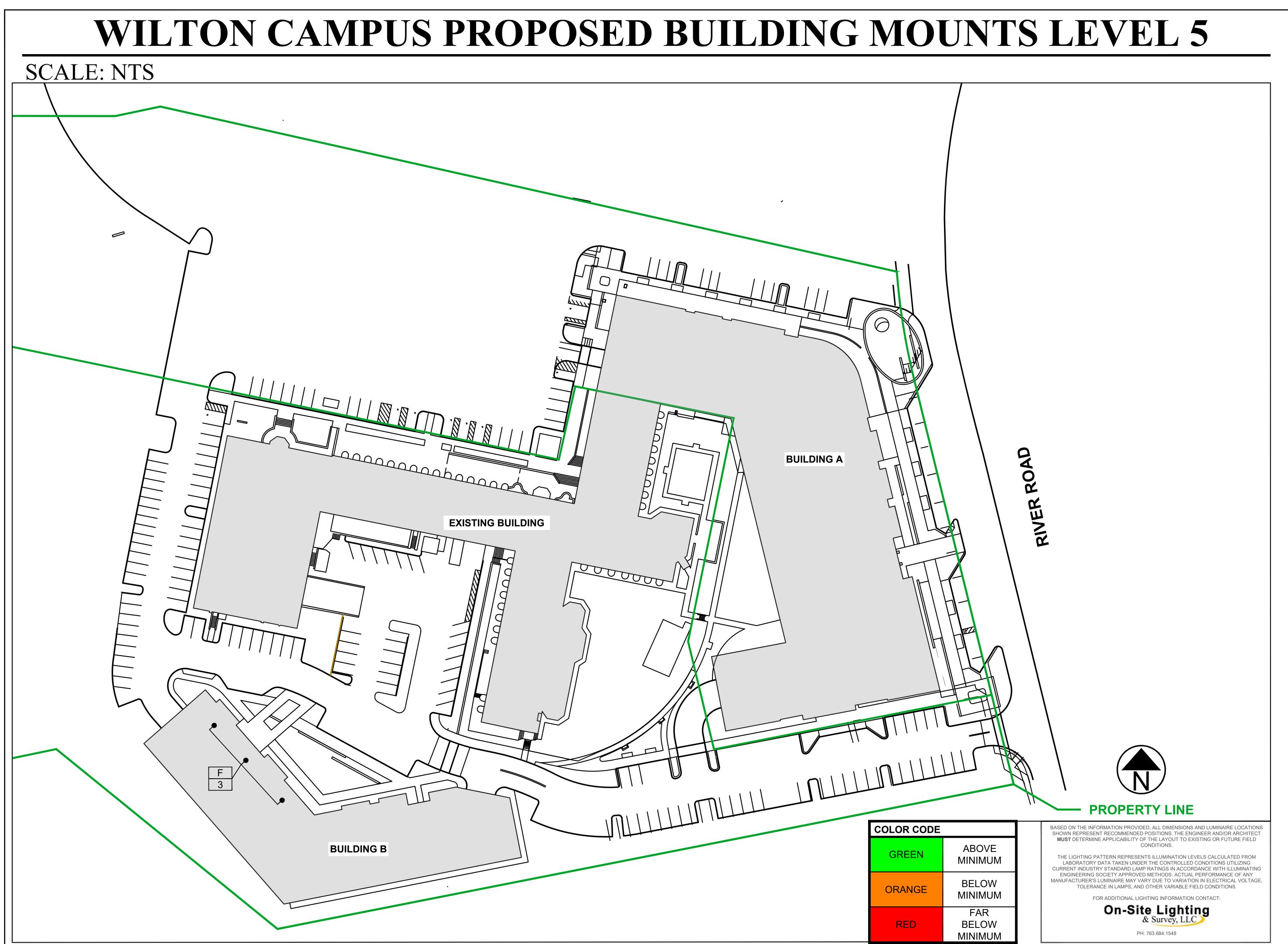
Or	n-Site Lighting & Survey, LLC
COMPANY INFO	1111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048
111	SKIMCO REALTY
PROJECT INFO	WILTON CAMPUS 15 RIVER ROAD WILTON, CT 06897
ENGINEER INFO	
ENGINEER SEAL	
REVISIONS	#DATEINITDESCRIPTION104.08.2024DMWADDED BOLLARDS, POLE LOCATIONS204.16.2024DMWSPECIFICATION CHANGE111111111111111111111111
SHEET DESCRIPTION	PROPOSED BUILDING MOUNT PLAN
PROJECT #	116910
	04.04.2024
DESIGN	3
AGI	D.M.WARZECKA
: CAD	D.M.WARZECKA
SHEET#:	SL203 2



Or	On-Site Lighting & Survey, LLC						
COMPANY INFO	OINI NUTURE 11111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048						
111	€ KIMCO REALTY						
PROJECT INFO	WILTON CAMPUS 15 RIVER ROAD WILTON, CT 06897						
ENGINEER INFO							
ENGINEER SEAL							
REVISIONS	#DATEINITDESCRIPTION104.08.2024DMWADDED BOLLARDS, POLE LOCATIONS204.16.2024DMWSPECIFICATION CHANGE4III4III5III6III6III7III7III8III9II						
SHEET DESCRIPTION	PROPOSED BUILDING MOUNT PLAN						
PROJECT #	116910						
	04.04.2024						
DESIGN	3						
AGI	D.M.WARZECKA						
CAD	D.M.WARZECKA						
SHEET#	SL204						



Or	-Site Lighting & Survey, LLC						
COMPANY INFO	1111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048						
11	EXIMCO REALTY						
PROJECT INFO	WILTON CAMPUS 15 RIVER ROAD WILTON, CT 06897						
ENGINEER INFO							
ENGINEER SEAL							
REVISIONS	#DATEINITDESCRIPTION104.08.2024DMWADDED BOLLARDS, POLE LOCATIONS204.16.2024DMWSPECIFICATION CHANGE4III4III5III6III6III7III7III8III9II						
SHEET DESCRIPTION	PROPOSED BUILDING MOUNT PLAN						
PROJECT #	116910						
	04.04.2024						
DESIGN	3						
AGI	D.M.WARZECKA						
CAD	D.M.WARZECKA						
SHEET#:	SL205 2						



Or	n-Site Lighting & Survey, LLC						
COMPANY INFO	1111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048						
11	EXIMCO REALTY						
PROJECT INFO	WILTON CAMPUS 15 RIVER ROAD WILTON, CT 06897						
ENGINEER INFO							
ENGINEER SEAL							
REVISIONS	#DATEINITDESCRIPTION104.08.2024DMWADDED BOLLARDS, POLE LOCATIONS204.16.2024DMWSPECIFICATION CHANGE11111111111111111111111111111111						
SHEET DESCRIPTION	PROPOSED BUILDING MOUNT PLAN						
PROJECT #	116910						
	04.04.2024						
DESIGN	3						
AGI	D.M.WARZECKA						
t: CAD	D.M.WARZECKA						
SHEET#:	SL206 2						

WILTON CAMPUS PROPOSED SCHEDULES

BUILDI	BUILDING MOUNT SCHEDULE PROPOSED						
QTY	LABEL	MANUFACTURER CATALOG NUMBER/ DESCRIPTION					
88	А	COOPER LIGHTING	TCRS5S-BK				
12	В	BL LIGHTING	BL flexFORM D1-4000k-IP68-2811				
27	с	CONTECH LIGHTING	CYL6340K-X-WXPL-B				
12	D	GREEN CREATIVE	LES9040-X-MD-WET-BL				
5	E	CONTECH LIGHTING	CYL8240K-X-UDXVWV-B				
35	F	CONTECH LIGHTING	CY3T140K-X-AWXS-B				

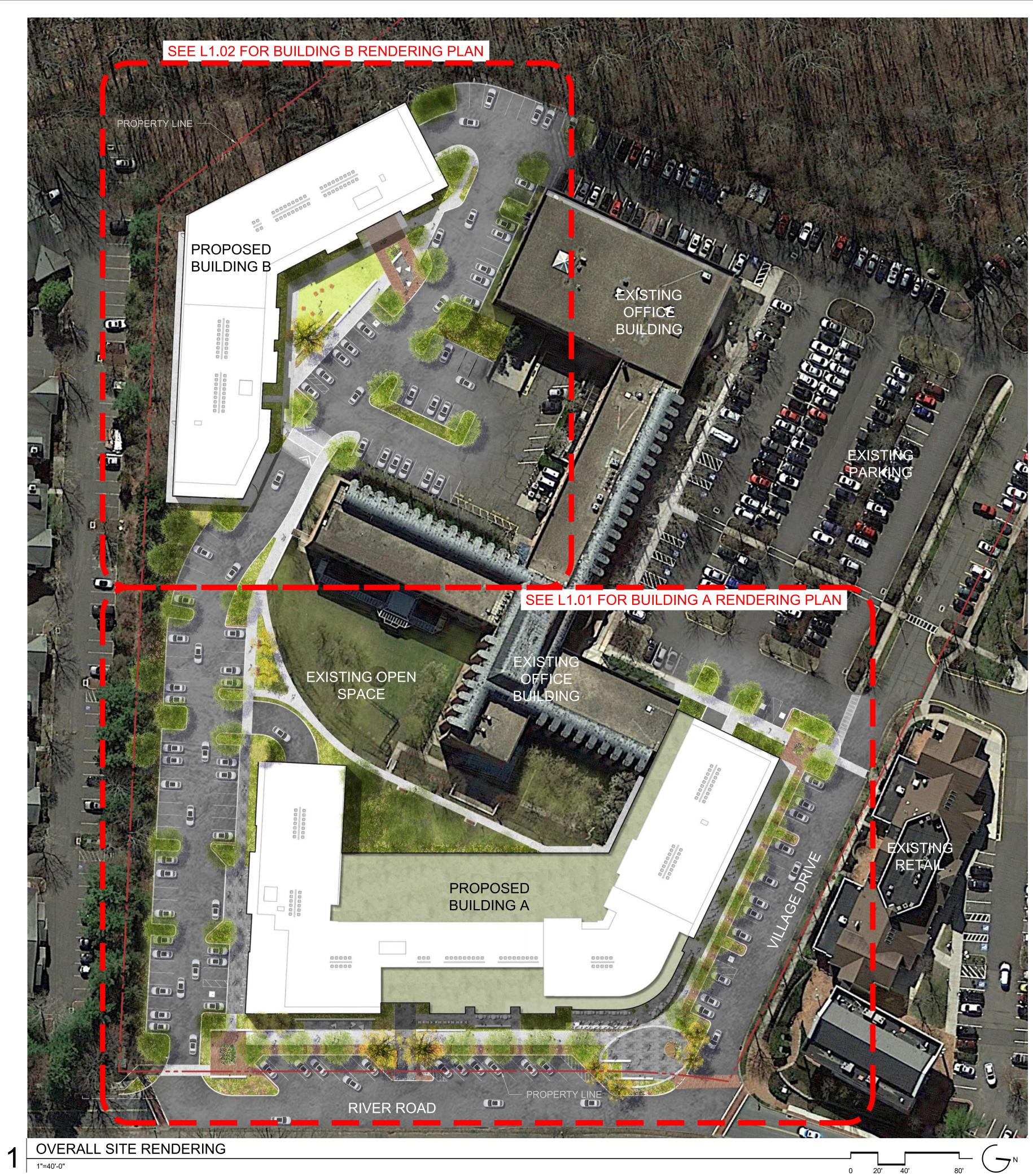
5	E	CO	NTECH LIGH	TING CYL8240K-X-U	DXVWV-B				LPD AREA SUMMARY					
35	F	cor	NTECH LIGH	TING CY3T140K-X-A	NXS-B				Label	Area	Total Watts	LPD	Perimeter	
									SITE		36234	6607	0.018	2912
LUMINA	AIRE S	CHE	EDULE						COLOR CODE		BASED ON THE INFOR	MATION PROVIDED, ALL DIN	/ENSIONS AND L	UMINAIRE LOCATIONS
Symbol	Qt	ty	Label	Arrangement	LLF	Description		BUG Rating	COLOR CODE		SHOWN REPRESENT	RECOMMENDED POSITIONS APPLICABILITY OF THE LAY CONDITIONS	S. THE ENGINEER OUT TO EXISTING	R AND/OR ARCHITECT
-	10	D	A-1	SINGLE	0.600	EXISTING 100W MH T-5 20'-0 MTG HT		B1-U3-G1	GREEN	ABOVE MINIMUM	THE LIGHTING PATTERN REPRESENTS ILLUMINATION LEVELS CALCULATED FROM LABORATORY DATA TAKEN UNDER THE CONTROLLED CONDITIONS UTILIZING			
	30	D	L-1	SINGLE	0.900	NEW BASE, POLE, & AREA FIXT 191W LED T	5W 20'-0 MTG HT (4000K/25984 LUMENS) LSI MPP-LED-25L-SIL-5W-40-70CRI	B5-U4-G3		BELOW		INDUSTRY STANDARD LAMP RATINGS IN ACCORDANCE WITH ILLI ERING SOCIETY APPROVED METHODS. ACTUAL PERFORMANCE URER'S LUMINAIRE MAY VARY DUE TO VARIATION IN ELECTRICA		
	3		M-1	SINGLE	0.900	NEW BASE, POLE, & AREA FIXT 149W LED T	5W 20'-0 MTG HT (4000K/10685 LUMENS) LSI MPP-LED-20L-SIL-5W-40-70CRI	B4-U4-G3	ORANGE MINIMUM		TOLERANCE IN LAMPS, AND OTHER VARIABLE FIELD CONDITIONS. FOR ADDITIONAL LIGHTING INFORMATION CONTACT:			ACT:
	11	1	N-1	SINGLE	0.900	NEW LOCATION BOLLARD 29W LED 3'-8 MTC	G HT (4000K/2320 LUMENS) LSI MRB-LED-30L-ACR-A-40	B1-U2-G1		FAR		On-Site Li & Surve	ghting	
	7		P-1	SINGLE	0.900	NEW BASE, POLE, & AREA FIXT 67W LED T2	20'-0 MTG HT (4000K/10685 LUMENS) LSI MPP-LED-10L-SIL-2-40-70CRI	B2-U3-G2	RED	BELOW MINIMUM		PH: 763.684.15		

ſ	CALCULATION SUMMARY
	Label
	SITE AT GRADE
	BUILDING A PARKING

MAIN PARKING

0	On-Site Lighting & Survey, LLC					
COMPANY INFO	OIN AND MUCH 1111 HIGHWAY 25 NORTH SUITE 201 BUFFALO MN 55313 PH:763.684.1548 FAX:763.682.9048					
-		KI	M	1 C	ALT	Y ™
PROJECT INFO		C	AM IVE	TOP IPUS R ROZ CT 00	S AD	7
ENGINEER INFO						
ENGINEER SEAL						
REVISIONS	# 1 2	DATE 04.08.2024 04.16.2024		ADDED POLE I SPECI		LARDS, FIONS FION
SHEET DESCRIPTION		PR SCH		OSI DUL		
PRO.IFCT #		11	6	91()	
		04	.04.	2024		
DESIGN			3)		
AG		D.M.W		RZEC	CKA	
#: CAD		D.M.W				
SHEET		SL2	20'	7	REV #:	2

٩vg	Max	Min	Avg/Min	Max/Min	# Pts	%PtsRange
.97	10.6	0.0	N.A.	N.A.	880	N.A.
8.60	8.2	0.5	7.20	16.40	28	67.9
.99	10.3	2.2	2.27	4.68	93	92.5



4

6

7

8

9

2

3

1

1

13

11

10

12



1691 ပ 5-21 River Road, Wilton, Wilton Campus

Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

Architect CUBE3 56 High Street North Andover, MA 01845

Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL

	CAPE ARCH	Community of the second
ISSL	IED FOR	DATE
_ <u>1</u> 2	VDDAC SUBMISSION	03/28/2024 04/23/2024

PROJECT NO. 23018

DRAWN BY : SW

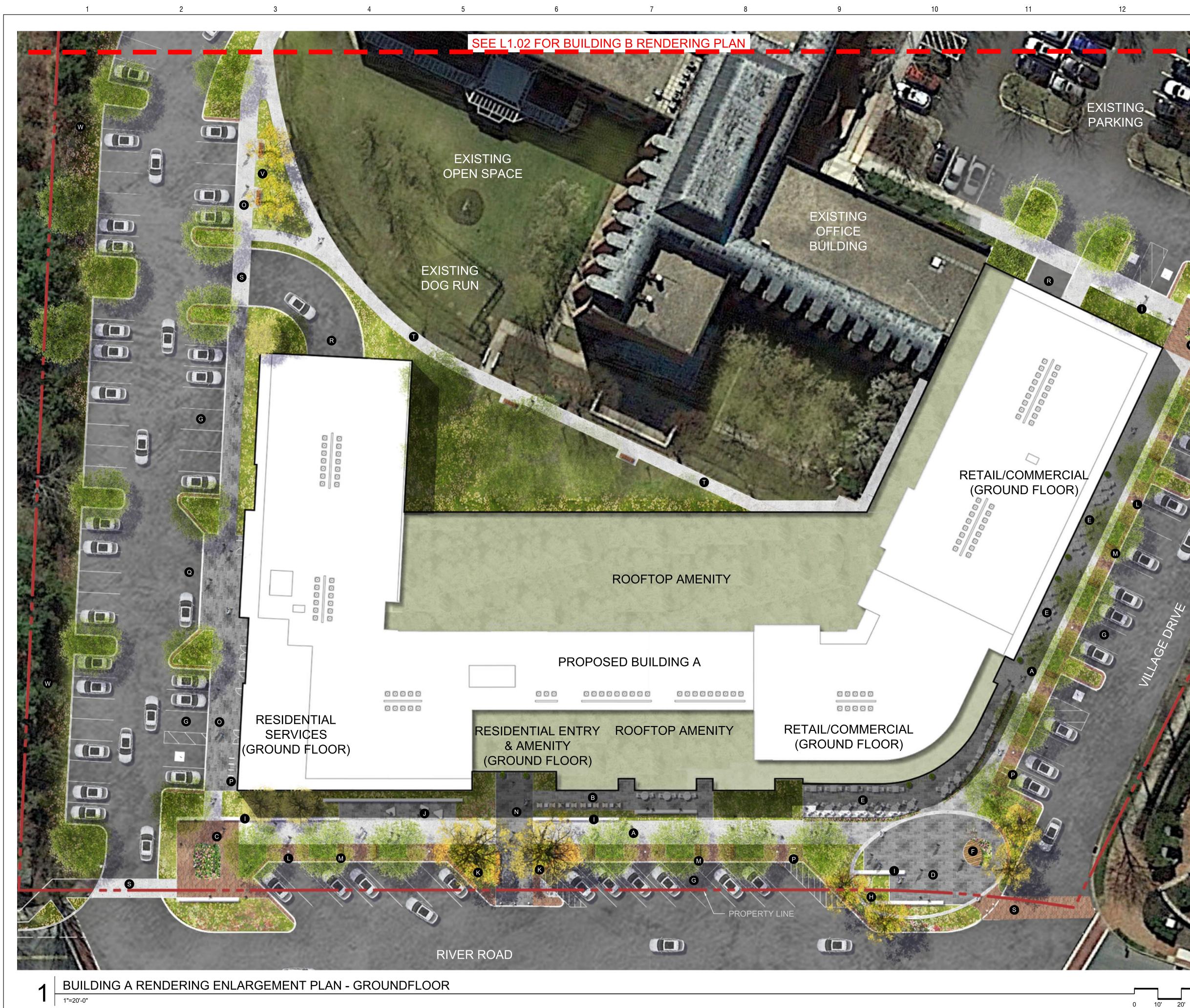
Reviewed by : Mr

SCALE : As Shown

L1.00 Overall Site Rendering

13

14 15 NOT FOR CONSTRUCTION



3

5

4

6

7

2



8

10



15



1691 5 5-21 River Road, Wilton, Campus Wilton

Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

Architect CUBE3 56 High Street North Andover, MA 01845

Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL

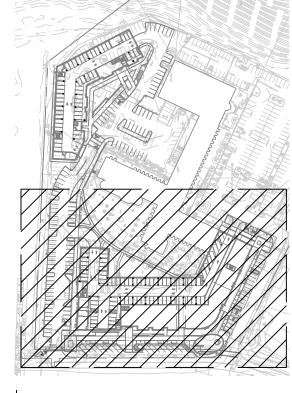


ISSUED FOR	DATE	
1 VDDAC SUBMISSION	<u>03/28/2024</u>	
2 LOCAL APPROVALS	04/23/2024	
<u> </u>		
PROJECT NO.	SCALE :	
23018	As Shown	
DRAWN BY : SW	reviewed by Mr	

L1.01 Building A Rendering Plan

LE	EGEND	
		_

- EXPANDED STREETSCAPE WITH TREES, SEATING AND AMENITIES
- B RESIDENTIAL AMENITY SPACES (PRIVATE)
- GATEWAY COMMUNITY SPACE WITH FOCAL FEATURE & SEAT WALLS
- D PLAZA/EVENT SPACE
- POTENTIAL OUTDOOR DINING AREAS
- BENCH/STAGE FEATURE
- G PUBLIC PARKING H PLAZA ACCENT AREA
- LINEAR SEAT WALLS/FEATURES
- J FOCAL POINT SEATING ELEMENTS
- K RIVER ROAD STREETSCAPE PLANTING
- STREET LIGHTS (SEE LIGHTING)
- M BENCHES/CONVERSATION AREAS
- N RESIDENTIAL LOBBY ARRIVAL
- O OPEN SPACE WALK/CONNECTION TO BUILDING B
- P BIKE RACKS
- Q SERVICE/DROP-OFF AREA
- **R** PARKING ENTRY
- S CROSSWALK
- OPEN SPACE WALK
- U LANDSCAPE AREA
- V PROPOSED BENCHES
- W EXISTING LANDSCAPE BUFFER TO REMAIN



KEY PLAN N.T.S.

40'

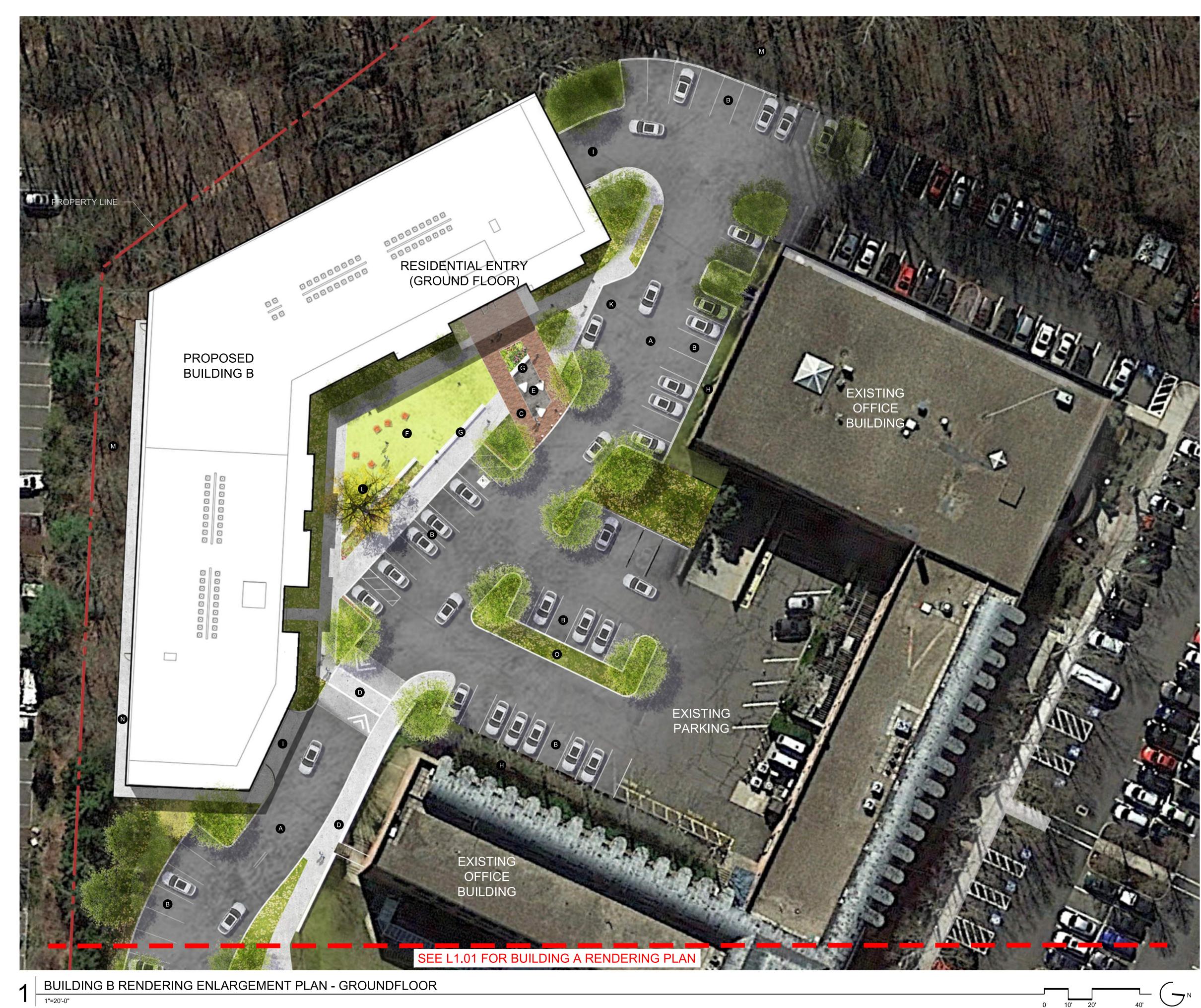
13

12

11

 $\bigcirc^{\scriptscriptstyle N}$

14 15 NOT FOR CONSTRUCTION



5

6

6

1

1

2

11

12

11

10

LEGEND

A REALIGNED SITE DRIVEWAY

B PROPOSED/REALIGNED PARKING

LINEAR SEAT WALLS/FEATURES

M EXISTING LANDSCAPE BUFFER TO REMAIN

H EXISTING LANDSCAPE AREA

K DELIVERY DROP-OFF ZONE

OPEN SPACE WALKWAY/CROSSWALK TO RIVER ROAD

C RESIDENTIAL ARRIVAL PLAZA

B SEATING ELEMENTS

E LAWN AREA

PARKING ENTRY

J FOCAL POINT TREE

RAISED CROSSWALK

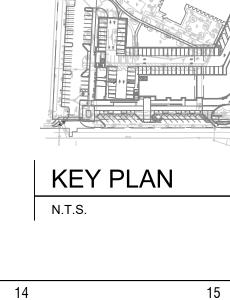
N EGRESS PATHWAY

O RAIN GARDEN

G

MAHAN RYKIEL A S S O C I A T E S I N C Whitehall Mill 3300 Clipper Mill Road Suite 200 Baltimore, MD 21211 410.235.6001

13



15 NOT FOR CONSTRUCTION



Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

Architect CUBE3 56 High Street North Andover, MA 01845

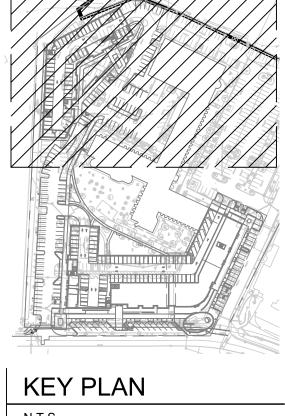
Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL

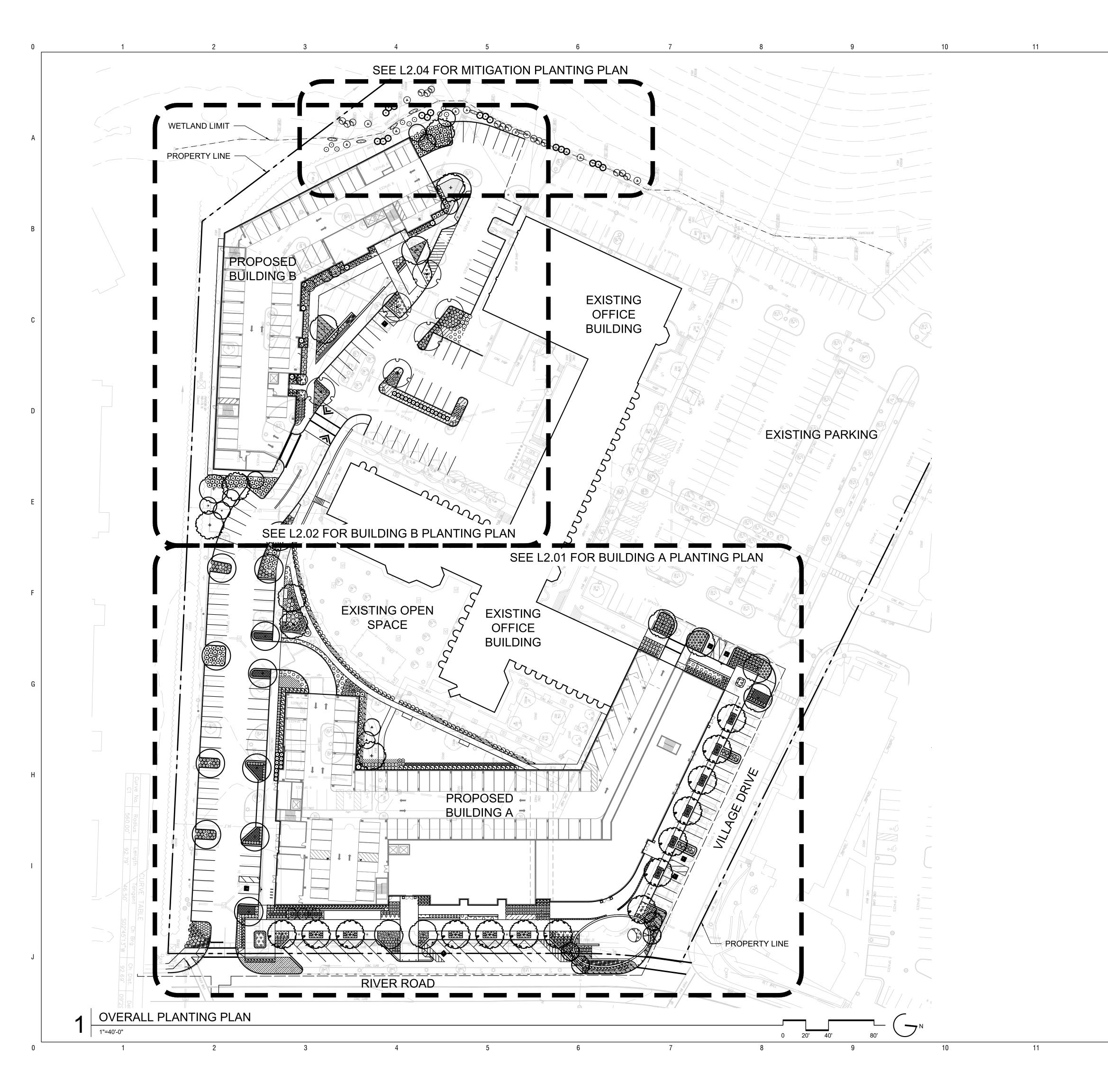


ISSUED FOR	DATE
1 VDDAC SUBMI 2 LOCAL APPRO	
PROJECT NO. 23018 DRAWN BY : SW	SCALE : As Shown REVIEWED BY MR

L1.02 Building B Rendering Plan



^{1&}quot;=20'-0"



13



Wilton Campus 1691 5-21 River Road, Wilton, CT

Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

Architect CUBE3 56 High Street North Andover, MA 01845

Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL



ISSUED FOR	DATE
1 VDDAC SUBMISSION 2 LOCAL APPROVALS	
PROJECT NO.	SCALE :
23018	As Shown
DRAWN BY :	Reviewed by :
SW	Mr

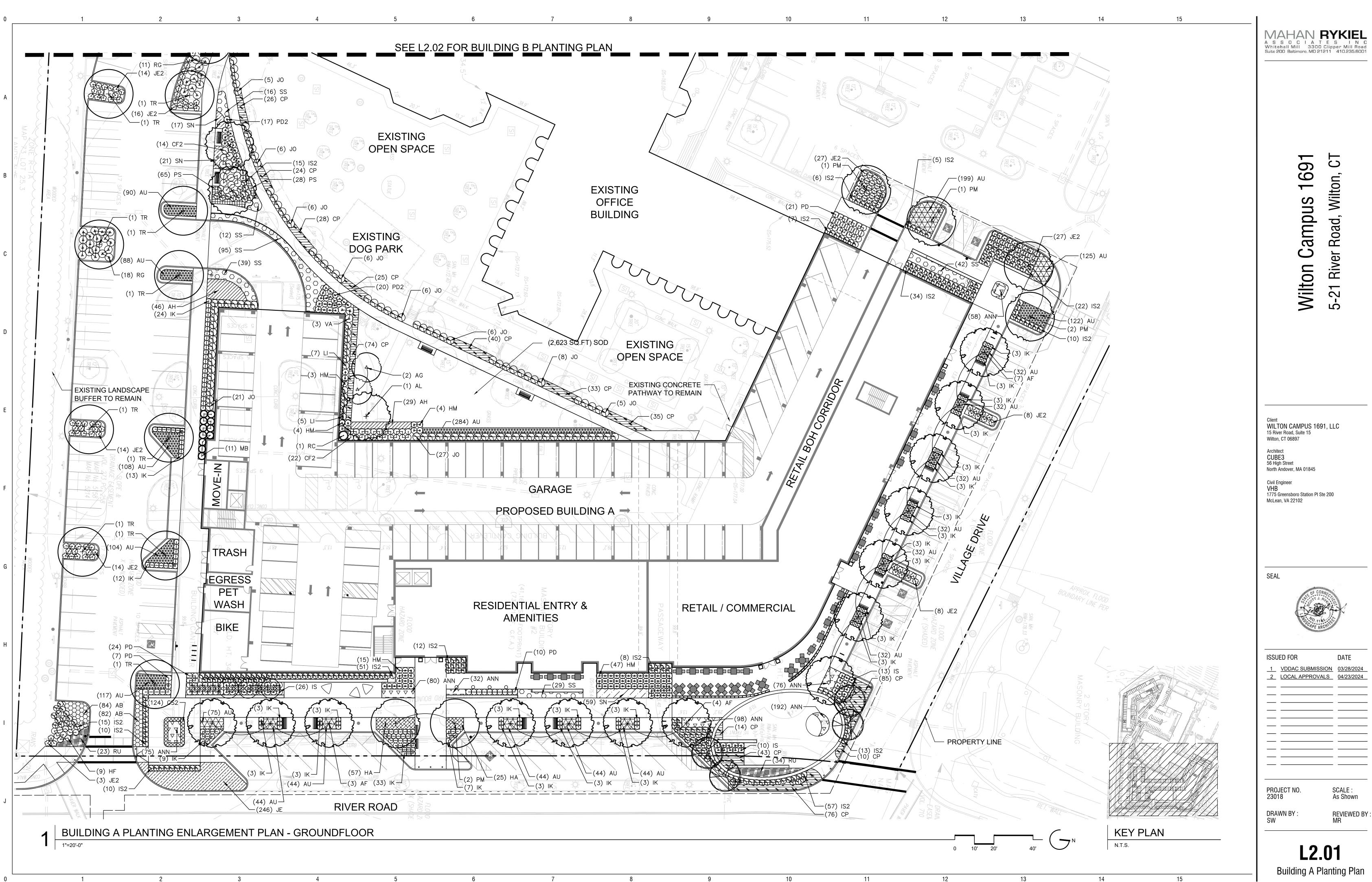
L2.00 Overall Planting Plan

13

14 15 NOT FOR CONSTRUCTION

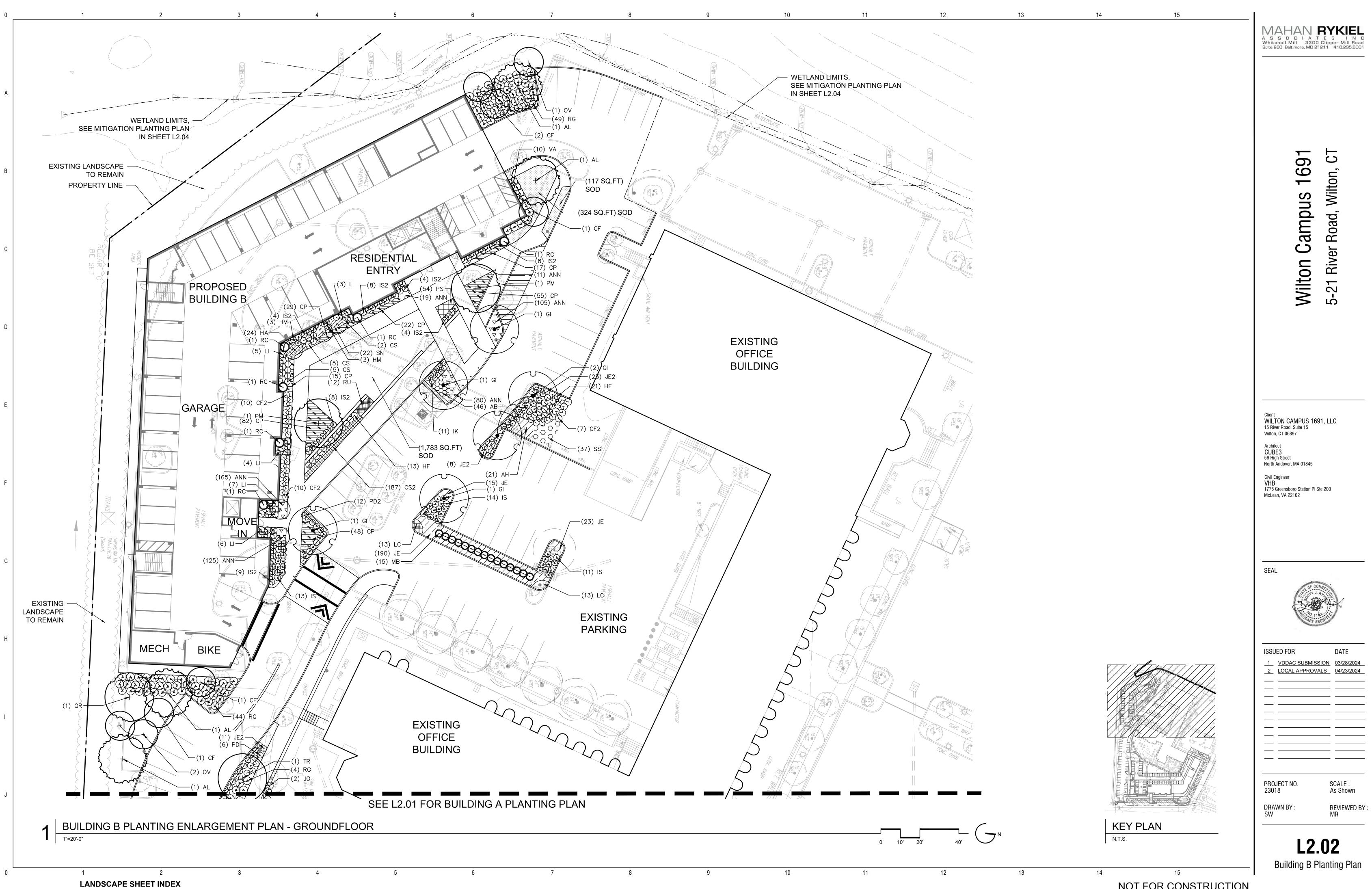
15

14





NOT FOR CONSTRUCTION



NOT FOR CONSTRUCTION

1

2

3

4

5

6

7

8

9

2

3

6

PLANT SCHEDULE

CODE	<u>QTY</u>	BOTANICAL / COMMON NAME	SIZE	CONTAINER	
ORNAN	IENTAL	TREES			
AG	2	Amelanchier x grandiflora `Autumn Brilliance`	8`-10` Ht.	B&B	
		Autumn Brilliance Apple Serviceberry			
CF	5	Cornus florida Flowering Dogwood	2"-2.5" Cal.	B&B	
OV	3	Ostrya virginiana	2.0"-2.5" Cal.	B&B	
		American Hophornbeam			
	TREES				
AF	14	Acer rubrum 'Frank Jr.' Redpointe® Maple	3"-3.5" Cal.	B&B	
AL	5	Acer saccharum 'Legacy' Legacy Sugar Maple	3"-3.5" Cal.	B&B	
GI	6	Gleditsia triacanthos inermis `Skycole`	3"-3.5" Cal.	B&B	
РΜ	8	Skyline® Honey Locust Platanus x acerifolia 'Morton Circle'	3"-3.5" Cal.	B&B	
QR	1	Exclamation!™ London Plane Tree Quercus rubra	3"-3.5" Cal.	B&B	
		Northern Red Oak			
TR	11	Tilia americana 'Redmond' Redmond American Linden	3"-3.5" Cal.	B&B	
SHRUB	c				
CS	<u>-</u> 12	Clethra alnifolia 'Sixteen Candles'	2'-3' Ht.	B&B/Cont.	
CF2	63	Sixteen Candles Summersweet Cornus sericea 'Farrow'	2'-3' Ht.	B&B/Cont.	
		Arctic Fire® Red Twig Dogwood			
HM	79	Hydrangea quercifolia `Munchkin` Munchkin Oakleaf Hydrangea	3'-4' Ht.	B&B/Cont.	
HF	43	Hypericum frondosum 'Sunburst' Sunburst St. John's Wort	2'-3' Ht.	B&B/Cont.	
IK	175	llex glabra 'Gem Box'	18" - 24" Spd.	Cont.	
S2	320	Gem Box Inkberry Holly Ilex glabra 'Shamrock'	2'-3' Ht.	B&B/Cont.	
IS	87	Shamrock Inkberry Holly Itea virginica 'Sprich'	2'-3' Ht.	B&B/Cont.	
		Little Henry® Sweetspire			
JE2	173	Juniperus communis 'Effusa' Effusa Common Juniper	18" - 24" Spd.	Cont.	
JO	98	Juniperus virginiana 'Grey Owl'	2'-3' Ht.	B&B/Cont.	
LI	37	Grey Owl Eastern Redcedar Leucothoe axillaris 'Sarah's Choice'	2'-3' Ht.	B&B/Cont.	
MB	26	Sarah's Choice Dog-Hobble Myrica pensylvanica 'Bobzam'	3'-4' Ht.	B&B/Cont.	
		Bobee™ Northern Bayberry			
PD2	49	Physocarpus opulifolius 'Donna May' Little Devil™ Dwarf Ninebark	2'-3' Ht.	B&B/Cont.	
PD	68	Potentilla fruticosa 'Fargo' Dakota Sunspot® Bush Cinquefoil	2'-3' Ht.	B&B/Cont.	
RC	7	Rhododendron carolinianum	3'-4' Ht.	B&B/Cont.	
RG	126	Carolina Rhododendron Rhus aromatica 'Gro-Low'	2'-3' Spd.	B&B/Cont.	
VA	13	Gro-Low Fragrant Sumac Viburnum dentatum 'Christom'	3'-4' Ht.	B&B/Cont.	
٧A	15	Blue Muffin® Arrowwood Viburnum	5-4 m.	Dad/Com.	
CODE	QTY	BOTANICAL / COMMON NAME	SIZE	CONTAINER	SPACING
<u>GROUN</u> AH	1D COVE 96	<u>ERS</u> Amsonia hubrichtii	#1	Cont.	24" o.c.
AB	212	Arkansas Bluestar Amsonia x 'Blue Ice'	#1	Cont.	15" o.c.
		Blue Ice Bluestar			
ANN	2,998	Annuals Annua Plants	#1	Cont.	6" o.c.
AU	1,724	Arctostaphylos uva-ursi Kinnikinnick	#1	Cont.	12" o.c.
CP	781	Carex pensylvanica	#1	Cont.	18" o.c.
CS2	311	Pennsylvania Sedge Chrysogonum virginianum 'Superstar'	#SP4	Cont.	10" o.c.
HA	106	Superstar Green-and-Gold Heuchera villosa 'Autumn Bride'	#1	Cont.	18" o.c.
		Autumn Bride Hairy Alumroot			
JE	474	Juncus effusus Soft Rush	#1	Cont.	18" o.c.
_C	26	Lobelia cardinalis Cardinal Flower	#1	Cont.	18" o.c.
S	147	Phlox subulata	#1	Cont.	12" o.c.
รบ	69	Creeping Phlox Rudbeckia x 'American Gold Rush'	#1	Cont.	24" o.c.
SS	270	American Gold Rush Coneflower Schizachyrium scoparium 'The Blues'	#1	Cont.	24" o.c.
50	210	The Blues Little Bluestem	π I	Cont.	2+ 0.0.
SN	119	Symphyotrichum novae-angliae	#1	Cont.	18" o.c.

10

11

12

13

14

15

NOT FOR CONSTRUCTION

7

1. CONTACT 'CALL BEFORE YOU DIG' AT 1-800-922-4455 TO HAVE UNDERGROUND UTILITY LINES MARKED BY THEM PRIOR TO START OF ANY EXCAVATION WORK.

q

2. EXACT LOCATION OF PROPOSED PLANTINGS AND SPECIES TYPES MAY VARY FROM THE PLAN BASED ON ACTUAL FIELD CONDITIONS.

8

- 3. SPRAY NEW PLANTINGS IMMEDIATELY AFTER INSTALLATION WITH A WHITE-TAILED DEER REPELLENT AND CONTINUE AS NEEDED TO MAINTAIN PLANTS FREE OF SIGNIFICANT DEER BROWSING.
- 4. PLNAT SPECIES SEBSTITIUTIONS MAY BE MADE WITH THE APPROVAL OF THE PROJECT LANDSCAPE ARCHITECT AND TOWN OF WILTON PRIOR TO PLANTING. SUBSTITUTED PLANTS SHALL BE AT AN EQUAL OR GREATER SIZE AS NOTED USING A SIMILAR TYPE PLANT.
- 5. MULCH AREAS AROUND NEW TREES AND SHRUBS WITH A 3" THICK LAYER OF SHREDDED CEDAR BARK MULCH. NEW TREES SHALL EACH HAVE A 5' MIN. DIA. MULCHED BED AND NEW SHRUBS SHALL EACH HAVE A MINIMUM 3' DIAMETER MULCHED BED. AREAS WITHIN 4" OF TREE TRUNKS SHALL BE MINTAINED FREE OF MULCH.
- 6. PLANTING METHODS SHALL BE IN ACCORDANCE WITH THE 'AMERICAN STANDARDS FOR NURSERY STOCK', LATEST EDITION, AS PUBLISHED BY THE AMERICAN NURSERY & LANDSCAPE ASSOCIATION.
 7. THE CONTRACTOR SHALL VERIFY WITH THE PROJECT ENGINEER THAT THE NEW PLANTINGS DO
- NOT INTERFERE WITH EXISTING AND/OR PROPOSED UTILITIES, SIGHT LINES, AND/OR STRUCTURES. 8. THE PLAN FOR PLANTING PURPOSES ONLY. SEE PLANS BY OTHERS FOR ADDITIONAL
- INFORMATION. 9. SEED LAWN AREAS WITH A HIGH-QUALITY TRIPLE FESCUE TURF MIX. SEED AREAS AT THE METHODS AND RATE RECOMMENDED BY THE MANUFACTURER. LIGHTLY MULCH SEEDED AREA WITH
- METHODS AND RATE RECOMMENDED BY THE MANUFACTURER. LIGHTLY MULCH SEEDED AREA WITH WEEK-FREE CLEAN HAY. A NURSE CROP SHALL BE ADDED TO THE SEED MIX ON SLOPES OF EXCESS OF 10%. LIGHTLY RAKE OR ROLL GROUND SURFACE ATER SOWING.



Wilton Campus 1691 5-21 River Road, Wilton, CT

Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

Architect CUBE3 56 High Street North Andover, MA 01845

Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL

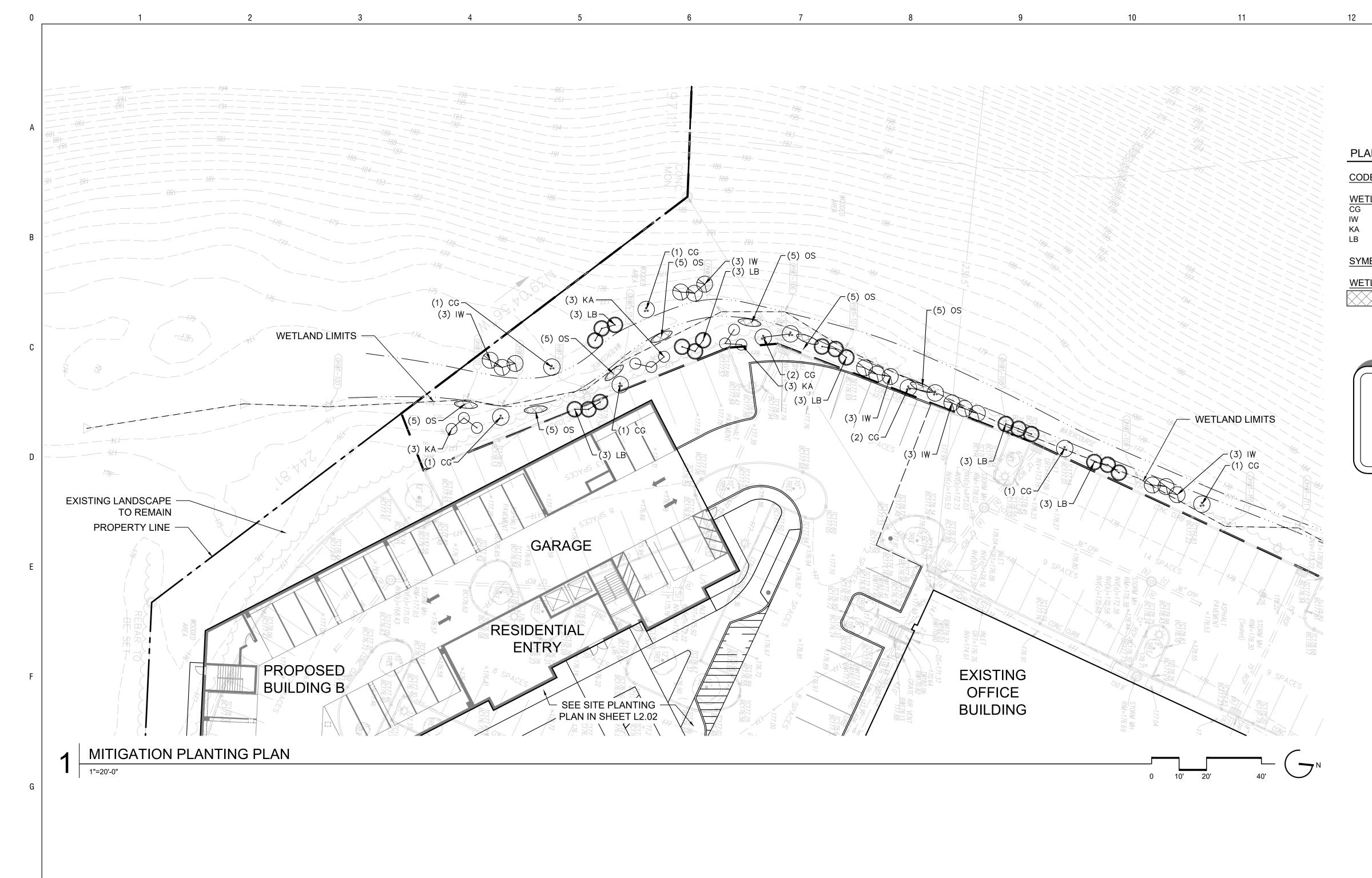


ISSUED FOR	DATE	
1 VDDAC SUBMISSION	N 03/28/2024	
2 LOCAL APPROVALS	04/23/2024	
PROJECT NO.	SCALE :	
23018	As Shown	
DRAWN BY : SW	REVIEWED BY MR	

L2.03 Plant Schedule

13

15



6

4

7

8

9

Η

1

2

3

11

10

A S S O C I A T E S I N C Whitehall Mill 3300 Clipper Mill Road Suite 200 Baltimore, MD 21211 410.235.6001

ANT SCHEDULE							
DE	<u>QTY</u>	BOTANICAL / COMMON NAME	<u>SIZE</u>	ROOT		REMARKS	
TLAND	SHRUE	3S					
	10	Cornus racemosa / Gray Dogwood	2'-3'	Cont.		FAC, 10' O.C.	
	15	llex verticillata / Winterberry	2'-3'	Cont.		FACW, 5' O.C.	
	9	Kalmia angustifolia / Sheep Laurel	2'-3'	Cont.		FAC, 6' O.C.	
	18	Lindera benzoin / Spicebush	2'-3'	Cont.		FACW, 5' O.C.	
<u>MBOL</u>	<u>QTY</u>	BOTANICAL / COMMON NAME	<u>SIZE</u>	CONTAINER	<u>SPACING</u>	REMARKS	
TLAND	GROUN	NDCOVER					
	35	Onoclea sensibilis / Sensitive Fern	QT.	Cont.	24" o.c.		

LANDSCAPE NOTES:

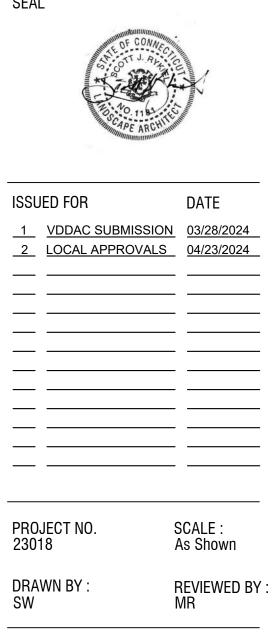
1. THE PLANT SPECIES AND DESIGN ON THIS MITIGATION PLANTING PLAN WERE SELECTED AND REVIEWED BY VHB WETLAND AND SOIL SCIENTISTS. Wilton Campus 1691 5-21 River Road, Wilton, CT

Client WILTON CAMPUS 1691, LLC 15 River Road, Suite 15 Wilton, CT 06897

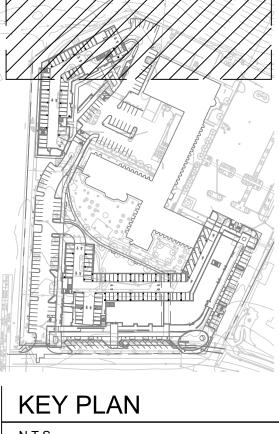
Architect CUBE3 56 High Street North Andover, MA 01845

Civil Engineer VHB 1775 Greensboro Station PI Ste 200 McLean, VA 22102

SEAL



L2.04 Mitigation Planting Plan



N.T.S.

13

¹⁴ ¹⁵ NOT FOR CONSTRUCTION

STORMWATER MANAGEMENT REPORT

Wilton Center Redevelopment

21-23 River Road Wilton, CT

PREPARED FOR

Wilton Campus 1691, LLC 500 North Broadway, Suite 201 Jericho, NY 11753

PREPARED BY



100 Great Meadow Road Suite 200 Wethersfield, CT, 06109

APRIL 2024



Table of Contents

Stormwater Report Narrative	5
Project Description	
Site Description	
Wetlands	
Existing Drainage Conditions	
Proposed Drainage Conditions	7
Environmentally Sensitive and Low Impact Development (LID) Techniques	9
Hydrologic Analysis	
Hydraulic Analysis	
FEMA	
Compensatory Flood Storage	

Appendices

Appendix A

NRCS Soil Survey Information Record Site Mapping

Appendix B

FEMA Floodway Map Flood Storage Computations Existing and Proposed Flood Figures

Appendix C

Water Quality Volumes Retention sizing Water Quality Unit Sizing Water Quality TSS StormCAD: Schematic StormCAD: Conduit Table (25-year storm event)

Appendix D

Geotechnical Report

<u>Appendix E</u>

Erosion and Sedimentation Control Measures

Appendix F

Long Term Stormwater and Operation and Maintenance Measures

Appendix G

HydroCAD: Existing Conditions HydroCAD: Proposed Conditions

List of Tables

Table No.	Description	Page
Table 2	Existing Conditions Hydrologic Data	7
Table 3	Proposed Conditions Hydrologic Data	8
Table 4	Peak Discharge Rates (cfs*)	10



Stormwater Report Narrative

Project Description

The Applicant, Wilton Campus 1691,LLC, is proposing to redevelop a portion of the site located at 21 River Road in Wilton, CT. The project will include the demolition of the existing building along River Road and construct a four-story, ±51,000 square foot (sf) building footprint with 97 residential apartment units on the second, third and fourth floors, and ±12,000 sf of commercial use on the first floor. The project also includes the construction of a five-story, ±24,000 sf standalone building footprint with 72 residential apartment units at the rear of the site. This adds a total of 169 residential units between the two buildings. The remaining building onsite will be retained with its existing use of office and retail space. Improved landscaping, utility infrastructure, parking, and significant stormwater management improvements will be proposed to support the redevelopment.

Site Description

The project site, as shown on Figure 1, is located within the Norwalk River Valley on the west side of River Road at 15-21 River Road in the Town of Wilton, Connecticut. The site is bounded by Wilton River Park Plaza to the north, River Road to the east, the Avalon apartment complex to the south, and dense wooded hillside to the west. Access to the site will utilize the existing curb cuts on the north and south ends of the property.

Wetlands

There are two separate wetland systems located on or adjacent to the project site. Wetlands associated with the Norwalk River are located on the eastern side of River Road. Though not directly within the limit of work, the 100ft upland review buffer associated with the river extends into the proposed development. A second wetland system associated with a small watercourse is located at the toe of slope along the western edge of the currently developed site. Work is proposed within the 100' upland review area to this westerly wetland system, predominately within already disturbed areas for existing parking fields. The westerly wetland system and watercourse itself will remain unaltered and be protected.

A Wetland & Watercourse Delineation Report was prepared on October 4, 2023, describing the wetland resources delineated within the project site. An additional Functions and Values report was compiled describing the minimal to no impact to the adjacent wetland systems as well as

proposed mitigation measures are included with this development program. These reports are included under separate cover.

According to the Natural Resources Conservation Service (NRCS), surface soils on the Site include primarily urban land classified as Hydrologic Soil Groups (HSG) D. Based on the soil evaluation included in Appendix A, the Site is not considered to be within an area of rapid infiltration (soils with a saturated hydraulic conductivity greater than 2.4 inches per hour).

Geotechnical investigation reported varying infiltration rates including one test area that was inconclusive due to an obstruction. Conservatively a rate of 1 in/hr was used for proposed modeling purposes. See Appendix D for geotechnical findings.

Existing Drainage Conditions

Under existing conditions, the Site is primarily developed with one large mixed use building containing office, retail, and restaurant space. The site is fairly flat with paved parking and ancillary landscaping surrounding the centralized building. There are numerous catch basins and yard drains dispersed through the site that primarily connect to an existing undersized infiltration conveyance system located along the southern property line. Per record drawings and conversations with the property manager, there does not appear to be any interior or exterior footing drains for the existing building area, but no excavations or exploratory investigations have been done at this time. There are two (2) sump pumps in the existing building, one in the west wing (area to remain) and one in the south wing (area to be demolished). Both sump pumps are connected to the existing storm drainage system (see Appendix A for mapping).

The site has 3 main drainage discharge points broken up into 4 drainage areas:

Drainage area 1a & 1b: The majority of the southern portion of the site (Drainage Area 1a and 1b, approximately 5.7ac) drains to on-site catch basins and into a closed drainage system. The western most portion of the southern area drains to a centralized curb-less vegetated rain garden with overflow area drain. Captured runoff from both areas flow through a series of 36" perforated pipes surrounded in stone along the southern property line. The system is approximately 700 feet in length and contains a chain of outlet control structures which assist in promoting infiltration of the captured runoff. The system, while effective in providing a low impact design feature, is undersized retaining less than the 1" water quality volume, thus the perforated pipes primarily serving as a conveyance measure for stormwater. Stormwater from larger storm events, or stormwater that is not infiltrated, is conveyed to an offline water quality unit prior to connecting to the closed drainage network in River Road. The size or adequacy of this existing water quality unit is unknown but is assumed to likely be undersized when considering the increased intensities of recent rainfall events and NOAA data. Stormwater ultimately discharges directly across the street into the Norwalk River (Design Point 1).

<u>Drainage area 2</u>: Drainage area 2 comprises the northern portion of the site and primarily encompasses existing building and parking fields to remain. The parking and landscape improvements along Village Drive is also included in this area. In total drainage area 2 consists of approximately 3.6 acres (primarily impervious area). Runoff captured by onsite catch basins flow to River Road through a series of pipes and structures. There is no record of any treatment for

stormwater for this drainage area. Similarly, stormwater from Design Point 2 ultimately discharges directly into the Norwalk River.

<u>Drainage Area 3:</u> Drainage area 3 is comprised mostly of the steep western hillside and the portion of the existing site immediately west of the existing parking lot curbline. Note that no runoff from the existing parking lot or development discharges to this drainage area or its design point. This area drains to a watercourse located just off the western curbline and flows to the south. The area is mostly wooded with grass along the curbline of the parking area. The wetland system associated with this drainage area is to remain and be protected. Stormwater runoff from this area is conveyed offsite to the southwest via the existing watercourse (Design Point 3).

Design points 1 and 2 denote the closed drainage system in River Road which flow to the Norwalk River. Design Point 3 is a disconnected watercourse that flows to the west. Table 2 below provides a summary of the existing conditions hydrologic data.

Drainage Area	Discharge Location	Design Point	Area (Acres)	Curve Number	Time of Concentration (min)
1a	Norwalk River (South)	DP1	2.8	94	5
1b	Norwalk River (South)	DP1	2.9	93	5
2	Norwalk River (North)	DP2	3.6	97	5
3	Watercourse (West)	DP3	3.1	77	10.9

Table 2 Existing Conditions Hydrologic Data

Proposed Drainage Conditions

Under proposed conditions the site will mimic existing drainage conditions. A portion of the large, centralized building fronting River Road will be demolished and replaced with a structure with a similar sized footprint. Grades surrounding the site will remain relatively flat with a new residential building located along the southwestern property line. Wetlands and the existing watercourse will not be altered and will remain protected.

Through conversations with Town staff, the site as proposed, is designed to retain the volume from 1" of stormwater runoff for the entire new proposed roof areas. Only the proposed building roof drains will connect to a new retention system. The remainder of the site stormwater runoff will bypass the retention system, and pass through hydrodynamic water quality units to provide treatment, prior to connecting to the existing drainage system within River Road. A portion of the existing 36" perforated pipe retention system is proposed to remain (approx. 350LF). Although these existing pipes are not accounted for as part of the provided volume to satisfy the retention for the 1" volume, they are proposed to connect to the new underground concrete chamber system. Through geotechnical investigations, it was found that the bottom of these existing 36" pipes to remain are within seasonal high groundwater, thus, limiting their effectiveness at retention/infiltration. However, by keeping a portion of the existing system and implementing a "new" supplemental system, allows for the preservation of the existing swale and vegetation along the southern property border. The newer system was placed at a higher elevation than the existing system as geotechnical investigations found seasonal high

groundwater at approximately 7.5 feet below existing grade. In order to keep a minimum 2-3foot separation between the underground retention system and groundwater, the elevation of the proposed system needed to be raised. In addition, a backflow preventor is proposed to prevent floodwaters from the Norwalk River from entering the system (see FEMA section below for further discussion on floodplain).

A rain garden is proposed north of Building B in a centralized curb-less island designed to capture overland flow and infiltrate the Stormwater runoff from the surrounding area. An elevated area drain will capture overflow that is not infiltrated and direct it to the closed on-site drainage system.

The proposed site will result in an increase of approximately 6,000sf of impervious area. A small underground detention system is proposed in the western portion of the site near Building B to aid in the reduction of peak flow rates at the discharge point in River Road. As previously stated, a conservative infiltration rate of 1.0 in/hr was accounted for in the hydrologic calculations and analysis.

Figure 3 illustrates the proposed "post construction" drainage conditions for the project. As shown, the Site is divided into 7 drainage areas that discharge treated stormwater to the 3 existing Design Points. Table 3 below provides a summary of the proposed conditions hydrologic data.

Drainage Area	Discharge Location	Design Point	Area (Acres)	Curve Number	Time of Concentration (min)
_1a	Norwalk River (South)	DP1	1.2	93	5
1b	Norwalk River (South)	DP1	0.6	98	5
1c	Norwalk River (South)	DP1	2.9	92	5
1d	Norwalk River (South)	DP1	1.2	98	5
2	Norwalk River (North)	DP2	3.4	96	5
3	Watercourse (West)	DP3	3.1	77	10.9

Table 3 Proposed Conditions Hydrologic Data

<u>Drainage Area 1:</u> This area will be broken into 4 segments 1a, 1b, 1c, and 1d, all of which connect within the site limits and discharge through the system in River Road to the Norwalk River (Design Point 1).

- Area 1a comprises the southwestern portion of the site. This portion of the site drains to either the rain garden or is collected with deep sump and hooded catch basins (where feasible). (Note, to be conservative with peak discharge flow rates and area limitations of the rain garden, the rain garden was not modeled).

- Area 1b is the entire roof of Building B which is connected to the offline retention system along the southern property line.

- Area 1c consists of the existing office building and landscaped courtyard area immediately south to remain along with the new parking area within the limit of work (with the exception of the new proposed parking area along Village Drive). This area is collected entirely by deep sump and hooded catch basins and treated by hydrodynamic water quality units prior to connecting to the closed drainage system in River Road and ultimately discharging to the Norwalk River (Design Point 1).

- Area 1d is the entire roof of Building A which is connected to the offline retention system along the southern property line.

<u>Drainage Area 2</u>: The area comprising drainage area 2 is primarily comprised of the existing building and existing parking area at the northern portion of the site. The proposed parking and improvements along Village Road and exiting the proposed parking garage are included in this drainage area. This area is collected by the existing drainage infrastructure and flows to a northern connection point in River Road discharging to the Norwalk River. The area going to this northern connection point is decreased under proposed conditions and therefore peak flows for all storm events have been reduced.

<u>Drainage Area 3:</u> Similar to existing conditions, drainage area 3 is comprised mostly of the steep western hillside and remaining land just off the curbing of the western parking lot or area behind Building B. This area drains to a watercourse located just off the western curbline and flows to the south (Design Point 3). The area is mostly wooded with some grass area adjacent to the parking area. The drainage area was only slightly modified due to the new building and parking area proposed. The on-site wetland system associated with this drainage area is to remain and be protected. A Wetland Mitigation Planting Plan is proposed (further detailed in the site in the site plans and wetland reports, under separate cover).

Environmentally Sensitive and Low Impact Development (LID) Techniques

Low Impact Development (LID) techniques and stormwater Best Management Practices (BMPs) implemented into the site design minimized disturbance to existing trees and vegetation with the priority at staying within existing project impervious limits. In addition, a rain garden was designed to capture runoff from a portion of the site located directly north of proposed Building B. Stormwater runoff is proposed to flow overland to the rain garden: a centralized curb-less island depressed with a raised overflow drain. Runoff is encouraged to infiltrate back into the ground and any overflow will be captured and connected to the close drainage system within the site.

As previously described herein, additional LID techniques include: catch basins with deep sumps and hooded outlets, and a new onsite retention system that is appropriately sized to capture the 1" rainfall event from the proposed roofs onsite. This system will connect to a portion of the existing retention system to provide additional volume (although the existing system to remain is not modeled due to groundwater presence, making for a conservative design approach).

Hydrologic Analysis

The rainfall-runoff response of the Site under existing and proposed conditions was evaluated for storm events with recurrence intervals of 2, 10, 25 and 100-years. Rainfall volumes used for this analysis were based on the National Weather Service NOAA, Atlas 14 data for the town of Wilton and are 3.55, 5.42, 6.59, and 8.39 inches respectively. Runoff coefficients for the pre- and post-development conditions, as previously shown in Tables 2 and 3 respectively, were determined using NRCS Technical Release 55 (TR-55) methodology as provided in HydroCAD. Drainage areas used in the analyses were described in previous sections and shown on Figures 2 and 3. The HydroCAD model is based on the NRCS Technical Release 20 (TR-20) Model for Project Formulation Hydrology. The results of the analysis, as summarized in Table 4 below, indicate that there is no increase in peak discharge rates between the existing and proposed conditions for all three discharge points.

Computations and supporting information regarding the hydrologic modeling are included in Appendix G.

Design Point	2-year	10-year	25-year	100-year
DP1: Norwalk River South				
Existing	21.7	32.3	38.7	47.5
Proposed	21.7	32.0	38.1	47.5
DP2: Norwalk River North				
Existing	14.3	20.8	24.9	31.0
Proposed	13.5	19.7	23.5	29.3
DP3: Norwalk River North				
Existing	4.6	8.9	11.7	16.0
Proposed	4.6	8.9	11.6	15.9

Table 4 Peak Discharge Rates (cfs*)

The hydrologic analysis only models the small detention/infiltration system adjacent to Building B. The larger retention system along the southern portion of the site (capturing and retaining the 1" volume from roof runoff) was not modeled in the hydrologic analysis for peak flow attenuation because this system is strictly sized for retaining that 1" volume from the roofs. It is an offline system, therefore for any larger storm events 2-year, 10-year, etc., which exceed the 1" rainfall volume, will bypass the retention system to the outlet. Therefore, any larger storm events entering will be released at a similar rate, thus not providing peak flow reduction. Modeling of this system is not necessary.

Hydraulic Analysis

The closed drainage system was designed for the 25-year storm event.

Drainage pipes were sized using Manning's Equation for full-flow capacity and the Rational Method. Additionally, the performance of the system was analyzed using StormCAD, a HEC-22 based program.

FEMA

The effective FEMA Flood Insurance Rate Map (FIRM) 09001C0383F dated June 18, 2010, as well as the associated FEMA Flood Insurance Study (FIS) for Fairfield County CT, includes Norwalk River in the vicinity of the site. Mapping shows portions of the site within the 1% (100year) and 0.2% (500yr) Annual Chance Flood Special Hazard Area (SFHAs) and the Norwalk River includes a Regulatory Floodway. VHB prepared a more detailed map of the site using the base flood elevations based on the site survey. It was found the 1% Annual Flood extends into River Road and Village Drive and up against the existing building on River Road (See Appendix B).

Compensatory Flood Storage

Due to the site being within a FEMA 100year special flood hazard area with varying base flood elevations, any filling within the Flood Zone will need to be compensated for under the proposed conditions. As documented within the Compensatory Flood Storage calculations in the Appendix, the proposed site provides adequate flood volume storage as under existing conditions, satisfying the FEMA compensatory flood volume requirement (see Appendix B).

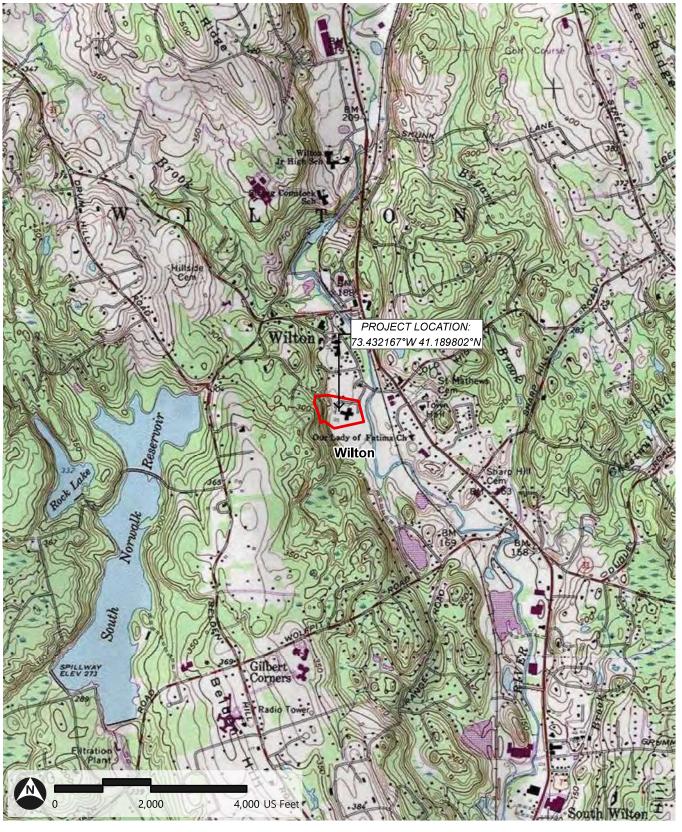
The proposed development improves site conditions by pulling the new building further back from River Road and allowing for proper grading along the frontage to protect the building. As a result, the new Building A's finish floor elevations are raised up and out of the potential 100year flood water elevations.

Figure 1 Site Locus Map

Figure 1: USGS Site Location Map

Wilton Campus Development | Wilton, Connecticut





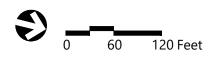
Source: USGS, VHB

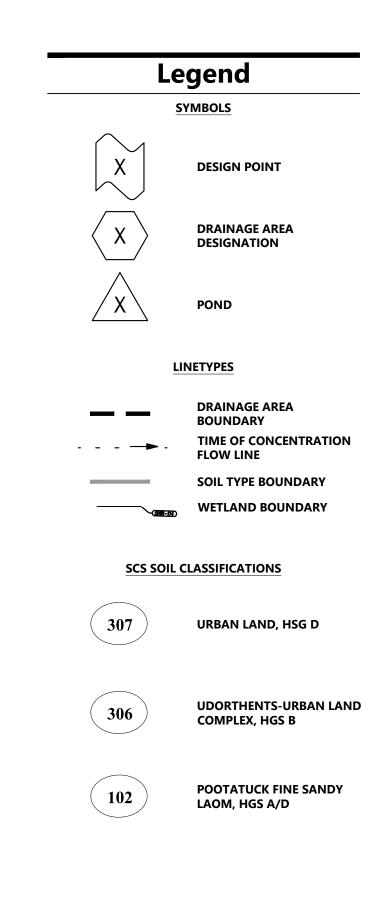
Project Location

Town Boundary

Figure 2 Existing Drainage Area









8

Existing Drainage Conditions

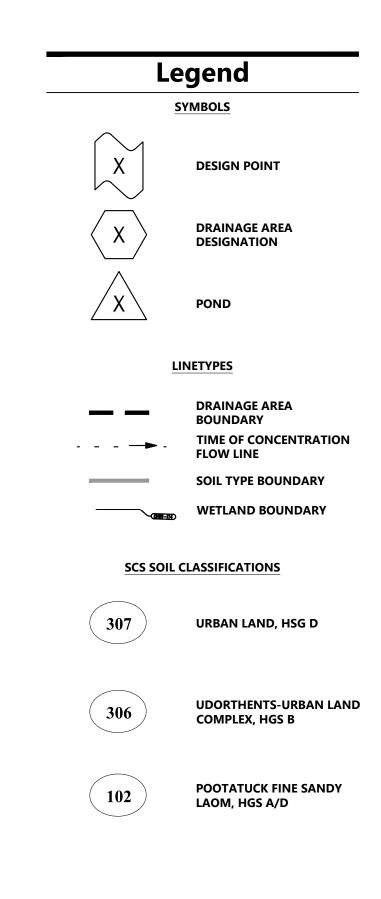
Figure

Wilton Center 21 River Road, Wilton, CT April 2024

Figure 3 Proposed Drainage Area









Proposed Drainage Conditions

Figure 3

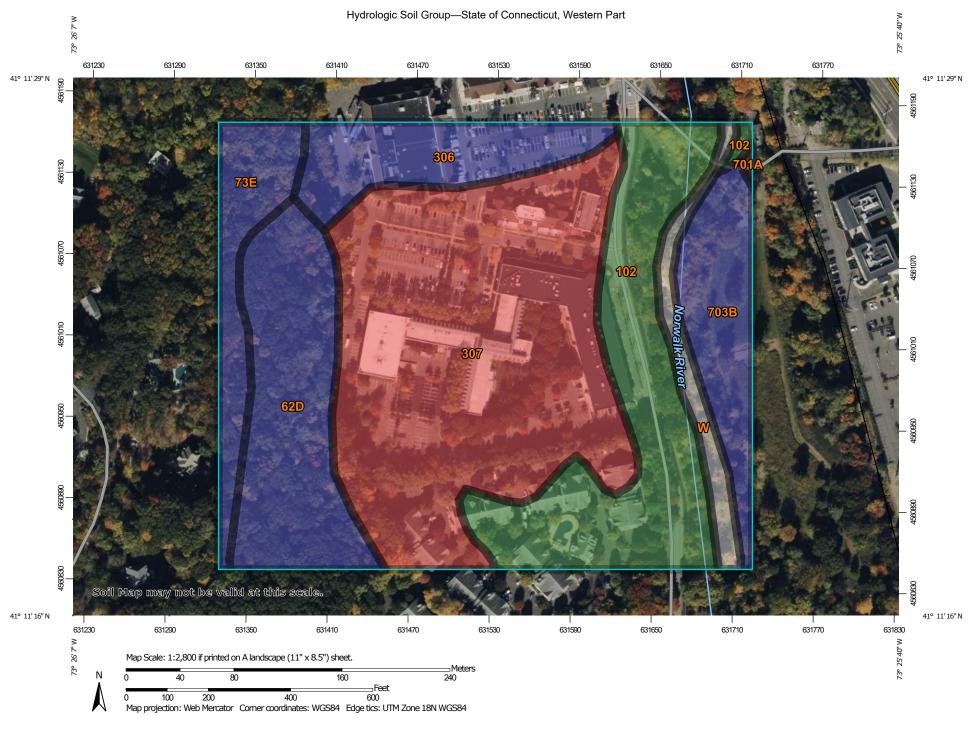
Wilton Center 21 River Road, Wilton, CT April 2024

Appendix A

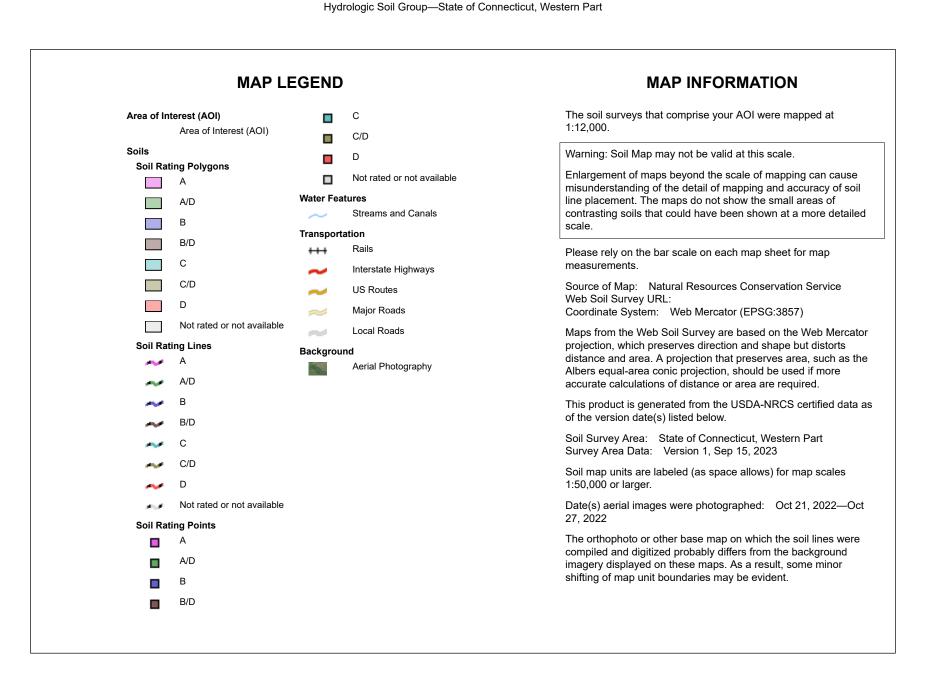
- > NRCS Soil Survey Information
- > Record Site Mapping

This page intentionally left blank.

NRCS Soil Survey Information



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
62D	Canton and Charlton fine sandy loams, 15 to 35 percent slopes, extremely stony	В	4.7	14.6%
73E	Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky	В	2.2	6.8%
102	Pootatuck fine sandy loam	A/D	6.3	19.4%
306	Udorthents-Urban land complex	В	2.6	8.1%
307	Urban land	D	12.9	39.7%
701A	Ninigret fine sandy loam, 0 to 3 percent slopes	B/D	0.0	0.1%
703B	Haven silt loam, 3 to 8 percent slopes	В	2.6	7.9%
W	Water		1.1	3.4%
Totals for Area of Interest		32.4	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

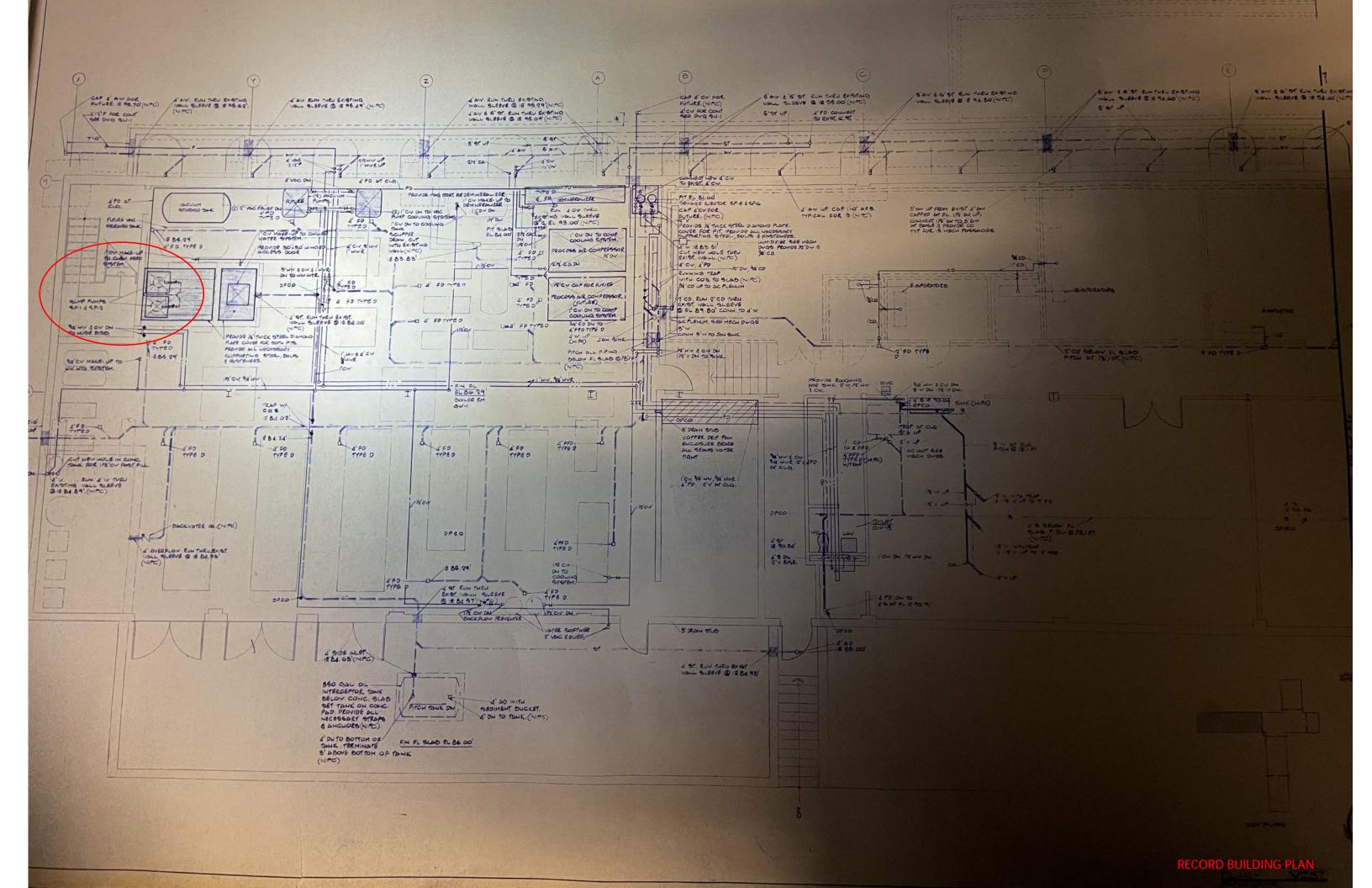
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

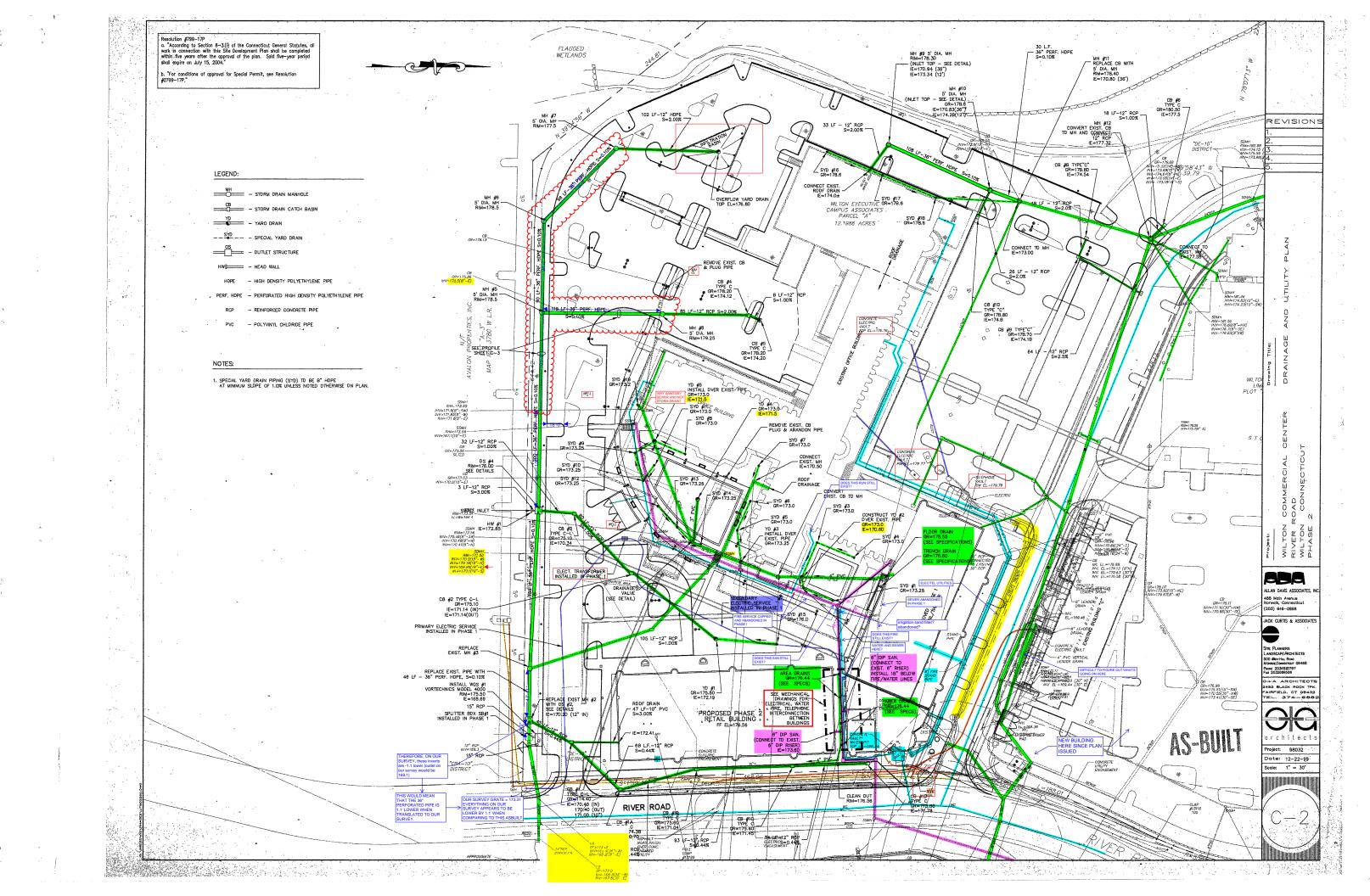
Rating Options

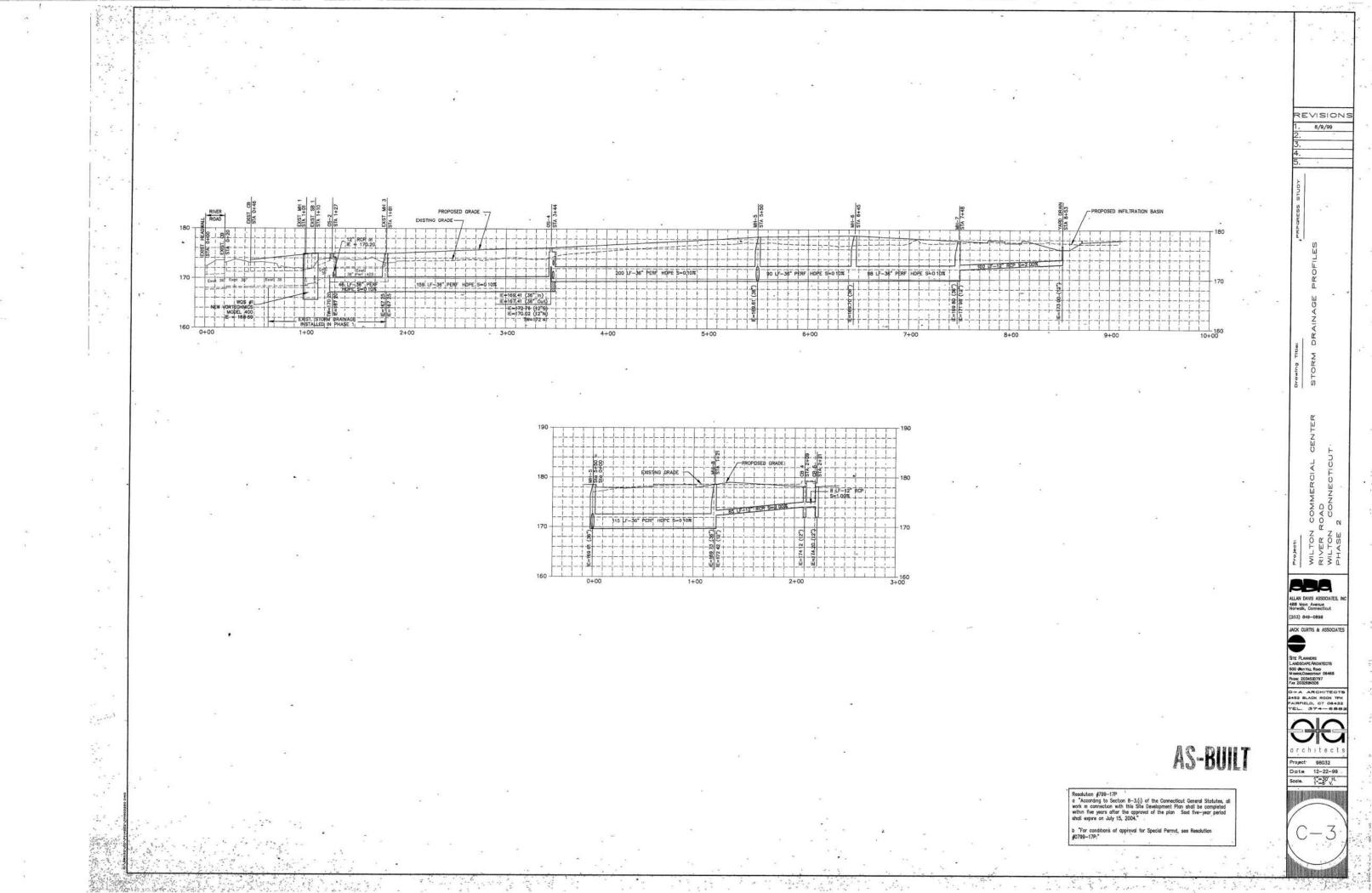
Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

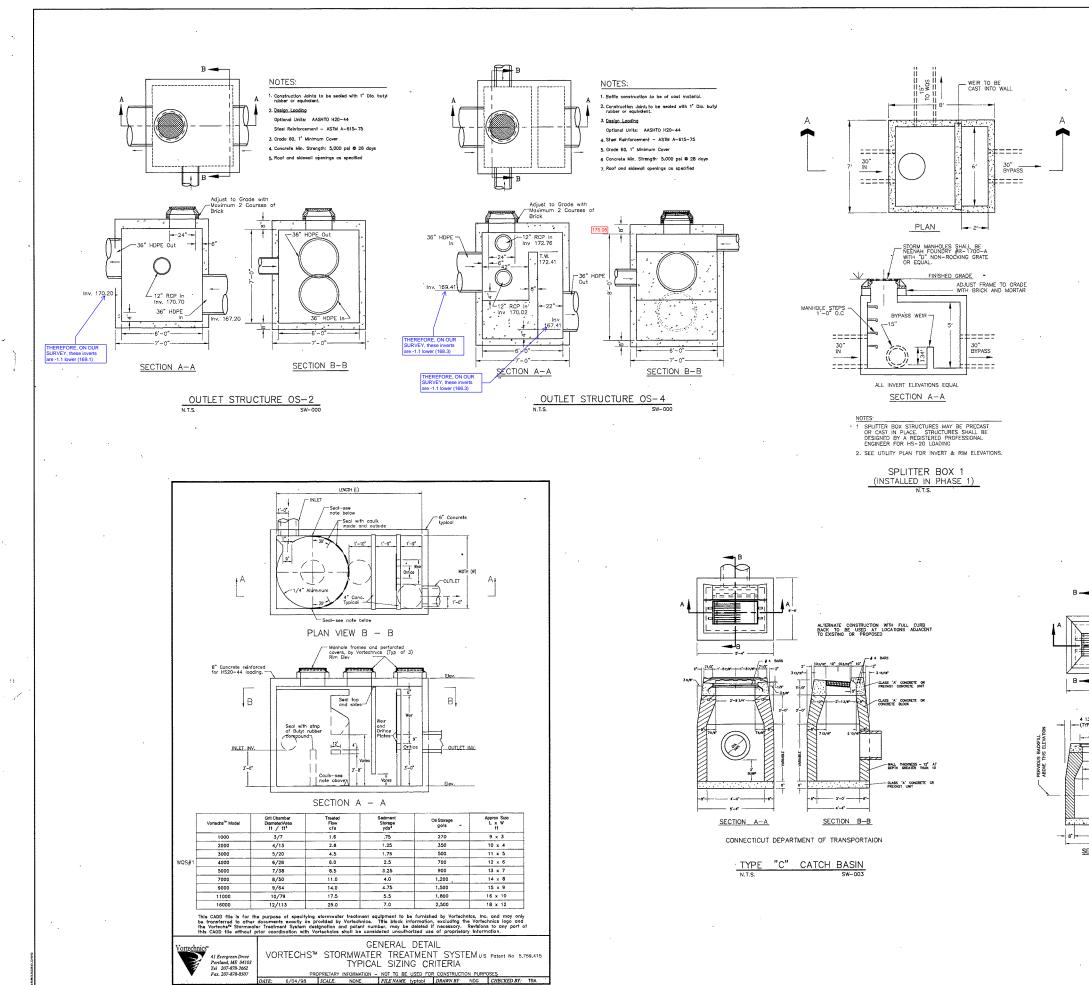
Record Site Mapping

B-4 Appendix A





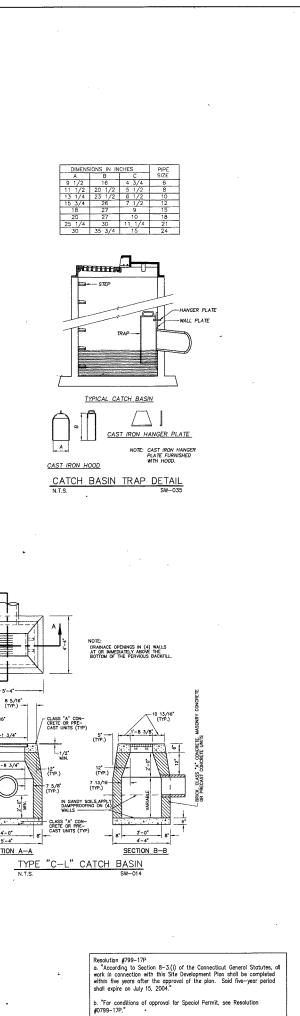




 $1 \supset 1$

4 13/16" ----(TYP.) 3'-1 3/4 4'- 0" 5'-4" SECTION A-A

- 5'-4"



RE 1. 2. 3. 4. 5.	VI 5	51	01	7	
Drawing Titia:	DRAINAGE AND UTILITY DETAILS				
Project: Drawl	WILTON COMMERCIAL CENTER DRA	RIVER ROAD	WILTON CONNECTICUT	PHASE 2	
488 Mo Norwalk (203) 8 JACK C STE PL LANDSC 500 Put Monroe C	AANNERS AANNE AANNE	s CCHIT Rote CT 7980 12- N.	е с 222- Т.S.		
		7)) /	

Appendix B

- > FEMA Floodway Map
- > Flood Storage Computations

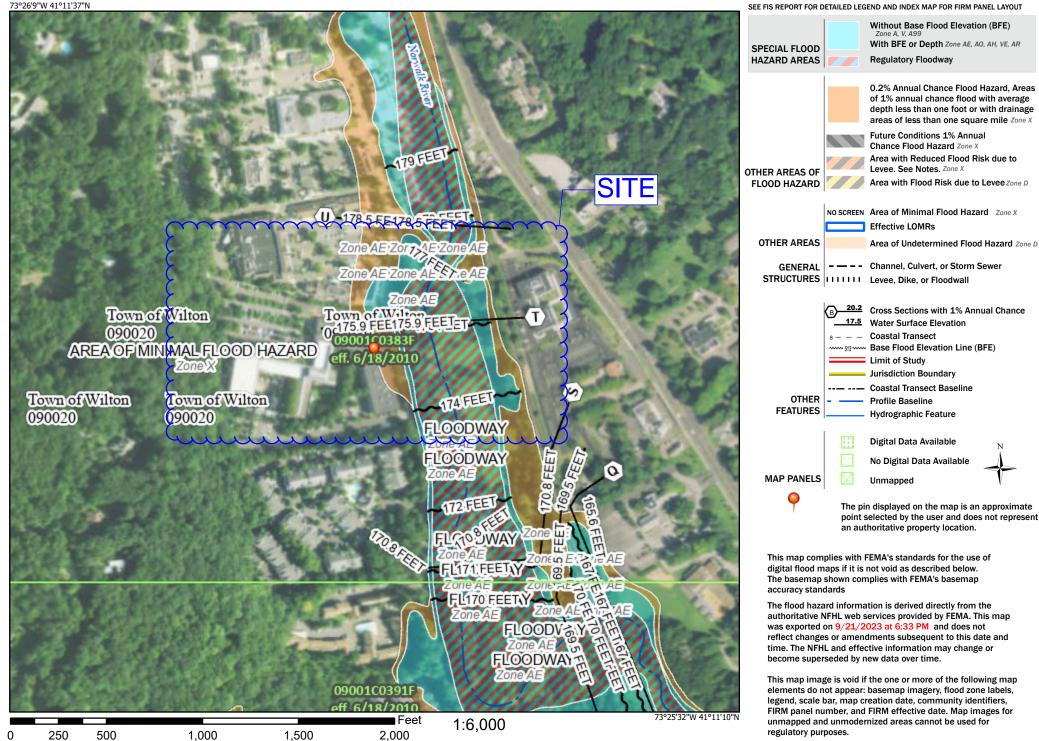
This page intentionally left blank.

FEMA Floodway Map

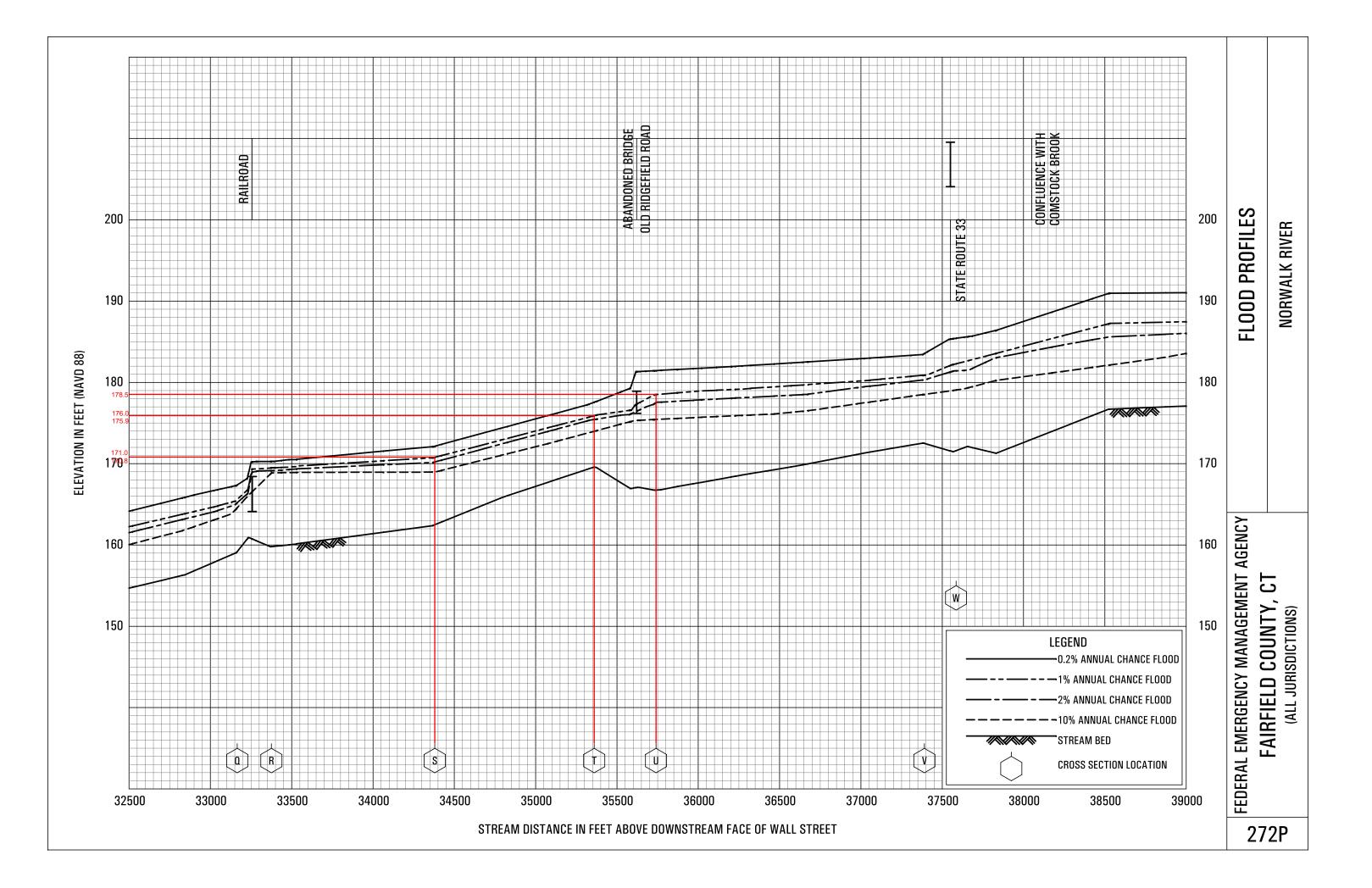
National Flood Hazard Layer FIRMette



Legend



Basemap Imagery Source: USGS National Map 2023



Flood Storage Computations

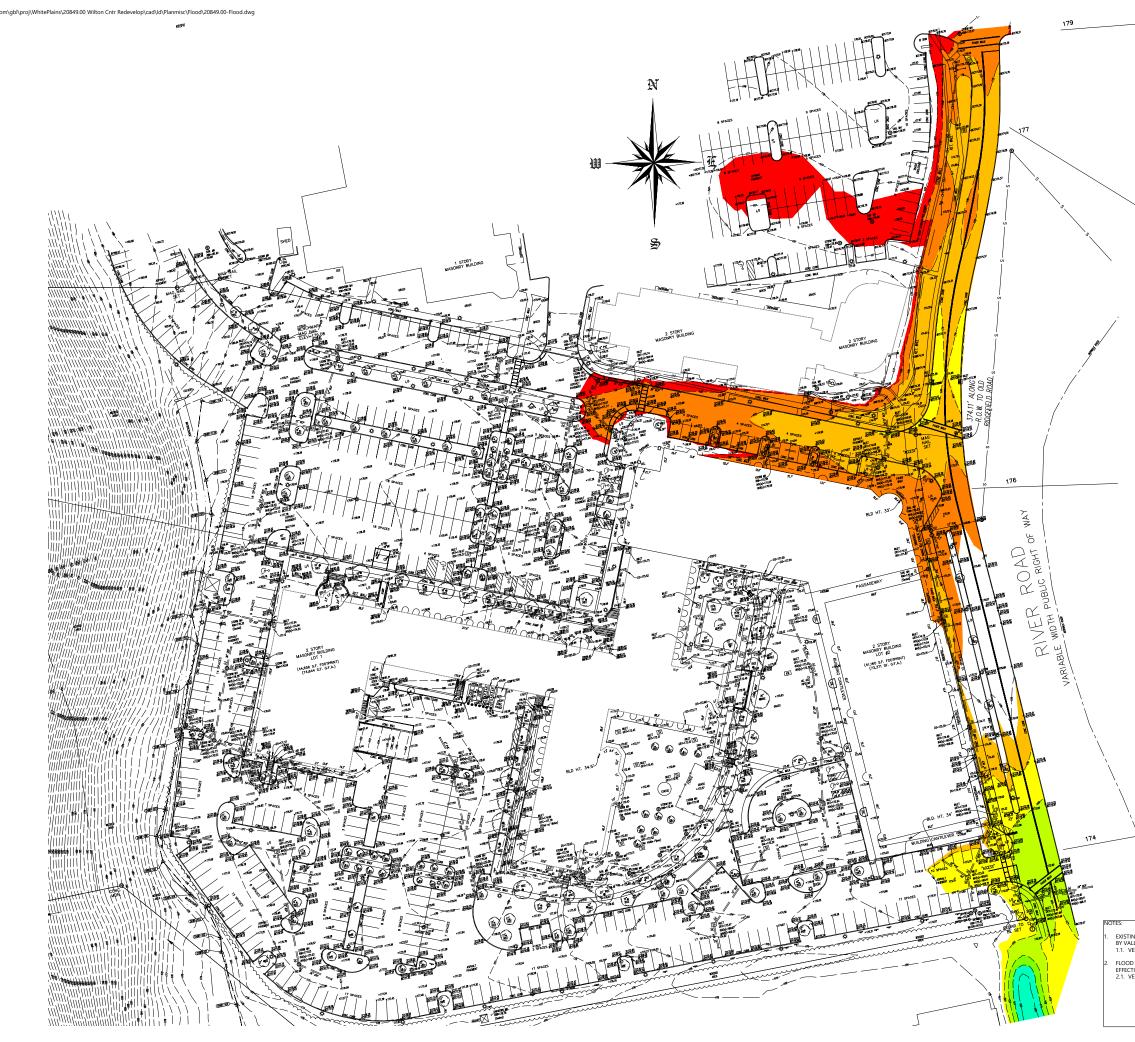
C-4 Appendix B



Title:	Existing VS Proposed Flood Storage Volume
Site Address:	21-23 River Rd, Wilton, CT
VHB Job No:	20849.00
Date:	4/16/2024

	Existing		Proo	psed
Elevation Range	Volume (CY)	Cumuliative	Volume (CY)	Cumulative
177 - 176	2434	5 <i>,</i> 898	2488	6,046
176 - 175	1880	3,464	1901	3,558
175 - 174	983	1,584	1036	1,657
174 - 173	419	601	428	621
173 - 172	107	182	118	193
172 - 171	48	75	48	75
171 - 170	27	27	27	27

Delta (CY)	Cumuliative Delta (CY)
54	148
21	94
53	73
9	20
11	11
0	0
0	0

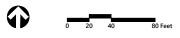




100 Great Meadow Road Suite 200 Wethersfield, CT 06109 860.807.4300

EXISTING CONDITIONS Surface Elevation Data

No.	Min. Elev.	Max. Elev.	Color	Volume
177 - 176	0.00	1.00		2434
176 - 175	1.00	2.00		1880
175 - 174	2.00	3.00		983
174 - 173	3.00	4.00		419
173 - 172	4.00	5.00		107
172 - 171	5.00	6.00		48
171 - 170	6.00	7.00		27



Wilton Center Redevelopment

15-21 River Road Wilton, Connecticut

MB

Review

MRG MRG 10/20/2023

Not Approved For Construction

Existing Conditions FEMA 100YR Base Flood Elevation Map

EXISTING CONDITIONS INFORMATION AND TOPOGRAPHY BASED OFF SURVEY PROVIDED BY VALLEY LAND SERVICES, LLC, SURVEY LATEST REVISION DATE: 10/4/2023 1.1. VERTICAL DATUM = NAVD 88 ELOOD MATRON INFORMATION IS DEPUTED BROW FEMALE COD STUDY 00001C0392E

FLOOD HAZARD INFORMATION IS DERIVED FROM FEMA FLOOD STUDY 09001C0383F EFFECTIVE DATE: JUNE 18, 2010 2.1. VERTICAL DATUM = NAVD 88 **F-1.0**

Project Number 20849.00





100 Great Meadow Suite 200 Wethersfield, CT 06109 860.807.4300

PROPOSED CONDITIONS Surface Elevation Data

No.	Min. Elev.	Max. Elev.	Color	Volume
177 - 176	0.00	1.00		2488
176 - 175	1.00	2.00		1901
175 - 174	2.00	3.00		1036
174 - 173	3.00	4.00		428
173 - 172	4.00	5.00		118
172 - 171	5.00	6.00		48
171 - 170	6.00	7.00		27



Wilton Center Redevelopment

15-21 River Road Wilton, Connecticut

MB Review

10/20/2023

MRG

Not Approved For Construction

Proposed Conditions FEMA 100YR Base Flood Elevation Map

EXISTING CONDITIONS INFORMATION AND TOPOGRAPHY BASED OFF SURVEY PROVIDE BY VALLEY LAND SERVICES, LLC, SURVEY LATEST REVISION DATE: 10/4/2023 1.1. VERTICAL DATUM = NAVD 88

FLOOD HAZARD INFORMATION IS DERIVED EFFECTIVE DATE: JUNE 18, 2010 2.1. VERTICAL DATUM = NAVD 88

F-2.0 Sheet 1 1

Project Number 20849.00

Appendix C

- > Water Quality Volumes
- > Retention sizing
- > Water Quality Unit Sizing
- > Water Quality TSS
- > StormCAD: Schematic

> StormCAD: Conduit Table (25-year storm event)

This page intentionally left blank.

Water Quality Volumes

Water Quality Volume Calculations



Project: Wilton Center Redevelopment	By: KEE	Date: 4/4/24
Location: 21 River Road, Wilton, CT	Checked: MRG	Date: 4/4/24

Basin Name	Building A (new roof only)	Building B		
Rainfall, P	1.00 in.	1.00 in.		а
Area, A	1.17 ac	0.56 ac		b
Impervious Cover Area	1.17 ac	0.56 ac		С
% Impervious, I	100 %	100 %		
Volumetric Runoff Coeff., R	0.950	0.950		d
Water Quality	0.093 ac-ft	0.044 ac-ft		e
Volume, WQV	4,045 cf	1,928 cf		
			5,973 Total (cf)	_

^a First one inch of rainfall; 2004 Connecticut Stormwater Quality Manual and per Town of Wilton

^b Area tributary to the stormwater management basin

 $^{\rm c}$ Impervious cover area tributary to the stormwater management basin

^d R=0.05+0.009*I; Section 7.4.1 from 2004 Connecticut Stormwater Quality Manual

^e WQV=P*R*A/12; Section 7.4.1 from 2004 Connecticut Stormwater Quality Manual

Retention Sizing

Summary for Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

4' underground concrete chambers OFFLINE for 1" WQV retention. System on plan will show slightly smaller since we will be able to reuse the 350' portion of the existing 36" perforated pipe that is within the existing swale under existing mature vegetation.

[43] Hint: Has no inflow (Outflow=Zero)

Volume	Invert	Avail.Sto	rage Stora	age Description
#1	170.80'	6,27	75 cf Storn	mTrapListed below Inside #2
#2	170.80'	-	0 cf Custo	om Stage Data (Prismatic)Listed below (Recalc)
			6,275	5 cf Overall - 6,275 cf Embedded = 0 cf
		6,27	75 cf Total	Available Storage
Elevatio		n.Store		
(fee		ic-feet)		
· · · ·				
170.8 171.0	-	0 392		
171.0		785		
171.5		1,177		
171.8		1,906		
171.0		2,634		
172.3		3,362		
172.5		4,091		
172.8		4,819		
173.0		5,547		
173.3		6,275		
	-	-) -		
Elevatio	n Su	rf.Area	Inc.Store	Cum.Store
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)
170.8	0	2,510	0	0
173.3	0	2,510	6,275	6,275
Device	Routing	Invert	Outlet Devi	ricos
	<u> </u>			r Exfiltration over Horizontal area Phase-In= 0.01'
#1 #2	Discarded	170.80' 173.30'		
#2	Primary	173.30		x 0.5' breadth Broad-Crested Rectangular Weir i) 0.20 0.40 0.60 0.80 1.00
			· · · · ·	glish) 2.80 2.92 3.08 3.30 3.32
			COEL (LIIY	JIGH 2.00 2.32 0.00 0.00 0.02
Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge)				

1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

Water Quality Unit Sizing



Project:	Wilton Center Redevelopment	Project #	20849
Location:	21 River Road, Wilton, CT		
Calculated by:	KEE	Date:	4/17/2024
Checked by:	MRG	Date:	4/17/2024
Title	Water Quality Flow Calculations		

102					
Area Impervious:	0.261	Acres			
Total Area [A]:	0.326	Acres			
l:	80.00	%			
R:	0.77				
WQV:	0.02	Ac-ft			
Q:	0.77	Inches			
CN:	98				
Ρ:	1.00	inch			
la:	0.041				
Tc:	5.00	minutes			
q u:	700.00				
WQF:	0.27	CFS			

103

Area Impervious:	0.570	Acres
Total Area [A]:	0.801	Acres
1:	71.22	%
R:	0.69	
WQV:	0.05	Ac-ft
Q:	0.69	Inches
CN:	97	
P:	1.00	inch
la:	0.062	
Tc:	5.00	minutes
q u:	700.00	
WQF:	0.61	CFS

107		
Area Impervious:	0.383	Acres
Total Area [A]:	0.504	Acres
1:	75.99	%
R:	0.73	
WQV:	0.03	Ac-ft
Q:	0.73	Inches
CN:	97	
P:	1.00	inch
la:	0.062	
Tc:	5.00	minutes
q u:	700.00	
WQF:	0.40	CFS

109		
Area Impervious:	0.078	Acres
Total Area [A]:	0.092	Acres
1:	84.78	%
R:	0.81	
WQV:	0.01	Ac-ft
Q:	0.81	Inches
CN:	98	
P:	1.00	inch
la:	0.041	
Tc:	5.00	minutes
q u:	700.00	
WQF:	0.08	CFS

111		
Area Impervious:	0.167	Acres
Total Area [A]:	0.182	Acres
1:	91.76	%
R:	0.88	
WQV:	0.01	Ac-ft
Q:	0.88	Inches
CN:	99	
Ρ:	1.00	inch
la:	0.041	
Tc:	5.00	minutes
q u:	700.00	
WQF:	0.17	CFS

118		
Area Impervious:	0.300	Acres
Total Area [A]:	0.356	Acres
l:	84.35	%
R:	0.81	
WQV:	0.02	Ac-ft
Q:	0.81	Inches
CN:	98	
P:	1.00	inch
la:	0.041	
Tc:	5.00	minutes
q u:	700.00	
WQF:	0.32	CFS

Water Quality TSS

Estimated Net Annual Solids Load Reduction Based on the Rational Rainfall Method



21-23 RIVER RD REDEVELOPMENT



WILTON, CT WOU 102

AREA WEIGHTED C TC	0.33 acres 0.78 5.00 minutes	CASCADE MODEL PARTICLE SIZE RAINFALL STATION	CS-3 110 34	microns	
Rainfall Intensity ¹ (in/hr)	Percent Rainfall Volume ¹	Hydraulic Loading Rate (gpm/ft2)	Removal Efficiency (%)	Incremental Remov (%)	
0.02	9.7%	0.32	100.0	9.7	
0.04	9.7%	0.65	100.0	9.7	
0.06	9.8%	0.97	100.0	9.8	
0.08	7.7%	1.29	100.0	7.7	
0.10	8.0%	1.61	100.0	8.0	
0.12	5.4%	1.94	100.0	5.4	
0.14	4.7%	2.26	100.0	4.7	
0.16	5.5%	2.58	100.0	5.5	
0.18	3.5%	2.91	100.0	3.5	
0.20	4.1%	3.23	100.0	4.1	
0.25	6.5%	4.04	100.0	6.5	
0.30	5.5%	4.84	100.0	5.5	
0.35	4.0%	5.65	100.0	4.0	
0.40	2.0%	6.46	100.0	2.0	
0.45	2.1%	7.27	100.0	2.1	
0.50	2.0%	8.07	100.0	2.0	
0.75	5.1%	12.11	100.0	5.1	
1.00	2.5%	16.15	96.7	2.4	
1.50	1.8%	24.22	89.1	1.6	
2.00	0.5%	32.29	81.5	0.4	
				99.6	
		Removal Et	fficiency Adjustment ² =	6.5%	
Predicted % Annual Rainfall Treated = 93.5			93.5%		
	Predicted Net Annual Load Removal Efficiency = 93.2%				

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

Estimated Net Annual Solids Load Reduction Based on the Rational Rainfall Method



21-23 RIVER RD REDEVELOPMENT



WILTON, CT WQU 103

AREA WEIGHTED C TC	0.80 0.73 5.00	acres minutes	CASCADE MODEL PARTICLE SIZE RAINFALL STATION	CS-3 110 34	microns
Rainfall Intensity ¹ (in/hr)		t Rainfall ume ¹	Hydraulic Loading Rate (gpm/ft2)	Removal Efficiency (%)	Incremental Remova (%)
0.02	9	.7%	0.74	100.0	9.7
0.04	9.	.7%	1.48	100.0	9.7
0.06	9.	.8%	2.22	100.0	9.8
0.08	7.	.7%	2.97	100.0	7.7
0.10	8	.0%	3.71	100.0	8.0
0.12	5	.4%	4.45	100.0	5.4
0.14	4.	.7%	5.19	100.0	4.7
0.16	5.	.5%	5.93	100.0	5.5
0.18	3.	.5%	6.67	100.0	3.5
0.20	4.	.1%	7.42	100.0	4.1
0.25	6	.5%	9.27	100.0	6.5
0.30	5	.5%	11.12	100.0	5.5
0.35	4.	.0%	12.98	99.7	4.0
0.40	2	.0%	14.83	98.0	1.9
0.45	2	.1%	16.69	96.2	2.1
0.50	2.	.0%	18.54	94.5	1.9
0.75	5	1%	27.81	85.8	4.4
1.00	2	.5%	37.08	77.0	1.9
1.50	1	.8%	55.62	59.6	1.1
2.00	0	.5%	63.50	44.7	0.2
					97.5
Removal Efficiency Adjustment ² =			6.5%		
Predicted % Annual Rainfall Treated = 93.5%					
			Predicted Net Annual Loa	a Removal Efficiency =	91.0%





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

21-23 RIVER RD REDEVELOPMENT WILTON, CT

Area Weighted C t _c CDS Model	0.50 ac 0.76 5 min 2015-4			t Site Designation Rainfall Station # reatment Capacity	WQU 107 34 1.4 cfs
<u>Rainfall</u> Intensity ¹ (in/hr)	<u>Percent Rainfall</u> <u>Volume¹</u>	<u>Cumulative Rainfall</u> <u>Volume</u>	<u>Total Flowrate</u> (cfs)	<u>Treated</u> Flowrate (cfs)	Incremental Removal (%)
0.02	9.7%	9.7%	0.01	0.01	9.4
0.04	9.7%	19.4%	0.02	0.02	9.3
0.06	9.8%	29.2%	0.02	0.02	9.4
0.08	7.7%	36.9%	0.03	0.03	7.3
0.10	8.0%	44.9%	0.04	0.04	7.7
0.12	5.4%	50.3%	0.05	0.05	5.2
0.14	4.7%	55.0%	0.05	0.05	4.4
0.16	5.5%	60.5%	0.06	0.06	5.2
0.18	3.5%	63.9%	0.07	0.07	3.2
0.20	4.1%	68.0%	0.08	0.08	3.8
0.25	6.5%	74.5%	0.10	0.10	6.0
0.30	5.5%	80.0%	0.11	0.11	5.0
0.35	4.0%	84.0%	0.13	0.13	3.6
0.40	2.0%	86.0%	0.15	0.15	1.8
0.45	2.1%	88.1%	0.17	0.17	1.9
0.50	2.0%	90.2%	0.19	0.19	1.8
0.75	5.1%	95.3%	0.29	0.29	4.3
1.00	2.5%	97.8%	0.38	0.38	1.9
1.50	1.8%	99.5%	0.57	0.57	1.2
2.00	0.5%	100.0%	0.76	0.76	0.3
	92.8 Removal Efficiency Adjustment ² = 6.5% Predicted % Annual Rainfall Treated = 93.5% Predicted Net Annual Load Removal Efficiency = 86.4% 1 - Based on 10 years of hourly precipitation data from NCDC station 806, Bridgeport WSO ARPT, Fairfield County, C				
		Predicted Net	Predicted % Annual t Annual Load Rem tation 806, Bridgepo	Rainfall Treated = oval Efficiency = rt WSO ARPT, Fai	93 86 rfield Cou





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

21-23 RIVER RD REDEVELOPMENT WILTON, CT

Area Weighted C t _c CDS Model	0.09 ac 0.81 5 min 2015-4			t Site Designation Rainfall Station # reatment Capacity	WQU 109 34 1.4 cfs	
<u>Rainfall</u> Intensity ¹ (in/hr)	<u>Percent Rainfall</u> <u>Volume¹</u>	<u>Cumulative Rainfall</u> <u>Volume</u>	<u>Total Flowrate</u> (cfs)	<u>Treated</u> Flowrate (cfs)	Incremental Removal (%)	
0.02	9.7%	9.7%	0.00	0.00	9.4	
0.04	9.7%	19.4%	0.00	0.00	9.4	
0.06	9.8%	29.2%	0.00	0.00	9.5	
0.08	7.7%	36.9%	0.01	0.01	7.4	
0.10	8.0%	44.9%	0.01	0.01	7.8	
0.12	5.4%	50.3%	0.01	0.01	5.3	
0.14	4.7%	55.0%	0.01	0.01	4.5	
0.16	5.5%	60.5%	0.01	0.01	5.3	
0.18	3.5%	63.9%	0.01	0.01	3.3	
0.20	4.1%	68.0%	0.01	0.01	3.9	
0.25	6.5%	74.5%	0.02	0.02	6.3	
0.30	5.5%	80.0%	0.02	0.02	5.3	
0.35	4.0%	84.0%	0.03	0.03	3.9	
0.40	2.0%	86.0%	0.03	0.03	1.9	
0.45	2.1%	88.1%	0.03	0.03	2.0	
0.50	2.0%	90.2%	0.04	0.04	1.9	
0.75	5.1%	95.3%	0.06	0.06	4.8	
1.00	2.5%	97.8%	0.07	0.07	2.3	
1.50	1.8%	99.5%	0.11	0.11	1.6	
2.00	0.5%	100.0%	0.15	0.15	0.4	
1 - Based on 1	96.4 Removal Efficiency Adjustment ² = 6.5% Predicted % Annual Rainfall Treated = 93.5% Predicted Net Annual Load Removal Efficiency = 89.9% 1 - Based on 10 years of hourly precipitation data from NCDC station 806, Bridgeport WSO ARPT, Fairfield County, CT					
2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.						





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

21-23 RIVER RD REDEVELOPMENT WILTON, CT

Volume1 9.7% 9.7% 9.8%	Cumulative Rainfall Volume 9.7%	Total Flowrate	Treated					
9.7%	0 70/	<u>(cfs)</u>	<u>Treated</u> Flowrate (cfs)	<u>Incremental</u> Removal (%)				
	÷	0.00	0.00	9.4				
9.8%	19.4%	0.01	0.01	9.4				
	29.2%	0.01	0.01	9.5				
7.7%	36.9%	0.01	0.01	7.4				
8.0%	44.9%	0.02	0.02	7.8				
5.4%	50.3%	0.02	0.02	5.2				
4.7%	55.0%	0.02	0.02	4.5				
5.5%	60.5%	0.02	0.02	5.3				
				3.3				
				3.9				
	74.5%			6.2				
				5.2				
				3.8				
				1.9				
	88.1%	0.07	0.07	2.0				
	90.2%	0.08	0.08	1.9				
5.1%	95.3%	0.12	0.12	4.7				
				2.2				
				1.5				
0.5%	100.0%	0.31	0.31	0.4				
95.4 Removal Efficiency Adjustment ² = 6.5% Predicted % Annual Rainfall Treated = 93.5% Predicted Net Annual Load Removal Efficiency = 89.0% 1 - Based on 10 years of hourly precipitation data from NCDC station 806, Bridgeport WSO ARPT, Fairfield County, CT								
	3.5% 4.1% 6.5% 5.5% 4.0% 2.0% 2.1% 2.0% 5.1% 2.5% 1.8% 0.5%	4.1% 68.0% 6.5% 74.5% 5.5% 80.0% 4.0% 84.0% 2.0% 86.0% 2.1% 88.1% 2.0% 90.2% 5.1% 95.3% 2.5% 97.8% 1.8% 99.5% 0.5% 100.0%	4.1% 68.0% 0.03 6.5% 74.5% 0.04 5.5% 80.0% 0.05 4.0% 84.0% 0.05 2.0% 86.0% 0.06 2.1% 88.1% 0.07 2.0% 90.2% 0.08 5.1% 95.3% 0.12 2.5% 97.8% 0.15 1.8% 99.5% 0.23 0.5% 100.0% 0.31	4.1% $68.0%$ 0.03 0.03 $6.5%$ $74.5%$ 0.04 0.04 $5.5%$ $80.0%$ 0.05 0.05 $4.0%$ $84.0%$ 0.05 0.05 $2.0%$ $86.0%$ 0.06 0.06 $2.1%$ $88.1%$ 0.07 0.07 $2.0%$ $90.2%$ 0.08 0.08 $5.1%$ $95.3%$ 0.12 0.12 $2.5%$ $97.8%$ 0.15 0.15 $1.8%$ $99.5%$ 0.23 0.23 $0.5%$ $100.0%$ 0.31 0.31				





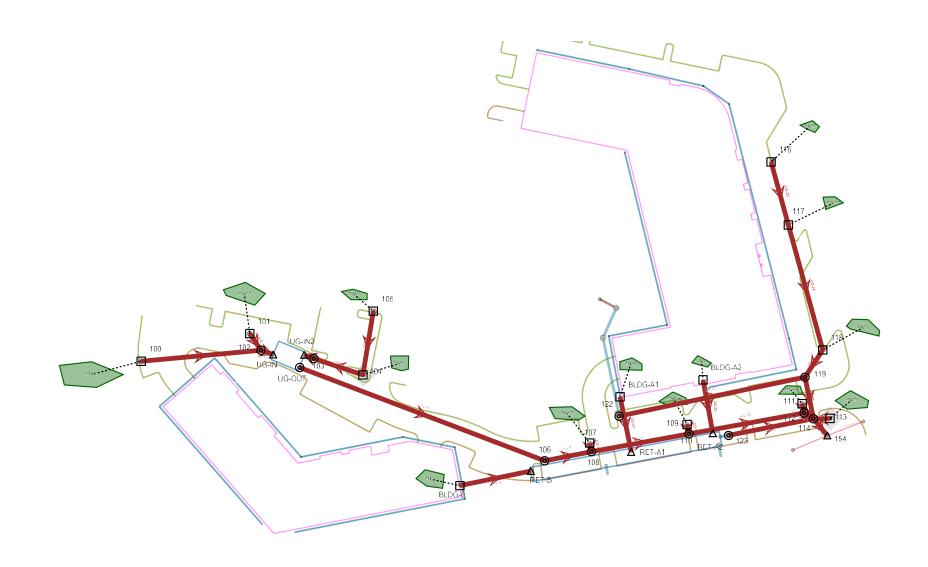
CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

21-23 RIVER RD REDEVELOPMENT WILTON, CT

Weighted C t _c CDS Model	0.36 ac 0.81 5 min 2015-4		Unit Site Designation WQU 1 Rainfall Station # 34 CDS Treatment Capacity 1.4 cfs						
<u>Rainfall</u> Intensity ¹ (in/hr)	<u>Percent Rainfall</u> <u>Volume¹</u>	<u>Cumulative Rainfall</u> <u>Volume</u>	<u>Total Flowrate</u> (cfs)	<u>Treated</u> Flowrate (cfs)	<u>Incremental</u> Removal (%)				
0.02	9.7%	9.7%	0.01	0.01	9.4				
0.04	9.7%	19.4%	0.01	0.01	9.4				
0.06	9.8%	29.2%	0.02	0.02	9.5				
0.08	7.7%	36.9%	0.02	0.02	7.4				
0.10	8.0%	44.9%	0.03	0.03	7.7				
0.12	5.4%	50.3%	0.03	0.03	5.2				
0.14	4.7%	55.0%	0.04	0.04	4.4				
0.16	5.5%	60.5%	0.05	0.05	5.2				
0.18	3.5%	63.9%	0.05	0.05	3.3				
0.20	4.1%	68.0%	0.06	0.06	3.9				
0.25	6.5%	74.5%	0.07	0.07	6.1				
0.30	5.5%	80.0%	0.09	0.09	5.1				
0.35	4.0%	84.0%	0.10	0.10	3.7				
0.40	2.0%	86.0%	0.11	0.11	1.8				
0.45	2.1%	88.1%	0.13	0.13	1.9				
0.50	2.0%	90.2%	0.14	0.14	1.8				
0.75	5.1%	95.3%	0.22	0.22	4.4				
1.00	2.5%	97.8%	0.29	0.29	2.1				
1.50	1.8%	99.5%	0.43	0.43	1.3				
2.00	0.5%	100.0%	0.57	0.57	0.3				
1 - Based on 1 2 - Reduction o	93.9 Removal Efficiency Adjustment ² = 6.5% Predicted % Annual Rainfall Treated = 93.5% Predicted Net Annual Load Removal Efficiency = 87.5% 1 - Based on 10 years of hourly precipitation data from NCDC station 806, Bridgeport WSO ARPT, Fairfield County, CT								

StormCAD: Schematic

Scenario: Base



StormCAD: Conduit Table (25-year Storm Event)

Scenario: Base Current Time Step: 0 h FlexTable: Conduit Table

Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (Scaled) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Capacity (Full Flow) (cfs)	Flow / Capacity (Design) (%)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Cover (Start) (ft)	Cover (Stop) (ft)
100	173.90	102	173.35	130.7	0.004	10.0	0.013	0.94	2.78	0.62	1.42	65.9	174.39	173.97	1.77	3.12
101	173.80	102	173.60	21.7	0.009	12.0	0.013	1.28	4.04	0.42	3.42	37.5	174.28	174.02	2.00	2.70
102	173.35	UG-IN	173.20	14.1	0.017	12.0	0.013	2.12	5.74	0.51	4.60	46.0	173.97	173.71	2.95	3.20
BLDG-B	173.00	RET-B	171.50	78.7	0.019	12.0	0.013	4.37	7.08	0.73	4.92	88.9	173.88	172.23	4.50	2.50
UG-OUT	173.25	106	171.80	284.8	0.005	18.0	0.013	6.55	4.78	0.99	7.50	87.4	174.34	172.79	2.85	1.10
106	171.80	108	171.20	51.9	0.012	18.0	0.013	6.55	6.63	1.36	11.30	58.0	172.79	172.56	1.10	1.50
108	171.20	110	170.90	107.7	0.003	24.0	0.013	9.84	4.24	1.27	11.94	82.5	172.56	172.17	1.00	2.00
112	170.40	114	170.20	11.9	0.017	24.0	0.013	11.56	8.78	1.01	29.34	39.4	171.62	171.21	1.40	2.50
114	167.75	154	167.60	23.7	0.006	30.0	0.013	31.76	7.58	1.92	32.65	97.3	169.73	169.52	4.45	1.90
107	171.40	108	171.20	9.6	0.024	12.0	0.013	3.30	4.20	1.36	5.56	59.3	172.63	172.56	1.70	2.00
111	170.50	112	170.40	10.4	0.011	12.0	0.013	1.34	1.71	1.22	3.66	36.7	171.63	171.62	1.80	2.40
105	174.30	104	173.80	70.2	0.007	12.0	0.013	1.47	3.81	0.90	3.01	48.9	174.81	174.70	2.00	2.00
104	173.80	103	173.40	53.1	0.008	15.0	0.013	4.96	5.29	0.89	5.78	85.8	174.70	174.29	1.75	2.75
103	173.40	UG-IN2	173.25	14.3	0.012	15.0	0.013	4.91	6.13	0.80	6.94	70.8	174.30	174.05	2.75	2.90
110	170.90	112	170.40	127.1	0.004	24.0	0.013	10.39	4.93	1.22	14.19	73.2	172.17	171.62	2.00	1.40
109	171.60	110	171.40	10.3	0.022	12.0	0.013	0.64	4.58	0.77	5.31	12.1	172.16	172.17	2.00	2.50
113	168.50	114	168.30	18.0	0.011	18.0	0.013	0.40	2.97	1.43	11.08	3.6	169.73	169.73	2.00	4.90
BLDG-A1	171.80	RET-A1	171.50	57.6	0.005	15.0	0.013	4.57	4.33	0.87	4.66	98.0	172.79	172.37	2.70	2.25
BLDG-A2	171.80	RET-A2	171.50	56.5	0.005	15.0	0.013	4.57	4.37	0.87	4.71	97.0	172.78	172.37	2.70	2.35
116	171.90	117	171.50	71.1	0.006	12.0	0.013	0.87	3.04	0.39	2.67	32.5	172.29	171.89	1.80	2.30
117	171.30	118	170.60	140.9	0.005	12.0	0.013	1.33	3.24	0.61	2.51	52.9	171.82	171.21	2.50	1.70
118	170.60	119	170.20	35.4	0.011	15.0	0.013	2.32	5.05	0.50	6.87	33.8	171.21	170.70	1.45	2.85
119	167.90	114	167.75	46.1	0.003	24.0	0.013	10.47	4.58	1.98	12.90	81.1	169.81	169.73	4.40	4.95
122	168.45	119	167.90	206.4	0.003	24.0	0.013	8.17	4.02	1.91	11.68	70.0	170.03	169.81	4.55	4.40
123	172.40	114	172.00	94.0	0.004	24.0	0.013	12.33	5.26	1.26	14.76	83.6	173.80	173.26	1.00	0.70

\\vhb\gbl\proj\WhitePlains\20849.00 Wilton Cntr Redevelop\tech\Drainage\StormCAD\20849_STormCAD.stsw

Appendix D

> Geotechnical Report

This page intentionally left blank.

Geotechnical Report



April 18, 2024

Consulting Engineers and Scientists

Nicholas Brown KIMCO Realty 500 North Broadway, Suite 201 Jericho, NY 11753

Reference: Site Infiltration Testing Results 21-23 River Road Redevelopment Wilton, CT

Dear Mr. Brown:

This letter report presents the results of GEI's recent test boring investigations and infiltration testing at the site.

Project Understanding

We understand proposed development on the referenced property is to consist of two (2) new multi-use buildings constructed over the footprint of the existing retail and commercial campus. Site grades are expected to remain largely consistent between the current and new developments.

To date, we have been provided with the "*Grading and Drainage Plan, C-3.0,*", dated 04/18/24, by VHB. We understand at this time that site stormwater management is to be accomplished using a series of underground detention chambers installed beneath the current (and future) parking areas along the south side of the property.

Test Borings

The boring locations were laid out from the provided site plan using approximate measurements from site features and handheld GPS. Approximate boring locations relative to the site plan are shown on Figure 1.

Five (5) soil test borings (VB-1 through VB-5) were performed at the site on April 3, 2024, by Cisco Geotechnical, LLC, under subcontract to GEI, using a GeoProbe rig. The appropriate one-call utility location service (Call Before You Dig) was contacted prior to our arrival. Each boring location was also pre-scanned for utilities using geophysical methods. Boring logs are attached.

Borings were first advanced using augering techniques through asphalt to at or near the requested infiltration testing depth. Infiltration testing was then conducted at most locations using the procedures referenced below. Following completion of this testing, soil samples were obtained using a continuous macrocore sampler to up to 5 feet below the testing interval. Each boring was logged and photographed by a GEI representative.

All borings were backfilled with drill cuttings upon completion and patched at the surface using

Infiltration Testing Results, Wilton, CT April 18, 2024 Page 2

cold-patch asphalt.

Elevations referenced in this report and on the attached boring logs were estimated from the provided topographic plan of the property.

In-place Permeability Testing

Downhole falling-head infiltration testing was conducted within all borings, with exception of VB-3, at depths of 4.2 to 5.0 feet below existing grade. In borings VB-3 and VB-4, infiltration testing was initially unsuccessful at depth due to proximity of the groundwater table. A second test was then conducted at shallower depth at VB-4 in an offset boring.

Following advancement of the boring to the testing depth, approximately 12 inches of filter sand was installed within the borehole and a 2-inch PVC casing suitably embedded. Falling-head testing was then conducted, the results of which are attached.

Subsurface Conditions

The referenced property lies on a broad sand and gravel outwash plain extending westward from the Norwalk River and adjacent River Road.

Soils encountered during the investigation were generally classified as silty gravelly sand to sandy gravel with about 10 to 20 percent non-plastic fines and about 30 to 55 percent gravel to cobbles. Materials were also noted within the sampler to be locked in a tight matrix.

Groundwater Conditions

Groundwater was directly measured in borings VB-3 and VB-4 at depths of 8.0 feet and 7.5 feet, respectively. At the other locations, groundwater measurements were influenced by the addition of water for infiltration testing, but were interpreted from soil and sampler conditions to be at similar depths. We note that this investigation was conducted during an exceedingly wet seasonal pattern.

The groundwater conditions affecting this facility are expected to be highly reflective of seasonal patterns and, in particular, water levels in the Norwalk River. Groundwater measurements made at different times and different locations may be significantly different than the measurements taken as part of this investigation.

Subsurface Drainage Design

Infiltration testing results, where not influenced by obstructions or other outlying features (as noted on the testing results), varied between 0.95 and 5.04 inches/hour. In boring VB-2, in our opinion, introduction of water during the first test appears to have opened a preferential water path and influenced the second run. Boring VB-1 appears to have encountered a dormant utility at the testing depth, which caused restriction of downward infiltration.

Based on the results of the borings, proposed stormwater management features would likely be founded in relatively uniform, moderately well-draining sands and gravels. The investigation

Infiltration Testing Results, Wilton, CT April 18, 2024 Page 3

program included in-place permeability testing within four (4) of the test borings, the results of which are attached. Based on these results, we recommend assuming a field-measured infiltration rate of **2.0 inches/hour** for design.

Per CT DEEP regulations, a factor of safety of 2.0 should be applied to the field-measured value for stormwater calculations.

Closure

We look forward to our continued efforts in moving this project forward. Please call Matt at (860) 368-5301 should you have any questions or require any clarifications.

Sincerely, GEI CONSULTANTS, INC.

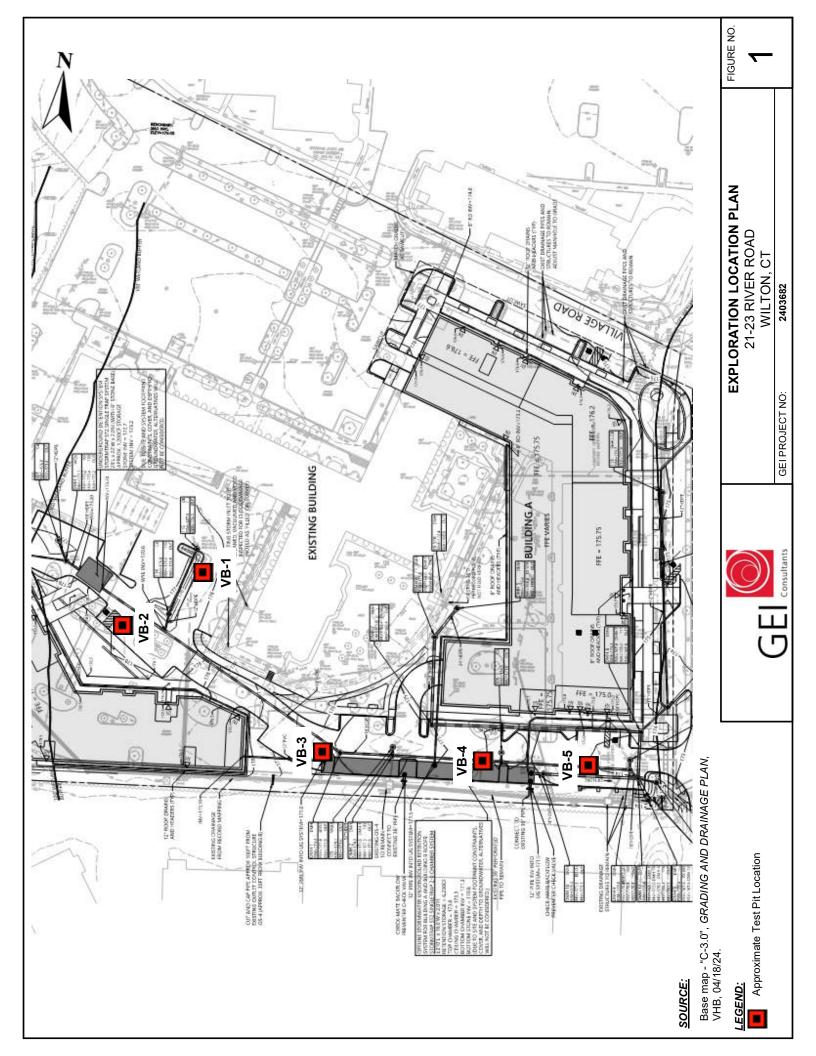
up

Matthew Glunt, P.E. Senior Geotechnical Engineer

Enclosure: Exploration Location Plan Boring Logs Infiltration Testing Results

alm

Thomas Rezzani, E.I.T. Geotechnical Professional



			RMATION	Location	Diam					BORING
			See Boring				DATE START/END:	1/3/202	24 - 4/3/2024	
			TUM:				DRILLING COMPANY:			VB-1
			l (ft): 8.0				DRILLER NAME: J. H	-		
			T. Rezza				RIG TYPE: 7822DT			PAGE 1 of 1
			ORMATIO	N						
			E: <u>N/A</u>				CASING I.D./O.D.: _N			
			D.: <u>3.25</u>		ncn		DRILL ROD O.D.:N	/I		REL I.D./O.D. NA / NA
					.5 4/3/202	24 GW leve	l interpreted			
							·			
	ABBRI	EVIATIO	RQD WOF	= Recovery	Length ality Designa Sound Core of Rods	ation s>4 in / Pen.	S = Split Spoon Sample C = Core Sample U = Undisturbed Sample % SC = Sonic Core DP = Direct Push Sample HSA = Hollow-Stem Auger		Qp = Pocket Penetrometer Strength Sv = Pocket Torvane Shear Strength LL = Liquid Limit PI = Plasticity Index PID = Photoionization Detector I.D./O.D. = Inside Diameter/Outside D	NA, NM = Not Applicable, Not Measured Blows per 6 in.: 140-lb hammer falling 30 inches to drive a 2-inch-O.D. split spoon sampler. iameter
Γ			Sa	ample Inf	ormation			ne		
	Elev. (ft)	Depth (ft)	Sample No.	Depth (ft)	Pen./ Rec. (in)	Blows per 6 in. or RQD	Drilling Remarks/ Field Test Data	Layer Name	Soil and I	Rock Description
	-	_								SILTY SAND WITH GRAVEL (SM); gravel, ~15% NP fines, brown,
GEI DATA TEMPLATE 2013.GDT 4/18/24	- - 170	_ 5	S1	3 to 8	60/49		Filter sand introduced @ 3.0-4.2 ft. Infiltration test @ 4.2 ft.	SAND & GRAVEL	SAND (GW ² GM); ~55% F-C fines, brown, wet (test water	DED GRAVEL WITH SILT AND gravel, ~35% F-C sand, ~10% NP).
GEI WOBURN STD 1-LOCATION-LAYER NAME WILTON CAMPUS SW BORINGS.GPJ GEI DATA TEMPLATE 2013.GDT 4/18/24		- - 10 -							Planned Extent. Backfilled with drill cuttings a	and cold patch asphalt.
	NOTES	3:						CITY	JECT NAME: 21-23 River Rd Re ISTATE: Wilton, Connecticut PROJECT NUMBER: 2403682	development GEI Consultants



VB- 1 (3.0 to 8.0 FT) <u>Photographer:</u> T. Rezzani Note Filter Sand at top of sample



			RMATION		Dian					BORING
			See Boring				DATE START/END:	4/3/20	24 - 4/3/2024	
			TUM:				DRILLING COMPANY			VB-2
			I (ft): 9.0				DRILLER NAME: J.	-		
			T. Rezza				RIG TYPE: 7822DT			PAGE 1 of 1
			ORMATIO E: N/A	N			CASING I.D./O.D.: N	Δ/ ΝΔ		REL TYPE: N/A
			D.: 3.25	inch / 6.5 i	inch		DRILL ROD O.D.: N			REL I.D./O.D. NA / NA
			THOD: G							<u></u>
w	ATE	R LEVE	L DEPTHS	(ft): <u></u>	.5 4/3/202	24 GW leve	l interpreted			
A	BBRI	EVIATIC	RQE	. = Recovery) = Rock Qu	/ Length ality Designa Sound Core of Rods	ation es>4 in / Pen.	S = Split Spoon Sample C = Core Sample U = Undisturbed Sample % SC = Sonic Core DP = Direct Push Sample HSA = Hollow-Stem Auger		NA, NM = Not Applicable, Not Measured Blows per 6 in.: 140-lb hammer falling 30 inches to drive a 2-inch-O.D. split spoon sampler. iameter	
			S	ample Inf	ormation			he		
	lev. (ft)	Depth (ft)	Sample No.	Depth (ft)	Pen./ Rec. (in)	Blows per 6 in. or RQD	Drilling Remarks/ Field Test Data	Layer Name	Soil and I	Rock Description
RINGS.GPJ_GEI DATA TEMPLATE 2013.GDT_4/18/24 	- - - - 70	- 5	S1	4 to 9	60/39		Filter sand introduced @ 4.0-5.0 ft. Infiltration test @ 5.0 ft.	SAND & GRAVEL	~70% F-C sand, ~15% F-C sobbles, brown dry.	SILTY SAND WITH GRAVEL (SM); gravel, ~15% NP fines, frequent VITH GRAVEL (SM); ~45% F-C % NP fines, brown, wet (test water).
GEI WOBURN STD 1-LOCATION-LAYER NAME WILTON CAMPUS SW BORINGS.GPJ GEI DATA TEMPLATE 2013.GDT 4/18/24	- - - - OTES	— 10 - - -						PRO	Backfilled with drill cuttings a	
GEI WOBUI								СІТҮ	/STATE: Wilton, Connecticut PROJECT NUMBER: 2403682	GEI Consultants



VB- 2 (4.0 to 9.0 FT) <u>Photographer:</u> T. Rezzani Note Filter Sand at top of sample



			RMATION							BORING
			ee Boring							BORING
			FACE EL.	· /						VB-3
								-		VD-J
			(ft): <u>13.</u> T. Rezza				DRILLER NAME: H RIG TYPE: 7822DT	тарр		
Ľ			1. INC22d							PAGE 1 of 1
	RILLI	NG INF	ORMATION	1						
F	IAMM	ER TYP	E: N/A				CASING I.D./O.D.: N	∿ NA	CORE BAR	RREL TYPE:N/A
			D.: 3.25		nch		DRILL ROD O.D.: N			RREL I.D./O.D. NA / NA
			HOD:Ge							
۷	VATE	R LEVEI	DEPTHS	(ft): <u></u>	.0 4/3/202	24				
A	BBRI	EVIATIO	RQD	= Recovery = Rock Qua	Length ality Designa Sound Core of Rods	tion s>4 in / Pen.	S = Split Spoon Sample C = Core Sample U = Undisturbed Sample SC = Sonic Core DP = Direct Push Sample HSA = Hollow-Stem Auger		Qp = Pocket Penetrometer Strength Sv = Pocket Torvane Shear Strength LL = Liquid Limit PI = Plasticity Index PID = Photoionization Detector I.D./O.D. = Inside Diameter/Outside D	NA, NM = Not Applicable, Not Measured Blows per 6 in.: 140-lb hammer falling 30 inches to drive a 2-inch-O.D. split spoon sampler. iiameter
			Sa	ample Inf	ormation			ne		
	Elev. (ft)	Depth (ft)	Sample No.	Depth (ft)	Pen./ Rec. (in)	Blows per 6 in. or RQD	Drilling Remarks/ Field Test Data	Layer Name		Rock Description
	_	_								WIDELY GRADED SAND WITH vl); ~50% F-C sand, ~40% F-C vn, dry to moist.
4/18/24	-	-					Rig chatter (cobbles)			
GEI WOBURN STD 1-LOCATION-LAYER NAME WILTON CAMPUS SW BORINGS GFJ GEI DATA TEMPLATE 2013.GDT 4/18/24	170 — - -	— 5 — —						SAND & GRAVEL		
CAMPUS SW BURINGS.GPJ	_	- 10	S1	8 to 13	60/51					ADED GRAVEL WITH SILT AND : gravel, ~35% F-C sand, ~10% NP vet.
	_	-							Planned Extent.	
	_	-							Backfilled with drill cuttings a	and cold patch asphalt.
	IOTES	5:						CITY/	JECT NAME: 21-23 River Rd Re STATE: Wilton, Connecticut ROJECT NUMBER: 2403682	development GEI Consultants



VB- 3 (8.0 to 13.0 FT) <u>Photographer:</u> T. Rezzani



			RMATION							BORING
				Location I				1010-		DONING
				(ft): 174						VB-4
								-		V D-4
			I (ft): <u>13</u> T. Rezza				DRILLER NAME: RIG TYPE: 7822DT	марр		
										PAGE 1 of 1
	DRILL	ING INF	ORMATIO	N						
			E: <u>N/A</u>				CASING I.D./O.D.: N			RREL TYPE: N/A
			-	inch / 6.5 i	nch		DRILL ROD O.D.: NI	И	CORE BA	RREL I.D./O.D. NA / NA
			THOD: G		.5 4/3/202	24				
	WAIL		LDEFING	(iii). <u>+</u> /	.5 4/5/202					
	ABBRI	EVIATIC	Rec RQI WO	. = Penetrati . = Recovery) = Rock Qu = Length of R = Weight c H = Weight c	Length ality Designa Sound Core of Rods	ıtion s>4 in / Pen.	S = Split Spoon Sample C = Core Sample U = Undisturbed Sample % SC = Sonic Core DP = Direct Push Sample HSA = Hollow-Stem Auger		Qp = Pocket Penetrometer Strength Sv = Pocket Torvane Shear Strength LL = Liquid Limit PI = Plasticity Index PID = Photoionization Detector I.D./O.D. = Inside Diameter/Outside I	Blows per 6 in.: 140-lb hammer falling 30 inches to drive a 2-inch-O.D. split spoon sampler.
			S	ample Inf	ormation			ne		
	Elev. (ft)	Depth (ft)	Sample No.	Depth (ft)	Pen./ Rec. (in)	Blows per 6 in. or RQD	Drilling Remarks/ Field Test Data	Layer Name	Soil and	Rock Description
	_	_								WIDELY GRADED SAND WITH M); ~50% F-C sand, ~40% F-C wn, dry.
GEI WOBURN STD 1-LOCATION-LAYER NAME WILTON CAMPUS SW BORINGS:GPJ GEI DATA TEMPLATE 2013:GDT 4/18/24	- 170 — - - - - - - - - - - - - - - - - - - -	5 5 10 10	S1	8 to 13	60/49		Filter sand introduced @ 4.0-5.0 ft. (offset hole) Infiltration test @ 5.0 ft. (offset hole)	SAND & GRAVEL		
	NOTES	3 :						CITY	ECT NAME: 21-23 River Rd R STATE: Wilton, Connecticut ROJECT NUMBER: 2403682	
ڻ ا								~		ULI Consult



VB- 4 (8.0 to 13.0 FT) <u>Photographer:</u> T. Rezzani



		RMATION							BORING
LOCA	TION: _	See Boring	Location F	Plan.					BURING
		FACE EL.				DATE START/END:			
		тим:					-		VB-5
		l (ft): 8.5					Knapp		
LOGO	ED BY:	T. Rezza	ni			RIG TYPE: 7822DT			PAGE 1 of 1
DRILI	ING INF	ORMATION	1						
		E: <u>N/A</u>				CASING I.D./O.D.: N			RREL TYPE: N/A
		D.: <u>3.25 i</u>		nch		DRILL ROD O.D.: N	М	CORE BAI	RREL I.D./O.D. NA / NA
		THOD: Ge		F 1/0/00					
WAI	RLEVE	LDEPTHS	(π): <u>¥</u> /	.5 4/3/202	24 GW leve	el interpreted			
ABBF	REVIATIO	RQD	= Recovery = Rock Qua	Length ality Designa Sound Core of Rods	ation ss>4 in / Pen.	S = Split Spoon Sample C = Core Sample U = Undisturbed Sample % SC = Sonic Core DP = Direct Push Sample HSA = Hollow-Stem Auger		NA, NM = Not Applicable, Not Measured Blows per 6 in.: 140-lb hammer falling 30 inches to drive a 2-inch-O.D. split spoon sampler. Diameter	
		Sa	ample Inf	ormation			ЭГ		
Elev. (ft)	Depth (ft)	Sample No.	Depth (ft)	Pen./ Rec. (in)	Blows per 6 in. or RQD	Drilling Remarks/ Field Test Data	Layer Name	Soil and	Rock Description
								DRILL CUTTINGS (0-5.0'):	SILTY SAND WITH GRAVEL (SM);
GEI WOBURN STD 1-LOCATION-LAYER NAME WILTON CAMPUS SW BORINGS.GPJ GEI DATA TEMPLATE 2013.GDT 4/18/24		S1	4 to 8.5	54/27		Filter sand introduced @ 4.0-5.0 ft. Infiltration test @ 5.0 ft.	SAND & GRAVEL	dry. S1 (5.0-8.5'): WIDELY GRA	
160 - 160 -	5:						PRO	JECT NAME: 21-23 River Rd Re	edevelopment
GEI WOBUI							СІТҮ	/STATE: Wilton, Connecticut PROJECT NUMBER: 2403682	GEI Consultants



VB- 5 (4.0 to 8.5 FT) <u>Photographer:</u> T. Rezzani Note Filter Sand at top of sample





WELL CALCULATIONS

<i>k'</i> –	$d^2 \left(\frac{\pi}{11} \frac{k'_v}{k_v} \frac{D}{m} + L\right)_{lm} H_1$	
κ _v –	$D^2(t_2 - t_1) = \frac{1}{H_2}$	

("Soil in casing in uniform soil," Lambe and Whitman, 1969.)

Diameter, sand pack	15.875	D (cm)	Depth of Test	4.2 FT
Diam., PVC	5.08	d (cm)	Depth to GW	7.5 ft (interpreted)
PVC Stick Up	91	L (cm)		
Test Length	35.6	L (cm)	Soil Descr.	WIDELY GRADED GRAVEL WITH SILT
k'v/kv	1	Assumed		AND SAND (GW-SM); ~55% F-C gravel, 35% F-C sand, ~10% NP fines, brown (FILL).

<u>Test 1</u>

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	**k _v (in/hr)
0.00	0		
67.06	15	#DIV/0!	#DIV/0!
82.30	30	5.61E-02	79.45
88.39	45	1.96E-02	27.72
94.49	60	1.83E-02	25.87
94.49	120	0.00E+00	0.00

Test 2

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	**k _v (in/hr)
0.00	0		
60.96	15	#DIV/0!	#DIV/0!
82.30	30	8.21E-02	116.42
85.34	45	9.95E-03	14.11
88.39	60	9.60E-03	13.61
91.44	120	2.32E-03	3.29
91.44	300	0.00E+00	0.00

****TEST INFLUENCED BY OBSTRUCTION**



WELL CALCULATIONS

$k'_{v} = \frac{d^{2}(\frac{\pi}{11}\frac{k'_{v}}{k_{v}}\frac{D}{m} + L)}{D^{2}(t_{2} - t_{1})}\ln\frac{H_{1}}{H_{2}}$		("Soil in casing ir	n uniform soil," Lambe an	d Whitman, 1969.)
Diameter, sand pack	15.875	D (cm)	Depth of Test	5.0 FT
Diam., PVC	5.08	d (cm)	Depth to GW	7.5 ft (interpreted)
PVC Stick Up	61	L (cm)		
Test Length	30.5	L (cm)	Soil Descr.	
k'v/kv	1	Assumed		SILTY SAND WITH GRAVEL (SM); ~45% F-C sand, ~35% F-C gravel, ~20% NP fines, brown.

Test 1

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	k₂ (in/hr)
0.00	0		
131.06	30	1.73E-02	24.50
137.16	45	1.09E-02	15.40
140.21	60	5.25E-03	7.45
143.26	75	5.14E-03	7.29
146.30	90	5.03E-03	7.13
146.61	105	4.97E-04	0.71
		AVERAGE	5.04
<u>Test 2</u>			

Height	Time	Vertical Perm.	Vertical Perm.	
H (cm)	t (seconds)	kv (cm/sec)	k₂ (in/hr)	
0.00	0			
131.06	30	8.61E-02	121.96	
146.30	45	2.63E-02	37.27	
152.40	60	9.76E-03	13.83	
		AVERAGE	25.55	**Preferential path; outlie



WELL CALCULATIONS

$k'_{\nu} = \frac{d^2(\frac{\pi}{11}\frac{k'_{\nu}}{k_{\nu}}\frac{D}{m} + L)}{D^2(t_2 - t_1)} \ln\frac{H_1}{H_2}$		("Soil in casing in	uniform soil," Lambe an	d Whitman, 19	969.)
Diameter, sand pack	15.875	D (cm)	Depth of Test	5.0	FT
Diam., PVC	5.08	d (cm)	Depth to GW	7.	.5 ft
PVC Stick Up	69	L (cm)			
Test Length	30.5	L (cm)	Soil Descr.	WIDELY GRA	DED GRAVEL WITH SILT
k'v/kv	1	Assumed		•	5W-GM); ~55% F-C gravel, d, ~10% NP fines, with st.

<u>Test 1</u>

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	kv (in/hr)
0.00	0		
82.30	30	1.84E-02	26.07
112.78	45	7.53E-02	106.74
115.82	60	6.37E-03	9.03
117.35	120	7.81E-04	1.11
118.87	180	7.71E-04	1.09
120.40	300	3.81E-04	0.54
121.92	360	7.52E-04	1.07
		AVERAGE	0.95

<u>Test 2</u>

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	kv (in/hr)
0.00	0		
85.34	30	1.77E-02	25.11
88.39	45	8.39E-03	11.89
88.39	60	0.00E+00	0.00
89.92	120	1.02E-03	1.45
91.44	180	1.00E-03	1.42
94.49	240	1.96E-03	2.78
96.01	300	9.56E-04	1.36
96.32	360	1.89E-04	0.27
		AVERAGE	1.45



WELL CALCULATIONS

$k'_{v} = \frac{d^{2}(\frac{\pi}{11}\frac{k'_{v}}{k_{v}}\frac{D}{m} + L)}{D^{2}(t_{2} - t_{1})}\ln\frac{H_{1}}{H_{2}}$		("Soil in casing in uniform soil," Lambe and Whitman, 1969.)			
Diameter, sand pack	15.875	D (cm)	Depth of Test	5.0	FT
Diam., PVC	5.08	d (cm)	Depth to GW	7.5 ft (in	terpreted)
PVC Stick Up	69	L (cm)			
Test Length	30.5	L (cm)	Soil Descr.	SILTY SAND V	VITH GRAVEL (SM); ~45% F-
k'v/kv	1	Assumed		C sand, ~30% brown.	F-C gravel, ~25% NP fines,

Test 1

Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	kv (in/hr)
0.00	0		
70.10	30	1.06E-02	15.06
73.15	120	1.70E-03	2.40
79.25	180	4.78E-03	6.78
83.82	240	3.35E-03	4.75
88.39	300	3.17E-03	4.50
91.44	360	2.03E-03	2.87
		AVERAGE	4.26

<u>Test 2</u>			
Height	Time	Vertical Perm.	Vertical Perm.
H (cm)	t (seconds)	kv (cm/sec)	k₂ (in/hr)
0.00	0		
68.58	30	5.37E-03	7.61
70.10	60	2.63E-03	3.72
73.15	120	2.54E-03	3.60
77.72	180	3.62E-03	5.13
79.25	240	1.16E-03	1.64
82.30	300	2.26E-03	3.20
85.34	360	2.17E-03	3.08
		AVERAGE	3.40

Appendix E

>Erosion and Sedimentation Control Measures

This page intentionally left blank.

Erosion and Sedimentation Control Measures

The following erosion and sedimentation controls are for use during the earthwork and construction phases of the project. The following controls are provided as recommendations for the site contractor.

Silt Fencing

Silt fence sill be installed on the down gradient side of the project as shown on the plans. In areas where high runoff velocities or high sediment loads are expected, straw barriers will be installed up-gradient of silt fencing. This semi-permeable barrier made of a synthetic porous fabric will provide additional protection. The silt fences and hay bale barrier will be replaced as determined by periodic field inspections.

Catch Basin Protection

Newly constructed and existing catch basins will be protected with silt sacks throughout construction.

Gravel and Construction Entrance/Exit

A temporary crushed-stone construction entrance/exit will be constructed. A cross slope will be placed in the entrance to direct runoff to a protected catch basin inlet or settling area.

Vegetative Slope Stabilization

Stabilization of open soil surfaces will be implemented within 14 days after grading or construction activities have temporarily or permanently ceased, unless there is sufficient snow cover to prohibit implementation. Vegetative slope stabilization will be used to minimize erosion on slopes of 3:1 or flatter. Annual grasses, such as annual rye, will be used to ensure rapid germination and production of root mass. Permanent stabilization will be completed with the planting of perennial grasses or legumes. Establishment of temporary and permanent vegetative cover may be established by hydro-seeding or sodding. A suitable topsoil, good seedbed preparation, and adequate lime, fertilizer and water will be provided for effective establishment of these vegetative stabilization methods. Mulch will also be used after permanent seeding to protect soil from the impact of falling rain and to increase the capacity of the soil to absorb water.

Maintenance

- The contractor or subcontractor will be responsible for implementing each control shown on the Sedimentation and Erosion Control Plan. In accordance with EPA regulations, the contractor must sign a copy of a certification to verify that a plan has been prepared and that permit regulations are understood.
- The on-site contractor will inspect all sediment and erosion control structures periodically and after each rainfall event. Records of the inspections will be prepared and maintained on-site by the contractor.
- > Silt shall be removed from behind barriers if greater than 6-inches deep or as needed.
- > Damaged or deteriorated items will be repaired immediately after identification.
- Sediment that is collected in structures shall be disposed of properly and covered if stored on-site.
- Erosion control structures shall remain in place until all disturbed earth has been securely stabilized. After removal of structures, disturbed areas shall be regraded and stabilized as necessary.

The sedimentation and erosion control plan is included in project plan set; a reduced version and Erosion Control Maintenance checklist is included here for quick reference.

load	Evaluation Checklist
Proposed Development- Wilton, CT – 21 River Road	Best Management Practices – Maintenance/ Evaluation Checklist
Proposed	Best Ma

Construction Practices

Best Management	Inspection	Date		Minimum Maintenance	Cleaning/Repair Needed	Date of	Performed
Practice	Frequency	Inspected	Inspector	and Key Items to Check	□yes □no (List Items)	Cleaning/Repair	by
Silt Fencing	Once per week						
	or after a $1''$ or						
	greater storm						
	event						
Catch Basin	Once per week						
Protection	or after a $1''$ or						
	greater storm						
	event						
Stabilized	Once per week						
Construction Exit	or after a $1''$ or						
	greater storm						
	event						
Temporary	Once per week						
Sediment Basin	or after a 1" or						
	greater storm						
	event						
Vegetated Slope	Once per week						
Stabilization	or after a 1" or						
	greater storm						
	event						

Stormwater Control Manager

Appendix F

>Long Term Stormwater and Operation and Maintenance Measures

This page intentionally left blank.

Long Term Stormwater and Operation and Maintenance Measures

Project Information

Site

Project Name:	Wilton Center Redevelopment
Address or Locus:	21-23 River Road
City, State & Zip:	Wilton, CT 06897

Wilton Campus 1691, LLC

Jericho, NY 11753

500 North Broadway, Suite 201

Developer

Client Name:	
Client Address:	

Client City, State & Zip:

Client Telephone No.:

Client Cell Phone:

Client E-Mail:

NBrown@kimcorealty.com

Site Supervisor

- Site Manager Name:
- Site Manager Address:
- Site Manager City, State & Zip:
- Site Manager Telephone No.:
- Site Manager Cell Phone:
- Site Manager E-Mail:

Long Term Stormwater Maintenance Measures –

The following maintenance program is proposed to ensure the continued effectiveness of the structural water quality controls previously described:

- Inspect stormwater basins once annually, in the spring, for cracking or erosion of side slopes, embankments, and accumulated sediment. Necessary sediment removal, earth repair, and/or reseeding will be performed immediately upon identification.
- Inspect sediment traps/forebays monthly for erosion of side slopes and accumulated sediment. Necessary sediment removal, earth repair and/or reseeding shall be performed immediately upon identification. Clean traps/ forebays approximately four times per year or as needed.
- Clean all catch basins once annually to remove accumulated sand, sediment, and floatable products or as needed based on use.
- > Paved areas will be swept, at a minimum, two (2) times per year.
- Routinely pick up and remove litter from the parking areas, islands and perimeter landscape areas in addition to regular pavement sweeping.
- Routinely inspect all dumpster and compactor locations for spills. Remove all trash litter from the enclosure and dispose of properly.

Pavement Systems

Standard Asphalt Pavement

- Sweep or vacuum standard asphalt pavement areas at least two times per year with a commercial cleaning unit and properly dispose of removed material.
- > Recommended sweeping schedule:
 - Oct/Nov
 - > Apr/May
- More frequent sweeping of paved surfaces will result in less accumulation in catch basins, less cleaning of subsurface structures, and less disposal costs.
- Check dumpster areas frequently for spillage and/or pavement staining and clean as necessary.

Structural Stormwater Management Devices

Catch Basins

- > All catch basins shall be inspected and cleaned a minimum of at least once per year.
- Sediment (if more than six inches deep) and/or floatable pollutants shall be pumped from the basin and disposed of at an approved offsite facility in accordance with all applicable regulations.

- Any structural damage or other indication of malfunction will be reported to the site manager and repaired as necessary
- > During colder periods, the catch basin grates must be kept free of snow and ice.
- During warmer periods, the catch basin grates must be kept free of leaves, litter, sand, and debris.

Subsurface Detention & Retention Systems

- The subsurface detention and retention systems will be inspected at least once each year by removing the manhole/access port covers and determining the thickness of sediment that has accumulated in the sediment removal row.
- If sediment is more than six inches deep, it must be suspended via flushing with clean water and removed using a vactor truck.
- Manufacturer's specifications and instructions for cleaning the sediment removal row should be consulted.
- Emergency overflow pipes will be examined at least once each year and verified that no blockage has occurred.
- > System will be observed after rainfalls to see if it is properly draining.

Structural Water Quality Devices

- FOLLOW MANUFACTURER'S INSTRUCTIONS ON O&M REQUIREMENTS AND METHODOLOGY
- > Inspect devices monthly for the first three months after construction.
- After initial three month period, all water quality units are to be inspected at least four times per year and cleaned a minimum of at least once per year or when sediment reaches 8" in depth.
- Follow manufacturer instructions for inspection and cleaning and contact manufacturer if system is malfunctioning.

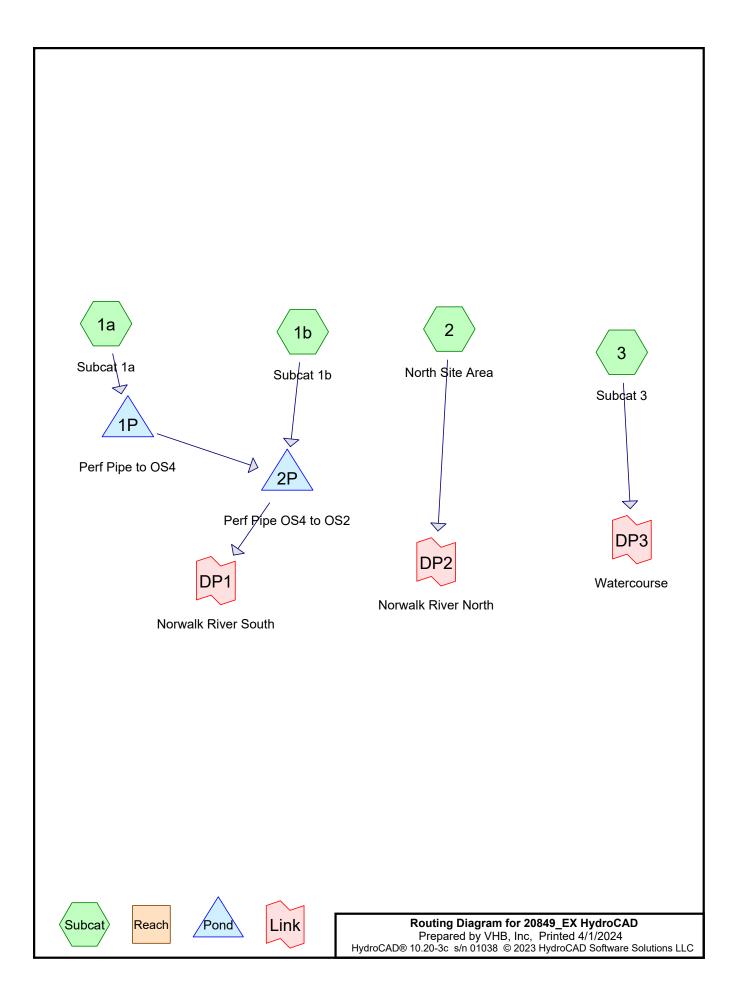
Roof Drain Leaders

- > Perform routine roof inspections quarterly.
- ► Keep roofs clean and free of debris.
- > Keep roof drainage systems clear.
- > Keep roof access limited to authorized personnel.
- > Clean inlets draining to the subsurface bed twice per year as necessary.

Appendix G

>HydroCAD: Existing Conditions >HydroCAD: Proposed Conditions This page intentionally left blank.

HydroCAD: Existing Conditions



20849_EX HydroCAD Prepared by VHB, Inc HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC

Printed 4/1/2024 Page 2

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	CT-WILTON 24-hr S1	2-yr	Default	24.00	1	3.55	2
2	10-yr	CT-WILTON 24-hr S1	10-yr	Default	24.00	1	5.42	2
3	25-yr	CT-WILTON 24-hr S1	25-yr	Default	24.00	1	6.59	2
4	100-yr	CT-WILTON 24-hr S1	100-yr	Default	24.00	1	8.39	2

Rainfall Events Listing

20849_EX HydroCAD	
Prepared by VHB, Inc	Printed 4/1/2024
HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC	Page 3

Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.497	89	<50% Grass cover, Poor, HSG D (1a, 1b, 2, 3)
1.400	80	>75% Grass cover, Good, HSG D (1a, 1b, 2, 3)
7.286	98	Unconnected pavement, HSG D (1a, 1b, 2, 3)
2.930	77	Woods, Good, HSG D (3)
0.268	79	Woods/grass comb., Good, HSG D (1a, 1b, 3)
12.380	90	TOTAL AREA

20849_EX HydroCAD

Prepared by VHB, Inc HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Printed 4/1/2024 Page 4

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
12.380	HSG D	1a, 1b, 2, 3
0.000	Other	
12.380		TOTAL AREA

20849_EX HydroCAD

Prepared by VHB, Inc	Printed 4/1/2024
HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC	Page 5

Ground Covers (all nodes)										
 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers			
 0.000	0.000	0.000	0.497	0.000	0.497	<50% Grass cover, Poor	1a, 1b, 2, 3			
0.000	0.000	0.000	1.400	0.000	1.400	>75% Grass cover, Good	1a, 1b, 2, 3			
0.000	0.000	0.000	7.286	0.000	7.286	Unconnected pavement	1a, 1b, 2, 3			
0.000	0.000	0.000	2.930	0.000	2.930	Woods, Good	3			
0.000	0.000	0.000	0.268	0.000	0.268	Woods/grass comb., Good	1a, 1b, 3			
0.000	0.000	0.000	12.380	0.000	12.380	TOTAL AREA				

20849_EX HydroCAD	
Prepared by VHB, Inc	Printed 4/1/2024
HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC	Page 6
	_

Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill	Node
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	Name
 1	2P	170.20	169.10	25.0	0.0440	0.013	0.0	36.0	0.0	

Time span=0.00-30.00 hrs, dt=0.02 hrs, 1501 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1a: Subcat1a	Runoff Area=2.817 ac 74.88% Impervious Runoff Depth=2.88" Tc=5.0 min CN=94 Runoff=10.84 cfs 0.677 af
Subcatchment1b: Subcat1b	Runoff Area=2.892 ac 71.97% Impervious Runoff Depth=2.78" Tc=5.0 min CN=93 Runoff=10.85 cfs 0.671 af
Subcatchment2: North Site Area	Runoff Area=3.564 ac 86.82% Impervious Runoff Depth=3.09" Tc=5.0 min CN=96 Runoff=14.31 cfs 0.919 af
Subcatchment3: Subcat3	Runoff Area=3.108 ac 0.04% Impervious Runoff Depth=1.47" Flow Length=865' Tc=10.9 min CN=77 Runoff=4.58 cfs 0.380 af
Pond 1P: Perf Pipe to OS4 Discarded=0.04 cfs	Peak Elev=173.09' Storage=5,663 cf Inflow=10.84 cfs 0.677 af 0.076 af Primary=10.82 cfs 0.495 af Outflow=10.86 cfs 0.571 af
Pond 2P: Perf Pipe OS4 to OS2 Discarded=0.01 cfs	Peak Elev=172.07' Storage=2,312 cf Inflow=21.67 cfs 1.166 af 0.031 af Primary=21.65 cfs 1.089 af Outflow=21.66 cfs 1.120 af
Link DP1: Norwalk River South	Inflow=21.65 cfs 1.089 af Primary=21.65 cfs 1.089 af
Link DP2: Norwalk River North	Inflow=14.31 cfs 0.919 af Primary=14.31 cfs 0.919 af
Link DP3: Watercourse	Inflow=4.58 cfs 0.380 af Primary=4.58 cfs 0.380 af

Total Runoff Area = 12.380 ac Runoff Volume = 2.647 af Average Runoff Depth = 2.57" 41.15% Pervious = 5.094 ac 58.85% Impervious = 7.286 ac

Summary for Subcatchment 1a: Subcat 1a

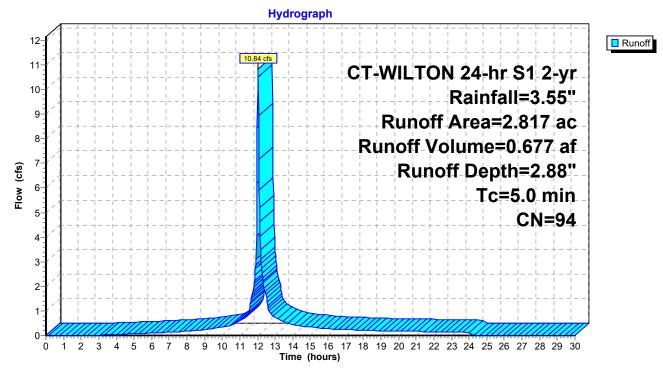
Runoff = 10.84 cfs @ 12.02 hrs, Volume= Routed to Pond 1P : Perf Pipe to OS4

0.677 af, Depth= 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area	(ac)	CN	Desc	cription		
0.	121	89	<50%	6 Grass co	over, Poor,	, HSG D
0.	375	80	>75%	6 Grass co	over, Good	d, HSG D
2.	109	98	Unco	onnected p	oavement, l	HSG D
0.	212	79	Woo	ds/grass c	omb., Goo	od, HSG D
2.	817	94	Weig	hted Aver	age	
0.	708		25.1	2% Pervio	us Area	
2.	109		74.8	8% Imperv	ious Area	
2.	109		100.0	00% Unco	nnected	
Tc	Leng	th	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
5.0						Direct Entry,
						-

Subcatchment 1a: Subcat 1a



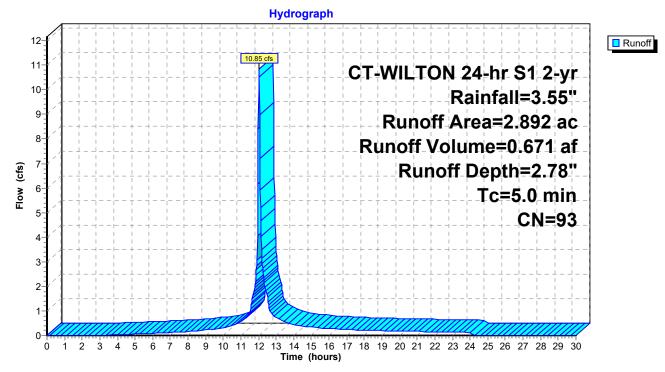
Summary for Subcatchment 1b: Subcat 1b

Runoff = 10.85 cfs @ 12.02 hrs, Volume= 0.671 af, Depth= 2.78" Routed to Pond 2P : Perf Pipe OS4 to OS2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (a	c) C	N D	escription		
0.05	56 8	39 <5	50% Grass co	over, Poor,	r, HSG D
0.72	23 8	30 >7	75% Grass co	over, Good	d, HSG D
2.08	31 9	98 Ui	nconnected p	avement, l	HSG D
0.03	31 7	79 W	oods/grass c	omb., Goo	od, HSG D
2.89	92 9	93 W	eighted Aver	age	
0.81	11	28	3.03% Pervio	us Area	
2.08	31	71	1.97% Imperv	vious Area	1
2.08	31	10	0.00% Unco	nnected	
Tc L (min)	ength (feet)	Slop (ft/f		Capacity (cfs)	
5.0					Direct Entry,

Subcatchment 1b: Subcat 1b



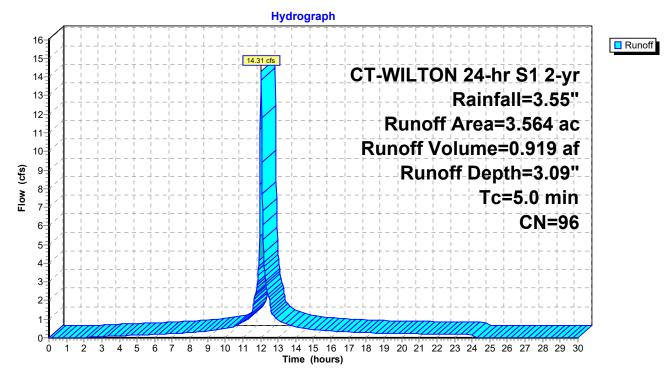
Summary for Subcatchment 2: North Site Area

Runoff = 14.31 cfs @ 12.02 hrs, Volume= 0.919 af, Depth= 3.09" Routed to Link DP2 : Norwalk River North

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area	(ac)	CN	Desc	Description				
0.	281	89	<50%	6 Grass co	over, Poor,	HSG D		
0.	189	80	>75%	6 Grass co	over, Good	I, HSG D		
3.	094	98	Unco	onnected p	avement, I	HSG D		
3.	564	96	Weig	hted Aver	age			
0.	470		13.1	8% Pervio	us Area			
3.	094			86.82% Impervious Area				
3.	094		100.0	00% Unco	nnected			
_								
Tc	Leng		Slope	Velocity	Capacity	Description		
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)			
5.0						Direct Entry,		

Subcatchment 2: North Site Area



Summary for Subcatchment 3: Subcat 3

Runoff = 4.58 cfs @ 12.10 hrs, Volume= 0 Routed to Link DP3 : Watercourse

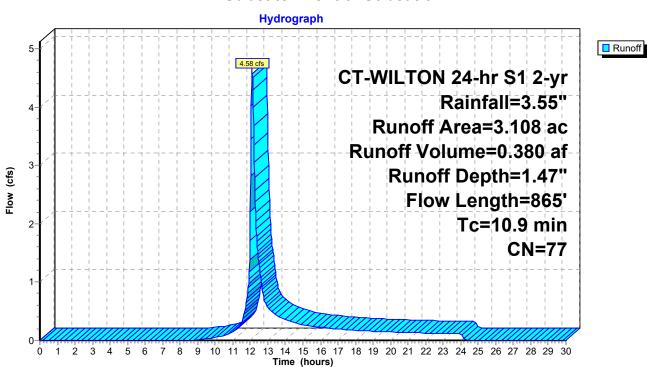
0.380 af, Depth= 1.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area	(ac) C	N Des	scription					
0.	040	89 <50	50% Grass cover, Poor, HSG D					
0.	112	80 >75	% Grass c	over, Good	, HSG D			
0.	001	98 Uno	connected p	pavement, l	HSG D			
2.	930		ods, Good,					
0.	025	79 Wo	ods/grass o	comb., Goo	d, HSG D			
3.	108		ighted Avei	•				
-	107		96% Pervio					
	001		4% Impervi					
0.	001	100	.00% Uncc	onnected				
Та	Longth	Slope	Volocity	Capacity	Description			
Tc (min)	Length	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
(min)	(feet)			(015)				
7.7	50	0.2300	0.11		Sheet Flow, Wooday Danaa undarbruch n= 0,800 D2= 3 EE"			
1.3	215	0.3255	2.85		Woods: Dense underbrush n= 0.800 P2= 3.55"			
1.5	215	0.3200	2.00		Shallow Concentrated Flow,			
1.9	600	0.0117	5.16	82.54	Woodland Kv= 5.0 fps Channel Flow,			
1.9	000	0.0117	5.10	02.04	Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040			
10.9	865	Total						
10.9	605	TUIAI						

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 2-yr Rainfall=3.55" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 12



Subcatchment 3: Subcat 3

Summary for Pond 1P: Perf Pipe to OS4

Inflow Area = 2.817 ac, 74.88% Impervious, Inflow Depth = 2.88" for 2-yr event 10.84 cfs @ 12.02 hrs, Volume= Inflow = 0.677 af Outflow = 10.86 cfs @ 12.02 hrs, Volume= 0.571 af, Atten= 0%, Lag= 0.0 min Discarded = 0.04 cfs @ 12.02 hrs, Volume= 0.076 af Primary = 10.82 cfs @ 12.02 hrs, Volume= 0.495 af Routed to Pond 2P : Perf Pipe OS4 to OS2

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 173.09' @ 12.02 hrs Surf.Area= 3,067 sf Storage= 5,663 cf

Plug-Flow detention time= 150.5 min calculated for 0.570 af (84% of inflow) Center-of-Mass det. time= 74.1 min (865.4 - 791.3)

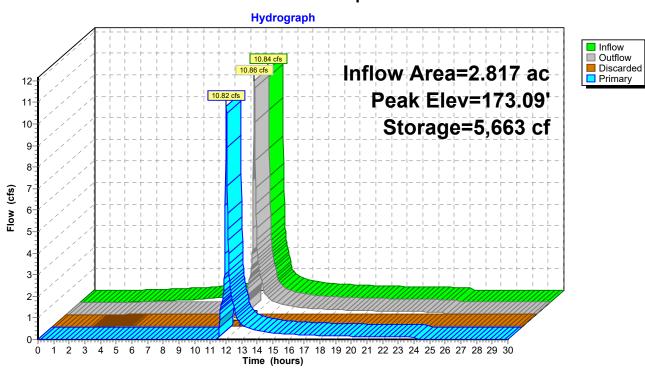
Volume	Invert	Avail	.Storage	Storage Descriptio	n	
#1	169.41'		2,743 cf			2
				L= 388.0' S= 0.00		
#2	168.91'		1,622 cf	72.0" W x 42.0" H		
				L= 388.0' S= 0.00		
				-	-	I = 5,405 cf x 30.0% Voids
#3	169.61'		813 cf	36.0" Round Pipe		4
				L= 115.0' S= 0.00		
#4	169.11'		481 cf	72.0" W x 42.0" H		
				L= 115.0' S= 0.00		
				-		= 1,602 cf_x 30.0% Voids
#5	172.40'		5,249 cf	Custom Stage Da	ta (Irregular)Listed	d below (Recalc)
		1	0,906 cf	Total Available Sto	rage	
					•	
Elevatior	n Su	rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area
(feet)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)
172.40)	1	1.0	0	0	1
173.00		10	15.0	3	3	19
174.00		2,050	300.0	734	737	7,165
175.00		7,550	570.0	4,511	5,249	25,863
	-	,		, -	-, -	- ,
Device	Routing	Inv	ert Outle	et Devices		
#1	Primary	172.	41' 72.0	" W x 32.0" H Vert	Weir Plate C= 0.	600
	5			ted to weir flow at lo	w heads	
#2	Discarded	168.	91' 0.50	0 in/hr Exfiltration	over Surface area	a Phase-In= 0.01'
		_				
Discardo	d OutElow	May-0.0		$2.02 \text{ bro } \square M = 172.0$	0' (Eroo Dischar	(or

Discarded OutFlow Max=0.04 cfs @ 12.02 hrs HW=173.09' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=10.72 cfs @ 12.02 hrs HW=173.09' (Free Discharge) -1=Weir Plate (Orifice Controls 10.72 cfs @ 2.64 fps)

20849_EX HydroCAD

Prepared by VHB, Inc



Pond 1P: Perf Pipe to OS4

Summary for Pond 2P: Perf Pipe OS4 to OS2

Page 15

Inflow Area =	5.709 ac, 7	3.41% Impervious, Ir	nflow Depth = 2.45" for 2-yr event
Inflow =	21.67 cfs @	12.02 hrs, Volume=	1.166 af
Outflow =	21.66 cfs @	12.02 hrs, Volume=	1.120 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.01 cfs @	12.02 hrs, Volume=	0.031 af
Primary =	21.65 cfs @	12.02 hrs, Volume=	1.089 af
Routed to Link	KDP1 : Norwa	lk River South	

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 172.07' @ 12.02 hrs Surf.Area= 1,236 sf Storage= 2,312 cf

Plug-Flow detention time= 44.5 min calculated for 1.119 af (96% of inflow) Center-of-Mass det. time= 22.0 min (839.0 - 817.0)

Volume	Invert	Avail.	Storage	Storage Description					
#1	167.20'		1,449 cf		36.0" Round Pipe Storage Inside #2				
				L= 205.0' S= 0.00					
#2	166.70'		857 cf	72.0" W x 42.0" H					
				L= 205.0' S= 0.00					
						$d = 2,856 \text{ cf } \times 30.0\% \text{ Voids}$			
#3	170.20'		5,259 cf	Custom Stage Da	ata (Irregular)Liste	d below (Recalc)			
			7,565 cf	Total Available Sto	orage				
Elevatio	on Su	ırf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(fee		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)			
170.2	20	1	1.0	0	0	1			
173.0	00	10	15.0	13	13	30			
174.0	00	2,050	300.0	734	748	7,175			
175.0	00	7,550	570.0	4,511	5,259	25,873			
Device	Routing	Inv	ert Outl	et Devices					
#1	Discarded	166.	70' 0.50	0 in/hr Exfiltration	over Surface are	a Phase-In= 0.01'			
#2	Primary	170.3	20' 36.0	" Round Culvert					
	-		L= 2	5.0' CPP, end-sec	tion conforming to	fill, Ke= 0.500			
			Inlet	/ Outlet Invert= 170).20'/169.10' S=	0.0440 '/' Cc= 0.900			
			n= 0	.013 Corrugated P	E, smooth interior,	Flow Area= 7.07 sf			
	ed OutFlow		-	2.02 hrs HW=172.0	06' (Free Dischar	ge)			

1=Exfiltration (Exfiltration Controls 0.01 cfs)

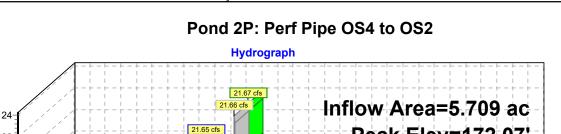
Primary OutFlow Max=21.46 cfs @ 12.02 hrs HW=172.06' (Free Discharge) ←2=Culvert (Inlet Controls 21.46 cfs @ 4.65 fps)

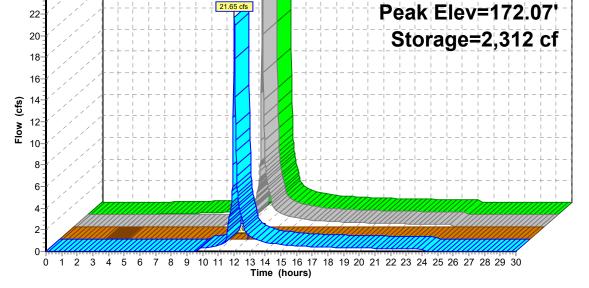
20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 2-yr Rainfall=3.55" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 16

Inflow
Outflow

Discarded Primary

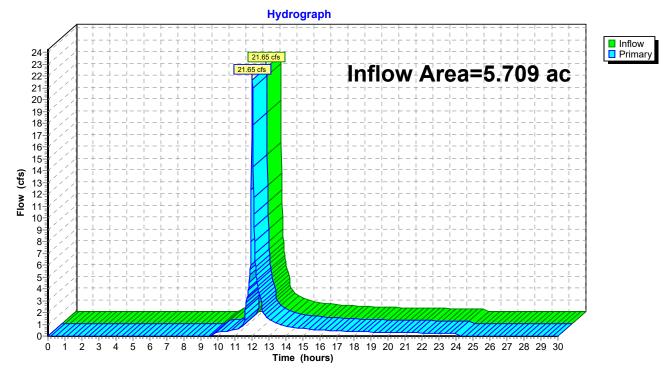




Summary for Link DP1: Norwalk River South

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 2.29" for 2-yr event Inflow = 21.65 cfs @ 12.02 hrs, Volume= 1.089 af Primary = 21.65 cfs @ 12.02 hrs, Volume= 1.089 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

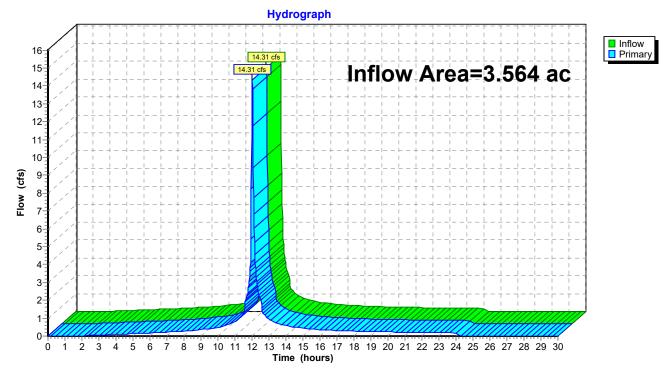


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Area = 3.564 ac, 86.82% Impervious, Inflow Depth = 3.09" for 2-yr event Inflow = 14.31 cfs @ 12.02 hrs, Volume= 0.919 af Primary = 14.31 cfs @ 12.02 hrs, Volume= 0.919 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

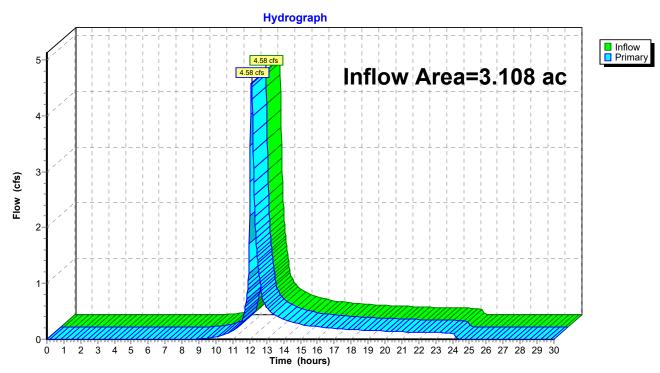


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse

Inflow Area	a =	3.108 ac,	0.04% Impervious,	Inflow Depth = 1.4	47" for 2-yr event
Inflow	=	4.58 cfs @	12.10 hrs, Volume	e= 0.380 af	
Primary	=	4.58 cfs @	12.10 hrs, Volume	e= 0.380 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse

Runoff by SCS	EXISTING CONDITIONS CT-WILTON 24-hr S1 10-yr Rainfall=5.42" Printed 4/1/2024 Printed 4/1/2024 Page 20 00-30.00 hrs, dt=0.02 hrs, 1501 points TR-20 method, UH=SCS, Weighted-CN +Trans method - Pond routing by Stor-Ind method
Subcatchment1a: Subcat1a	Runoff Area=2.817 ac 74.88% Impervious Runoff Depth=4.72" Tc=5.0 min CN=94 Runoff=16.11 cfs 1.109 af
Subcatchment1b: Subcat1b	Runoff Area=2.892 ac 71.97% Impervious Runoff Depth=4.61" Tc=5.0 min CN=93 Runoff=16.32 cfs 1.111 af
Subcatchment2: North Site Area	Runoff Area=3.564 ac 86.82% Impervious Runoff Depth=4.95" Tc=5.0 min CN=96 Runoff=20.84 cfs 1.470 af
Subcatchment3: Subcat3	Runoff Area=3.108 ac 0.04% Impervious Runoff Depth=2.98" Flow Length=865' Tc=10.9 min CN=77 Runoff=8.92 cfs 0.771 af
Pond 1P: Perf Pipe to OS4 Discarded=0.04 cf	Peak Elev=173.29' Storage=5,690 cf Inflow=16.11 cfs 1.109 af fs 0.080 af Primary=15.96 cfs 0.921 af Outflow=16.00 cfs 1.001 af
Pond 2P: Perf Pipe OS4 to OS2 Discarded=0.01 cf	Peak Elev=172.61' Storage=2,316 cf Inflow=32.28 cfs 2.032 af fs 0.033 af Primary=32.25 cfs 1.954 af Outflow=32.26 cfs 1.986 af
Link DP1: Norwalk River South	Inflow=32.25 cfs 1.954 af

Link DP2: Norwalk River North

Link DP3: Watercourse

Inflow=20.84 cfs 1.470 af Primary=20.84 cfs 1.470 af

Primary=32.25 cfs 1.954 af

Inflow=8.92 cfs 0.771 af Primary=8.92 cfs 0.771 af

Total Runoff Area = 12.380 acRunoff Volume = 4.461 afAverage Runoff Depth = 4.32"41.15% Pervious = 5.094 ac58.85% Impervious = 7.286 ac

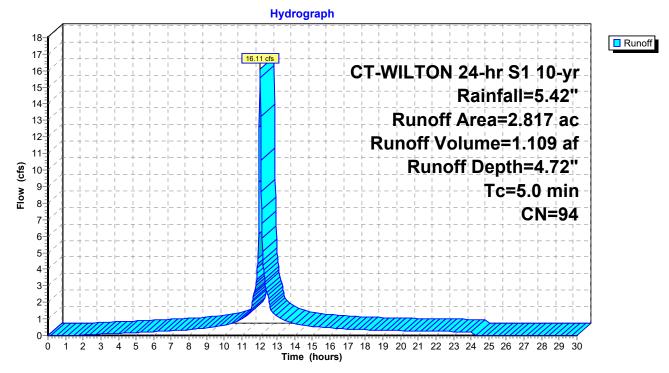
Summary for Subcatchment 1a: Subcat 1a

Runoff = 16.11 cfs @ 12.02 hrs, Volume= Routed to Pond 1P : Perf Pipe to OS4 1.109 af, Depth= 4.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac)	CN	Desc	cription		
0.	121	89	<50%	6 Grass co	over, Poor,	r, HSG D
0.	375	80			over, Good	
2.	109	98	Unco	onnected p	avement, I	HSG D
0.	212	79	Woo	ds/grass c	omb., Goo	od, HSG D
2.	817	94	Weig	hted Aver	age	
0.	708		25.1	2% Pervio	us Area	
2.	109		74.8	8% Imperv	vious Area	l de la constante de
2.	109		100.	00% Unco	nnected	
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•
5.0			(1010)	(10300)	(003)	Direct Entry,
0.0						,,,

Subcatchment 1a: Subcat 1a



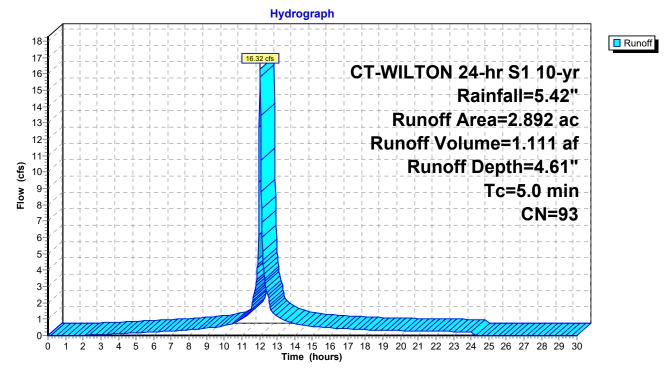
Summary for Subcatchment 1b: Subcat 1b

Runoff = 16.32 cfs @ 12.02 hrs, Volume= Routed to Pond 2P : Perf Pipe OS4 to OS2 1.111 af, Depth= 4.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac)	CN	Desc	cription		
0.	056	89	<50%	% Grass co	over, Poor,	, HSG D
0.	723	80	>75%	% Grass co	over, Good	d, HSG D
2.	081	98	Unco	onnected p	avement, I	HSG D
0.	031	79	Woo	ds/grass c	omb., Goo	od, HSG D
2.	892	93	Weig	phted Aver	age	
0.	811		28.0	3% Pervio	us Area	
2.	081		71.9	7% Imperv	ious Area	
2.	081		100.	00% Unco	nnected	
-					O	
Tc	Leng		Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
5.0						Direct Entry,

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 2: North Site Area

20.84 cfs @ 12.02 hrs, Volume= Runoff = Routed to Link DP2 : Norwalk River North

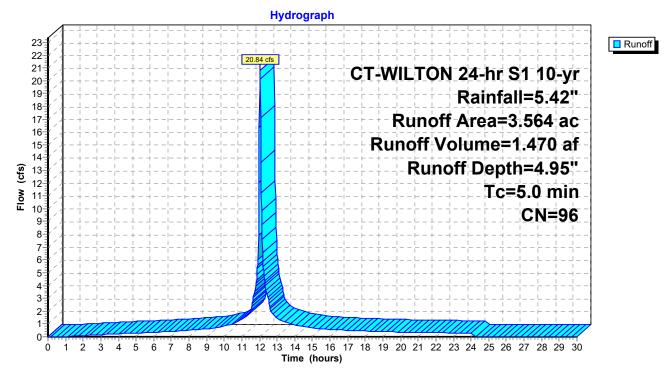
1.470 af, Depth= 4.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	a (ac)	CN	Desc	cription							
(0.281	89	<50%	<50% Grass cover, Poor, HSG D							
(0.189	80	>75%	% Grass c	over, Good	d, HSG D					
	3.094	98	Unco	onnected p	pavement, l	HSG D					
	3.564	96	Weig	ghted Aver	age						
(0.470 13.18% Pervious Area										
	3.094		86.8	2% Imperv	/ious Area						
	3.094		100.	00% Unco	nnected						
Tc			Slope	Velocity	Capacity	Description					
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
5.0						Direct Entry,					

Direct Entry,

Subcatchment 2: North Site Area



Summary for Subcatchment 3: Subcat 3

Runoff 8.92 cfs @ 12.10 hrs, Volume= = Routed to Link DP3 : Watercourse

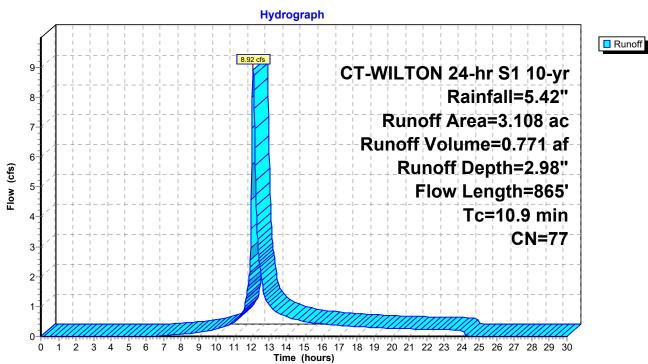
0.771 af, Depth= 2.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac) (CN De	scription							
0.	040	89 <50	50% Grass cover, Poor, HSG D							
0.	112	80 >7	5% Grass c	over, Good	, HSG D					
0.	001	98 Un	ر connected	pavement, l	HSG D					
2.	930		ods, Good,							
0.	025	79 Wo	ods/grass o	comb., Goo	d, HSG D					
3.	108	77 We	ighted Ave	rage						
-	107		96% Pervic							
	001		4% Impervi							
0.	.001	100	0.00% Unco	onnected						
Та	Longth	Clana	Valacity	Canaaitu	Description					
Tc (min)	Length	Slope (ft/ft)		Capacity (cfs)	Description					
(min)	(feet)			(05)						
7.7	50	0.2300	0.11		Sheet Flow,					
1.0	045	0 2255			Woods: Dense underbrush n= 0.800 P2= 3.55"					
1.3	215	0.3255	5 2.85		Shallow Concentrated Flow,					
1.9	600	0.0117	5.16	90 E1	Woodland Kv= 5.0 fps					
1.9	000	0.0117	5.10	82.54	Channel Flow, Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040					
10.0	005	Tatal			AICa- 10.0 SI FCIIII- 11.0 I- 1.43 II- 0.040					
10.9	865	Total								

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 10-yr Rainfall=5.42" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 25



Subcatchment 3: Subcat 3

Prepared by VHB, Inc

Summary for Pond 1P: Perf Pipe to OS4

Inflow Area = 2.817 ac, 74.88% Impervious, Inflow Depth = 4.72" for 10-yr event 16.11 cfs @ 12.02 hrs, Volume= Inflow = 1.109 af Outflow = 16.00 cfs @ 12.03 hrs, Volume= 1.001 af, Atten= 1%, Lag= 0.1 min Discarded = 0.04 cfs @ 12.03 hrs, Volume= 0.080 af Primary = 15.96 cfs @ 12.03 hrs, Volume= 0.921 af Routed to Pond 2P : Perf Pipe OS4 to OS2

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 173.29' @ 12.03 hrs Surf.Area= 3,258 sf Storage= 5,690 cf

Plug-Flow detention time= 114.2 min calculated for 1.001 af (90% of inflow) Center-of-Mass det. time= 59.5 min (836.7 - 777.2)

Volume	Invert	Avail	.Storage	Storage Descriptio	n				
#1	169.41'		2,743 cf	36.0" Round Pipe Storage Inside #2					
#2	168.91'		1,622 cf	L= 388.0' S= 0.0010 '/' 72.0" W x 42.0" H Box Stone					
				L= 388.0' S= 0.00	L= 388.0' S= 0.0010 '/'				
#3	169.61'		813 cf	8,148 cf Overall - 2 36.0" Round Pipe	-	l = 5,405 cf x 30.0% Voids 4			
				L= 115.0' S= 0.00					
#4	169.11'		481 cf	72.0" W x 42.0" H					
				L= 115.0' S= 0.00					
				-		= 1,602 cf_x 30.0% Voids			
#5	172.40'		5,249 cf	Custom Stage Da	ta (Irregular)Listed	d below (Recalc)			
		1	0,906 cf	Total Available Sto	rage				
Elevation	su Su	rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(feet)	1	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)			
172.40		1	1.0	0	0	1			
173.00)	10	15.0	3	3	19			
174.00)	2,050	300.0	734	737	7,165			
175.00)	7,550	570.0	4,511	5,249	25,863			
Device I	Routing	Inv	vert Outle	et Devices					
	Primary	172.		0" W x 32.0" H Vert. Weir Plate C= 0.600					
	•		Limit	ted to weir flow at lo	w heads				
#2 I	Discarded	ed 168.91' 0.500 in/hr Exfiltration over Surface area Phase-In= 0.01'							
Discardo	Discarded OutElow Max=0.04 afe @ 12.03 bro. HW=173.20' (Erea Discharge)								

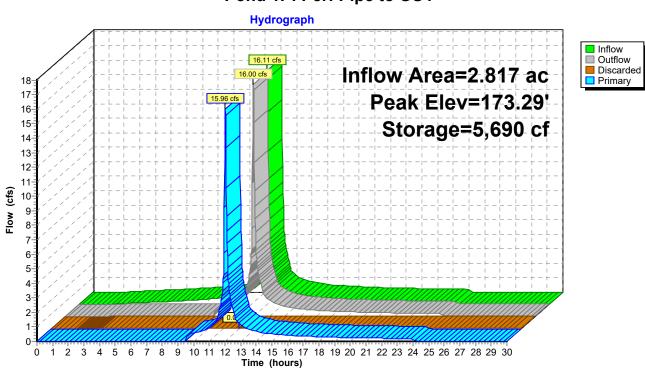
Discarded OutFlow Max=0.04 cfs @ 12.03 hrs HW=173.29' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=15.81 cfs @ 12.03 hrs HW=173.29' (Free Discharge) -1=Weir Plate (Orifice Controls 15.81 cfs @ 3.01 fps)

20849_EX HydroCAD

Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 10-yr Rainfall=5.42" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 27



Pond 1P: Perf Pipe to OS4

Summary for Pond 2P: Perf Pipe OS4 to OS2

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 4.27" for 10-yr event 32.28 cfs @ 12.02 hrs, Volume= Inflow = 2.032 af Outflow = 32.26 cfs @ 12.02 hrs, Volume= 1.986 af, Atten= 0%, Lag= 0.0 min Discarded = 0.01 cfs @ 12.02 hrs, Volume= 0.033 af Primary = 32.25 cfs @ 12.02 hrs, Volume= 1.954 af Routed to Link DP1 : Norwalk River South

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 172.61' @ 12.02 hrs Surf.Area= 1,238 sf Storage= 2,316 cf

Plug-Flow detention time= 29.8 min calculated for 1.986 af (98% of inflow) Center-of-Mass det. time= 15.8 min (817.9 - 802.1)

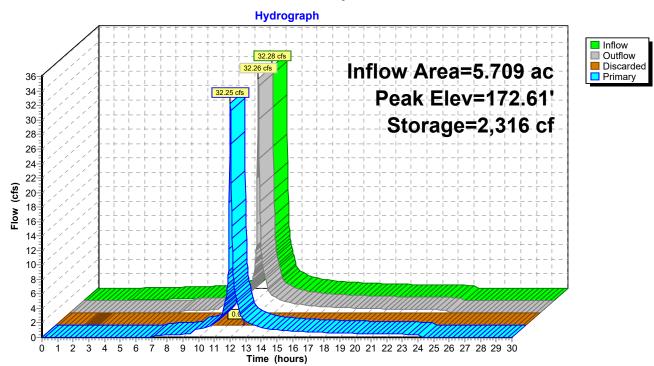
Volume	Invert	Avail.	Storage	Storage Description	on				
#1	167.20'		1,449 cf		36.0" Round Pipe Storage Inside #2				
					L= 205.0' S= 0.0010 '/'				
#2	166.70'		857 cf	72.0" W x 42.0" H					
				L= 205.0' S= 0.00					
				-	-	d = 2,856 cf x 30.0% Voids			
#3	170.20'	Ę	5,259 cf	Custom Stage Da	ata (Irregular)Liste	d below (Recalc)			
		-	7,565 cf	Total Available Sto	orage				
Elevatio		rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(fee		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)			
	1		()			(39-11)			
170.2		1	1.0	0	0	1			
173.0		10	15.0	13	13	30			
174.0	00	2,050	300.0	734	748	7,175			
175.0	00	7,550	570.0	4,511	5,259	25,873			
Device	Routing	Inve	ert Outl	et Devices					
#1	Discarded	166.7	70' 0.50	0 in/hr Exfiltration	over Surface are	a Phase-In= 0.01'			
#2	Primary	170.2	20' 36.0	" Round Culvert					
	,			5.0' CPP, end-sec	tion conforming to	fill Ke= 0 500			
						0.0440 '/' Cc= 0.900			
						Flow Area= 7.07 sf			
			11-0	.010 Confugated P					
	Discarded OutFlow Max=0.01 cfs @ 12.02 hrs HW=172.60' (Free Discharge)								

1=Exfiltration (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=31.96 cfs @ 12.02 hrs HW=172.60' (Free Discharge) ←2=Culvert (Inlet Controls 31.96 cfs @ 5.27 fps)

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 10-yr Rainfall=5.42" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 29

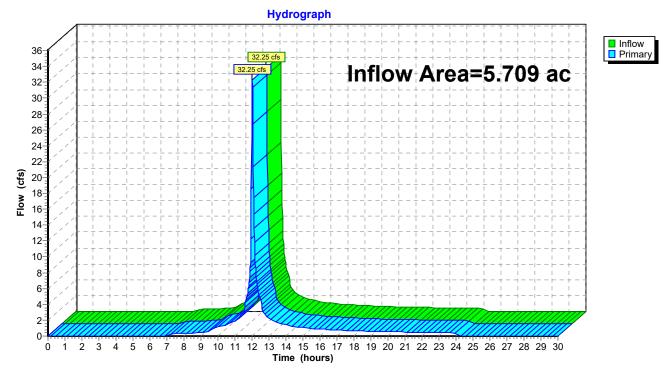


Pond 2P: Perf Pipe OS4 to OS2

Summary for Link DP1: Norwalk River South

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 4.11" for 10-yr event Inflow = 32.25 cfs @ 12.02 hrs, Volume= 1.954 af Primary = 32.25 cfs @ 12.02 hrs, Volume= 1.954 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

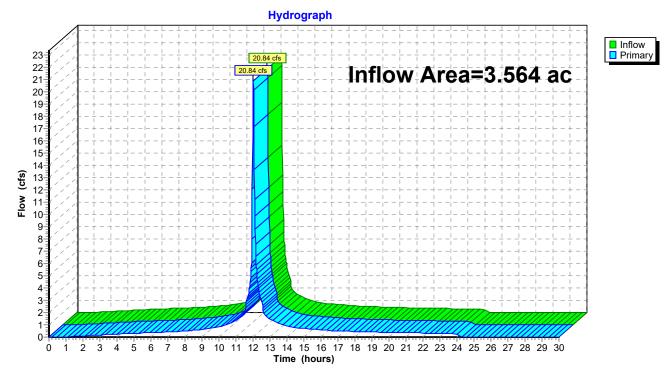


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Area = 3.564 ac, 86.82% Impervious, Inflow Depth = 4.95" for 10-yr event Inflow = 20.84 cfs @ 12.02 hrs, Volume= 1.470 af Primary = 20.84 cfs @ 12.02 hrs, Volume= 1.470 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

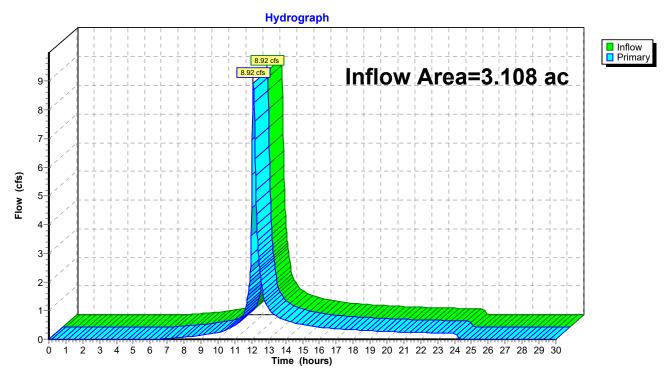




Summary for Link DP3: Watercourse

Inflow Are	a =	3.108 ac,	0.04% Impervious,	Inflow Depth =	2.98" for 10-yr event
Inflow	=	8.92 cfs @	12.10 hrs, Volume	e= 0.771 a	af
Primary	=	8.92 cfs @	12.10 hrs, Volume	e= 0.771 a	af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse

	00-30.00 hrs, dt=0.02 hrs, 1501 points
	TR-20 method, UH=SCS, Weighted-CN Trans method - Pond routing by Stor-Ind method
Subcatchment1a: Subcat1a	Runoff Area=2.817 ac 74.88% Impervious Runoff Depth=5.88" Tc=5.0 min CN=94 Runoff=19.33 cfs 1.381 af
Subcatchment1b: Subcat1b	Runoff Area=2.892 ac 71.97% Impervious Runoff Depth=5.77" Tc=5.0 min CN=93 Runoff=19.65 cfs 1.389 af
Subcatchment2: North Site Area	Runoff Area=3.564 ac 86.82% Impervious Runoff Depth=6.12" Tc=5.0 min CN=96 Runoff=24.85 cfs 1.816 af
Subcatchment3: Subcat3	Runoff Area=3.108 ac 0.04% Impervious Runoff Depth=4.00" Flow Length=865' Tc=10.9 min CN=77 Runoff=11.69 cfs 1.036 af
Pond 1P: Perf Pipe to OS4 Discarded=0.04 cfs	Peak Elev=173.40' Storage=5,726 cf Inflow=19.33 cfs 1.381 af s 0.081 af Primary=19.12 cfs 1.192 af Outflow=19.16 cfs 1.273 af
Pond 2P: Perf Pipe OS4 to OS2 Discarded=0.01 cfs	Peak Elev=172.97' Storage=2,319 cf Inflow=38.75 cfs 2.582 af s 0.033 af Primary=38.71 cfs 2.502 af Outflow=38.72 cfs 2.535 af
Link DP1: Norwalk River South	Inflow=38.71 cfs 2.502 af Primary=38.71 cfs 2.502 af
Link DP2: Norwalk River North	Inflow=24.85 cfs 1.816 af Primary=24.85 cfs 1.816 af

Link DP3: Watercourse

Total Runoff Area = 12.380 ac Runoff Volume = 5.622 af Average Runoff Depth = 5.45" 41.15% Pervious = 5.094 ac 58.85% Impervious = 7.286 ac

Inflow=11.69 cfs 1.036 af Primary=11.69 cfs 1.036 af

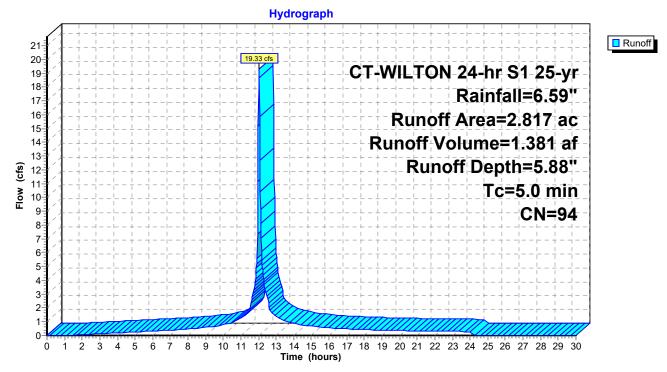
Summary for Subcatchment 1a: Subcat 1a

Runoff = 19.33 cfs @ 12.02 hrs, Volume= Routed to Pond 1P : Perf Pipe to OS4 1.381 af, Depth= 5.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area ((ac)	CN	Desc	cription		
0.1	121	89	<50%	6 Grass co	over, Poor,	, HSG D
0.3	375	80	>75%	6 Grass co	over, Good	d, HSG D
2.1	109	98	Unco	onnected p	avement, I	HSG D
0.2	212	79	Woo	ds/grass c	omb., Goo	od, HSG D
2.8	817	94	Weig	hted Aver	age	
0.7	708		25.1	2% Pervio	us Area	
2.1	109		74.8	8% Imperv	vious Area	
2.7	109		100.	00% Unco	nnected	
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1a: Subcat 1a



Summary for Subcatchment 1b: Subcat 1b

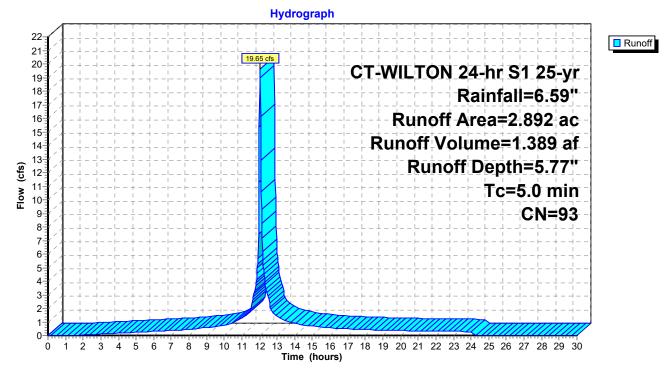
Runoff = 19.65 cfs @ 12.02 hrs, Volume= 1 Routed to Pond 2P : Perf Pipe OS4 to OS2

1.389 af, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area ((ac)	CN	Desc	cription			
0.0	056	89	<50%	% Grass co	over, Poor,	HSG D	
0.7	723	80	>75%	% Grass co	over, Good	HSG D	
2.0	081	98	Unco	onnected p	pavement, l	SG D	
0.0	031	79	Woo	ds/grass c	omb., Goo	, HSG D	
2.8	892	93	Weig	ghted Aver	age		
0.8	811		28.0	3% Pervio	us Area		
2.0	081		71.9	7% Imperv	/ious Area		
2.0	081		100.	00% Unco	nnected		
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0						Direct Entry,	

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 2: North Site Area

Runoff = 24.85 cfs @ 12.02 hrs, Volume= 1. Routed to Link DP2 : Norwalk River North

1.816 af, Depth= 6.12"

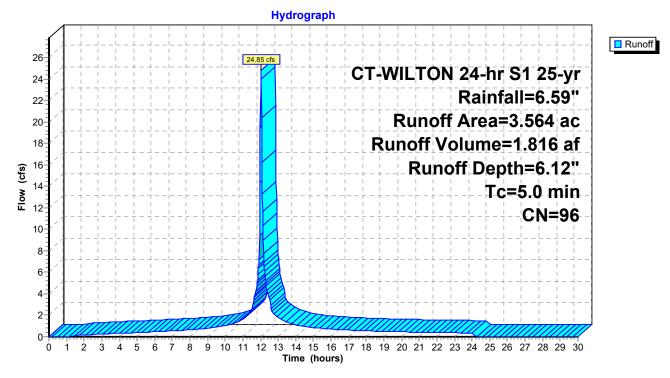
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

_	Area	(ac)	CN	Desc	cription							
	0.	281	89	<50%	<50% Grass cover, Poor, HSG D							
	0.	189	80	>75%	% Grass co	over, Good	, HSG D					
_	3.	094	98	Unco	onnected p	pavement, l	HSG D					
	3.	564	96	Weig	ghted Aver	age						
	0.	0.470 13.18% Pervious Area										
	3.	094		86.8	2% Imper	/ious Area						
	3.	094		100.	00% Unco	nnected						
	Та	اممع	th	Clana	Volocity	Consoitu	Description					
	Tc (min)	Leng		Slope	Velocity	Capacity	Description					
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	Б 0						Diract Entry					

5.0

Direct Entry,

Subcatchment 2: North Site Area



Summary for Subcatchment 3: Subcat 3

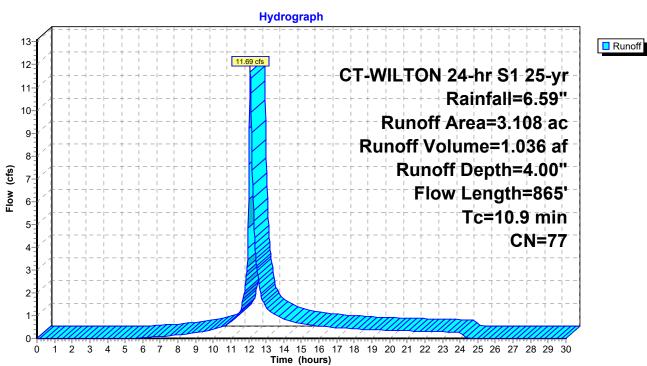
Runoff = 11.69 cfs @ 12.10 hrs, Volume= Routed to Link DP3 : Watercourse 1.036 af, Depth= 4.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area (a	ac) C	N Des	cription							
0.0	40 8	9 <50°	50% Grass cover, Poor, HSG D							
0.1	12 8	0 >75°	% Grass c	over, Good	, HSG D					
0.0	01 9	8 Unc	onnected p	pavement, l	HSG D					
2.9	30 7	7 Woo	ds, Good,	HSG D						
0.0)25 7	<u>'9 Woc</u>	ods/grass o	omb., Goo	d, HSG D					
3.1	08 7	7 Wei	ghted Aver	age						
3.1	-		6% Pervio							
0.0			% Impervi							
0.0	01	100.	00% Unco	nnected						
т	1	01	Mala altri	0	Description					
	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
7.7	50	0.2300	0.11		Sheet Flow,					
4.0	o / =				Woods: Dense underbrush n= 0.800 P2= 3.55"					
1.3	215	0.3255	2.85		Shallow Concentrated Flow,					
1.0	000	0.0447	F 40	00 54	Woodland Kv= 5.0 fps					
1.9	600	0.0117	5.16	82.54	Channel Flow,					
					Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040					
10.9	865	Total								

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 25-yr Rainfall=6.59" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 38



Subcatchment 3: Subcat 3

Summary for Pond 1P: Perf Pipe to OS4

Inflow Area = 2.817 ac, 74.88% Impervious, Inflow Depth = 5.88" for 25-yr event 19.33 cfs @ 12.02 hrs, Volume= 1.381 af Inflow = Outflow = 19.16 cfs @ 12.03 hrs, Volume= 1.273 af, Atten= 1%, Lag= 0.2 min Discarded = 0.04 cfs @ 12.03 hrs, Volume= 0.081 af Primary = 19.12 cfs @ 12.03 hrs, Volume= 1.192 af Routed to Pond 2P : Perf Pipe OS4 to OS2

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 173.40' @ 12.03 hrs Surf.Area= 3,427 sf Storage= 5,726 cf

Plug-Flow detention time= 98.4 min calculated for 1.273 af (92% of inflow) Center-of-Mass det. time= 52.9 min (823.9 - 771.0)

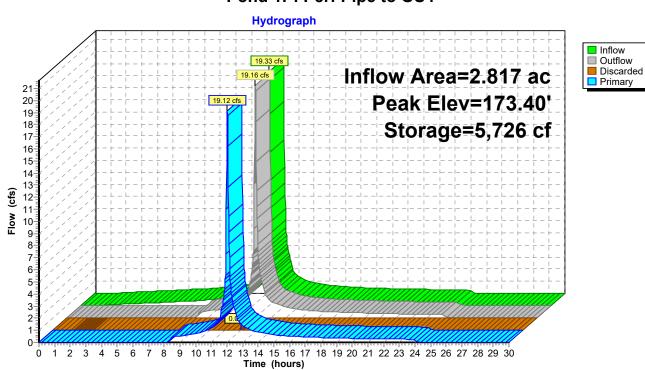
Volume	Invert	Avail.	Storage	Storage Descriptio	n				
#1	169.41'		2,743 cf	36.0" Round Pipe Storage Inside #2 L= 388.0' S= 0.0010 '/'					
#2	168.91'		1,622 cf	72.0" W x 42.0" H Box Stone L= 388.0' S= 0.0010 '/'					
#3	169.61'		813 cf	-	8,148 cf Overall - 2,743 cf Embedded = 5,405 cf x 30.0% Voids 36.0" Round Pipe Storage Inside #4				
#4	169.11'		481 cf	72.0" W x 42.0" H L= 115.0' S= 0.00	Box Stone				
#5	172 40'		5 240 of	2,415 cf Overall - 8	13 cf Embedded =	1,602 cf x 30.0% Vo	ids		
#3	172.40'		5,249 cf			a below (Recald)			
		I	0,906 CI	Total Available Sto	rage				
Elevation	_	rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(feet	/	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>			
172.40		1	1.0	0	0	1			
173.00 174.00		10 2,050	15.0 300.0	3 734	3 737	19 7,165			
174.00		2,050 7,550	570.0	4,511	5,249	25,863			
175.00	5	7,550	570.0	4,511	5,249	25,005			
Device	Routing	Inv	ert Outle	et Devices					
#1	Primary	172.	41' 72.0	" W x 32.0" H Vert.	Weir Plate C= 0.	600			
	2		Limit	nited to weir flow at low heads					
#2	Discarded	168.	91' 0.50	00 in/hr Exfiltration over Surface area Phase-In= 0.01'					
Diogordo	Disperded OutElow Max=0.04 of $(2.02 \text{ bro} H)W=172.40!$ (Erec Dispherec)								

Discarded OutFlow Max=0.04 cfs @ 12.03 hrs HW=173.40' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=18.91 cfs @ 12.03 hrs HW=173.40' (Free Discharge) -1=Weir Plate (Orifice Controls 18.91 cfs @ 3.19 fps)

20849_EX HydroCAD

Prepared by VHB, Inc



Pond 1P: Perf Pipe to OS4

Summary for Pond 2P: Perf Pipe OS4 to OS2

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 5.43" for 25-yr event 38.75 cfs @ 12.03 hrs, Volume= Inflow 2.582 af = Outflow = 38.72 cfs @ 12.03 hrs, Volume= 2.535 af, Atten= 0%, Lag= 0.0 min Discarded = 0.01 cfs @ 12.03 hrs, Volume= 0.033 af Primary = 38.71 cfs @ 12.03 hrs, Volume= 2.502 af Routed to Link DP1 : Norwalk River South

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 172.97' @ 12.03 hrs Surf.Area= 1,240 sf Storage= 2,319 cf

Plug-Flow detention time= 24.6 min calculated for 2.534 af (98% of inflow) Center-of-Mass det. time= 13.4 min (807.6 - 794.2)

Volume	Invert	Avail.	Storage	Storage Description	n					
#1	167.20'		1,449 cf	36.0" Round Pip	36.0" Round Pipe Storage Inside #2					
					L= 205.0' S= 0.0010 '/'					
#2	166.70'		857 cf							
				L= 205.0' S= 0.00						
	(=0.00)					$d = 2,856 \text{ cf } \times 30.0\% \text{ Voids}$				
#3	170.20'		5,259 cf	Custom Stage Da	ita (Irregular)Liste	d below (Recalc)				
			7,565 cf	Total Available Sto	orage					
Elevatio	on Su	ırf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area				
(fee		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)				
170.2	20	1	1.0	0	0	1				
173.0	00	10	15.0	13	13	30				
174.0	00	2,050	300.0	734	748	7,175				
175.0	00	7,550	570.0	4,511	5,259	25,873				
Device	Routing	Inv	ert Outle	et Devices						
#1	Discarded	166.	70' 0.50	0 in/hr Exfiltration	over Surface are	a Phase-In= 0.01'				
#2	Primary	170.	20' 36.0	" Round Culvert						
	-		L= 2	5.0' CPP, end-sec	tion conforming to	fill, Ke= 0.500				
			Inlet	/ Outlet Invert= 170).20'/169.10' S=	0.0440 '/' Cc= 0.900				
			n= 0	.013 Corrugated Pl	E, smooth interior,	Flow Area= 7.07 sf				
Discarded OutFlow Max=0.01 cfs @ 12.03 hrs HW=172.95' (Free Discharge)										

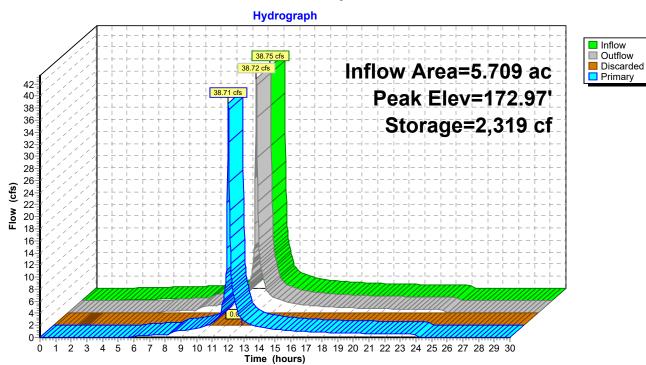
1=Exfiltration (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=38.35 cfs @ 12.03 hrs HW=172.95' (Free Discharge) ←2=Culvert (Inlet Controls 38.35 cfs @ 5.65 fps)

EXISTING CONDITIONS

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 25-yr Rainfall=6.59" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 42

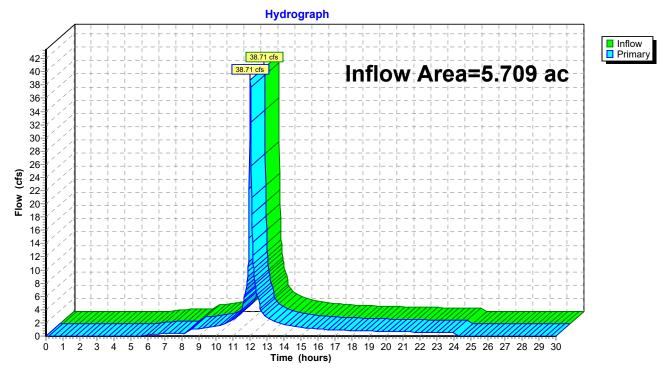


Pond 2P: Perf Pipe OS4 to OS2

Summary for Link DP1: Norwalk River South

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 5.26" for 25-yr event Inflow = 38.71 cfs @ 12.03 hrs, Volume= 2.502 af Primary = 38.71 cfs @ 12.03 hrs, Volume= 2.502 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

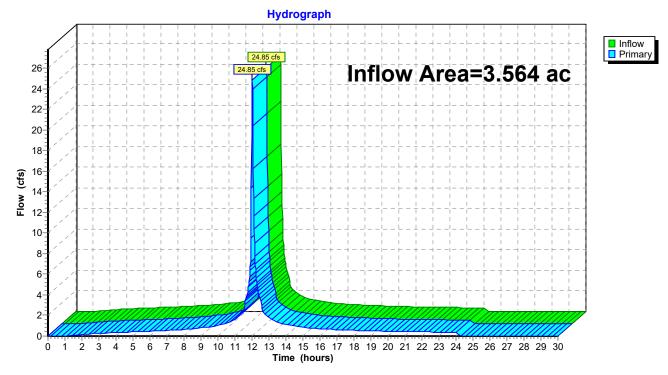


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Area = 3.564 ac, 86.82% Impervious, Inflow Depth = 6.12" for 25-yr event Inflow = 24.85 cfs @ 12.02 hrs, Volume= 1.816 af Primary = 24.85 cfs @ 12.02 hrs, Volume= 1.816 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

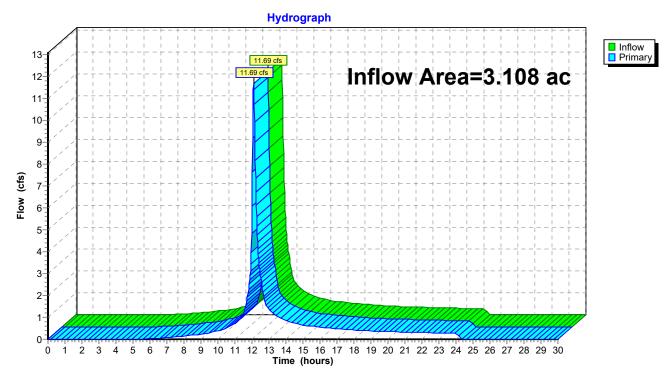


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse

Inflow Are	a =	3.108 ac,	0.04% Impervious,	Inflow Depth =	4.00" for 25-yr event
Inflow	=	11.69 cfs @	12.10 hrs, Volume	e= 1.036 a	af
Primary	=	11.69 cfs @	12.10 hrs, Volume	e= 1.036 a	af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse

Time span=0.00-30.00 hrs, dt=0.02 hrs, 1501 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1a: Subcat1a	Runoff Area=2.817 ac 74.88% Impervious Runoff Depth=7.67" Tc=5.0 min CN=94 Runoff=24.25 cfs 1.800 af
Subcatchment1b: Subcat1b	Runoff Area=2.892 ac 71.97% Impervious Runoff Depth=7.55" Tc=5.0 min CN=93 Runoff=24.73 cfs 1.819 af
Subcatchment2: North Site Area	Runoff Area=3.564 ac 86.82% Impervious Runoff Depth=7.91" Tc=5.0 min CN=96 Runoff=31.00 cfs 2.349 af
Subcatchment3: Subcat3	Runoff Area=3.108 ac 0.04% Impervious Runoff Depth=5.63" Flow Length=865' Tc=10.9 min CN=77 Runoff=15.98 cfs 1.459 af
Pond 1P: Perf Pipe to OS4 Discarded=0.04 ct	Peak Elev=173.56' Storage=5,815 cf Inflow=24.25 cfs 1.800 af is 0.082 af Primary=23.88 cfs 1.611 af Outflow=23.92 cfs 1.693 af
Pond 2P: Perf Pipe OS4 to OS2 Discarded=0.02 ct	Peak Elev=173.64' Storage=2,539 cf Inflow=48.56 cfs 3.430 af s 0.034 af Primary=47.46 cfs 3.343 af Outflow=47.48 cfs 3.377 af
Link DP1: Norwalk River South	Inflow=47.46 cfs 3.343 af Primary=47.46 cfs 3.343 af
Link DP2: Norwalk River North	Inflow=31.00 cfs 2.349 af Primary=31.00 cfs 2.349 af
Link DP3: Watercourse	Inflow=15.98 cfs 1.459 af Primary=15.98 cfs 1.459 af

Total Runoff Area = 12.380 ac Runoff Volume = 7.428 af Average Runoff Depth = 7.20" 41.15% Pervious = 5.094 ac 58.85% Impervious = 7.286 ac

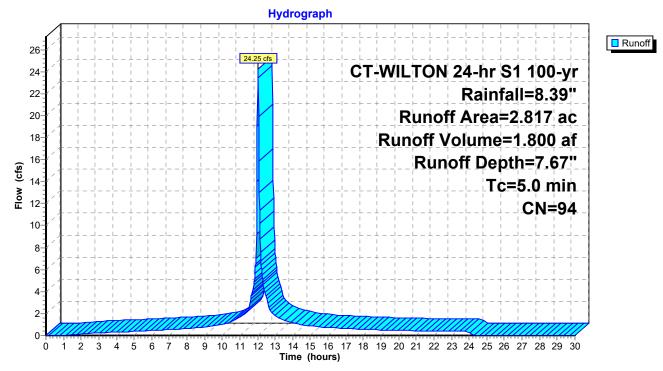
Summary for Subcatchment 1a: Subcat 1a

Runoff = 24.25 cfs @ 12.02 hrs, Volume= Routed to Pond 1P : Perf Pipe to OS4 1.800 af, Depth= 7.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area (ac)	CN	Desc	ription		
0.1	121	89	<50%	6 Grass co	over, Poor,	; HSG D
0.3	375	80	>75%	6 Grass co	over, Good	d, HSG D
2.1	109	98	Unco	onnected p	avement, I	HSG D
0.2	212	79	Woo	ds/grass c	omb., Goo	od, HSG D
2.8	317	94	Weig	hted Aver	age	
0.7	708		25.1	2% Pervio	us Area	
2.1	109		74.8	8% Imperv	vious Area	
2.7	109		100.0	00% Unco	nnected	
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	
5.0	•		///	, , , , , , , , , , , , , , , , , , ,		Direct Entry,

Subcatchment 1a: Subcat 1a



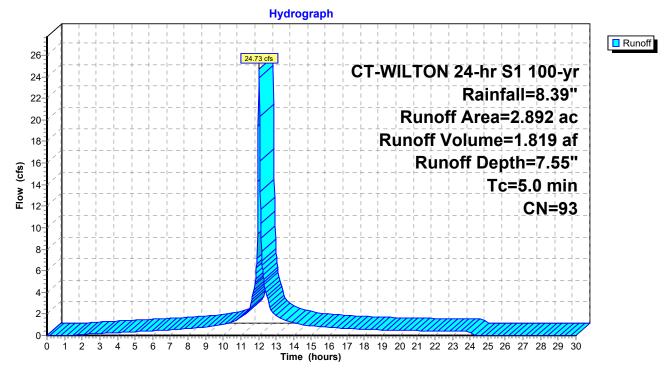
Summary for Subcatchment 1b: Subcat 1b

Runoff = 24.73 cfs @ 12.02 hrs, Volume= 1.819 af, Depth= 7.55" Routed to Pond 2P : Perf Pipe OS4 to OS2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

	Area (a	c) C	N Des	cription			
	0.05	56 8	9 <50	% Grass c	over, Poor,	HSG D	
	0.72	23 8	0 >75	% Grass co	over, Good	, HSG D	
	2.08	31 S	8 Unc	onnected p	pavement, l	HSG D	
	0.03	31 7	'9 Woo	ods/grass o	omb., Goo	d, HSG D	
-	2.89	92 9	3 Wei	ghted Aver	age		
	0.81	1	28.0	3% Pervio	us Area		
	2.08	31	71.9	7% Imperv	/ious Area		
	2.08	31	100.	00% Unco	nnected		
	Tc L	.ength	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.0					Direct Entry,	

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 2: North Site Area

31.00 cfs @ 12.02 hrs, Volume= Runoff = Routed to Link DP2 : Norwalk River North

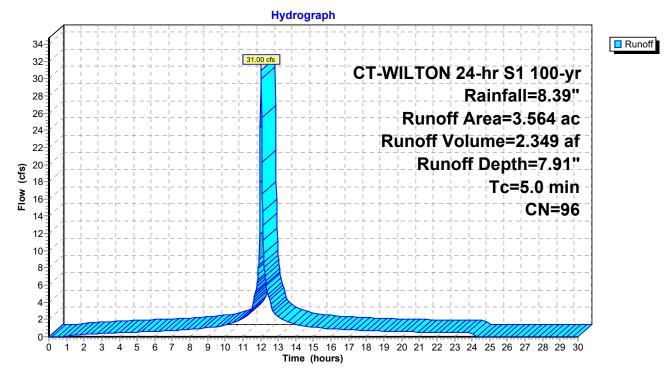
2.349 af, Depth= 7.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area	(ac)	CN	Desc	cription		
0	.281	89	<50%	6 Grass c	over, Poor,	, HSG D
0	.189	80	>75%	6 Grass co	over, Good	d, HSG D
3	.094	98	Unco	onnected p	pavement, l	HSG D
3	.564	96	Weig	hted Aver	age	
0	.470		13.18	8% Pervio	us Area	
3	.094		86.82	2% Imperv	/ious Area	
3	.094		100.0	00% Unco	nnected	
Тс	Leng		Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
5.0						Direct Entry,

Direct Entry,

Subcatchment 2: North Site Area



Summary for Subcatchment 3: Subcat 3

Runoff = 15.98 cfs @ 12.10 hrs, Volume= Routed to Link DP3 : Watercourse

1.459 af, Depth= 5.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area	(ac) C	N Des	cription						
0	.040 8	39 <50	% Grass c	over, Poor,	HSG D				
0	.112 8	30 >75	% Grass c	over, Good	, HSG D				
0	.001 9	98 Unc	nconnected pavement, HSG D						
2	.930	77 Woo	Voods, Good, HSG D						
0.	.025	79 Woo	ods/grass o	omb., Goo	d, HSG D				
3	.108	77 Wei	ghted Aver	age					
	.107		6% Pervio						
	.001		% Impervi						
0.	.001	100.	.00% Unco	nnected					
т	1	01	\/_l!	0	Description				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
7.7	50	0.2300	0.11		Sheet Flow,				
					Woods: Dense underbrush n= 0.800 P2= 3.55"				
1.3	215	0.3255	2.85		Shallow Concentrated Flow,				
1.0	-								
-				•• • •	Woodland Kv= 5.0 fps				
1.9	600	0.0117	5.16	82.54	Channel Flow,				
-	600		5.16	82.54					

20849_EX HydroCAD Prepared by VHB, Inc

1 0

Ó

EXISTING CONDITIONS CT-WILTON 24-hr S1 100-yr Rainfall=8.39" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 51

Hydrograph Runoff 17 15.98 cfs 16-CT-WILTON 24-hr S1 100-yr 15 Rainfall=8.39" 14 Runoff Area=3.108 ac 13-12-Runoff Volume=1.459 af 11 Runoff Depth=5.63" 10 (cfs) Flow Length=865' Tc=10.9 min 7 CN=77 6-5-4 3-2

Subcatchment 3: Subcat 3

9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Time (hours) 3 2 4 5 6 7 8 1

Summary for Pond 1P: Perf Pipe to OS4

Inflow Area = 2.817 ac, 74.88% Impervious, Inflow Depth = 7.67" for 100-yr event 24.25 cfs @ 12.02 hrs, Volume= Inflow = 1.800 af Outflow = 23.92 cfs @ 12.03 hrs, Volume= 1.693 af, Atten= 1%, Lag= 0.4 min Discarded = 0.04 cfs @ 12.03 hrs, Volume= 0.082 af Primary = 23.88 cfs @ 12.03 hrs, Volume= 1.611 af Routed to Pond 2P : Perf Pipe OS4 to OS2

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 173.56' @ 12.03 hrs Surf.Area= 3,743 sf Storage= 5,815 cf

Plug-Flow detention time= 81.3 min calculated for 1.692 af (94% of inflow) Center-of-Mass det. time= 44.9 min (808.8 - 763.9)

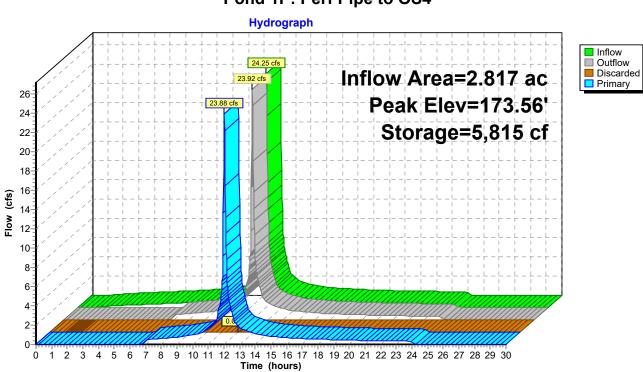
Volume	Invert	Avail	.Storage	Storage Descriptio	n		
#1	169.41'		2,743 cf			2	
				L= 388.0' S= 0.00			
#2	168.91'		1,622 cf	72.0" W x 42.0" H			
				L= 388.0' S= 0.00			
				-	-	l = 5,405 cf x 30.0% Voids	;
#3	169.61'		813 cf	36.0" Round Pipe		4	
				L= 115.0' S= 0.00			
#4	169.11'		481 cf	72.0" W x 42.0" H			
				L= 115.0' S= 0.00			
				-		= 1,602 cf x 30.0% Voids	
#5	172.40'		5,249 cf	Custom Stage Da	ta (Irregular)Listed	d below (Recalc)	
		1	0,906 cf	Total Available Sto	rage		
					•		
Elevatior	ו Su	rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(feet)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
172.40)	1	1.0	0	0	1	
173.00		10	15.0	3	3	19	
174.00		2,050	300.0	734	737	7,165	
175.00		7,550	570.0	4,511	5,249	25,863	
	-	,		, -	-, -	-,	
Device	Routing	Inv	ert Outle	et Devices			
#1	Primary	172.	41' 72.0	" W x 32.0" H Vert.	Weir Plate C= 0.	.600	
	,		Limi	ted to weir flow at lo	w heads		
#2	Discarded	168.	91' 0.50	0 in/hr Exfiltration	over Surface area	a Phase-In= 0.01'	
Discardo	d OutElow	Max-0.0		$2.02 \text{ bro } \square M = 172 \mu$	56' (Eroo Dischar	no)	

Discarded OutFlow Max=0.04 cfs @ 12.03 hrs HW=173.56' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=23.62 cfs @ 12.03 hrs HW=173.56' (Free Discharge) -1=Weir Plate (Orifice Controls 23.62 cfs @ 3.44 fps)

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 100-yr Rainfall=8.39" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 53



Pond 1P: Perf Pipe to OS4

Summary for Pond 2P: Perf Pipe OS4 to OS2

Inflow Area =	5.709 ac, 73.41% Im	pervious, Inflow D	epth = 7.21" for 100-yr event				
Inflow =	48.56 cfs @ 12.03 hrs	s, Volume=	3.430 af				
Outflow =	47.48 cfs @ 12.04 hrs	s, Volume=	3.377 af, Atten= 2%, Lag= 0.5 min				
Discarded =	0.02 cfs @ 12.04 hrs	s, Volume=	0.034 af				
Primary =	47.46 cfs @ 12.04 hrs	s, Volume=	3.343 af				
Routed to Link DP1 : Norwalk River South							

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs / 2 Peak Elev= 173.64' @ 12.04 hrs Surf.Area= 2,147 sf Storage= 2,539 cf

Plug-Flow detention time= 20.6 min calculated for 3.375 af (98% of inflow) Center-of-Mass det. time= 10.9 min (795.3 - 784.4)

Volume	Invert	Avai	I.Storage	Storage Descriptio	n				
#1	167.20'		1,449 cf		36.0" Round Pipe Storage Inside #2				
				L= 205.0' S= 0.00					
#2	166.70'		857 cf	72.0" W x 42.0" H					
				L= 205.0' S= 0.00					
						d = 2,856 cf x 30.0% Void	ds		
#3	170.20'		5,259 cf	Custom Stage Da	i ta (Irregular) Liste	d below (Recalc)			
			7,565 cf	Total Available Sto	orage				
F laundian	0			la a Otana	Ourse Otherse				
Elevation		rf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(feet)		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)			
170.20		1	1.0	0	0	1			
173.00)	10	15.0	13	13	30			
174.00)	2,050	300.0	734	748	7,175			
175.00)	7,550	570.0	4,511	5,259	25,873			
Device	D a t ¹	1		at Daviese					
	Routing			et Devices					
	Discarded			0 in/hr Exfiltration	over Surface are	a Phase-In= 0.01'			
#2 F	Primary	170		" Round Culvert					
				5.0' CPP, end-sec					
						0.0440 '/' Cc= 0.900			
			n= 0	.013 Corrugated Pl	E, smooth interior,	Flow Area= 7.07 sf			
	Discarded OutFlow Max=0.02 cfs @ 12.04 hrs HW=173.62' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.02 cfs)								

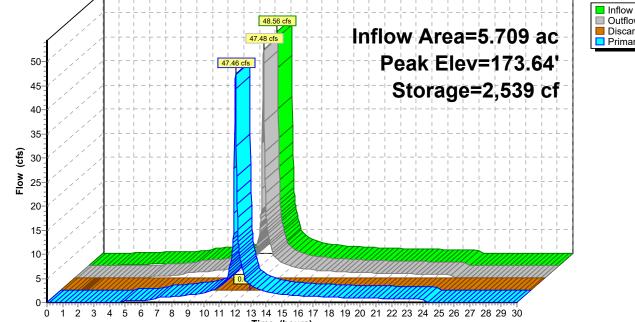
Primary OutFlow Max=47.11 cfs @ 12.04 hrs HW=173.62' (Free Discharge) **2=Culvert** (Inlet Controls 47.11 cfs @ 6.66 fps)

20849_EX HydroCAD Prepared by VHB, Inc

EXISTING CONDITIONS CT-WILTON 24-hr S1 100-yr Rainfall=8.39" Printed 4/1/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 55

Hydrograph Inflow
Outflow 48.56 cfs 47.48 cfs Inflow Area=5.709 ac Discarded Primary Peak Elev=173.64' 47.46 cfs 50 45 Storage=2,539 cf 40 35-**(cfs**) 30-20-15 10-5 0 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Time (hours) 1 2 3 4 5 6 Ó Ż 8

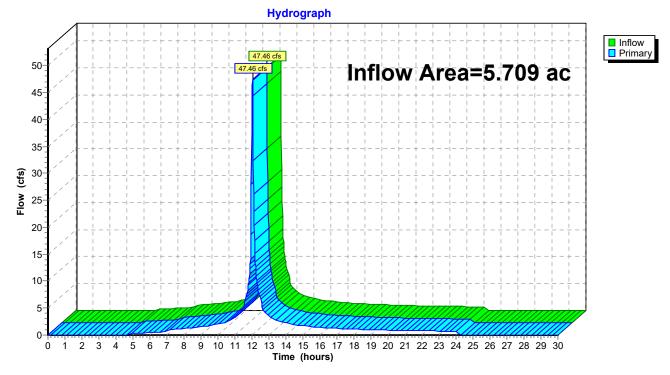
Pond 2P: Perf Pipe OS4 to OS2



Summary for Link DP1: Norwalk River South

Inflow Area = 5.709 ac, 73.41% Impervious, Inflow Depth = 7.03" for 100-yr event Inflow = 47.46 cfs @ 12.04 hrs, Volume= 3.343 af Primary = 47.46 cfs @ 12.04 hrs, Volume= 3.343 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

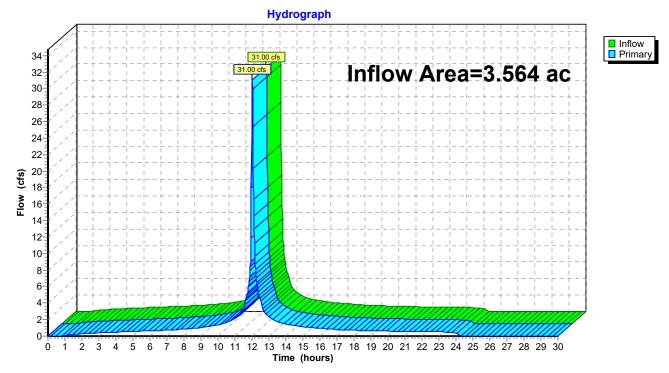


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Area = 3.564 ac, 86.82% Impervious, Inflow Depth = 7.91" for 100-yr event Inflow = 31.00 cfs @ 12.02 hrs, Volume= 2.349 af Primary = 31.00 cfs @ 12.02 hrs, Volume= 2.349 af, Atten= 0%, Lag= 0.0 min Routed to nonexistent node 2L

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

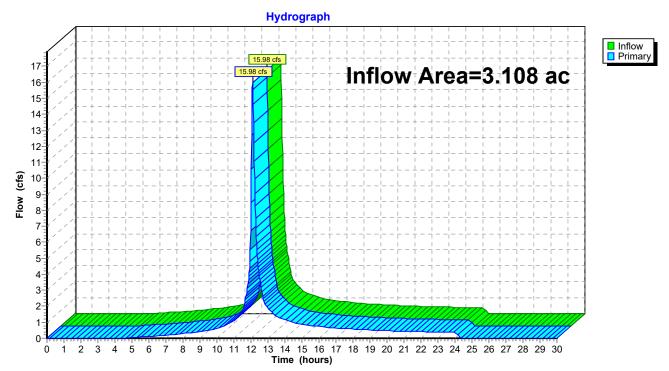


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse

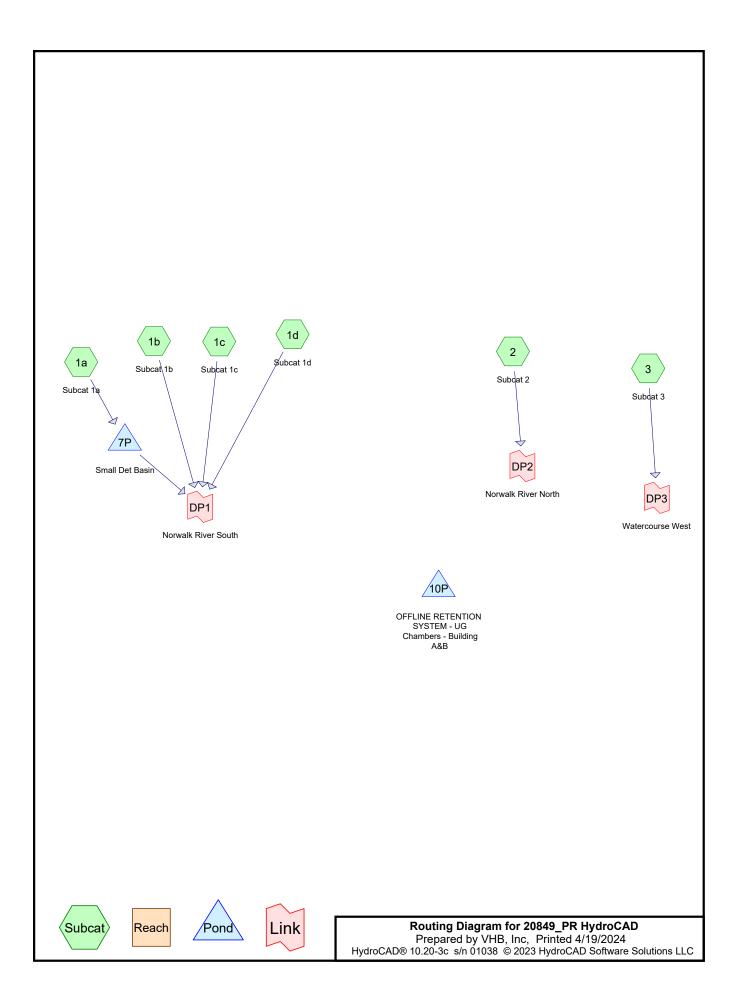
Inflow Are	a =	3.108 ac,	0.04% Impervious,	Inflow Depth =	5.63"	for 100-yr event
Inflow	=	15.98 cfs @	12.10 hrs, Volume	= 1.459 a	af	
Primary	=	15.98 cfs @	12.10 hrs, Volume	= 1.459 a	af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse

HydroCAD: Proposed Conditions



20849_PR HydroCAD

Prepared by VHB, Inc	
HydroCAD® 10.20-3c s/n 01038	© 2023 HydroCAD Software Solutions LLC

Printed 4/19/2024 Page 2

E	Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
	1	2-yr	CT-WILTON 24-hr S1	2-yr	Default	24.00	1	3.55	2
	2	10-yr	CT-WILTON 24-hr S1	10-yr	Default	24.00	1	5.42	2
	3	25-yr	CT-WILTON 24-hr S1	25-yr	Default	24.00	1	6.59	2
	4	100-yr	CT-WILTON 24-hr S1	100-yr	Default	24.00	1	8.39	2

Rainfall Events Listing

Printed 4/19/2024 Page 3

Area Listing (selected nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.284	89	<50% Grass cover, Poor, HSG D (1a, 2, 3)
1.628	80	>75% Grass cover, Good, HSG D (1a, 1b, 1c, 1d, 2, 3)
7.428	98	Unconnected pavement, HSG D (1a, 1b, 1c, 1d, 2, 3)
2.918	77	Woods, Good, HSG D (3)
0.123	79	Woods/grass comb., Good, HSG D (1c)
12.381	90	TOTAL AREA

PROPOSED CONDITIONS

20849_PR HydroCAD

Prepared by VHB, Inc HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Printed 4/19/2024 Page 4

Soil Listing (selected nodes)

Soil Group	Subcatchment Numbers
HSG A	
HSG B	
HSG C	
HSG D	1a, 1b, 1c, 1d, 2, 3
Other	
	TOTAL AREA
	Group HSG A HSG B HSG C HSG D

20849_PR HydroCAD

0.000

0.000

0.000

12.381

Prepared by VHB, IncPrinted 4/19/2024HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLCPage 5

Ground Covers (selected nodes)										
HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers			
0.000	0.000	0.000	0.284	0.000	0.284	<50% Grass cover, Poor	1a, 2, 3			
0.000	0.000	0.000	1.628	0.000	1.628	>75% Grass cover, Good	1a, 1b,			
							1c, 1d, 2, 3			
0.000	0.000	0.000	7.428	0.000	7.428	Unconnected pavement	1a, 1b,			
							1c, 1d,			
							2, 3			
0.000	0.000	0.000	2.918	0.000	2.918	Woods, Good	3			
0.000	0.000	0.000	0.123	0.000	0.123	Woods/grass comb., Good	1c			
	(acres) 0.000 0.000 0.000 0.000	(acres) (acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	HSG-A (acres) HSG-B (acres) HSG-C (acres) 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	HSG-A (acres)HSG-B (acres)HSG-C (acres)HSG-D (acres)0.0000.0000.0000.2840.0000.0000.0001.6280.0000.0000.0007.4280.0000.0000.0002.918	HSG-A (acres) HSG-B (acres) HSG-C (acres) HSG-D (acres) Other (acres) 0.000 0.000 0.000 0.284 0.000 0.000 0.000 0.000 1.628 0.000 0.000 0.000 0.000 7.428 0.000 0.000 0.000 0.000 2.918 0.000	HSG-A (acres)HSG-B (acres)HSG-C (acres)HSG-D (acres)Other (acres)Total (acres)0.0000.0000.0000.2840.0000.2840.0000.0000.0001.6280.0001.6280.0000.0000.0007.4280.0007.4280.0000.0000.0002.9180.0002.918	HSG-A (acres) HSG-B (acres) HSG-C (acres) HSG-D (acres) Other (acres) Total (acres) Ground Cover 0.000 0.000 0.000 0.284 0.000 0.284 <50% Grass cover, Poor			

0.000

12.381

TOTAL AREA

Summary for Subcatchment 1a: Subcat 1a

4.66 cfs @ 12.02 hrs, Volume= Runoff = Routed to Pond 7P : Small Det Basin

0.288 af, Depth= 2.78"

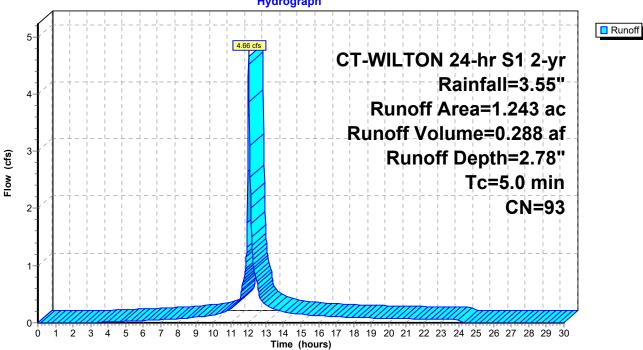
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (ac)	CN	Description
0.002	89	<50% Grass cover, Poor, HSG D
0.348	80	>75% Grass cover, Good, HSG D
0.894	98	Unconnected pavement, HSG D
1.243	93	Weighted Average
0.349		28.11% Pervious Area
0.894		71.89% Impervious Area
0.894		100.00% Unconnected
Tc Len	gth S	Slope Velocity Capacity Description
(min) (fe	et)	(ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment 1a: Subcat 1a



Hydrograph

Summary for Subcatchment 1b: Subcat 1b

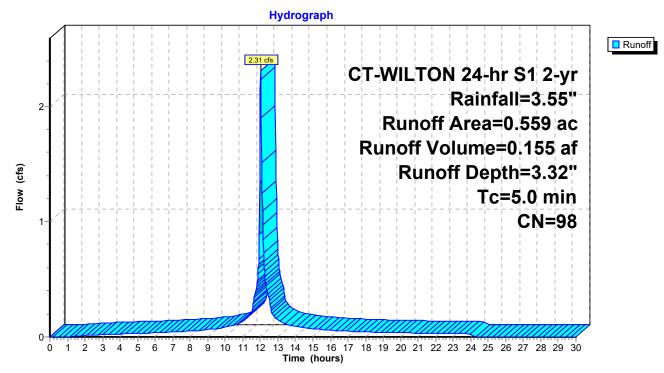
Runoff = 2.31 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.155 af, Depth= 3.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area	(ac)	CN	Desc	ription		
0.	000	80	>75%	6 Grass co	over, Good	d, HSG D
0.	559	98	Unco	onnected p	oavement, I	HSG D
0.	559	98	Weig	hted Aver	age	
0.	000		0.019	% Perviou	s Area	
0.	559			•	∕ious Area	
0.	559		100.0	00% Unco	nnected	
Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 1c: Subcat 1c

Runoff = 10.75 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.659 af, Depth= 2.68"

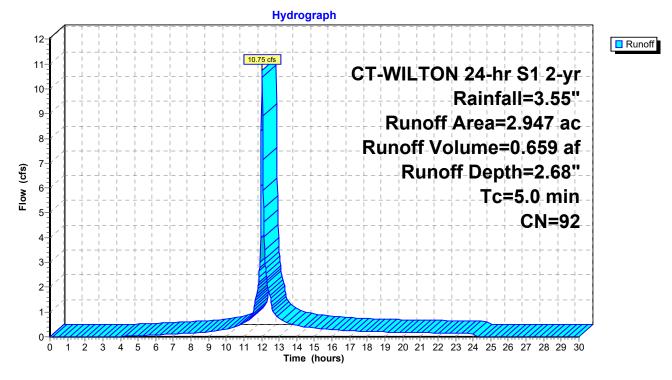
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (ac	c) CN	Description
0.91	4 80	>75% Grass cover, Good, HSG D
1.91	0 98	Unconnected pavement, HSG D
0.12	3 79	Woods/grass comb., Good, HSG D
2.94	7 92	Weighted Average
1.03	57	35.19% Pervious Area
1.91	0	64.81% Impervious Area
1.91	0	100.00% Unconnected
Tc Lo	ength	Slope Velocity Capacity Description
(min)	(feet)	(ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment 1c: Subcat 1c



Summary for Subcatchment 1d: Subcat 1d

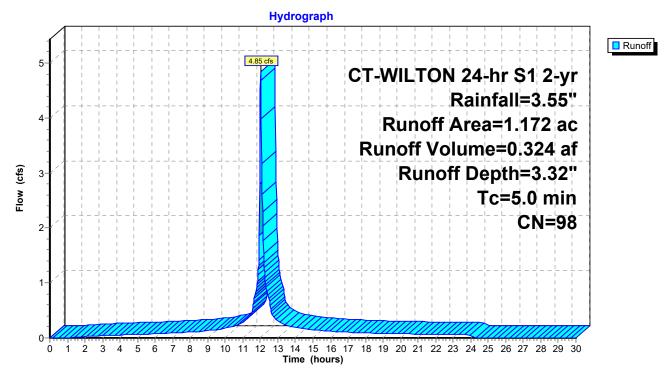
Runoff = 4.85 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.324 af, Depth= 3.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (a	ac) (CN	Desc	ription		
0.0	01	80	>75%	6 Grass co	over, Good	1, HSG D
1.1	71	98	Unco	onnected p	avement, l	HSG D
1.1	72	98	Weig	hted Aver	age	
0.0	01		0.05	% Perviou	s Area	
1.1	71		99.95	5% Imperv	ious Area	
1.1	71		100.0	00% Unco	nnected	
Tc (min)	Length (feet)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1d: Subcat 1d



Summary for Subcatchment 2: Subcat 2

Runoff = 13.52 cfs @ 12.02 hrs, Volume= Routed to Link DP2 : Norwalk River North 0.868 af, Depth= 3.09"

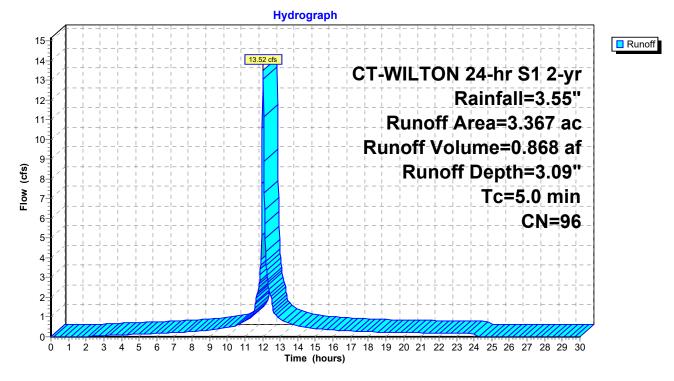
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (ac)	CN	Desc	cription			
0.2	254	89	<50%	% Grass co	over, Poor,	, HSG D	
0.2	231	80	>75%	% Grass co	over, Good	d, HSG D	
2.8	382	98	Unco	onnected p	avement, I	HSG D	
3.3	367	96	Weig	hted Aver	age		
0.4	485		14.3	9% Pervio	us Area		
2.8	382		85.6	85.61% Impervious Area			
2.8	382		100.0	00% Unco	nnected		
Tc (min)	Length (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	

5.0

Direct Entry,

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 4.55 cfs @ 12.10 hrs, Volume= 0.378 Routed to Link DP3 : Watercourse West

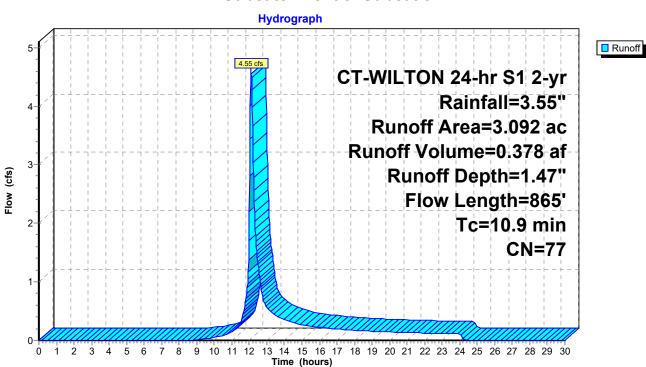
0.378 af, Depth= 1.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 2-yr Rainfall=3.55"

Area (ac) C	N Des	cription						
0.0	028 8	9 <50°	50% Grass cover, Poor, HSG D						
0.1	135 8	0 >75°	% Grass c	over, Good	, HSG D				
0.0	D11 9	8 Unc	onnected p	pavement, l	HSG D				
2.9	918 7	7 Woo	ds, Good,	HSG D					
3.0	092 7	7 Weig	ghted Aver	age					
3.0	081	99.6	4% Pervio	us Area					
0.0	011	0.36	% Impervi	ous Area					
0.0	011	100.	00% Unco	nnected					
_		-		-					
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
7.7	50	0.2300	0.11		Sheet Flow,				
					Woods: Dense underbrush n= 0.800 P2= 3.55"				
1.3	215	0.3255	2.85		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
1.9	600	0.0117	5.16	82.54	Channel Flow,				
1.9	600	0.0117	5.16	82.54	Channel Flow, Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040				

20849_PR HydroCAD Prepared by VHB, Inc

PROPOSED CONDITIONS CT-WILTON 24-hr S1 2-yr Rainfall=3.55" Printed 4/19/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 12



Subcatchment 3: Subcat 3

Summary for Pond 7P: Small Det Basin

Inflow Area =	1.243 ac, 7	1.89% Impervious, Inf	low Depth = 2.78" for 2-yr event
Inflow =	4.66 cfs @	12.02 hrs, Volume=	0.288 af
Outflow =	4.11 cfs @	12.05 hrs, Volume=	0.288 af, Atten= 12%, Lag= 1.8 min
Discarded =	0.02 cfs @	5.82 hrs, Volume=	0.026 af
Primary =	4.09 cfs @	12.05 hrs, Volume=	0.262 af
Routed to Link	DP1 : Norwa	lk River South	

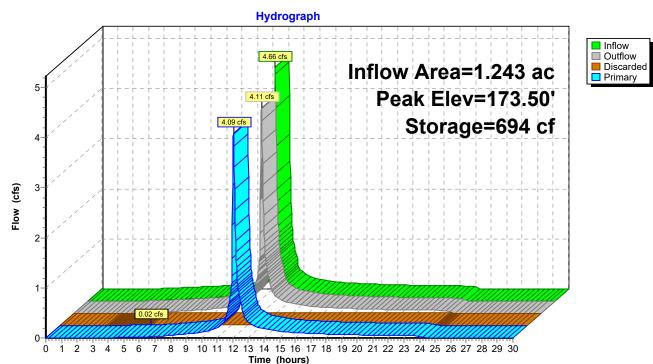
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 173.50' @ 12.05 hrs Surf.Area= 692 sf Storage= 694 cf

Plug-Flow detention time= 6.4 min calculated for 0.288 af (100% of inflow) Center-of-Mass det. time= 6.3 min (804.4 - 798.1)

Volume	Inve	rt Avail.	.Storage	Storage De	scription			
#1	172.5	0'	1,728 cf	StormTrap	Listed below	Inside #2		
#2	172.5	0'	2 cf	Custom St	age Data (Pri	smatic)Listed	below (Recalc)	
				1,730 cf Ov	erall - 1,728 c	f Embedded =	2 cf	
			1,730 cf	Total Availa	ble Storage			
	0							
Elevatio	-	um.Store						
(fee	1	ubic-feet)						
172.5	-	0						
172.7	-	108						
173.2	-	216						
173.2		324						
173.5	50	525						
173.7	'5	725						
174.0	0	926						
174.2	25	1,126						
174.5	50	1,327						
174.7	'5	1,527						
175.0	00	1,728						
		o ()		01	0 01			
Elevatio		Surf.Area		.Store	Cum.Store			
(fee		(sq-ft)	(CUDI	c-feet)	(cubic-feet)			
172.5	-	692		0	0			
175.0	00	692		1,730	1,730			
Device	Routing	Inv	ert Outl	et Devices				
#1	Primary	172.			Vert Orifice	/Grate C= 0.0	600	
	. minury	172.			w at low head			
#2	Primary	173.				Grate C= 0.6	00	
π∠	i minary	170.			w at low head			
#3	Discarde	d 172.					Phase-In= 0.01'	
110	Biotaide	G 172.						

Discarded OutFlow Max=0.02 cfs @ 5.82 hrs HW=172.53' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=4.06 cfs @ 12.05 hrs HW=173.50' (Free Discharge) -1=Orifice/Grate (Orifice Controls 3.50 cfs @ 3.73 fps) -2=Orifice/Grate (Orifice Controls 0.56 cfs @ 2.26 fps)



Pond 7P: Small Det Basin

Summary for Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

4' underground concrete chambers OFFLINE for 1" WQV retention. System on plan will show slightly smaller since we will be able to reuse the 350' portion of the existing 36" perforated pipe that is within the existing swale under existing mature vegetation.

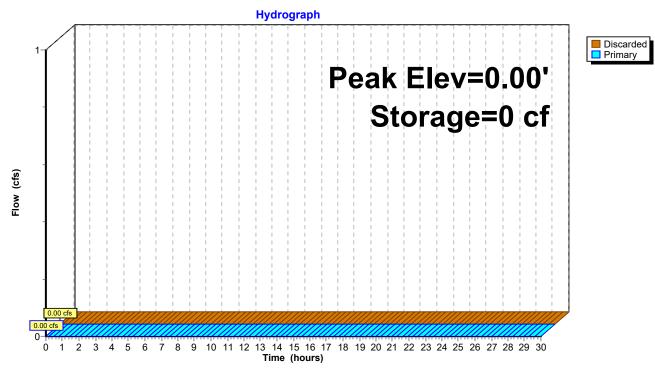
Volume	Invert	Avail.Sto	rage Stora	age Description				
#1	170.80'	6,2	75 cf Storr	mTrapListed below Inside #2				
#2	170.80'	,		om Stage Data (Prismatic)Listed below (Recalc)				
				5 cf Overall - 6,275 cf Embedded = 0 cf				
		6,2	75 cf Total	Available Storage				
Elevatio	n Cur	m.Store						
(fee		pic-feet)						
170.8	50 50	0						
171.0		392						
171.3	0	785						
171.5	5	1,177						
171.8		1,906						
172.0		2,634						
172.3		3,362						
172.5		4,091						
172.8		4,819						
173.0		5,547						
173.3	0	6,275						
Elevatio	n Su	urf.Area	Inc.Store	cum.Store				
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)				
170.8		2,510	0					
173.3	0	2,510	6,275	6,275				
Device	Routing	Invert	Outlet Dev	vices				
#1	Discarded	170.80'	1.000 in/h	r Exfiltration over Horizontal area Phase-In= 0.01'				
#2	Primary	173.30'	6.0' long	x 0.5' breadth Broad-Crested Rectangular Weir				
	-		Head (feet	t) 0.20 0.40 0.60 0.80 1.00				
			Coef. (Eng	glish) 2.80 2.92 3.08 3.30 3.32				
D'- '								
	Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge)							

1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

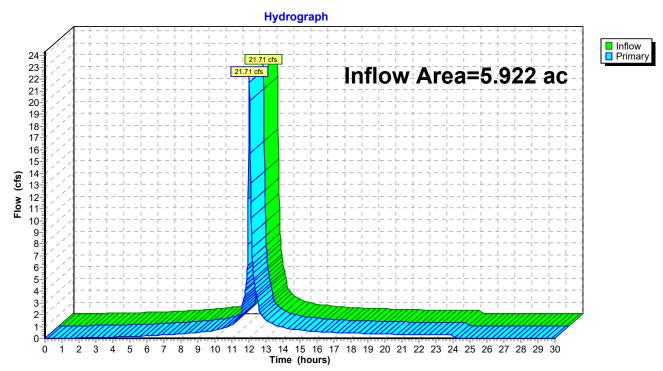
Page 16



Summary for Link DP1: Norwalk River South

Inflow Are	ea =	5.922 ac, 76.57% Impervious, Inflow Depth = 2.84" for 2-yr event
Inflow	=	21.71 cfs @ 12.03 hrs, Volume= 1.400 af
Primary	=	21.71 cfs @ 12.03 hrs, Volume= 1.400 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

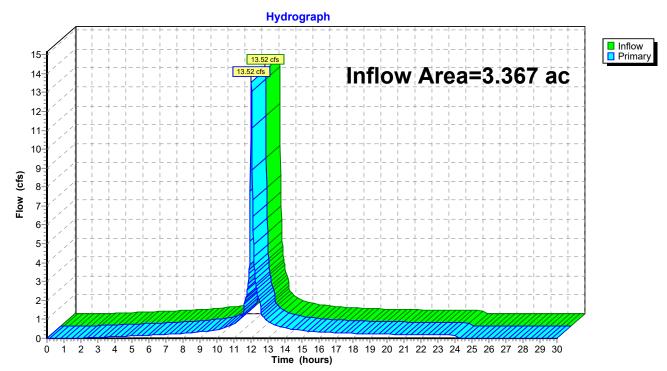


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Are	a =	3.367 ac, 85.61% Impervious, Inflow Depth = 3.09" for 2-yr even	ıt
Inflow	=	13.52 cfs @ 12.02 hrs, Volume= 0.868 af	
Primary	=	13.52 cfs @ 12.02 hrs, Volume= 0.868 af, Atten= 0%, Lag=	0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

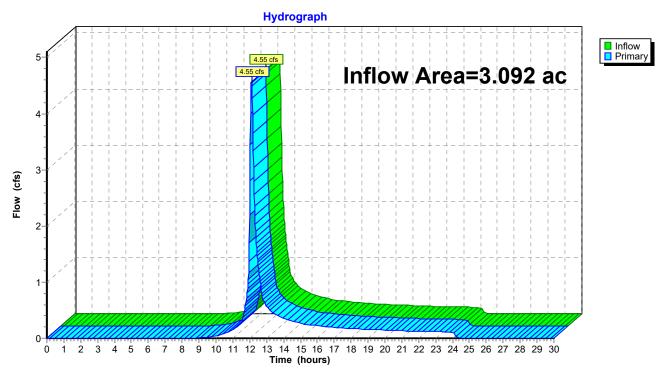


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse West

Inflow Are	a =	3.092 ac,	0.36% Impervious,	Inflow Depth = 1	.47" for 2-yr event
Inflow	=	4.55 cfs @	12.10 hrs, Volume	e= 0.378 af	
Primary	=	4.55 cfs @	12.10 hrs, Volume	e= 0.378 af	, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse West

Summary for Subcatchment 1a: Subcat 1a

Runoff = 7.02 cfs @ 12.02 hrs, Volume= Routed to Pond 7P : Small Det Basin

0.478 af, Depth= 4.61"

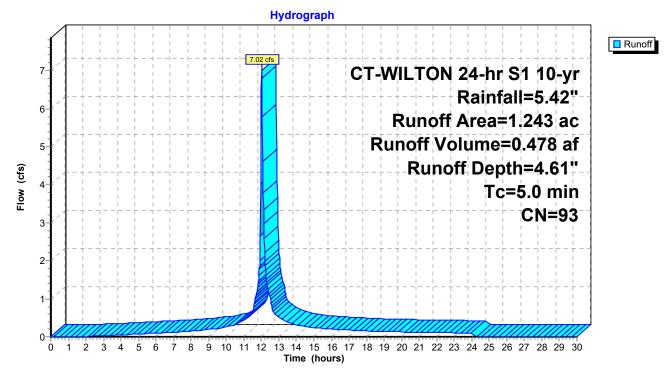
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

A	rea (ac)	CN	Descr	iption					
	0.002	89	<50%	Grass co	over, Poor,	, HSG D			
	0.348	80	>75%	Grass co	over, Good,	d, HSG D			
	0.894	98	Uncor	nnected p	avement, ł	HSG D			
	1.243	93	Weigh	Weighted Average					
	0.349		28.11	28.11% Pervious Area					
	0.894		71.89	% Imperv	ious Area				
	0.894		100.00	0% Unco	nnected				
	Tc Leng	th S	Slope '	Velocity	Capacity	Description			
(m	nin) (fee	et)	(ft/ft)	(ft/sec)	(cfs)				

5.0

Direct Entry,

Subcatchment 1a: Subcat 1a



Summary for Subcatchment 1b: Subcat 1b

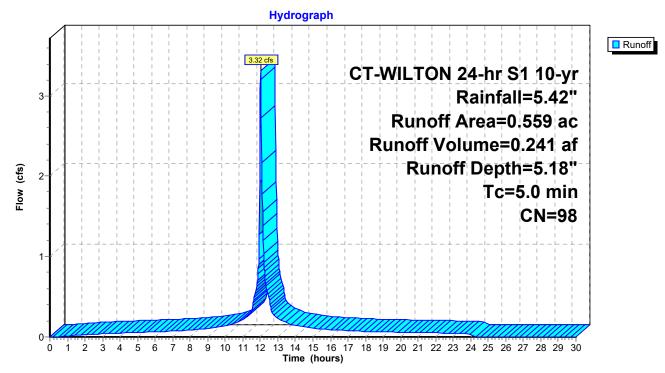
Runoff = 3.32 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.241 af, Depth= 5.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac)	CN	Desc	ription		
0.	000	80	>75%	6 Grass co	over, Good	1, HSG D
0.	559	98	Unco	onnected p	avement, l	HSG D
0.	559	98	Weig	hted Aver	age	
0.	000		0.01	% Perviou	s Ārea	
0.	559				vious Area	
0.	559		100.0	00% Unco	nnected	
Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 1c: Subcat 1c

Runoff = 16.39 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South 1.105 af, Depth= 4.50"

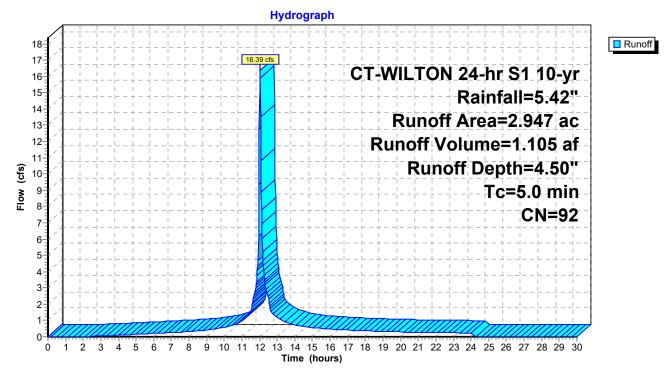
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac)	CN	Desc	cription					
0.	914	80	>75%	% Grass co	over, Good	, HSG D			
1.	910	98	Unco	onnected p	avement, ł	HSG D			
0.	123	79	Woo	ds/grass c	omb., Goo	d, HSG D			
2.	947	92	Weig	ghted Aver	age				
1.	037		35.1	35.19% Pervious Area					
1.	910		64.8	1% Imperv	ious Area				
1.	910		100.0	00% Unco	nnected				
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
(min)	(iee	;i)	(\mathbf{n},\mathbf{n})	(it/sec)					

5.0

Direct Entry,

Subcatchment 1c: Subcat 1c



Summary for Subcatchment 1d: Subcat 1d

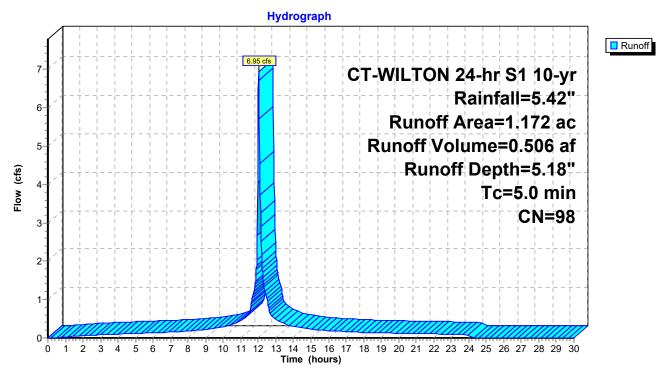
Runoff = 6.95 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.506 af, Depth= 5.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area	(ac)	CN	Desc	ription		
0.	.001	80	>75%	6 Grass co	over, Good	d, HSG D
1.	.171	98	Unco	onnected p	avement, l	HSG D
1.	172	98	Weig	hted Aver	age	
0.	.001		0.05	% Perviou	s Ārea	
1.	.171		99.9	5% Imperv	vious Area	
1.	.171		100.0	00% Unco	nnected	
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1d: Subcat 1d



Summary for Subcatchment 2: Subcat 2

Runoff = 19.69 cfs @ 12.02 hrs, Volume= Routed to Link DP2 : Norwalk River North 1.389 af, Depth= 4.95"

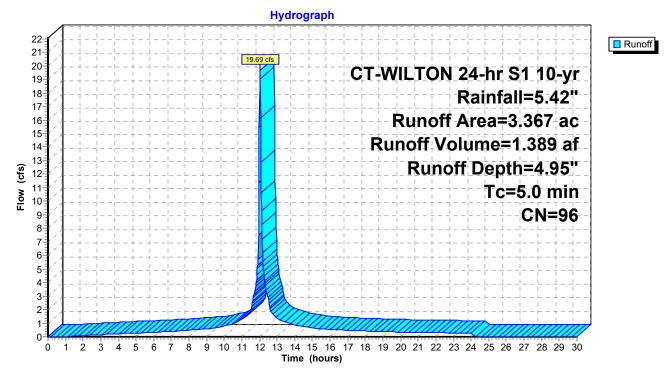
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

Area (a	ac) (CN	Des	cription			
0.2	254	89	<509	% Grass c	over, Poor,	, HSG D	
0.2	231	80	>759	% Grass c	over, Good	d, HSG D	
2.8	882	98	Unco	onnected p	pavement, l	HSG D	
3.3	867	96	Weig	ghted Aver	age		
0.4	85		14.39% Pervious Area				
2.8	382		85.6	1% Imperv	/ious Area		
2.8	882		100.	00% Unco	nnected		
Tc (min)	Length (feet)		ope t/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	

5.0

Direct Entry,

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 8.87 cfs @ 12.10 hrs, Volume= 0.7 Routed to Link DP3 : Watercourse West

0.767 af, Depth= 2.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 10-yr Rainfall=5.42"

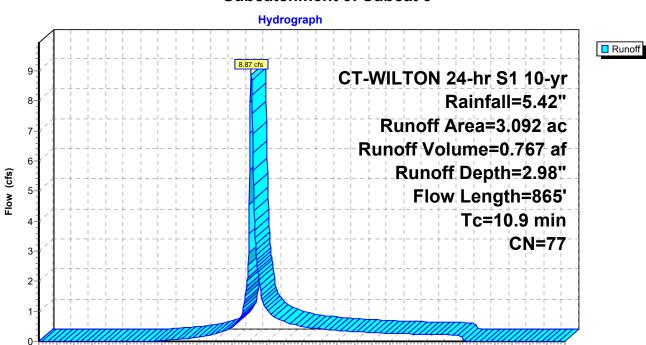
Area (a	ic) C	N Des	cription					
0.02	28 8	39 <50	<50% Grass cover, Poor, HSG D					
0.13	35 8	80 >75	% Grass c	over, Good	, HSG D			
0.01	11 g	8 Unc	onnected p	pavement, l	HSG D			
2.91	<u>18 7</u>	'7 Woo	ods, Good,	HSG D				
3.09	92 7	7 Wei	ghted Aver	age				
3.08	81	99.6	4% Pervio	us Area				
0.01			% Impervi					
0.01	11	100.	00% Uncc	nnected				
Tc L	_ength	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description			
7.7	50	0.2300	0.11	()	Sheet Flow,			
		0.2000	••••		Woods: Dense underbrush n= 0.800 P2= 3.55"			
1.3	215	0.3255	2.85		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
1.9	600	0.0117	5.16	82.54	Channel Flow,			
					Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040			
10.9	865	Total						

20849_PR HydroCAD Prepared by VHB, Inc

1

Ò

PROPOSED CONDITIONS CT-WILTON 24-hr S1 10-yr Rainfall=5.42" Printed 4/19/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 26



Subcatchment 3: Subcat 3

7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 Time (hours) 2 3 4 5 6

Summary for Pond 7P: Small Det Basin

Inflow Area =	1.243 ac, 7	1.89% Impervious, Infl	ow Depth = 4.61" for 10-yr event
Inflow =	7.02 cfs @	12.02 hrs, Volume=	0.478 af
Outflow =	5.83 cfs @	12.06 hrs, Volume=	0.478 af, Atten= 17%, Lag= 2.2 min
Discarded =	0.02 cfs @	3.40 hrs, Volume=	0.029 af
Primary =	5.81 cfs @	12.06 hrs, Volume=	0.449 af
Routed to Link	DP1 : Norwa	lk River South	

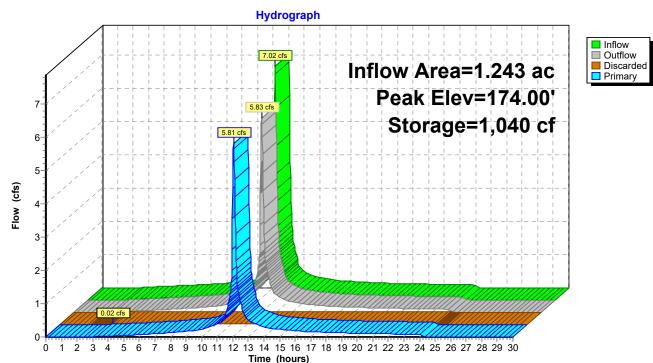
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 174.00' @ 12.06 hrs Surf.Area= 692 sf Storage= 1,040 cf

Plug-Flow detention time= 5.8 min calculated for 0.477 af (100% of inflow) Center-of-Mass det. time= 5.8 min (789.0 - 783.1)

Volume	Inve	rt Avail.S	Storage	Storage Descri	ption	
#1	172.50)' 1	,728 cf	StormTrap List	ted below Inside #2	
#2	172.50)'	2 cf		e Data (Prismatic)Liste	
				1,730 cf Overa	II - 1,728 cf Embedded	I = 2 cf
		1	,730 cf	Total Available	Storage	
Elevatio	-	um.Store				
(fee	/ /	ubic-feet)				
172.5	-	0				
172.7	-	108				
173.2	-	216				
173.2		324				
173.5	-	525				
173.7	5	725				
174.0	0	926				
174.2	5	1,126				
174.5	0	1,327				
174.7	5	1,527				
175.0	0	1,728				
					_	
Elevatio		Surf.Area		-	Im.Store	
(fee	t)	(sq-ft)	(cubio	-feet) (cu	<u>bic-feet)</u>	
172.5	0	692		0	0	
175.0	0	692		1,730	1,730	
Device	Routing	Inve	ert Outle	et Devices		
#1	Primary	172.5	0' 15.0	' W x 9.0" H Ve	ert. Orifice/Grate C=	0.600
	,		Limi	ed to weir flow a	at low heads	
#2	Primary	173.0	0' 6.0"	W x 6.0" H Ver	t. Orifice/Grate C= 0	.600
			Limit	ed to weir flow a	at low heads	
#3	Discardeo	172.5	0' 1.00) in/hr Exfiltrat	ion over Surface area	a Phase-In= 0.01'

Discarded OutFlow Max=0.02 cfs @ 3.40 hrs HW=172.53' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=5.81 cfs @ 12.06 hrs HW=174.00' (Free Discharge) -1=Orifice/Grate (Orifice Controls 4.77 cfs @ 5.09 fps) -2=Orifice/Grate (Orifice Controls 1.04 cfs @ 4.16 fps)



Pond 7P: Small Det Basin

Summary for Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

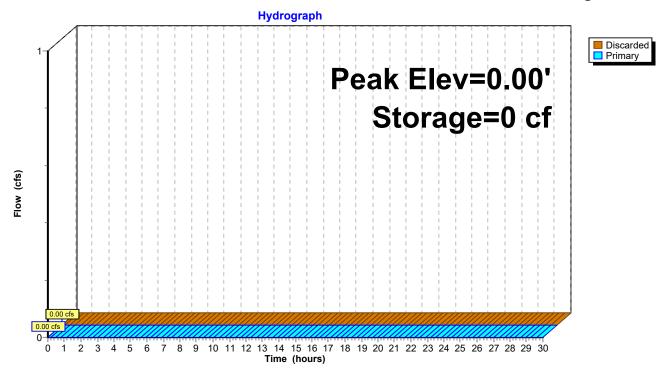
4' underground concrete chambers OFFLINE for 1" WQV retention. System on plan will show slightly smaller since we will be able to reuse the 350' portion of the existing 36" perforated pipe that is within the existing swale under existing mature vegetation.

Volume	Invert	Avail.Sto	rage Stor	age Description		
#1	170.80'			rmTrap Listed below Inside #2		
#2	170.80'			tom Stage Data (Prismatic)Listed below (Recalc)		
			6,27	75 cf Overall - 6,275 cf Embedded = 0 cf		
		6,27	75 cf Tota	al Available Storage		
Elevatio	n Cun	n.Store				
(fee	-	ic-feet)				
170.8		0				
170.0		392				
171.3		785				
171.5		1,177				
171.8		1,906				
172.0		2,634				
172.3	0	3,362				
172.5	5	4,091				
172.8	-	4,819				
173.0		5,547				
173.3	0	6,275				
Elevatio	n Su	rf.Area	Inc.Store	e Cum.Store		
(fee		(sq-ft)	(cubic-feet	-		
170.8	0	2,510		0 0		
173.3	0	2,510	6,27	5 6,275		
Device	Routing	Invert	Outlet De			
#1	Discarded	170.80'		hr Exfiltration over Horizontal area Phase-In= 0.01'		
#2	Primary	173.30'		x 0.5' breadth Broad-Crested Rectangular Weir		
			· ·	et) 0.20 0.40 0.60 0.80 1.00		
			Coel. (En	glish) 2.80 2.92 3.08 3.30 3.32		
Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge)						

1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

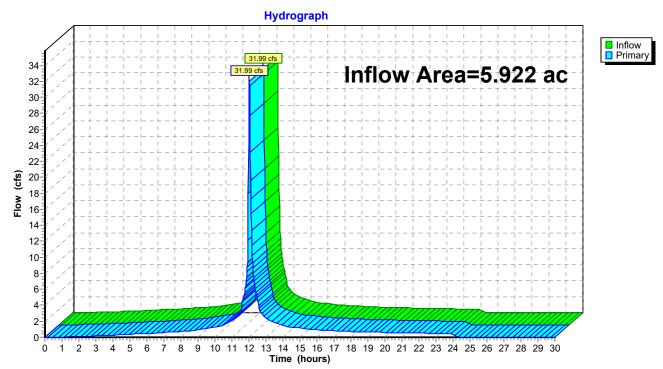
Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B



Summary for Link DP1: Norwalk River South

Inflow Are	a =	5.922 ac, 76.57% Impervious, Inflow Depth = 4.66" for 10-yr event
Inflow	=	31.99 cfs @ 12.03 hrs, Volume= 2.302 af
Primary	=	31.99 cfs @ 12.03 hrs, Volume= 2.302 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

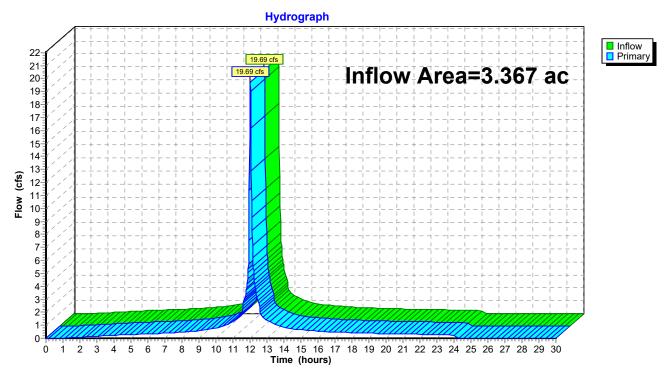


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Are	ea =	3.367 ac, 85.61% Impervious, Inflow Depth = 4.95" for 10-yr event
Inflow	=	19.69 cfs @ 12.02 hrs, Volume= 1.389 af
Primary	=	19.69 cfs @ 12.02 hrs, Volume= 1.389 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

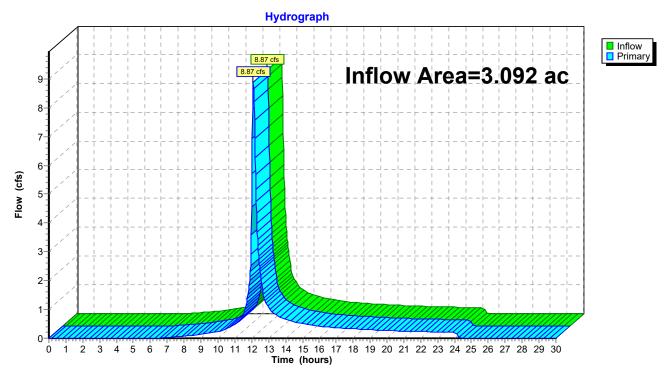


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse West

Inflow Are	a =	3.092 ac,	0.36% Impervious, Infl	ow Depth = 2.98"	for 10-yr event
Inflow	=	8.87 cfs @	12.10 hrs, Volume=	0.767 af	
Primary	=	8.87 cfs @	12.10 hrs, Volume=	0.767 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse West

Summary for Subcatchment 1a: Subcat 1a

Runoff = 8.45 cfs @ 12.02 hrs, Volume= Routed to Pond 7P : Small Det Basin

0.597 af, Depth= 5.77"

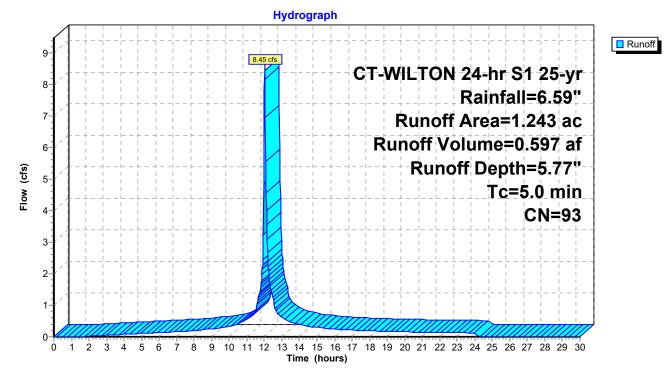
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area (ac)	CN	Desc	cription						
0.0	002	89	<50%	% Grass co	over, Poor,	HSG D				
0.3	348	80	>75%	% Grass co	over, Good	HSG D				
.0	394	98	Unco	onnected p	pavement, l	ISG D				
1.2	243	93	Weig	ghted Aver	age					
0.3	0.349		28.1	28.11% Pervious Area						
0.8	0.894		71.8	71.89% Impervious Area						
0.894			100.	100.00% Unconnected						
Тс	Lengt	:h	Slope	Velocity	Capacity	Description				
(min)	(fee		(ft/ft)	(ft/sec)	(cfs)	I.				

5.0

Direct Entry,

Subcatchment 1a: Subcat 1a



Summary for Subcatchment 1b: Subcat 1b

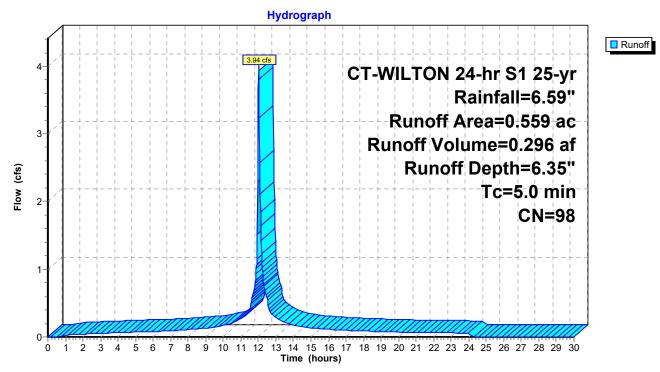
Runoff = 3.94 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.296 af, Depth= 6.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area	(ac)	CN	Desc	Description						
0	.000	80	>75%	6 Grass co	over, Good	, HSG D				
0	.559	98	Unco	onnected p	avement, I	HSG D				
0	.559	98	Weig	Weighted Average						
0	.000		0.010	% Perviou	s Area					
0	.559		99.99	9% Imperv	∕ious Area					
0	0.559 100.0		00% Unco	nnected						
Тс	Leng	th S	Slope	Velocity	Capacity	Description				
(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	•				
5.0						Direct Entry,				

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 1c: Subcat 1c

Runoff = 19.81 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South 1.388 af, Depth= 5.65"

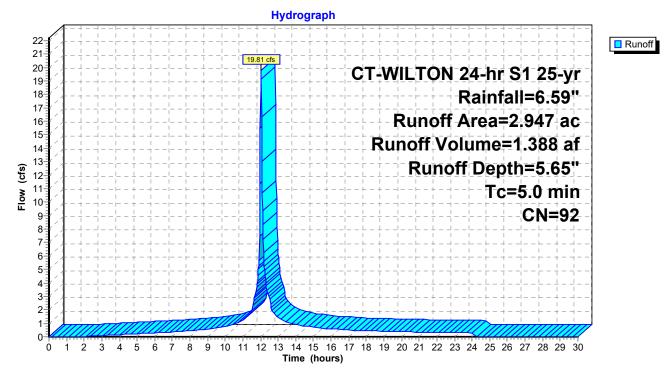
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area (ac)	CN	Description							
0.914	80	>75% Grass cover, Good, HSG D							
1.910	98	Unconnected pavement, HSG D							
0.123	79	Woods/grass comb., Good, HSG D							
2.947	92	Weighted Average							
1.037		35.19% Pervious Area							
1.910		64.81% Impervious Area							
1.910		100.00% Unconnected							
Tc Leng (min) (fe		Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)							

5.0

Direct Entry,

Subcatchment 1c: Subcat 1c



Summary for Subcatchment 1d: Subcat 1d

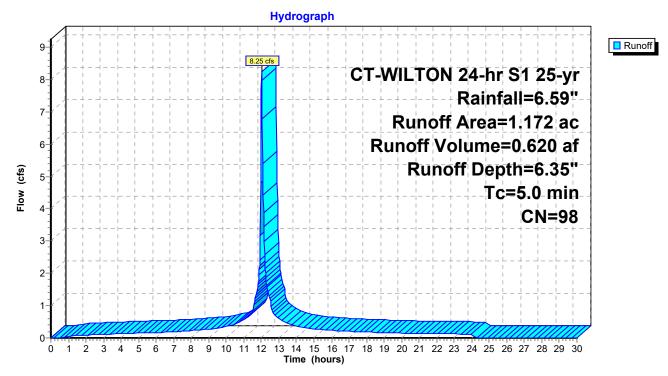
Runoff = 8.25 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

0.620 af, Depth= 6.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area (a	ac) (CN	Desc	Description						
0.0	01	80	>75%	6 Grass co	over, Good	1, HSG D				
1.1	71	98	Unco	onnected p	avement, l	HSG D				
1.1	72	98	Weig	Weighted Average						
0.0	01		0.05	% Perviou	s Ārea					
1.1	1.171 99.95% Impervious Area				ious Area					
1.1	71		100.0	00% Unco	nnected					
Tc (min)	Length (feet)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
5.0						Direct Entry,				

Subcatchment 1d: Subcat 1d



Summary for Subcatchment 2: Subcat 2

Runoff = 23.47 cfs @ 12.02 hrs, Volume= Routed to Link DP2 : Norwalk River North 1.716 af, Depth= 6.12"

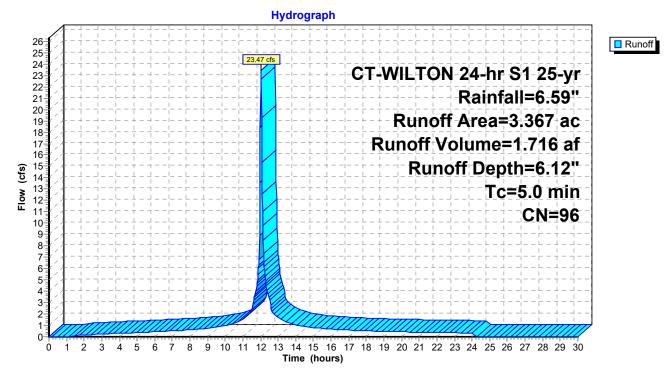
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area	(ac)	CN	Desc	Description						
0.	254	89	<509	% Grass co	over, Poor,	HSG D				
0.	231	80	>75	% Grass co	over, Good	, HSG D				
2.	882	98	Unco	onnected p	pavement, I	HSG D				
3.	367	96	Weig	Weighted Average						
0.4	485		14.3	14.39% Pervious Area						
2.	882		85.6	1% Imperv	/ious Area					
2.	2.882			00% Unco	nnected					
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				

5.0

Direct Entry,

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 11.63 cfs @ 12.10 hrs, Volume= Routed to Link DP3 : Watercourse West

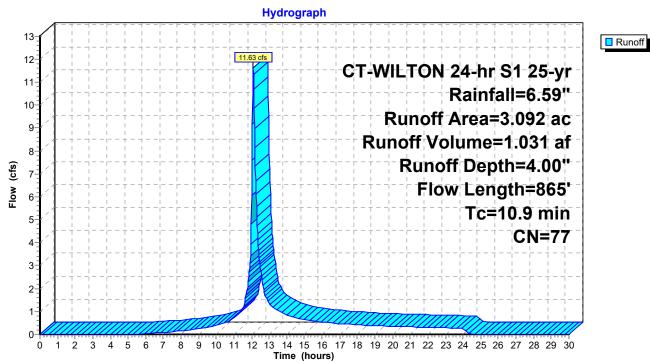
1.031 af, Depth= 4.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 25-yr Rainfall=6.59"

Area (ac)) C	N Dese	cription					
0.028	38	9 <509	50% Grass cover, Poor, HSG D					
0.135	58	0 >75 ^c	% Grass c	over, Good	, HSG D			
0.011	19	8 Unco	onnected p	pavement, l	HSG D			
2.918	37	7 Woo	ds, Good,	HSG D				
3.092	2 7	7 Weig	ghted Aver	age				
3.081	1	99.6	4% Pervio	us Area				
0.011	1	0.36	% Impervi	ous Area				
0.011	1	100.	00% Unco	nnected				
	ength	Slope	Velocity	Capacity	Description			
<u>(min)</u> (feet)	(ft/ft)	(ft/sec)	(cfs)				
7.7	50	0.2300	0.11		Sheet Flow,			
					Woods: Dense underbrush n= 0.800 P2= 3.55"			
1.3	215	0.3255	2.85		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
1.9	600	0.0117	5.16	82.54	Channel Flow,			
					Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040			
10.9	865	Total						

20849_PR HydroCAD Prepared by VHB, Inc

PROPOSED CONDITIONS CT-WILTON 24-hr S1 25-yr Rainfall=6.59" Printed 4/19/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 40



Subcatchment 3: Subcat 3

Summary for Pond 7P: Small Det Basin

Inflow Area =	1.243 ac, 7	1.89% Impervious, I	nflow Depth = 5.77" for 25-yr event				
Inflow =	8.45 cfs @	12.02 hrs, Volume=	0.597 af				
Outflow =	6.78 cfs @	12.06 hrs, Volume=	0.597 af, Atten= 20%, Lag= 2.4 min				
Discarded =	0.02 cfs @	2.64 hrs, Volume=	0.030 af				
Primary =	6.76 cfs @	12.06 hrs, Volume=	0.568 af				
Routed to Link DP1 : Norwalk River South							

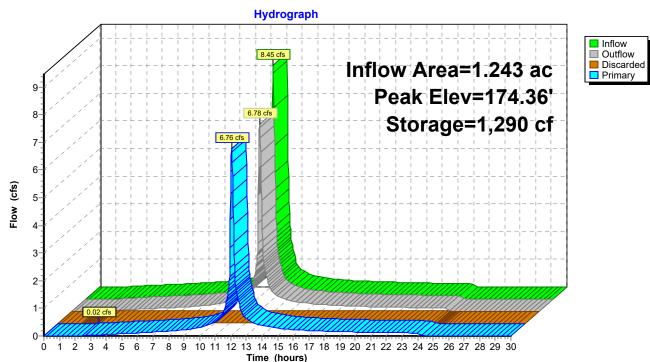
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 174.36' @ 12.06 hrs Surf.Area= 692 sf Storage= 1,290 cf

Plug-Flow detention time= 5.6 min calculated for 0.597 af (100% of inflow) Center-of-Mass det. time= 5.6 min (782.1 - 776.5)

Volume	Invei	t Avail.St	orage	Storage De	scription			
#1	172.50)' 1,	728 cf	StormTrap	Listed below	Inside #2		
#2	172.50)'	2 cf				below (Recalc)	
				1,730 cf Ov	erall - 1,728 c	of Embedded =	= 2 cf	
		1,	730 cf	Total Availa	able Storage			
Elevatio		um.Store						
(fee	-	uni.Store ibic-feet)						
	/ /	/						
172.5	-	0						
172.7	-	108						
173.2		216						
173.2	-	324						
173.5		525						
173.7	-	725						
174.0	-	926						
174.2		1,126						
174.5	-	1,327						
174.7		1,527						
175.0	0	1,728						
Elevatio	n S	Surf.Area	Inc	Store	Cum.Store			
(fee	t)	(sq-ft)	(cubi	c-feet)	(cubic-feet)			
172.5	i0	692		0	0			
175.0	-	692		1,730	1,730			
	•			.,	.,			
Device	Routing	Inver	t Outle	et Devices				
#1	Primary	172.50	' 15.0	" W x 9.0" H	Vert. Orifice	e/Grate C= 0.0	600	
	2		Limi	ted to weir fle	ow at low hea	ds		
#2	Primary	173.00	6.0"	W x 6.0" H	Vert. Orifice/	Grate C= 0.6	00	
	2		Limi	ted to weir fle	ow at low hea	ds		
#3	Discardeo	172.50	' 1.00	0 in/hr Exfil	tration over \$	Surface area	Phase-In= 0.01'	

Discarded OutFlow Max=0.02 cfs @ 2.64 hrs HW=172.53' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=6.74 cfs @ 12.06 hrs HW=174.36' (Free Discharge) -1=Orifice/Grate (Orifice Controls 5.48 cfs @ 5.84 fps) -2=Orifice/Grate (Orifice Controls 1.26 cfs @ 5.05 fps)



Pond 7P: Small Det Basin

Summary for Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

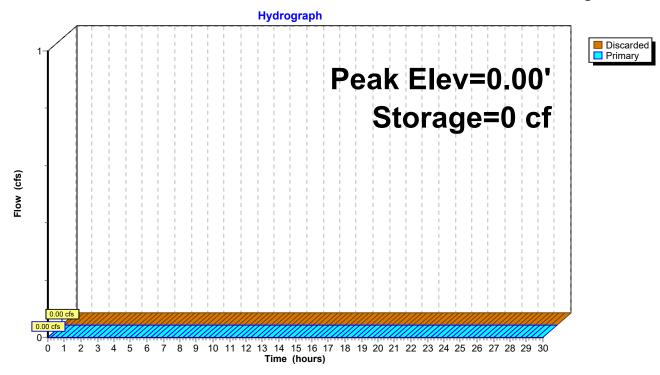
4' underground concrete chambers OFFLINE for 1" WQV retention. System on plan will show slightly smaller since we will be able to reuse the 350' portion of the existing 36" perforated pipe that is within the existing swale under existing mature vegetation.

Volume	Invert	Avail.Sto	rage Stora	age Description				
#1	170.80'	6,2	75 cf Storr	mTrapListed below Inside #2				
#2	170.80'			om Stage Data (Prismatic)Listed below (Recalc)				
			6,275	5 cf Overall - 6,275 cf Embedded = 0 cf				
		6,2	75 cf Total	Available Storage				
Elevatio	on Cur	n.Store						
(fee		pic-feet)						
170.8	80	0						
171.0		392						
171.3	80	785						
171.5	55	1,177						
171.8		1,906						
172.0		2,634						
172.3		3,362						
172.5		4,091						
172.8		4,819						
173.0		5,547						
173.3	50	6,275						
Elevatio		urf.Area	Inc.Store					
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)				
170.8		2,510	0	·				
173.3	80	2,510	6,275	6,275				
Device	Routing	Invert	Outlet Dev	vices				
#1	Discarded	170.80'	1.000 in/h	r Exfiltration over Horizontal area Phase-In= 0.01'				
#2	Primary	173.30'	6.0' long 2	x 0.5' breadth Broad-Crested Rectangular Weir				
	-		Head (feet	:) 0.20 0.40 0.60 0.80 1.00				
			Coef. (Eng	lish) 2.80 2.92 3.08 3.30 3.32				
 -								
	Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge)							

1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

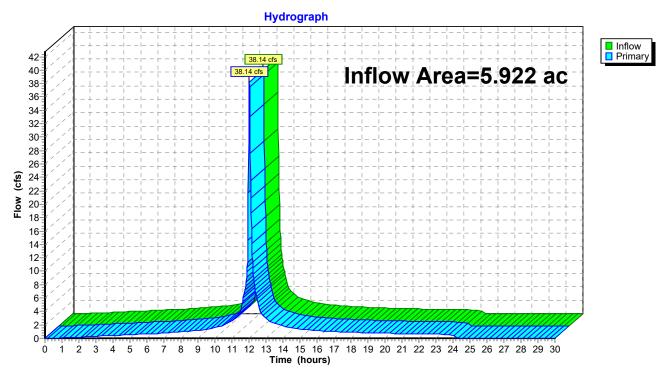
Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B



Summary for Link DP1: Norwalk River South

Inflow Are	ea =	5.922 ac, 76.57% Impervious, Inflow Depth = 5.82" for 25-yr event
Inflow	=	38.14 cfs @ 12.03 hrs, Volume= 2.872 af
Primary	=	38.14 cfs @ 12.03 hrs, Volume= 2.872 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

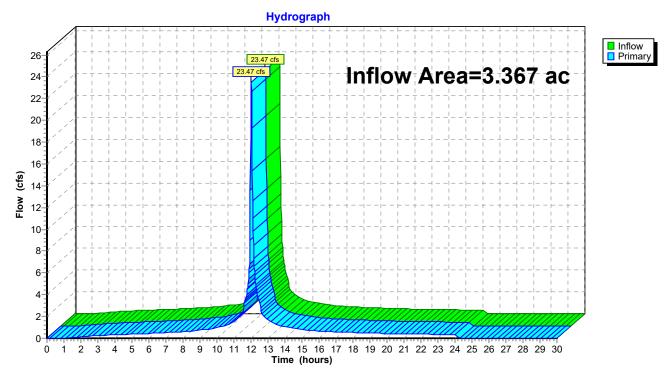


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Are	a =	3.367 ac, 85.61% Impervious, Inflow Depth = 6.12" for 25-yr event
Inflow	=	23.47 cfs @ 12.02 hrs, Volume= 1.716 af
Primary	=	23.47 cfs @ 12.02 hrs, Volume= 1.716 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

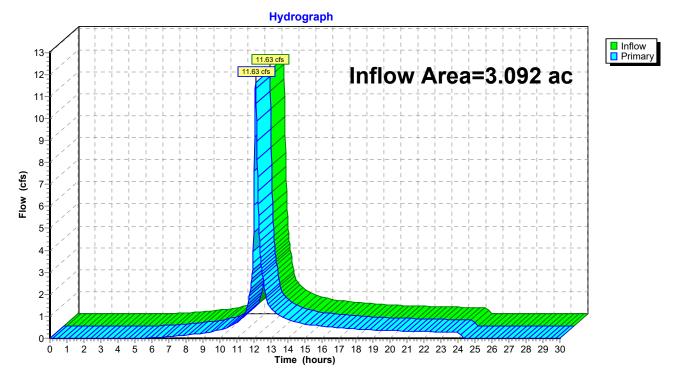


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse West

Inflow Are	a =	3.092 ac,	0.36% Impervious,	Inflow Depth = 4.0	0" for 25-yr event
Inflow	=	11.63 cfs @	12.10 hrs, Volume	e= 1.031 af	
Primary	=	11.63 cfs @	12.10 hrs, Volume	e= 1.031 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse West

Summary for Subcatchment 1a: Subcat 1a

Runoff = 10.63 cfs @ 12.02 hrs, Volume= Routed to Pond 7P : Small Det Basin 0.782 af, Depth= 7.55"

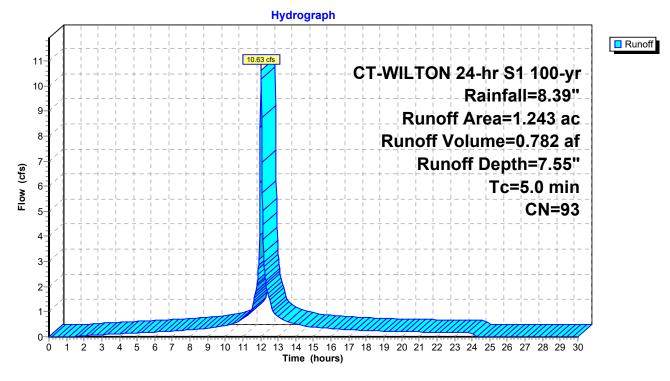
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Are	a (ac)	CN	Desc	Description						
	0.002	89	<50%	% Grass co	over, Poor,	, HSG D				
	0.348	80	>75%	% Grass co	over, Good,	d, HSG D				
	0.894	98	Unco	Unconnected pavement, HSG D						
	1.243	93	Weig	Weighted Average						
	0.349		28.1	28.11% Pervious Area						
0.894 71.89% Impervious Area										
	0.894		100.0	00% Unco	nnected					
Т	c Leng	th S	Slope	Velocity	Capacity	Description				
(min) (fee	et)	(ft/ft)	(ft/sec)	(cfs)					

5.0

Direct Entry,

Subcatchment 1a: Subcat 1a



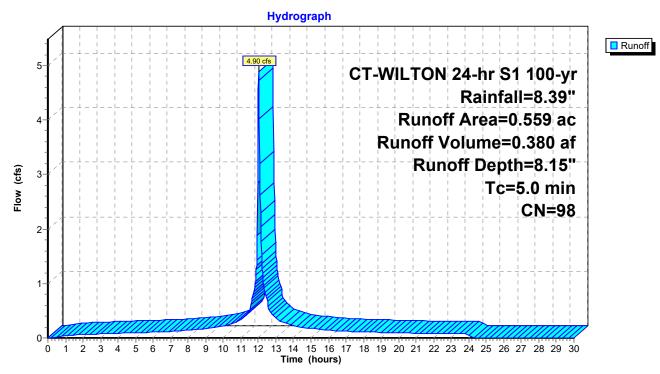
Summary for Subcatchment 1b: Subcat 1b

Runoff = 4.90 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South 0.380 af, Depth= 8.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

 Area	(ac)	CN	Desc	cription				
0.	000	80	>75%	6 Grass co	over, Good	, HSG D		
 0.	559	98	Unco	onnected p	avement, l	HSG D		
0.	559	98	Weig	hted Aver	age			
0.	000		0.01	% Perviou	s Ārea			
0.559 99.99% Impervious Area								
0.559 100.00% Unconnected								
-			~	N / N · · ·	O	D		
Tc	Lengt		Slope	Velocity	Capacity	Description		
 (min)	(feet	t)	(ft/ft)	(ft/sec)	(cfs)			
5.0						Direct Entry,		

Subcatchment 1b: Subcat 1b



Summary for Subcatchment 1c: Subcat 1c

Runoff = 25.02 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South

1.825 af, Depth= 7.43"

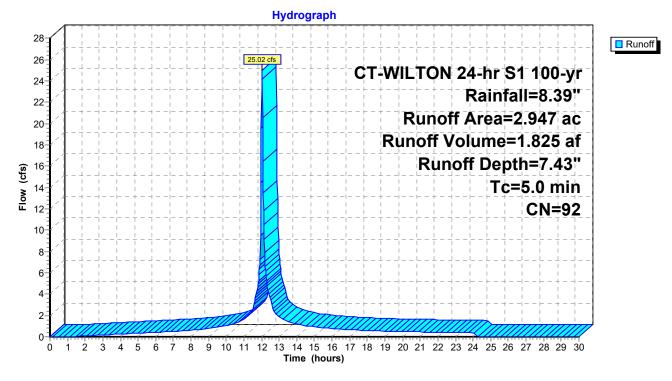
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

 Area (ac)	CN	Desc	cription			
0.914	80	>759	% Grass co	over, Good	1, HSG D	
1.910	98	Unco	onnected p	pavement, l	HSG D	
 0.123	79	Woo	ds/grass c	comb., Goo	od, HSG D	
 2.947	92	Weig	ghted Aver	age		
1.037		35.1	9% Pervio	us Area		
1.910		64.8	1% Imperv	/ious Area		
1.910		100.	00% Unco	nnected		
	ngth	Slope	Velocity	Capacity	Description	
(min) (fe	eet)	(ft/ft)	(ft/sec)	(cfs)		

5.0

Direct Entry,

Subcatchment 1c: Subcat 1c



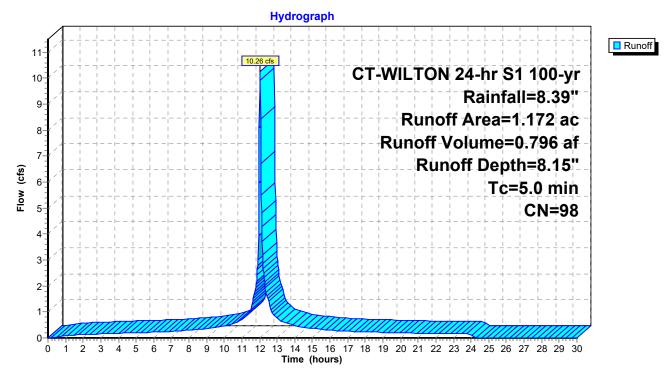
Summary for Subcatchment 1d: Subcat 1d

Runoff = 10.26 cfs @ 12.02 hrs, Volume= Routed to Link DP1 : Norwalk River South 0.796 af, Depth= 8.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area	(ac)	CN	Desc	cription		
0	.001	80	>75%	6 Grass co	over, Good	d, HSG D
1	.171	98	Unco	onnected p	pavement, l	HSG D
1	.172	98	Weig	hted Aver	age	
0	.001		0.05	% Perviou	s Area	
1.	1.171 99.95% Impervious Area				ious Area	
1.	1.171 100.00% Unconnected			00% Unco	nnected	
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0						Direct Entry,

Subcatchment 1d: Subcat 1d



Summary for Subcatchment 2: Subcat 2

Runoff = 29.29 cfs @ 12.02 hrs, Volume= Routed to Link DP2 : Norwalk River North 2.219 af, Depth= 7.91"

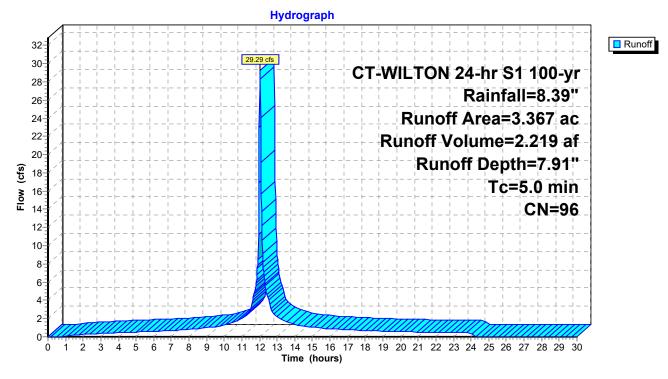
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area (ac)	CN	Description
0.254	89	<50% Grass cover, Poor, HSG D
0.231	80	>75% Grass cover, Good, HSG D
2.882	98	Unconnected pavement, HSG D
3.367	96	Weighted Average
0.485		14.39% Pervious Area
2.882		85.61% Impervious Area
2.882		100.00% Unconnected
Tc Ler	ngth S	Slope Velocity Capacity Description
(min) (f	eet)	(ft/ft) (ft/sec) (cfs)

5.0

Direct Entry,

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 15.90 cfs @ 12.10 hrs, Volume= 1.452 af, Depth= 5.63" Routed to Link DP3 : Watercourse West

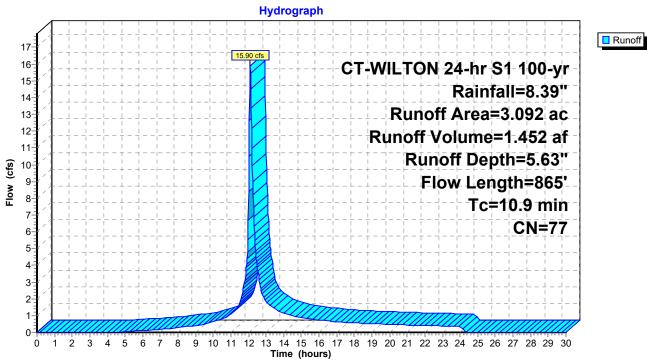
t

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs CT-WILTON 24-hr S1 100-yr Rainfall=8.39"

Area (a	c) C	N Des	cription						
0.02	28 8	9 <50	% Grass c	over, Poor,	HSG D				
0.13	35 8	so >75	5% Grass cover, Good, HSG D						
0.01	11 9			pavement, l	HSG D				
2.91	18 7	'7 Woo	ods, Good,	HSG D					
3.09	92 7	7 Wei	ghted Aver	rage					
3.08	31	99.6	4% Pervio	us Area					
0.01		0.36	% Impervi	ous Area					
0.01	11	100.	00% Uncc	onnected					
Tal	onath	Clana	Valacity	Canaaitu	Description				
	_ength	Slope	Velocity (ft/sec)	Capacity	Description				
(min)	(feet)	<u>(ft/ft)</u>		(cfs)					
7.7	50	0.2300	0.11		Sheet Flow,				
1.0	045	0 0055	0.05		Woods: Dense underbrush n= 0.800 P2= 3.55"				
1.3	215	0.3255	2.85		Shallow Concentrated Flow,				
1.0	600	0 0 4 4 7	E 40	00 54	Woodland Kv= 5.0 fps				
1.9	600	0.0117	5.16	82.54	Channel Flow,				
	0.05	T ()			Area= 16.0 sf Perim= 11.0' r= 1.45' n= 0.040				
10.9	865	Total							

20849_PR HydroCAD Prepared by VHB, Inc

PROPOSED CONDITIONS CT-WILTON 24-hr S1 100-yr Rainfall=8.39" Printed 4/19/2024 HydroCAD® 10.20-3c s/n 01038 © 2023 HydroCAD Software Solutions LLC Page 54



Subcatchment 3: Subcat 3

Summary for Pond 7P: Small Det Basin

Inflow Area =	1.243 ac, 7	1.89% Impervious, Infl	ow Depth = 7.55" for 100-yr event				
Inflow =	10.63 cfs @	12.02 hrs, Volume=	0.782 af				
Outflow =	8.14 cfs @	12.07 hrs, Volume=	0.782 af, Atten= 23%, Lag= 2.6 min				
Discarded =	0.02 cfs @	1.96 hrs, Volume=	0.030 af				
Primary =	8.13 cfs @	12.07 hrs, Volume=	0.752 af				
Routed to Link DP1 : Norwalk River South							

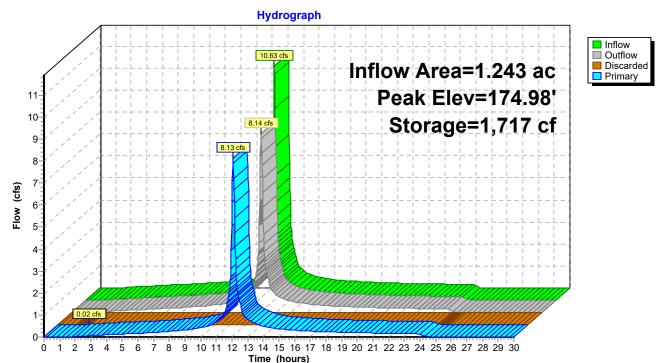
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 174.98' @ 12.07 hrs Surf.Area= 692 sf Storage= 1,717 cf

Plug-Flow detention time= 5.3 min calculated for 0.782 af (100% of inflow) Center-of-Mass det. time= 5.3 min (774.2 - 768.9)

Volume	Inver	t Avail.Sto	orage \$	Storage Description
#1	172.50)' 1,7	28 cf	StormTrapListed below Inside #2
#2	172.50)'		Custom Stage Data (Prismatic)Listed below (Recalc)
				1,730 cf Overall - 1,728 cf Embedded = 2 cf
		1,7	30 cf	Total Available Storage
	~	0.		
Elevatio	-	um.Store		
(fee		ibic-feet)		
172.5	-	0		
172.7	-	108		
173.2		216		
173.2	-	324		
173.5		525		
173.7	-	725		
174.0	-	926		
174.2		1,126		
174.5	-	1,327		
174.7		1,527		
175.0	0	1,728		
Elevatio	n S	Surf.Area	Inc.§	Store Cum.Store
(fee		(sq-ft)	(cubic-	-
172.5	1	692		
175.0	-	692	1	1,730 1,730
110.0	•	002		1,100
Device	Routing	Invert	Outlet	t Devices
#1	Primary	172.50'	15.0"	W x 9.0" H Vert. Orifice/Grate C= 0.600
	,		Limite	ed to weir flow at low heads
#2	Primary	173.00'	6.0" V	W x 6.0" H Vert. Orifice/Grate C= 0.600
	,		Limite	ed to weir flow at low heads
#3	Discardeo	172.50'	1.000	in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.02 cfs @ 1.96 hrs HW=172.53' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=8.08 cfs @ 12.07 hrs HW=174.96' (Free Discharge) -1=Orifice/Grate (Orifice Controls 6.51 cfs @ 6.94 fps) -2=Orifice/Grate (Orifice Controls 1.57 cfs @ 6.29 fps)



Pond 7P: Small Det Basin

Summary for Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B

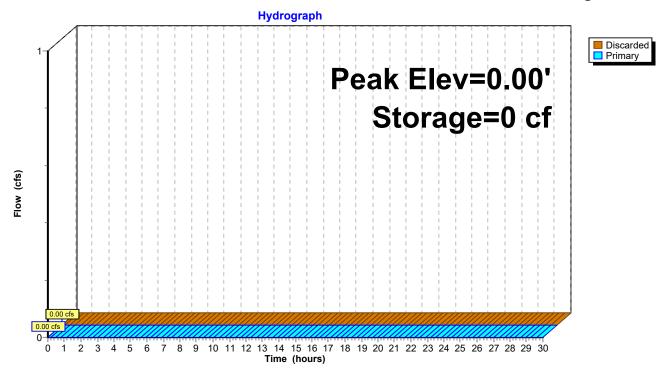
4' underground concrete chambers OFFLINE for 1" WQV retention. System on plan will show slightly smaller since we will be able to reuse the 350' portion of the existing 36" perforated pipe that is within the existing swale under existing mature vegetation.

Volume	Invert	Avail.Sto	rage Stora	age Description					
#1	170.80'	6,2	75 cf Storr	mTrapListed below Inside #2					
#2	170.80'								
			6,275	6,275 cf Overall - 6,275 cf Embedded = 0 cf					
		6,2	75 cf Total	Available Storage					
Elevatio	on Cur	n.Store							
(fee		pic-feet)							
170.8	80	0							
171.0		392							
171.3	80	785							
171.5	55	1,177							
171.8		1,906							
172.0		2,634							
172.3		3,362							
172.5		4,091							
172.8		4,819							
173.0		5,547							
173.3	50	6,275							
Elevatio		urf.Area	Inc.Store						
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)					
170.8		2,510	0	•					
173.3	80	2,510	6,275	6,275					
Device	Routing	Invert	Outlet Dev	vices					
#1	Discarded	170.80'	1.000 in/h	r Exfiltration over Horizontal area Phase-In= 0.01'					
#2	Primary	173.30'	6.0' long 2	x 0.5' breadth Broad-Crested Rectangular Weir					
	-		Head (feet	i) 0.20 0.40 0.60 0.80 1.00					
			Coef. (Eng	glish) 2.80 2.92 3.08 3.30 3.32					
			·						
	Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge)								

1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=0.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

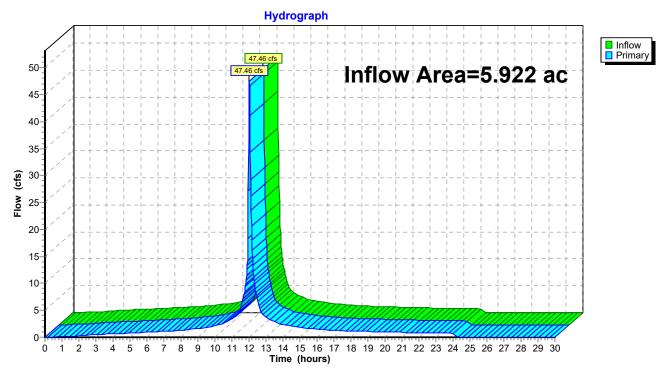
Pond 10P: OFFLINE RETENTION SYSTEM - UG Chambers - Building A&B



Summary for Link DP1: Norwalk River South

Inflow Are	a =	5.922 ac, 76.57% Impervious, Inflow Depth = 7.60" for 100-yr event
Inflow	=	47.46 cfs @ 12.03 hrs, Volume= 3.753 af
Primary	=	47.46 cfs @ 12.03 hrs, Volume= 3.753 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

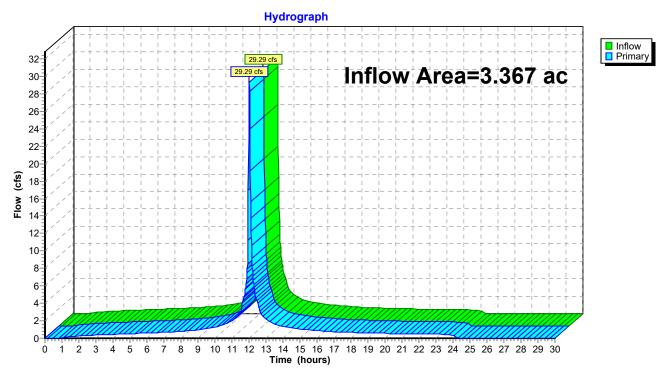


Link DP1: Norwalk River South

Summary for Link DP2: Norwalk River North

Inflow Area =		3.367 ac, 85.61% Impervious, Inflow Depth = 7.91" for 100-yr event
Inflow	=	29.29 cfs @ 12.02 hrs, Volume= 2.219 af
Primary	=	29.29 cfs @ 12.02 hrs, Volume= 2.219 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs

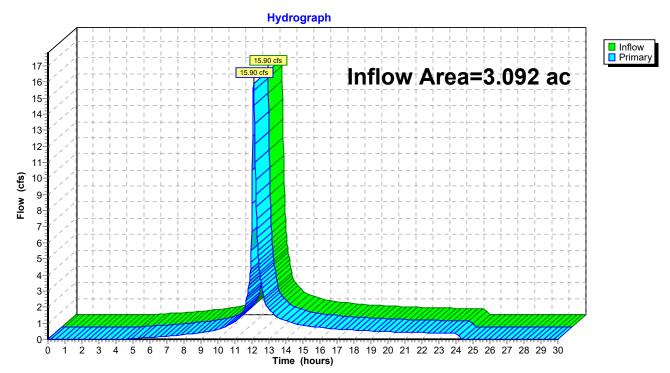


Link DP2: Norwalk River North

Summary for Link DP3: Watercourse West

Inflow Area =		3.092 ac,	0.36% Impervious,	Inflow Depth = 5	5.63" for 100-yr event
Inflow	=	15.90 cfs @	12.10 hrs, Volume	= 1.452 at	f
Primary	=	15.90 cfs @	12.10 hrs, Volume	e= 1.452 at	f, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs



Link DP3: Watercourse West