Peak Engineers, LLC

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August 31, 2023 Revised November 17, 2023

Frank Smeriglio, P.E.
Department of Public Works
Town of Wilton
Town Hall Annex
238 Danbury Road
Wilton, CT 06897

Re: 53 Sugar Loaf Drive, SDP #6-23

Robert Lupinski 53 Sugar Loaf Drive

Wilton, CT

Proposed Grading New Construction

Drainage Narrative

Dear Mr. Smeriglio:

This Drainage Narrative has been prepared to address comment No. 3 of your Memorandum to assistant town planner D. White on July 24, 2023. Comment No. 3. States:

Design engineer shall evaluate and submit calculations for pre-construction versus post construction storm runoff, as well as storm runoff generated during the construction phase of the project.

This project proposes the de-construction of a retaining wall along the north, west and south sides of the property and earthwork to regrade portions of the site.

This Drainage Narrative will describe the site and make comparisons to the post-construction (post-activity) site conditions and the pre-construction site condition. In April 2011 an application was submitted to the Planning and Zoning Commission for proposed grading on the site. Applications materials included an existing topo plan. Peak has utilized that 2011 plan as the pre-construction (pre-activity) site conditions for this report. On or about this time, 2011, Town agencies granted permission to add square

footage to the building increasing the roof area to 3,264 square feet and the gravel driveway area to 3,887 square feet.

Pre-Activity Condition

The entire site is approximately 1.0012 acres of residential property located on the west side of Sugar Loaf Drive. The entire property slopes to the west.

The State of Ct Web Soil Survey reveals that the majority of the site is Canton and Charlton fine sandy loams 8-15%. The western edge of the property is Charlton-Chatfield complex, 15-45% slopes. The flattest slopes are on the eastern property edge near the road. Please see the attached CT Web Soil report. The Hydrologic soil grouping corresponds with the slope of the land with the majority of the flatter slopes being Hydraulic Group B, mid-range slopes C and the steep western edge E.

Some of the property border areas are wooded.

The pre-activity house roof area is 2,168 square feet and the gravel driveway is 1,450 square feet.

The vast majority of the pre-activity site includes slopes exceeding 8% and the western edge exceeds 20%. Please see the attached plan titled 2011 Contour Sketch plan, Slope Study, G1.

Deep soil testing, performed for a septic replacement area in 2011, reveal soils described as red brown fine sandy loams to 24" underlain with grey fine to medium sands to 72", and some broken rock was encountered from 3-6' depth. The soil percolation rate is 1"/10 minutes.

Current Site Conditions

On November 9, 2023, Peak Engineers, LLC performed deep soil testing and deep percolation testing for the design of a storm water infiltration system. The testing was performed in the northeast corner of the property.

Based on the soil testing the area has been worked and is described as:

0-6" of topsoil

6-30" moderately compact fill, silty brown fine sandy loam 30-62" bright red brown fine sandy loam, some broken rock 62-78" red brown fine sandy loam, lenses of tan sand Roots to 60".

A percolation test was performed at 47", in the original red brown fine sandy loam. The test percolation rate is 1"/11.4 minutes.

The dwelling does not have any gutters, allowing water to drip to the building edge. The builder waterproofed the foundation walls and placed gravel against the walls with a footing drain. There is approximately 12" of topsoil above the gravel. Water from the roof drips and is absorbed in the topsoil and makes its way through the gravel to the footing drain pipe. The drains run to the northwest corner of the building. Until recently these pipes were connected and exited the retaining wall located on the western property line. The builder cut and capped the terminal pipe on November 8, 2023, at the building, effectively abandoning the discharge pipe.

Post-Activity Condition

This project proposes to deconstruct the wall, grade slopes down to the wall, meeting town zoning regulations and then provide flat areas west and north of the house for living areas. Please see plan titled 2023 Proposed Contour Sketch Plan, Slope Study, G2, revised November 17, 2023. This plan demonstrates that the proposed grading will alter existing steep slopes north and west of the house and transform areas to living spaces with slopes of between 3 and 6%. These large flatter areas are effective in allowing water to infiltrate the ground.

Methodology and Calculations

Utilizing Technical Release 55 runoff curve numbers and HydroCad Storm water program we have calculated the Pre-Activity and Post-Activity peak design flows for the proposed improvements to the design Node. We utilized the CTDOT Engineering Bulletin EB-2015-2 Precipitation Frequency Estimates and the NOAA precipitation frequency data server interactive map to determine the precipitation frequency estimates. The design storm is the 25-year storm generating 6.63 inches of rain in a 24-hour period. Please see the attached page.

Proposed Drainage Facilities

The footing drain pipes will discharge into a sump pump pit at the northwest corner of the building. The HydroCad Software program has been utilized to size a gallery and stone infiltration system which will effectively store the water and then promote infiltration of the collected water from the roof. The calculations indicate that during the 25-year design storm the system will not overflow. A yard drain is proposed to allow the less frequent larger storms to overflow onto the upper lawn area.

Please see sheet 3 and 4 for a Summary of HydroCad output peak rate of flows and volumes generated by the sites 25 year design storm of 6.63" in a period or 24 hours.

Nada	Pre-Activity Volume	Post-Activity Volume	Change Volume	% Change
Node	15,090 CF	11,475 CF	-3615 CF	-24%
Node	Pre-Activity Flow, CFS	Post-Activity Flow CFS	Change CFS	% Change
node	4.53	2.69	-1.84 cfs	-40.6%

Design Considerations and Best Management Practices

The storm water management plan proposes to minimize the impacts of the roof water and driveway water by utilizing systems of best management practices to handle the sites storm water. The components of the system are described below.

- 1. BMP-no point discharge. The building will not have gutters. Through a series of facilities the roof water will enter an infiltration system.
- 2. BMP-disconnected impervious areas. Roof, driveway and other hard surfaces flow onto lawn area.
- 3. BMP-recharge soils. The site proposes a gravel driveway allowing water from minor storms to infiltrate the soils.
- 4. BMP- promote groundwater infiltration. Subsequent to 2011, grading was performed to dramatically flatten the sites slopes, especially in the large lawn area to the north of the house and to the west of the house. This grading allows water to infiltrate soils and decreases the time of concentration to the property line.
- 5. BMP-reduce erosion potential. The finished slope embankment includes a reverse bench mid-way down the slope. Reverse benches are effective in decreasing water flow velocity and limiting potential for erosion.

Construction Methodology to Mitigate Runoff During Construction.

The Site Development Plan-2 (LP.2), prepared by Environmental Land Solutions, includes a row of silt fence along the entire property width and a second row of silt fence inside the site. The location of this fence will prevent upstream water from entering the construction zone and dramatically reduce the chance of sediment transport. During the work, a swale will be constructed at the lowest limit of the work. This swale will act as a

landing point for the boulders as they are taken off the wall and the swale will also act as a temporary water and sediment storage area. Please see Cross Section B-B on plan LP.2.

Conclusions

This project proposes a regrading of the site. When compared to the 2011 preconstruction site the post-construction site will have many areas of flatter gentler slopes that will allow water to infiltrate soils and slow water down as it crosses the site. The HydroCad study confirms that the site grading will effectivity decrease the peak rate of flow and peak volume of flow from the site.

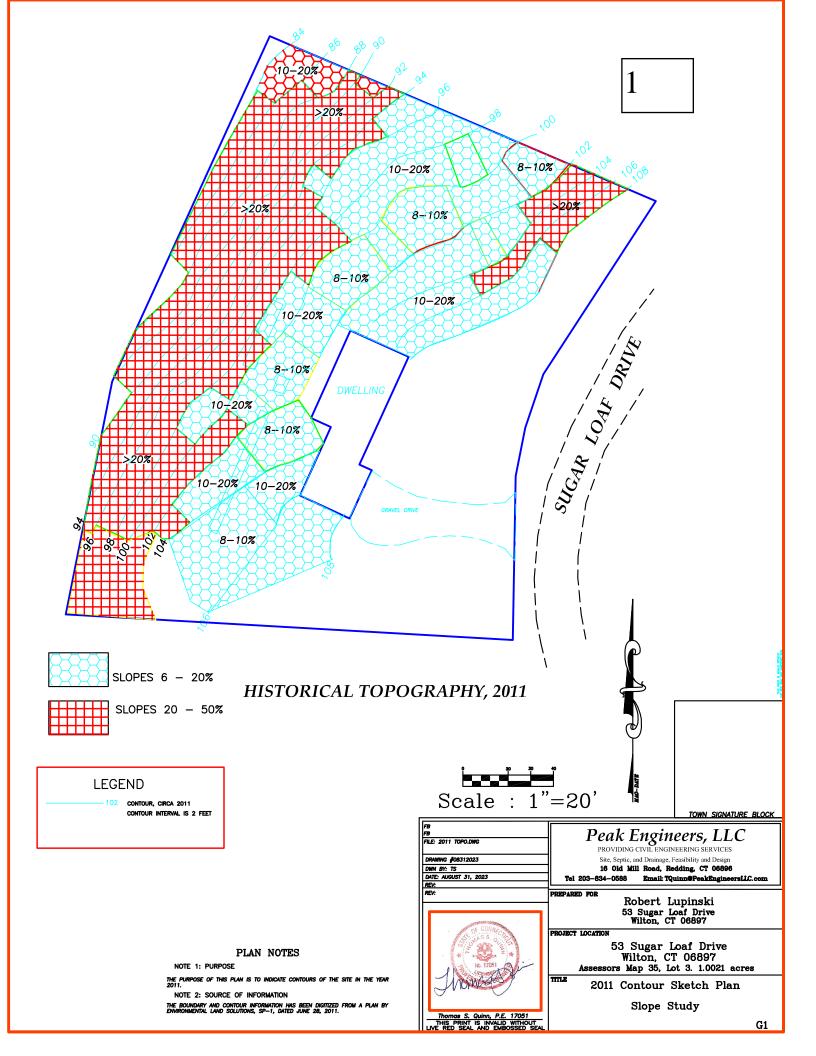
It is the opinion of Peak Engineers, LLC that the site can be developed in a manner that will not increase the design flow rate (25-year storm) or design flow volume from the property and will not generate drainage that will adversely impact the adjoining or downstream properties. The proposed grading will be performed in a manner that will not alter the existing drainage patterns.

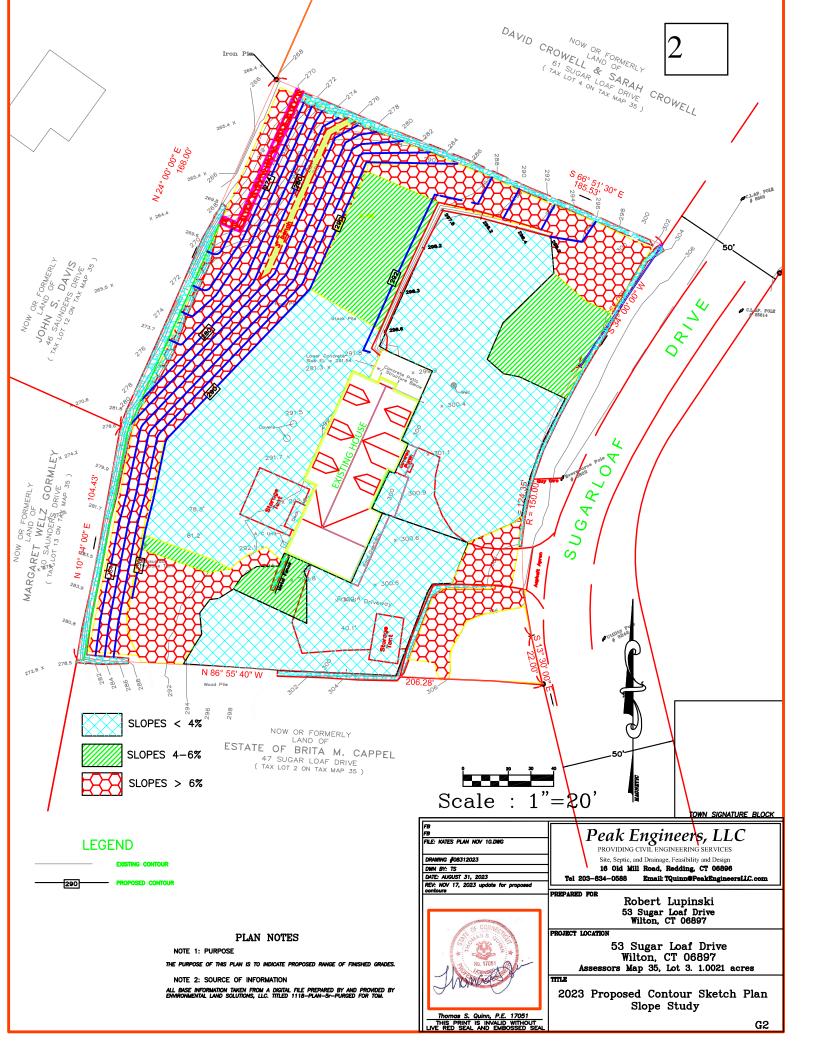
The proper installation of temporary and well as permanent sediment and erosion controls, following the 2002 Connecticut Erosion and Sediment Guidelines, will help reduce the effects of the construction on the downstream properties. Peak Engineers, LLC recommends that a site monitor be required to perform weekly site observations as well as review immediately prior to an expected rain event.

Respectfully submitted,



For Peak Engineers, LLC, Thomas S. Quinn, P.E.





PRE-ACTIVITY

Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

Printed 9/11/2023

Prepared by Peak Engineers, LLC

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Events for Link 2: WEST PROPERTY LINE

Ever	nt Inflow	Primary	Volume	Elevation
	(cfs)	(cfs)	(cubic-feet)	(feet)
2 YR WILTON NOA	A 1.69	1.69	5,724	0.00
10 year WILTON NOA	A 3.40	3.40	11,315	0.00
25 year WILTON NOA	A 4.53	4.53	15,090	0.00

POST-ACTIVITY

Type III 24-hr 25 year WILTON NOAA Rainfall=6.63" Printed 11/21/2023

Prepared by Peak Engineers, LLC

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Events for Link 5: WEST PROPERTY LINE

Event	Inflow	Primary	Volume	Elevation
	(cfs)	(cfs)	(cubic-feet)	(feet)
2 YR WILTON NOAA	0.84	0.84	3,779	0.00
10 year WILTON NOAA	1.93	1.93	8,299	0.00
25 year WILTON NOAA	2.69	2.69	11,475	0.00



NOAA Atlas 14, Volume 10, Version 3 Location name: Wilton, Connecticut, USA* Latitude: 41.2225°, Longitude: -73.4311° Elevation: 294 ft** * source: ESRI Maps ** source: USGS





POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PD5-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									
Duration					recurrence					
	1	2	5	10	25	50	100	200	500	1000
5-min	0.362 (0.278-0.464)	0.423 (0.324-0.542)	0.522 (0.399-0.670)	0.604 (0.459-0.779)	0.717 (0.529-0.955)	0.803 (0.580-1.09)	0.891 (0.625-1.24)	0.985 (0.661-1.40)	1.12 (0.723-1.63)	1.22 (0.771-1.82
10-min	0.513 (0.394-0.657)	0.599 (0.459-0.767)	0.739 (0.565-0.950)	0.856 (0.651-1.10)	1.02 (0.749-1.35)	1.14 (0.822-1.54)	1.26 (0.886-1.76)	1.40 (0.937-1.99)	1.58 (1.02-2.31)	1.72 (1.09-2.57
15-min	0.604 (0.464-0.773)	0.705 (0.541-0.903)	0.870 (0.665-1.12)	1.01 (0.766-1.30)	1.20 (0.881-1.59)	1.34 (0.967-1.81)	1.48 (1.04-2.07)	1.64 (1.10-2.34)	1.86 (1.20-2.72)	2.03 (1.28-3.02
30-min	0.846 (0.650-1.08)	0.985 (0.755-1.26)	1.21 (0.927-1.56)	1.40 (1.06-1.81)	1.66 (1.22-2.21)	1.86 (1.34-2.51)	2.06 (1.44-2.85)	2.26 (1.52-3.22)	2.54 (1.64-3.72)	2.75 (1.74-4.10
60-min	1.09 (0.836-1.39)	1.26 (0.970-1.62)	1.55 (1.19-2.00)	1.79 (1.36-2.31)	2.12 (1.56-2.82)	2.38 (1.71-3.20)	2.63 (1.84-3.64)	2.88 (1.94-4.11)	3.22 (2.09-4.72)	3.48 (2.20-5.18
2-hr	1.40 (1.08-1.78)	1.65 (1.27-2.09)	2.05 (1.57-2.61)	2.38 (1.82-3.05)	2.84 (2.10-3.76)	3.18 (2.32-4.29)	3.54 (2.50-4.92)	3.94 (2.65-5.57)	4.50 (2.92-6.55)	4.94 (3.14-7.32
3-hr	1.61 (1.25-2.04)	1.90 (1.47-2.42)	2.39 (1.84-3.03)	2.78 (2.14-3.56)	3.33 (2.48-4.41)	3.75 (2.74-5.04)	4.18 (2.97-5.81)	4.67 (3.15-6.59)	5.38 (3.50-7.81)	5.97 (3.80-8.81
6-hr	2.02 (1.58-2.55)	2.42 (1.88-3.04)	3.05 (2.37-3.86)	3.58 (2.76-4.54)	4.31 (3.23-5.68)	4.86 (3.57-6.51)	5.43 (3.89-7.53)	6.11 (4.13-8.56)	7.10 (4.63-10.2)	7.93 (5.06-11.6
12-hr	2.50 (1.96-3.12)	3.00 (2.35-3.75)	3.82 (2.98-4.79)	4.50 (3.49-5.67)	5.43 (4.09-7.11)	6.13 (4.53-8.17)	6.88 (4.95-9.47)	7.74 (5.26-10.8)	9.03 (5.91-12.9)	10.1 (6.46-14.7
24-hr	2.94 (2.31-3.64)	3.57 (2.81-4.43)	4.60 (3.61-5.73)	5.45 (4.26-6.82)	6.63 (5.02-8.63)	7.51 (5.58-9.96)	8.45 (6.12-11.6)	9.56 (6.52-13.2)	11.2 (7.37-16.0)	12.6 (8.12-18.3
2-day	3.30 (2.62-4.07)	4.08 (3.23-5.03)	5.34 (4.22-6.61)	6.39 (5.02-7.94)	7.83 (5.98-10.2)	8.90 (6.67-11.8)	10.1 (7.36-13.8)	11.5 (7.85-15.8)	13.7 (8.99-19.3)	15.5 (10.0-22.3
3-day	3.58 (2.85-4.40)	4.43 (3.52-5.45)	5.82 (4.61-7.17)	6.97 (5.49-8.63)	8.56 (6.55-11.1)	9.73 (7.31-12.8)	11.0 (8.08-15.0)	12.6 (8.62-17.2)	15.0 (9.88-21.1)	17.1 (11.0-24.4
4-day	3.85 (3.07-4.71)	4.74 (3.78-5.82)	6.21 (4.93-7.64)	7.43 (5.87-9.17)	9.11 (6.98-11.7)	10.3 (7.79-13.6)	11.7 (8.59-15.9)	13.3 (9.16-18.2)	15.9 (10.5-22.3)	18.0 (11.7-25.7
7-day	4.61 (3.69-5.61)	5.59 (4.48-6.81)	7.20 (5.74-8.80)	8.53 (6.77-10.5)	10.4 (7.97-13.2)	11.7 (8.85-15.3)	13.2 (9.70-17.8)	14.9 (10.3-20.3)	17.6 (11.6-24.5)	19.8 (12.8-28.1
10-day	5.35 (4.30-6.49)	6.39 (5.13-7.76)	8.09 (6.47-9.85)	9.49 (7.55-11.6)	11.4 (8.81-14.5)	12.9 (9.72-16.7)	14.4 (10.6-19.3)	16.2 (11.2-21.9)	18.8 (12.5-26.2)	21.0 (13.6-29.7
20-day	7.58 (6.13-9.14)	8.75 (7.07-10.6)	10.7 (8.58-12.9)	12.2 (9.79-14.9)	14.4 (11.1-18.1)	16.1 (12.1-20.5)	17.8 (13.0-23.3)	19.6 (13.6-26.3)	22.2 (14.8-30.6)	24.2 (15.7-33.9
30-day	9.42 (7.65-11.3)	10.7 (8.66-12.8)	12.7 (10.3-15.3)	14.4 (11.6-17.5)	16.8 (13.0-20.9)	18.6 (14.1-23.5)	20.4 (14.9-26.5)	22.3 (15.5-29.7)	24.7 (16.6-34.0)	26.6 (17.4-37.2
45-day	11.7 (9.52-14.0)	13.0 (10.6-15.6)	15.3 (12.4-18.3)	17.1 (13.8-20.6)	19.7 (15.3-24.3)	21.6 (16.4-27.2)	23.6 (17.2-30.3)	25.5 (17.8-33.8)	27.9 (18.7-38.2)	29.7 (19.4-41.4
60-day	13.6 (11.1-16.2)	15.0 (12.2-17.9)	17.4 (14.1-20.8)	19.3 (15.6-23.2)	22.0 (17.1-27.2)	24.1 (18.3-30.2)	26.2 (19.1-33.5)	28.1 (19.7-37.2)	30.6 (20.6-41.6)	32.3 (21.1-44.8

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical



MAP LEGEND

US Routes Stony Spot Wet Spot Other Rails **Water Features Fransportation** W 8 ŧ Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Closed Depression Special Point Features Borrow Pit Clay Spot **Gravel Pit** Area of Interest (AOI) Blowout Soils

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator distance and area. A projection that preserves area, such as the projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Survey Area Data: Version 22, Sep 12, 2022 State of Connecticut Soil Survey Area:

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Oct 21, 2022—Oct

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

> Slide or Slip Sodic Spot

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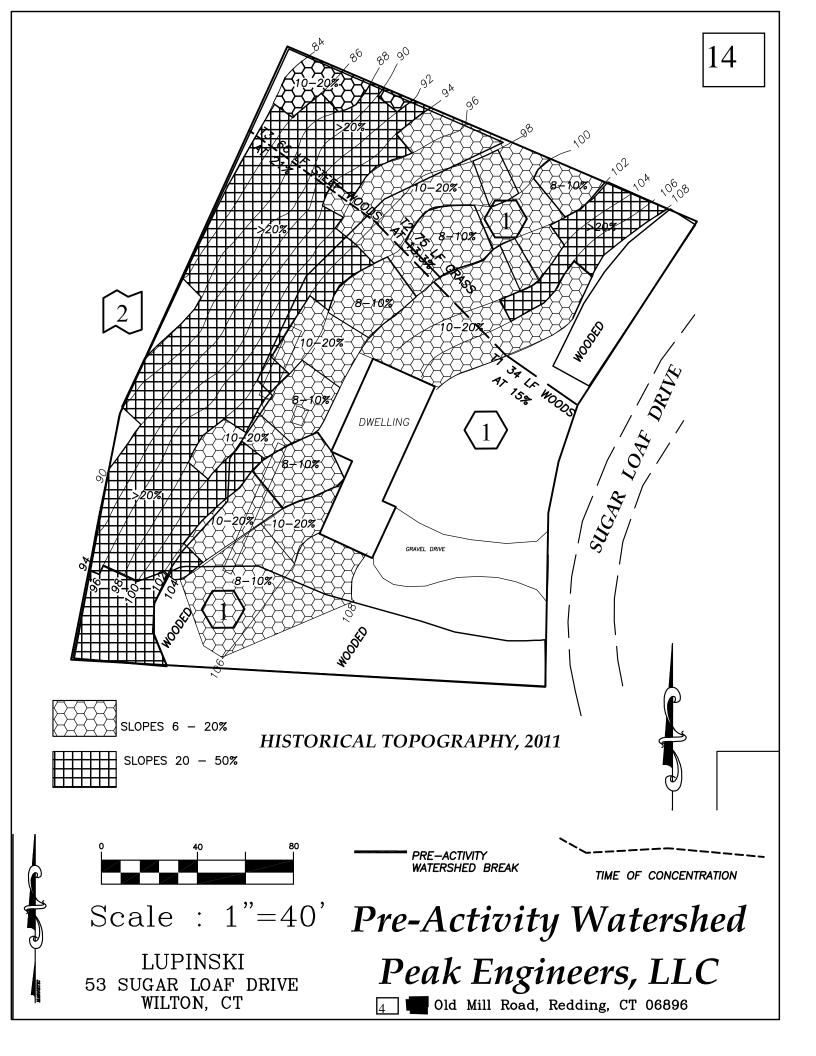
USDA

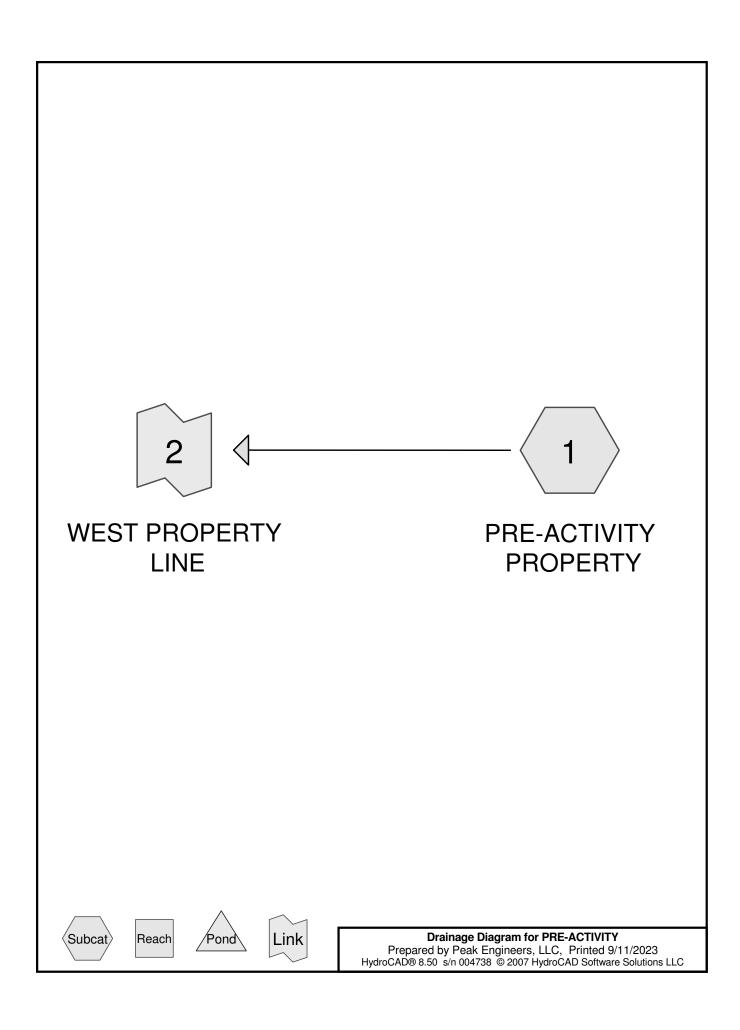
Soil Map—State of Connecticut 53 Sugar Loaf Drive Wilton

8

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes	0.0	2.1%
60C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes	0.9	86.0%
73E	Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky	0.1	11.9%
Totals for Area of Interest	'	1.0	100.0%





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Summary for Subcatchment 1: PRE-ACTIVITY PROPERTY

Runoff = 4.53 cfs @ 12.11 hrs, Volume= 15,090 cf, Depth= 4.15"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

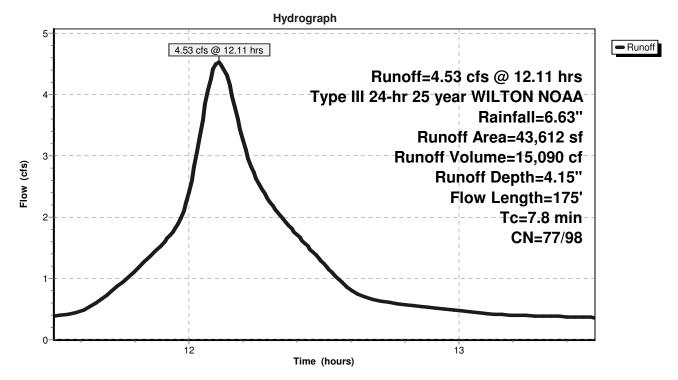
	Area (sf)	CN	Description		
*	2,168	98	HOUSE RC	OF	
*	1,450	85	Driveway gr	ravel	
	20,744	74	>75% Grass	cover, Goo	od, HSG C
	6,540	70	Woods, Goo	od, HSG C	
	12,710	83	Woods, Poo	r, HSG D	
	43,612	78	Weighted A	verage	
	41,444	77	Pervious Ar	ea	
	2,168	98	Impervious	Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.8	34	0.1500	0.15		Sheet Flow, sheet lightwoods
					Woods: Light underbrush $n=0.400$ P2= 3.57"
3.5	75	0.1330	0.36		Sheet Flow, sheet flow over grass
					Grass: Short n= 0.150 P2= 3.57"
0.5	66	0.2100	2.29		Shallow Concentrated Flow, shall conc woods
					Woodland Kv= 5.0 fps
7.8	175	Total			

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Subcatchment 1: PRE-ACTIVITY PROPERTY



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Summary for Link 2: WEST PROPERTY LINE

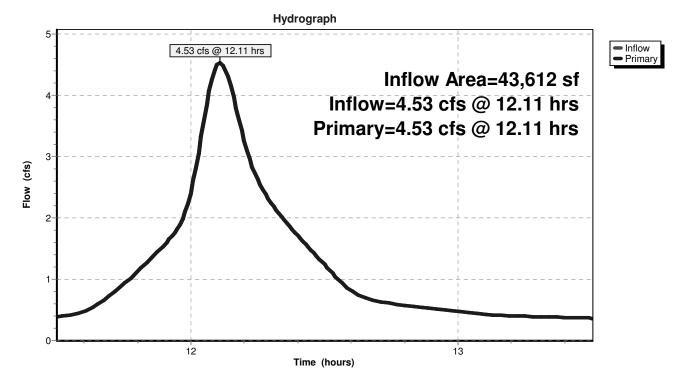
Inflow Area = 43,612 sf, 4.97% Impervious, Inflow Depth = 4.15" for 25 year WILTON NOAA e

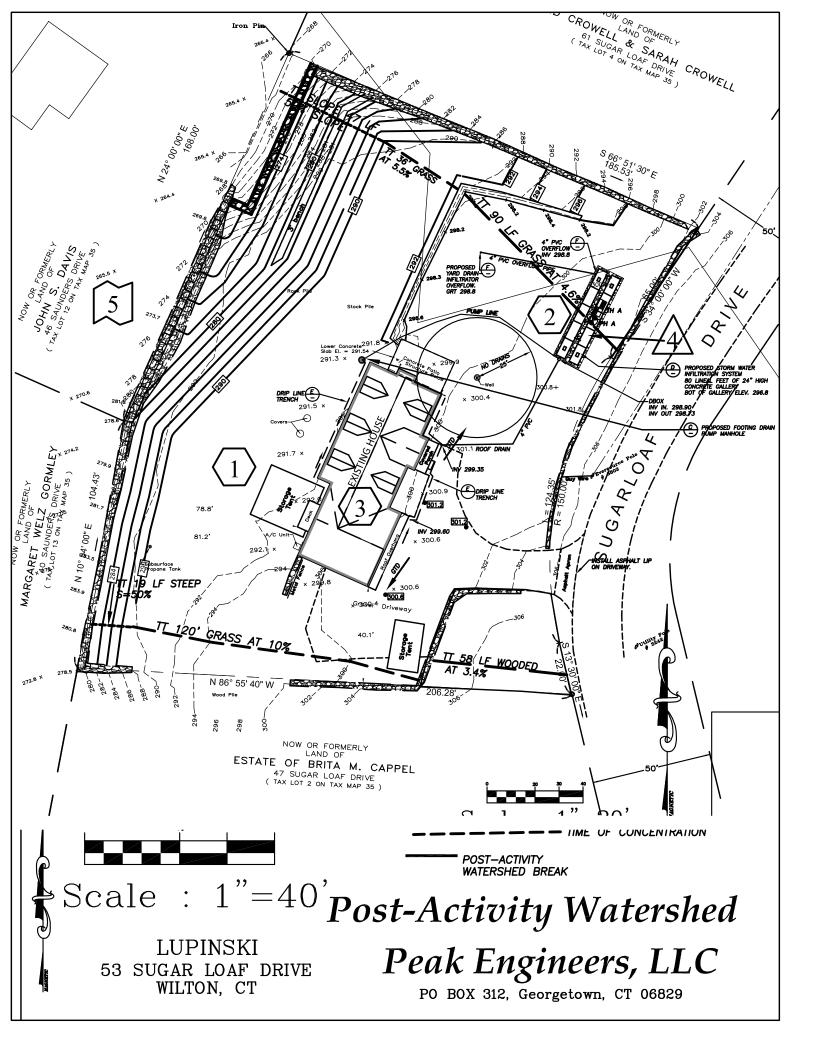
Inflow = 4.53 cfs @ 12.11 hrs, Volume= 15,090 cf

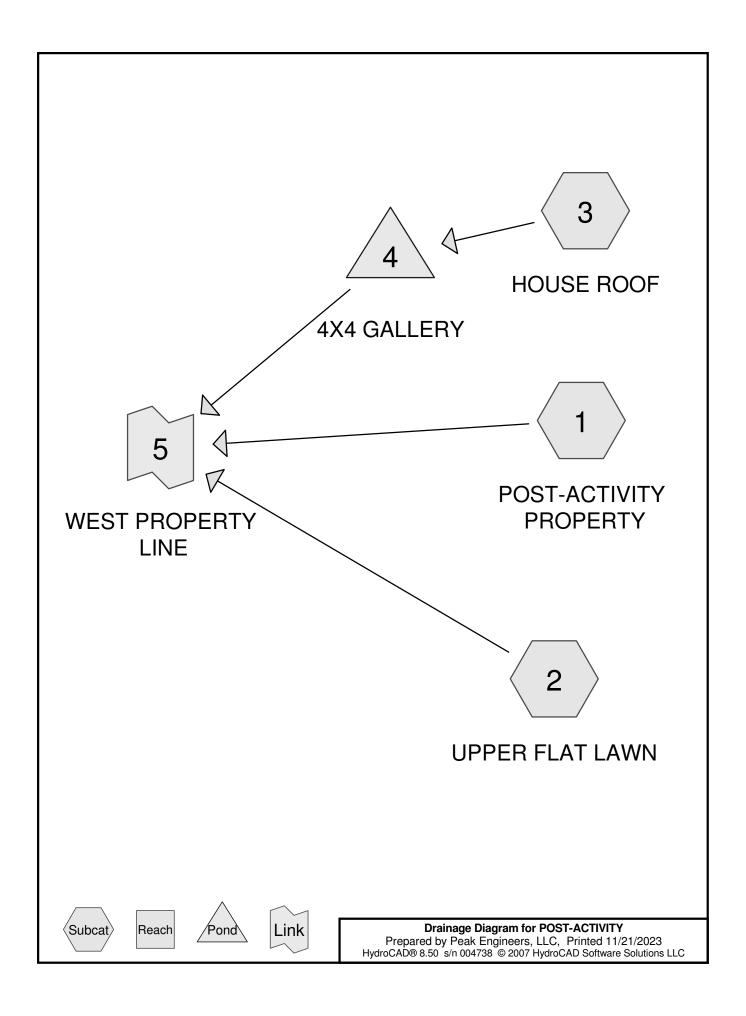
Primary = 4.53 cfs @ 12.11 hrs, Volume= 15,090 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs

Link 2: WEST PROPERTY LINE







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Summary for Subcatchment 1: POST-ACTIVITY PROPERTY

Runoff = 2.25 cfs @ 12.22 hrs, Volume= 9,504 cf, Depth= 3.72"

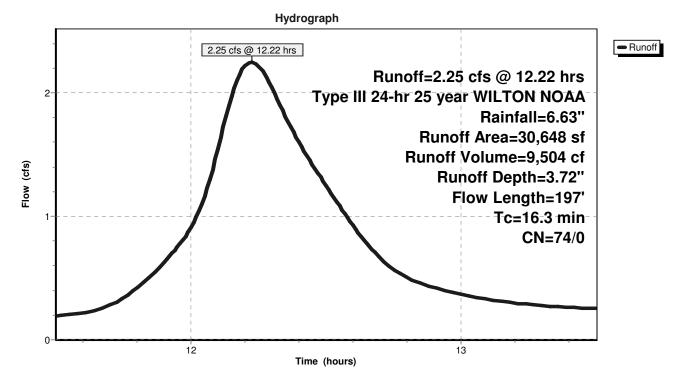
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	A	rea (sf)	CN	Description		
*		3,887	85	Driveway, C	Gravel	
		16,340	74	>75% Grass	cover, Goo	od, HSG C
		2,174	66	Woods, Poo		
		8,247	71	Pinyon/junip	oer range, C	Good, HSG D
		30,648 74 Weighted Average			verage	
		30,648	74	Pervious Ar	ea	
	Tc	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	10.6	58	0.0340	0.09		Sheet Flow, SHEET FLOW WOODS
						Woods: Light underbrush $n=0.400$ P2= 3.57"
	5.6	120	0.1000	0.35		Sheet Flow, sheet flow across grass
						Grass: Short $n = 0.150 P2 = 3.57$ "
	0.1	19	0.5000	4.95		Shallow Concentrated Flow, SHAL CONC STEEP
_						Short Grass Pasture Kv= 7.0 fps
	16.3	197	Total			

Prepared by Peak Engineers, LLC
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Subcatchment 1: POST-ACTIVITY PROPERTY



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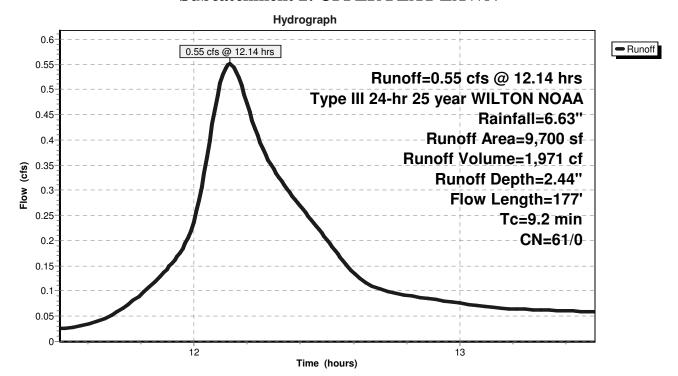
Summary for Subcatchment 2: UPPER FLAT LAWN

Runoff = 0.55 cfs @ 12.14 hrs, Volume= 1,971 cf, Depth= 2.44"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

_	A	rea (sf)	CN I	Description			
_		9,700	61 >	>75% Grass	cover, Goo	od, HSG B	
-		9,700	61 F	Pervious Are	ea		ļ
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
_	6.3	94	0.0460	0.25		Sheet Flow, SHEET FLOW UPPER LAWN	ļ
						Grass: Short n= 0.150 P2= 3.57"	
	2.7	36	0.0550	0.22		Sheet Flow, SHEET FLOW GRASS LOWER LAWN	
	0.0	4.5	2.5000	4.05		Grass: Short n= 0.150 P2= 3.57"	
	0.2	47	0.5000	4.95		Shallow Concentrated Flow, SHALL CONC FLOW S	ľŁ
_						Short Grass Pasture Kv= 7.0 fps	
	9.2	177	Total				

Subcatchment 2: UPPER FLAT LAWN



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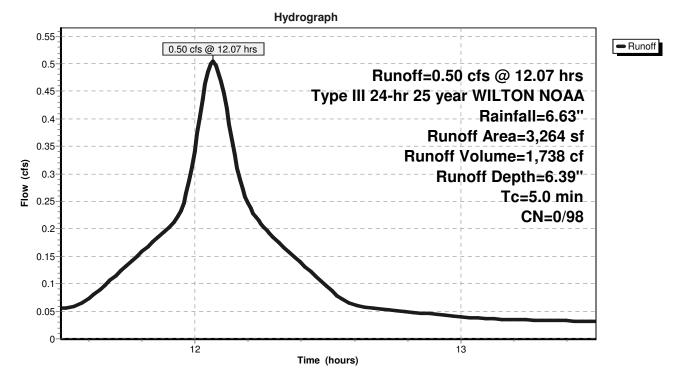
Summary for Subcatchment 3: HOUSE ROOF

Runoff = 0.50 cfs @ 12.07 hrs, Volume= 1,738 cf, Depth= 6.39"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	Area (sf)	CN	Description			
*	3,264	98	HOUSE ROOF TO DRIP LINE			
	3,264	98	Impervious	Area		
Tc (min)	Length (feet)	Slope (ft/ft	•	Capacity (cfs)	Description	
5.0					Direct Entry, DIRECT FLOW	

Subcatchment 3: HOUSE ROOF



POST-ACTIVITY

#1

#2

Primary

Discarded

Prepared by Peak Engineers, LLC

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Summary for Pond 4: 4X4 GALLERY

Inflow Area =	3,264 sf,100.00% Impervious,	, Inflow Depth = 6.39" for 25 year WILTON NOAA e
Inflow =	0.50 cfs @ 12.07 hrs, Volume=	1,738 cf
Outflow =	0.03 cfs @ 10.70 hrs, Volume=	1,738 cf, Atten= 94%, Lag= 0.0 min
Discarded =	0.03 cfs @ 10.70 hrs, Volume=	1,738 cf
Primary =	0.00 cfs @ 0.05 hrs, Volume=	0 cf

Routing by Stor-Ind method, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Peak Elev= 298.67' @ 13.56 hrs Surf.Area= 504 sf Storage= 694 cf Flood Elev= 300.00' Surf.Area= 504 sf Storage= 724 cf

Plug-Flow detention time= 172.6 min calculated for 1,738 cf (100% of inflow) Center-of-Mass det. time= 172.5 min (915.3 - 742.8)

Volume	Invert	Avail.Storage	Storage Description
#1	296.30'	271 cf	6.00'W x 8.40'L x 2.60'H Prismatoid x 10
			$1,310 \text{ cf Overall } -634 \text{ cf Embedded} = 677 \text{ cf } \times 40.0\% \text{ Voids}$
#2	296.80'	453 cf	48.0"W x 24.0"H x 8.00'L Galley 4x8x2 x 10 Inside #1
		724 cf	Total Available Storage
Device	Routing	Invert Out	let Devices

298.80' **4.0" Horiz. Orifice/Grate** Limited to weir flow C= 0.600

2.630 in/hr Exfiltration over Horizontal area

Discarded OutFlow Max=0.03 cfs @ 10.70 hrs HW=296.34' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.03 cfs)

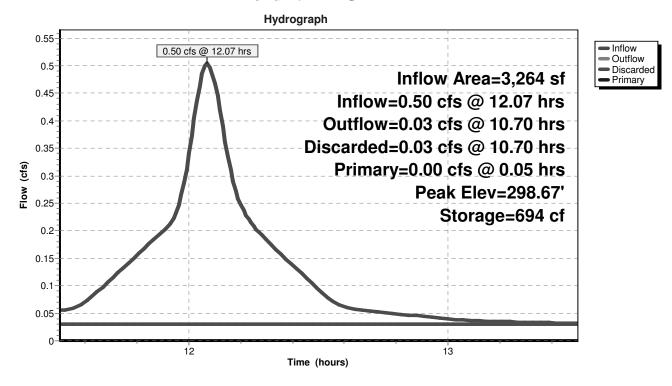
296.30'

Primary OutFlow Max=0.00 cfs @ 0.05 hrs HW=296.30' (Free Discharge) —1=Orifice/Grate (Controls 0.00 cfs)

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Pond 4: 4X4 GALLERY



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Summary for Link 5: WEST PROPERTY LINE

Inflow Area = 43,612 sf, 7.48% Impervious, Inflow Depth = 3.16" for 25 year WILTON NOAA e

Inflow = 2.69 cfs @ 12.21 hrs, Volume= 11,475 cf

Primary = 2.69 cfs @ 12.21 hrs, Volume= 11,475 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs

Link 5: WEST PROPERTY LINE

