# Peak Engineers, LLC

PROVIDING CIVIL ENGINEERING SERVICES Physical Address: 4 Old Mill Road, Redding, CT Postage: PO BOX 312, Georgetown, Conn. 06829 Tel 203-834-0588 tquinn@PeakEngineersLLC.com

March 19, 2024

Frank Smeriglio, P.E. Department of Public Works Town of Wilton Town Hall Annex 238 Danbury Road Wilton, CT 06897

Re: 53 Sugar Loaf Drive, SDP #6-23
Robert Lupinski
53 Sugar Loaf Drive
Wilton, CT
Proposed Grading New Construction
Drainage Narrative, Current vs Post (March 12, 2024 Grading Plan)

Dear Mr. Smeriglio:

This project proposes the de-construction of a retaining wall along the north, west and south sides of the property and earthwork to regrade portions of the site.

This Drainage Narrative has been prepared to compare the sites Current condition and the proposed Post-Activity condition which is the March 12, 2024 Grading Plan. The March 12, 2024 Plan includes all drainage facilities indicated on the previously submitted and reviewed Plan and Drainage Narrative dated January 26, 2024.

The Current condition is described as having; residential structure, several temporary tents, hardscape patio, areas of bare earth and steep slope.

The post-activity condition proposes several facilities to mitigate the sites drainage water.

- 1. A perimeter gravel trench and pipe will collect water from the residence roof, large portion of the gravel driveway and the eastern lawn and direct the water to a gallery and stone storm water infiltration system.
- 2. A gravel trench located at the top of the proposed slope will intercept sheet flow and allow the initial rain volumes to infiltrate the soils. A steel

garden edge will be installed to ensure sheet flow during occasions of larger storms.

3. The impervious tents and the side concrete patio will be removed.

This report will find that the proposed drainage facilities will effectively reduce the sites design storm peak flows and volumes below Current levels.

#### **Description of the Property**

The entire site is approximately 1.0012 acres of residential property located on the west side of Sugar Loaf Drive. The entire property slopes to the west.

The State of Ct Web Soil Survey reveals that the majority of the site is Canton and Charlton fine sandy loams 8-15%. The western edge of the property is Charlton-Chatfield complex, 15-45% slopes. The flattest slopes are on the eastern property edge near the road. Please see the attached CT Web Soil report. The Hydrologic soil grouping corresponds with the slope of the land with the majority of the flatter slopes being Hydraulic Group B, mid-range slopes C and the steep western edge E.

Deep soil testing, performed for a septic replacement area in 2011, reveal soils described as red brown fine sandy loams to 24" underlain with grey fine to medium sands to 72", and some broken rock was encountered from 3-6' depth. The soil percolation rate is 1"/10 minutes.

On November 9, 2023, Peak Engineers, LLC performed deep soil testing and deep percolation testing for the design of a storm water infiltration system. The testing was performed in the northeast corner of the property.

Based on the soil testing the area has been worked and is described as:

0-6" of topsoil6-30" moderately compact fill, silty brown fine sandy loam30-62" bright red brown fine sandy loam, some broken rock62-78" red brown fine sandy loam, lenses of tan sandRoots to 60".

A percolation test was performed at 47", in the original red brown fine sandy loam. The test percolation rate is 1"/11.4 minutes.

The dwelling does not have any gutters, allowing water to drip to the building edge. The builder waterproofed the foundation walls and placed gravel against the walls with a footing drain. There is approximately 12" of topsoil above the gravel. Water from the roof drips and is absorbed in the topsoil and makes its way through the gravel to the footing drain pipe. The drains run to the northwest corner of the building and to the western property line.

#### Methodology and Calculations

Utilizing Technical Release 55 runoff curve numbers and HydroCad Storm water program we have calculated the Current and Post-Activity peak design flows for the proposed improvements to the design Node. We utilized the CTDOT Engineering Bulletin EB-2015-2 Precipitation Frequency Estimates and the NOAA precipitation frequency data server interactive map to determine the precipitation frequency estimates. The design storm is the 25-year storm generating 6.63 inches of rain in a 24-hour period. Please see the attached page.

#### Proposed Drainage Facilities

The footing drain pipes will discharge into a sump pump pit at the northwest corner of the building. The HydroCad Software program has been utilized to size a gallery and stone infiltration system which will effectively store the water and then promote infiltration of the collected water from the roof. The calculations indicate that during the 25-year design storm the system will not overflow. A yard drain is proposed to allow the less frequent larger storms to overflow onto the upper lawn area.

# Please see sheet 5 and 6 for a Summary of HydroCad output peak rate of flows and volumes generated by the sites 25 year design storm of 6.63" in a period or 24 hours.

	Current Volume	March 12 Plar Post-Activity Volume	n Change Volume	% Change	Jan 26 Plan Post-Activity Volume
Node	13,859 CF	9,742 CF	-4,117 CF	-29.7%	9,622 CF
Node	Current Flow, CFS	Post-Activity Flow CFS	Change CFS	% Change	Post-Act Flow CFS
Node	3.06 cfs	2.54 cfs	-0.52 cfs	-17.0%	3.06 cfs

#### **Design Considerations and Best Management Practices**

The storm water management plan proposes to minimize the impacts of the roof water and driveway water by utilizing systems of best management practices to handle the sites storm water. The components of the system are described below.

1. BMP-no point discharge. The building will not have gutters. Through a series of facilities the roof water will enter an infiltration system.

- 2. BMP-disconnected impervious areas. Roof, driveway and other hard surfaces flow onto lawn area.
- 3. BMP-recharge soils. The site proposes a gravel driveway allowing water from minor storms to infiltrate the soils.
- 4. BMP- promote groundwater infiltration. Subsequent to 2011, grading was performed to dramatically flatten the sites slopes, especially in the large lawn area to the north of the house and to the west of the house. This grading allows water to infiltrate soils and decreases the time of concentration to the property line.
- 5. BMP-reduce erosion potential. The finished slope embankment includes a reverse bench mid-way down the slope. Reverse benches are effective in decreasing water flow velocity and limiting potential for erosion.

## Conclusions

The HydroCad study confirms that the site grading will effectivity decrease the peak rate of flow and peak volume of flow from the site. The study also confirms that the March 12, 2024 grading plan is equally effective in reducing the sites peak rate of flow and peak volume of flow as the previously reviewed and approved plan dated January 26, 2024.

It is the opinion of Peak Engineers, LLC that the proposed drainage systems and grading will result in a decrease in the design flow rate (25-year storm) and design flow volume from the property when compared to the Current condition. The proposed grading will be performed in a manner that will not alter the existing or historical drainage patterns.

The proper installation of temporary and well as permanent sediment and erosion controls, following the 2002 Connecticut Erosion and Sediment Guidelines, will help reduce the effects of the construction on the downstream properties. Peak Engineers, LLC recommends that a site monitor be required to perform weekly site observations as well as review immediately prior to an expected rain event.

Respectfully submitted,



For Peak Engineers, LLC, Thomas S. Quinn, P.E.

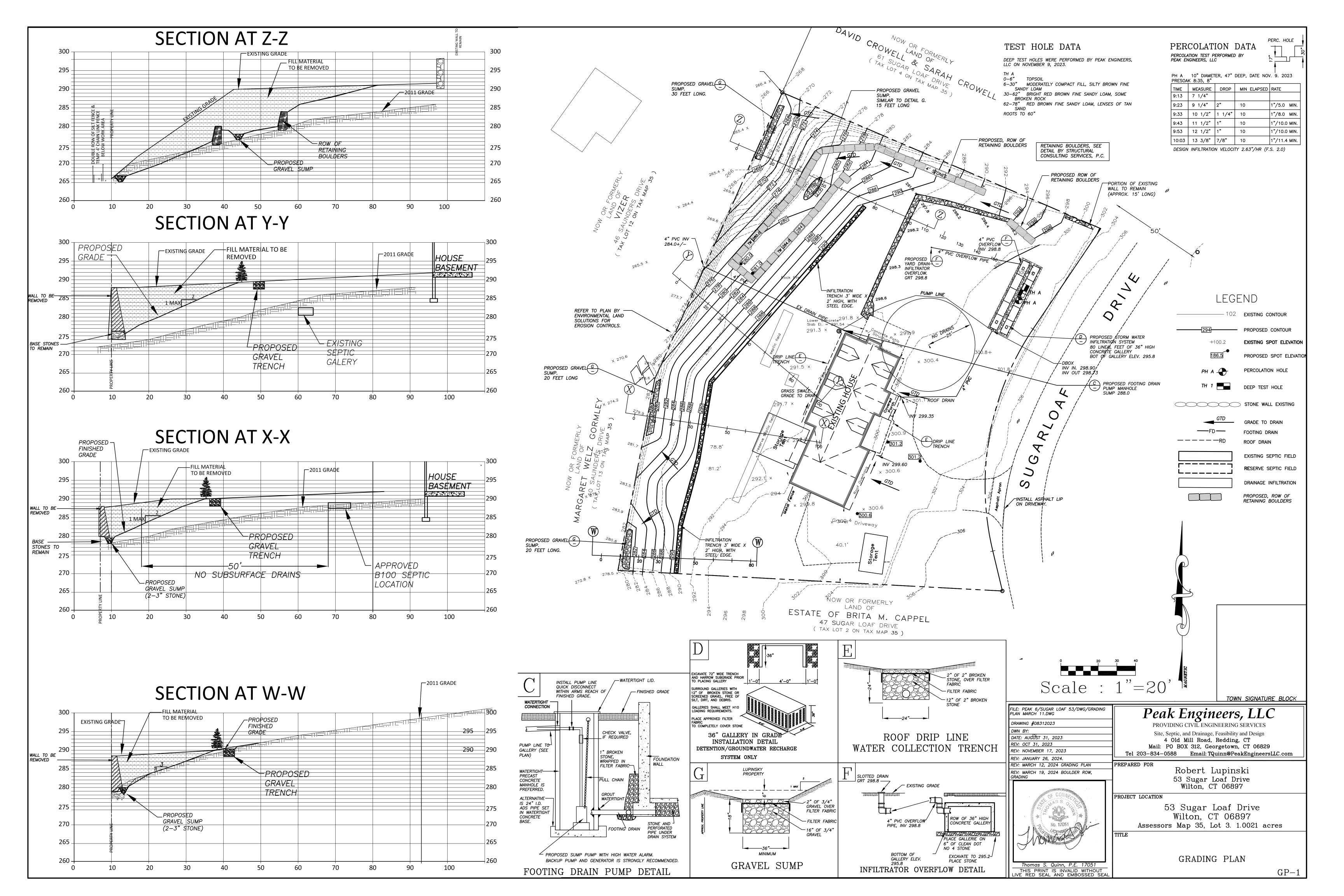
# **Events for Link 6: WEST PROPERTY LINE**

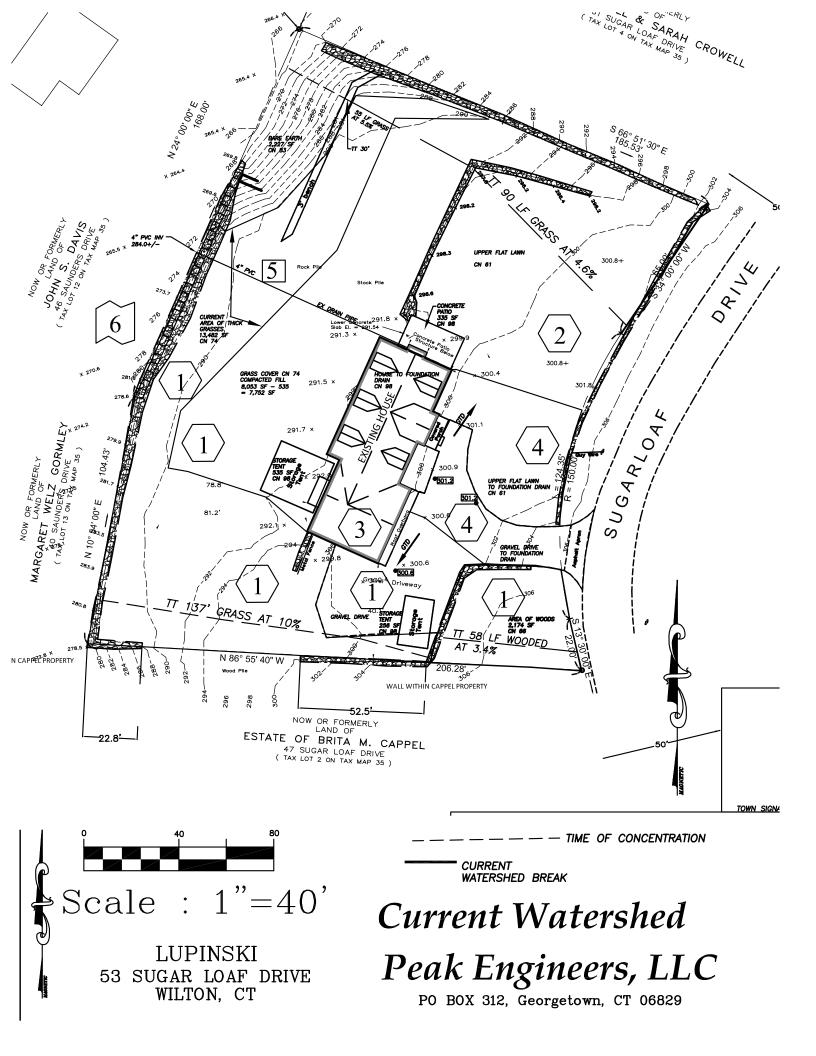
Event	Inflow	Primary	Volume	Elevation
	(cfs)	(cfs)	(cubic-feet)	(feet)
2 YR WILTON NOAA	1.04	1.04	5,102	0.00
10 year WILTON NOAA	2.40	2.40	10,288	0.00
25 year WILTON NOAA	3.06	3.06	13,859	0.00

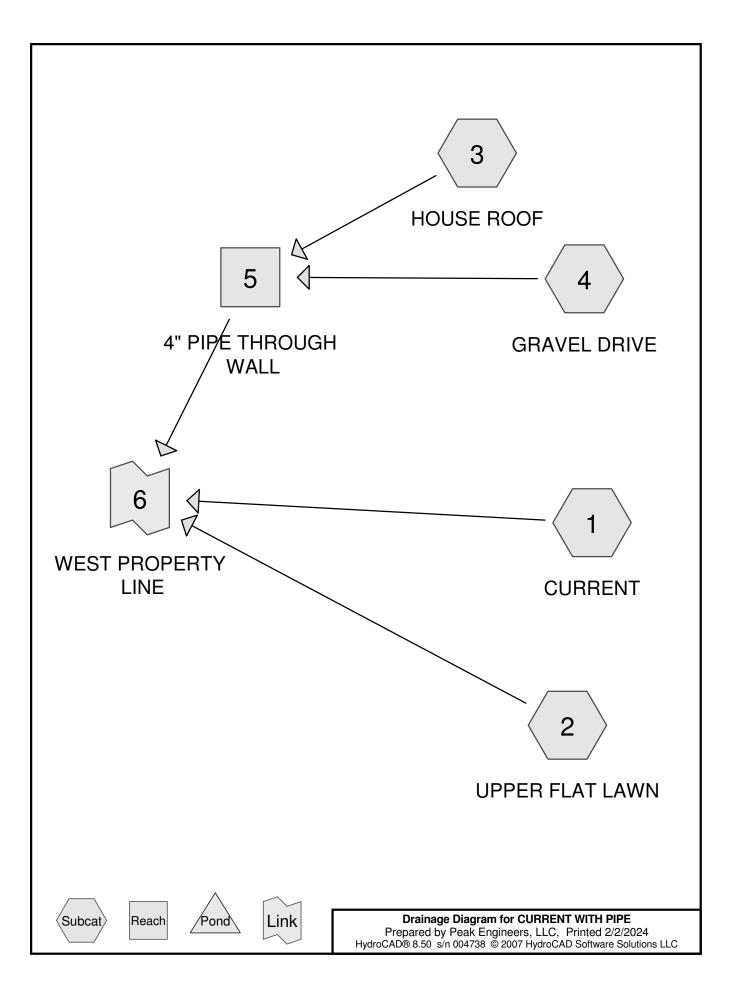
# **Summary for Link 5: WEST PROPERTY LINE**

Inflow Are	ea =	43,612 s	f, 7.48% Impervious,	Inflow Depth =	2.68" for	25 year WILTON NOAA e
Inflow	=	2.54 cfs @	12.26 hrs, Volume=	9,742 cf		
Primary	=	2.54 cfs @	12.26 hrs, Volume=	9,742 cf,	Atten= 0%	, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs







# CURRENT WITH PIPE Prepared by Peak Engineers, LLC HydroCAD® 8.50 s/n 004738 © 2007 HydroCAD Software Solutions LLC

# Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
7,241	61	>75% Grass cover, Good, HSG B (2)
2,459	61	FLAT LAWN (4)
2,174	66	Woods, Poor, HSG B (1)
7,752	74	>75% Grass cover, Good, HSG B (1)
13,482	74	>75% Grass cover, Good, HSG C (1)
2,227	83	BARE EARTH (1)
2,123	85	Driveway, Gravel (1)
1,764	85	GRAVEL DRIVE (4)
3,264	98	HOUSE ROOF TO DRIP LINE (3)
1,126	98	TENTS AND PATIO (1)
43,612		TOTAL AREA

# **Summary for Subcatchment 1: CURRENT**

Runoff = 2.19 cfs @ 12.23 hrs, Volume= 9,448 cf, Depth= 3.93"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

<i>I</i>	Area (sf)	CN	Г	Description		
*	2,123	85	Г	Driveway, C	Gravel	
*	7,752	74	>	75% Grass	cover, Goo	od, HSG B
	2,174	66	V	Voods, Poo	r, HSG B	
	13,482	74	>	75% Grass	cover, Goo	od, HSG C
*	2,227	83	В	ARE EAR	TH	
*	1,126	98	Τ	ENTS AN	D PATIO	
	28,884	76	V	Veighted A	verage	
	27,758	75	Р	ervious Ar	ea	
	1,126	98	Iı	mpervious .	Area	
Tc	$\mathcal{C}$	Slop		Velocity	Capacity	Description
(min)	(feet)	(ft/f	t)	(ft/sec)	(cfs)	
10.6	58	0.034	-0	0.09		Sheet Flow, SHEET FLOW WOODS
						Woods: Light underbrush $n=0.400$ P2= 3.57"
6.3	137	0.100	0	0.36		Sheet Flow, sheet flow across grass
						Grass: Short n= 0.150 P2= 3.57"
16.9	195	Total				

# **CURRENT WITH PIPE**

Prepared by Peak Engineers, LLC

Hydrograph - Runoff 2.19 cfs @ 12.23 hrs Runoff=2.19 cfs @ 12.23 hrs 2-Type III 24-hr 25 year WILTON NOAA Rainfall=6.63" Runoff Area=28,884 sf Runoff Volume=9,448 cf Flow (cfs) Runoff Depth=3.93" Flow Length=195' Tc=16.9 min 1 CN=75/98 0 12 13 Time (hours)

# **Subcatchment 1: CURRENT**

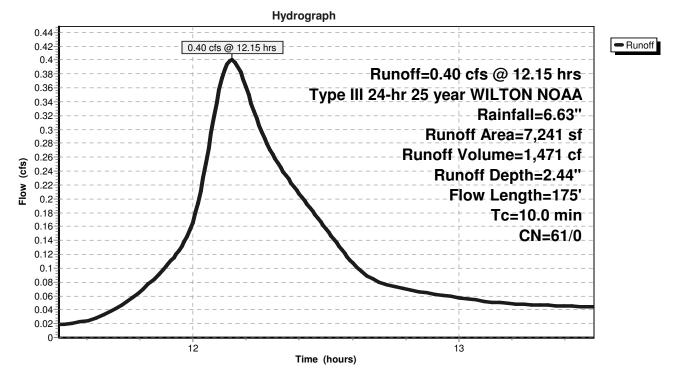
# Summary for Subcatchment 2: UPPER FLAT LAWN

Runoff = 0.40 cfs @ 12.15 hrs, Volume= 1,471 cf, Depth= 2.44"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	A	rea (sf)	CN ]	Description		
		7,241	61 2	>75% Grass	cover, Goo	od, HSG B
		7,241	61	Pervious Ar	ea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	6.1	90	0.0460	0.25		Sheet Flow, SHEET FLOW UPPER LAWN
						Grass: Short n= 0.150 P2= 3.57"
	3.8	55	0.0550	0.24		Sheet Flow, SHEET FLOW GRASS LOWER LAWN
						Grass: Short $n=0.150$ P2= 3.57"
	0.1	30	0.5000	7.07		Shallow Concentrated Flow, SHALL CONC FLOW STR
_						Nearly Bare & Untilled Kv= 10.0 fps
	10.0	175	Total			

# Subcatchment 2: UPPER FLAT LAWN



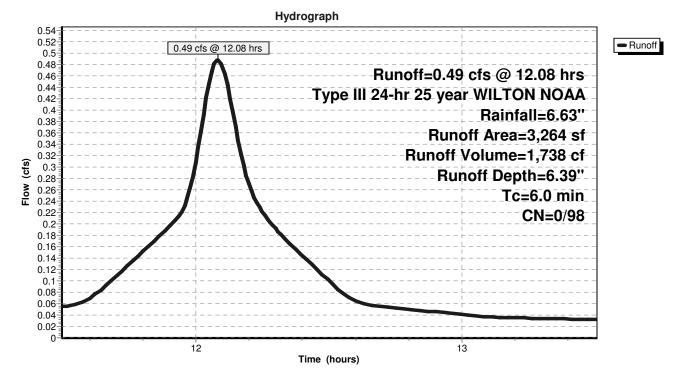
# **Summary for Subcatchment 3: HOUSE ROOF**

Runoff = 0.49 cfs @ 12.08 hrs, Volume= 1,738 cf, Depth= 6.39"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

A	Area (sf)	CN	Description								
*	3,264	98	HOUSE RO	HOUSE ROOF TO DRIP LINE							
	3,264	98	Impervious .	Area							
m	T .1	<b>C1</b>	<b>T</b> 7 <b>1</b>	<b>a</b>							
Tc	Length	Slope	e Velocity	Capacity	Description						
$(\min)$	(feet)	(ft/ft	) (ft/sec)	(cfs)							
6.0					Direct Entry, DIRECT FLOW						

## **Subcatchment 3: HOUSE ROOF**



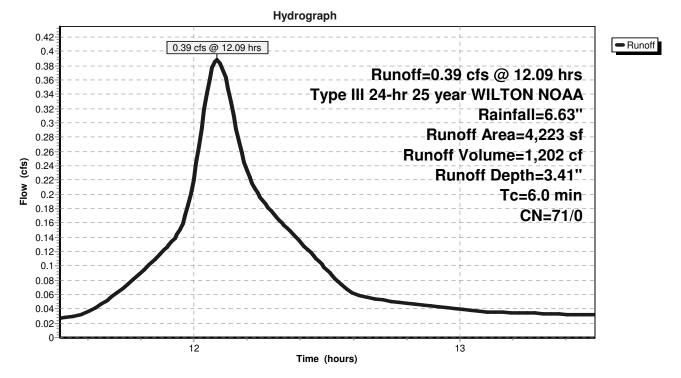
# **Summary for Subcatchment 4: GRAVEL DRIVE**

Runoff = 0.39 cfs @ 12.09 hrs, Volume= 1,202 cf, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

A	rea (sf)	CN	Description		
*	1,764	85	GRAVEL D	RIVE	
*	2,459	61	FLAT LAW	N	
	4,223	71	Weighted A	verage	
	4,223	71	Pervious Are	ea	
Tc (min)	Length (feet)	Slop (ft/ft	•	Capacity (cfs)	Description
6.0					Direct Entry,

### **Subcatchment 4: GRAVEL DRIVE**



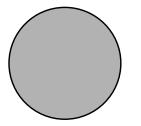
# Summary for Reach 5: 4" PIPE THROUGH WALL

Inflow Are	ea =	7,487 s	f, 43.60% Ir	mpervious,	Inflow Depth =	4.71" fo	or 25	year WILTON	NOAA e
Inflow	=	0.87 cfs @	12.09 hrs, V	Volume=	2,940 cf				
Outflow	=	0.56 cfs @	12.01 hrs, V	Volume=	2,940 cf,	Atten= 36	5%, I	Lag= 0.0 min	

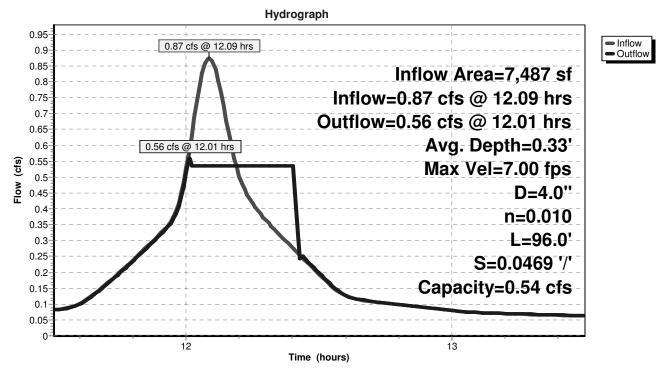
Routing by Stor-Ind method, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Max. Velocity= 7.00 fps, Min. Travel Time= 0.2 min Avg. Velocity = 2.83 fps, Avg. Travel Time= 0.6 min

Peak Storage= 8 cf @ 12.02 hrs, Average Depth at Peak Storage= 0.33' Bank-Full Depth= 0.33', Capacity at Bank-Full= 0.54 cfs

4.0" Diameter Pipe, n= 0.010 Length= 96.0' Slope= 0.0469 '/' Inlet Invert= 288.50', Outlet Invert= 284.00'



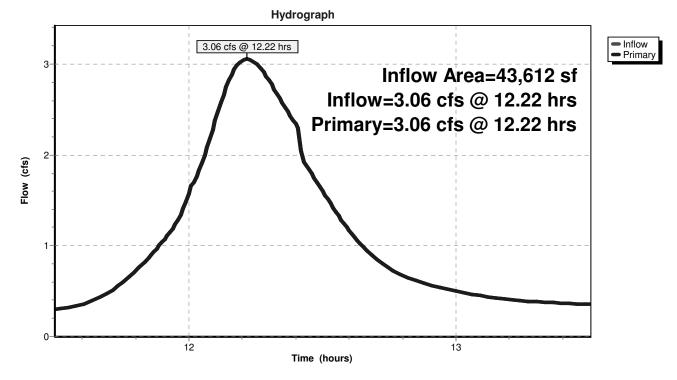




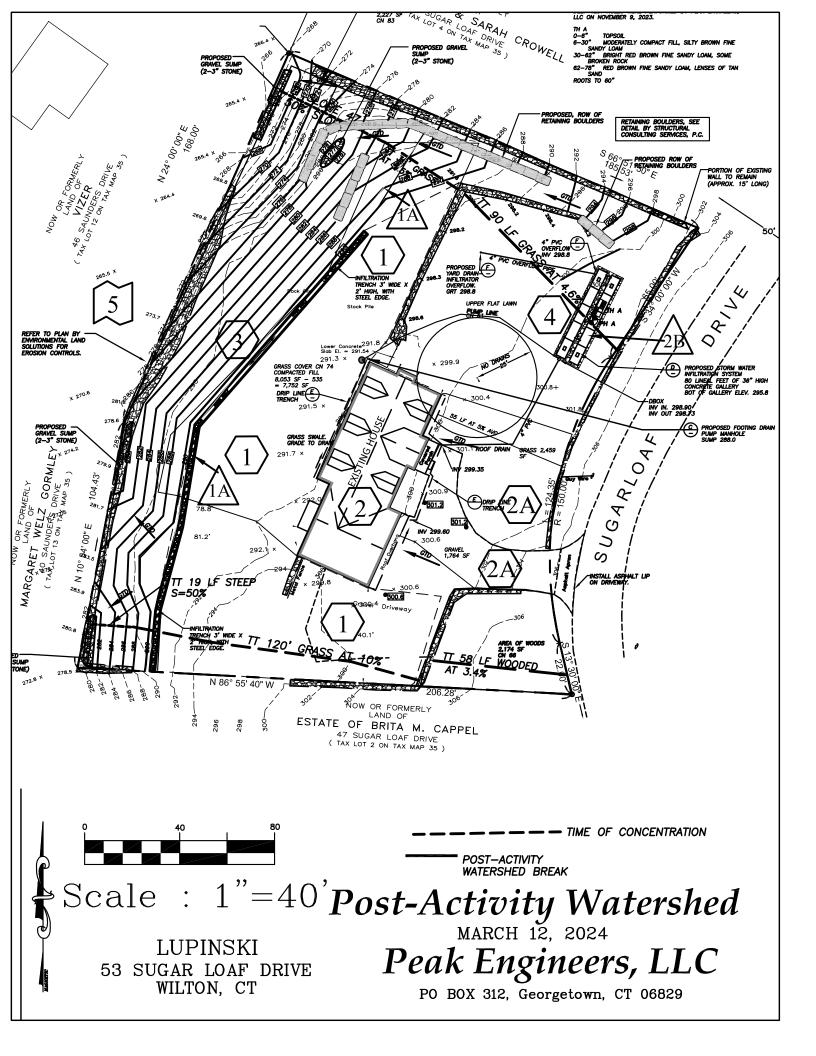
# **Summary for Link 6: WEST PROPERTY LINE**

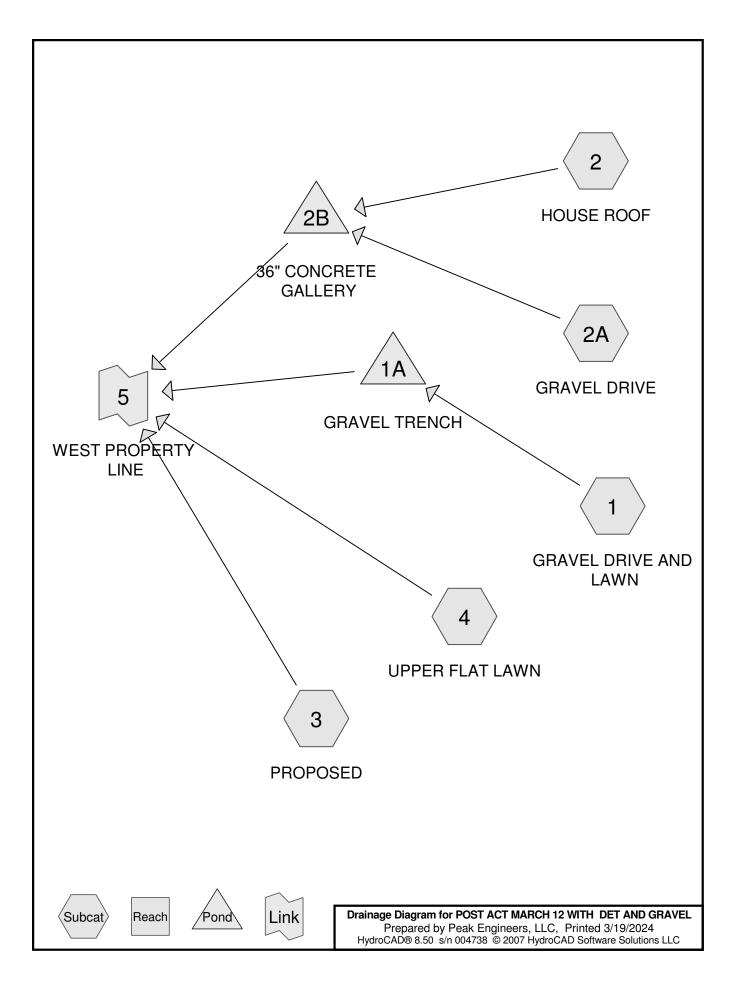
Inflow Ar	ea =	43,612 s	f, 10.07% Impervious,	Inflow Depth =	3.81" for	25 year WILTON NOAA e
Inflow	=	3.06 cfs @	12.22 hrs, Volume=	13,859 cf		-
Primary	=	3.06 cfs @	12.22 hrs, Volume=	13,859 cf,	Atten= 0%	, Lag= $0.0 \min$

Primary outflow = Inflow, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs



# Link 6: WEST PROPERTY LINE



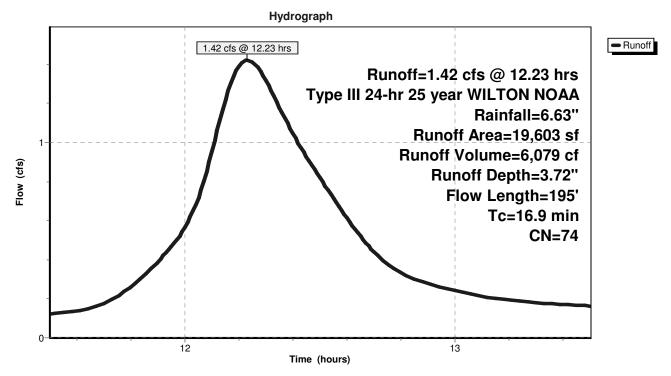


## Summary for Subcatchment 1: GRAVEL DRIVE AND LAWN

Runoff = 1.42 cfs @ 12.23 hrs, Volume= 6,079 cf, Depth= 3.72''

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	A	Area (sf)	CN	Description							
*		2,123	85	Driveway, C	Driveway, Gravel						
*		7,752	74	>75% Grass	cover, Goo	od, HSG B					
		7,554	74	>75% Grass	cover, Goo	od, HSG C					
		2,174	66	Woods, Poo	r, HSG B						
		19,603	74	Weighted A	verage						
		19,603		Pervious Ar	ea						
	Tc	Length	Slope	e Velocity	Capacity	Description					
(	min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
	10.6	58	0.0340	) 0.09		Sheet Flow, SHEET FLOW WOODS					
						Woods: Light underbrush $n=0.400$ P2= 3.57"					
	6.3	137	0.1000	0.36		Sheet Flow, sheet flow across grass					
						Grass: Short n= 0.150 P2= 3.57"					
	16.9	195	Total								



# Subcatchment 1: GRAVEL DRIVE AND LAWN

# **Summary for Pond 1A: GRAVEL TRENCH**

19,603 sf, 0.00% Impervious,	Inflow Depth = $3.72$ "	for 25 year WILTON NOAA e
-2 cfs @ 12.23 hrs, Volume=	6,079 cf	
9 cfs @ 12.24 hrs, Volume=	6,079 cf, Atten=	0%, Lag= 0.6 min
2 cfs @ 9.52 hrs, Volume=	1,568 cf	
7 cfs @ 12.24 hrs, Volume=	4,511 cf	
	2 cfs @ 12.23 hrs, Volume= 9 cfs @ 12.24 hrs, Volume= 2 cfs @ 9.52 hrs, Volume=	9 cfs @       12.24 hrs, Volume=       6,079 cf, Atten=         2 cfs @       9.52 hrs, Volume=       1,568 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Peak Elev= 290.11' @ 12.24 hrs Surf.Area= 636 sf Storage= 350 cf Flood Elev= 290.40' Surf.Area= 636 sf Storage= 350 cf

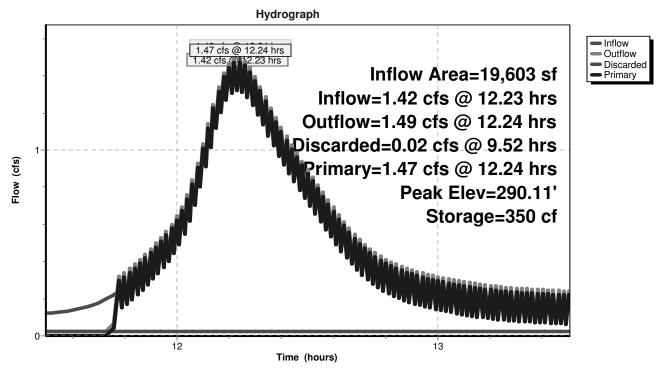
Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 52.7 min ( 887.1 - 834.4 )

Volume	Invert	Avail.Stora	ge Storage Description
#1	288.00'	3	cf 3.00'W x 135.00'L x 2.00'H Prismatoid STONE TRENCH
			810 cf Overall x 0.4% Voids
#2	288.50'	347	cf 3.00'W x 77.00'L x 1.50'H Prismatoid GRASS SWALE
		350	cf Total Available Storage
Device	Routing	Invert	Outlet Devices
#1	Primary	290.10'	285.0' long Sharp-Crested Rectangular Weir
	·	,	2 End Contraction(s) 0.5' Crest Height
#2	Discarded	288.00'	1.500 in/hr Exfiltration over Horizontal area

**Discarded OutFlow** Max=0.02 cfs @ 9.52 hrs HW=288.50' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=1.47 cfs @ 12.24 hrs HW=290.11' TW=0.00' (Dynamic Tailwater) —1=Sharp-Crested Rectangular Weir (Weir Controls 1.47 cfs @ 0.38 fps)





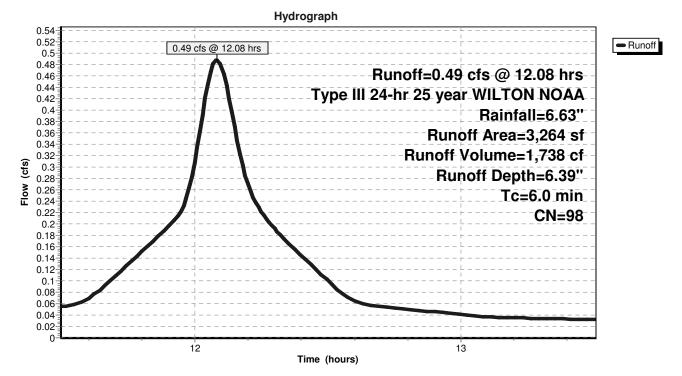
# **Summary for Subcatchment 2: HOUSE ROOF**

Runoff = 0.49 cfs @ 12.08 hrs, Volume= 1,738 cf, Depth= 6.39"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	Area (sf)	CN	Description		
*	3,264	98	HOUSE RO	OF TO DR	IP LINE
	3,264		Impervious	Area	
Tc	E Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0					Direct Entry, DIRECT FLOW

## **Subcatchment 2: HOUSE ROOF**



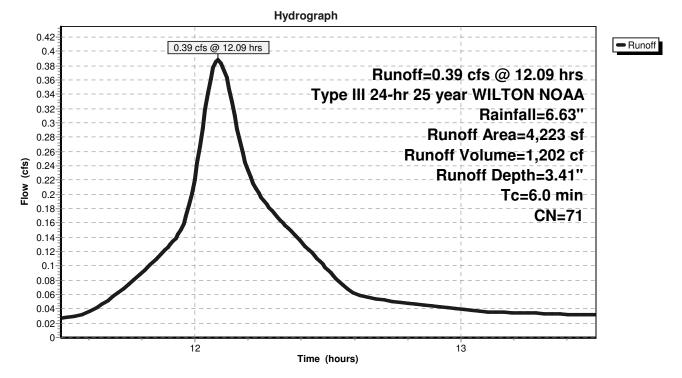
# Summary for Subcatchment 2A: GRAVEL DRIVE

Runoff = 0.39 cfs @ 12.09 hrs, Volume= 1,202 cf, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

A	area (sf)	CN	Description		
*	1,764	85	GRAVEL D	RIVE	
*	2,459	61	FLAT LAW	'N	
	4,223 4,223	71	Weighted A Pervious Ar	U	
Tc (min)	Length (feet)	Slop (ft/ft	•	Capacity (cfs)	Description
6.0					Direct Entry,

### Subcatchment 2A: GRAVEL DRIVE



# Summary for Pond 2B: 36" CONCRETE GALLERY

Inflow Area =	7,487 sf, 43.60% Impervious,	Inflow Depth = 4.71" for 25 year WILTON NOAA e
Inflow =	0.87 cfs @ 12.09 hrs, Volume=	2,940 cf
Outflow =	0.49 cfs @ 12.27 hrs, Volume=	2,940 cf, Atten= 44%, Lag= 11.0 min
Discarded =	0.03 cfs @ 10.66 hrs, Volume=	2,383 cf
Primary =	0.46 cfs @ 12.27 hrs, Volume=	557 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Peak Elev= 299.98' @ 12.27 hrs Surf.Area= 504 sf Storage= 1,004 cf Flood Elev= 300.00' Surf.Area= 504 sf Storage= 1,004 cf

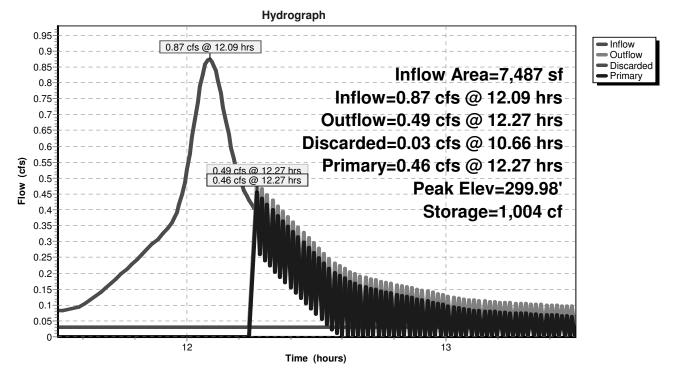
Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 243.8 min (1,023.2 - 779.4)

Volume	Invert	Avail.Storage	Storage Description
#1	295.20'	380 cf	6.00'W x 8.40'L x 3.60'H Prismatoid x 10
			1,814 cf Overall - 865 cf Embedded = 950 cf x 40.0% Voids
#2	295.80'	624 cf	<b>48.0''W x 36.0''H x 8.00'L Galley 4x4x3</b> x 10 Inside #1
		1,004 cf	Total Available Storage
Device	Routing	Invert Out	let Devices

#1	Primary	298.80'	4.0" Horiz. Orifice/Grate	Limited to weir flow $C = 0.600$
#2	Discarded	295.20'	2.630 in/hr Exfiltration ove	er Horizontal area

**Discarded OutFlow** Max=0.03 cfs @ 10.66 hrs HW=295.25' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.46 cfs @ 12.27 hrs HW=299.98' TW=0.00' (Dynamic Tailwater) -1=Orifice/Grate (Orifice Controls 0.46 cfs @ 5.23 fps)



# Pond 2B: 36" CONCRETE GALLERY

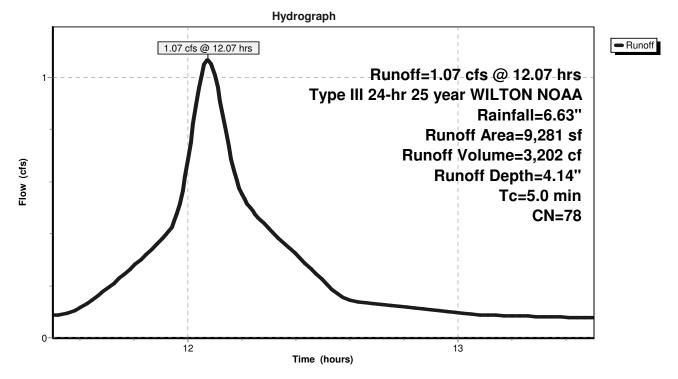
# **Summary for Subcatchment 3: PROPOSED**

Runoff = 1.07 cfs @ 12.07 hrs, Volume= 3,202 cf, Depth= 4.14''

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

	A	rea (sf)	CN	Description		
*		9,281	78	2:1 SLOPE	VEGETAT	ED
		9,281		Pervious Ar	ea	
	Tc	Length	Slope	Velocity	Capacity	Description
_(n	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•
	5.0					Direct Entry, DIRECT FLOW

### Subcatchment 3: PROPOSED



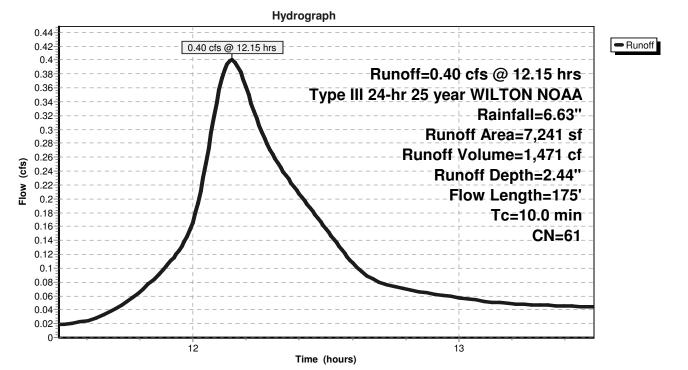
# Summary for Subcatchment 4: UPPER FLAT LAWN

Runoff = 0.40 cfs @ 12.15 hrs, Volume= 1,471 cf, Depth= 2.44"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 year WILTON NOAA Rainfall=6.63"

_	Α	rea (sf)	CN	Description				
_	7,241 61 >75% Grass cover, Good, HSG B							
_		7,241		Pervious Ar	ea			
	Tc (min)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description		
-	6.1	90	0.0460	0.25		Sheet Flow, SHEET FLOW UPPER LAWN		
	3.8	55	0.0550	0.24		Grass: Short n= 0.150 P2= 3.57" Sheet Flow, SHEET FLOW GRASS LOWER L	AWN	
	0.1	30	0.5000	7.07		Grass: Short n= 0.150 P2= 3.57" Shallow Concentrated Flow, SHALL CONC FL Nearly Bare & Untilled Kv= 10.0 fps	.OW STE	
_	10.0	175	Total			· · · · ·		

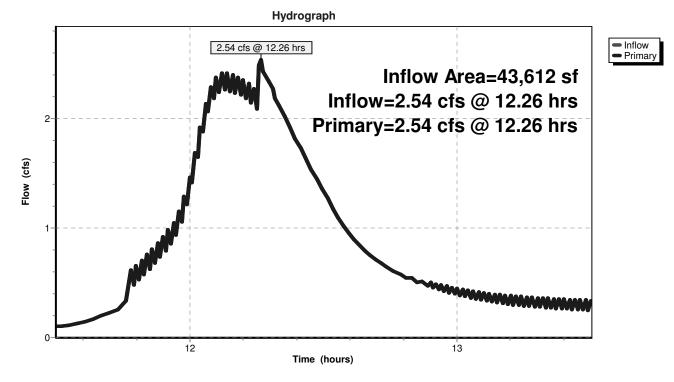
# Subcatchment 4: UPPER FLAT LAWN



# **Summary for Link 5: WEST PROPERTY LINE**

Inflow Ar	ea =	43,612 s	f, 7.48% Impervious,	Inflow Depth =	2.68" fo	or 25 year WILTON NOAA e
Inflow	=	2.54 cfs @	12.26 hrs, Volume=	9,742 cf		-
Primary	=	2.54 cfs @	12.26 hrs, Volume=	9,742 cf,	Atten= 04	%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.05-36.00 hrs, dt= 0.01 hrs



# Link 5: WEST PROPERTY LINE