





lighe&Bond

64 Danbury Road Wilton, CT 06897

Engineering Report

Prepared For:

Town of Wilton, Planning and Zoning Commission

December 2023

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Section 1 Introduction and Site Conditions

Tighe & Bond has prepared this report at the request of Fuller Development, LLC ("Applicant"), to support their applications to the Town of Wilton Planning & Zoning Commission and Inlands Wetlands Commission for a proposed 8-building residential development with 93 units.

The 64 Danbury Road site is an approximately 4.84-acre unit located on the northern extents of a larger 22.27-acre parcel of land, the entirety of which is bounded by Danbury Road to the west, wooded area and residential properties to the east, and commercial properties to the north and south. The proposed development consists of the construction of a 93-unit residential development, at-grade parking, stormwater management systems, utility services, lighting, and associated landscaping. Refer to **Figure 1**, Site Location Map, in **Appendix A**.

Tighe & Bond has inspected the property and analyzed available soils, drainage, utility, wetland, and topographic information. Drainage calculations and stormwater management design have been prepared in accordance with the 2000 Connecticut Department of Transportation (CTDOT) Drainage Manual, and the Connecticut Department of Energy and Environmental (DEEP) Protection 2004 Stormwater Quality Manual. The drainage calculations include a hydrologic and hydraulic analysis of the existing conditions and the proposed development. Specifically, the calculations include an analysis of the on-site stormwater management measures and their performance in handling peak flow attenuation and pollutant removals. The report also includes a summary of the site floodplain management for Copts Brook, the available existing and proposed utilities to service the property, and the proposed soil erosion and sedimentation control measures incorporated during construction.

1.1 Existing Conditions

The existing site consists of an office building with a 15,500 square-foot footprint and atgrade parking. The development site is located within Wilton's DE-5R (East) Design Enterprise District Zone. A significant portion of the site is impervious, including paved parking areas, sidewalks, and building roof area, with landscaping and lawns generally around the perimeter of the site. Utility services include underground water, natural gas, electric, and tele-data, which ultimately connect to service mains and overhead lines in Danbury Road.

The site is located on Danbury Road (Route 7) which is a north-south four lane State maintained major arterial roadway, with dedicated left turn lanes for a traffic light at the main entrance. The roadway is generally 50 feet wide and widens to roughly 60-feet along the frontage of the site to accommodate the aforementioned left turn lanes.

The topography of the site slopes primarily from east to west towards Copts Brook and Route 7. There is a series of catch basins and inlet structures on the existing site, which capture runoff and discharges to 54" RCP along the northern end of the site. The front yard of the property partially lies within the 500-year flood plain for the Norwalk River, while a small part of the middle of the property lies within the 100-year floodplain for

Copts Brook. This floodplain and site hydrology will be discussed in greater detail later in this report.

1.2 Project Proposal

The 8-building residential development with 93 units includes driveways and parking areas throughout the site. The development will use the current entry drive and the same point of access to Danbury Road as the other properties at 50 and 60 Danbury Road. A centrally located clubhouse and pool is proposed for the development immediately adjacent to the existing entry loop roadway. The site development plan also includes a network of sidewalks for pedestrian circulation and retaining walls to minimize the overall development footprint and grading impacts, as well as to establish required finished floor elevations. New utility services for the property are proposed including underground water, natural gas, electric, tel-com and sanitary sewer.

Stormwater management will be accommodated on-site. Surface runoff will be collected in catch basins and inlet structures located throughout the site and tie into the existing drainage infrastructure to be maintained. Underground infiltration systems have been designed to reduce peak flows and provide stormwater treatment, prior to discharge. The stormwater management system has been designed to treat the 0.5-inch water quality volume and remove a high level of pollutants. This will be discussed in greater detail later in the report.

1.3 Site Soils

The U.S. Department of Agriculture's National Resource Conservation Service (NRCS) Web Soil Survey indicates the following soil types are present on the site:

Urban Land (307): Urban land is mostly covered by streets, parking lots, buildings, and other structures of urban areas. Slopes range from 0 to 33 percent. No drainage class is assigned, and the complex does not meet hydric criteria.

Udorthents-Urban Land Complex (306): Udorthents is a miscellaneous land type used to denote moderately well to excessively drained earthen material which has been so disturbed by cutting, filling, or grading that the original soil profile can no longer be discerned. Udorthents consist of very deep, moderately well drained to excessively drained soils on uplands, terraces and plains. They are highly disturbed soils commonly associated with construction and building or surface mining. Typically, more than 2 feet of the original soil has been removed or it has been covered with more than 2 feet of earthy fill. Texture to a depth of 60 inches, varies from silt loam to extremely gravelly sand. Slopes range from 0 to 35 percent.

Canton and Charlton Fine Sandy Loams (60C & 61C): The Charlton component is typically found on hills, uplands while the Chatfield component is typically found on bedrock-controlled ridges, uplands, bedrock-controlled hills. The parent material of both soils consists of coarse-loamy melt-out till derived from granite and/or schist and/or gneiss with a natural drainage class of well drained. These soil does not meet hydric criteria. Slope ranges from 8 to 15 percent.

A copy of the NRCS Soil Resource Report is included in **Appendix B** of this report.

Soil permeability for the site was estimated to be 1-inch per hour for the design of the proposed stormwater management systems and are in part based on historic design assumptions used for the site. We believe the estimate is conservative given the soil classifications, furthermore permeability estimates will be field verified at the site prior to the completion of construction documents to confirm the design assumptions are accurate.

1.4 Wetlands

Wetlands soils were delineated and flagged by Otto Theall, professional soil scientist on February and March, 2017 and located in the field by D'Andrea Surveying & Engineering, P.C. Wetland flags and limits are depicted on the project drawing sheets.

Section 2 Stormwater Management

2.1 Existing Site Hydrologic Analysis

To review the impact of the proposed development on the existing site, an existing conditions hydrologic analysis was performed. Under existing conditions, stormwater runoff from the site generally flows from east to west towards Copts Brook and Danbury Road (US Route 7). There are a series of catch basins and inlet structures on the 64 Danbury Road site that capture runoff and discharge to a 54" RCP culvert that crosses Danbury Road and outlets to the Norwalk River. This culvert takes the majority of runoff from 64 Danbury Road as well as from 60 Danbury Road and the recently expanded parking garage. There are three oversized perforated pipes within this existing drainage network that provide nominal storage/infiltration for runoff from the parking areas and one water quality structure that treats a small portion of the parking area as well. In addition, there is an existing subsurface retention system near the site entry from Danbury Road that collects runoff from most of the circular entry drive before discharging it to the 54-inch RCP culvert. Lastly, the culvert also receives flow from Copts Brook and ultimately conveys the aggregate runoff from all these areas to the Norwalk River. The last segment of the 54" RCP culvert along the southern edge of the property has been designated as Design Point B for our analysis.

There are 2 additional design points in the northeastern portion of the site which are used to analyze overland flow to Copts Brook and overland flow offsite to the northeast. These are denoted as Design Points A & C respectively.

The drainage areas for the existing site and contributing areas have been delineated into sub-watershed areas and are shown on the Existing Conditions Watershed Map (Figure EX-WS), which is included in **Appendix C** of this report.

Impervious and pervious areas, weighted curve number, and time of concentration were calculated for each watershed area and developed into hydrologic model to determine the project's peak flow and volume, as part of the comparative hydrology analysis. Precipitation data for the hydrologic modeling were developed from NOAA's Atlas 14 Point Precipitation Frequency Estimates online utility. The site-specific precipitation depths for a 24-hour durations storm are shown in **Table 2-1** below.

Table 2-1
24-hour Duration Precipitation Depth

	2-Year	10-Year	25-Year	50-Year	100-Year
Depth (in)	3.52	5.38	6.54	7.41	8.34

A breakdown of existing watershed areas, existing volumetric hydrographs, and the existing watershed map are included in **Appendix C** of this report.

2.1.1 Floodplain Management

The Federal Emergency Management Agency's Flood Insurance Rate Map (FIRM) for Fairfield County, effective June 18, 2010 shows a portion of the site within Zone X

(shaded) Norwalk River 500-year floodplain along Danbury Road, and the floodway and Zone A of Copts Brook, as shown in **Figure 2** in **Appendix A**.

Zone A is studied by approximate methods, and therefore does not have established base flood elevations or a regulatory floodway. Since there is no available base flood data for Copt's Brook, we prepared a hydrologic and hydraulic analysis of the Copt's Brook watershed contributing to the drainage inlet on the site to establish a base flood elevation. Please refer to Section 3, Floodplain Management, for more details.

2.2 Proposed Site Hydrologic and Hydraulic Analysis

A stormwater management system has been designed for the proposed development to reduce or maintain existing peak flows and improve water quality for the site. The proposed stormwater management system consists of catch basins and inlets throughout the development site as well as water quality structures, underground infiltration systems, and outlet protection. The stormwater management system will maintain existing drainage piping to maximum extent practical and utilize Best Management Practices for stormwater treatment.

Under proposed conditions, drainage patterns will generally remain the same, largely flowing in a westerly direction and ultimately discharging to the 54" RCP culvert for Copts Brook. Drainage structures have been located throughout the site to collect stormwater runoff from paved and landscaped surfaces. Due to the various locations of the proposed buildings and the need to maintain a significant portion of the existing drainage network, the proposed drainage system has been split into six different sub-systems around the site. Infiltration systems have been designed for each area to promote infiltration and provide treatment of stormwater runoff. The bottom elevation of each system was also designed to be at or above the elevations for the existing infiltration pipes on site to ensure they are above the known ground water table. Ultimately, these systems converge into a single piped location at the western edge of the site. The existing retention system located adjacent to the main entry at Danbury Road will remain in place and unchanged. The contributing area for this system is minimally impacted by the proposed development plan and any changes to discharge flows will be negligible. Likewise, the 42-inch perforated pipe which receives runoff from 60 Danbury Road will remain in place as well and the proposed stormwater management system has been designed around it.

Lastly, a small portion of the site consisting of lawn area and 7 patios behind Buildings 7 and 8 is captured using area drains and discharged directly to the hillside adjacent to Copts Brook. A riprap apron and level spreader have been designed to reduce outlet velocities and provide erosion control prior to this discharge.

2.2.1 Proposed Site Hydrology

The proposed conditions hydrologic analysis consists of sub-watershed areas at each inlet structure of the development property. For each proposed watershed area, weighted curve numbers and times of concentration were calculated and utilized in the proposed conditions hydrologic model. The infiltration systems were also modeled to determine the effectiveness in reducing peak discharges from the site. **Table 2-2** below provides a summary of the peak discharges under existing and proposed conditions for the 2, 10, 25, 50, and 100 year storm events.

Table 2-2
Summary of Stormwater Peak Discharge (cfs)

		Storm Frequency (Years)						
Discharge Location	Condition	2	10	25	50	100		
	Existing	1.083	3.109	4.569	5.724	7.011		
Copts Brook (DP-A)	Proposed	1.044	2.888	4.203	5.239	6.398		
	% Reduction	-3.6%	-7.1%	-8.0%	-8.5%	-8.7%		
54" RCP	Existing	16.45	27.7	36.49	42.76	49.09		
Culvert	Proposed	15.38	27.64	35.87	42.12	49.08		
(DP-B)	% Reduction	-6.5%	-0.2%	-1.7%	-1.5%	0.0%		
	Existing	0.05	0.199	0.314	0.408	0.513		
Offsite Runoff (DP-C)	Proposed	0.039	0.138	0.212	0.272	0.339		
	% Reduction	-22.0%	-30.7%	-32.5%	-33.3%	-33.9%		

Table 2-3 provides a summary of the peak volumetric runoff under existing and proposed conditions for the 2, 10, 25, 50, and 100 year storm events.

Table 2-3
Summary of Stormwater Peak Discharge (cfs)

-		Storm Frequency (Years)						
Discharge Location	Condition	2	10	25	50	100		
	Existing	5,241	13,137	18,910	23,526	28,668		
Copts Brook (DP-A)	Proposed	4,941	12,129	17,344	21,499	26,117		
, ,	% Reduction	-5.7%	-7.7%	-8.3%	-8.6%	-8.9%		
54" RCP	Existing	59,393	112,913	147,095	172,958	200,754		
Culvert	Proposed	53,163	105,995	140,665	167,137	195,622		
(DP-B)	% Reduction	-10.5%	-6.1%	-4.4%	-3.4%	-2.6%		
	Existing	288	839	1,264	1,611	2,003		
Offsite Runoff (DP-C)	Proposed	160	442	655	827	1,022		
,	% Reduction	-44.4%	-47.3%	-48.2%	-48.7%	-49.0%		

The proposed conditions watershed map, curve number and time of concentration worksheets, and volumetric hydrographs are included in **Appendix D**.

2.2.2 Water Quality Volume

The design includes capturing and treating one-half inch of rainfall for the water quality volume to remove stormwater pollutants on an average annual basis.

Section 6(B)(i) of the Connecticut DEEP General Permit for the Discharge of Stormwater from Small Municipal Separate Storm Sewer Systems "MS4 General Permit" requires where an existing site exceeds 40 percent directly connected impervious area (DCIA), that one-half of the water quality volume is to be retained onsite. The Town of Wilton is registered under the MS4 General Permit (Registration #GSM000040), and therefore is subject to its provisions and requirements. The project site contains more than 40 percent directly connected impervious area. As a result, the standard for water quality treatment is one half of the water quality volume.

The infiltration systems have been designed to provide the required treatment volume. **Table 2-4** below summarizes the required and provided treatment volume for the site.

Table 2-4
Summary of Treatment Volume (cu ft)

Infiltration Cychon 1	Required Treatment Volume	749
Infiltration System - 1	Provided Treatment Volume	1,370
To filturation Constant	Required Treatment Volume	704
Infiltration System - 2	Provided Treatment Volume	1,022
To fill working County 2	Required Treatment Volume	1,265
Infiltration System - 3	Provided Treatment Volume	2,240
Indibuntion Cychon 4	Required Treatment Volume	308
Infiltration System - 4	Provided Treatment Volume	520
Indilbuntion Cychon F	Required Treatment Volume	1,442
Infiltration System - 5	Provided Treatment Volume	1,450
Infiltration System 6	Required Treatment Volume	1,349
Infiltration System - 6	Provided Treatment Volume	4,069

The water quality volume calculation sheets are included in **Appendix F**.

2.2.3 Hydraulic Capacity and Outlet Velocity

The stormwater collection system has been designed to convey the 25-year storm event as required by the CTDOT 2000 Drainage Manual. The system was designed by analyzing sub-areas corresponding to each inlet structure and calculating weighted runoff coefficients and times of concentration. The discharge from the six infiltration systems as well as the inlet flow for Copts Brook to the culvert are modeled as known constant flows, and do not take into account offsetting peaks between their respective hydrographs. Therefore, the analyzed flows within the piped drainage system are very conservative and the available capacity and hydraulic grade lines would only improve when accounting for the delayed time for flow in Copts Brook to peak. These values were entered into a storm sewers model using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3. Based upon this analysis, the proposed storm system has the capacity to convey the 25-year storm event. Hydraulic calculation worksheets and storm sewers output results are included in **Appendix E**.

2.3 Method of Hydrology and Hydraulic Analysis

The following storm drainage design criteria were used for all drainage pipe systems:

- 1. Design storm rainfall data from NOAA Atlas 14 Point Precipitation Frequency Estimates
- Piped storm drainage system and the outlets are designed for a 25-year storm event.
- 3. Minimum time of concentration = 5 minutes
- 4. For SCS peak flow calculations, Curve Number were as follows:
 - a. Impervious (Pavement/Roof Areas) = 98
 - b. Landscaped and Lawn Areas (HSG-B) = 69
 - c. Landscaped and Lawn Areas (HSG-D) = 84
 - d. Wooded Areas (HSG-B) = 55
 - e. Wooded Areas (HSG-D) = 77
- 5. For rational peak flow calculations, runoff coefficients were as follows:
 - a. Impervious (Pavement/Roof) areas = 0.90
 - b. Landscaped and Lawn Areas = 0.30
- 6. Minimum diameter of pipes = 12 inches, excluding roof leaders, underdrains, yard drains and foundation drains
- 7. Minimum pipe slope = 0.5 percent

- 8. Watershed areas delineated using polylines in AutoCAD Civil 3D 2018.
- 9. Comparative hydrology analyzed using Hydraflow Hydrographs Extension for AutoCAD Civil 3D 2018, Version 2018.3
- 10. Storm drainage system analyzed using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3

2.4 Best Management Practices

The stormwater management plan for the proposed site uses "Best Management Practices" (BMPs) to remove a high percentage of sediments in accordance with the Connecticut Department of Energy and Environmental Protection "Stormwater General Permit Criteria".

The BMPs include:

<u>Catch Basins and Yard Drains with Sumps and Bell Traps:</u> Catch basins and yard drains with sumps and bell traps collect sediment and prevent discharge of oil and other pollutants into the storm drainage system. All new catch basins and yard drains on-site will have 24-inch sumps with several also maintaining bell traps.

<u>Hydrodynamic Separators:</u> Hydrodynamic separators serve as pretreatment and prevent transport of oils and sediment further downstream. The proposed stormwater management system utilizes Contech CDS units prior to discharge into the underground infiltration systems. The Contech CDS units have been sized in accordance with the 2004 CTDEEP Stormwater Quality Manual. Sizing calculations are provided in **Appendix F.**

<u>Underground Infiltration</u>: Underground Infiltration serves as a primary treatment practice, reduces peak flow rates, and promotes groundwater recharge. The proposed stormwater management system utilizes plastic chambers surrounded by stone and filter fabric and an outlet control structure designed to attenuate peak flows.

<u>Level Spreader</u>: Level Spreaders serve as a secondary treatment practice that are utilized to reduce stormwater discharge velocities to non-erosive levels.

2.5 Pollutant Loading Analysis

Pollutant loadings for the existing and proposed conditions were calculated using the method prescribed by Debo and Reese in "Municipal Stormwater Management", 1995. This method determines the mass of pollutant loading by inputting the fraction of impervious area, the contributing area, the mean annual rainfall, and the event mean concentration of pollutant (EMC). The EMC is based upon the pollutant analyzed and the general characteristic of the contributing area – residential, commercial, or open space.

For the proposed conditions, the contributing area was further broken down into contributing areas to certain best management practices (BMPs). Pollutant loading reductions were taken at certain BMPs, depending upon the removal efficiency of the BMP as stated in the 2003 edition of Debo and Reese. Pollutant removal efficiencies for

proprietary products were taken from a report entitled "Final Report: Stormwater Treatment Devices Section 319 Project" submitted to the Connecticut Department of Environmental Protection, Bureau of Water Management by the University of Connecticut Department of Natural Resources Management and Engineering, April 15, 2002. This report provides results of field testing for pollutant removal on different types of proprietary stormwater treatment devices installed throughout the State of Connecticut. Based upon these pollutant reductions, we have determined that pollutant loadings will be less for the proposed conditions, as shown in **Table 2-5** below. The pollutant loading calculation sheets are included in **Appendix F**.

Table 2-5
Pollutant Loading Summary

	Pollutant						
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre-Treatment	lb/yr/1-in	2.534	0.511	134.694	0.192	0.044	0.180
Proposed, Post-Treatment	lb/yr/1-in	1.680	0.224	11.403	0.099	0.021	0.068
Reduction, Pre to Post Treat		34%	56%	92%	48%	52%	62%

2.6 Stormwater Maintenance and Inspection Schedule

Stormwater management systems require periodic maintenance to ensure they function as designed. The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, roof leaders, piping, hydrodynamic separators, underground infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures:</u> The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator:</u> The Contech CDS Units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand, and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration:</u> The underground infiltration system will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader:</u> The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plant species or tree saplings.

Stormwater System Outfalls: The stormwater system outfalls shall be inspected two times annually as well as after every major storm, for slope integrity, soil moisture, vegetated health, soil stability, soil compaction, soil erosion, ponding and sediment accumulation. If the rip rap has been displaced, undermined or damaged, it should be replaced immediately. The channel immediately below the outlet should be checked to see that erosion is not occurring. The downstream channel will be kept clear of obstructions, such as fallen trees, debris, leaves and sediment that could change flow patterns and/or tail water depths in pipes. Repairs must be carried out immediately to avoid additional damage to the outlet protection apron.

Maintenance & Inspection Forms are included in Appendix G.

Section 3 Floodplain Management & Hydraulics

3.0 Background

FEMA studied Copts Brook using approximate methods as a part of the Flood Insurance Study (FIS) for Fairfield County, dated June 18, 2010. Therefore, the entire length of the watercourse was assigned Zone A, with no defined base flood elevation or floodway.

3.1 Basis of Modeling

Since no detailed base flood elevations are available on Copts Brook, Tighe & Bond prepared a hydrologic study of the 435-acre watershed contributory to the 54-inch RCP inlet on the site. We utilized the HEC-HMS hydrologic model, which includes inputs for land coverage, basin area, time of concentration, travel time, and areas of storage. See **Appendix H** for further additional information.

We subdivided the watershed into three watershed subarea, and included two areas of storage. One located on-site immediately upstream of the 54-inch RCP inlet, and the area behind Wilton Acres Road, extending northeasterly to Clover Drive and Westport Road. Storage available on-site was computed using topographic survey data, while storage at Wilton Acres Road was determined using available LiDAR topographic data.

3.2 Flow Rates

Since the FIS did not study Copts Brook using detailed methods, there are no published discharges for the watercourse. The purpose of the hydrologic model was to develop a discharge for the 25- and 100-year events, as well as a corresponding water surface elevation at the inlet to the 54-inch RCP.

Table 3-1
Computed Flow Rates to the 54" RCP Inlet

Return Frequency (years)	Annual Chance Probability	Flow Rate (cfs)
25	4%	120.3
100	1%	163.1

3.3 Water Surface Elevations

We used the storage-discharge feature in concert with the incoming flow rate to develop water surface elevations at the 54-inch RCP inlet for the purposes of creating a base flood elevation for design purposes. **Table 3-2** summarizes the resulting water surface elevations for the 25-year and 100-year events:

Table 3-2
Computed Water Surface Elevations at the 54" RCP Inlet

Return Frequency (years)	Annual Chance Probability	WSEL (NAVD88)		
25	4%	137.9		
100	1%	139.6		

3.4 Compliance with Local Floodplain Regulations

Section 29-9.F.7 of the Wilton Zoning Regulations requires the following:

- k. Equal Conveyance: Within the floodplain, except those areas which are tidally influenced, as designated on the Flood Insurance Rate Map (FIRM) for the community, encroachments resulting from filling, new construction or substantial improvements involving an increase in footprint of the structure, are prohibited unless the applicant provides certification by a registered professional engineer demonstrating, with supporting hydrologic and hydraulic analyses performed in accordance with standard engineering practice, that such encroachments shall not result in any (0.00 feet) increase in flood levels (base flood elevation). Work within the floodplain and the land adjacent to the floodplain, including work to provide compensatory storage shall not be constructed in such a way so as to cause an increase in flood stage or flood velocity.
- I. Compensatory Storage: The water holding capacity of the floodplain, except those areas which are tidally influenced, shall not be reduced. Any reduction caused by filling, new construction or substantial improvements involving an increase in footprint to the structure, shall be compensated for by deepening and/or widening of the floodplain, storage shall be provided on-site, unless easements have been gained from adjacent property owners; it shall be provided within the same hydraulic reach and a volume not previously used for flood storage; it shall be hydraulically comparable and incrementally equal to the theoretical volume of flood water at each elevation, up to and including the 100-year flood elevation, which would be displaced by the proposed project. Such compensatory volume shall have an unrestricted hydraulic connection to the same waterway or water body. Compensatory storage can be provided off-site if approved by the municipality.

3.4.1 Equal Conveyance

The proposal does not diminish floodplain storage, and therefore base flood elevations will not increase as a result of the proposal. The additional floodplain storage provided would have the effect of reducing base flood elevations by a de minimis amount.

3.4.2 Compensatory Storage

The footprint for Building 4 is proposed to be within the existing paved parking lot immediately west of Copts Brook. This area is also within the calculated floodplain for Copts Brook. In order to mitigate the impacts of the proposed development, the residential portion of the building which extends over the floodplain will be elevated on

columns to allow potential floodwaters to go under the building while allowing the garage portion outside the floodplain to remain at grade. Since the placement of building columns and a retaining wall within the floodplain would result in a loss of floodplain storage volume, we have proposed revised grading beneath the building footprint to provide additional flood storage. The grading as proposed results in a net cut of approximately 250 CF within the floodplain boundary, compensating for the approximately 40 CF occupied by the columns and retaining walls of the proposed building. The development plan as proposed would therefore increase floodplain storage on-site. Provided in **Table 3-3** below is a summary of the Compensatory Flood Storage volumes being proposed for Copts Brook.

Table 3-3
Compensatory Flood Storage (NAVD88)

	100-year Water Surface Elevation (NAVD88)						
Elevation (NAVD88)	Existing (CF)	Proposed (CF)	Difference (CF)				
134.0	-	-	-				
135.0	1,112	1,112	0				
136.0	2,707	2,707	0				
137.0	4,910	4,910	0				
138.0	8,101	8,101	0				
139.0	12,633	12,633	0				
140.0	19,028	19,278	250				

Section 4 Site Utility Services

4.1 Water and Fire Protection Services

Water and fire protection services to the site will be provided by The Aquarion Water Company (Aquarion). Services to the proposed buildings will be fed from the reported 12-inch main located in Danbury Road. An existing hydrant is located just north of the site on Danbury Road and a second hydrant is located just south of the main entry to the site. In addition, two new hydrants are proposed within the site to service the proposed development.

The estimated daily water demand for the proposed residential development is approximately 24,300 gallons per day (GPD). The estimated peak hour demand is 68 gallons per minute (GPM), determined using a maximum-to-average-day ratio of 4.0.

4.2 Electric and Tel-Data Service

Electric service to the site is provided by Eversource Electric Company and telephone and cable are provided by Altice and Frontier. Underground primary service lines are located within the main entry loop driveway with an existing electric vault located near the southeastern corner of the existing building.

4.3 Gas Service

Eversource Gas Company provides natural gas service to the site. Eversource Gas Company maintains a gas main in Danbury Road and a service lateral to 60 Danbury Road thru the easement in the main entry loop. The current development plan shows the replacement of the existing gas service lateral within the Eversource easement; however, once service loads are better understood the existing lateral will be evaluated to determine if it can be re-used to service the entire development area.

Furthermore, once the estimated peak demand for the total project is determined, Eversource Gas Company will provide a letter of service availability.

4.4 Sanitary Sewer Service

The project site is located within the Wilton WPCA Sewershed.

Based on available Town maps, there is a 24-inch gravity sanitary sewer located in Danbury Road. The proposed development will connect to the sewer main at the existing manhole in front of the site. WPCA approval will be required for all sewer connections.

The projected wastewater flows associated with the proposed development were calculated based on the 93 residential units – comprised of 31 one-bedroom units, 55 two-bedroom units, and 7 three-bedroom units – for a total of 162 bedrooms and a flow rate of 150 gallons per day (GPD) per bedroom. A peaking factor of 4 was applied to the average daily flows to estimate peak flows. **Table 4-1** below summarizes the projected average and peak daily sanitary sewer flows for the site.

Table 4-1 - Projected Average and Peak Daily Sanitary Sewer Flows

Wastewater Requirements								
Development		Design	Criteria	Average	Peak Flow			
Use	Units / Bedrooms	GPD	Unit	Daily Flow (GPD)	(GPM)*			
Residential	93 / 162	150	Per Bedroom	24,300	68			

^{*} Peak factor of 4 was applied to average daily flows to estimate peak flows; New England Interstate Water Pollution Control Commission, 2011.

Section 5 Soil Erosion and Sedimentation Control

5.1 SESC Narrative

General

The proposed development is entitled "64 Danbury Road" in Wilton, Connecticut.

Estimated:

Project Start: Spring 2024

Project Completion: Summer 2026

Erosion Control Narrative refers to drawings C-501 through C-504.

The proposed site development will consist of building demolition, clearing and grubbing the existing site, excavation, construction of stormwater management, utilities, and rough grading of building, parking areas, sidewalks and curbing.

The development is located on Danbury Road in Wilton, Connecticut.

The stormwater management measures will address the stormwater quality once the site has been constructed and stabilized. Sedimentation and erosion control measures will be installed during construction which will minimize adverse impacts from construction activities.

All sedimentation and erosion control measures proposed for this development have been designed in accordance with the "2024 Connecticut Guidelines for Soil Erosion and Sedimentation Control" as published by the Connecticut Council on Soil Erosion and Water Conservation. Additional guidelines have also been followed that are available from the Connecticut Department of Environmental Protection as recommended for sedimentation control during construction activities.

Construction Sequence – Initial Phase

- 1. Conduct a pre-construction meeting with the Owner or Owner's Representative, Town Engineer, Design Engineer, Site Engineer, Contractor and Site Superintendent to establish the limits of construction, construction procedures and material stockpile areas.
- Field stake the limits of construction.
- 3. Install all applicable soil and erosion control measures around the perimeter of the site to the extent possible. this will include siltation fence around the project as shown on the plans.
- 4. Install construction access road and anti-tracking pavement in the areas as shown on the plans. All construction access shall be into the site through the anti-tracking pads.

- 5. Establish temporary staging area.
- 6. Begin building demolition and pavement removal.
- 7. Construct the initial storm drainage as shown on the drainage plans.
- 8. Install water quality systems and associated drainage network to the maximum extent practicable. Grade the area around the storm drainage system as necessary.
- 9. Begin rough roadway grading.
- 10. Install remaining drainage system to the extent necessary to provide positive drainage.
- 11. Begin installation of sanitary sewer system, water, and other utilities to extent necessary.
- 12. Provide silt fence/haybale barrier around soil stockpile area. Provide temporary vegetative cover (defined in erosion control notes) on all exposed surfaces.
- 13. Begin building construction.
- 14. Pave binder course on parking and driveways for non-porous pavement areas.
- 15. Establish temporary vegetative cover.

Construction Sequence – Final Phase

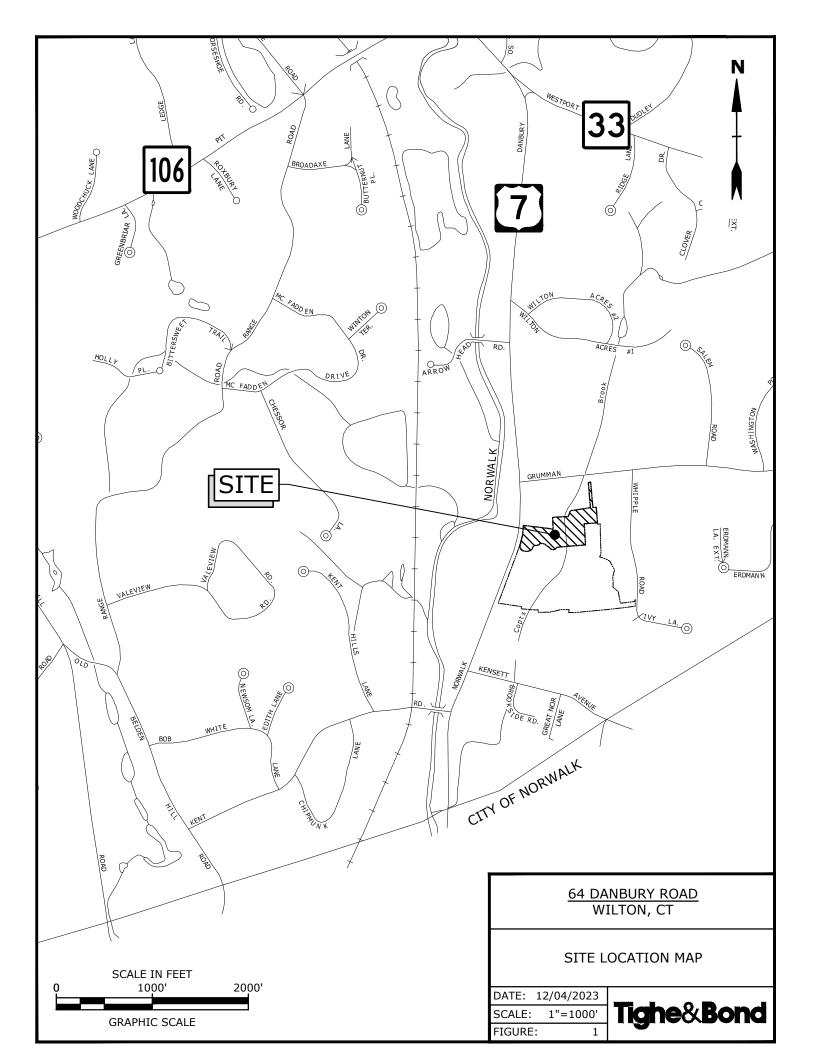
- 1. Repair perimeter sediment & erosion controls as needed.
- 2. Clean/replace controls from previous phase as needed.
- 3. Fine grade site.
- 4. Continue construction of building.
- 5. Complete construction of sidewalks.
- 6. Establish final vegetative cover and landscaping.
- 7. Pave surface course on roadways.
- 8. Remove erosion controls when site is stabilized.

5.2 Soil Erosion and Sedimentation Control Notes

- All sedimentation and erosion control measures shall be constructed in accordance with the standards and specifications of the "2024 Connecticut Guidelines for Soil Erosion and Sediment Control", DEP Bulletin No. 34, and all amendments and addenda thereto as published by the Connecticut Department of Environmental Protection.
- 2. Land disturbance shall be kept to the minimum necessary for construction operations.
- 3. All erosion control measures shall be installed as shown on the plan and elsewhere as ordered by the engineer.
- 4. All catch basins shall be protected with a silt sacks, haybale ring, silt fence or block and stone inlet protection throughout the construction period and until all disturbed areas are thoroughly stabilized.
- 5. Whenever possible, erosion and sediment control measures shall be installed prior to construction. See "Erosion Control Narrative".
- 6. Additional control measures shall be installed during the construction period as ordered by the engineer.
- 7. All sedimentation and erosion control measures shall be maintained in effective condition throughout the construction period.
- 8. Sediment removed shall be disposed of offsite or in a manner as required by the Engineer.
- 9. The construction contractor shall be responsible for construction and maintenance of all control measures throughout the construction period.
- 10. All disturbed areas to be left exposed for more than 30 days shall be protected with a temporary vegetative cover. Seed these areas with perennial ryegrass at the rate of 40 lbs. per acre (1 lb. per 1,000 sq. ft). Apply soil amendments and mulch as required to establish a uniform stand of vegetation over all disturbed areas.
- 11. The construction contractor shall utilize approved methods/materials for preventing the blowing and movement of dust from exposed soil surfaces onto adjacent properties and site areas.
- 12. The construction contractor shall maintain a supply of silt fence/haybales and antitracking crushed stone on site for emergency repairs.
- 13. All drainage structures shall be periodically inspected weekly by the construction contractor and cleaned to prevent the build-up of silt.
- 14. The construction contractor shall carefully coordinate the placement of erosion control measures with the phasing of construction.
- 15. Keep all paved surfaces clean. Sweep and scrape before forecasted storms.

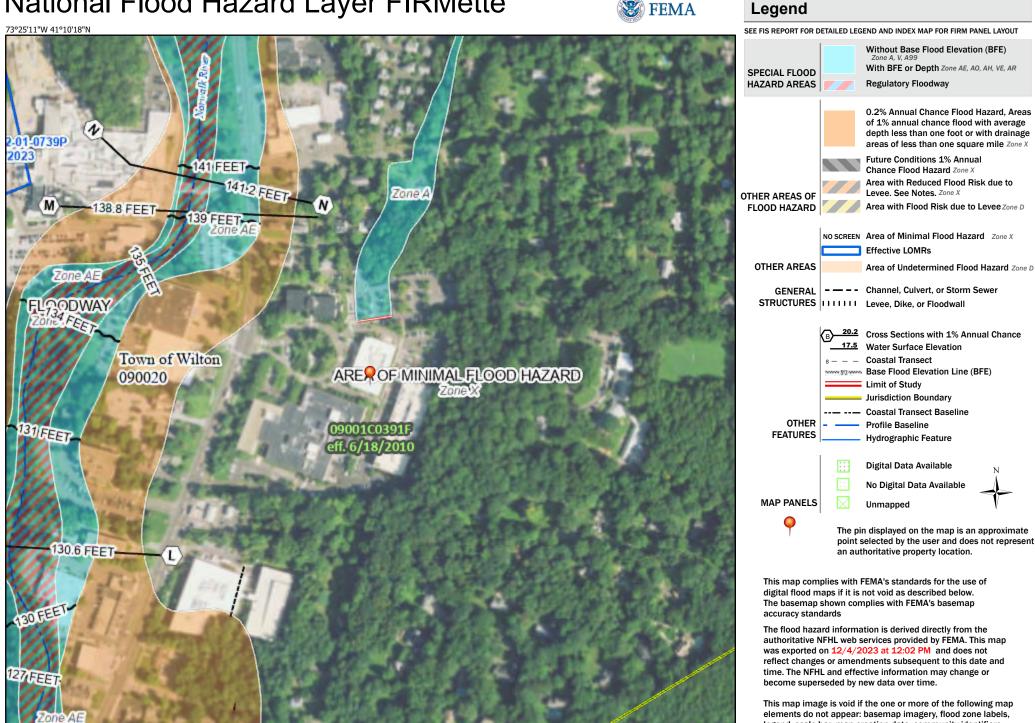
- 16. Treat all unpaved surface with 4" minimum of topsoil prior to final stabilization.
- 17. Haybale barriers and silt fencing shall be installed along the toe of critical cut and fill slopes.
- 18. The contractor shall notify the Town officials prior to the installation of erosion controls, cutting of trees, or any excavation.
- 19. All trucks leaving the site must be covered.
- 20. Some control measures are permanent. These structures shall be cleaned and replenished at the end of construction. locations of the permanent control structures are shown on the drainage plans.
- 21. All sedimentation and erosion controls shall be checked weekly and/or after each rain fall event. Necessary repairs shall be made without delay.
- 22. Prior to any forecasted rainfall, erosion and sediment controls shall be inspected and repaired as necessary.
- 23. After all disturbed areas have been stabilized, erosion controls may be removed once authorization to do so has been secured from the Owner. Disturbed areas shall be seeded and mulched.
- 24. All embankment slopes 3:1 or greater to be stabilized with erosion control blanket, North American Green SC150BN or approved equivalent, unless otherwise noted on plans.

APPENDIX A



National Flood Hazard Layer FIRMette





Feet

2,000

250

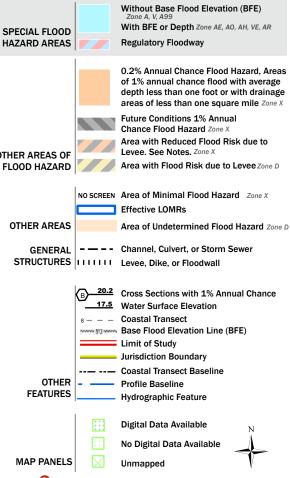
500

1,000

1.500

1:6,000

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

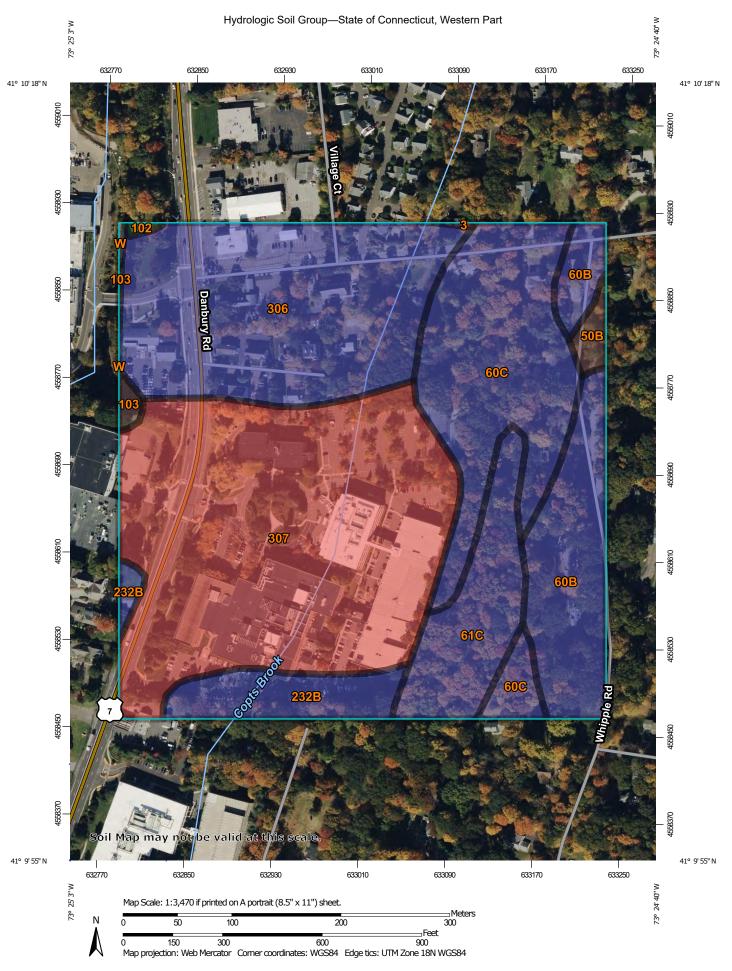


This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 12/4/2023 at 12:02 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

APPENDIX B



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:12.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: State of Connecticut, Western Part Survey Area Data: Version 1, Sep 15, 2023 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Oct 21, 2022—Oct 27. 2022 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	0.0	0.0%
50B	Sutton fine sandy loam, 3 to 8 percent slopes	B/D	0.4	0.9%
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes		5.4	10.6%
60C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes	В	8.4	16.7%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	В	3.8	7.4%
102	Pootatuck fine sandy loam	A/D	0.1	0.1%
103	Rippowam fine sandy loam	B/D	0.2	0.5%
232B	Haven-Urban land complex, 0 to 8 percent slopes	В	2.5	4.9%
306	Udorthents-Urban land complex	В	11.3	22.4%
307	Urban land	D	18.4	36.3%
W	Water		0.0	0.1%
Totals for Area of Inter	rest		50.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



NOAA Atlas 14, Volume 10, Version 3 Location name: Wilton, Connecticut, USA* Latitude: 41.1679°, Longitude: -73.4146° Elevation: 141 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

D				Average	recurrence	interval (ye	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.365 (0.286-0.461)	0.425 (0.333-0.537)	0.523 (0.408-0.663)	0.604 (0.468-0.770)	0.716 (0.536-0.946)	0.801 (0.586-1.08)	0.888 (0.629-1.23)	0.981 (0.662-1.40)	1.11 (0.719-1.63)	1.21 (0.766-1.82
10-min	0.518 (0.405-0.654)	0.602 (0.471-0.761)	0.740 (0.577-0.938)	0.855 (0.664-1.09)	1.01 (0.759-1.34)	1.14 (0.831-1.53)	1.26 (0.892-1.75)	1.39 (0.938-1.98)	1.57 (1.02-2.31)	1.71 (1.08-2.57
15-min	0.609 (0.477-0.769)	0.709 (0.555-0.896)	0.872 (0.680-1.10)	1.01 (0.781-1.28)	1.19 (0.894-1.58)	1.34 (0.977-1.80)	1.48 (1.05-2.06)	1.64 (1.10-2.33)	1.85 (1.20-2.72)	2.02 (1.28-3.03
30-min	0.849 (0.665-1.07)	0.987 (0.772-1.25)	1.21 (0.946-1.54)	1.40 (1.08-1.78)	1.66 (1.24-2.19)	1.86 (1.36-2.49)	2.06 (1.45-2.84)	2.26 (1.53-3.22)	2.53 (1.64-3.73)	2.74 (1.74-4.12
60-min	1.09 (0.853-1.38)	1.26 (0.990-1.60)	1.55 (1.21-1.97)	1.79 (1.39-2.28)	2.12 (1.59-2.80)	2.38 (1.74-3.19)	2.63 (1.85-3.63)	2.88 (1.95-4.11)	3.22 (2.09-4.73)	3.47 (2.20-5.20
2-hr	1.39 (1.10-1.75)	1.64 (1.29-2.06)	2.05 (1.61-2.59)	2.39 (1.87-3.03)	2.86 (2.16-3.76)	3.22 (2.37-4.31)	3.58 (2.56-4.96)	3.98 (2.70-5.64)	4.54 (2.96-6.64)	4.99 (3.17-7.44
3-hr	1.60 (1.26-2.00)	1.90 (1.50-2.38)	2.39 (1.88-3.00)	2.80 (2.20-3.54)	3.37 (2.55-4.42)	3.79 (2.81-5.08)	4.24 (3.04-5.86)	4.74 (3.21-6.69)	5.45 (3.55-7.94)	6.03 (3.84-8.96
6-hr	2.01 (1.60-2.50)	2.41 (1.92-2.99)	3.06 (2.42-3.81)	3.60 (2.83-4.51)	4.34 (3.30-5.67)	4.90 (3.65-6.52)	5.48 (3.97-7.57)	6.16 (4.20-8.65)	7.15 (4.68-10.4)	7.98 (5.09-11.8)
12-hr	2.48 (1.99-3.06)	2.99 (2.39-3.69)	3.80 (3.03-4.71)	4.48 (3.55-5.58)	5.42 (4.15-7.04)	6.12 (4.59-8.11)	6.86 (4.99-9.42)	7.72 (5.28-10.8)	8.99 (5.90-12.9)	10.0 (6.43-14.7
24-hr	2.90 (2.34-3.55)	3.52 (2.84-4.32)	4.54 (3.64-5.58)	5.38 (4.29-6.66)	6.54 (5.05-8.45)	7.41 (5.59-9.77)	8.34 (6.11-11.4)	9.43 (6.47-13.1)	11.1 (7.28-15.8)	12.4 (7.99-18.1
2-day	3.20 (2.60-3.90)	3.97 (3.22-4.83)	5.21 (4.21-6.36)	6.24 (5.01-7.67)	7.67 (5.95-9.86)	8.72 (6.63-11.5)	9.86 (7.29-13.5)	11.2 (7.74-15.5)	13.4 (8.83-19.0)	15.2 (9.78-22.0
3-day	3.44 (2.80-4.17)	4.28 (3.48-5.19)	5.65 (4.58-6.87)	6.78 (5.46-8.29)	8.34 (6.50-10.7)	9.50 (7.24-12.4)	10.8 (7.98-14.7)	12.3 (8.47-16.8)	14.6 (9.68-20.7)	16.7 (10.7-24.0
4-day	3.67 (3.00-4.44)	4.56 (3.72-5.51)	6.00 (4.88-7.28)	7.20 (5.81-8.78)	8.85 (6.91-11.3)	10.1 (7.70-13.1)	11.4 (8.46-15.5)	13.0 (8.98-17.8)	15.5 (10.2-21.8)	17.6 (11.3-25.2
7-day	4.36 (3.58-5.24)	5.33 (4.37-6.41)	6.90 (5.64-8.32)	8.20 (6.66-9.94)	10.0 (7.83-12.7)	11.3 (8.68-14.7)	12.8 (9.48-17.1)	14.5 (10.0-19.6)	17.0 (11.3-23.8)	19.1 (12.4-27.3
10-day	5.05 (4.16-6.04)	6.06 (4.99-7.26)	7.71 (6.32-9.27)	9.09 (7.40-11.0)	11.0 (8.61-13.8)	12.4 (9.50-15.9)	13.9 (10.3-18.5)	15.6 (10.9-21.1)	18.1 (12.1-25.3)	20.2 (13.1-28.8
20-day	7.12 (5.91-8.47)	8.26 (6.84-9.82)	10.1 (8.34-12.1)	11.6 (9.54-14.0)	13.8 (10.8-17.1)	15.4 (11.8-19.5)	17.0 (12.6-22.3)	18.8 (13.2-25.2)	21.2 (14.2-29.4)	23.2 (15.1-32.7
30-day	8.85 (7.36-10.5)	10.1 (8.37-11.9)	12.1 (9.99-14.3)	13.7 (11.3-16.4)	16.0 (12.6-19.8)	17.8 (13.7-22.3)	19.5 (14.4-25.3)	21.3 (15.0-28.5)	23.7 (15.9-32.7)	25.5 (16.6-36.0
45-day	11.0 (9.18-13.0)	12.3 (10.3-14.5)	14.5 (12.0-17.1)	16.3 (13.4-19.4)	18.7 (14.8-23.0)	20.7 (15.9-25.8)	22.6 (16.7-29.0)	24.4 (17.2-32.4)	26.8 (18.0-36.8)	28.5 (18.6-39.9
60-day	12.8 (10.7-15.0)	14.2 (11.9-16.7)	16.5 (13.7-19.5)	18.4 (15.2-21.8)	21.0 (16.7-25.7)	23.1	25.0	26.9	29.3	31.0

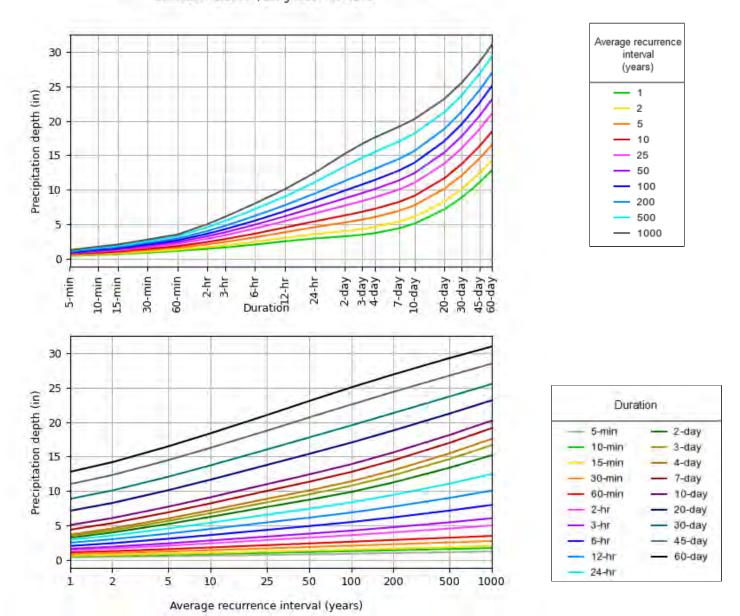
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 41.1679°, Longitude: -73.4146°



NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Wed Dec 20 14:31:53 2023

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Maps & aerials

Small scale terrain



NOAA Atlas 14, Volume 10, Version 3 Location name: Wilton, Connecticut, USA* Latitude: 41.1679°, Longitude: -73.4146° Elevation: 141 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/ho										
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	4.38 (3.43-5.53)	5.10 (4.00-6.44)	6.28 (4.90-7.96)	7.25 (5.62-9.24)	8.59 (6.43-11.4)	9.61 (7.03-12.9)	10.7 (7.55-14.8)	11.8 (7.94-16.8)	13.3 (8.63-19.6)	14.5 (9.19-21.8)
10-min	3.11 (2.43-3.92)	3.61 (2.83-4.57)	4.44 (3.46-5.63)	5.13 (3.98-6.54)	6.08 (4.55-8.04)	6.81 (4.99-9.16)	7.55 (5.35-10.5)	8.34 (5.63-11.9)	9.43 (6.11-13.9)	10.3 (6.51-15.4)
15-min	2.44 (1.91-3.08)	2.84 (2.22-3.58)	3.49 (2.72-4.42)	4.03 (3.12-5.13)	4.77 (3.58-6.31)	5.34 (3.91-7.18)	5.92 (4.20-8.22)	6.54 (4.42-9.32)	7.39 (4.80-10.9)	8.07 (5.10-12.1)
30-min	1.70 (1.33-2.14)	1.97 (1.54-2.50)	2.42 (1.89-3.07)	2.80 (2.17-3.57)	3.31 (2.48-4.37)	3.71 (2.71-4.98)	4.11 (2.90-5.68)	4.52 (3.05-6.44)	5.07 (3.29-7.46)	5.48 (3.47-8.23)
60-min	1.09 (0.853-1.38)	1.26 (0.990-1.60)	1.55 (1.21-1.97)	1.79 (1.39-2.28)	2.12 (1.59-2.80)	2.38 (1.74-3.19)	2.63 (1.85-3.63)	2.88 (1.95-4.11)	3.22 (2.09-4.73)	3.47 (2.20-5.20)
2-hr	0.696 (0.549-0.873)	0.821 (0.647-1.03)	1.03 (0.805-1.29)	1.20 (0.933-1.52)	1.43 (1.08-1.88)	1.61 (1.18-2.16)	1.79 (1.28-2.48)	1.99 (1.35-2.82)	2.27 (1.48-3.32)	2.49 (1.58-3.72)
3-hr	0.532 (0.421-0.665)	0.632 (0.500-0.791)	0.797 (0.627-1.00)	0.933 (0.730-1.18)	1.12 (0.848-1.47)	1.26 (0.935-1.69)	1.41 (1.01-1.95)	1.58 (1.07-2.23)	1.81 (1.18-2.64)	2.01 (1.28-2.98)
6-hr	0.335 (0.267-0.416)	0.402 (0.319-0.499)	0.510 (0.404-0.636)	0.600 (0.473-0.752)	0.724 (0.551-0.946)	0.817 (0.609-1.09)	0.915 (0.662-1.26)	1.03 (0.701-1.44)	1.19 (0.781-1.73)	1.33 (0.849-1.96)
12-hr	0.206 (0.165-0.254)	0.247 (0.198-0.305)	0.315 (0.251-0.391)	0.372 (0.294-0.463)	0.449 (0.344-0.583)	0.507 (0.380-0.672)	0.569 (0.414-0.782)	0.641 (0.438-0.893)	0.746 (0.489-1.07)	0.834 (0.533-1.22)
24-hr	0.120 (0.097-0.148)	0.146 (0.118-0.180)	0.189 (0.151-0.232)	0.224 (0.178-0.277)	0.272 (0.210-0.352)	0.308 (0.233-0.407)	0.347 (0.254-0.475)	0.392 (0.269-0.544)	0.461 (0.303-0.659)	0.518 (0.332-0.755)
2-day	0.066 (0.054-0.081)	0.082 (0.066-0.100)	0.108 (0.087-0.132)	0.130 (0.104-0.159)	0.159 (0.123-0.205)	0.181 (0.138-0.238)	0.205 (0.151-0.280)	0.234 (0.161-0.322)	0.278 (0.183-0.395)	0.316 (0.203-0.457)
3-day	0.047 (0.038-0.057)	0.059 (0.048-0.072)	0.078 (0.063-0.095)	0.094 (0.075-0.115)	0.115 (0.090-0.148)	0.131 (0.100-0.172)	0.149 (0.110-0.203)	0.170 (0.117-0.233)	0.203 (0.134-0.287)	0.231 (0.149-0.333)
4-day	0.038 (0.031-0.046)	0.047 (0.038-0.057)	0.062 (0.050-0.075)	0.075 (0.060-0.091)	0.092 (0.071-0.117)	0.104 (0.080-0.136)	0.118 (0.088-0.161)	0.135 (0.093-0.185)	0.161 (0.106-0.227)	0.183 (0.118-0.262)
7-day	0.025 (0.021-0.031)	0.031 (0.025-0.038)	0.041 (0.033-0.049)	0.048 (0.039-0.059)	0.059 (0.046-0.075)	0.067 (0.051-0.087)	0.075 (0.056-0.102)	0.086 (0.059-0.116)	0.101 (0.067-0.141)	0.113 (0.073-0.162)
10-day	0.021 (0.017-0.025)	0.025 (0.020-0.030)	0.032 (0.026-0.038)	0.037 (0.030-0.045)	0.045 (0.035-0.057)	0.051 (0.039-0.066)	0.057 (0.042-0.077)	0.065 (0.045-0.088)	0.075 (0.050-0.105)	0.084 (0.054-0.119)
20-day	0.014 (0.012-0.017)	0.017 (0.014-0.020)	0.021 (0.017-0.025)	0.024 (0.019-0.029)	0.028 (0.022-0.035)	0.032 (0.024-0.040)	0.035 (0.026-0.046)	0.039 (0.027-0.052)	0.044 (0.029-0.061)	0.048 (0.031-0.068)
30-day	0.012 (0.010-0.014)	0.013 (0.011-0.016)	0.016 (0.013-0.019)	0.019 (0.015-0.022)	0.022 (0.017-0.027)	0.024 (0.018-0.031)	0.027 (0.020-0.035)	0.029 (0.020-0.039)	0.032 (0.022-0.045)	0.035 (0.023-0.049)
45-day	0.010 (0.008-0.011)	0.011 (0.009-0.013)	0.013 (0.011-0.015)	0.015 (0.012-0.017)	0.017 (0.013-0.021)	0.019 (0.014-0.023)	0.020 (0.015-0.026)	0.022 (0.015-0.030)	0.024 (0.016-0.034)	0.026 (0.017-0.036)
60-day	0.008 (0.007-0.010)	0.009 (0.008-0.011)	0.011 (0.009-0.013)	0.012 (0.010-0.015)	0.014 (0.011-0.017)	0.016 (0.012-0.019)	0.017 (0.012-0.022)	0.018 (0.013-0.024)	0.020 (0.013-0.027)	0.021 (0.014-0.030)

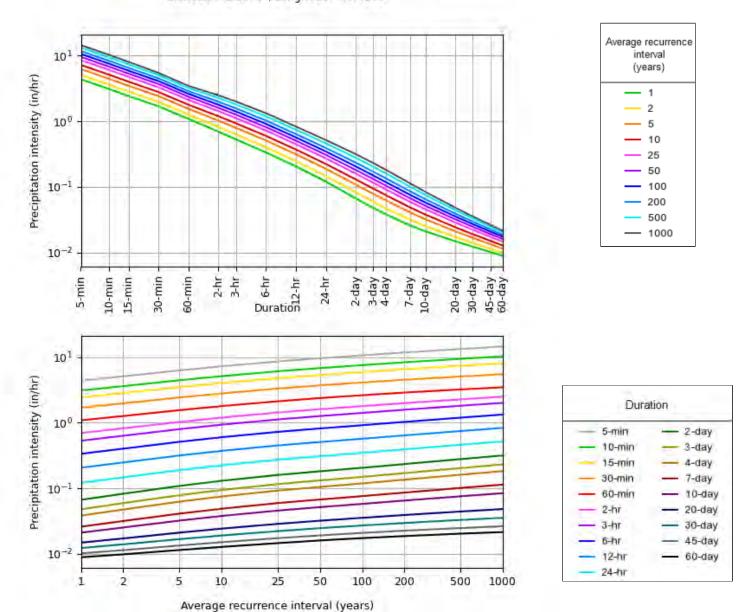
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based intensity-duration-frequency (IDF) curves Latitude: 41.1679°, Longitude: -73.4146°



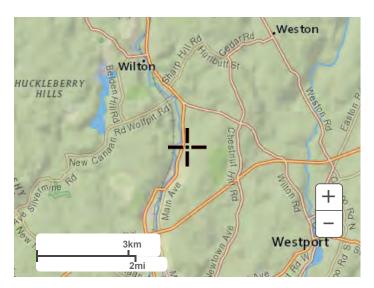
NOAA Atlas 14, Volume 10, Version 3

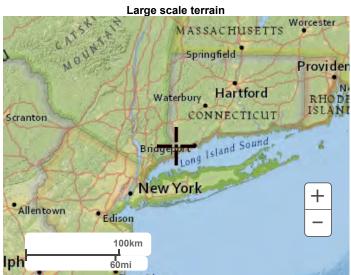
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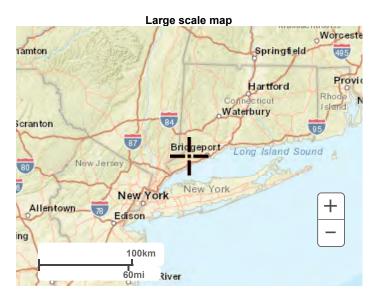
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Maps & aerials

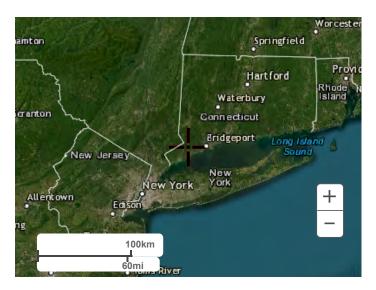
Small scale terrain







Large scale aerial



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National Weather Service
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<u>Disclaimer</u>

APPENDIX C



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: **EX WS-01**

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.091	98	8.8866
Landscaped and Lawns (HSG-B)	0.622	69	42.8858
Landscaped and Lawns (HSG-D)	0.080	84	6.6818
Wooded (HSG-B)	0.916	55	50.3750
Wooded (HSG-D)	0.235	77	18.0621
	1.942		126.891

Weighted CN: 65

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	225	0.2	16.11

Total Tc = 16.1 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: EX WS-02A

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.906	98	88.7872
Landscaped and Lawns (HSG-B)	0.154	69	10.6367
Landscaped and Lawns (HSG-D)	0.138	84	11.5895
Wooded (HSG-B)	0.350	55	19.2753
Wooded (HSG-D)	0.129	77	9.9414
	1.678		140.230

Weighted CN: 84

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.4	10	0.02	3.35	
Segment B - C	0.24	84	0.02	12.22	
Segment C - D	0.015	67	0.033	0.91	

Total Tc = 16.5 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: EX WS-02B

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.006	98	0.5917
Landscaped and Lawns (HSG-B)	0.005	69	0.3738
Landscaped and Lawns (HSG-D)	0.120	84	10.0545
Wooded (HSG-B)	0.029	55	1.6061
Wooded (HSG-D)	0.025	77	1.9604
,	0.186		14.586

Weighted CN: 79

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	84	0.072	11.02

Total Tc = 11.0 Min.

Gutter and pipe time of concentration computed using Manning's equation

Designation: EX WS-02C

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.391	98	38.3293
Landscaped and Lawns (HSG-D)	0.199	84	16.7287
	0.590		55.058

Weighted CN: 93

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	108	0.08	8.58
Segment B - C	0.015	82	0.067	0.80

Total Tc = 9.4 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: EX WS-02D

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	1.683	98	164.9397
Landscaped and Lawns (HSG-D)	0.313	84	26.3300
Wooded (HSG-B)	0.231	55	12.7096
Wooded (HSG-D)	0.018	77	1.3823
	2.246		205.362

Weighted CN: 91

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	52	0.11	6.34
Segment B - C	0.24	65	0.17	4.23
Segment C - D	0.015	43	0.045	0.56

Total Tc = 11.1 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: **EX WS-02E**

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.126	98	12.3580
Landscaped and Lawns (HSG-D)	0.020	84	1.6430
	0.146		14.001

Weighted CN: 96

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min					
Segment A - B	0.24	6	0.02	1.48	
Segment B - C	0.015	94	0.01	1.92	

Total Tc = 3.4 Min.

USE 5.0 Min. (MIN)

Note: Overland time of concentration computed using "Kinematic Wave" equation



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: EX WS-02F

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.704	98	68.9667
Landscaped and Lawns (HSG-D)	0.274	84	23.0229
Wooded (HSG-D)	0.034	77	2.6356
	1.012		94.625

Weighted CN: 93

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	35	0.025	5.55

Total Tc = 5.5 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: EX WS-02G

Location:

Note:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.159	98	15.5459
Landscaped and Lawns (HSG-D)	0.124	84	10.3997
	0.282		25.946

Weighted CN: 92

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	46	0.025	6.91

Total Tc = 6.9 Min.

Overland time of concentration computed using "Kinematic Wave" equation



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: EX WS-02H

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.166	98	16.2591
Landscaped and Lawns (HSG-D)	0.450	84	37.8309
	0.616		54.090

Weighted CN: 88

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	65	0.025	9.11
Segment B - C	0.015	6	0.02	0.16
Segment C - D	0.25	53	0.025	7.99

Total Tc = 17.3 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: **EX WS-02I**

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.577	98	56.5165
Landscaped and Lawns (HSG-D)	0.810	84	68.0311
	1.387		124.548

Weighted CN: 90

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	82	0.06	7.73
Segment B - C	0.015	6	0.02	0.16
Segment C - D	0.25	97	0.04	10.74

Total Tc = 18.6 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation



Description: Existing CN & Tc Calculations
Prepared By: AVC Date: December 4, 2023

Designation: EX WS-02J

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.343	98	33.5756
	0.343		33.576

Weighted CN: 98

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	75	0.02	1.21

Total Tc = 1.2 Min. USE 5.0 Min. (MIN)

Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: EX WS-03

Location:

Note:

Cover Type	Area, ac	CN	A x CN
Landscaped and Lawns (HSG-B)	0.043	69	2.9542
Wooded (HSG-B)	0.111	55	6.0909
	0.154		9.045

Weighted CN: 59

Time of Concentration

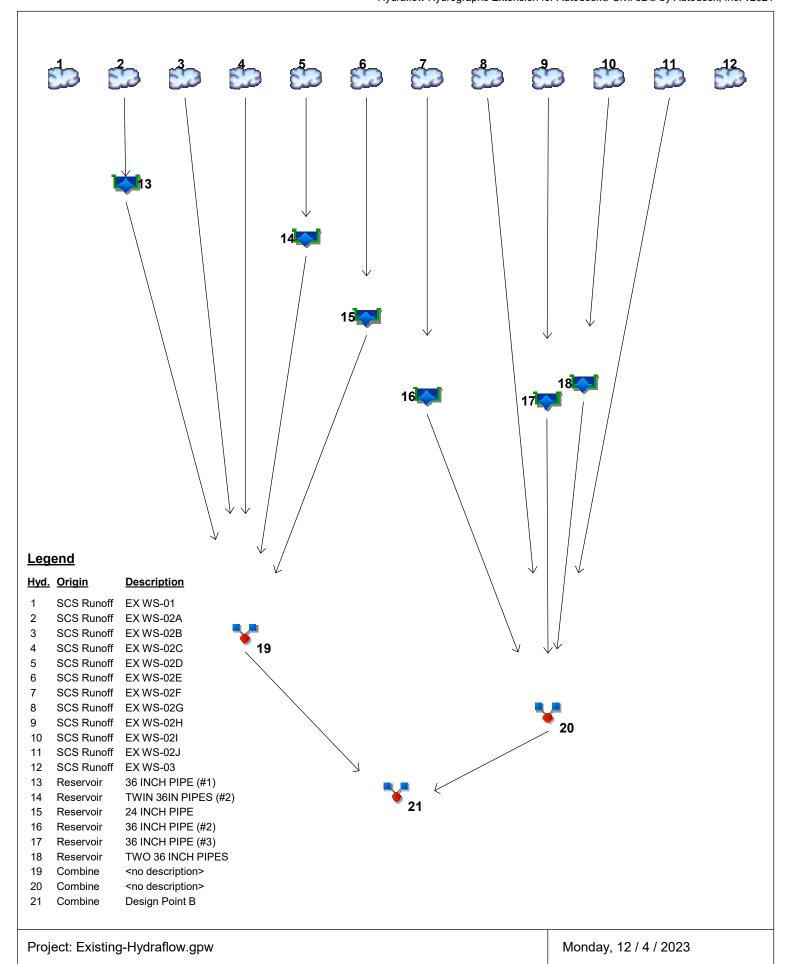
(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min.					
Segment A - B	0.4	25	0.08	4.01	
Segment B - C	0.24	60	0.05	6.47	

Total Tc = 10.5 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Watershed Model Schematic



Hydrograph Return Period Recap

lyd.	Hydrograph	Inflow		Peak Outflow (cfs)							Hydrograph
0.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			1.083			3.109	4.569	5.724	7.011	EX WS-01
2	SCS Runoff			2.850			5.245	6.758	7.893	9.103	EX WS-02A
3	SCS Runoff			0.283			0.569	0.755	0.895	1.046	EX WS-02B
4	SCS Runoff			1.664			2.685	3.315	3.785	4.285	EX WS-02C
5	SCS Runoff			5.519			9.148	11.39	13.06	14.84	EX WS-02D
6	SCS Runoff			0.468			0.731	0.894	1.015	1.145	EX WS-02E
7	SCS Runoff			3.039			4.896	6.042	6.897	7.807	EX WS-02F
8	SCS Runoff			0.774			1.265	1.567	1.793	2.033	EX WS-02G
)	SCS Runoff			1.152			1.996	2.521	2.913	3.330	EX WS-02H
10	SCS Runoff			2.779			4.677	5.852	6.727	7.659	EX WS-02I
11	SCS Runoff			1.132			1.741	2.120	2.404	2.707	EX WS-02J
12	SCS Runoff			0.050			0.199	0.314	0.408	0.513	EX WS-03
13	Reservoir	2		2.833			5.228	6.739	7.874	8.866	36 INCH PIPE (#1)
14	Reservoir	5		5.358			8.916	11.13	12.78	14.56	TWIN 36IN PIPES (#2)
15	Reservoir	6		0.449			0.704	0.908	1.042	1.129	24 INCH PIPE
16	Reservoir	7		2.993			4.822	5.901	6.741	7.332	36 INCH PIPE (#2)
17	Reservoir	9		0.105			2.300	2.826	2.899	3.311	36 INCH PIPE (#3)
18	Reservoir	10		2.761			4.647	5.822	6.701	7.629	TWO 36 INCH PIPES
19	Combine	3, 4, 13,		10.17			17.43	21.96	25.35	28.95	<no description=""></no>
20	Combine	14, 15, 8, 11, 16,		6.802			11.11	14.53	18.18	20.65	<no description=""></no>
21	Combine	17, 18, 19, 20		16.45			27.70	36.49	42.76	49.09	Design Point B

Proj. file: Existing-Hydraflow.gpw

Monday, 12 / 4 / 2023

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

	,				Hydrafi	ow Hydrograph	is Extension for Ai	utodesk® Civil 3D® by Autodesk, Inc. v20	
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.083	2	734	5,241				EXWS-01
2	SCS Runoff	2.850	2	730	11,602				EXWS-02A
3	SCS Runoff	0.283	2	730	1,101				EXWS-02B
4	SCS Runoff	1.664	2	726	5,899				EX WS-02C
5	SCS Runoff	5.519	2	728	21,524				EX WS-02D
6	SCS Runoff	0.468	2	724	1,523				EXWS-02E
7	SCS Runoff	3.039	2	724	9,485				EXWS-02F
8	SCS Runoff	0.774	2	726	2,719				EX WS-02G
9	SCS Runoff	1.152	2	732	5,114				EX WS-02H
10	SCS Runoff	2.779	2	732	12,419				EX WS-02I
11	SCS Runoff	1.132	2	724	3,836				EXWS-02J
12	SCS Runoff	0.050	2	734	288				EXWS-03
13	Reservoir	2.833	2	732	9,516	2	143.56	1,493	36 INCH PIPE (#1)
14	Reservoir	5.358	2	730	16,803	5	139.02	3,243	TWIN 36IN PIPES (#2)
15	Reservoir	0.449	2	724	891	6	139.60	475	24 INCH PIPE
16	Reservoir	2.993	2	724	8,038	7	139.42	1,181	36 INCH PIPE (#2)
17	Reservoir	0.105	2	848	1,259	9	137.46	3,651	36 INCH PIPE (#3)
18	Reservoir	2.761	2	734	9,331	10	135.68	2,406	TWO 36 INCH PIPES
19	Combine	10.17	2	730	34,210	3, 4, 13,			<no description=""></no>
20	Combine	6.802	2	726	25,182	14, 15, 8, 11, 16,			<no description=""></no>
21	Combine	16.45	2	728	59,393	17, 18, 19, 20			Design Point B
Existing-Hydraflow.gpw				Return F	Period: 2 Ye	 ear	Monday, 12	2 / 4 / 2023	

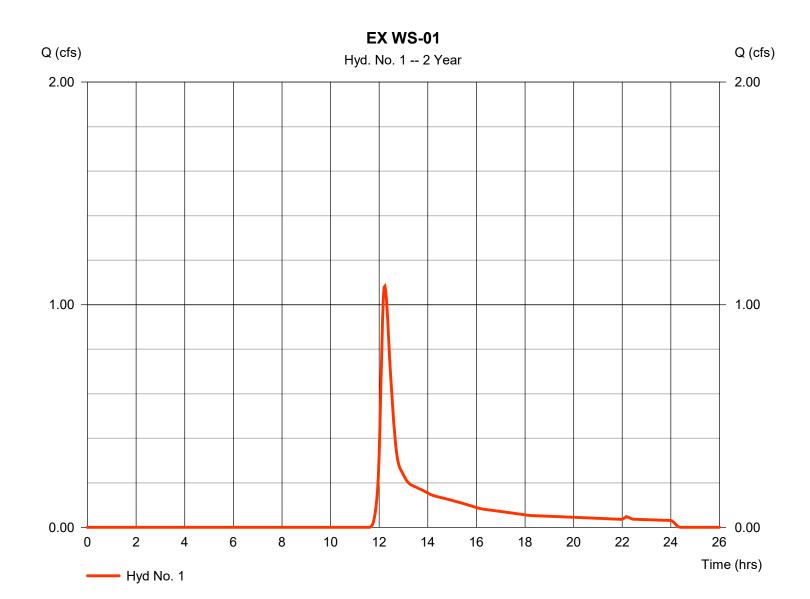
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 1

EX WS-01

Hydrograph type = SCS Runoff Peak discharge = 1.083 cfsStorm frequency = 2 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 5,241 cuft Drainage area Curve number = 1.942 ac= 65 = 0.0 % Hydraulic length Basin Slope = 0 ftTc method Time of conc. (Tc) = 16.10 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



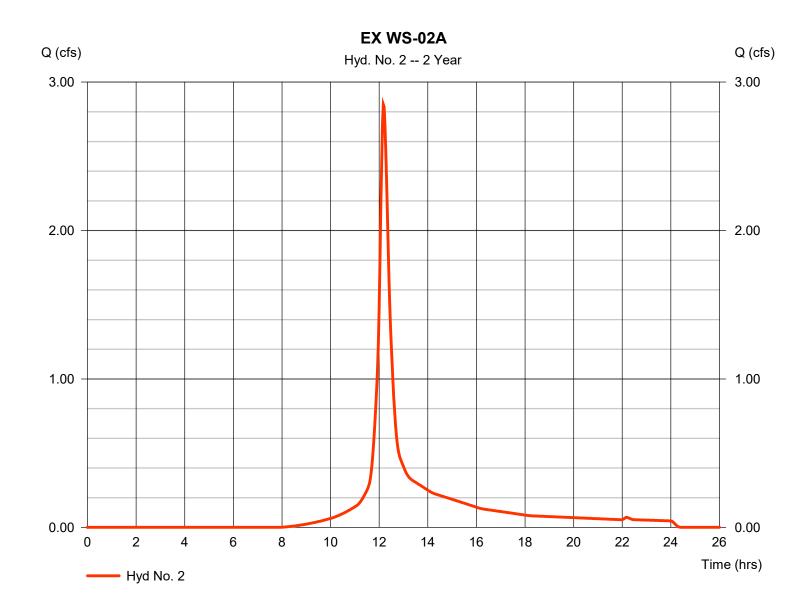
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Monday, 12 / 4 / 2023

Hyd. No. 2

EXWS-02A

Hydrograph type = SCS Runoff Peak discharge = 2.850 cfsStorm frequency = 2 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 11,602 cuft Drainage area = 1.678 ac Curve number = 84 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.50 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



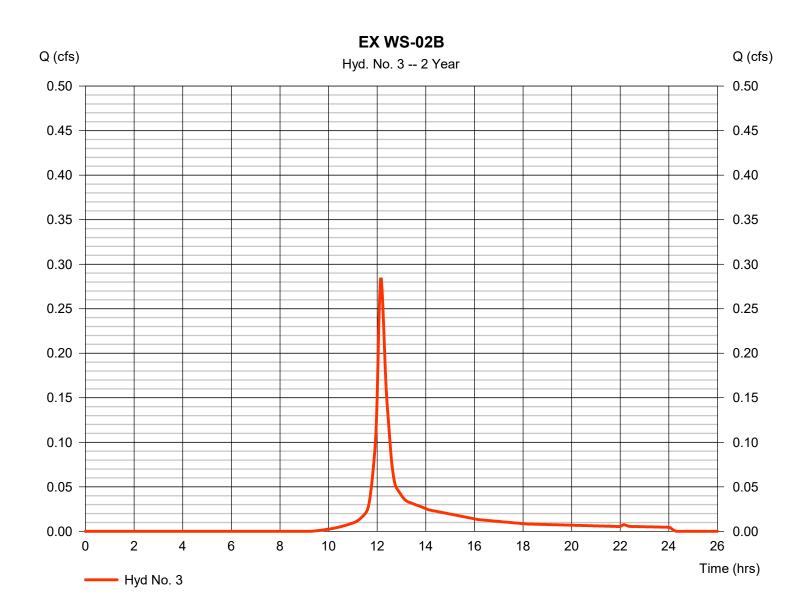
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Monday, 12 / 4 / 2023

Hyd. No. 3

EXWS-02B

Hydrograph type = SCS Runoff Peak discharge = 0.283 cfsStorm frequency = 2 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1,101 cuftDrainage area Curve number = 0.186 ac= 79 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.00 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



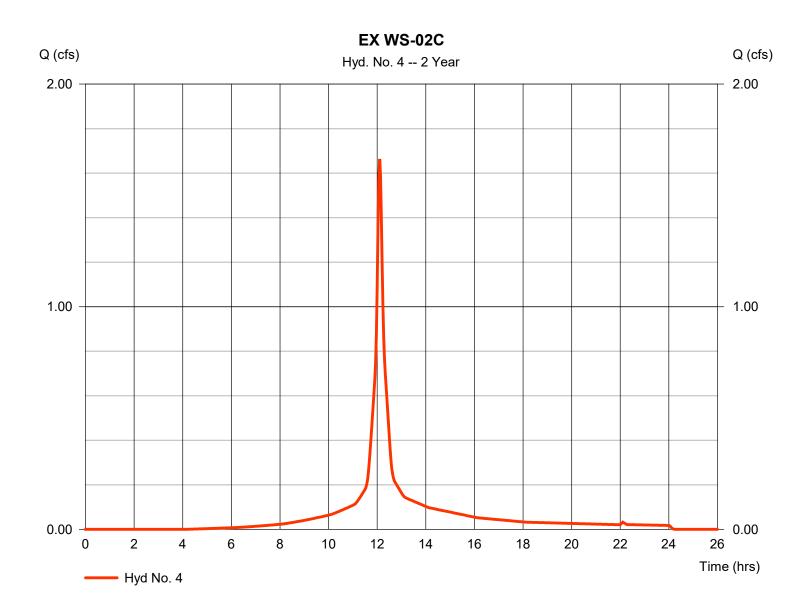
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Monday, 12 / 4 / 2023

Hyd. No. 4

EXWS-02C

Hydrograph type = SCS Runoff Peak discharge = 1.664 cfsStorm frequency = 2 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 5,899 cuftDrainage area = 0.590 acCurve number = 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



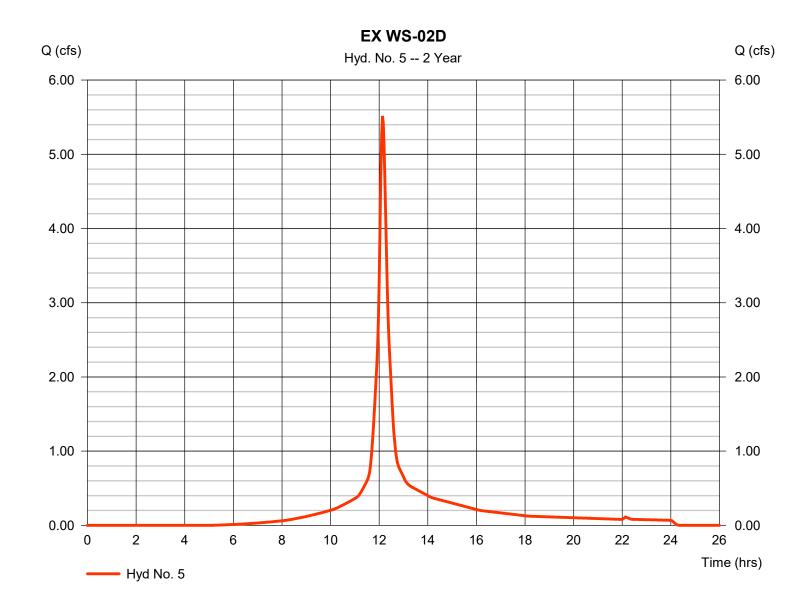
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 5

EXWS-02D

Hydrograph type = SCS Runoff Peak discharge = 5.519 cfsStorm frequency = 2 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 21,524 cuft Drainage area = 2.246 acCurve number = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User = 11.10 min Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



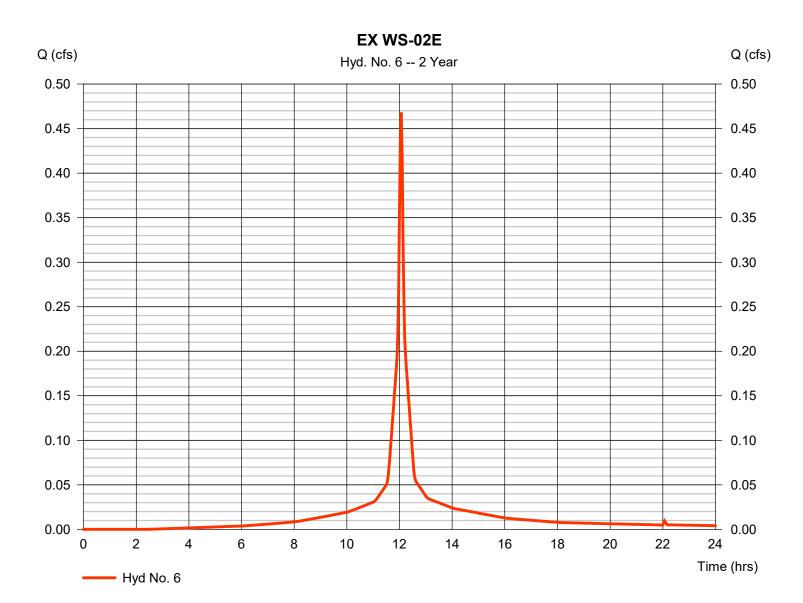
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 6

EXWS-02E

Hydrograph type = SCS Runoff Peak discharge = 0.468 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,523 cuftDrainage area = 0.146 acCurve number = 96 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



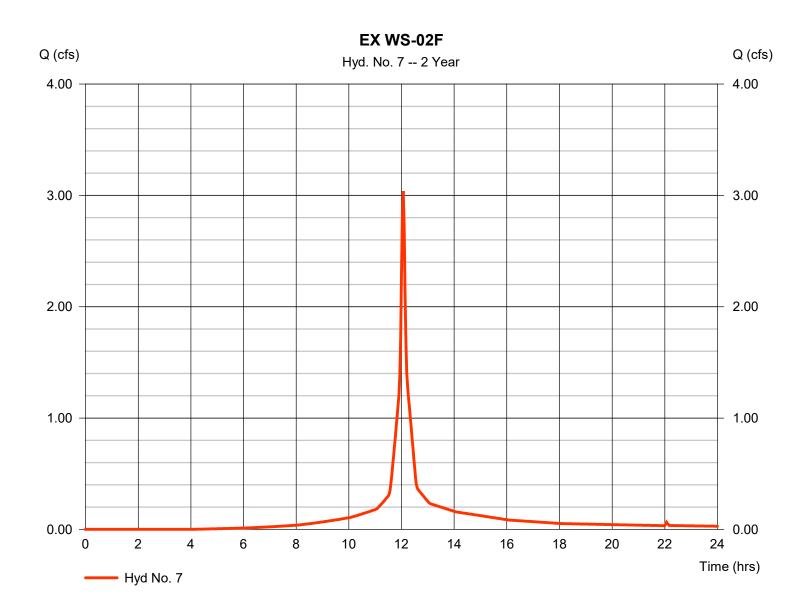
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 7

EXWS-02F

Hydrograph type = SCS Runoff Peak discharge = 3.039 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 9,485 cuft Drainage area Curve number = 1.012 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.50 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



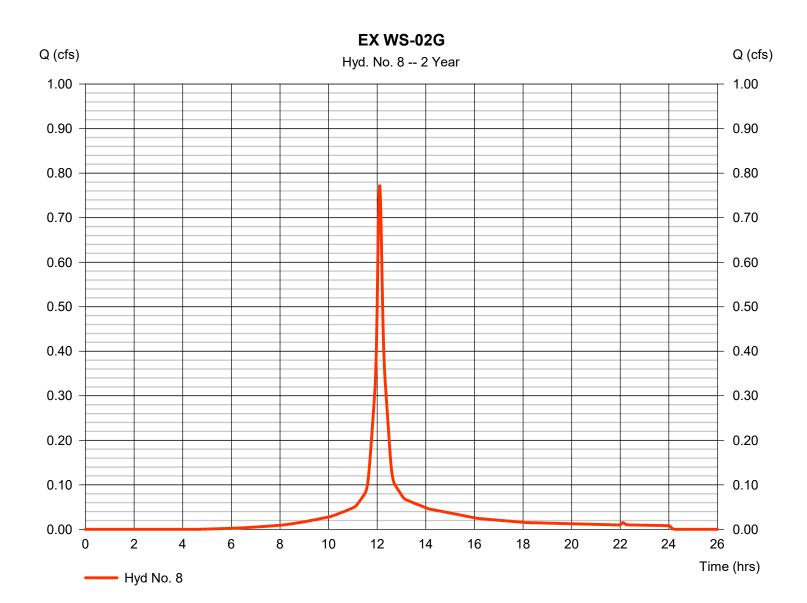
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 8

EXWS-02G

Hydrograph type = SCS Runoff Peak discharge = 0.774 cfsStorm frequency = 2 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 2,719 cuftDrainage area = 0.282 acCurve number = 92 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 6.90 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



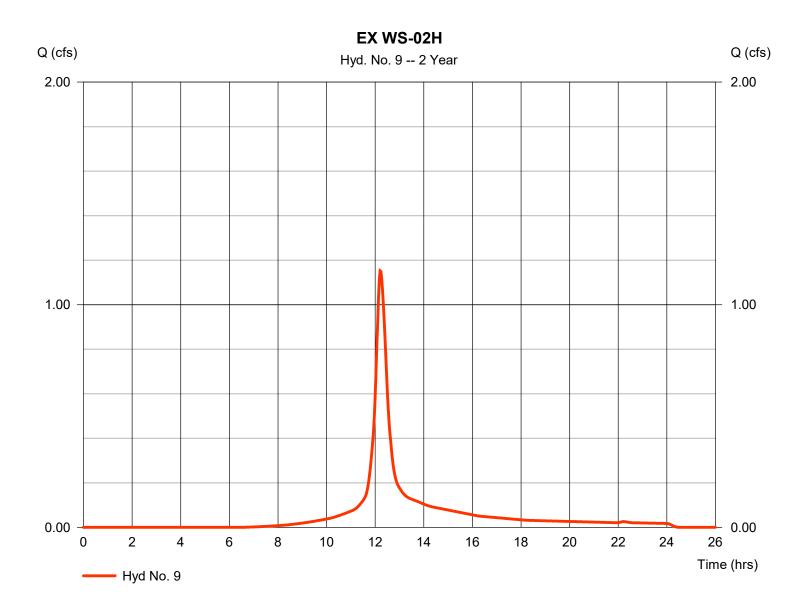
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 9

EXWS-02H

Hydrograph type = SCS Runoff Peak discharge = 1.152 cfsStorm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 5,114 cuftDrainage area = 0.616 acCurve number = 88 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 17.30 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



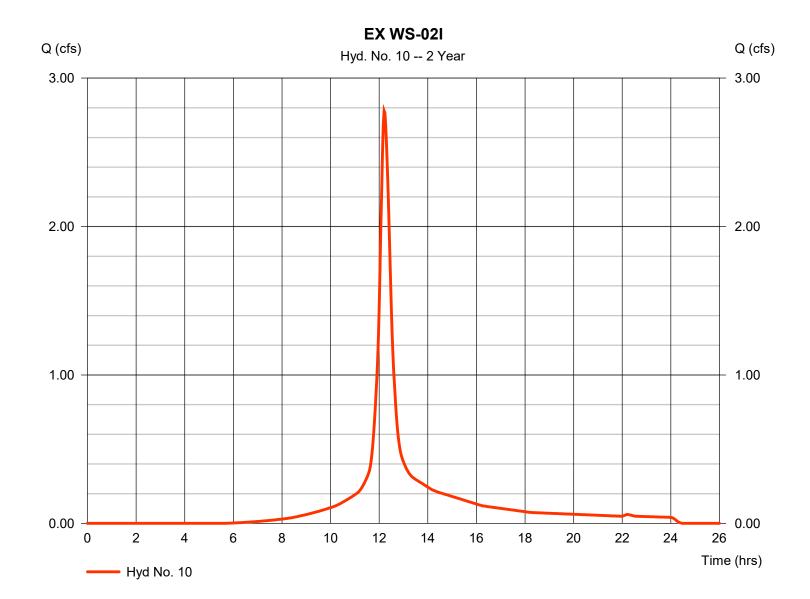
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 10

EX WS-02I

= 2.779 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ = 12,419 cuft Time interval = 2 min Hyd. volume Drainage area = 1.387 acCurve number = 90 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



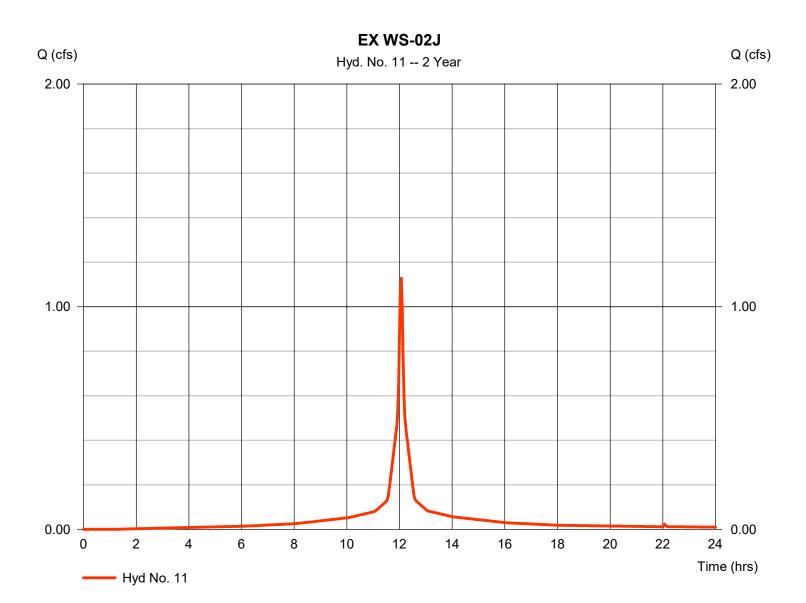
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 11

EXWS-02J

Hydrograph type = SCS Runoff Peak discharge = 1.132 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,836 cuft Drainage area = 0.343 acCurve number = 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



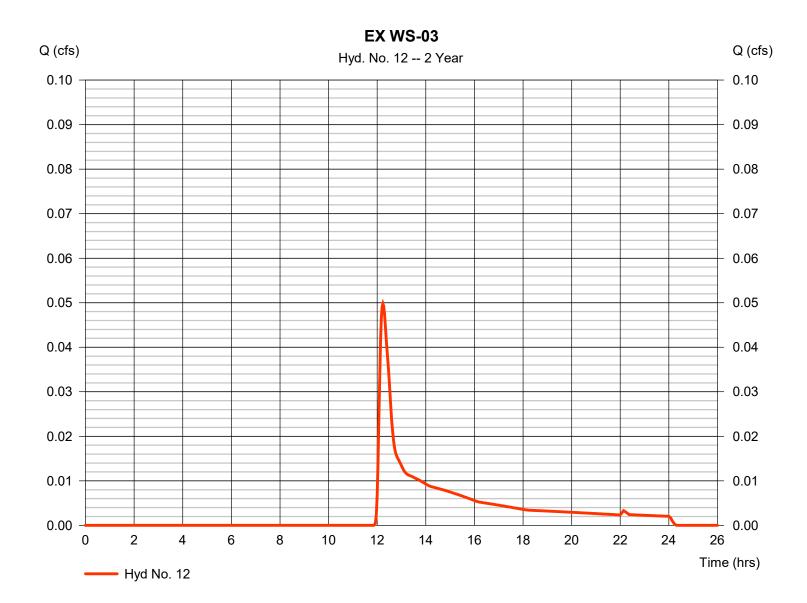
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 12

EX WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.050 cfsStorm frequency = 2 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 288 cuft Drainage area Curve number = 0.154 ac= 59 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.50 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

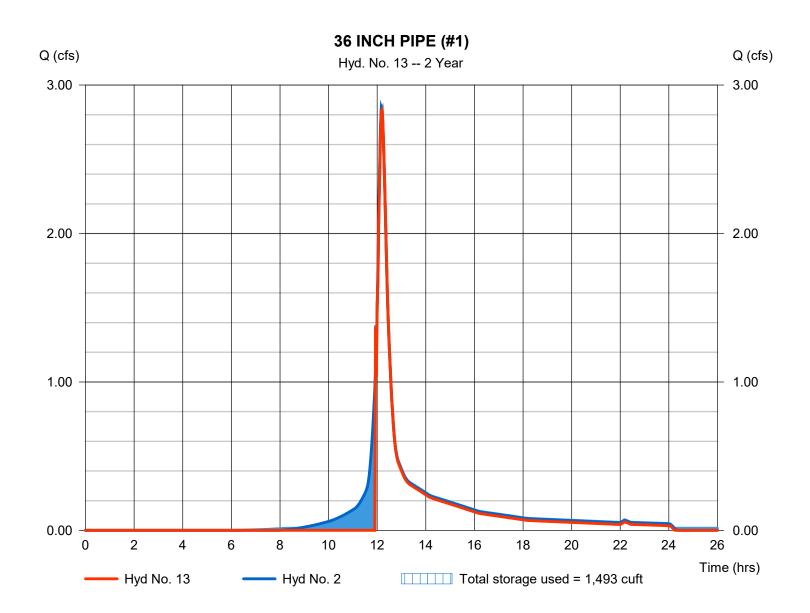
Monday, 12 / 4 / 2023

Hyd. No. 13

36 INCH PIPE (#1)

= Reservoir Hydrograph type Peak discharge = 2.833 cfsStorm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 9,516 cuftMax. Elevation Inflow hyd. No. = 2 - EX WS-02A = 143.56 ftReservoir name = 36IN - 1Max. Storage = 1,493 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 4 - 36IN - 1

Pond Data

UG Chambers -Invert elev. = 134.30 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 102.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No Epodesurse-bls-druterfiledet/con1&ଉପରେ ଅଧିବର୍ଷ ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର ଅଧିବର୍ଷ ଅଧିବର୍ଷ ଅଧିବର ଅଧିକ ଅଧିବର ଅଧି

Stage / Storage Table

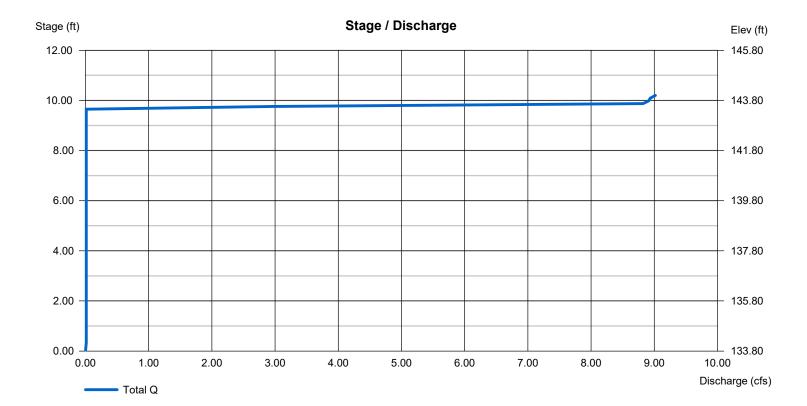
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	133.80	n/a	0	0
0.35	134.15	n/a	71	71
0.70	134.50	n/a	84	155
1.05	134.85	n/a	113	269
1.40	135.20	n/a	126	395
1.75	135.55	n/a	133	528
2.10	135.90	n/a	136	663
2.45	136.25	n/a	134	798
2.80	136.60	n/a	130	927
3.15	136.95	n/a	120	1,047
3.50	137.30	n/a	100	1,147
9.10	142.90	00	0	1,147
10.20	144.00	1,055	580	1,727

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 60.00	Inactive	Inactive	Inactive
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 143.50	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 137.70	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 26.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

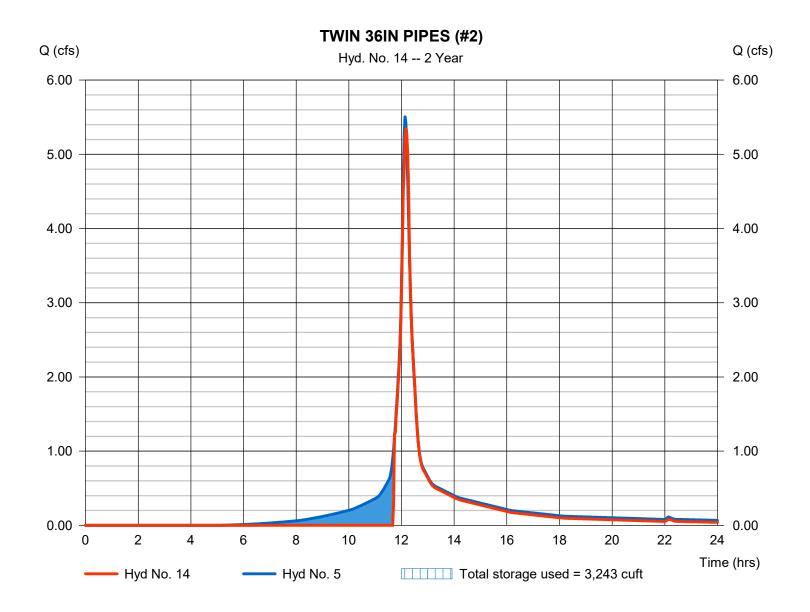
Monday, 12 / 4 / 2023

Hyd. No. 14

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 5.358 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 16,803 cuft = 5 - EX WS-02D Max. Elevation Inflow hyd. No. = 139.02 ftReservoir name = Northern Twin 36IN Max. Storage = 3,243 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 6 - Northern Twin 36IN

Pond Data

UG Chambers -Invert elev. = 131.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 120.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No Epodeserse-bls-driviterfinetel/cent@0.50/das/Waithræg5.00/dtarleteighetthræd.50/dt/driviteriale/dd/06/dlation. Begining Elevation = 138.30 ft

Stage / Storage Table

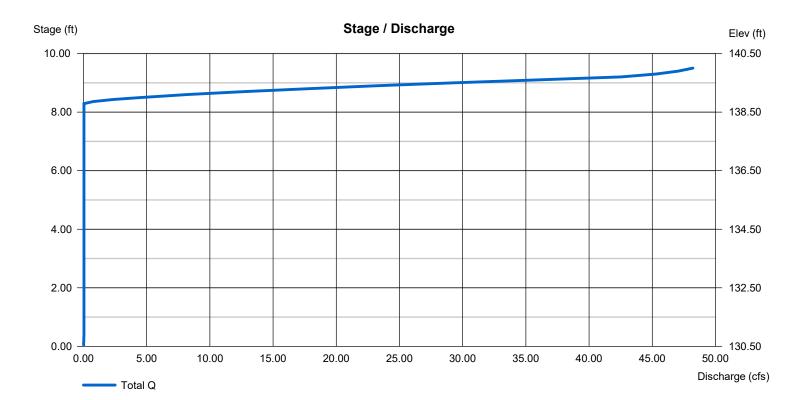
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	130.50	n/a	0	0
0.35	130.85	n/a	168	168
0.70	131.20	n/a	197	365
1.05	131.55	n/a	267	632
1.40	131.90	n/a	297	929
1.75	132.25	n/a	313	1,242
2.10	132.60	n/a	319	1,561
2.45	132.95	n/a	316	1,877
2.80	133.30	n/a	305	2,182
3.15	133.65	n/a	282	2,464
3.50	134.00	n/a	234	2,698
7.80	138.30	01	2	2,701
8.50	139.00	1,250	438	3,138
9.50	140.00	7,570	4,410	7,548

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 30.00	0.00	0.00	0.00	Crest Len (ft)	= 15.00	0.00	0.00	0.00
Span (in)	= 30.00	0.00	0.00	0.00	Crest El. (ft)	= 138.80	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 134.20	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 69.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

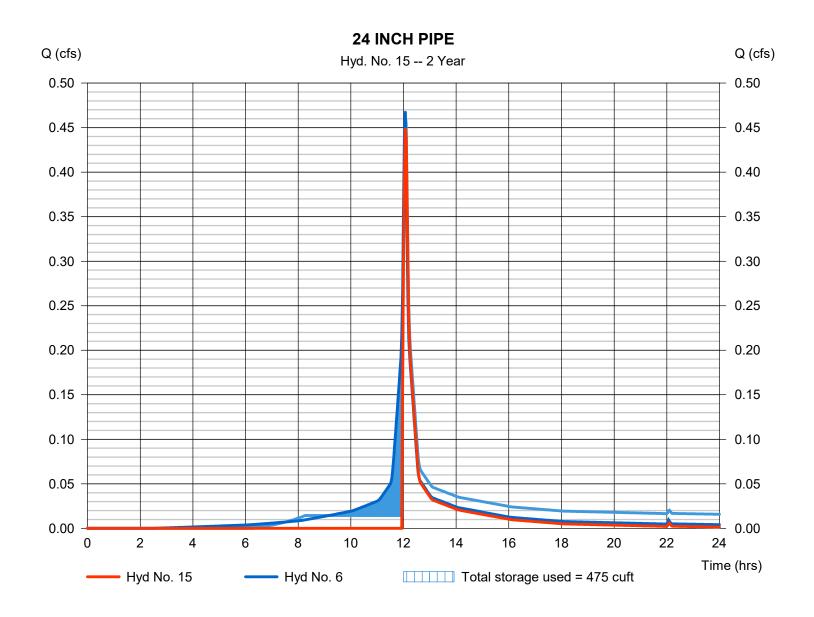
Monday, 12 / 4 / 2023

Hyd. No. 15

24 INCH PIPE

Hydrograph type Peak discharge = 0.449 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 891 cuft Inflow hyd. No. Max. Elevation = 6 - EX WS-02E $= 139.60 \, \text{ft}$ Reservoir name = 24INMax. Storage = 475 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 5 - 24IN

Pond Data

UG Chambers -Invert elev. = 135.00 ft, Rise x Span = 2.00 x 2.00 ft, Barrel Len = 29.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No Epotasurseblsehvterflietelvcent0xitrage/e.00dtarelegigtetthc2d5&edd fvoidslum4e0d200blation. Begining Elevation = 139.10 ft

Stage / Storage Table

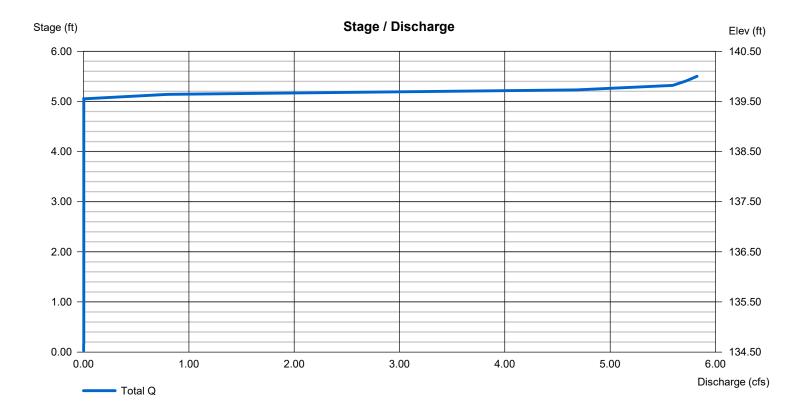
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	134.50	n/a	0	0
0.25	134.75	n/a	12	12
0.50	135.00	n/a	12	23
0.75	135.25	n/a	16	39
1.00	135.50	n/a	18	57
1.25	135.75	n/a	20	77
1.50	136.00	n/a	20	97
1.75	136.25	n/a	20	117
2.00	136.50	n/a	20	137
2.25	136.75	n/a	18	155
2.50	137.00	n/a	16	171
4.60	139.10	01	1	172
5.50	140.00	1,212	546	718

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 30.00	Inactive	Inactive	Inactive
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 139.60	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 137.10	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 55.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 2.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

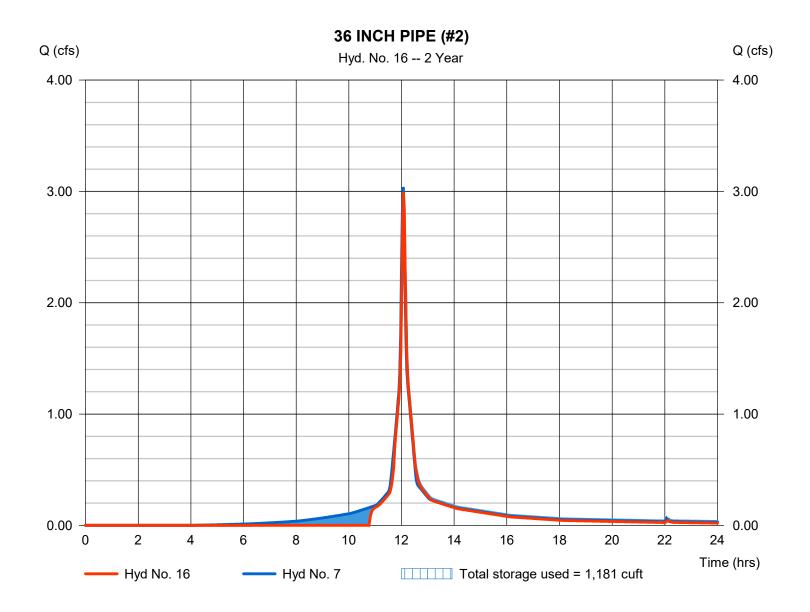
Monday, 12 / 4 / 2023

Hyd. No. 16

36 INCH PIPE (#2)

Hydrograph type = Reservoir Peak discharge = 2.993 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 8,038 cuft Inflow hyd. No. = 7 - EX WS-02F Max. Elevation = 139.42 ftReservoir name = 36in - 2Max. Storage = 1,181 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 1 - 36in - 2

Pond Data

UG Chambers -Invert elev. = 133.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 70.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No Epotasurseblsehvterflietekvcent020:5064ps/Widthrag5.80dqtareleighetthroid ട്രെൻവ

Stage / Storage Table

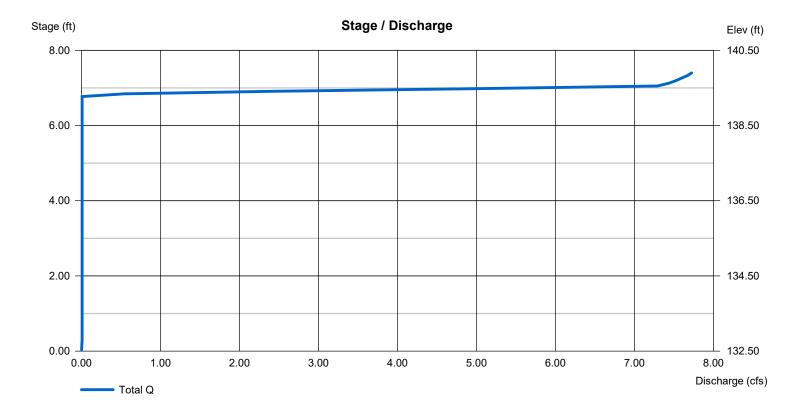
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	132.50	n/a	0	0
0.35	132.85	n/a	49	49
0.70	133.20	n/a	58	107
1.05	133.55	n/a	78	184
1.40	133.90	n/a	87	271
1.75	134.25	n/a	91	362
2.10	134.60	n/a	93	455
2.45	134.95	n/a	92	547
2.80	135.30	n/a	89	636
3.15	135.65	n/a	82	719
3.50	136.00	n/a	68	787
6.70	139.20	01	2	789
7.40	139.90	3,493	1,223	2,012

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 20.00	Inactive	Inactive	Inactive
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 139.30	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 135.20	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 30.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 2.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

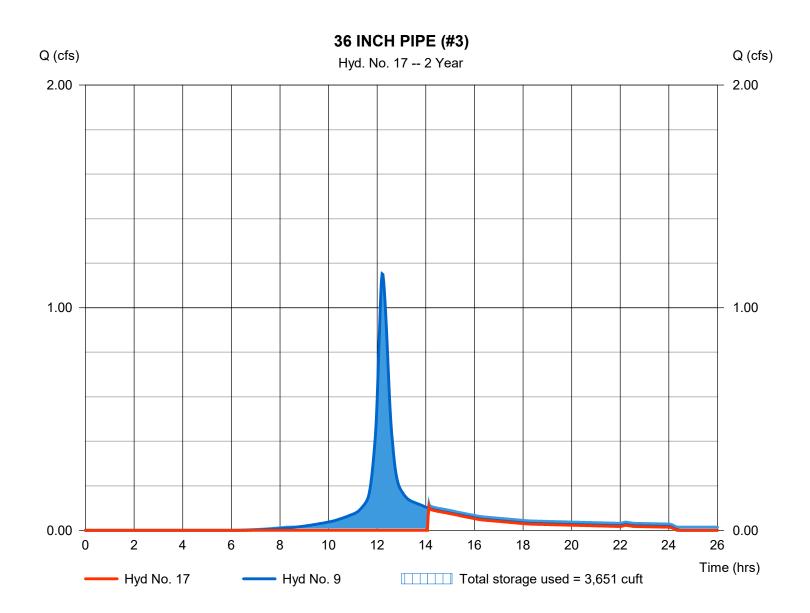
Monday, 12 / 4 / 2023

Hyd. No. 17

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 0.105 cfsStorm frequency = 2 yrsTime to peak $= 14.13 \, hrs$ Time interval = 2 min Hyd. volume = 1,259 cuft= 9 - EX WS-02H Max. Elevation Inflow hyd. No. = 137.46 ftReservoir name = 36in - 3Max. Storage = 3,651 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 3 - 36in - 3

Pond Data

UG Chambers -Invert elev. = 129.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 30.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No Epodes are selected to the selected by the selected

Stage / Storage Table

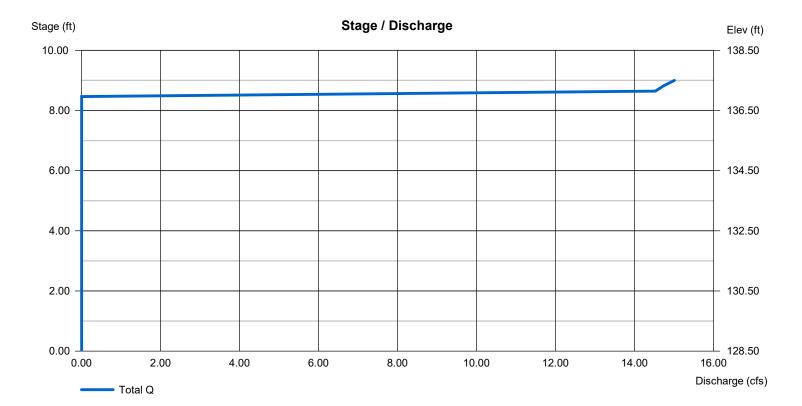
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	128.50	n/a	0	0
0.35	128.85	n/a	21	21
0.70	129.20	n/a	25	46
1.05	129.55	n/a	33	79
1.40	129.90	n/a	37	116
1.75	130.25	n/a	39	155
2.10	130.60	n/a	40	195
2.45	130.95	n/a	40	235
2.80	131.30	n/a	38	273
3.15	131.65	n/a	35	308
3.50	132.00	n/a	29	337
7.20	136.20	01	2	339
9.00	138.00	5,250	4,726	5,065

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 100.00	Inactive	Inactive	Inactive
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 137.50	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 130.90	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 13.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by)	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

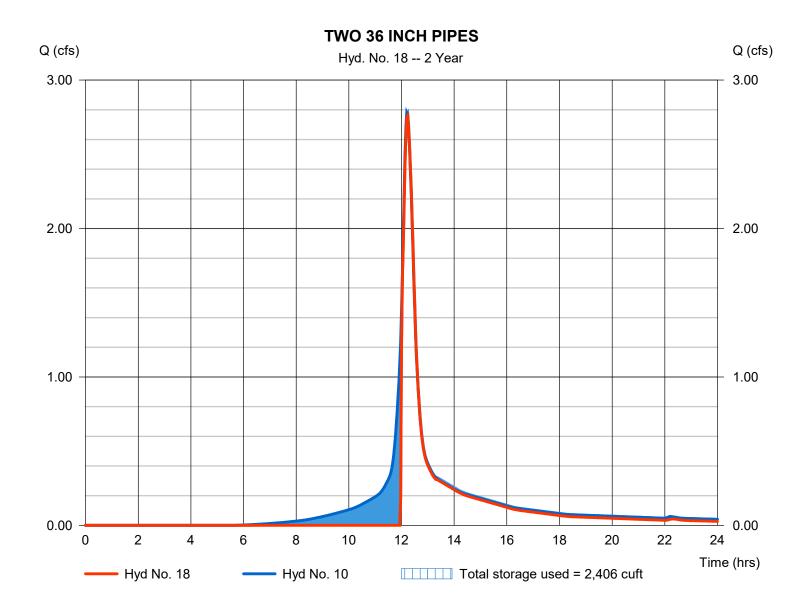
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Hyd. No. 18

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 2.761 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 9,331 cuftInflow hyd. No. Max. Elevation = 10 - EX WS-02I = 135.68 ftReservoir name = TWIN 36IN Max. Storage = 2,406 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Pond No. 2 - TWIN 36IN

Pond Data

UG Chambers -Invert elev. = 127.50 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 62.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No Epotasurseblsehvterflietelvcent@7r.@0ศasWidthræg5.80dtarlelæighetthroid ട്രെൽവ fvoidslum4e0@30dblation. Begining Elevation = 134.90 ft

Stage / Storage Table

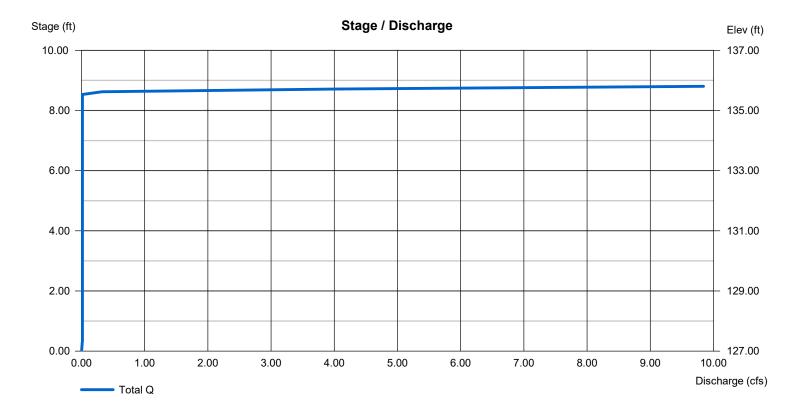
Stage (ft) Elevation (ft)		Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)	
0.00	127.00	n/a	0	0	
0.35	127.35	n/a	87	87	
0.70	127.70	n/a	102	189	
1.05	128.05	n/a	138	327	
1.40	128.40	n/a	153	480	
1.75	128.75	n/a	162	642	
2.10	129.10	n/a	165	806	
2.45	129.45	n/a	163	970	
2.80	129.80	n/a	157	1,127	
3.15	130.15	n/a	146	1,273	
3.50	130.50	n/a	121	1,394	
7.90	134.90	01	2	1,396	
8.80	135.80	2,590	1,166	2,562	

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 33.00	Inactive	Inactive	Inactive
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 135.60	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 129.60	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 70.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 2.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 19

<no description>

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 2 min

Inflow hyds. = 3, 4, 13, 14, 15

Peak discharge = 10.17 cfs
Time to peak = 12.17 hrs
Hyd. volume = 34,210 cuft
Contrib. drain. area = 0.776 ac

<no description> Q (cfs) Q (cfs) Hyd. No. 19 -- 2 Year 12.00 12.00 10.00 10.00 8.00 8.00 6.00 6.00 4.00 4.00 2.00 2.00 0.00 0.00 2 4 8 6 10 12 14 16 18 20 22 24 Time (hrs) Hyd No. 4 Hyd No. 19 Hyd No. 3 Hyd No. 13 Hyd No. 14 - Hyd No. 15

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

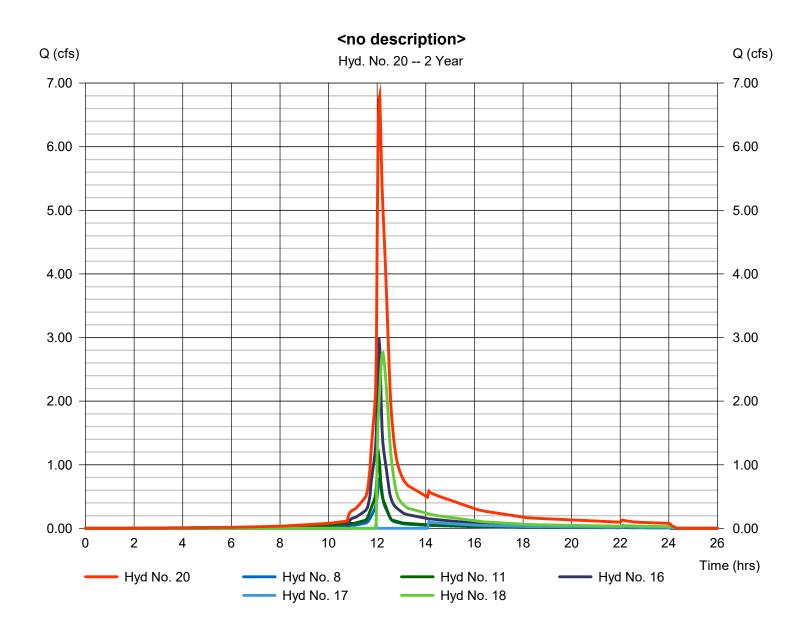
Hyd. No. 20

<no description>

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 2 min

Inflow hyds. = 8, 11, 16, 17, 18

Peak discharge = 6.802 cfs
Time to peak = 12.10 hrs
Hyd. volume = 25,182 cuft
Contrib. drain. area = 0.625 ac



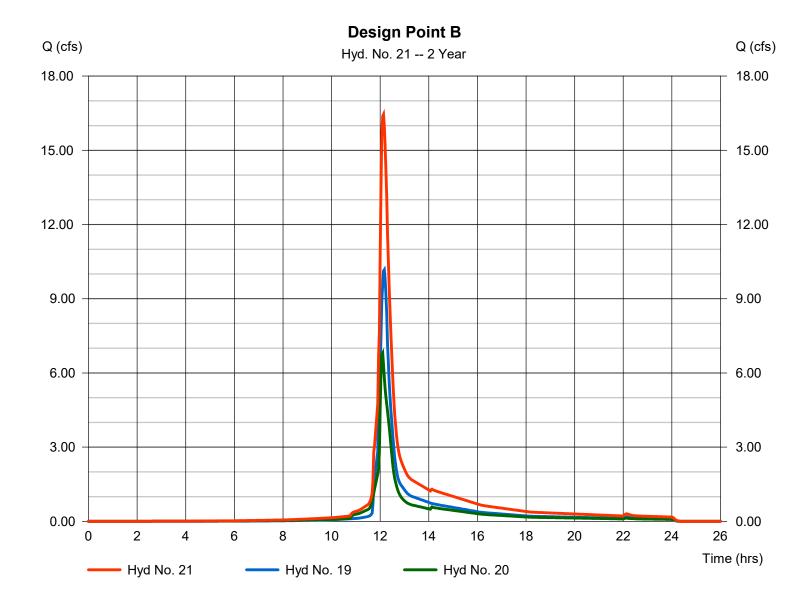
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 21

Design Point B

Hydrograph type = Combine Peak discharge = 16.45 cfsStorm frequency Time to peak = 2 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 59,393 cuft Inflow hyds. = 19, 20 Contrib. drain. area = 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	3.109	2	732	13,137				EX WS-01	
2	SCS Runoff	5.245	2	730	21,498				EX WS-02A	
3	SCS Runoff	0.569	2	728	2,180				EX WS-02B	
4	SCS Runoff	2.685	2	726	9,791				EX WS-02C	
5	SCS Runoff	9.148	2	728	36,588				EX WS-02D	
6	SCS Runoff	0.731	2	724	2,440				EX WS-02E	
7	SCS Runoff	4.896	2	724	15,744				EX WS-02F	
8	SCS Runoff	1.265	2	726	4,567				EX WS-02G	
9	SCS Runoff	1.996	2	732	9,014				EX WS-02H	
10	SCS Runoff	4.677	2	732	21,366				EX WS-02I	
11	SCS Runoff	1.741	2	724	6,003				EX WS-02J	
12	SCS Runoff	0.199	2	730	839				EX WS-03	
13	Reservoir	5.228	2	730	19,335	2	143.60	1,518	36 INCH PIPE (#1)	
14	Reservoir	8.916	2	730	31,682	5	139.12	3,650	TWIN 36IN PIPES (#2)	
15	Reservoir	0.704	2	724	1,793	6	139.63	493	24 INCH PIPE	
16	Reservoir	4.822	2	724	14,247	7	139.47	1,266	36 INCH PIPE (#2)	
17	Reservoir	2.300	2	738	5,135	9	137.49	3,722	36 INCH PIPE (#3)	
18	Reservoir	4.647	2	732	18,180	10	135.72	2,459	TWO 36 INCH PIPES	
19	Combine	17.43	2	730	64,781	3, 4, 13,			<no description=""></no>	
20	Combine	11.11	2	726	48,132	14, 15, 8, 11, 16,			<no description=""></no>	
21	Combine	27.70	2	728	112,913	17, 18, 19, 20			Design Point B	
Existing-Hydraflow.gpw					Return F	Return Period: 10 Year			Monday, 12 / 4 / 2023	

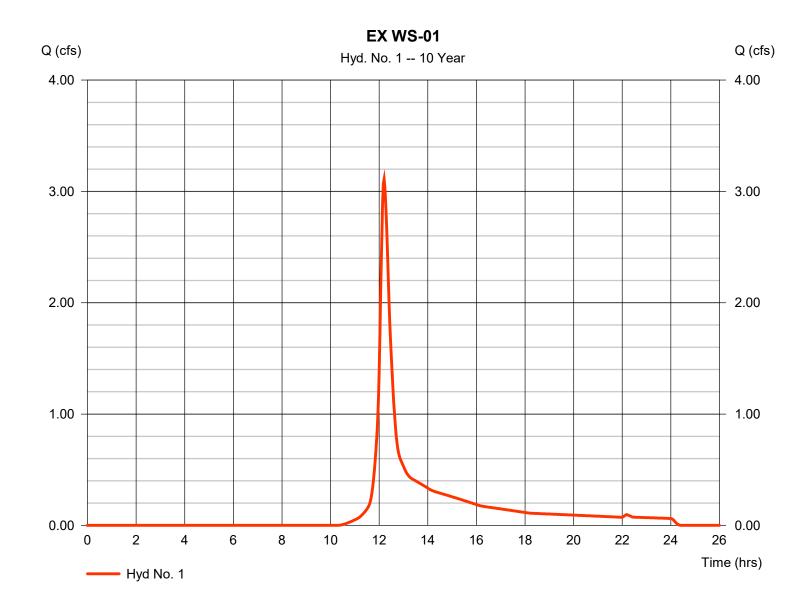
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 1

EX WS-01

Hydrograph type = SCS Runoff Peak discharge = 3.109 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 13,137 cuft Drainage area Curve number = 1.942 ac= 65 = 0.0 % Basin Slope Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.10 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

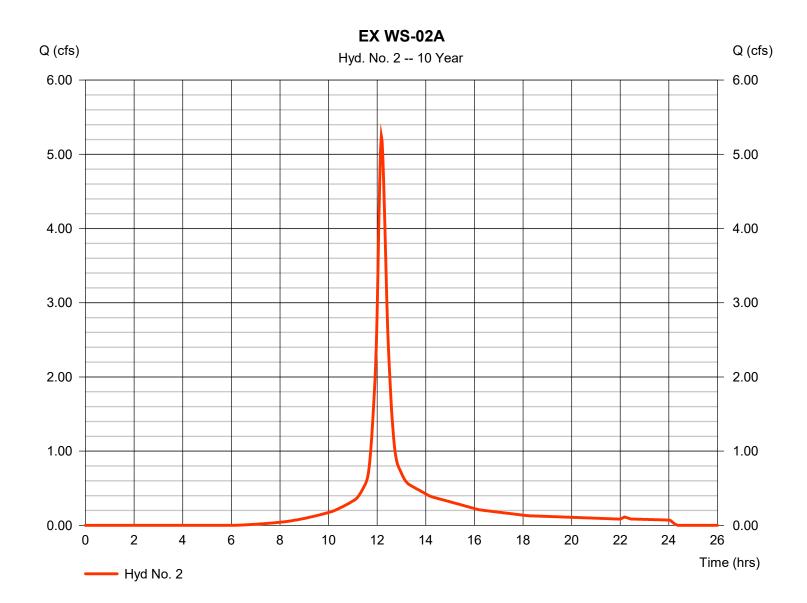
Monday, 12 / 4 / 2023

Hyd. No. 2

EXWS-02A

Hydrograph type = SCS Runoff Peak discharge = 5.245 cfsStorm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 21,498 cuft Drainage area Curve number = 1.678 ac= 84 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.50 min = User

Total precip. = 5.38 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Monday, 12 / 4 / 2023

= 484

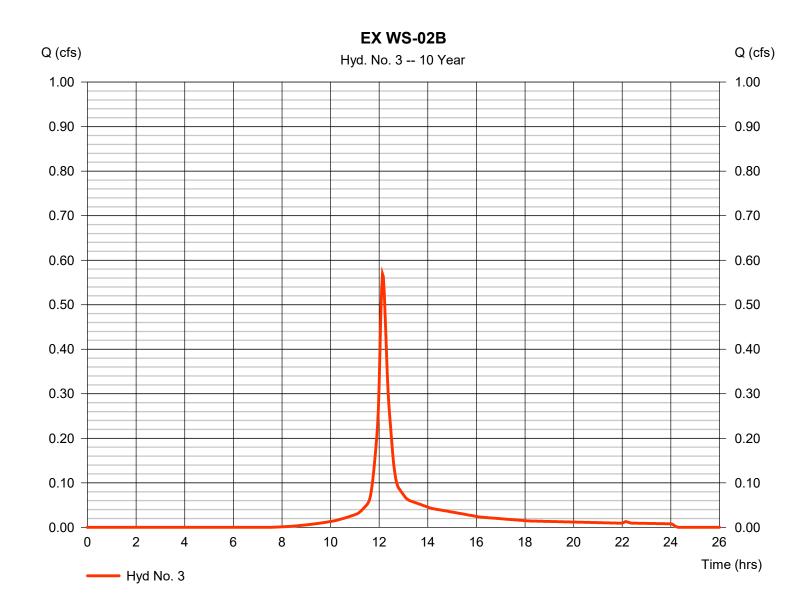
Hyd. No. 3

EXWS-02B

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 0.569 cfsStorm frequency = 10 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2.180 cuftDrainage area Curve number = 0.186 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 11.00 min = User Total precip. = 5.38 inDistribution = Type III

Shape factor



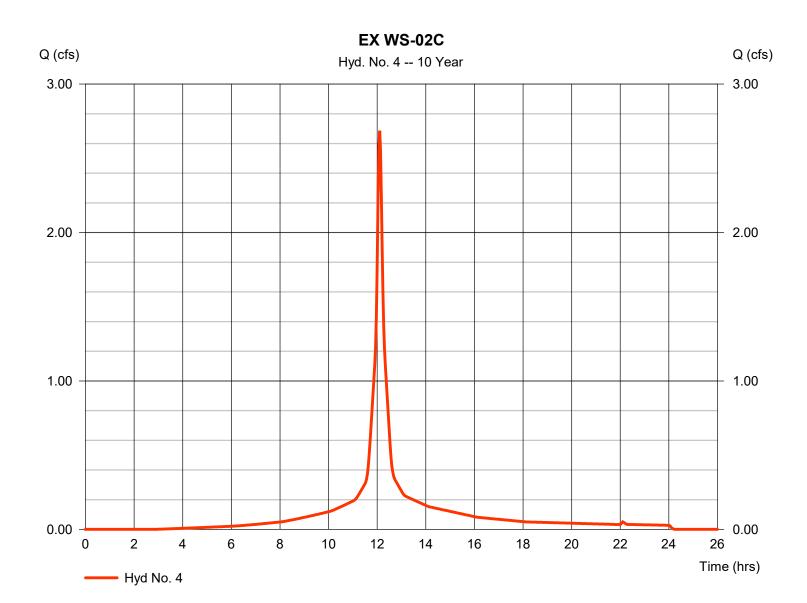
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 4

EXWS-02C

Hydrograph type = SCS Runoff Peak discharge = 2.685 cfsStorm frequency = 10 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 9,791 cuftDrainage area Curve number = 0.590 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



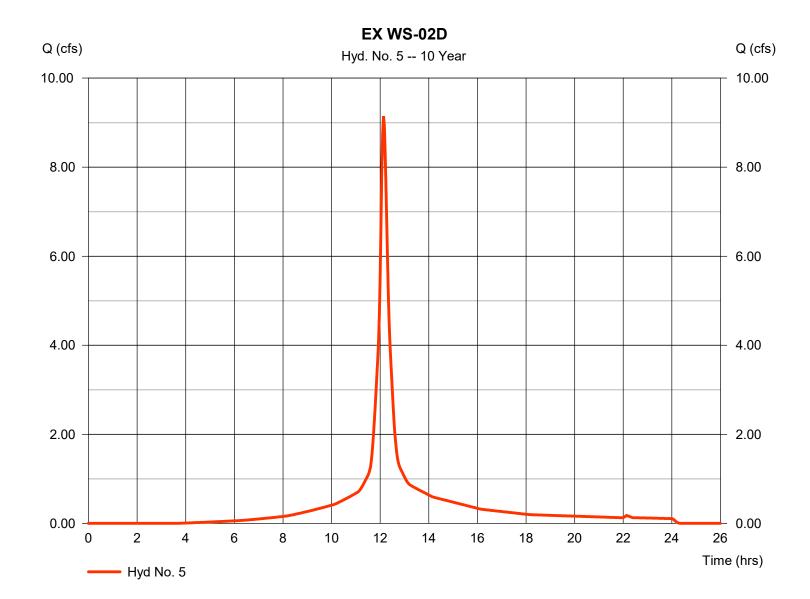
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 5

EXWS-02D

Hydrograph type = SCS Runoff Peak discharge = 9.148 cfsStorm frequency = 10 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 36,588 cuft Drainage area = 2.246 ac Curve number = 91 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 11.10 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



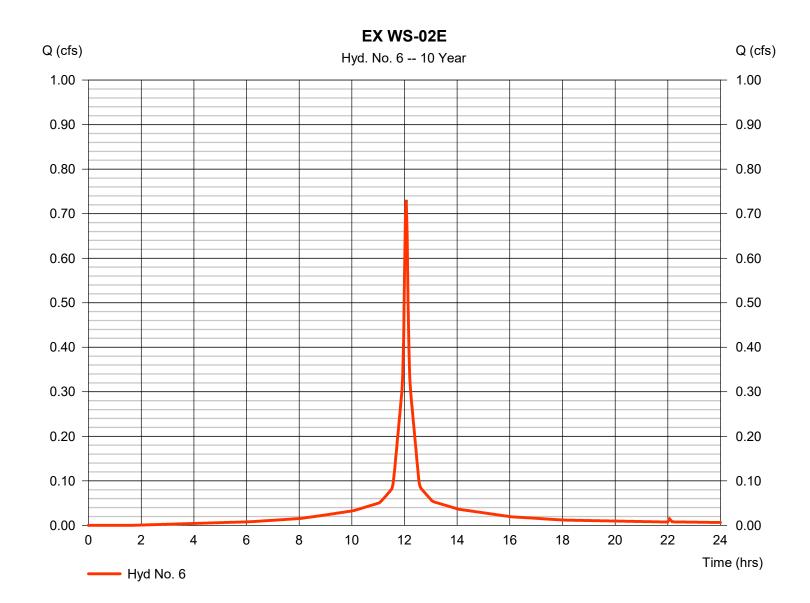
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 6

EXWS-02E

Hydrograph type = SCS Runoff Peak discharge = 0.731 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,440 cuftDrainage area Curve number = 0.146 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



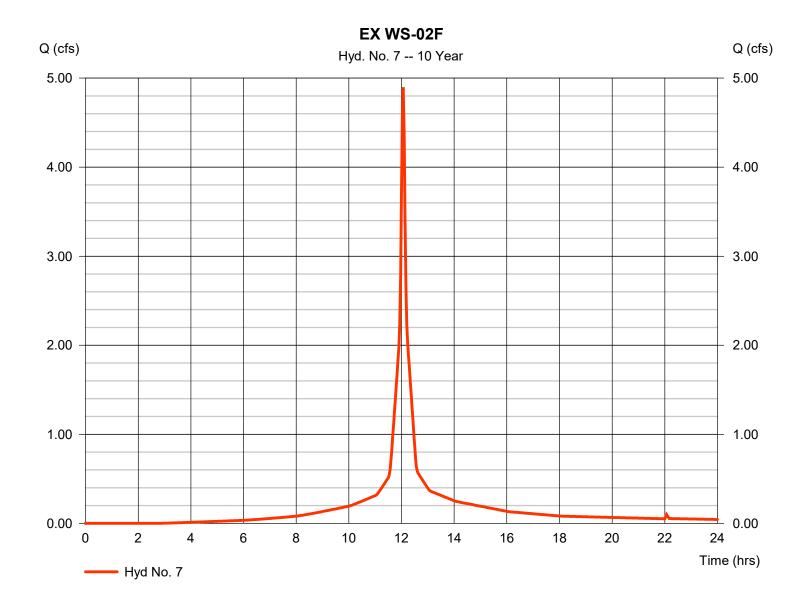
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 7

EXWS-02F

Hydrograph type = SCS Runoff Peak discharge = 4.896 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 15,744 cuft Curve number Drainage area = 1.012 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.50 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



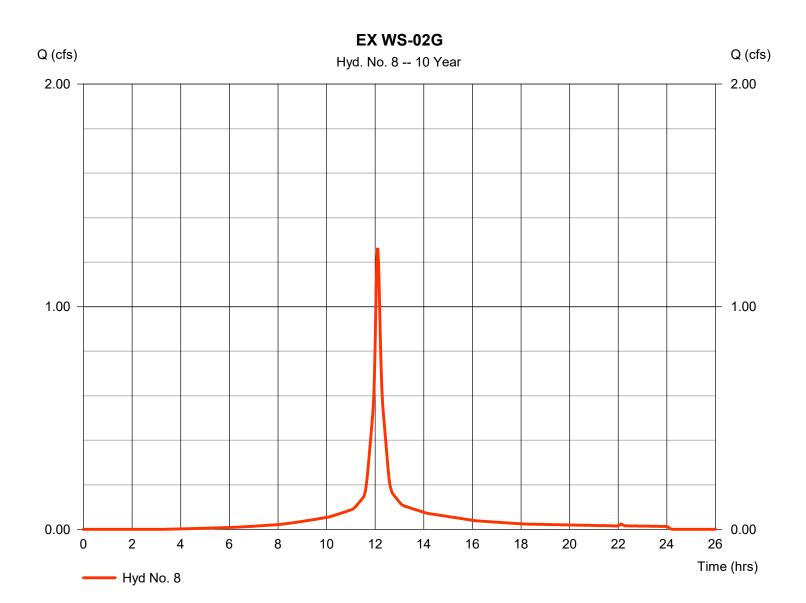
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 8

EXWS-02G

= SCS Runoff Hydrograph type Peak discharge = 1.265 cfsStorm frequency = 10 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 4,567 cuftDrainage area Curve number = 0.282 ac= 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 6.90 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



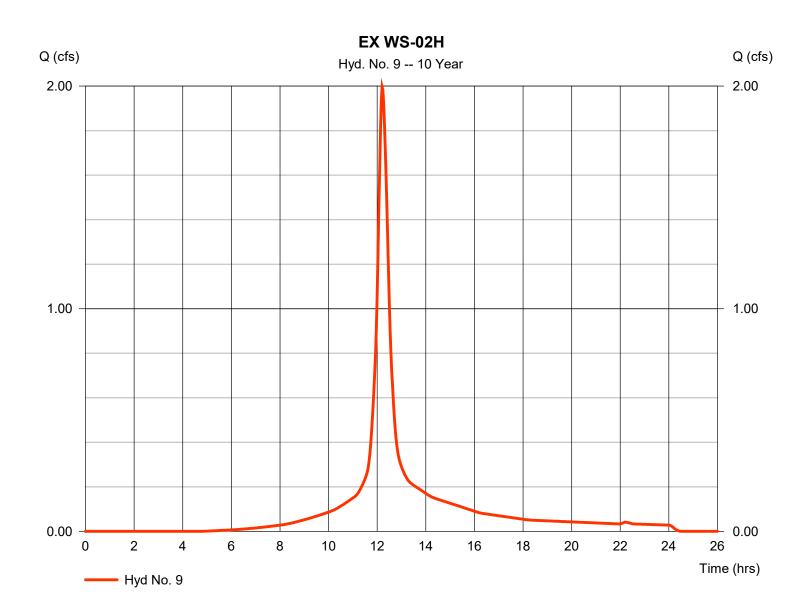
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 9

EXWS-02H

= SCS Runoff Hydrograph type Peak discharge = 1.996 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 9,014 cuftDrainage area Curve number = 0.616 ac= 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.30 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



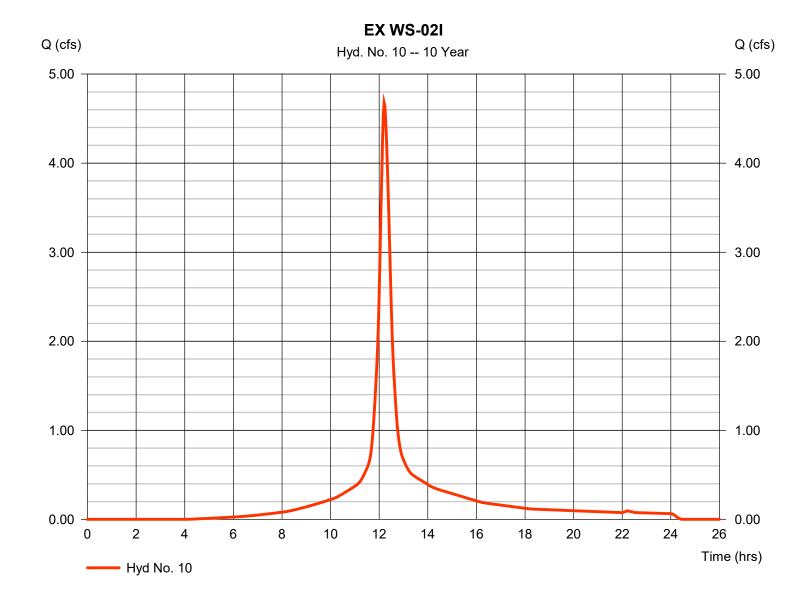
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 10

EX WS-02I

Hydrograph type = SCS Runoff Peak discharge = 4.677 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 21,366 cuft Drainage area = 1.387 acCurve number = 90 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



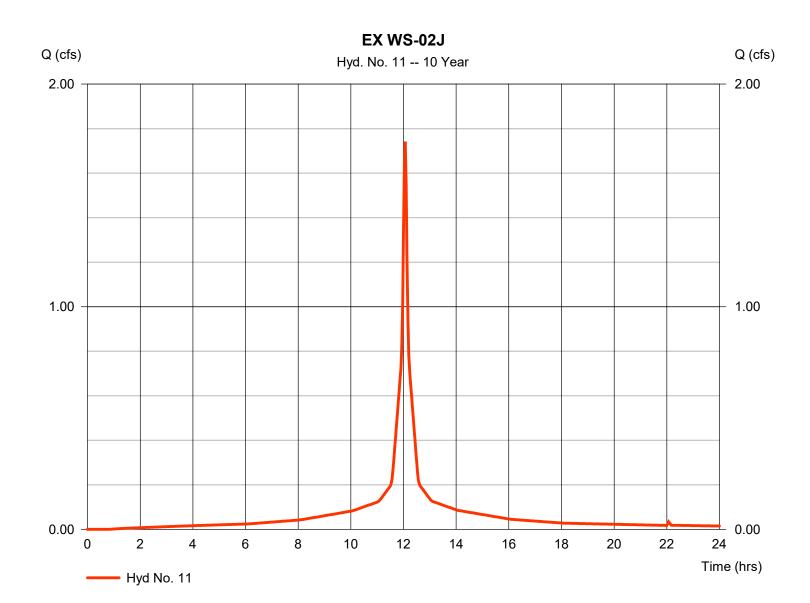
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 11

EXWS-02J

Hydrograph type = SCS Runoff Peak discharge = 1.741 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 6,003 cuftDrainage area Curve number = 0.343 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



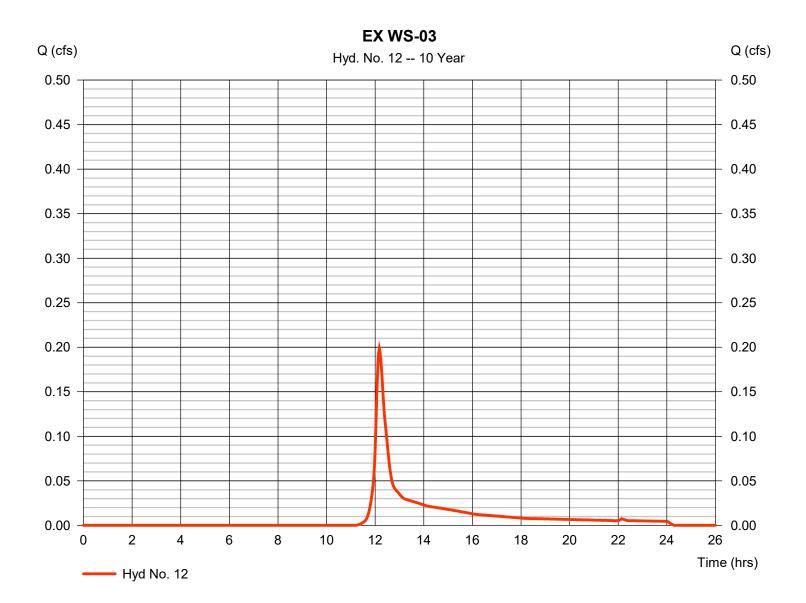
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 12

EX WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.199 cfsStorm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 839 cuft Drainage area Curve number = 0.154 ac= 59 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.50 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



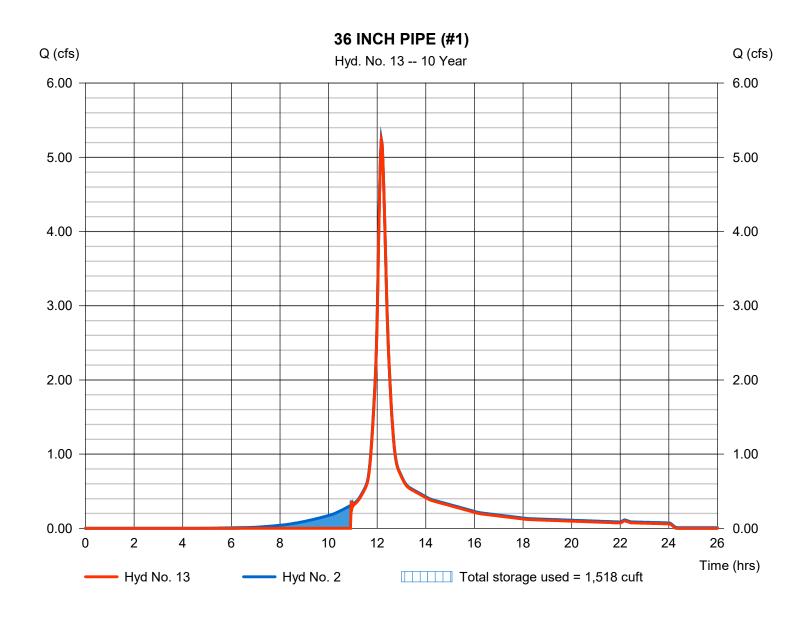
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 13

36 INCH PIPE (#1)

Hydrograph type Peak discharge = 5.228 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 19,335 cuft Max. Elevation Inflow hyd. No. = 2 - EX WS-02A $= 143.60 \, \text{ft}$ Reservoir name = 36IN - 1Max. Storage = 1,518 cuft



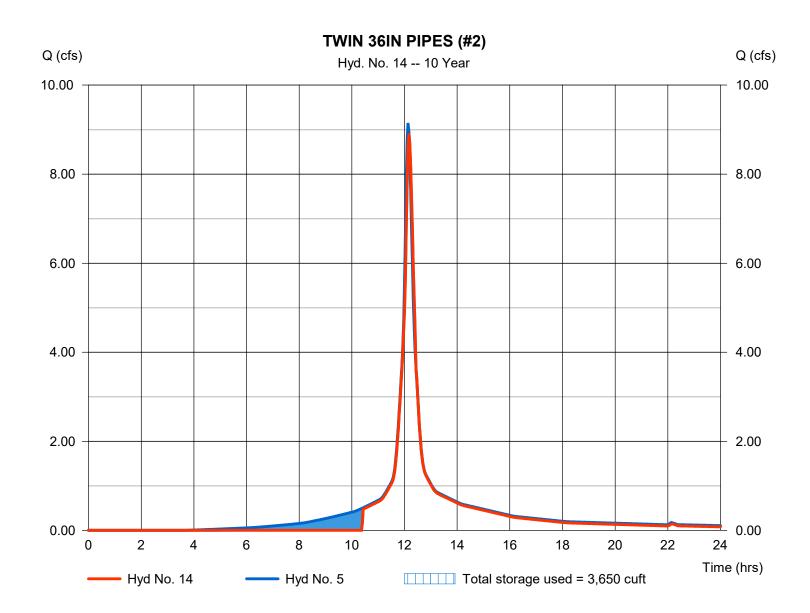
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 14

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 8.916 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 31,682 cuft = 5 - EX WS-02D Max. Elevation = 139.12 ftInflow hyd. No. = Northern Twin 36IN Reservoir name Max. Storage = 3,650 cuft



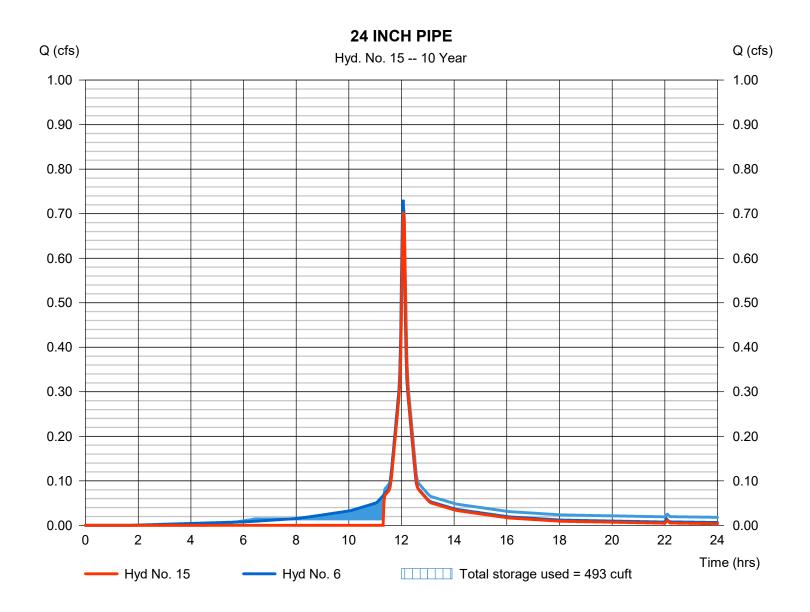
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 15

24 INCH PIPE

Hydrograph type Peak discharge = 0.704 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,793 cuftMax. Elevation Inflow hyd. No. = 6 - EX WS-02E $= 139.63 \, \text{ft}$ Reservoir name = 24INMax. Storage = 493 cuft



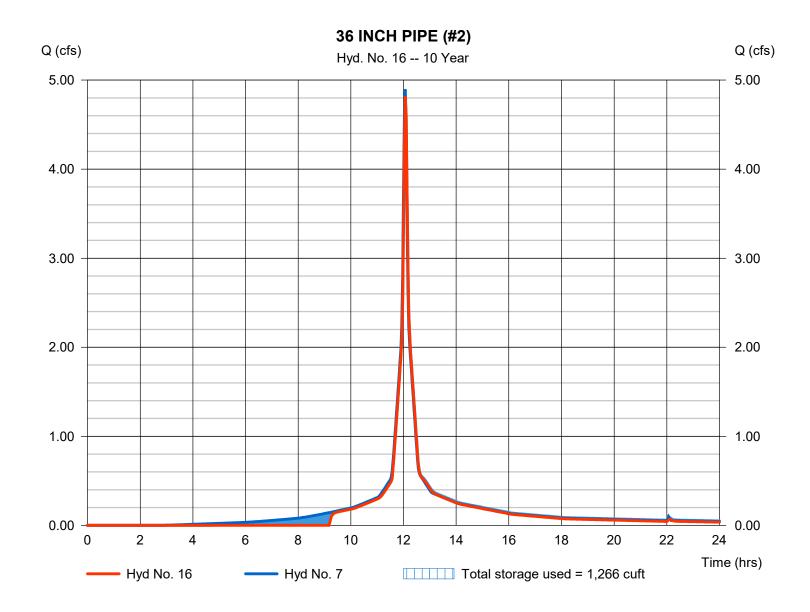
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 16

36 INCH PIPE (#2)

Hydrograph type = Reservoir Peak discharge = 4.822 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 14,247 cuft Inflow hyd. No. Max. Elevation = 7 - EX WS-02F = 139.47 ftReservoir name = 36in - 2Max. Storage = 1,266 cuft



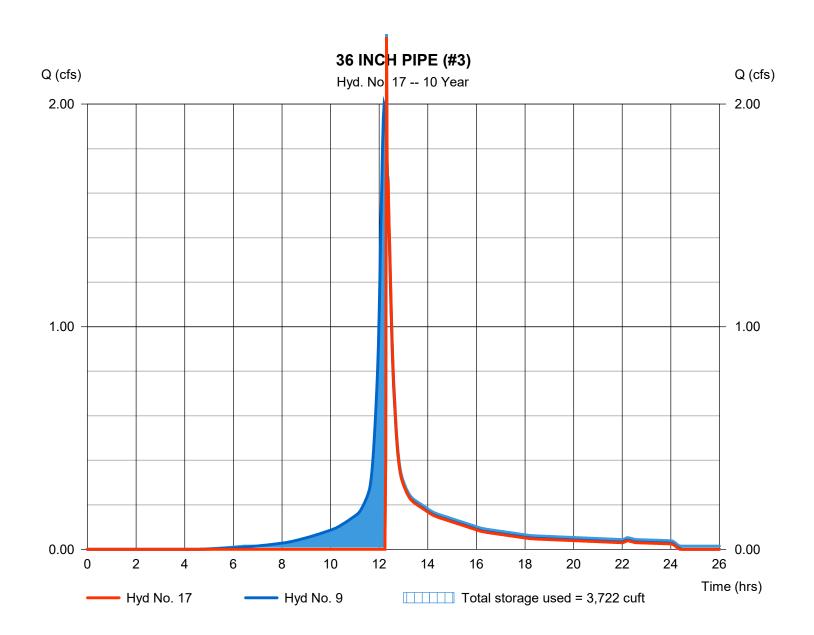
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 17

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 2.300 cfsStorm frequency = 10 yrsTime to peak $= 12.30 \, hrs$ Time interval = 2 min Hyd. volume = 5,135 cuftMax. Elevation Inflow hyd. No. = 9 - EX WS-02H = 137.49 ftReservoir name = 36in - 3Max. Storage = 3,722 cuft



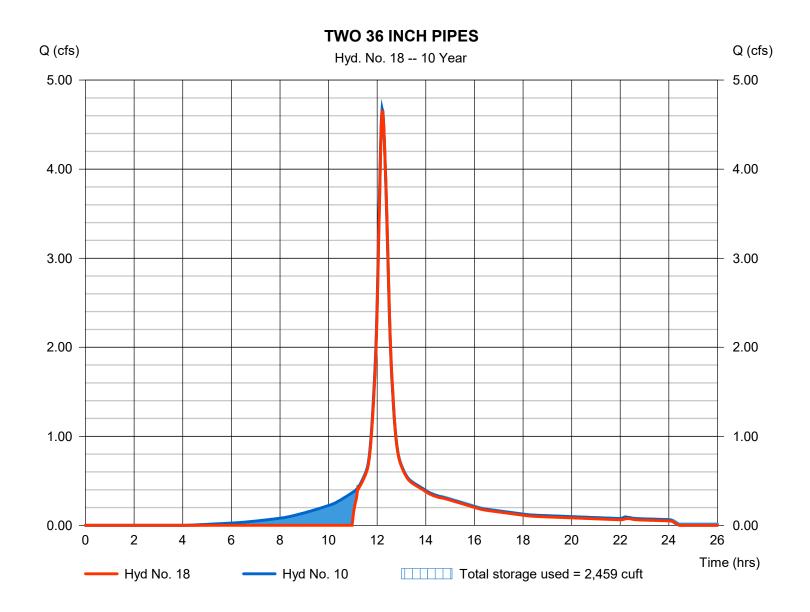
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 18

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 4.647 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 18,180 cuft Max. Elevation Inflow hyd. No. = 10 - EX WS-02I = 135.72 ftReservoir name = TWIN 36IN Max. Storage = 2,459 cuft



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

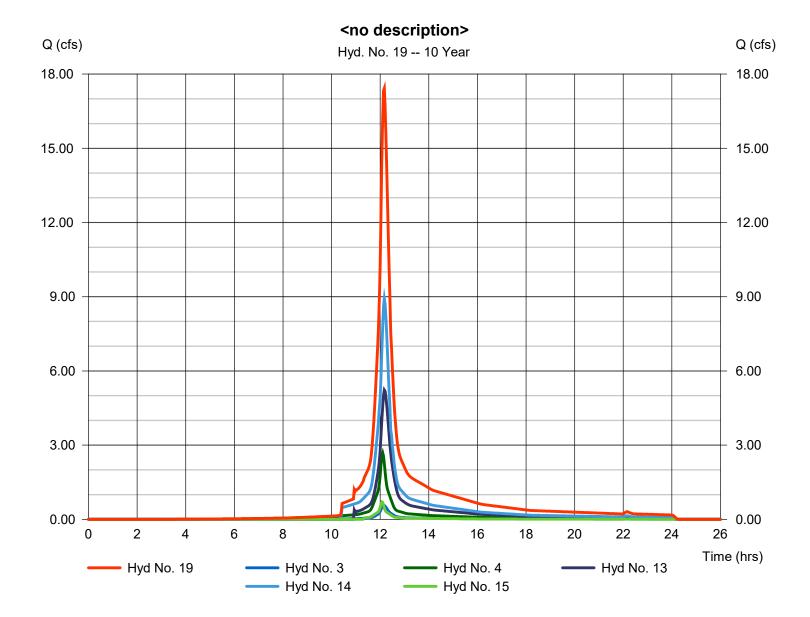
Hyd. No. 19

<no description>

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 2 min

Inflow hyds. = 3, 4, 13, 14, 15

Peak discharge = 17.43 cfs
Time to peak = 12.17 hrs
Hyd. volume = 64,781 cuft
Contrib. drain. area = 0.776 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

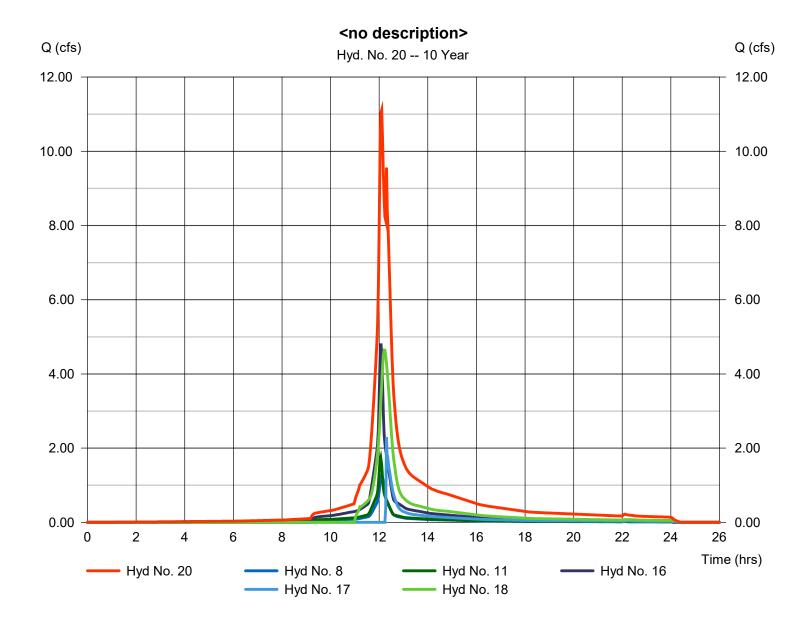
Hyd. No. 20

<no description>

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 2 min

Inflow hyds. = 8, 11, 16, 17, 18

Peak discharge = 11.11 cfs
Time to peak = 12.10 hrs
Hyd. volume = 48,132 cuft
Contrib. drain. area = 0.625 ac



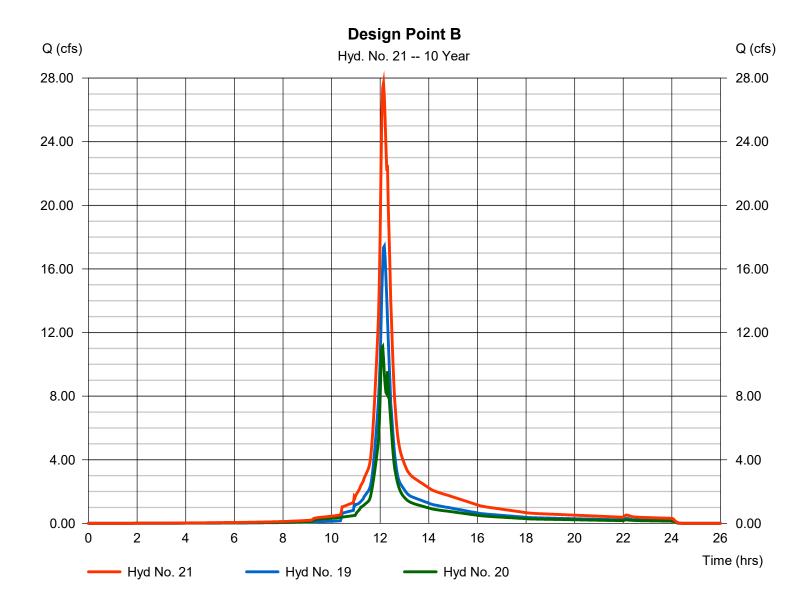
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 21

Design Point B

Hydrograph type = Combine Peak discharge = 27.70 cfsStorm frequency Time to peak = 10 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 112,913 cuft Inflow hyds. Contrib. drain. area = 19, 20= 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

lyd. lo.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	4.569	2	732	18,910				EX WS-01	
2	SCS Runoff	6.758	2	730	27,938				EX WS-02A	
3	SCS Runoff	0.755	2	728	2,900				EX WS-02B	
4	SCS Runoff	3.315	2	726	12,242				EX WS-02C	
5	SCS Runoff	11.39	2	728	46,130				EX WS-02D	
6	SCS Runoff	0.894	2	724	3,014				EXWS-02E	
7	SCS Runoff	6.042	2	724	19,686				EXWS-02F	
3	SCS Runoff	1.567	2	726	5,734				EX WS-02G	
9	SCS Runoff	2.521	2	732	11,510				EX WS-02H	
10	SCS Runoff	5.852	2	732	27,051				EX WS-02I	
11	SCS Runoff	2.120	2	724	7,355				EX WS-02J	
12	SCS Runoff	0.314	2	730	1,264				EX WS-03	
13	Reservoir	6.739	2	730	25,739	2	143.63	1,533	36 INCH PIPE (#1)	
14	Reservoir	11.13	2	730	41,147	5	139.17	3,870	TWIN 36IN PIPES (#2)	
15	Reservoir	0.908	2	724	2,362	6	139.64	501	24 INCH PIPE	
16	Reservoir	5.901	2	724	18,171	7	139.51	1,323	36 INCH PIPE (#2)	
17	Reservoir	2.826	2	730	7,621	9	137.50	3,739	36 INCH PIPE (#3)	
18	Reservoir	5.822	2	732	23,823	10	135.74	2,482	TWO 36 INCH PIPES	
19	Combine	21.96	2	730	84,390	3, 4, 13,			<no description=""></no>	
20	Combine	14.53	2	730	62,704	14, 15, 8, 11, 16,			<no description=""></no>	
21	Combine	36.49	2	730	147,095	17, 18, 19, 20			Design Point B	
Existing-Hydraflow.gpw					Return F	Return Period: 25 Year			Monday, 12 / 4 / 2023	

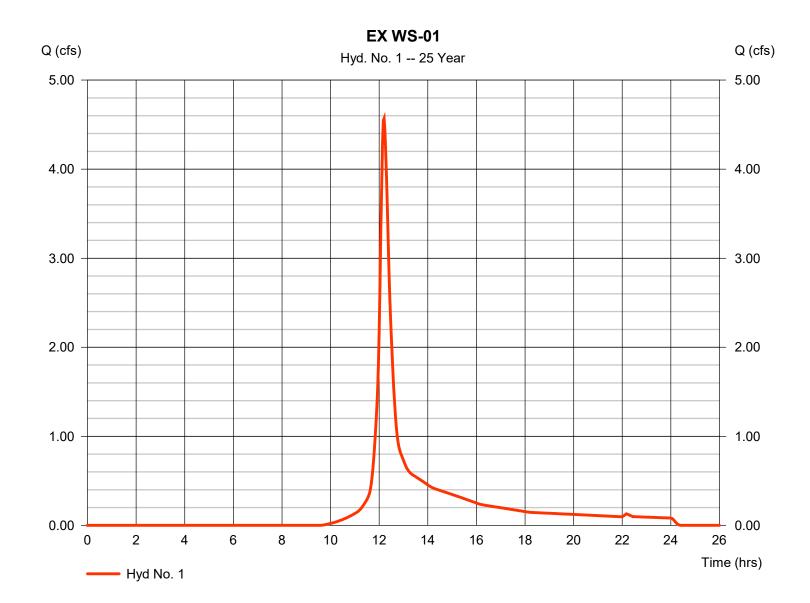
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 1

EX WS-01

Hydrograph type = SCS Runoff Peak discharge = 4.569 cfsStorm frequency = 25 yrs Time to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 18,910 cuft Drainage area Curve number = 65 = 1.942 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.10 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



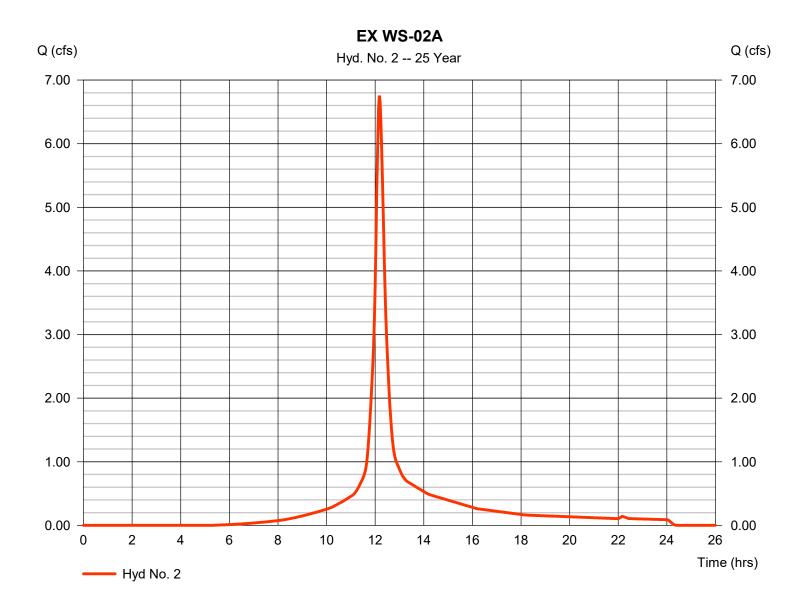
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 2

EXWS-02A

Hydrograph type = SCS Runoff Peak discharge = 6.758 cfsStorm frequency = 25 yrs Time to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 27,938 cuft Drainage area Curve number = 1.678 ac= 84 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.50 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



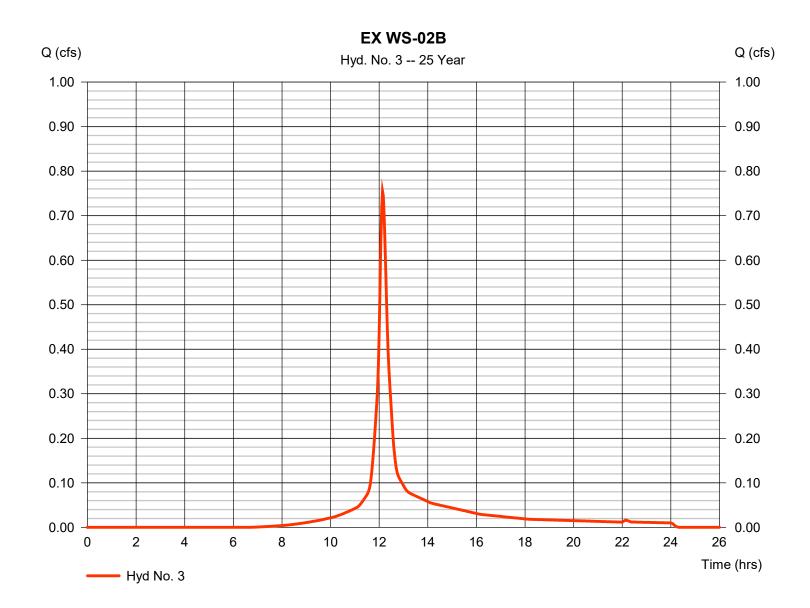
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 3

EXWS-02B

Hydrograph type = SCS Runoff Peak discharge = 0.755 cfsStorm frequency = 25 yrs Time to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2.900 cuftDrainage area Curve number = 0.186 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 11.00 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



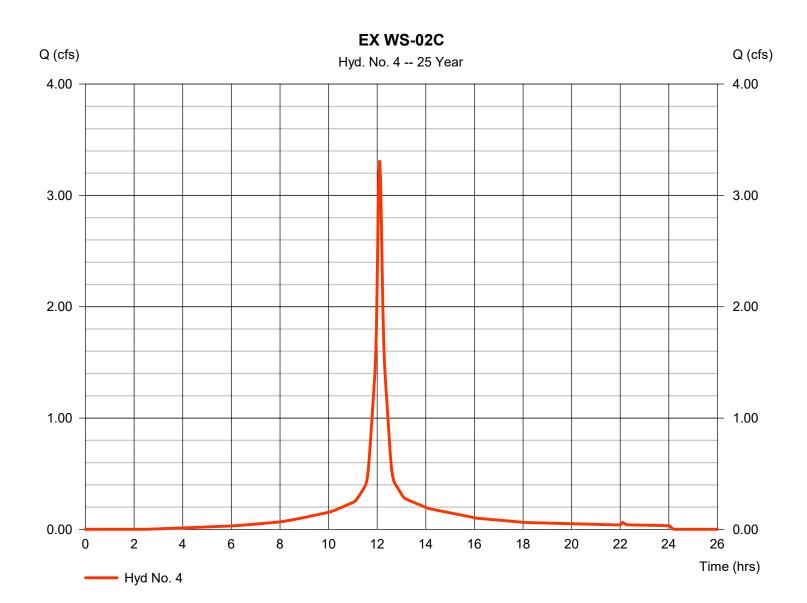
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 4

EXWS-02C

Hydrograph type = SCS Runoff Peak discharge = 3.315 cfsStorm frequency = 25 yrs Time to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 12,242 cuft Drainage area Curve number = 0.590 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



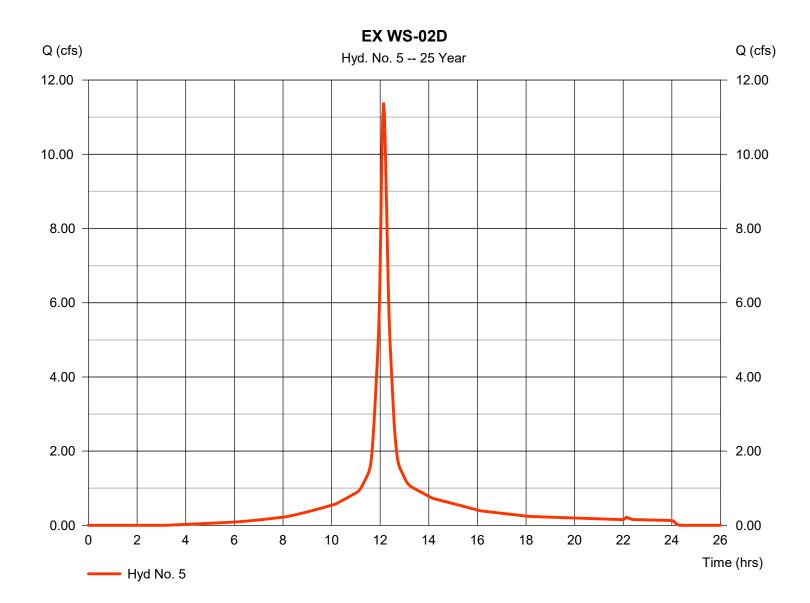
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 5

EXWS-02D

Hydrograph type = SCS Runoff Peak discharge = 11.39 cfsStorm frequency = 25 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 46,130 cuftDrainage area = 2.246 ac Curve number = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



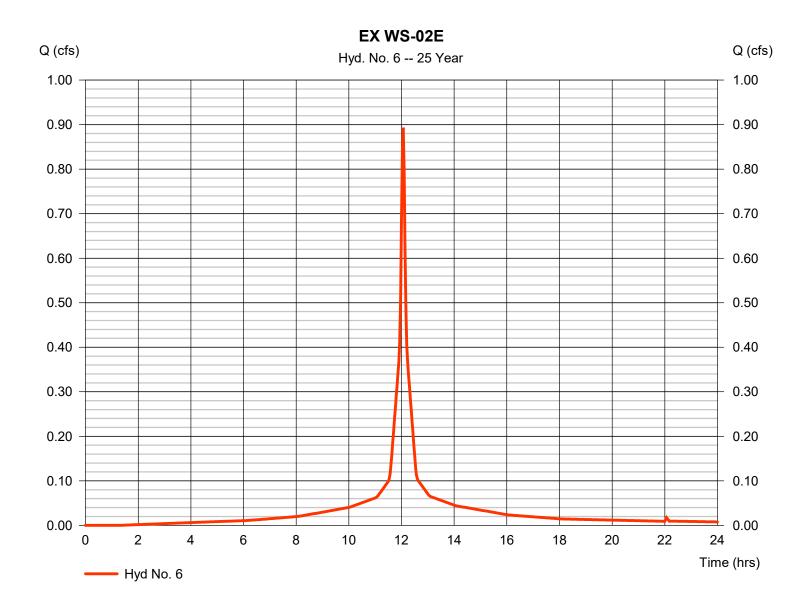
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 6

EXWS-02E

Hydrograph type = SCS Runoff Peak discharge = 0.894 cfsStorm frequency = 25 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 3,014 cuftDrainage area Curve number = 0.146 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



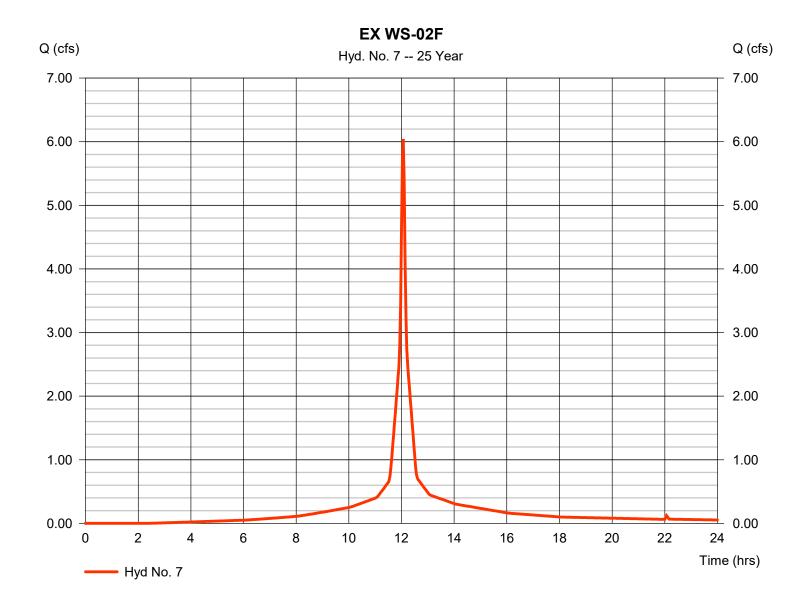
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 7

EXWS-02F

Hydrograph type = SCS Runoff Peak discharge = 6.042 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 19,686 cuft Drainage area Curve number = 93 = 1.012 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.50 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



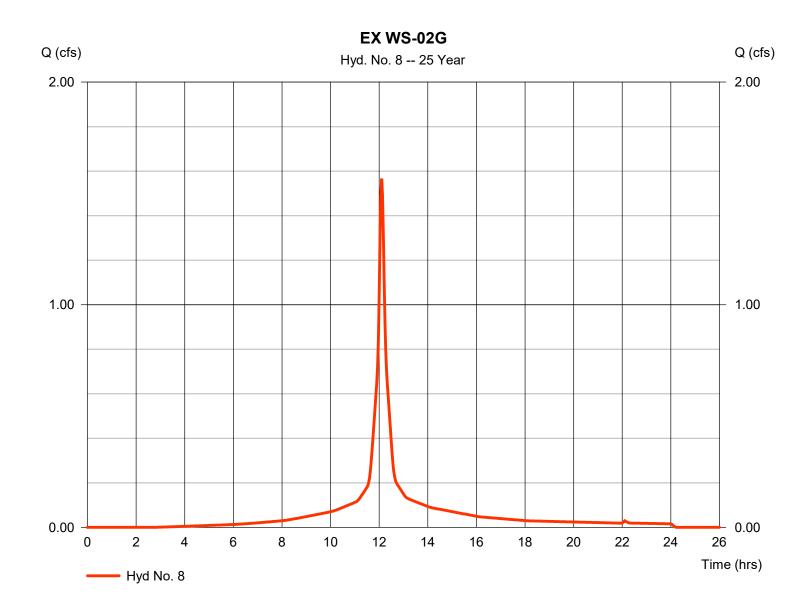
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 8

EXWS-02G

= SCS Runoff Hydrograph type Peak discharge = 1.567 cfsStorm frequency = 25 yrs Time to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 5,734 cuftDrainage area = 0.282 acCurve number = 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 6.90 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



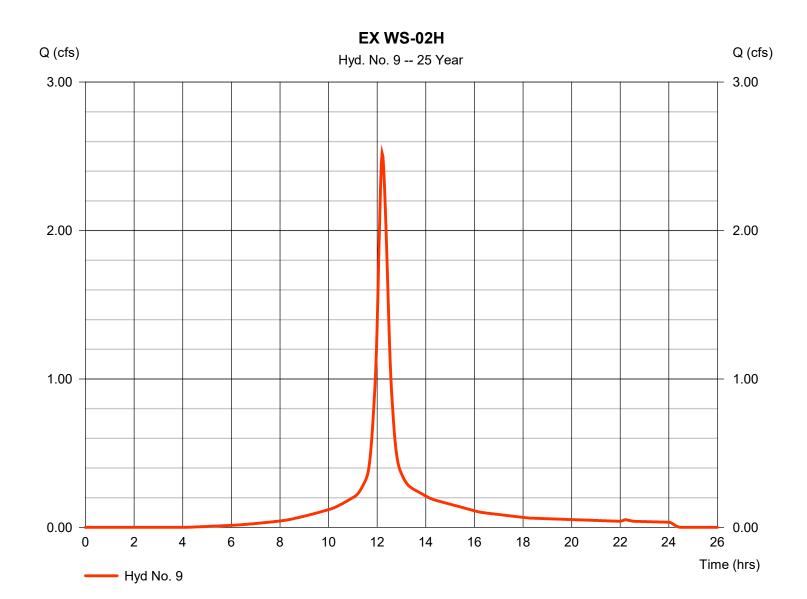
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 9

EXWS-02H

= SCS Runoff Hydrograph type Peak discharge = 2.521 cfsStorm frequency = 25 yrs Time to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 11,510 cuft Drainage area = 0.616 acCurve number = 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.30 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



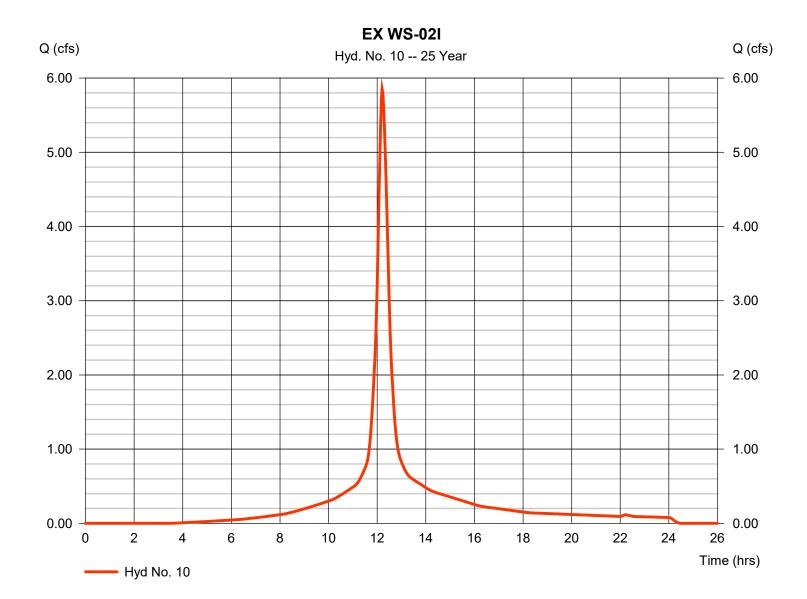
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 10

EX WS-02I

Hydrograph type = SCS Runoff Peak discharge = 5.852 cfsStorm frequency = 25 yrs Time to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 27,051 cuftDrainage area = 1.387 acCurve number = 90 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



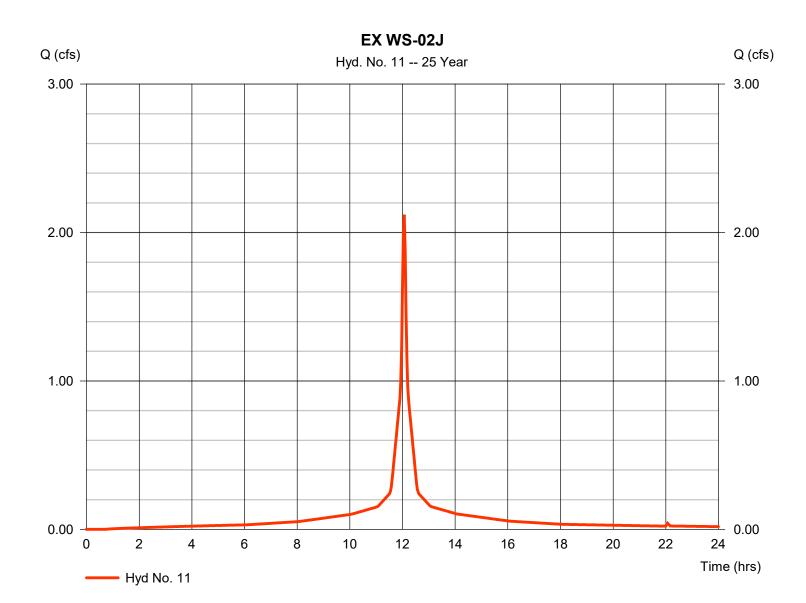
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 11

EXWS-02J

Hydrograph type = SCS Runoff Peak discharge = 2.120 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7,355 cuftDrainage area = 0.343 acCurve number = 98 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



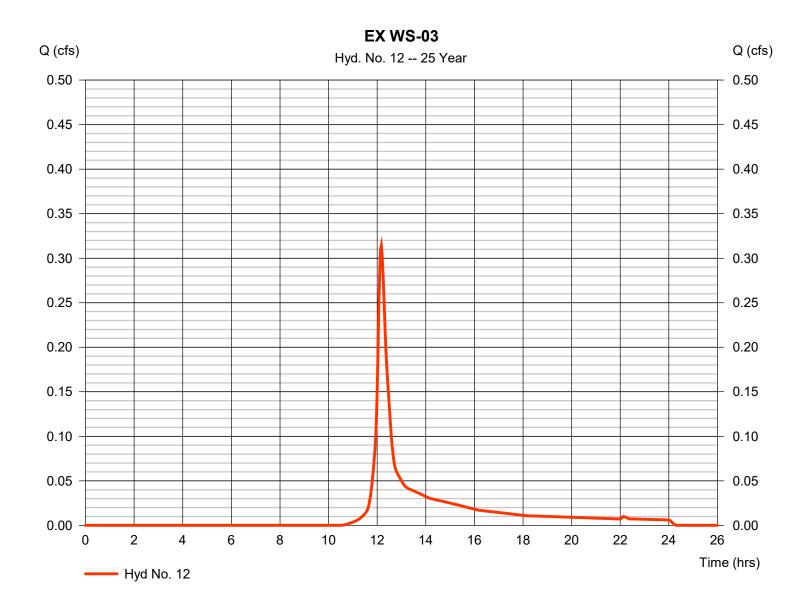
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 12

EX WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.314 cfsStorm frequency = 25 yrs Time to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1,264 cuft Drainage area Curve number = 0.154 ac= 59 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.50 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



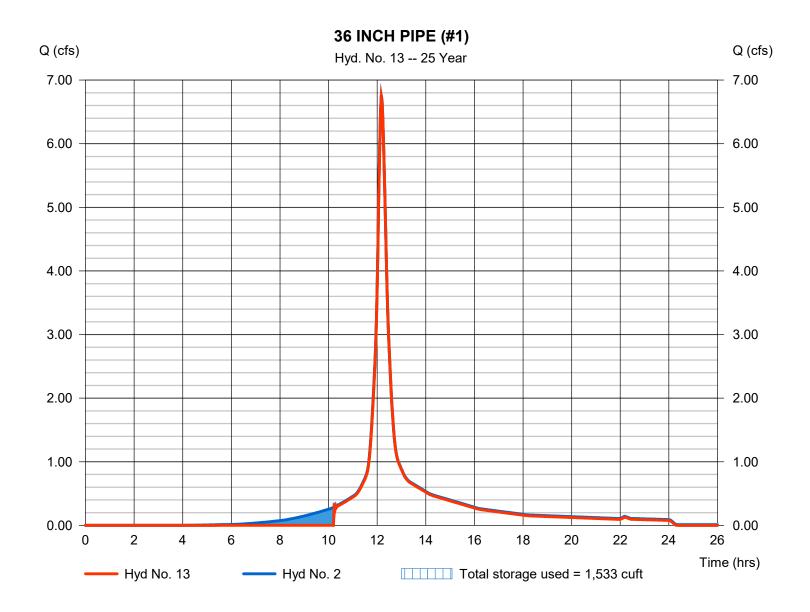
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 13

36 INCH PIPE (#1)

Hydrograph type = Reservoir Peak discharge = 6.739 cfsStorm frequency = 25 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 25,739 cuftMax. Elevation Inflow hyd. No. = 2 - EX WS-02A $= 143.63 \, \text{ft}$ Reservoir name = 36IN - 1Max. Storage = 1,533 cuft



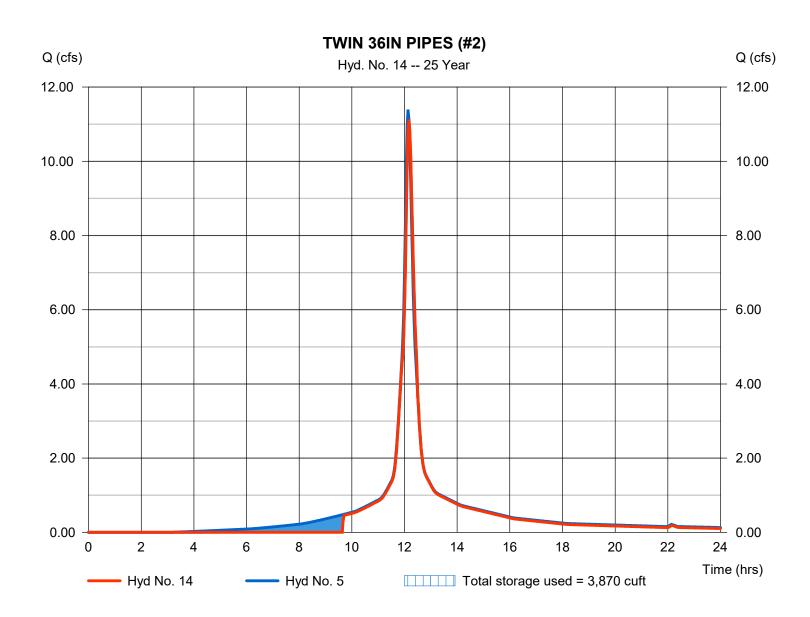
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 14

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 11.13 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 41,147 cuft Inflow hyd. No. = 5 - EX WS-02D Max. Elevation = 139.17 ft = Northern Twin 36IN Reservoir name Max. Storage = 3,870 cuft



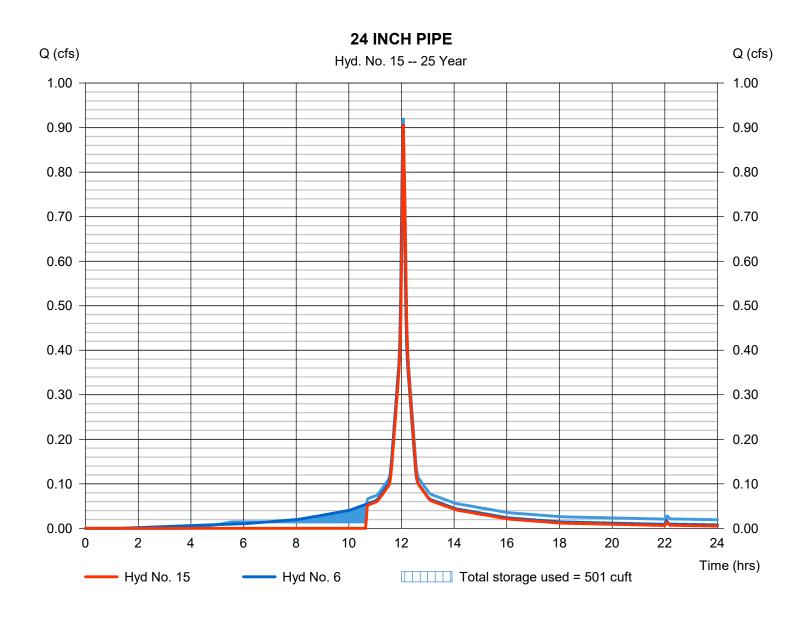
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 15

24 INCH PIPE

Hydrograph type Peak discharge = 0.908 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,362 cuftMax. Elevation Inflow hyd. No. = 6 - EX WS-02E = 139.64 ftReservoir name = 24INMax. Storage = 501 cuft



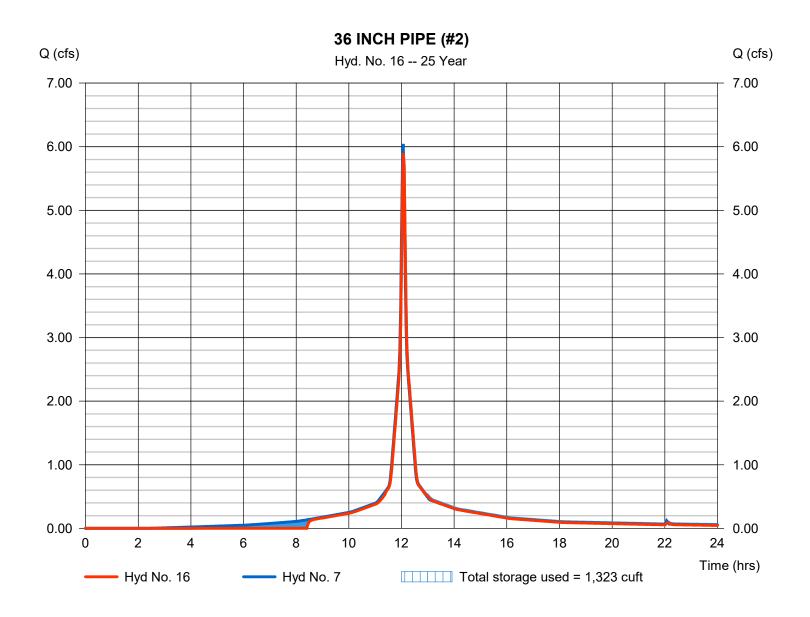
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 16

36 INCH PIPE (#2)

Hydrograph type = Reservoir Peak discharge = 5.901 cfsStorm frequency = 25 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 18,171 cuft = 7 - EX WS-02F Max. Elevation Inflow hyd. No. $= 139.51 \, \text{ft}$ Reservoir name = 36in - 2Max. Storage = 1,323 cuft



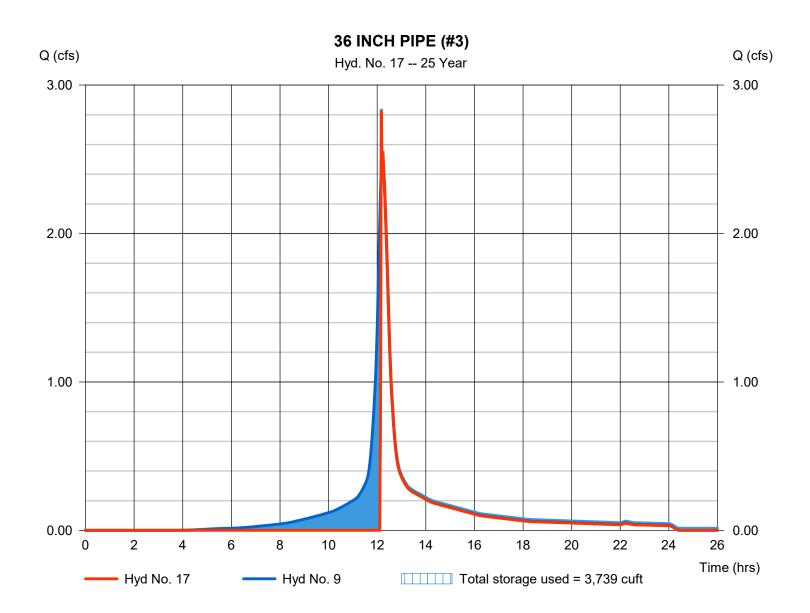
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 17

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 2.826 cfsStorm frequency = 25 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 7,621 cuft= 137.50 ft = 9 - EX WS-02H Max. Elevation Inflow hyd. No. Reservoir name = 36in - 3Max. Storage = 3,739 cuft



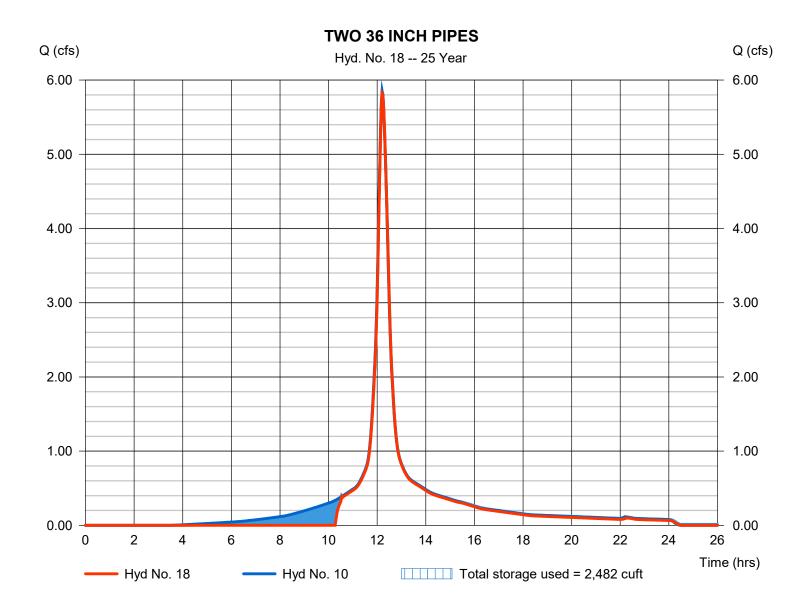
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 18

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 5.822 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 23,823 cuft Inflow hyd. No. Max. Elevation = 10 - EX WS-02I = 135.74 ftReservoir name = TWIN 36IN Max. Storage = 2,482 cuft



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

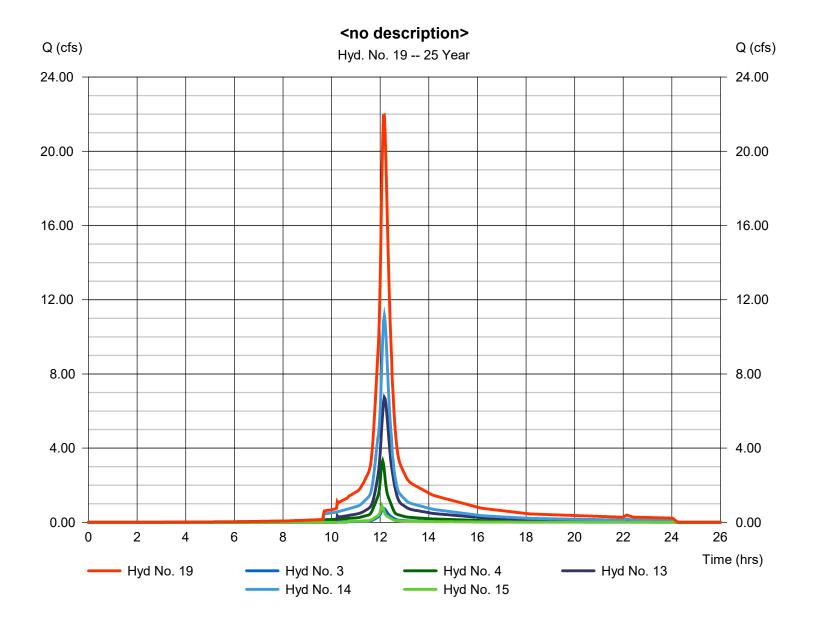
Hyd. No. 19

<no description>

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 2 min

Inflow hyds. = 3, 4, 13, 14, 15

Peak discharge = 21.96 cfs
Time to peak = 12.17 hrs
Hyd. volume = 84,390 cuft
Contrib. drain. area = 0.776 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

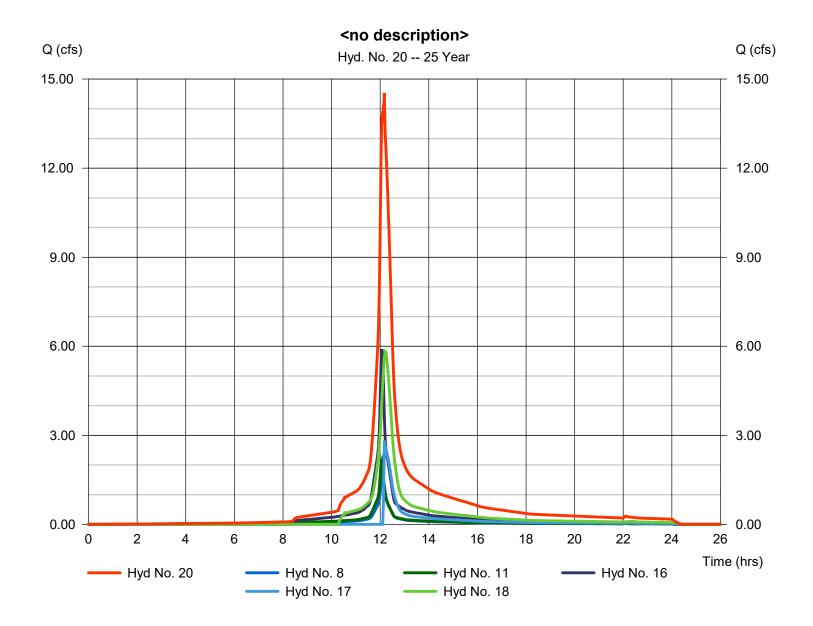
Hyd. No. 20

<no description>

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 2 min

Inflow hyds. = 8, 11, 16, 17, 18

Peak discharge = 14.53 cfs
Time to peak = 12.17 hrs
Hyd. volume = 62,704 cuft
Contrib. drain. area = 0.625 ac



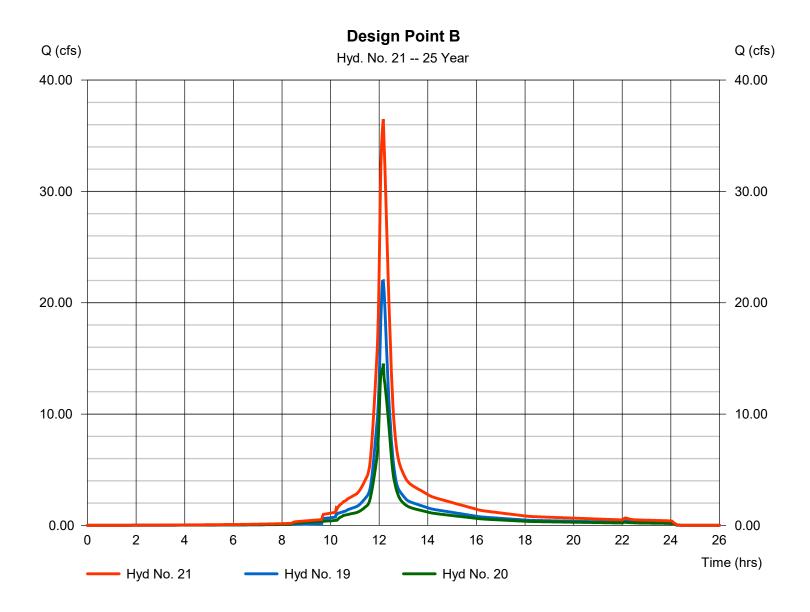
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 21

Design Point B

Hydrograph type = Combine Peak discharge = 36.49 cfsStorm frequency Time to peak = 25 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 147,095 cuft Inflow hyds. = 19, 20 Contrib. drain. area = 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

					Hydraf	low Hydrograph	s Extension for A	Extension for Autodesk® Civil 3D® by Autodesk, Inc. v20	
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	5.724	2	732	23,526				EX WS-01
2	SCS Runoff	7.893	2	730	32,844				EX WS-02A
3	SCS Runoff	0.895	2	728	3,454				EX WS-02B
4	SCS Runoff	3.785	2	726	14,087				EX WS-02C
5	SCS Runoff	13.06	2	728	53,326				EX WS-02D
6	SCS Runoff	1.015	2	724	3,444				EX WS-02E
7	SCS Runoff	6.897	2	724	22,653				EX WS-02F
8	SCS Runoff	1.793	2	726	6,613				EX WS-02G
9	SCS Runoff	2.913	2	732	13,399				EX WS-02H
10	SCS Runoff	6.727	2	732	31,344				EX WS-02I
11	SCS Runoff	2.404	2	724	8,370				EX WS-02J
12	SCS Runoff	0.408	2	730	1,611				EX WS-03
13	Reservoir	7.874	2	730	30,622	2	143.65	1,544	36 INCH PIPE (#1)
14	Reservoir	12.78	2	730	48,298	5	139.20	4,033	TWIN 36IN PIPES (#2)
15	Reservoir	1.042	2	724	2,790	6	139.65	503	24 INCH PIPE
16	Reservoir	6.741	2	724	21,127	7	139.53	1,370	36 INCH PIPE (#2)
17	Reservoir	2.899	2	732	9,505	9	137.50	3,742	36 INCH PIPE (#3)
18	Reservoir	6.701	2	732	28,092	10	135.75	2,500	TWO 36 INCH PIPES
19	Combine	25.35	2	730	99,252	3, 4, 13,			<no description=""></no>
20	Combine	18.18	2	724	73,706	14, 15, 8, 11, 16,			<no description=""></no>
21	Combine	42.76	2	728	172,958	17, 18, 19, 20			Design Point B
Ξxi	sting-Hydraflo			Return F	Return Period: 50 Year			Monday, 12 / 4 / 2023	

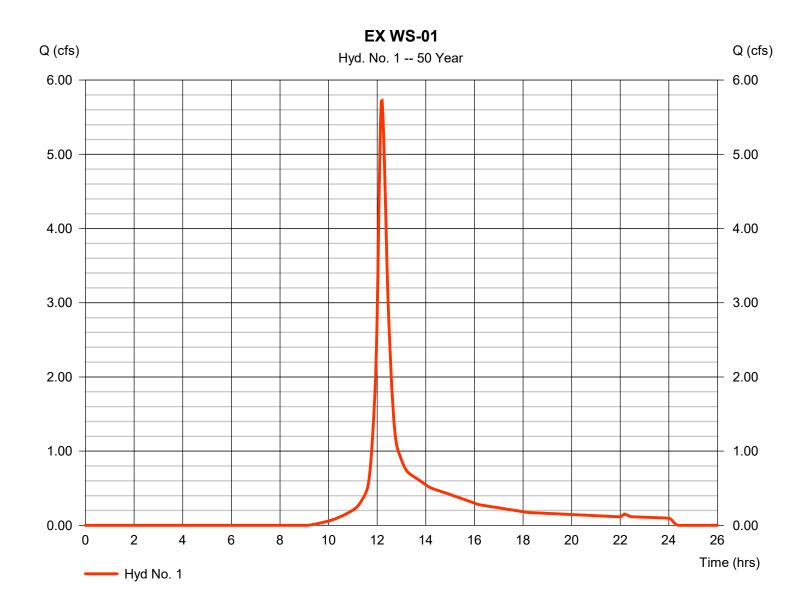
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 1

EX WS-01

Hydrograph type = SCS Runoff Peak discharge = 5.724 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 23,526 cuft Drainage area Curve number = 1.942 ac= 65 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.10 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



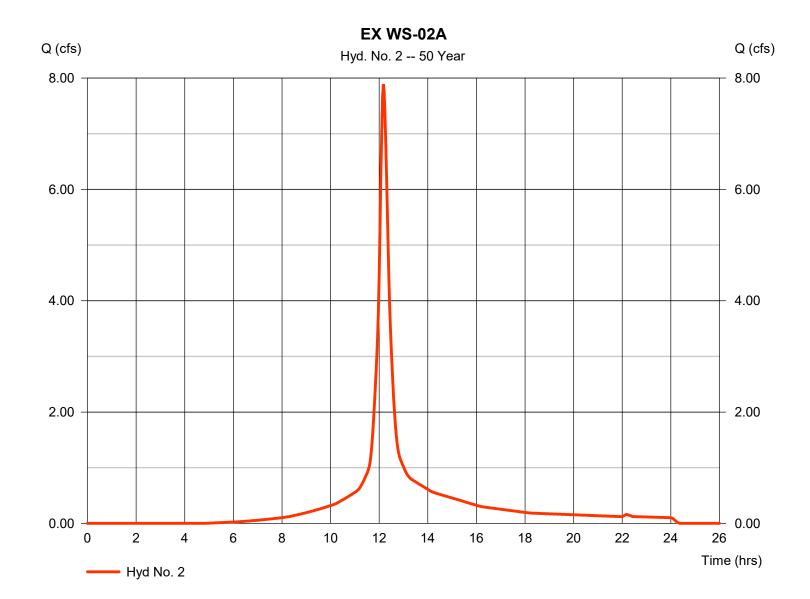
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 2

EXWS-02A

= SCS Runoff Hydrograph type Peak discharge = 7.893 cfsStorm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ = 32,844 cuft Time interval = 2 min Hyd. volume Drainage area Curve number = 1.678 ac= 84 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 16.50 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



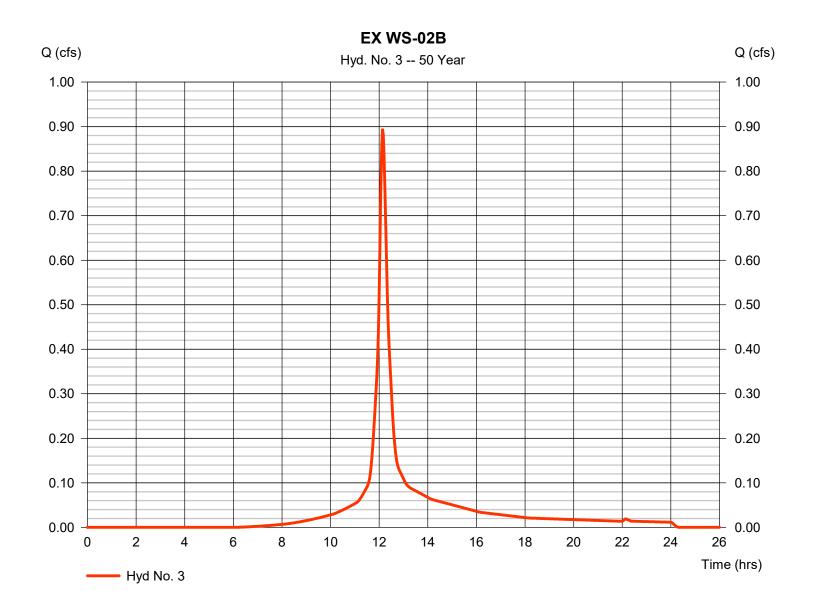
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 3

EXWS-02B

Hydrograph type = SCS Runoff Peak discharge = 0.895 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 3.454 cuft Drainage area Curve number = 0.186 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 11.00 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



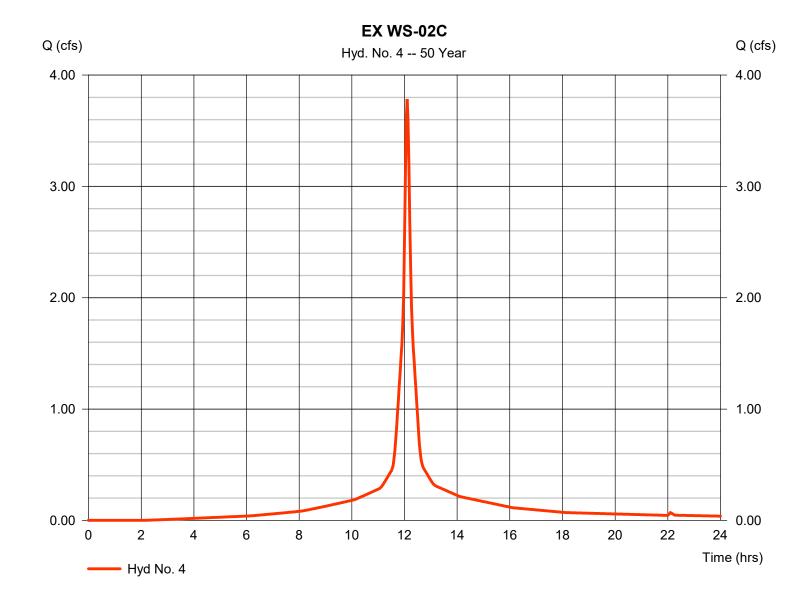
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 4

EXWS-02C

Hydrograph type = SCS Runoff Peak discharge = 3.785 cfsStorm frequency = 50 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 14,087 cuftDrainage area Curve number = 0.590 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



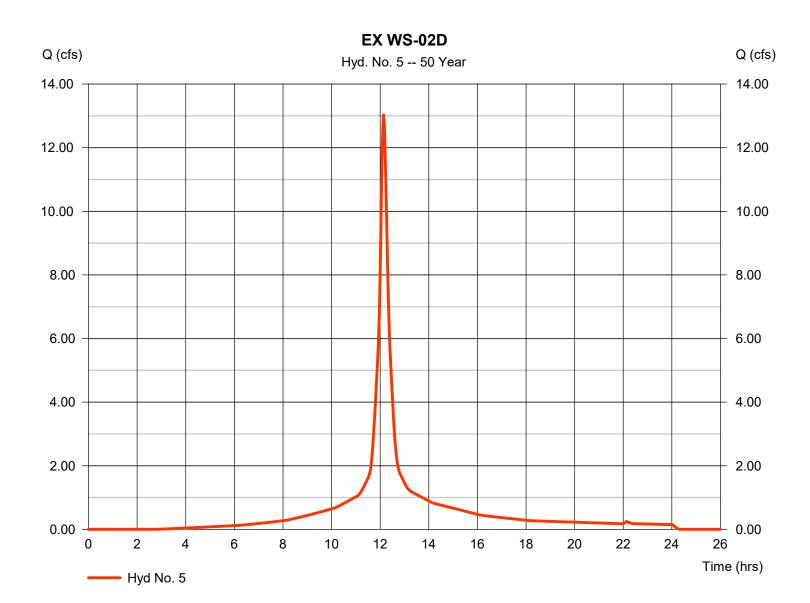
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 5

EXWS-02D

Hydrograph type = SCS Runoff Peak discharge = 13.06 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 53,326 cuft Drainage area = 2.246 ac Curve number = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



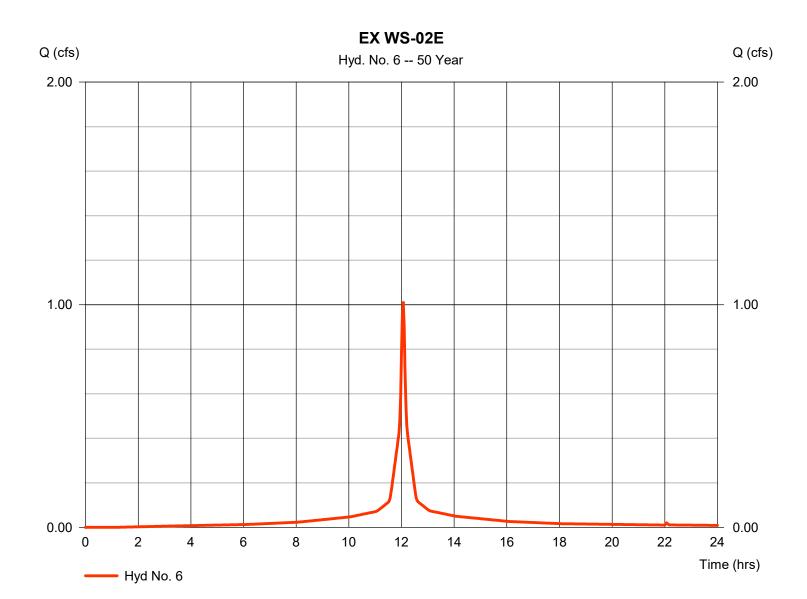
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 6

EXWS-02E

= SCS Runoff Hydrograph type Peak discharge = 1.015 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,444 cuftDrainage area = 0.146 acCurve number = 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



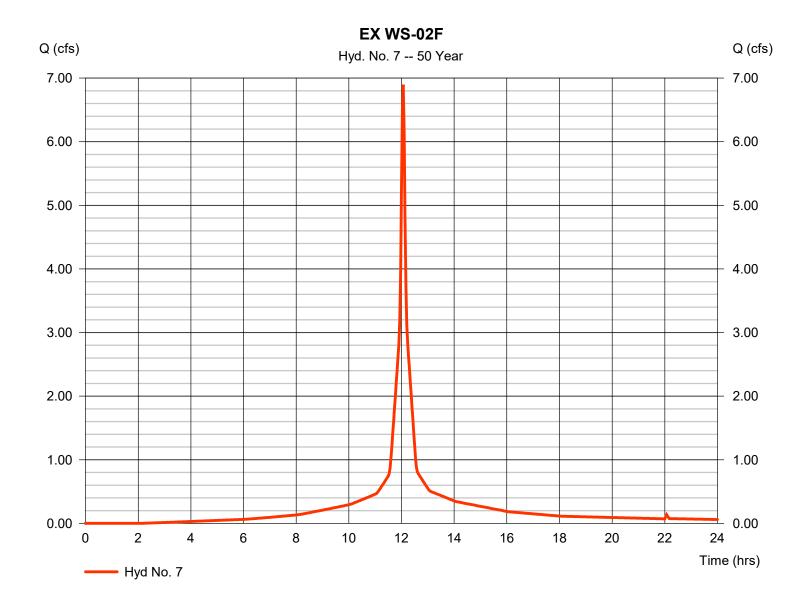
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 7

EXWS-02F

Hydrograph type = SCS Runoff Peak discharge = 6.897 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 22,653 cuft Drainage area Curve number = 1.012 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.50 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



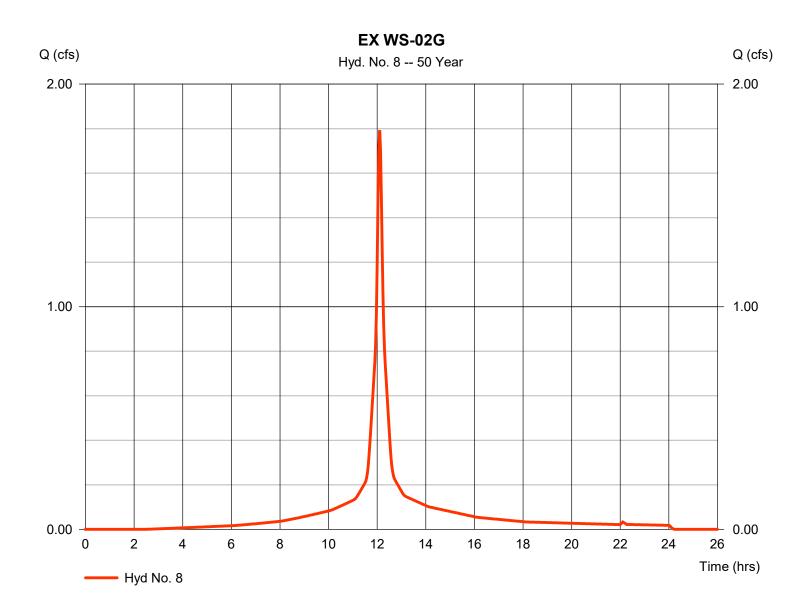
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 8

EXWS-02G

= SCS Runoff Hydrograph type Peak discharge = 1.793 cfsStorm frequency = 50 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 6,613 cuftDrainage area = 0.282 acCurve number = 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 6.90 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



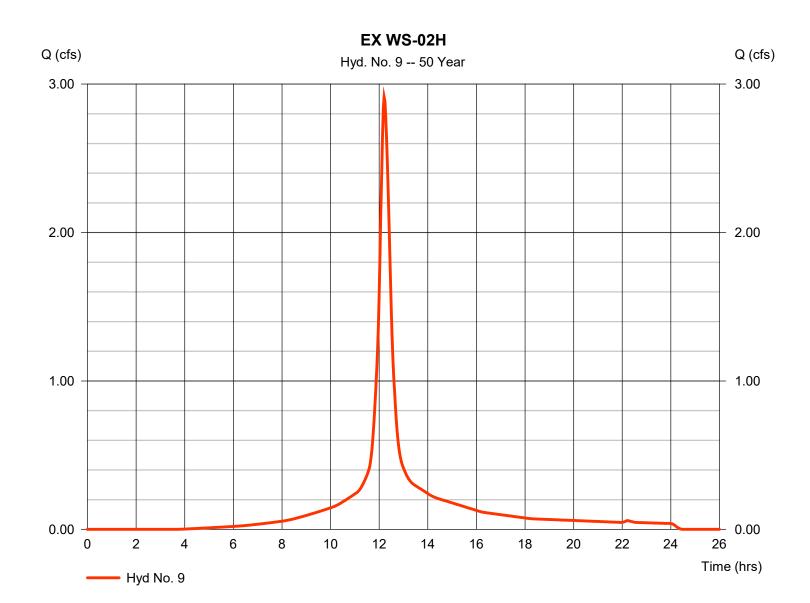
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 9

EXWS-02H

= SCS Runoff Hydrograph type Peak discharge = 2.913 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 13,399 cuft Drainage area Curve number = 0.616 ac= 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.30 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Monday, 12 / 4 / 2023

= 484

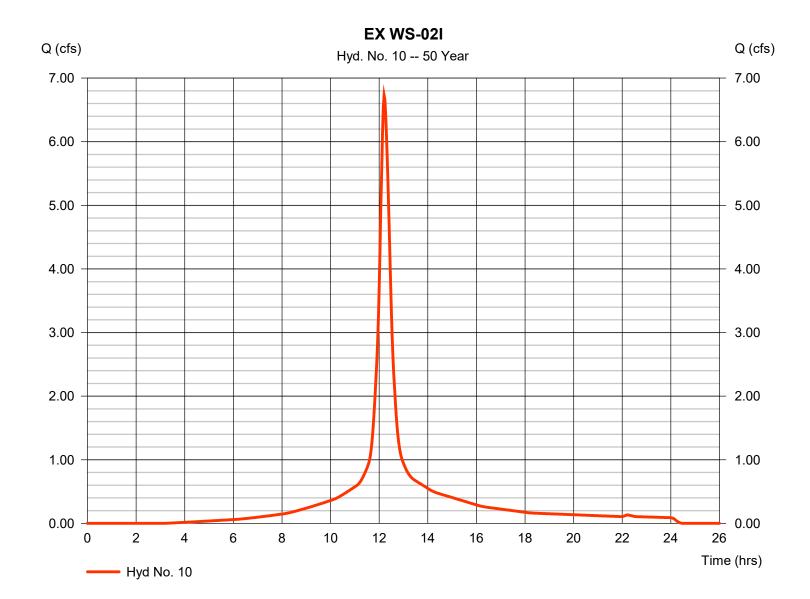
Hyd. No. 10

Storm duration

EX WS-02I

Hydrograph type = SCS Runoff Peak discharge = 6.727 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 31,344 cuft Drainage area = 1.387 acCurve number = 90 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 7.41 inDistribution = Type III

Shape factor



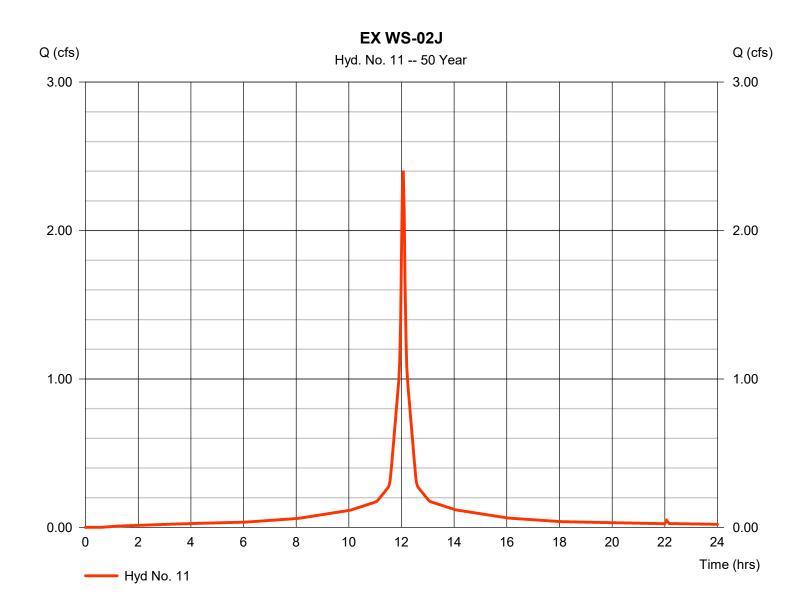
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 11

EXWS-02J

Hydrograph type = SCS Runoff Peak discharge = 2.404 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 8,370 cuftDrainage area Curve number = 0.343 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



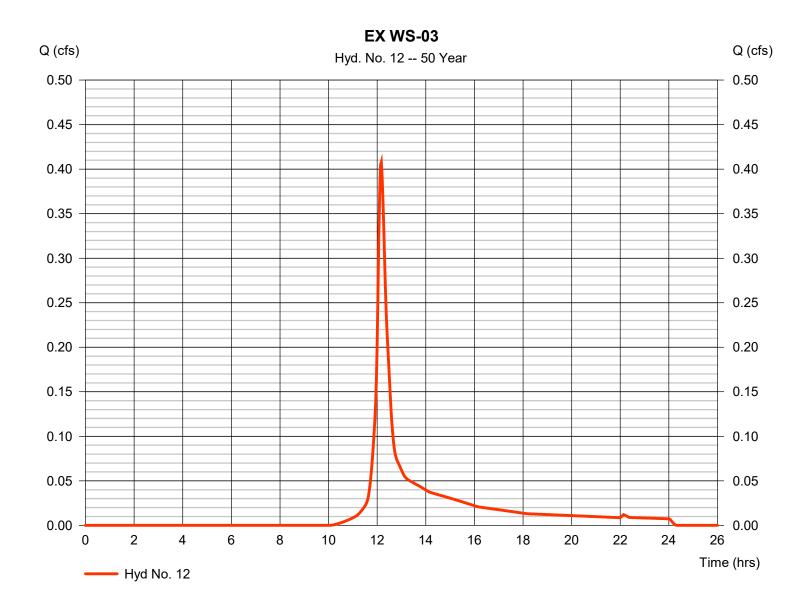
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 12

EX WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.408 cfsStorm frequency = 50 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1.611 cuft Drainage area Curve number = 0.154 ac= 59 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.50 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



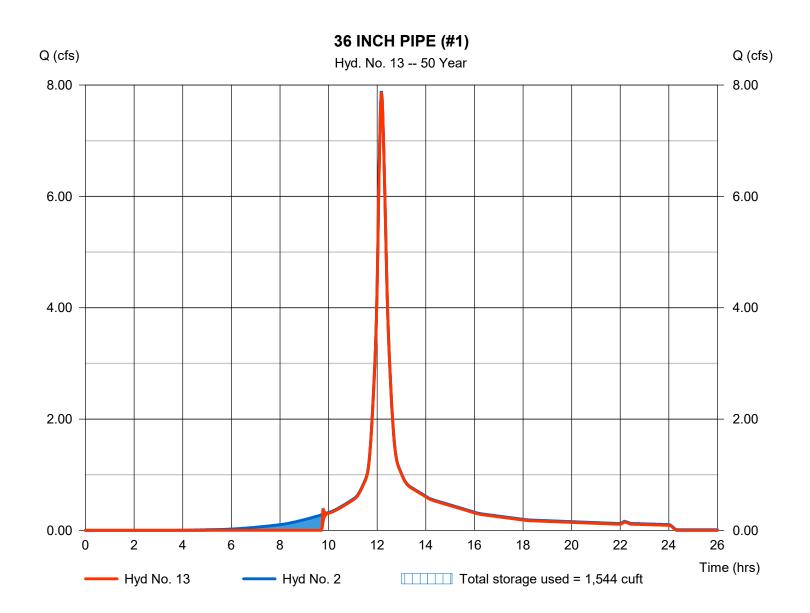
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 13

36 INCH PIPE (#1)

Hydrograph type = Reservoir Peak discharge = 7.874 cfsStorm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 30,622 cuftMax. Elevation Inflow hyd. No. = 2 - EX WS-02A $= 143.65 \, \text{ft}$ Reservoir name = 36IN - 1Max. Storage = 1,544 cuft



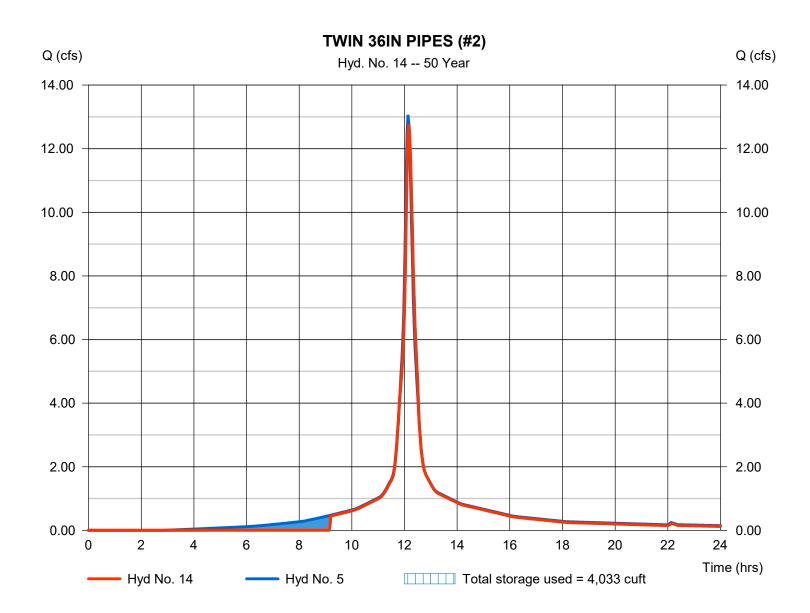
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 14

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 12.78 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 48,298 cuft = 5 - EX WS-02D Max. Elevation Inflow hyd. No. = 139.20 ft= Northern Twin 36IN Reservoir name Max. Storage = 4,033 cuft



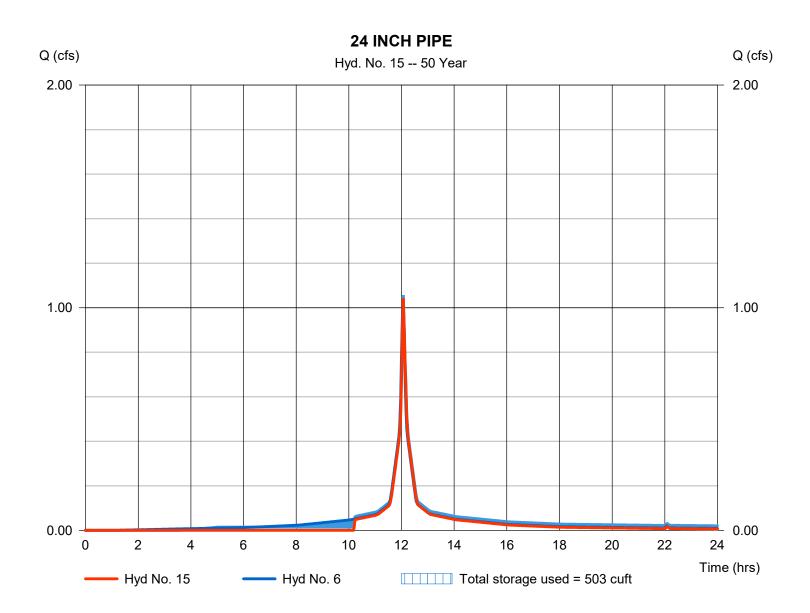
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 15

24 INCH PIPE

Hydrograph type = Reservoir Peak discharge = 1.042 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,790 cuftMax. Elevation Inflow hyd. No. = 6 - EX WS-02E $= 139.65 \, \text{ft}$ Reservoir name = 24INMax. Storage = 503 cuft



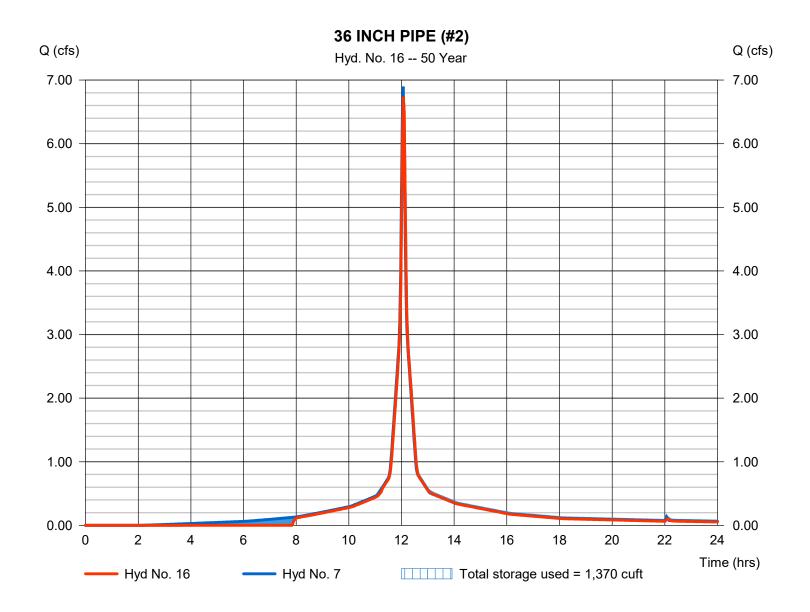
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 16

36 INCH PIPE (#2)

Hydrograph type = Reservoir Peak discharge = 6.741 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 21,127 cuft Inflow hyd. No. Max. Elevation = 7 - EX WS-02F = 139.53 ftReservoir name = 36in - 2Max. Storage = 1,370 cuft



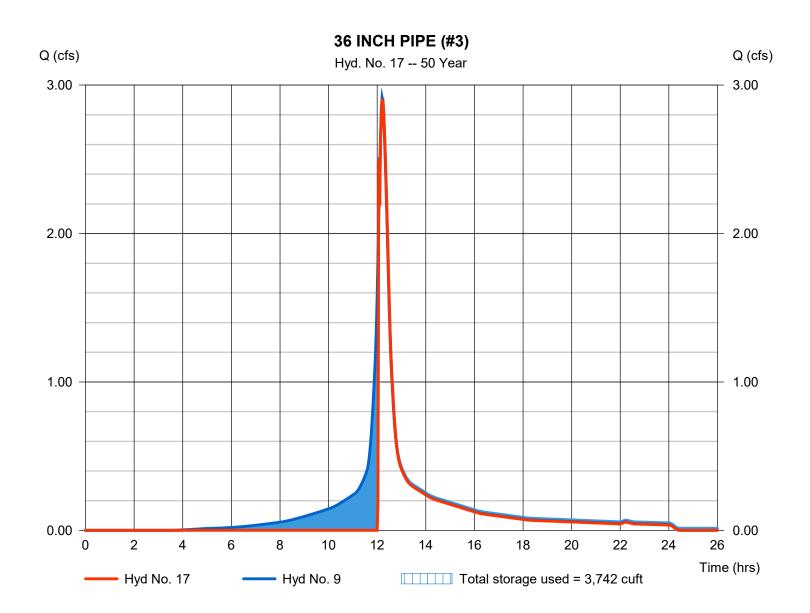
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 17

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 2.899 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 9,505 cuft= 137.50 ft Max. Elevation Inflow hyd. No. = 9 - EX WS-02H Reservoir name = 36in - 3Max. Storage = 3,742 cuft



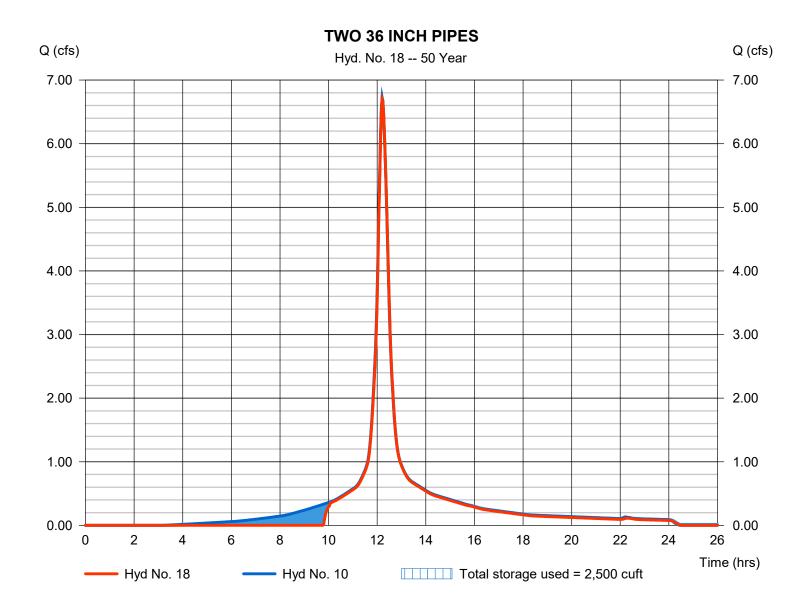
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Monday, 12 / 4 / 2023

Hyd. No. 18

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 6.701 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 28,092 cuft Inflow hyd. No. Max. Elevation = 10 - EX WS-02I $= 135.75 \, \text{ft}$ Reservoir name = TWIN 36IN Max. Storage = 2,500 cuft



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Monday, 12 / 4 / 2023

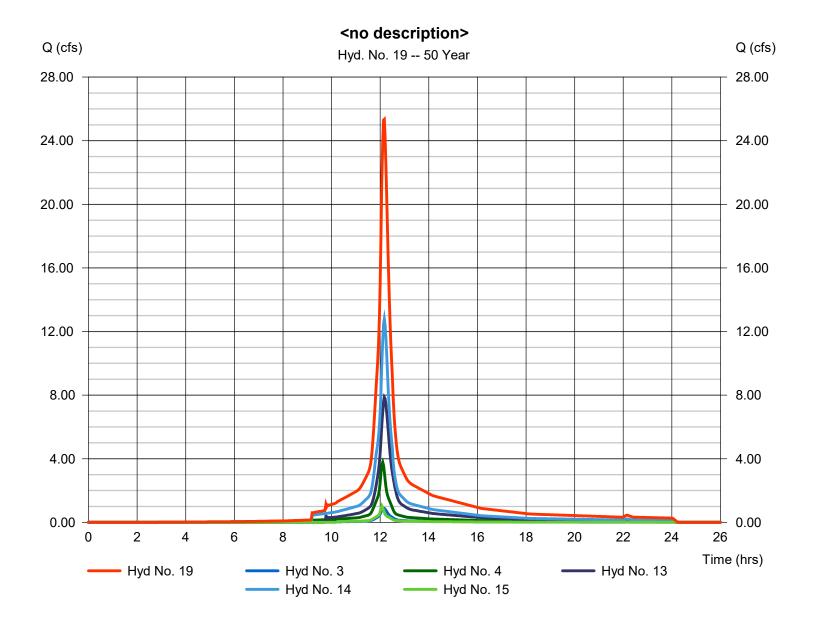
Hyd. No. 19

<no description>

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min

Inflow hyds. = 3, 4, 13, 14, 15

Peak discharge = 25.35 cfs
Time to peak = 12.17 hrs
Hyd. volume = 99,252 cuft
Contrib. drain. area = 0.776 ac



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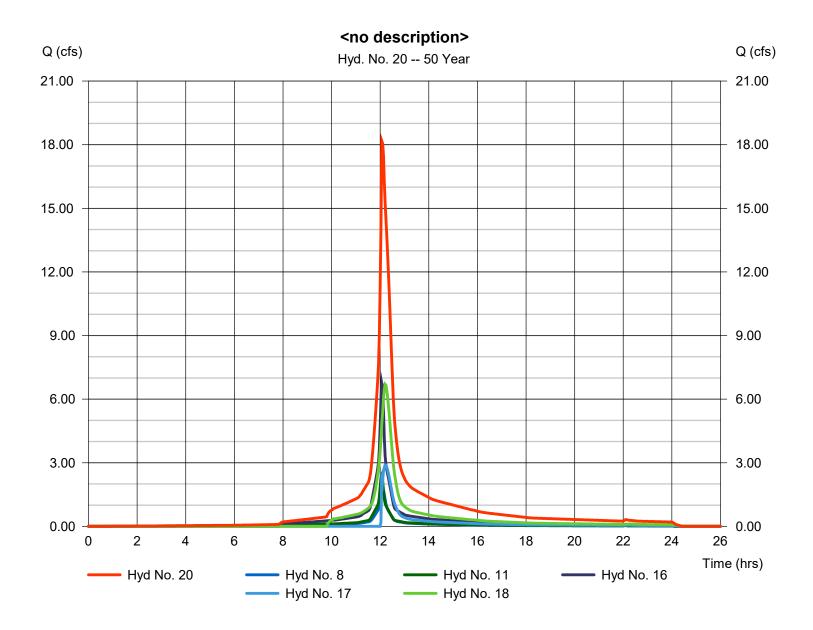
Hyd. No. 20

<no description>

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min

Inflow hyds. = 8, 11, 16, 17, 18

Peak discharge = 18.18 cfs
Time to peak = 12.07 hrs
Hyd. volume = 73,706 cuft
Contrib. drain. area = 0.625 ac



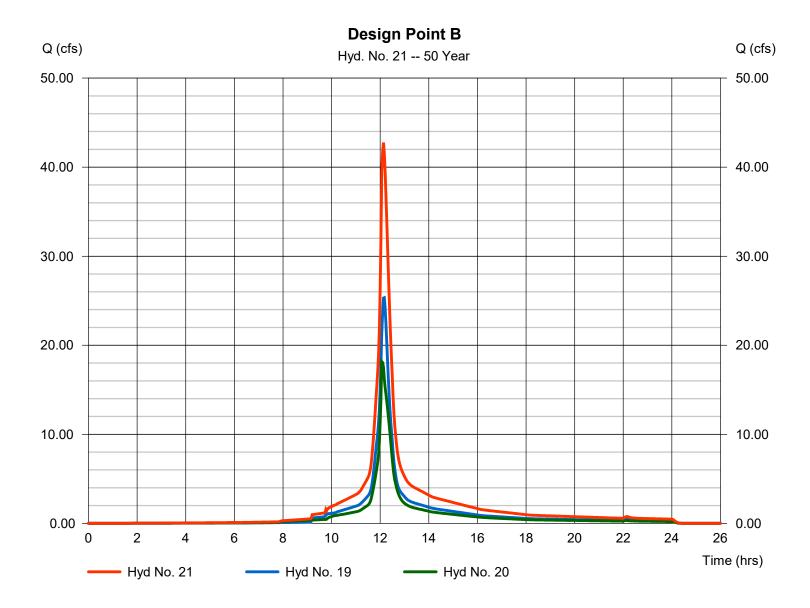
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Hyd. No. 21

Design Point B

Hydrograph type = Combine Peak discharge = 42.76 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 172,958 cuft Inflow hyds. Contrib. drain. area = 19, 20= 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	7.011	2	730	28,668				EX WS-01	
2	SCS Runoff	9.103	2	730	38,140				EX WS-02A	
3	SCS Runoff	1.046	2	728	4,056				EX WS-02B	
4	SCS Runoff	4.285	2	726	16,063				EX WS-02C	
5	SCS Runoff	14.84	2	728	61,043				EX WS-02D	
6	SCS Runoff	1.145	2	724	3,905				EX WS-02E	
7	SCS Runoff	7.807	2	724	25,830				EX WS-02F	
8	SCS Runoff	2.033	2	726	7,555				EX WS-02G	
9	SCS Runoff	3.330	2	732	15,431				EX WS-02H	
10	SCS Runoff	7.659	2	732	35,951				EX WS-02I	
11	SCS Runoff	2.707	2	724	9,455				EX WS-02J	
12	SCS Runoff	0.513	2	730	2,003				EX WS-03	
13	Reservoir	8.866	2	732	35,896	2	143.74	1,590	36 INCH PIPE (#1)	
14	Reservoir	14.56	2	730	55,977	5	139.24	4,189	TWIN 36IN PIPES (#2)	
15	Reservoir	1.129	2	724	3,248	6	139.65	504	24 INCH PIPE	
16	Reservoir	7.332	2	726	24,295	7	139.57	1,442	36 INCH PIPE (#2)	
17	Reservoir	3.311	2	732	11,531	9	137.50	3,755	36 INCH PIPE (#3)	
18	Reservoir	7.629	2	732	32,678	10	135.77	2,518	TWO 36 INCH PIPES	
19	Combine	28.95	2	728	115,241	3, 4, 13,			<no description=""></no>	
20	Combine	20.65	2	726	85,513	14, 15, 8, 11, 16,			<no description=""></no>	
21	Combine	49.09	2	728	200,754	17, 18, 19, 20			Design Point B	
Existing-Hydraflow.gpw					Return F	Return Period: 100 Year			Monday, 12 / 4 / 2023	

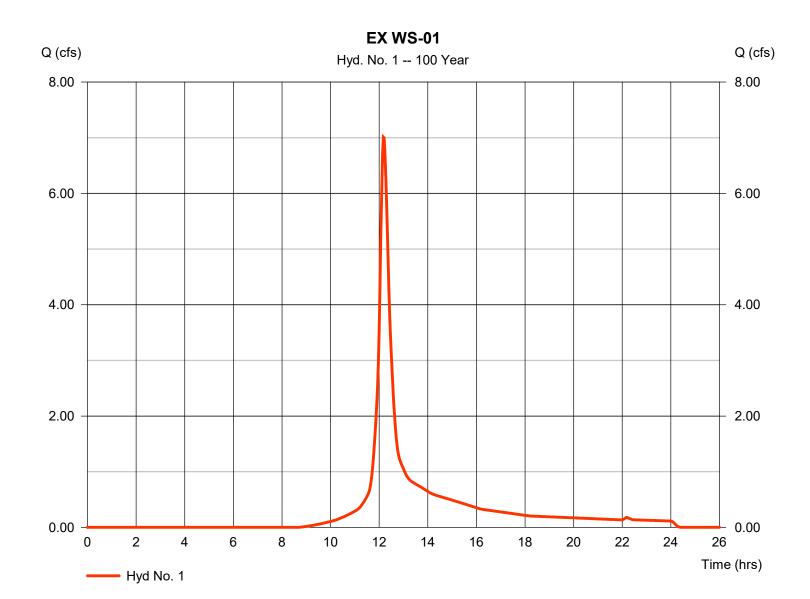
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 1

EX WS-01

Hydrograph type = SCS Runoff Peak discharge = 7.011 cfsStorm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ = 28,668 cuft Time interval = 2 min Hyd. volume Drainage area Curve number = 1.942 ac= 65 = 0.0 % = 0 ftBasin Slope Hydraulic length Tc method Time of conc. (Tc) = 16.10 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



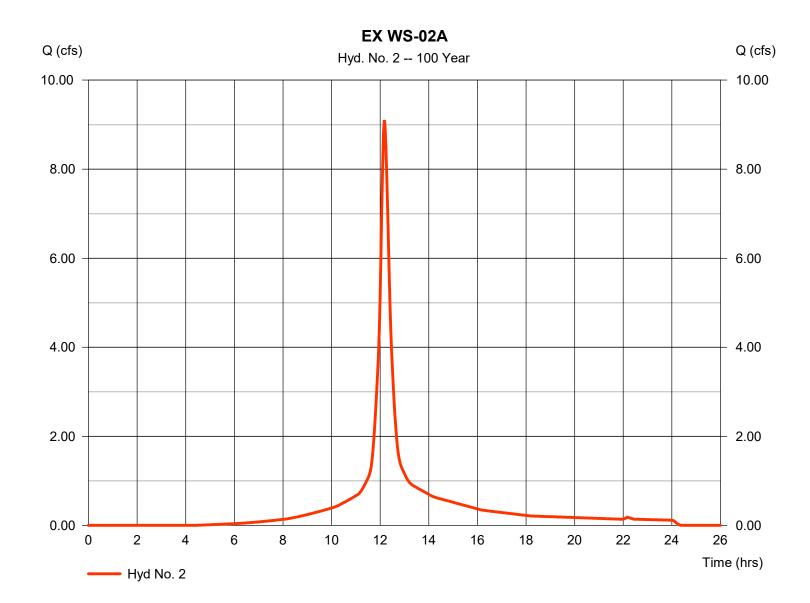
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Monday, 12 / 4 / 2023

Hyd. No. 2

EXWS-02A

Hydrograph type = SCS Runoff Peak discharge = 9.103 cfsStorm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 38,140 cuftDrainage area Curve number = 1.678 ac= 84 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.50 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

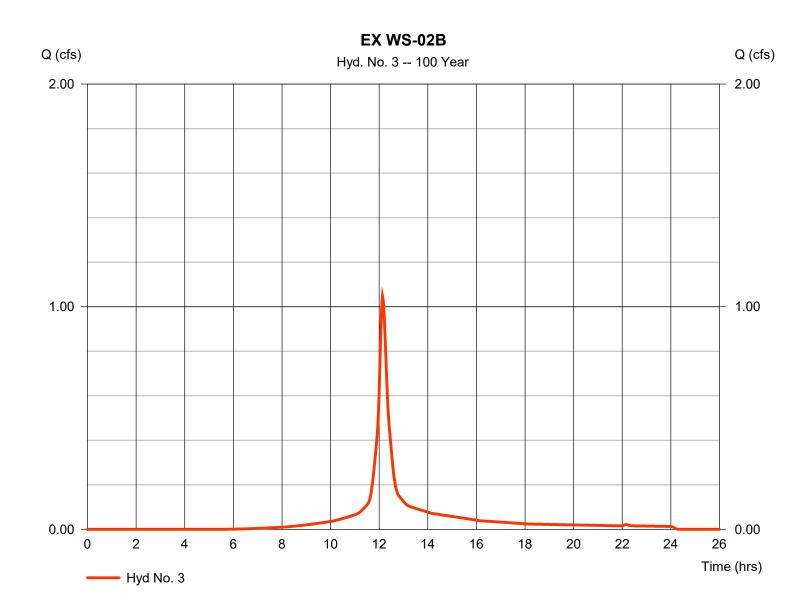


Monday, 12 / 4 / 2023

Hyd. No. 3

EXWS-02B

= SCS Runoff Hydrograph type Peak discharge = 1.046 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 4,056 cuftDrainage area Curve number = 0.186 ac= 79 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.00 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



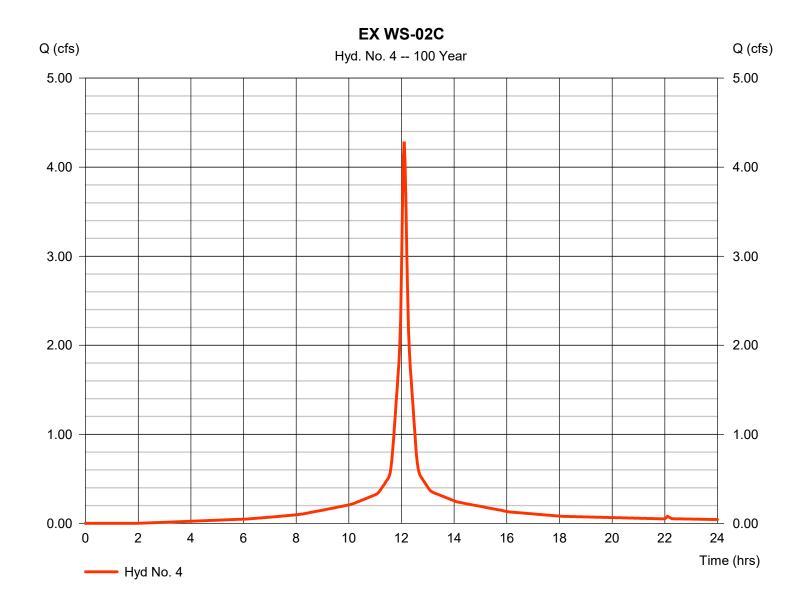
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Monday, 12 / 4 / 2023

Hyd. No. 4

EXWS-02C

Hydrograph type = SCS Runoff Peak discharge = 4.285 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 16,063 cuftDrainage area Curve number = 93 = 0.590 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

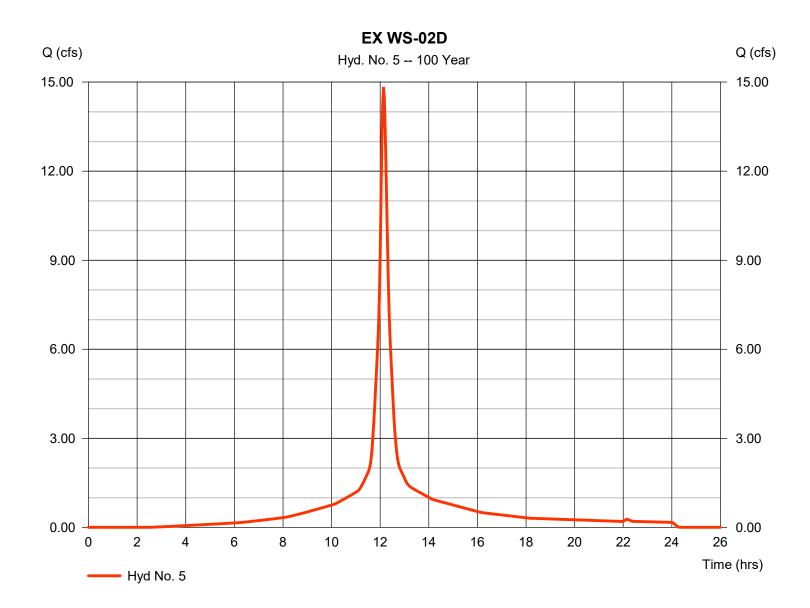


Monday, 12 / 4 / 2023

Hyd. No. 5

EXWS-02D

Hydrograph type = SCS Runoff Peak discharge = 14.84 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 61,043 cuft Drainage area = 2.246 ac Curve number = 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

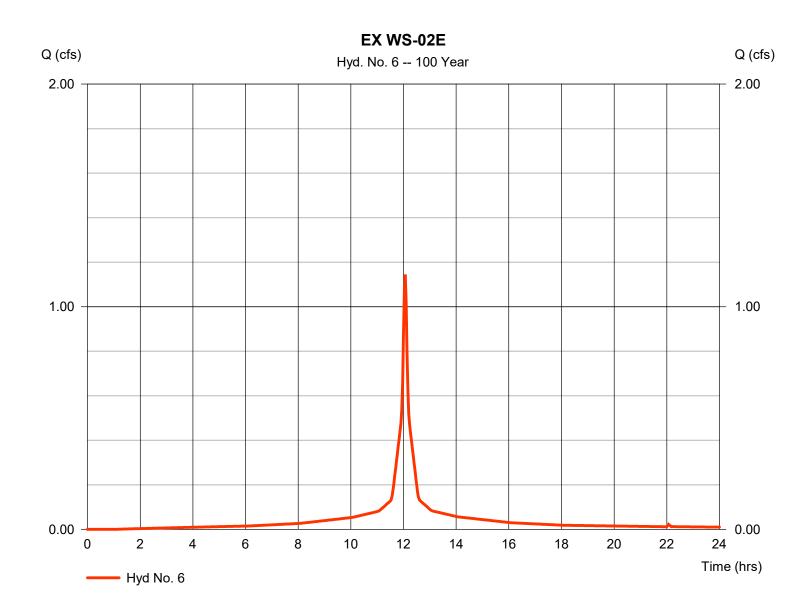


Monday, 12 / 4 / 2023

Hyd. No. 6

EXWS-02E

Hydrograph type = SCS Runoff Peak discharge = 1.145 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,905 cuftDrainage area Curve number = 0.146 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

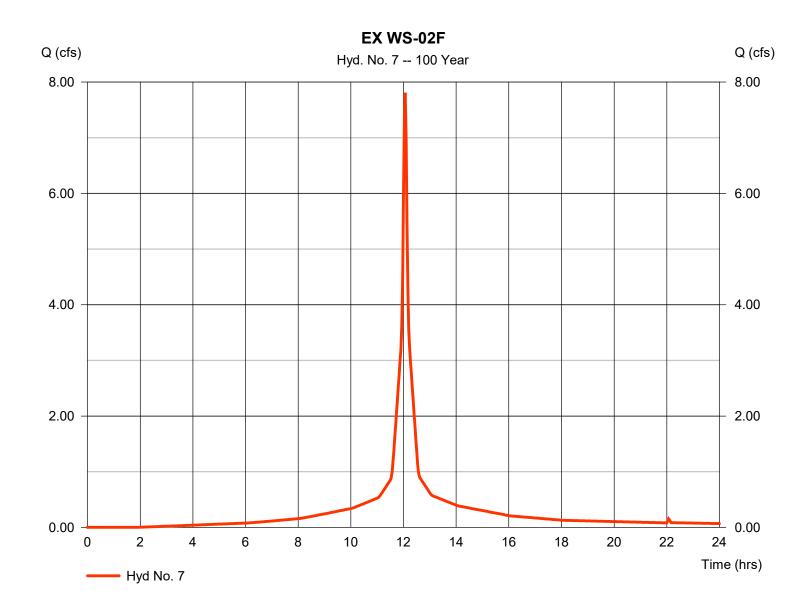


Monday, 12 / 4 / 2023

Hyd. No. 7

EXWS-02F

Hydrograph type = SCS Runoff Peak discharge = 7.807 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 25,830 cuftDrainage area Curve number = 1.012 ac= 93 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.50 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

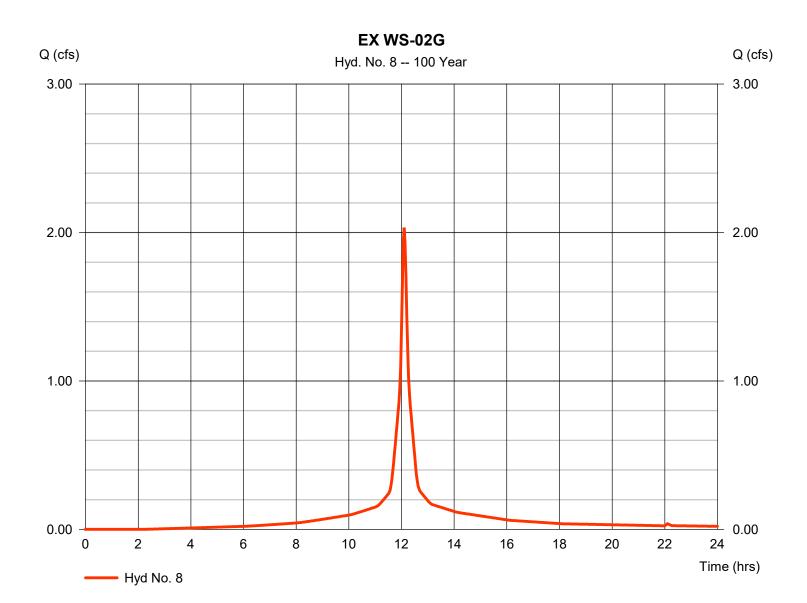


Monday, 12 / 4 / 2023

Hyd. No. 8

EXWS-02G

Hydrograph type = SCS Runoff Peak discharge = 2.033 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 7,555 cuftDrainage area = 0.282 acCurve number = 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 6.90 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

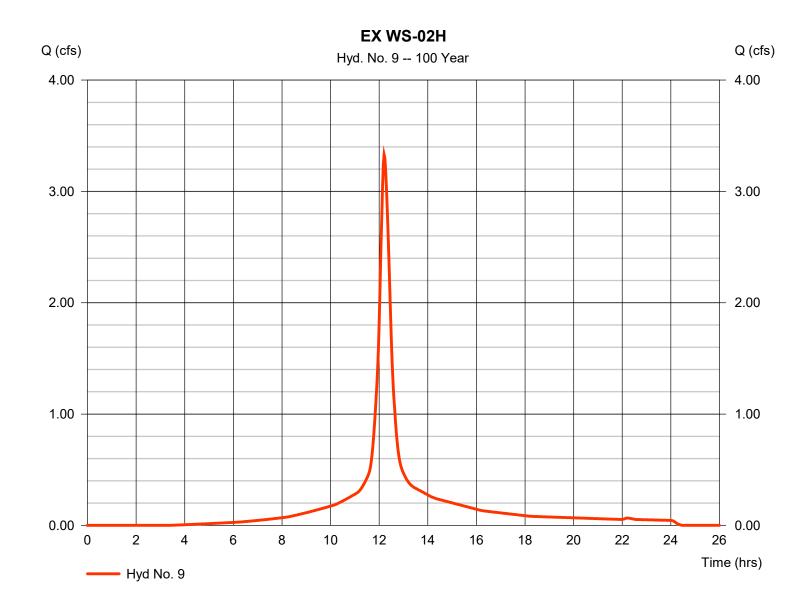


Monday, 12 / 4 / 2023

Hyd. No. 9

EXWS-02H

Hydrograph type = SCS Runoff Peak discharge = 3.330 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 15,431 cuft Drainage area Curve number = 0.616 ac= 88 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 17.30 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



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= 7.659 cfs

 $= 12.20 \, hrs$

= 90

= 0 ft

= 484

= 35,951 cuft

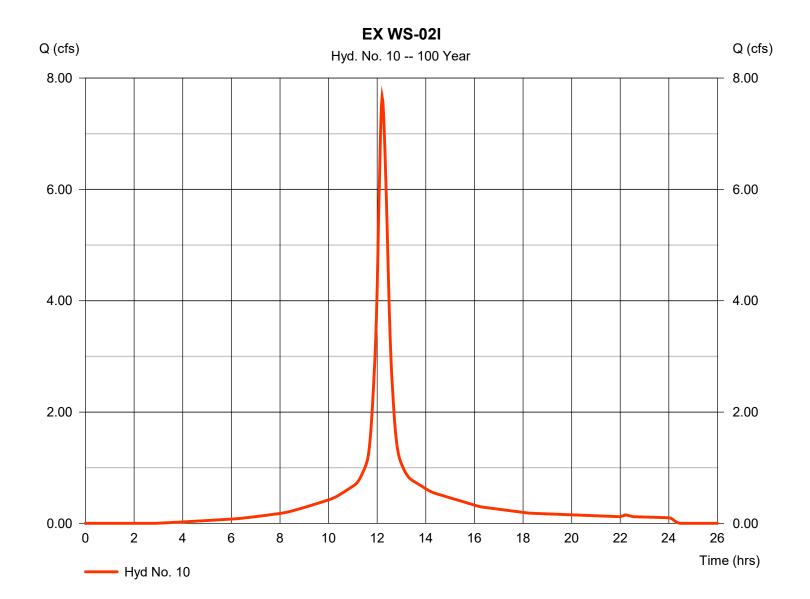
= 18.60 min

= Type III

Hyd. No. 10

EX WS-02I

Hydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak Time interval = 2 min Hyd. volume Drainage area = 1.387 acCurve number Basin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = User Total precip. = 8.34 inDistribution Storm duration = 24 hrs Shape factor

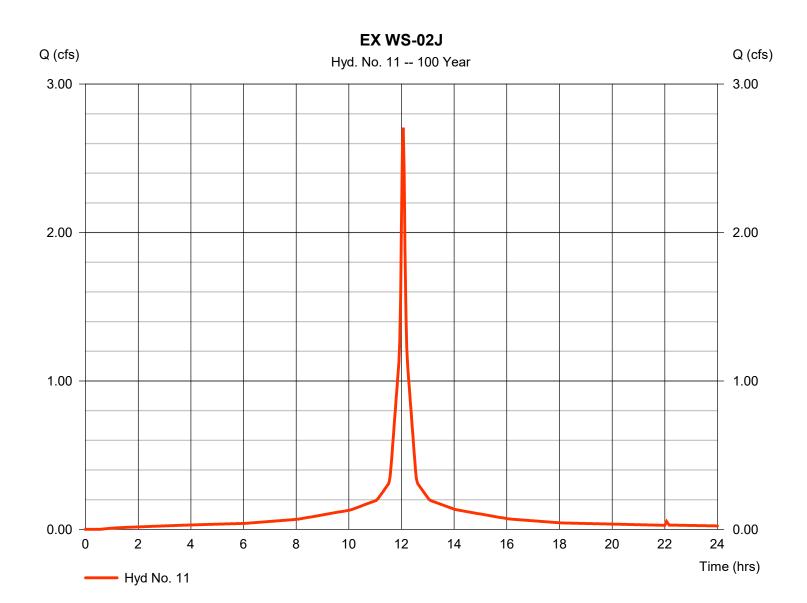


Monday, 12 / 4 / 2023

Hyd. No. 11

EXWS-02J

Hydrograph type = SCS Runoff Peak discharge = 2.707 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 9,455 cuftDrainage area Curve number = 0.343 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



= 24 hrs

Monday, 12 / 4 / 2023

= 484

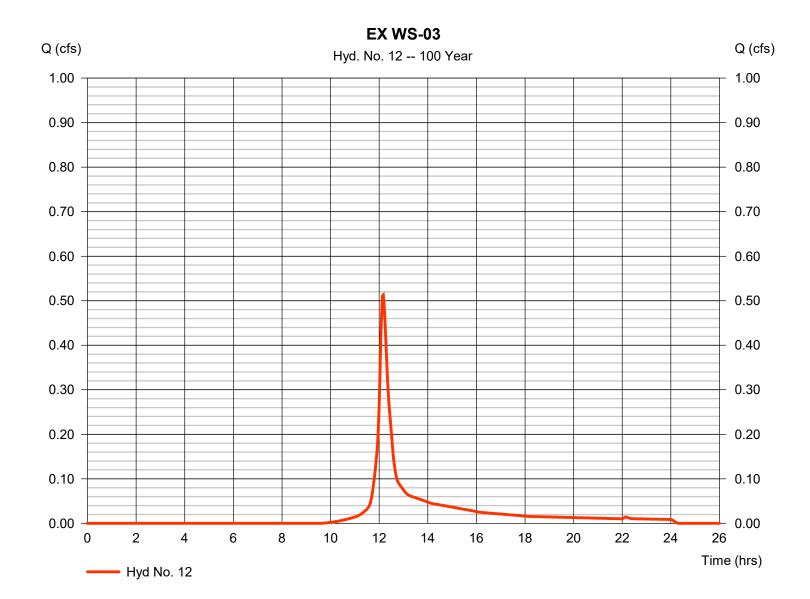
Hyd. No. 12

Storm duration

EX WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.513 cfsStorm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 2.003 cuftDrainage area Curve number = 0.154 ac= 59 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.50 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III

Shape factor



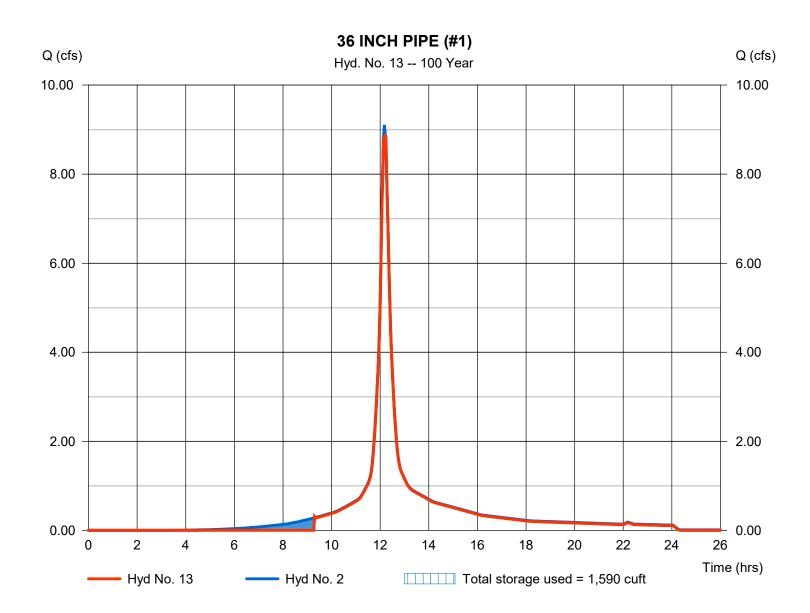
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Monday, 12 / 4 / 2023

Hyd. No. 13

36 INCH PIPE (#1)

Hydrograph type = Reservoir Peak discharge = 8.866 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 35,896 cuft Inflow hyd. No. Max. Elevation = 2 - EX WS-02A = 143.74 ftReservoir name = 36IN - 1Max. Storage = 1,590 cuft



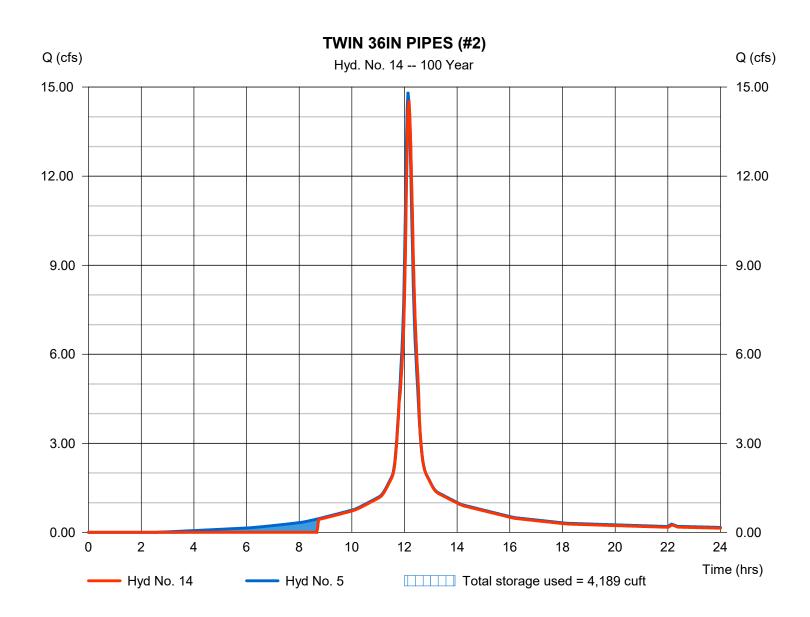
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Monday, 12 / 4 / 2023

Hyd. No. 14

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 14.56 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 55,977 cuftInflow hyd. No. Max. Elevation = 5 - EX WS-02D = 139.24 ft= Northern Twin 36IN Reservoir name Max. Storage = 4,189 cuft



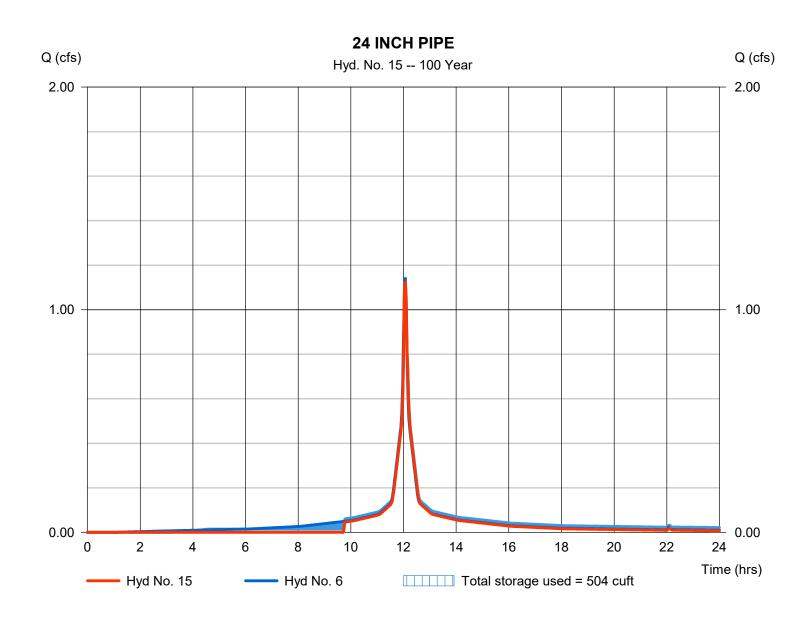
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Monday, 12 / 4 / 2023

Hyd. No. 15

24 INCH PIPE

Hydrograph type = Reservoir Peak discharge = 1.129 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,248 cuft Inflow hyd. No. Max. Elevation = 6 - EX WS-02E $= 139.65 \, \text{ft}$ Reservoir name = 24INMax. Storage = 504 cuft



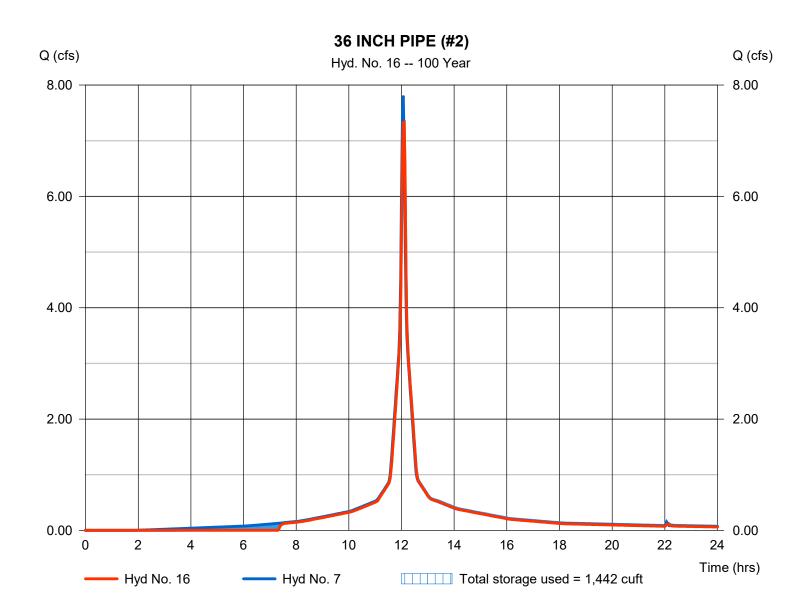
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Monday, 12 / 4 / 2023

Hyd. No. 16

36 INCH PIPE (#2)

Hydrograph type = Reservoir Peak discharge = 7.332 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 24,295 cuft Inflow hyd. No. Max. Elevation = 7 - EX WS-02F = 139.57 ftReservoir name = 36in - 2Max. Storage = 1,442 cuft



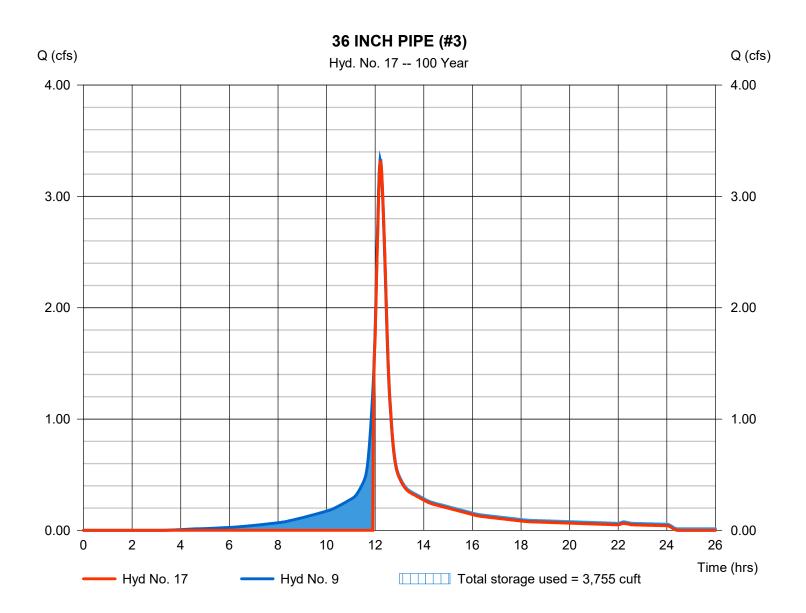
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 17

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 3.311 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 11,531 cuft Inflow hyd. No. Max. Elevation = 9 - EX WS-02H = 137.50 ftReservoir name = 36in - 3Max. Storage = 3,755 cuft



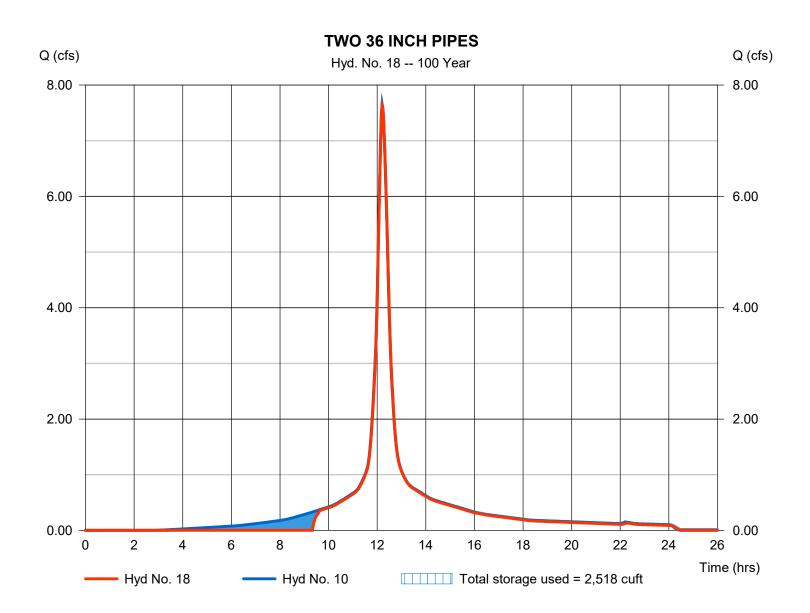
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 18

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 7.629 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 32,678 cuft Inflow hyd. No. Max. Elevation = 10 - EX WS-02I = 135.77 ftReservoir name = TWIN 36IN Max. Storage = 2,518 cuft



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

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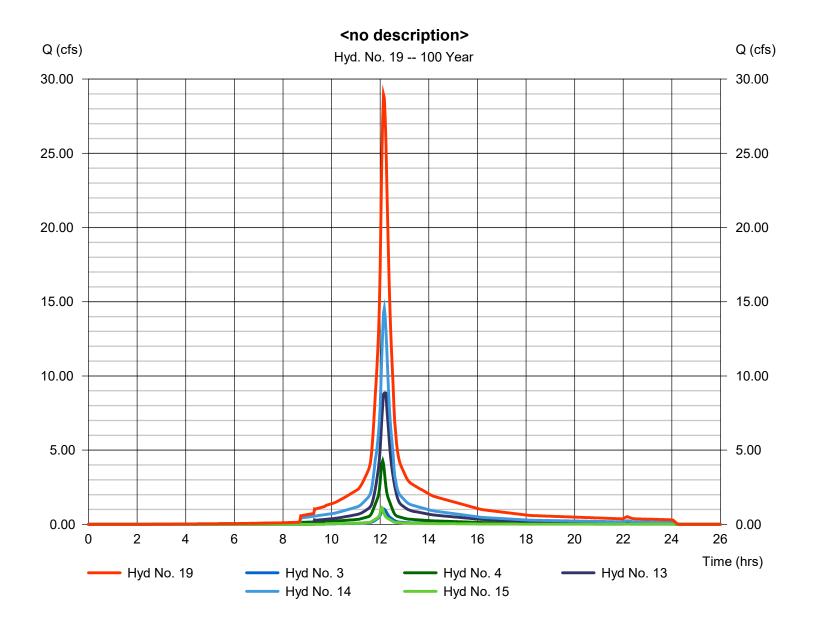
Hyd. No. 19

<no description>

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min

Inflow hyds. = 3, 4, 13, 14, 15

Peak discharge = 28.95 cfs
Time to peak = 12.13 hrs
Hyd. volume = 115,241 cuft
Contrib. drain. area = 0.776 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

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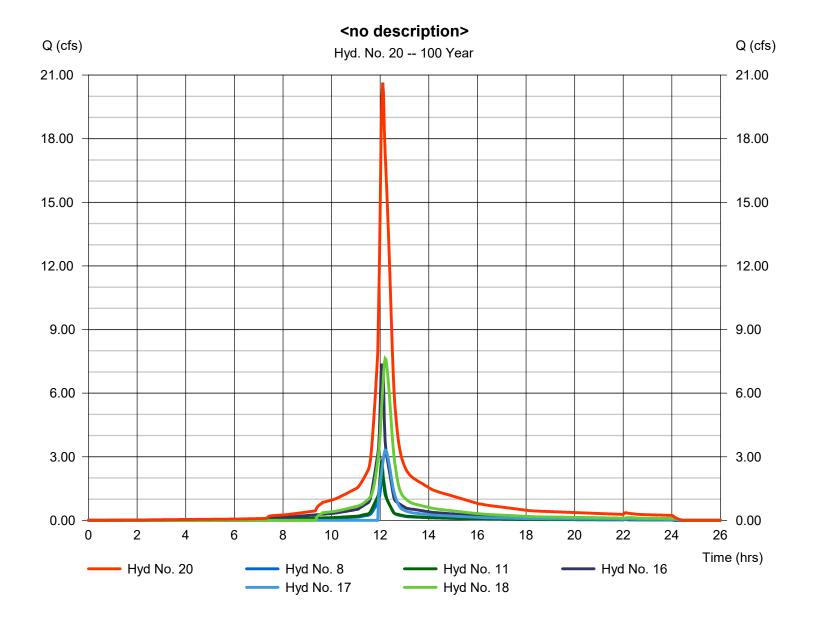
Hyd. No. 20

<no description>

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min

Inflow hyds. = 8, 11, 16, 17, 18

Peak discharge = 20.65 cfs
Time to peak = 12.10 hrs
Hyd. volume = 85,513 cuft
Contrib. drain. area = 0.625 ac



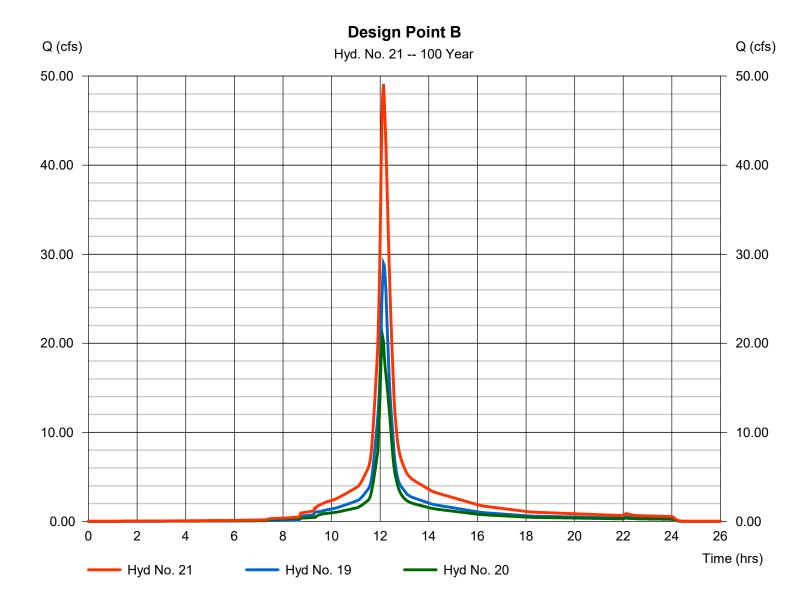
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Hyd. No. 21

Design Point B

Hydrograph type = Combine Peak discharge = 49.09 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 200,754 cuft Inflow hyds. Contrib. drain. area = 0.000 ac= 19, 20



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Monday, 12 / 4 / 2023

Return Period	Intensity-Du	quation Coefficients	(FHA)	
(Yrs)	rrs) B D		E	(N/A)
1	0.0000	0.0000	0.0000	
2	23.2694	3.7000	0.7019	
3	0.0000	0.0000	0.0000	
5	28.1517	3.6000	0.6982	
10	33.4115	3.8000	0.7042	
25	38.5092	3.6000	0.6982	
50	42.7840	3.6000	0.6957	
100	48.0560	3.6000	0.6997	

File name: WILTON.IDF

Intensity = B / (Tc + D)^E

Return												
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5.10	3.71	2.98	2.52	2.21	1.97	1.79	1.64	1.52	1.42	1.33	1.26
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.27	4.55	3.66	3.10	2.71	2.42	2.20	2.02	1.87	1.75	1.64	1.55
10	7.22	5.26	4.23	3.58	3.13	2.80	2.54	2.33	2.16	2.02	1.90	1.79
25	8.57	6.22	5.00	4.24	3.70	3.31	3.00	2.76	2.56	2.39	2.24	2.12
50	9.57	6.96	5.60	4.74	4.15	3.71	3.37	3.09	2.87	2.68	2.52	2.38
100	10.66	7.74	6.22	5.26	4.60	4.11	3.73	3.43	3.17	2.96	2.79	2.63

Tc = time in minutes. Values may exceed 60.

 $\label{thm:precip} Precip.\ file\ name: J:$$\T\T5000\ Toll\ Brothers\012\ Woodbridge\ Village\Calculations\Stormwater\WOODBRIDGE.pcp$

		F	Rainfall Precipitation Table (in)						
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
SCS 24-hour	2.95	3.52	0.00	4.65	5.38	6.54	7.41	8.34	
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Custom	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

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APPENDIX D



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-01

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.132	98	12.9317
Landscaped and Lawns (HSG-B)	0.702	69	48.4236
Landscaped and Lawns (HSG-D)	0.049	84	4.1441
Wooded (HSG-B)	0.712	55	39.1338
Wooded (HSG-D)	0.127	77	9.7682
	1.721		114.401

Weighted CN: 66

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.4	180	0.2	13.47	

Total Tc = 13.5 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02A(I)

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.433	98	42.4712
Landscaped and Lawns (HSG-B)	0.010	69	0.6621
Landscaped and Lawns (HSG-D)	0.015	84	1.3017
Wooded (HSG-B)	0.000	55	0.0000
	0.458		44.435

Weighted CN: 97

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.24	10	0.020	2.1		
Segment B - C	0.015	15	0.020	0.3		
Segment C - D	0.24	6	0.020	1.5		

Total Tc = 4.0 Min. Minimum Tc = 5.0 (MIN)

Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02A(II)

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.393	98	38.4756
Landscaped and Lawns (HSG-B)	0.126	69	8.7280
Landscaped and Lawns (HSG-D)	0.061	84	5.1372
Wooded (HSG-B)	0.103	55	5.6465
	0.683		57.987

Weighted CN: 85

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.4	10	0.02	3.35		
Segment B - C	0.24	84	0.02	12.22		
Segment C - D	0.015	143	0.04	1.54		

Total Tc = 17.1 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02B(I)

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.281	98	27.5462
Landscaped and Lawns (HSG-B)	0.022	69	1.5302
Landscaped and Lawns (HSG-D)	0.166	84	13.9653
Wooded (HSG-B)	0.064	55	3.5341
Wooded (HSG-D)	0.023	77	1.7535
	0.557		48.329

Weighted CN: 87

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	52	0.11	6.34
Segment B - C	0.24	3	0.11	0.43
Segment C - D	0.015	43	0.04	0.59

Total Tc = 7.4 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02B(II)

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.402	98	39.4115
Landscaped and Lawns (HSG-D)	0.001	84	0.0964
	0.403		39.508

Weighted CN: 98

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	35	0.045	0.5

Total Tc = 0.5 Min. Minimum Tc = 5.0 (MIN)

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02B(III)

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.031	98	3.0777
Landscaped and Lawns (HSG-D)	0.101	84	8.4887
	0.132		11.566

Weighted CN: 87

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	15	0.1	1.62

		Shallow Con	centrated Flow		
Segme	ent	Slope (ft/ft)	V (ft/s)	Length (ft)	Time (min.)
Segment B - C	unpaved	0.045	3.42	125	0.6
Segment C - D	unpaved	0.150	6.25	125	0.3

Total Tc = 2.6 Min.

USE 5.0 Min. (MIN)

Note: Overland time of concentration computed using "Kinematic Wave" equation Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02C

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.391	98	38.3293
Landscaped and Lawns (HSG-D)	0.185	84	15.5697
	0.576		53.899

Weighted CN: 93

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	108	0.08	8.58
Segment B - C	0.015	82	0.067	0.80

Total Tc = 9.4 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02D

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	1.683	98	164.9397
Landscaped and Lawns (HSG-D)	0.313	84	26.3281
Wooded (HSG-B)	0.231	55	12.7096
Wooded (HSG-D)	0.018	77	1.3823
	2.246		205.360

Weighted CN: 91

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	52	0.11	6.34
Segment B - C	0.24	65	0.17	4.23
Segment C - D	0.015	43	0.045	0.56

Total Tc = 11.1 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02E

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.177	98	17.3030
Landscaped and Lawns (HSG-B)	0.011	69	0.7793
Landscaped and Lawns (HSG-D)	0.015	84	1.2322
	0.203		19.315

Weighted CN: 95

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland							
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)			
Segment A - B	0.24	22	0.02	4.18			
Segment B - C	0.015	44	0.02	0.79			

Total Tc = 5.0 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02F

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.826	98	80.9512
Landscaped and Lawns (HSG-D)	0.197	84	16.5686
	1.023		97.520

Weighted CN: 95

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.24	31	0.025	5.04		

Total Tc = 5.0 Min.

Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02G

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.774	98	75.8520
Landscaped and Lawns (HSG-D)	0.156	84	13.1380
	0.930		88.990

Weighted CN: 96

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland							
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)			
Segment A - B	0.24	20	0.05	2.69			
Segment B - C	0.015	32	0.04	0.47			

Total Tc = 3.2 Min.

USE 5.0 Min. (MIN)

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-02H

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.037	98	3.6260
Landscaped and Lawns (HSG-D)	0.230	84	19.3358
	0.267		22.962

Weighted CN: 86

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland							
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)			
Segment A - B	0.24	45	0.04	5.62			
Segment B - C	0.015	6	0.02	0.16			
Seament C - D	0.25	53	0.025	7.99			

Total Tc = 13.8 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Description: **Proposed CN & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: PR WS-02I

Location:

Cover Type	Area, ac	CN	A x CN
Pavement/Roof	0.613	98	60.0329
Landscaped and Lawns (HSG-D)	0.684	84	57.4270
	1.296		117.460

Weighted CN: 91

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland							
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)			
Segment A - B	0.24	82	0.06	7.73			
Segment B - C	0.015	6	0.02	0.16			
Segment C - D	0.25	97	0.04	10.74			

Total Tc = 18.6 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: PR WS-03

Location:

Cover Type	Area, ac	CN	A x CN
Landscaped and Lawns (HSG-B)	0.035	69	2.4315
Wooded (HSG-B)	0.046	55	2.5366
	0.081		4.968

Weighted CN: 61

Time of Concentration

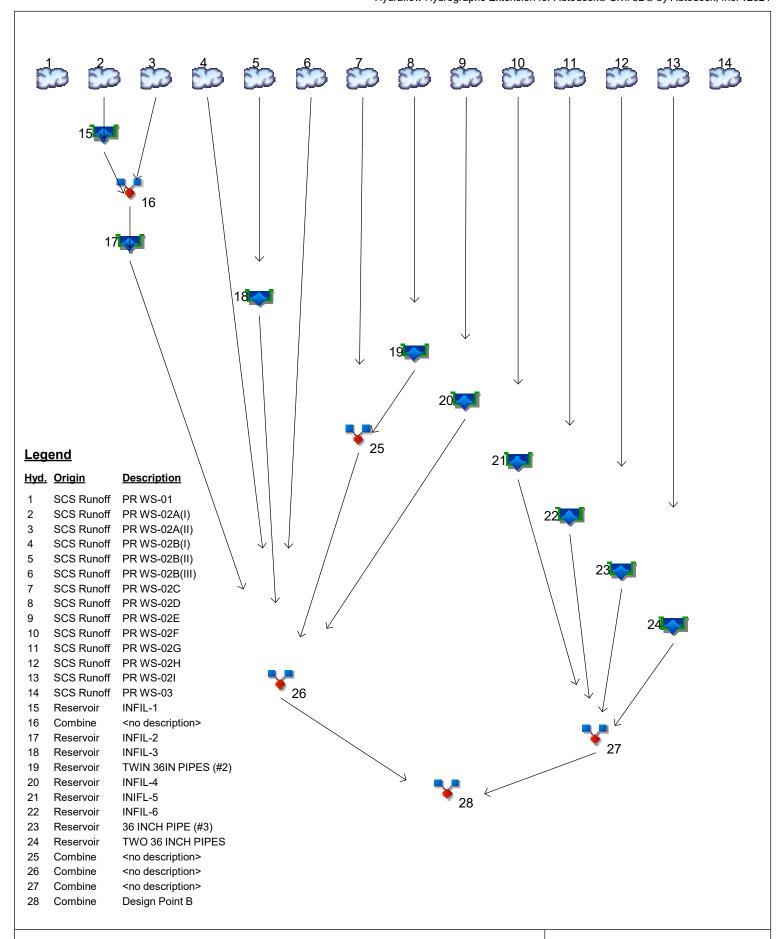
(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.24	44	0.05	5.05		

Total Tc = 5.1 Min.

Note: Overland time of concentration computed using "Kinematic Wave" equation Gutter and pipe time of concentration computed using Manning's equation

Watershed Model Schematic



Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

-	Hydrograph	Inflow	Peak Outflow (cfs)						Hydrograph		
No.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			1.044			2.888	4.203	5.239	6.398	PR WS-01
2	SCS Runoff			1.493			2.311	2.819	3.199	3.605	PR WS-02A(I)
3	SCS Runoff			1.141			2.068	2.652	3.089	3.556	PR WS-02A(II)
4	SCS Runoff			1.343			2.352	2.982	3.451	3.952	PR WS-02B(I)
5	SCS Runoff			1.330			2.046	2.491	2.824	3.181	PR WS-02B(II)
6	SCS Runoff			0.329			0.575	0.728	0.842	0.964	PR WS-02B(III)
7	SCS Runoff			1.625			2.622	3.236	3.695	4.184	PR WS-02C
8	SCS Runoff			5.519			9.148	11.39	13.06	14.84	PR WS-02D
9	SCS Runoff			0.639			1.006	1.234	1.404	1.585	PR WS-02E
10	SCS Runoff			3.218			5.072	6.217	7.074	7.986	PR WS-02F
11	SCS Runoff			2.983			4.656	5.692	6.467	7.294	PR WS-02G
12	SCS Runoff			0.491			0.876	1.116	1.296	1.488	PR WS-02H
13	SCS Runoff			2.681			4.450	5.543	6.358	7.225	PR WS-02I
14	SCS Runoff			0.039			0.138	0.212	0.272	0.339	PR WS-03
15	Reservoir	2		1.056			1.706	2.043	2.310	2.580	INFIL-1
16	Combine	3, 15		2.109			3.643	4.539	5.234	5.963	<no description=""></no>
17	Reservoir	16		2.076			3.595	4.408	5.080	5.776	INFIL-2
18	Reservoir	5		0.099			1.133	1.687	1.927	2.266	INFIL-3
19	Reservoir	8		5.358			8.916	11.13	12.78	14.56	TWIN 36IN PIPES (#2)
20	Reservoir	9		0.408			0.739	0.882	0.989	1.107	INFIL-4
21	Reservoir	10		2.783			4.208	4.987	5.575	6.323	INIFL-5
22	Reservoir	11		0.109			1.183	2.355	3.607	4.990	INFIL-6
23	Reservoir	12		0.000			0.000	0.070	0.167	0.704	36 INCH PIPE (#3)
24	Reservoir	13		2.660			4.422	5.516	6.332	7.197	TWO 36 INCH PIPES
25	Combine	7, 19,		6.742			11.13	13.91	15.96	18.23	<no description=""></no>
26	Combine	4, 6, 17,		10.48			18.99	23.97	27.38	31.28	<no description=""></no>
27	Combine	18, 20, 25 21, 22, 23,		5.018			8.793	12.22	14.97	17.81	<no description=""></no>
	Combine	24, 26, 27		15.38			27.64	35.87	42.12	49.08	Design Point B

Proj. file: J:\F\F0173 Fuller\001 64 Danbury Rd\Calculations\Stormwater\Proposed deliberty 2023

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

noff 1.044 noff 1.493 noff 1.343 noff 1.330 noff 0.329 noff 0.625 noff 0.639 noff 0.639 noff 0.491 noff 0.491 noff 0.039 r 1.056 2.109	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	732 724 734 726 724 724 726 728 724 724 724 730 732 726 728	4,941 4,947 5,042 4,598 4,507 988 5,759 21,524 2,044 10,300 9,701 2,000 12,044 160				PR WS-01 PR WS-02A(I) PR WS-02A(II) PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02E PR WS-02F PR WS-02F PR WS-02H PR WS-02I
noff 1.141 1.343 noff 1.330 noff 0.329 noff 1.625 noff 0.639 noff 0.639 noff 2.983 noff 0.491 noff 0.039 noff 0.491 noff 0.039 noff 1.056	2 2 2 2 2 2 2 2 2 2 2 2 2 2	734 726 724 724 726 728 724 724 724 730 732 726	5,042 4,598 4,507 988 5,759 21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02A(II) PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02C PR WS-02D PR WS-02E PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 1.343 noff 1.330 noff 0.329 noff 1.625 noff 5.519 noff 0.639 noff 2.983 noff 0.491 noff 0.491 noff 0.039 noff 1.056	2 2 2 2 2 2 2 2 2 2 2 2	726 724 724 726 728 724 724 724 730 732 726	4,598 4,507 988 5,759 21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 1.330 noff 0.329 noff 1.625 noff 5.519 noff 0.639 noff 3.218 noff 2.983 noff 0.491 noff 0.039 r 1.056	2 2 2 2 2 2 2 2 2 2 2	724 724 726 728 724 724 724 730 732 726	4,507 988 5,759 21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02B(III) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 0.329 noff 1.625 noff 5.519 noff 0.639 noff 3.218 noff 2.983 noff 0.491 noff 0.039 r 1.056	2 2 2 2 2 2 2 2 2 2	724 726 728 724 724 724 730 732 726	988 5,759 21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 1.625 noff 5.519 noff 0.639 noff 3.218 noff 2.983 noff 0.491 noff 0.039 r 1.056	2 2 2 2 2 2 2 2 2	726 728 724 724 724 730 732 726	5,759 21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 5.519 noff 0.639 noff 3.218 noff 2.983 noff 0.491 noff 0.039 r 1.056	2 2 2 2 2 2 2 2	728 724 724 724 730 732 726	21,524 2,044 10,300 9,701 2,000 12,044				PR WS-02D PR WS-02E PR WS-02F PR WS-02G PR WS-02H
noff 0.639 noff 3.218 noff 2.983 noff 0.491 noff 2.681 noff 0.039 r 1.056	2 2 2 2 2 2 2	724 724 724 730 732 726	2,044 10,300 9,701 2,000 12,044				PR WS-02E PR WS-02F PR WS-02G PR WS-02H
3.218 2.983 noff 0.491 noff 2.681 noff 0.039 r 1.056	2 2 2 2 2 2	724 724 730 732 726	10,300 9,701 2,000 12,044				PR WS-02F PR WS-02G PR WS-02H
2.983 noff 0.491 noff 2.681 noff 0.039 r 1.056	2 2 2 2 2	724 730 732 726	9,701 2,000 12,044				PR WS-02G PR WS-02H
noff 0.491 2.681 noff 0.039 r 1.056	2 2 2 2	730 732 726	2,000 12,044				PR WS-02H
2.681 noff 0.039 r 1.056	2 2 2	732 726	12,044				
noff 0.039 r 1.056	2	726					PR WS-02I
r 1.056	2		160				
		728					PR WS-03
2.109			2,364	2	144.98	1,745	INFIL-1
	2	730	7,406	3, 15			<no description=""></no>
r 2.076	2	732	5,871	16	136.61	1,233	INFIL-2
r 0.099	2	770	711	5	143.86	2,387	INFIL-3
r 5.358	2	730	16,803	8	139.02	3,243	TWIN 36IN PIPES (#2)
r 0.408	2	728	858	9	137.44	675	INFIL-4
r 2.783	2	726	7,104	10	136.12	2,281	INIFL-5
r 0.109	2	822	1,534	11	134.74	5,293	INFIL-6
r 0.000	2	720	0	12	132.37	1,808	36 INCH PIPE (#3)
r 2.660	2	734	8,938	13	135.68	2,403	TWO 36 INCH PIPES
6.742	2	728	22,562	7, 19,			<no description=""></no>
10.48	2	730	35,588	4, 6, 17,			<no description=""></no>
5.018	2	728	17,576	21, 22, 23,			<no description=""></no>
15.38	2	730	53,163	24, 26, 27			Design Point B
r	2.660	2.660 2 6.742 2 10.48 2 5.018 2	2.660 2 734 6.742 2 728 10.48 2 730 5.018 2 728 15.38 2 730	2.660 2 734 8,938 6.742 2 728 22,562 10.48 2 730 35,588 5.018 2 728 17,576 15.38 2 730 53,163	2.660 2 734 8,938 13 6.742 2 728 22,562 7, 19, 10.48 2 730 35,588 4, 6, 17, 18, 20, 25 5.018 2 728 17,576 21, 22, 23, 24, 24, 26, 27 15.38 2 730 53,163 26, 27	2.660 2 734 8,938 13 135.68 6.742 2 728 22,562 7, 19, 10.48 2 730 35,588 4, 6, 17, 18, 20, 25 21, 22, 23, 24, 15.38 2 730 53,163 26, 27	2.660 2 734 8,938 13 135.68 2,403 6.742 2 728 22,562 7, 19, 10.48 2 730 35,588 4, 6, 17, 18, 20, 25 21, 22, 23, 24, 5.018 2 728 17,576 21, 22, 23, 24, 24,

J:\F\F0173 Fuller\001 64 Danbury Rd\CalculatiRes\StoPtervioate2\Presposed-HydrafloTvu.espolay, 12 / 5 / 2023

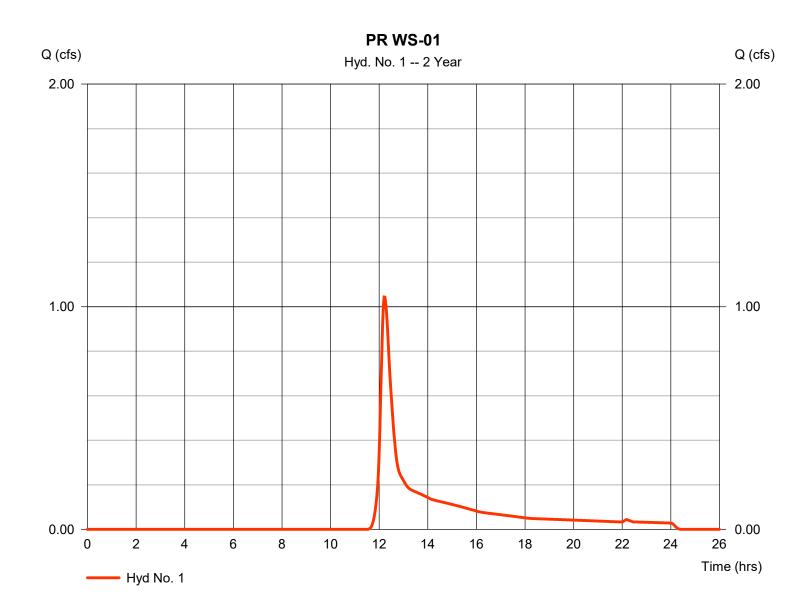
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 1

PR WS-01

Hydrograph type = SCS Runoff Peak discharge = 1.044 cfsStorm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 4,941 cuft Drainage area = 1.721 acCurve number = 66 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 13.50 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



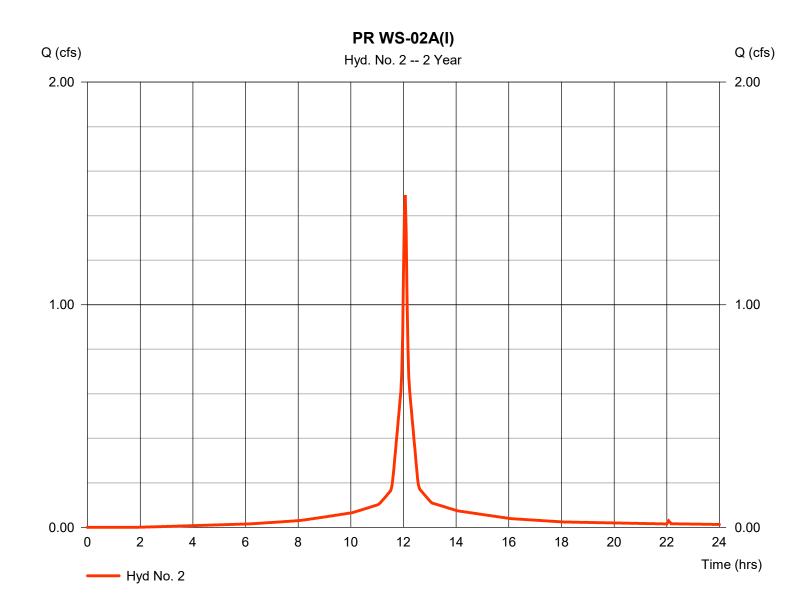
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 2

PR WS-02A(I)

Hydrograph type = SCS Runoff Peak discharge = 1.493 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,947 cuftDrainage area Curve number = 0.458 ac= 97 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



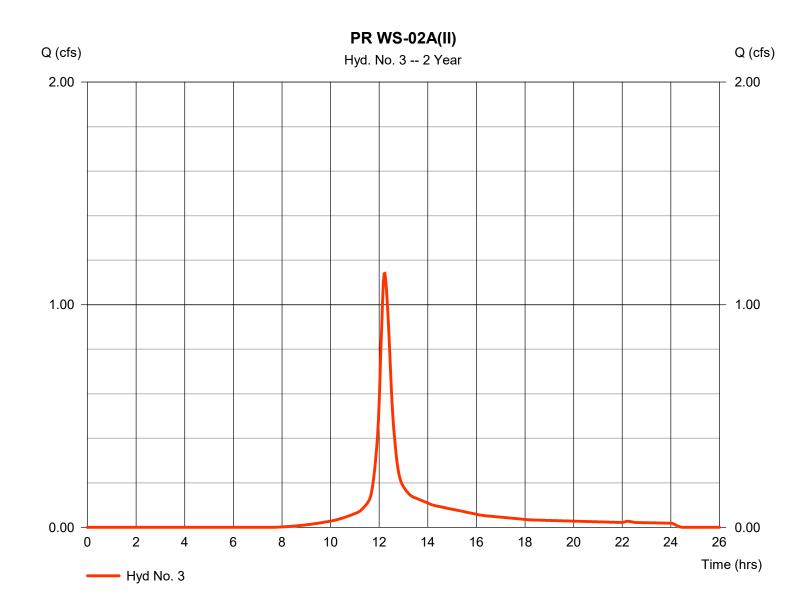
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 3

PRWS-02A(II)

Hydrograph type = SCS Runoff Peak discharge = 1.141 cfsStorm frequency = 2 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 5,042 cuftDrainage area Curve number = 0.683 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.10 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



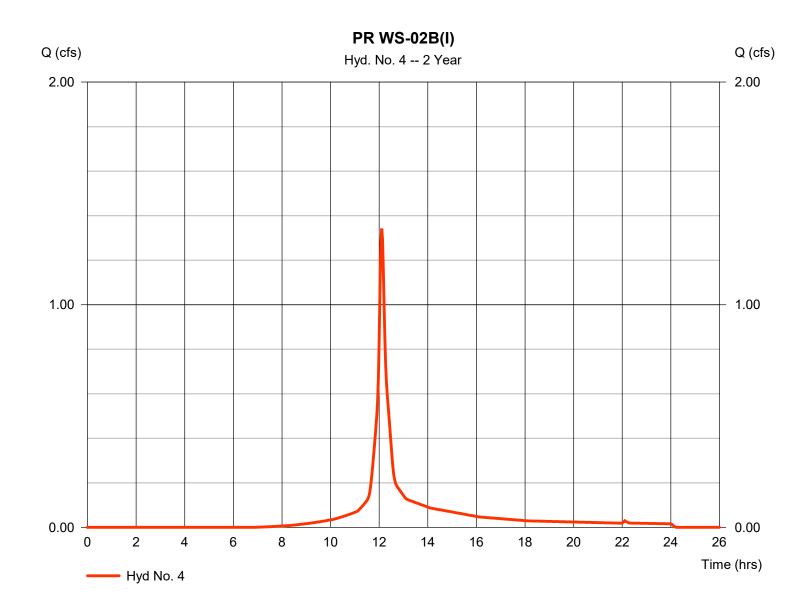
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 4

PR WS-02B(I)

Hydrograph type = SCS Runoff Peak discharge = 1.343 cfsStorm frequency = 2 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 4,598 cuftDrainage area = 0.576 acCurve number = 87 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 7.40 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



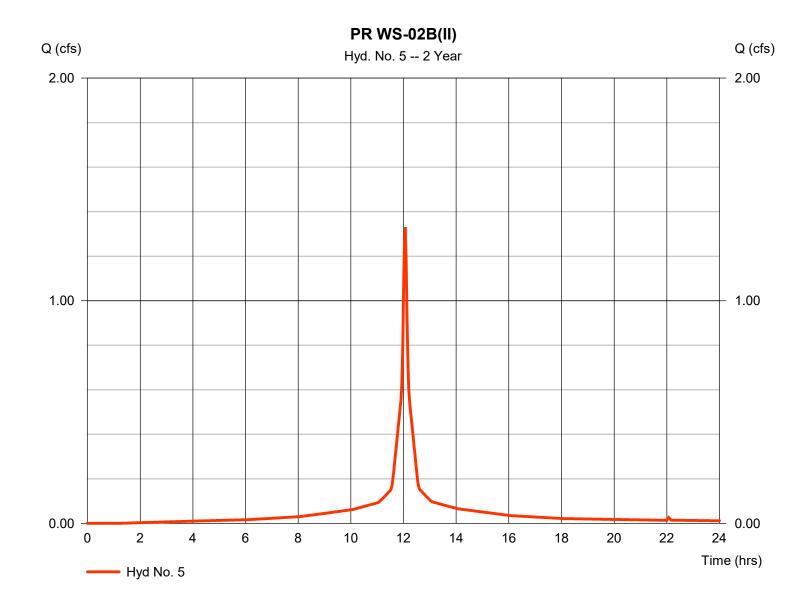
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 5

PRWS-02B(II)

Hydrograph type = SCS Runoff Peak discharge = 1.330 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,507 cuftDrainage area Curve number = 0.403 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



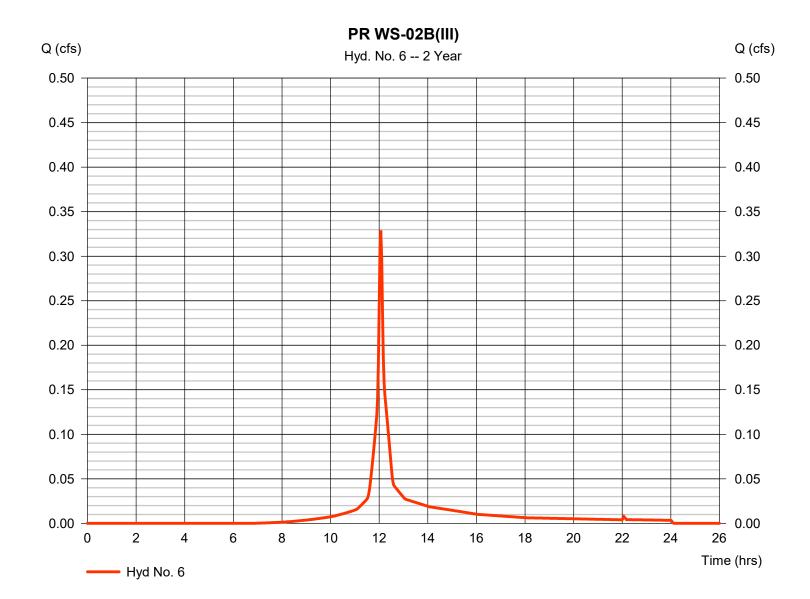
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 6

PR WS-02B(III)

Hydrograph type = SCS Runoff Peak discharge = 0.329 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 988 cuft Drainage area Curve number = 0.132 ac= 87 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



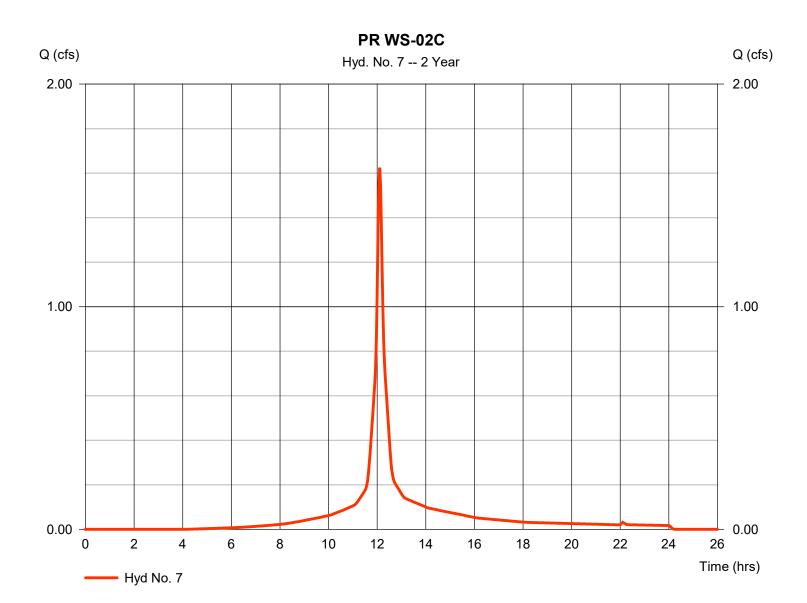
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 7

PRWS-02C

Hydrograph type = SCS Runoff Peak discharge = 1.625 cfsStorm frequency = 2 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 5,759 cuftDrainage area = 0.576 acCurve number = 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



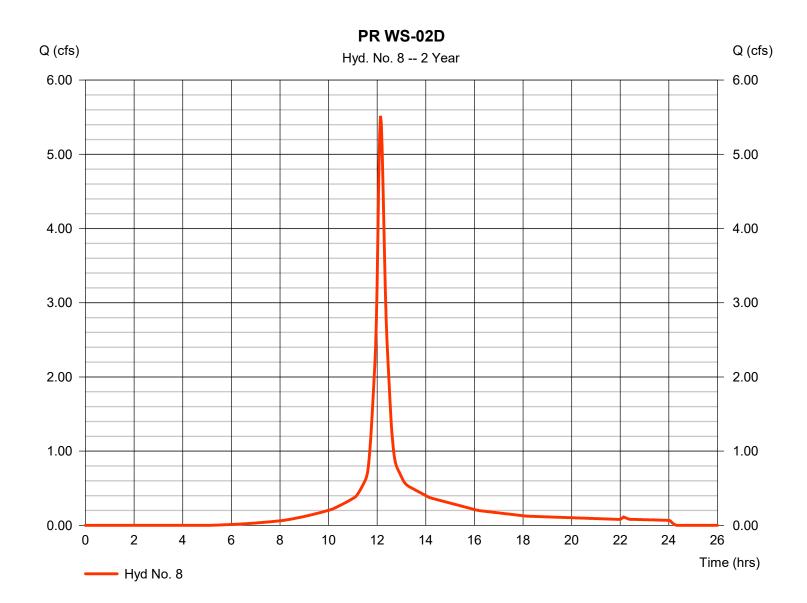
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 8

PRWS-02D

Hydrograph type = SCS Runoff Peak discharge = 5.519 cfsStorm frequency = 2 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 21,524 cuft Drainage area = 2.246 acCurve number = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 11.10 \, \text{min}$ Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



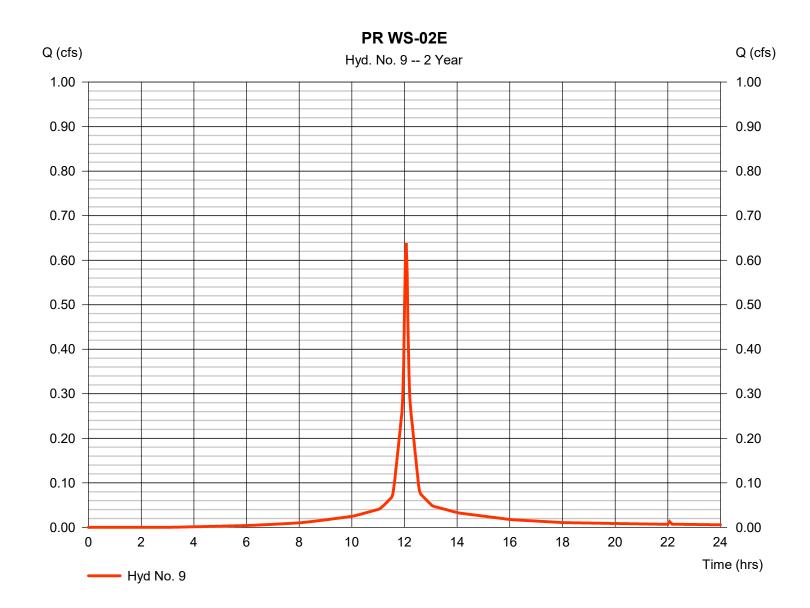
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 9

PRWS-02E

Hydrograph type = SCS Runoff Peak discharge = 0.639 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 2.044 cuft Drainage area = 0.203 acCurve number = 95 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



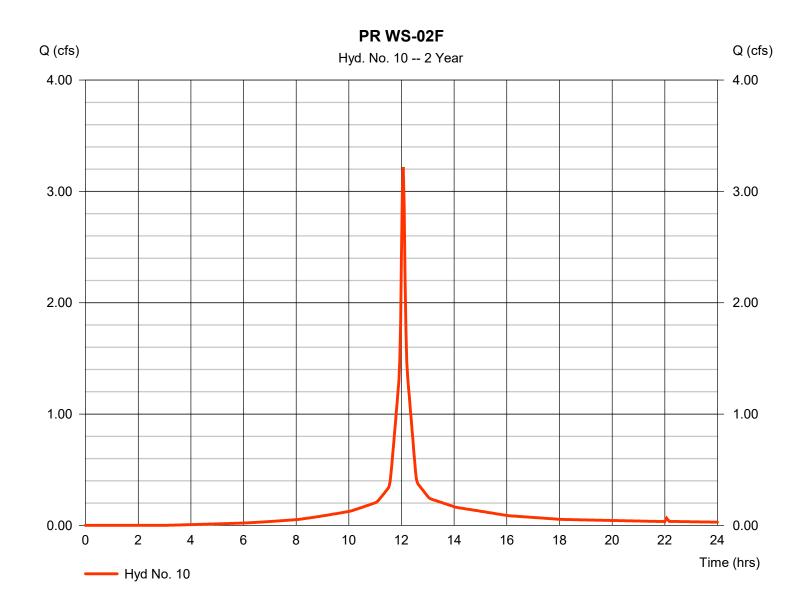
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 10

PR WS-02F

Hydrograph type = SCS Runoff Peak discharge = 3.218 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 10,300 cuftDrainage area = 1.023 acCurve number = 95 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



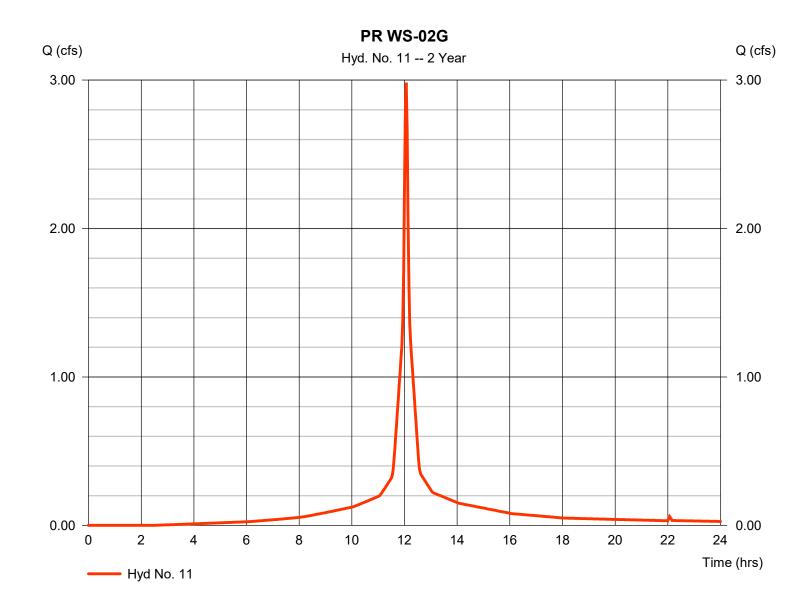
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 11

PRWS-02G

Hydrograph type = SCS Runoff Peak discharge = 2.983 cfsStorm frequency = 2 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 9,701 cuftDrainage area Curve number = 0.930 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Tuesday, 12 / 5 / 2023

= 484

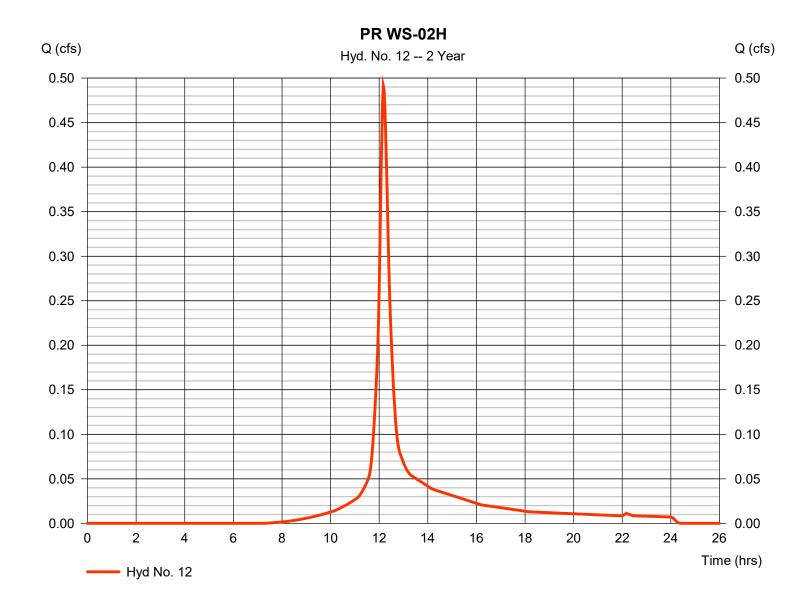
Hyd. No. 12

Storm duration

PRWS-02H

Hydrograph type = SCS Runoff Peak discharge = 0.491 cfsStorm frequency = 2 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 2.000 cuftDrainage area = 0.267 acCurve number = 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.80 min = User Total precip. = 3.52 inDistribution = Type III

Shape factor



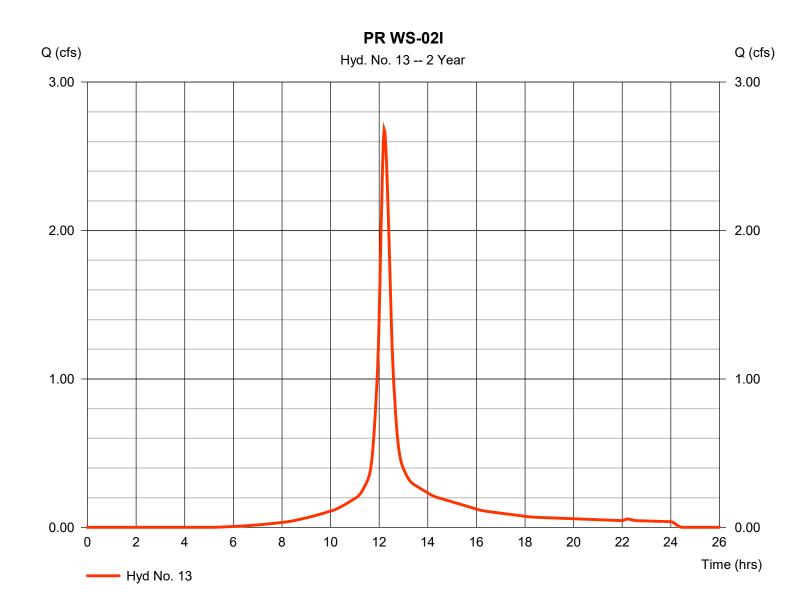
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 13

PR WS-02I

Hydrograph type = SCS Runoff Peak discharge = 2.681 cfsStorm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 12,044 cuft Drainage area = 1.296 ac Curve number = 91 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 18.60 min = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



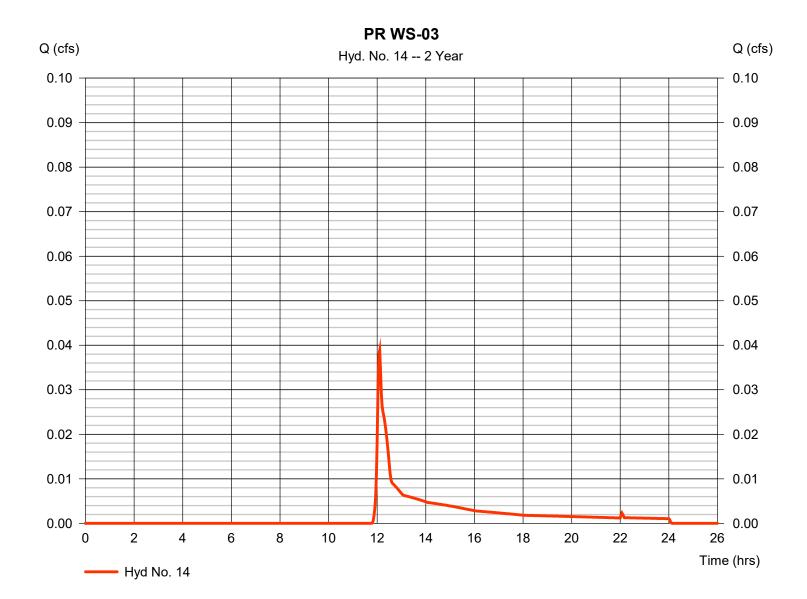
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 14

PR WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.039 cfsStorm frequency = 2 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 160 cuft Drainage area Curve number = 0.081 ac= 61 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.10 \, \text{min}$ = User Total precip. = 3.52 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



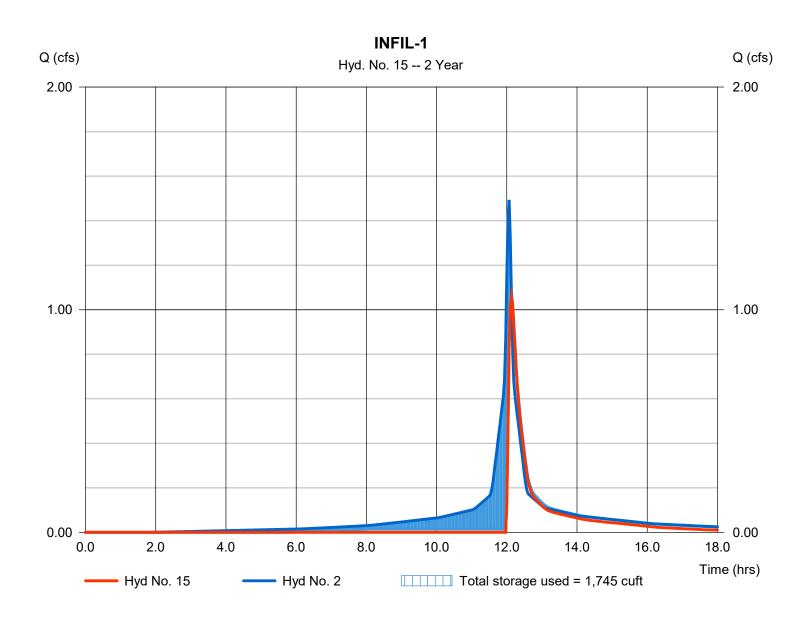
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 15

INFIL-1

= Reservoir Hydrograph type Peak discharge = 1.056 cfsStorm frequency = 2 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2,364 cuftInflow hyd. No. Max. Elevation = 2 - PR WS-02A(I)= 144.98 ftReservoir name = INFIL-1 Max. Storage = 1,745 cuft



Tuesday, 12 / 5 / 2023

Pond No. 10 - INFIL-1

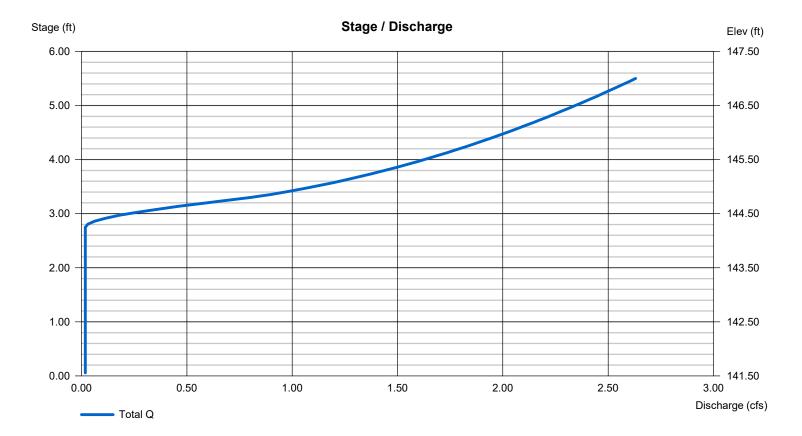
Pond Data

UG Chambers -Invert elev. = 142.25 ft, Rise x Span = 3.75 x 4.80 ft, Barrel Len = 48.72 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 141.50 ft, Width = 7.79 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.50	n/a	0	0
0.55	142.05	n/a	167	167
1.10	142.60	n/a	265	432
1.65	143.15	n/a	319	751
2.20	143.70	n/a	313	1,065
2.75	144.25	n/a	304	1,369
3.30	144.80	n/a	289	1,658
3.85	145.35	n/a	268	1,926
4.40	145.90	n/a	232	2,159
4.95	146.45	n/a	171	2,330
5.50	147.00	n/a	167	2,497

Culvert / Orifice Structures Weir Structures [PrfRsr] [A] [B] [C] [A] [B] [C] [D] = 12.00 8.00 0.00 0.00 0.00 0.00 = 0.000.00 Rise (in) Crest Len (ft) Span (in) = 12.008.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 142.95 144.25 0.00 0.00 Weir Type = ---= 20.00 0.50 0.00 0.00 Multi-Stage = No No No No Length (ft) 0.00 n/a = 1.00 1.00 Slope (%) = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 1.000 (by Contour) No = n/aYes No TW Elev. (ft) = 0.00Multi-Stage



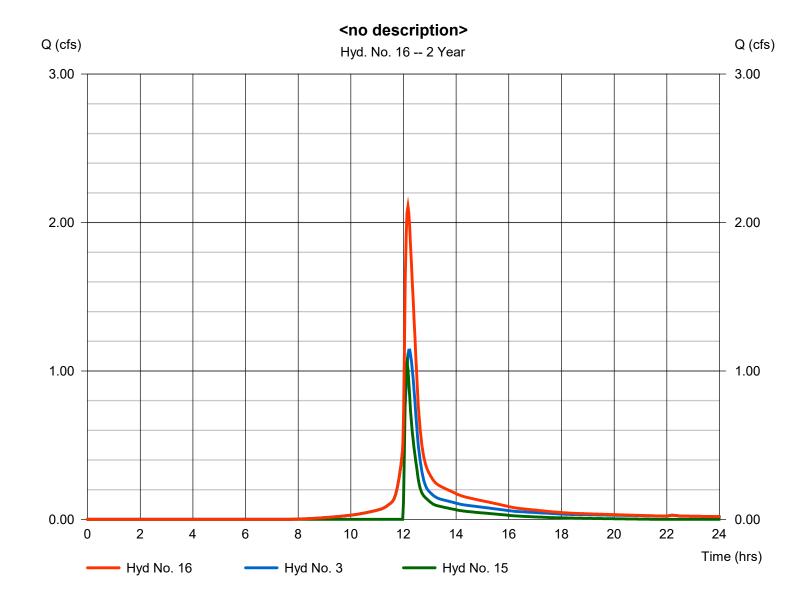
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 16

<no description>

Hydrograph type = Combine Peak discharge = 2.109 cfsStorm frequency = 2 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 7,406 cuft Inflow hyds. = 3, 15 Contrib. drain. area = 0.683 ac



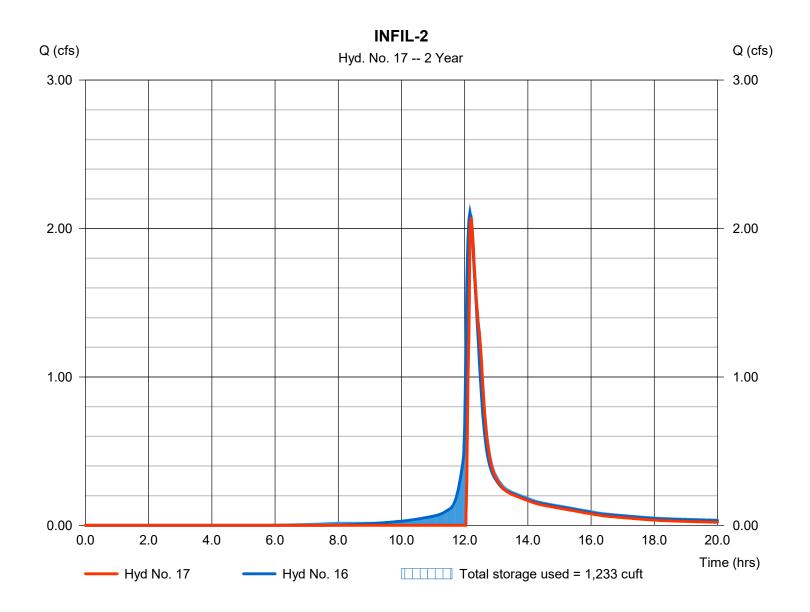
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 17

INFIL-2

Hydrograph type = Reservoir Peak discharge = 2.076 cfsStorm frequency = 2 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 5.871 cuftInflow hyd. No. Max. Elevation = 16 - <no description> $= 136.61 \, \text{ft}$ Reservoir name = INFIL-2 Max. Storage = 1,233 cuft



Tuesday, 12 / 5 / 2023

Pond No. 1 - INFIL-2

Pond Data

UG Chambers -Invert elev. = 133.75 ft, Rise x Span = 3.75 x 4.85 ft, Barrel Len = 63.06 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 133.00 ft, Width = 8.42 ft, Height = 5.50 ft, Voids = 40.00%

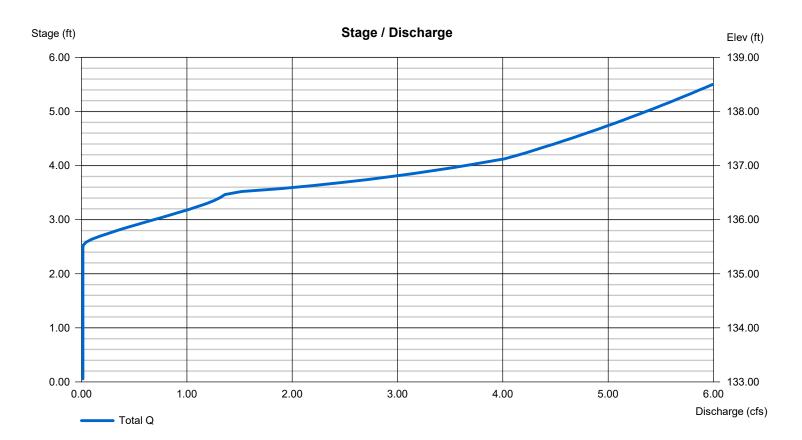
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	133.00	n/a	0	0
0.55	133.55	n/a	117	117
1.10	134.10	n/a	181	298
1.65	134.65	n/a	216	514
2.20	135.20	n/a	213	727
2.75	135.75	n/a	206	933
3.30	136.30	n/a	197	1,130
3.85	136.85	n/a	183	1,313
4.40	137.40	n/a	160	1,472
4.95	137.95	n/a	120	1,592
5.50	138.50	n/a	117	1,709

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	Inactive	Inactive	Inactive	Crest Len (ft)	Inactive	Inactive	Inactive	Inactive
Span (in)	= 12.00	10.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 2.60	3.33	3.33	3.33
Invert El. (ft)	= 135.50	136.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 8.00	0.50	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.00	1.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			



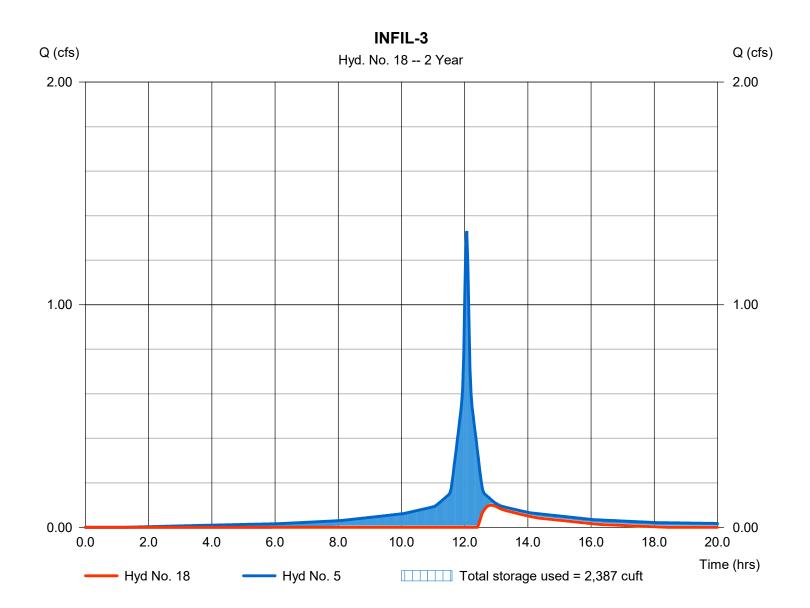
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 18

INFIL-3

= Reservoir Hydrograph type Peak discharge = 0.099 cfsStorm frequency = 2 yrsTime to peak $= 12.83 \, hrs$ Time interval = 2 min Hyd. volume = 711 cuft Inflow hyd. No. Max. Elevation = 5 - PR WS-02B(II)= 143.86 ftReservoir name = INFIL-3 Max. Storage = 2,387 cuft



Tuesday, 12 / 5 / 2023

Pond No. 9 - INFIL-3

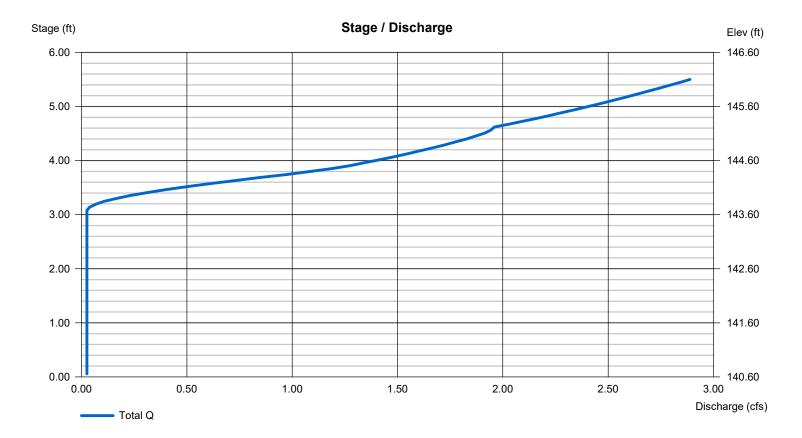
Pond Data

UG Chambers -Invert elev. = 141.35 ft, Rise x Span = 3.75 x 4.93 ft, Barrel Len = 70.23 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 140.60 ft, Width = 7.79 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	140.60	n/a	0	0
0.55	141.15	n/a	241	241
1.10	141.70	n/a	386	627
1.65	142.25	n/a	466	1,093
2.20	142.80	n/a	458	1,550
2.75	143.35	n/a	443	1,994
3.30	143.90	n/a	422	2,416
3.85	144.45	n/a	390	2,806
4.40	145.00	n/a	338	3,144
4.95	145.55	n/a	247	3,391
5.50	146.10	n/a	241	3,632

Culvert / Orifice Structures Weir Structures [PrfRsr] [A] [A] [B] [C] [B] [C] [D] = 12.00 0.00 0.00 0.00 10.00 0.00 Inactive 0.00 Rise (in) Crest Len (ft) Span (in) = 12.0010.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 1 Invert El. (ft) = 143.67 143.67 0.00 0.00 Weir Type = Broad = 19.00 0.50 0.00 0.00 Multi-Stage = Yes No No No Length (ft) 0.00 n/a = 1.00 1.00 Slope (%) = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 1.000 (by Contour) No = n/aYes No TW Elev. (ft) = 0.00Multi-Stage



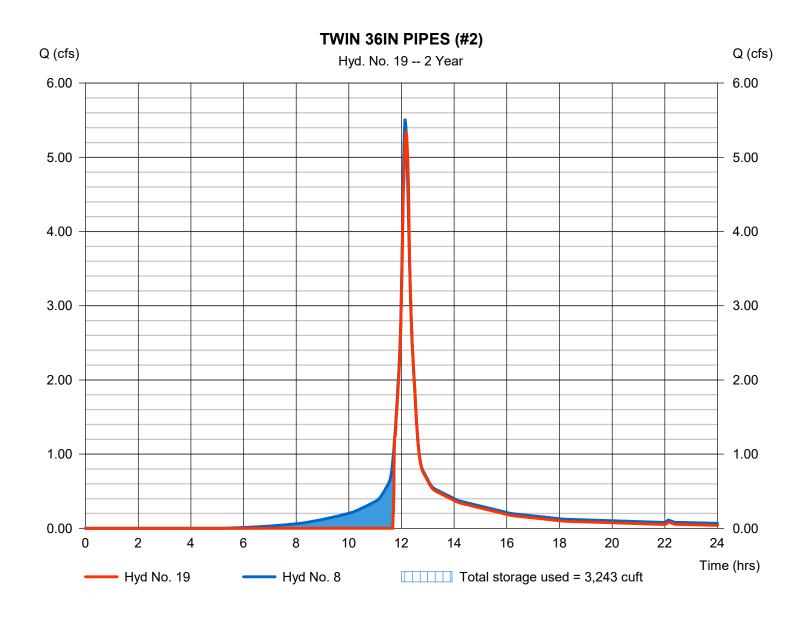
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 19

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 5.358 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 16,803 cuft Max. Elevation Inflow hyd. No. = 8 - PR WS-02D = 139.02 ftReservoir name = Northern Twin 36IN Max. Storage = 3,243 cuft



Tuesday, 12 / 5 / 2023

Pond No. 6 - Northern Twin 36IN

Pond Data

UG Chambers -Invert elev. = 131.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 120.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No Epodesurse-bls-d-ruderflinetel/cent@0.50/ds/SVAdthræg5.00/dtarlete-ighetth-coll-50

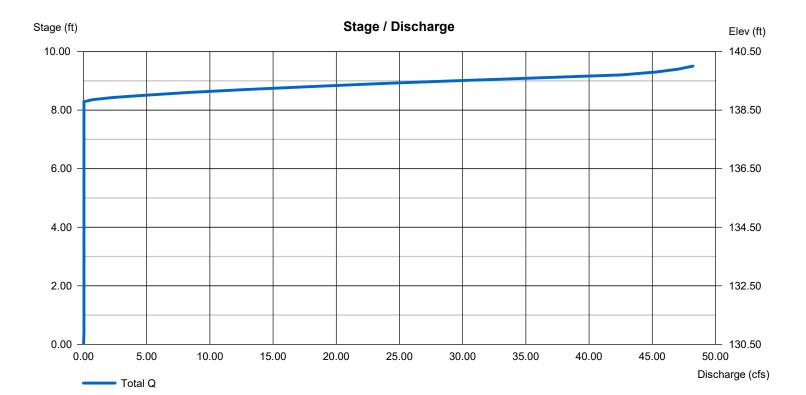
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	130.50	n/a	0	0
0.35	130.85	n/a	168	168
0.70	131.20	n/a	197	365
1.05	131.55	n/a	267	632
1.40	131.90	n/a	297	929
1.75	132.25	n/a	313	1,242
2.10	132.60	n/a	319	1,561
2.45	132.95	n/a	316	1,877
2.80	133.30	n/a	305	2,182
3.15	133.65	n/a	282	2,464
3.50	134.00	n/a	234	2,698
7.80	138.30	01	2	2,701
8.50	139.00	1,250	438	3,138
9.50	140.00	7,570	4,410	7,548

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 30.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 15.00	Inactive	Inactive	Inactive
Span (in)	= 30.00	0.00	0.00	0.00	Crest El. (ft)	= 138.80	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 134.20	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 69.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			



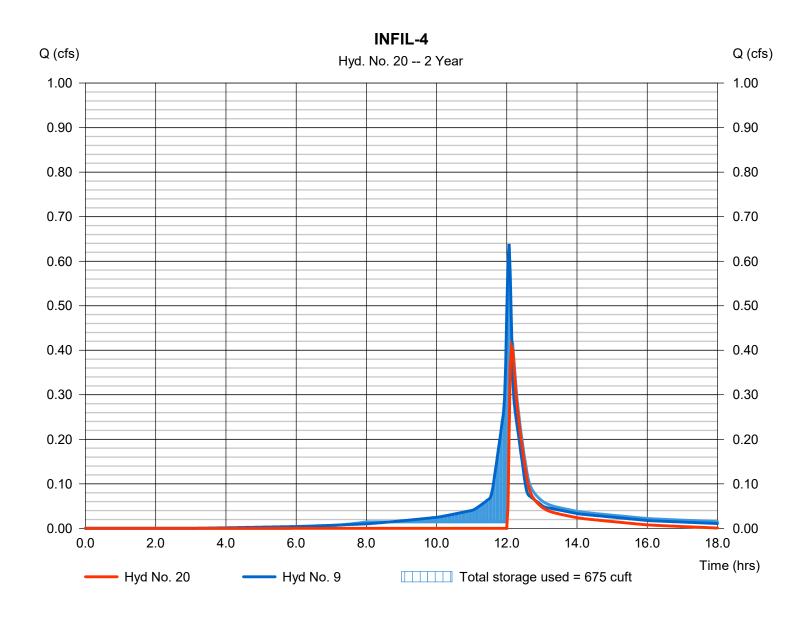
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Tuesday, 12 / 5 / 2023

Hyd. No. 20

INFIL-4

Hydrograph type Peak discharge = 0.408 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 858 cuft Inflow hyd. No. Max. Elevation = 9 - PR WS-02E = 137.44 ftReservoir name = INFIL-4 Max. Storage = 675 cuft



Tuesday, 12 / 5 / 2023

Pond No. 2 - INFIL-4

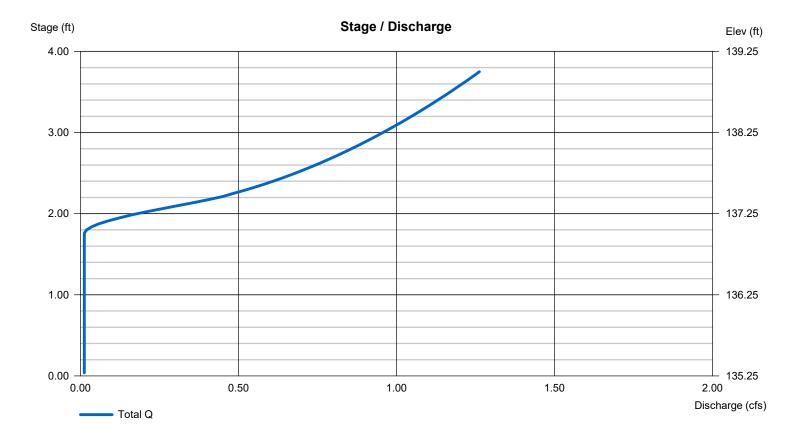
Pond Data

UG Chambers -Invert elev. = 136.00 ft, Rise x Span = 2.50 x 3.05 ft, Barrel Len = 46.34 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 135.25 ft, Width = 5.50 ft, Height = 3.75 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	135.25	n/a	0	0
0.38	135.63	n/a	76	76
0.75	136.00	n/a	76	153
1.13	136.38	n/a	140	293
1.50	136.75	n/a	138	431
1.88	137.13	n/a	135	567
2.25	137.50	n/a	131	697
2.63	137.88	n/a	123	820
3.00	138.25	n/a	112	932
3.38	138.63	n/a	89	1,021
3.75	139.00	n/a	76	1,098

Culvert / Orifice Structures Weir Structures [PrfRsr] [A] [C] [A] [B] [C] [B] [D] = 12.00 6.00 Inactive Inactive Inactive Inactive Inactive Inactive Rise (in) Crest Len (ft) Span (in) = 12.006.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 136.45 137.00 0.00 0.00 Weir Type = Broad = 28.00 0.50 0.00 0.00 Multi-Stage = Yes No No No Length (ft) 0.00 = 1.00 1.00 Slope (%) n/a = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 1.000 (by Contour) No = n/aYes No TW Elev. (ft) = 0.00Multi-Stage



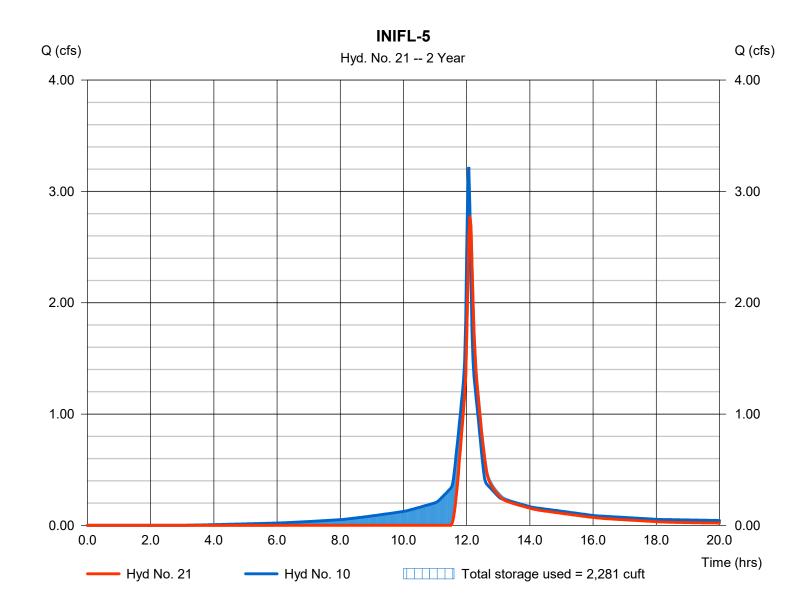
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Tuesday, 12 / 5 / 2023

Hyd. No. 21

INIFL-5

Hydrograph type = Reservoir Peak discharge = 2.783 cfsStorm frequency = 2 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 7,104 cuftInflow hyd. No. Max. Elevation = 136.12 ft= 10 - PR WS-02F Reservoir name = INIFL-5 Max. Storage = 2,281 cuft



Tuesday, 12 / 5 / 2023

Pond No. 3 - INIFL-5

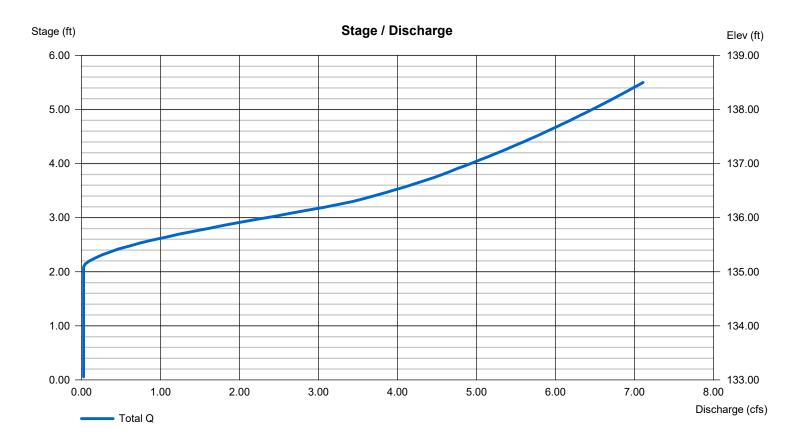
Pond Data

UG Chambers -Invert elev. = 133.75 ft, Rise x Span = 3.75 x 4.93 ft, Barrel Len = 70.23 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 133.00 ft, Width = 7.79 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	133.00	n/a	0	0
0.55	133.55	n/a	241	241
1.10	134.10	n/a	386	627
1.65	134.65	n/a	466	1,093
2.20	135.20	n/a	458	1,550
2.75	135.75	n/a	443	1,994
3.30	136.30	n/a	422	2,416
3.85	136.85	n/a	390	2,806
4.40	137.40	n/a	338	3,144
4.95	137.95	n/a	247	3,391
5.50	138.50	n/a	241	3,632

Culvert / Orifice Structures Weir Structures [PrfRsr] [A] [A] [B] [C] [B] [C] [D] = 15.00 0.00 0.00 0.00 0.00 15.00 0.00 Inactive Rise (in) Crest Len (ft) Span (in) = 15.0015.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 1 Invert El. (ft) = 135.00 135.08 0.00 0.00 Weir Type = Rect = 29.00 0.50 0.00 0.00 Multi-Stage = Yes No No No Length (ft) 0.00 n/a = 2.401.00 Slope (%) = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 1.000 (by Contour) No = n/aYes No TW Elev. (ft) = 0.00Multi-Stage



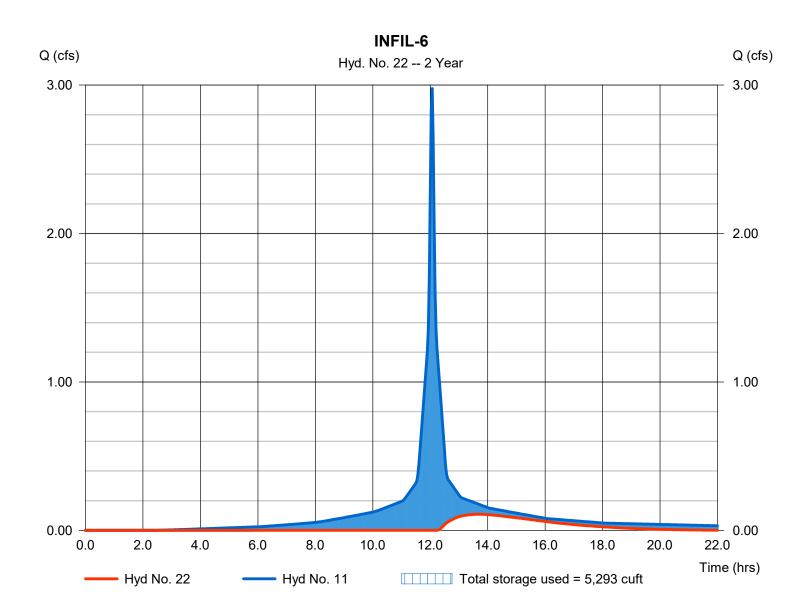
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Tuesday, 12 / 5 / 2023

Hyd. No. 22

INFIL-6

= Reservoir Hydrograph type Peak discharge = 0.109 cfsStorm frequency = 2 yrsTime to peak $= 13.70 \, hrs$ Time interval = 2 min Hyd. volume = 1,534 cuft Inflow hyd. No. Max. Elevation = 11 - PR WS-02G = 134.74 ftReservoir name = INFIL-6 Max. Storage = 5,293 cuft



Tuesday, 12 / 5 / 2023

Pond No. 7 - INFIL-6

Pond Data

Orifice Coeff.

Multi-Stage

= 0.60

= n/a

0.60

Yes

0.60

No

0.60

No

UG Chambers -Invert elev. = 132.75 ft, Rise x Span = 3.75 x 5.10 ft, Barrel Len = 184.95 ft, No. Barrels = 2, Slope = 0.00%, Headers = No **Encasement** -Invert elev. = 132.00 ft, Width = 7.79 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	132.00	n/a	0	0
0.55	132.55	n/a	634	634
1.10	133.10	n/a	1,030	1,664
1.65	133.65	n/a	1,247	2,911
2.20	134.20	n/a	1,225	4,136
2.75	134.75	n/a	1,186	5,322
3.30	135.30	n/a	1,128	6,450
3.85	135.85	n/a	1,042	7,492
4.40	136.40	n/a	898	8,389
4.95	136.95	n/a	651	9,041
5.50	137.50	n/a	634	9,675

Culvert / Orifice Structures Weir Structures [B] [PrfRsr] [A] [A] [C] [B] [C] [D] = 12.00 0.00 0.00 0.00 Inactive 0.00 = 0.000.00 Rise (in) Crest Len (ft) Span (in) = 12.000.00 0.00 0.00 Crest El. (ft) = 134.17 0.00 0.00 0.00 No. Barrels = 1 1 0 0 Weir Coeff. = 0.453.33 3.33 3.33 Invert El. (ft) = 132.500.00 0.00 0.00 Weir Type = 20 degV = 10.00 0.00 0.00 0.00 Multi-Stage = Yes No No No Length (ft) = 4.00 0.00 0.00 n/a Slope (%) = .013 N-Value .013 .013 n/a

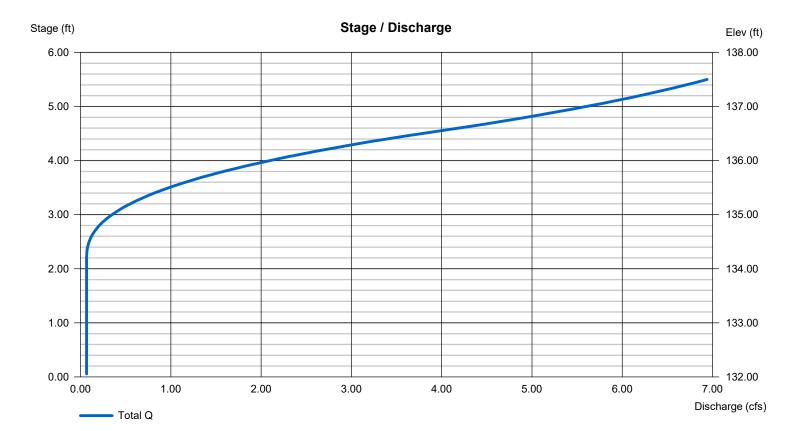
Exfil.(in/hr)

TW Elev. (ft)

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

= 0.00

= 1.000 (by Contour)



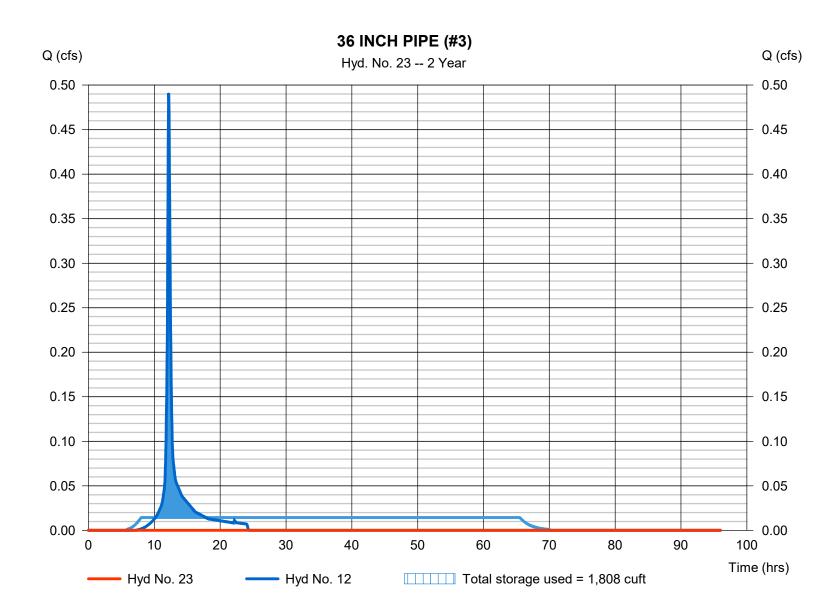
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Tuesday, 12 / 5 / 2023

Hyd. No. 23

36 INCH PIPE (#3)

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. Max. Elevation = 12 - PR WS-02H = 132.37 ftReservoir name = 36IN - 3Max. Storage = 1,808 cuft



Tuesday, 12 / 5 / 2023

Pond No. 4 - 36IN - 3

Pond Data

UG Chambers -Invert elev. = 129.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 30.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No Epodes are selected to the selected by the selected

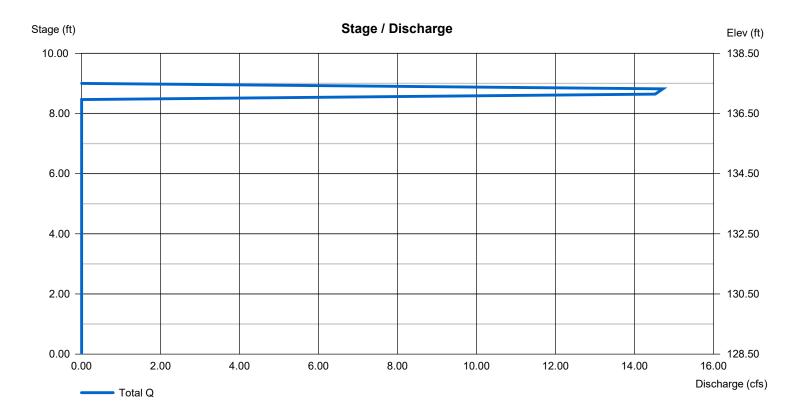
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	128.50	n/a	0	0
0.35	128.85	n/a	21	21
0.70	129.20	n/a	25	46
1.05	129.55	n/a	33	79
1.40	129.90	n/a	37	116
1.75	130.25	n/a	39	155
2.10	130.60	n/a	40	195
2.45	130.95	n/a	40	235
2.80	131.30	n/a	38	273
3.15	131.65	n/a	35	308
3.50	132.00	n/a	29	337
7.20	136.20	01	2	339
9.00	137.50	5,250	4,726	5,065

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 100.00	Inactive	Inactive	Inactive
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 137.50	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 130.90	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 13.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by)	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			



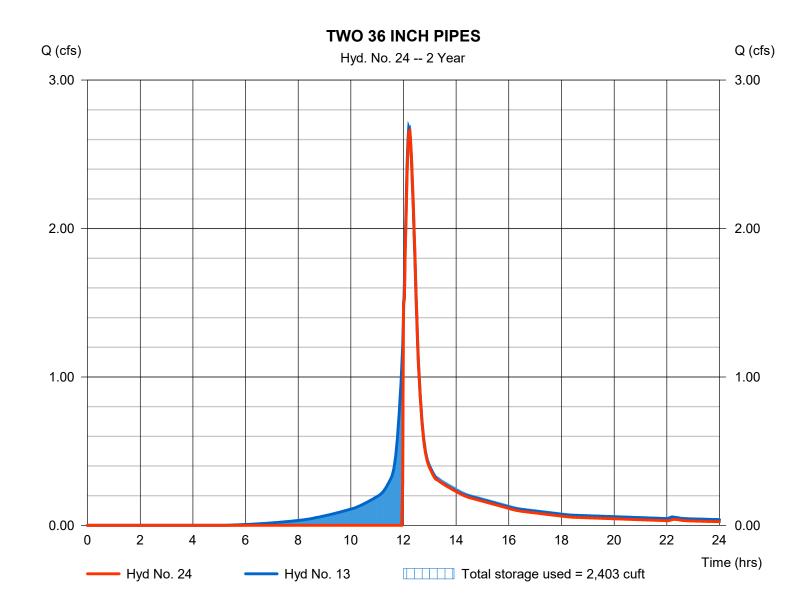
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Tuesday, 12 / 5 / 2023

Hyd. No. 24

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 2.660 cfs= Reservoir Storm frequency = 2 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 8,938 cuft Max. Elevation Inflow hyd. No. = 13 - PR WS-02I = 135.68 ftReservoir name = TWIN 36IN Max. Storage = 2,403 cuft



Tuesday, 12 / 5 / 2023

Pond No. 5 - TWIN 36IN

Pond Data

UG Chambers -Invert elev. = 127.50 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 62.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No Epotasurseblsehvterflietelvcent@7r.@0ศasWidthræg5.80dtarlelæighetthroid ട്രെൽവ fvoidslum4e0@30dblation. Begining Elevation = 134.90 ft

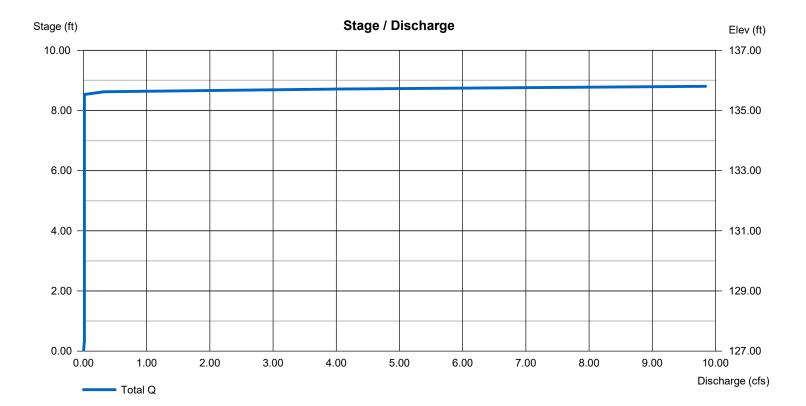
Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	127.00	n/a	0	0
0.35	127.35	n/a	87	87
0.70	127.70	n/a	102	189
1.05	128.05	n/a	138	327
1.40	128.40	n/a	153	480
1.75	128.75	n/a	162	642
2.10	129.10	n/a	165	806
2.45	129.45	n/a	163	970
2.80	129.80	n/a	157	1,127
3.15	130.15	n/a	146	1,273
3.50	130.50	n/a	121	1,394
7.90	134.90	01	2	1,396
8.80	135.80	2,590	1,166	2,562

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	Inactive	Inactive	Inactive	Crest Len (ft)	= 33.00	Inactive	Inactive	Inactive
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 135.60	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 129.60	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 70.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 2.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 1.000 (by Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			



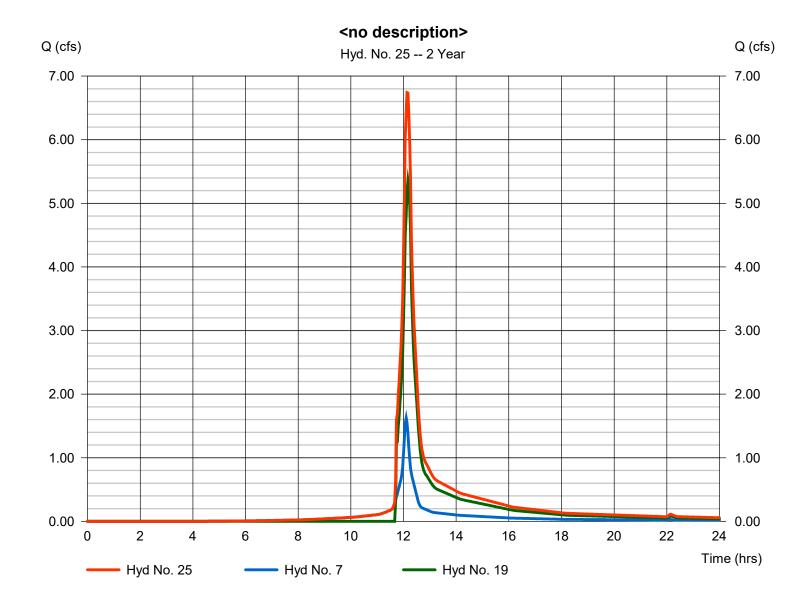
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Tuesday, 12 / 5 / 2023

Hyd. No. 25

<no description>

Hydrograph type = Combine Peak discharge = 6.742 cfsStorm frequency Time to peak = 2 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 22,562 cuft Inflow hyds. = 7, 19 Contrib. drain. area = 0.576 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

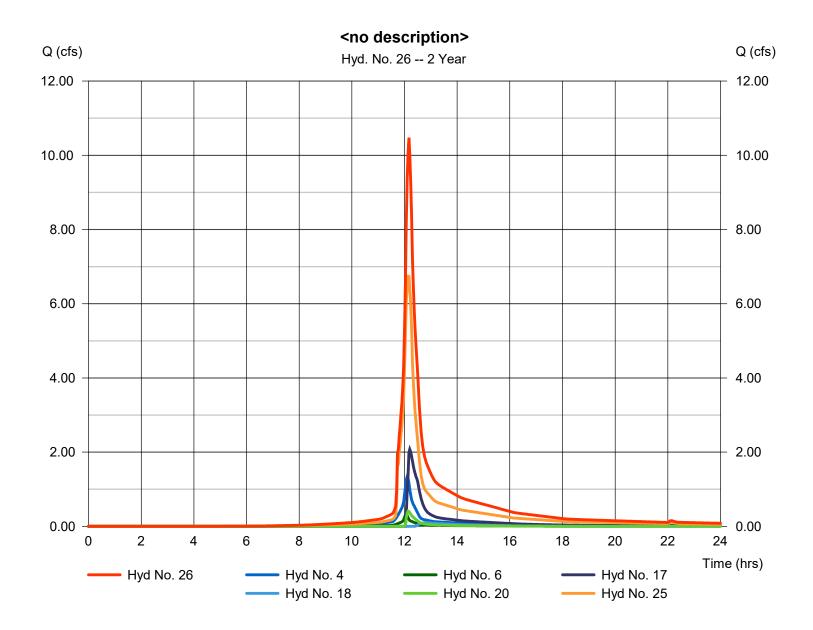
Hyd. No. 26

<no description>

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 2 min

Inflow hyds. = 4, 6, 17, 18, 20, 25

Peak discharge = 10.48 cfs
Time to peak = 12.17 hrs
Hyd. volume = 35,588 cuft
Contrib. drain. area = 0.708 ac



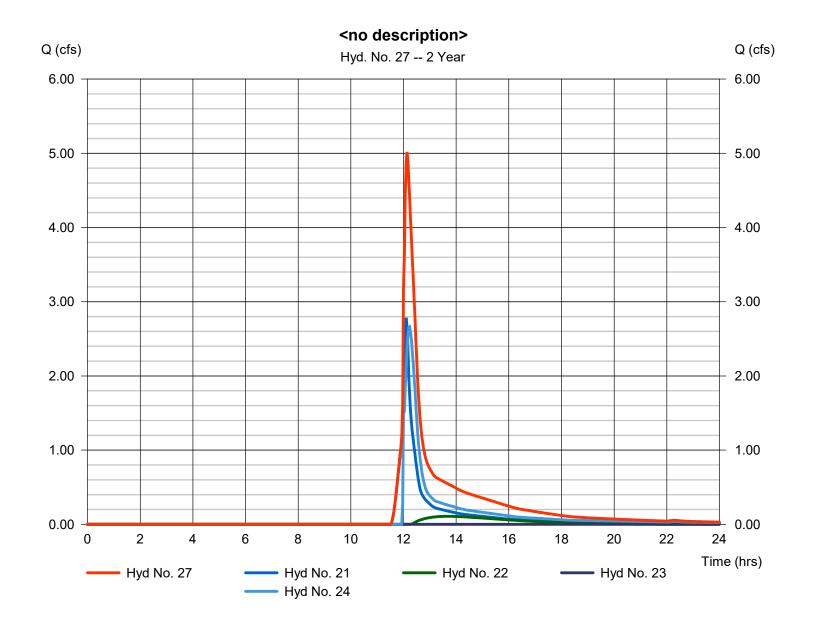
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 27

<no description>

Hydrograph type = Combine Peak discharge = 5.018 cfsStorm frequency = 2 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 17,576 cuft = 21, 22, 23, 24 Contrib. drain. area Inflow hyds. = 0.000 ac



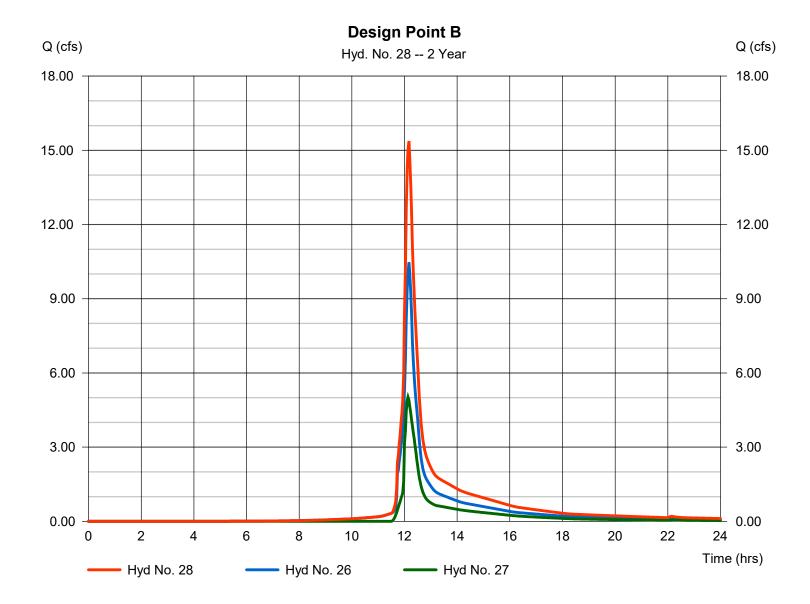
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 28

Design Point B

Hydrograph type = Combine Peak discharge = 15.38 cfsStorm frequency Time to peak = 2 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 53,163 cuft Inflow hyds. = 26, 27 Contrib. drain. area = 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

1 S S S S S S S S S S S S S S S S S S S	Hydrograph type (origin) GCS Runoff GCS Runoff GCS Runoff	Peak flow (cfs) 2.888 2.311	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
2 S 3 S 4 S	SCS Runoff			732	12.129				
3 S 4 S		2.311	2		,				PRWS-01
4 8	SCS Runoff		_	724	7,833				PR WS-02A(I)
		2.068	2	732	9,225				PR WS-02A(II)
5 S	SCS Runoff	2.352	2	726	8,205				PR WS-02B(I)
	SCS Runoff	2.046	2	724	7,053				PR WS-02B(II)
6 8	SCS Runoff	0.575	2	724	1,764				PR WS-02B(III)
7 8	SCS Runoff	2.622	2	726	9,558				PR WS-02C
8 8	SCS Runoff	9.148	2	728	36,588				PR WS-02D
9 8	SCS Runoff	1.006	2	724	3,313				PR WS-02E
10 8	SCS Runoff	5.072	2	724	16,697				PR WS-02F
11 8	SCS Runoff	4.656	2	724	15,541				PR WS-02G
12 8	SCS Runoff	0.876	2	730	3,613				PR WS-02H
13 8	SCS Runoff	4.450	2	732	20,472				PR WS-02I
14 S	SCS Runoff	0.138	2	724	442				PRWS-03
15 F	Reservoir	1.706	2	728	5,113	2	145.61	2,038	INFIL-1
16	Combine	3.643	2	730	14,338	3, 15			<no description=""></no>
17 F	Reservoir	3.595	2	732	12,718	16	136.99	1,353	INFIL-2
18 F	Reservoir	1.133	2	730	2,939	5	144.44	2,797	INFIL-3
19 F	Reservoir	8.916	2	730	31,682	8	139.12	3,650	TWIN 36IN PIPES (#2)
20 F	Reservoir	0.739	2	728	1,981	9	137.86	816	INFIL-4
21 F	Reservoir	4.208	2	726	13,323	10	136.63	2,653	INIFL-5
22 F	Reservoir	1.183	2	744	6,554	11	135.64	7,102	INFIL-6
23 F	Reservoir	0.000	2	676	0	12	132.37	3,398	36 INCH PIPE (#3)
24 F	Reservoir	4.422	2	732	17,270	13	135.72	2,454	TWO 36 INCH PIPES
25	Combine	11.13	2	730	41,240	7, 19,			<no description=""></no>
26	Combine	18.99	2	728	68,848	4, 6, 17,			<no description=""></no>
27	Combine	8.793	2	730	37,147	18, 20, 25 21, 22, 23,			<no description=""></no>
28 0	Combine	27.64	2	730	105,995	24, 26, 27			Design Point B

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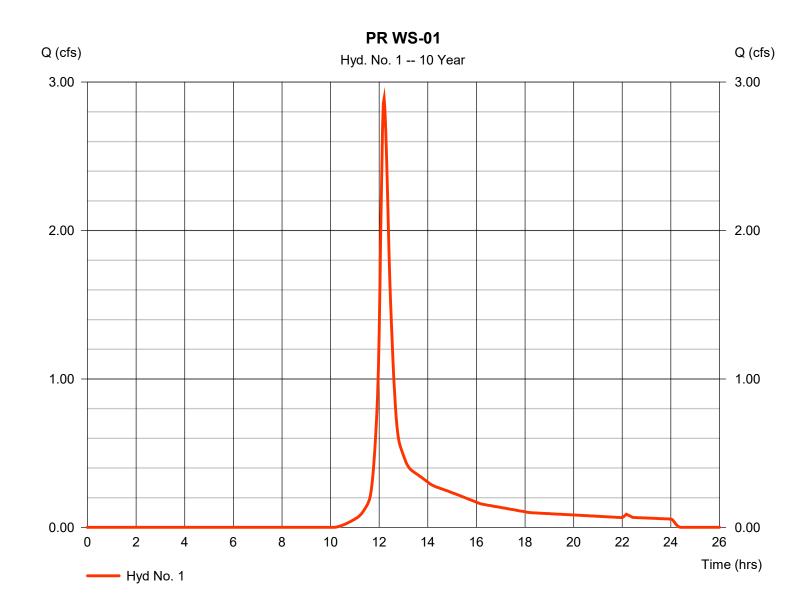
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Tuesday, 12 / 5 / 2023

Hyd. No. 1

PRWS-01

Hydrograph type = SCS Runoff Peak discharge = 2.888 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 12,129 cuft Drainage area = 1.721 acCurve number = 66 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.50 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



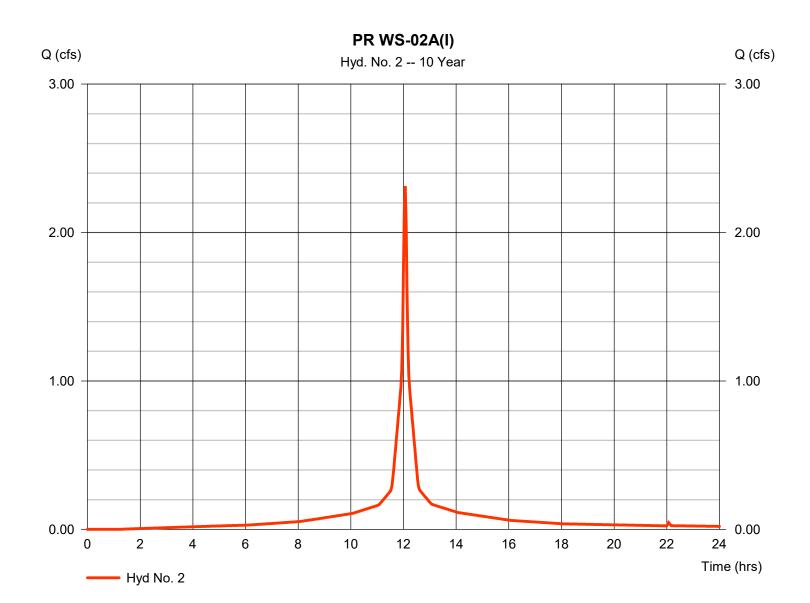
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Tuesday, 12 / 5 / 2023

Hyd. No. 2

PR WS-02A(I)

Hydrograph type = SCS Runoff Peak discharge = 2.311 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7.833 cuftDrainage area Curve number = 0.458 ac= 97 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



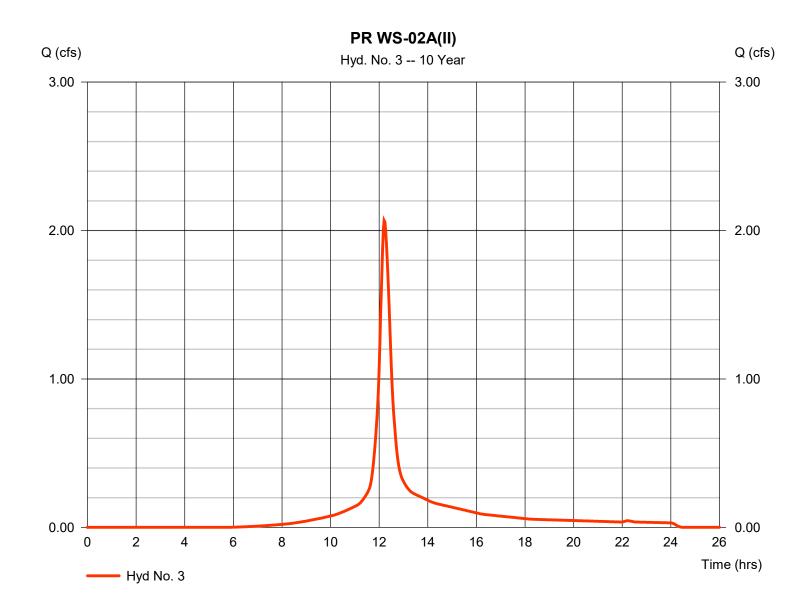
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Tuesday, 12 / 5 / 2023

Hyd. No. 3

PRWS-02A(II)

Hydrograph type = SCS Runoff Peak discharge = 2.068 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 9,225 cuftCurve number Drainage area = 0.683 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.10 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



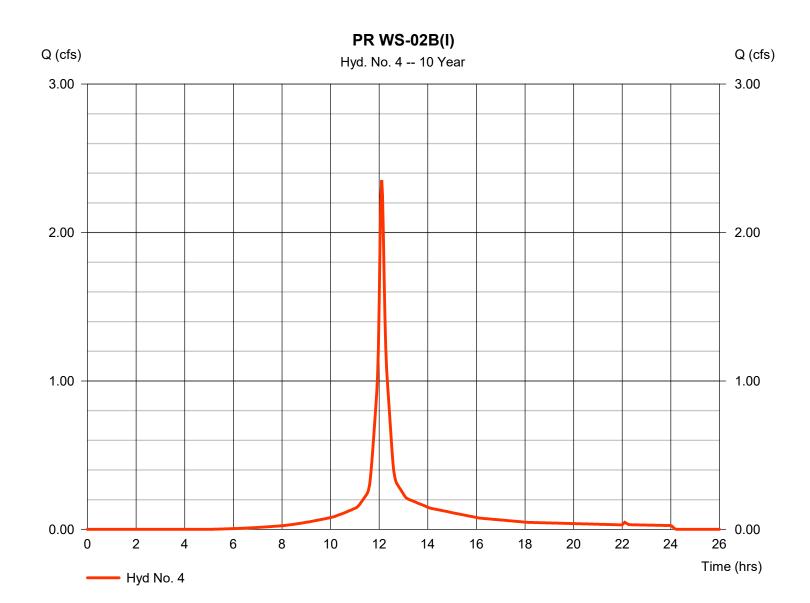
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 4

PR WS-02B(I)

Hydrograph type = SCS Runoff Peak discharge = 2.352 cfsStorm frequency = 10 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 8,205 cuft Drainage area Curve number = 0.576 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 7.40 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



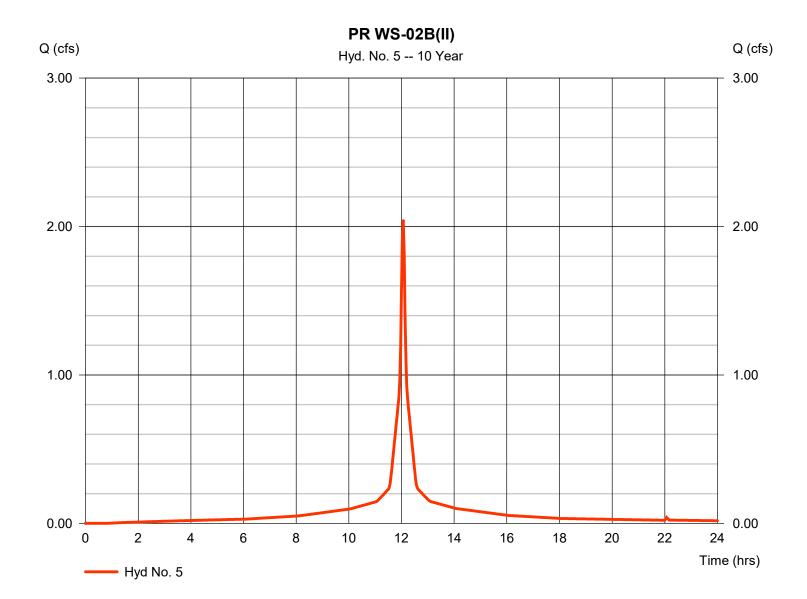
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Tuesday, 12 / 5 / 2023

Hyd. No. 5

PRWS-02B(II)

Hydrograph type = SCS Runoff Peak discharge = 2.046 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7,053 cuftDrainage area Curve number = 0.403 ac= 98 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



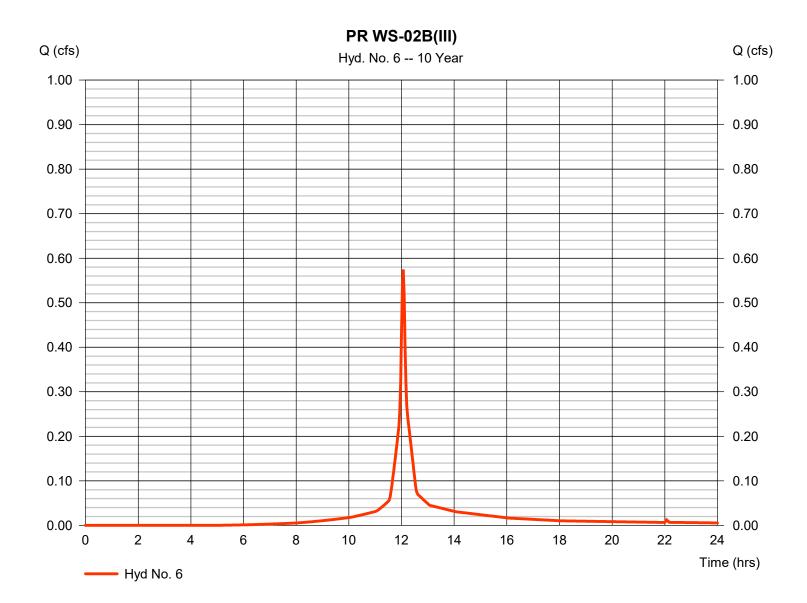
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Tuesday, 12 / 5 / 2023

Hyd. No. 6

PR WS-02B(III)

Hydrograph type = SCS Runoff Peak discharge = 0.575 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,764 cuftDrainage area Curve number = 0.132 ac= 87 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



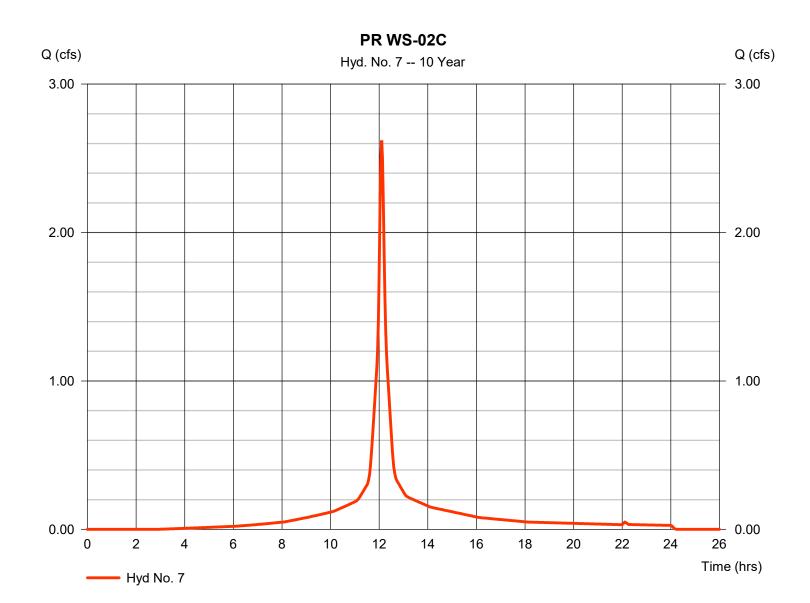
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 7

PRWS-02C

Hydrograph type = SCS Runoff Peak discharge = 2.622 cfsStorm frequency = 10 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 9,558 cuftDrainage area Curve number = 0.576 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



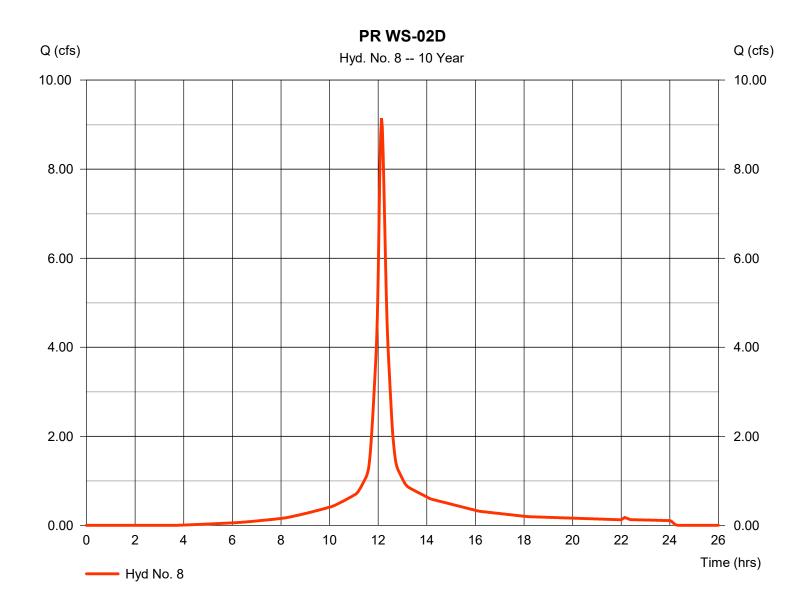
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Tuesday, 12 / 5 / 2023

Hyd. No. 8

PRWS-02D

Hydrograph type = SCS Runoff Peak discharge = 9.148 cfsStorm frequency = 10 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 36,588 cuft Drainage area = 2.246 acCurve number = 91 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 11.10 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



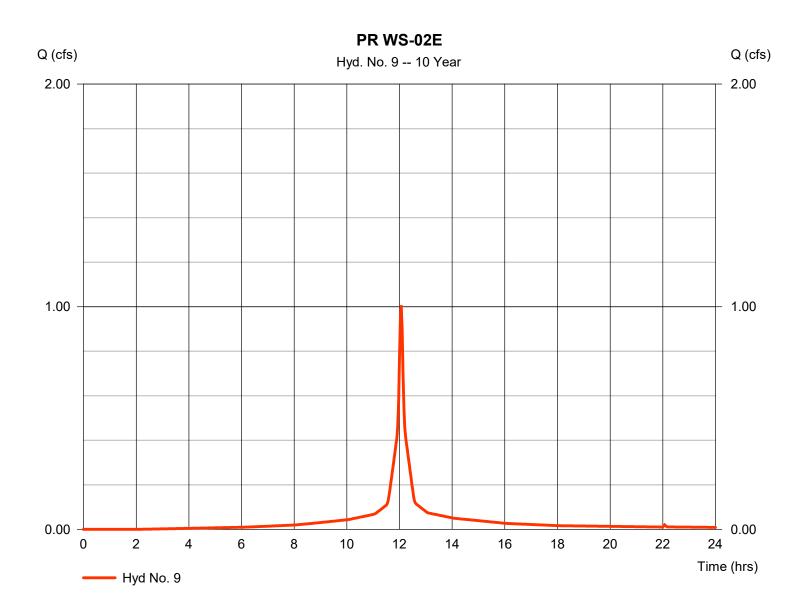
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 9

PRWS-02E

Hydrograph type = SCS Runoff Peak discharge = 1.006 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,313 cuftDrainage area = 0.203 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Tuesday, 12 / 5 / 2023

= 484

Hyd. No. 10

Storm duration

PR WS-02F

Hydrograph type = SCS Runoff Peak discharge = 5.072 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 16,697 cuft Drainage area Curve number = 1.023 ac= 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III

Shape factor

PR WS-02F Q (cfs) Q (cfs) Hyd. No. 10 -- 10 Year 6.00 6.00 5.00 5.00 4.00 4.00 3.00 3.00 2.00 2.00 1.00 1.00 0.00 0.00 2 4 6 8 10 12 14 16 18 20 22 24 Time (hrs) Hyd No. 10

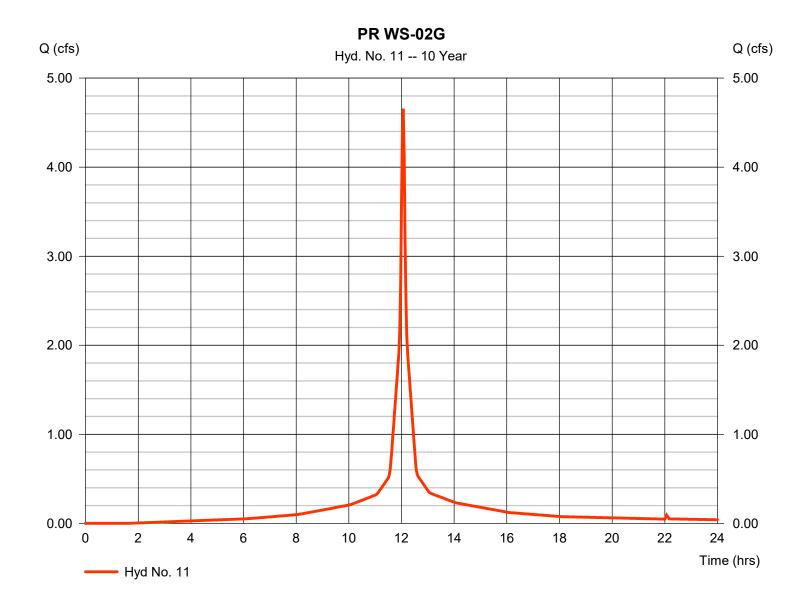
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Tuesday, 12 / 5 / 2023

Hyd. No. 11

PRWS-02G

Hydrograph type = SCS Runoff Peak discharge = 4.656 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 15,541 cuft Drainage area Curve number = 96 = 0.930 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



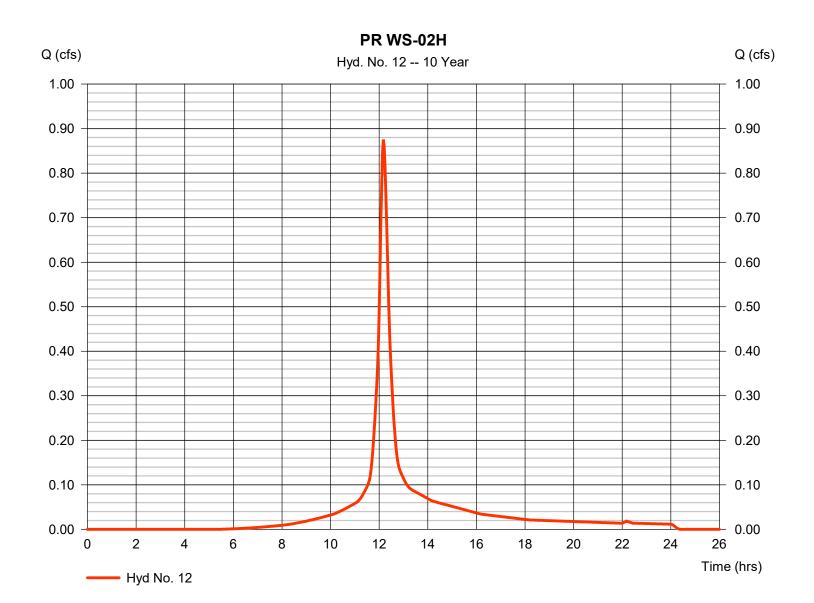
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Tuesday, 12 / 5 / 2023

Hyd. No. 12

PRWS-02H

Hydrograph type = SCS Runoff Peak discharge = 0.876 cfsStorm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 3,613 cuftDrainage area Curve number = 0.267 ac= 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.80 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



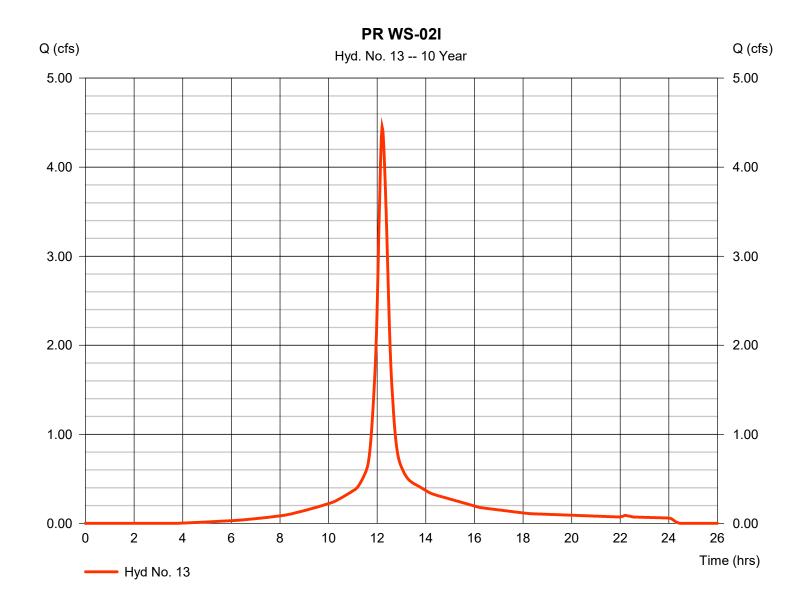
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Tuesday, 12 / 5 / 2023

Hyd. No. 13

PR WS-02I

Hydrograph type = SCS Runoff Peak discharge = 4.450 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 20,472 cuft = 1.296 acCurve number Drainage area = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



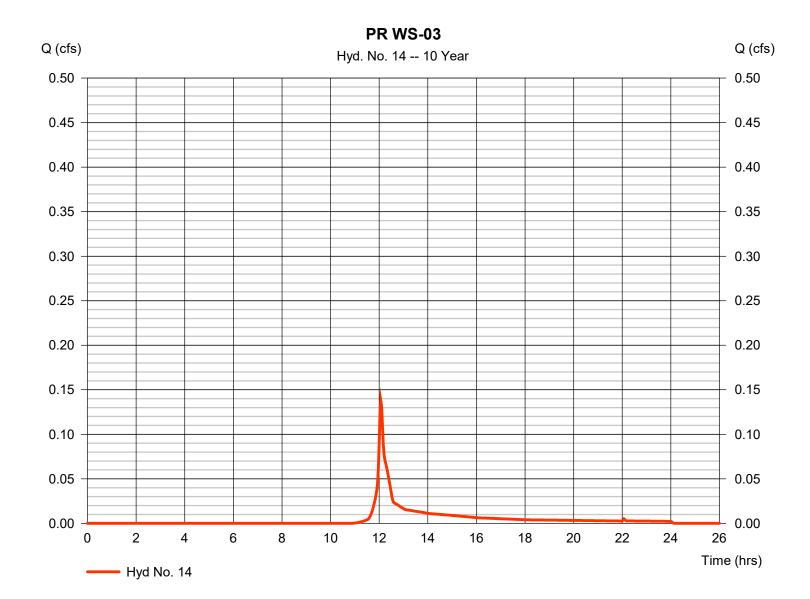
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Tuesday, 12 / 5 / 2023

Hyd. No. 14

PR WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.138 cfsStorm frequency = 10 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 442 cuft Drainage area Curve number = 0.081 ac= 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.10 \, \text{min}$ = User Total precip. = 5.38 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



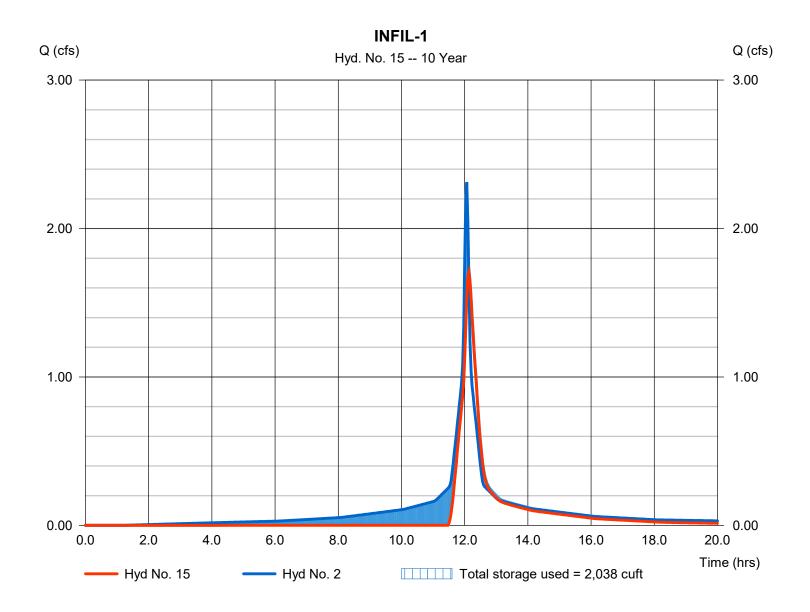
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Tuesday, 12 / 5 / 2023

Hyd. No. 15

INFIL-1

Hydrograph type = Reservoir Peak discharge = 1.706 cfsStorm frequency = 10 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 5,113 cuftInflow hyd. No. Max. Elevation = 2 - PR WS-02A(I)= 145.61 ft Reservoir name = INFIL-1 Max. Storage = 2,038 cuft



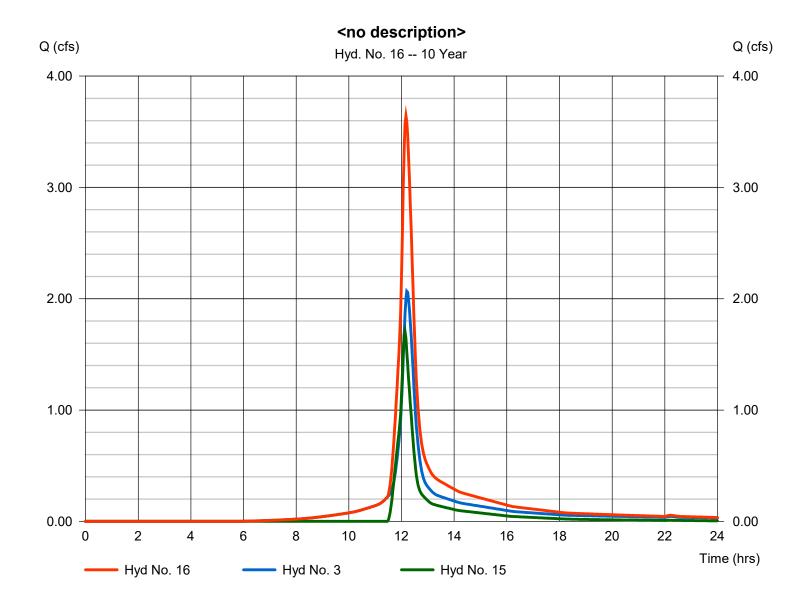
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Tuesday, 12 / 5 / 2023

Hyd. No. 16

<no description>

Hydrograph type = Combine Peak discharge = 3.643 cfsTime to peak Storm frequency = 10 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 14,338 cuft Inflow hyds. = 3, 15 Contrib. drain. area = 0.683 ac



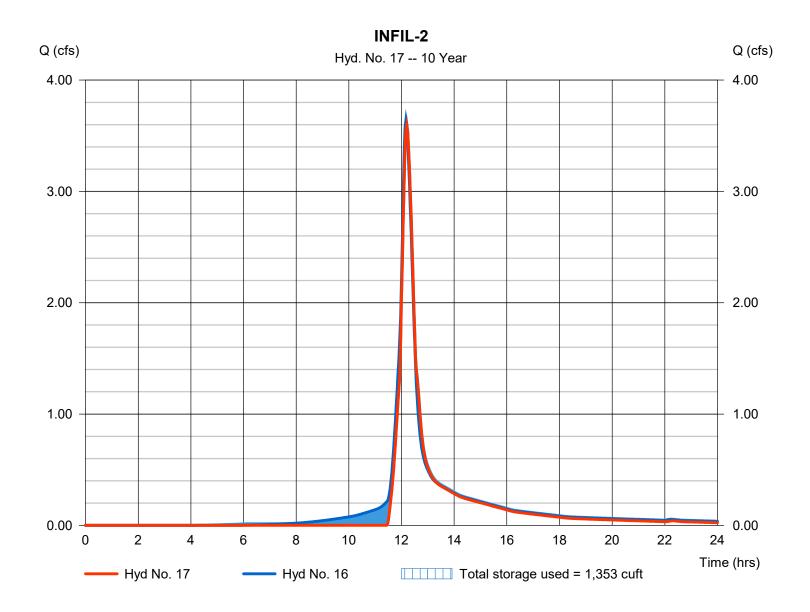
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Tuesday, 12 / 5 / 2023

Hyd. No. 17

INFIL-2

Hydrograph type = Reservoir Peak discharge = 3.595 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 12,718 cuft Inflow hyd. No. Max. Elevation = 16 - <no description> = 136.99 ftReservoir name = INFIL-2 Max. Storage = 1,353 cuft



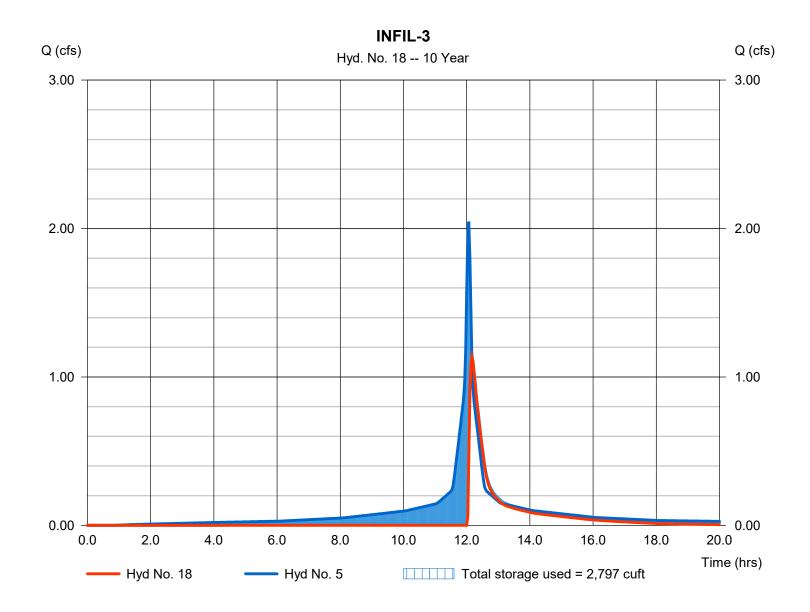
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Tuesday, 12 / 5 / 2023

Hyd. No. 18

INFIL-3

Hydrograph type = Reservoir Peak discharge = 1.133 cfsStorm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 2,939 cuftInflow hyd. No. Max. Elevation = 5 - PR WS-02B(II)= 144.44 ftReservoir name = INFIL-3 Max. Storage = 2,797 cuft



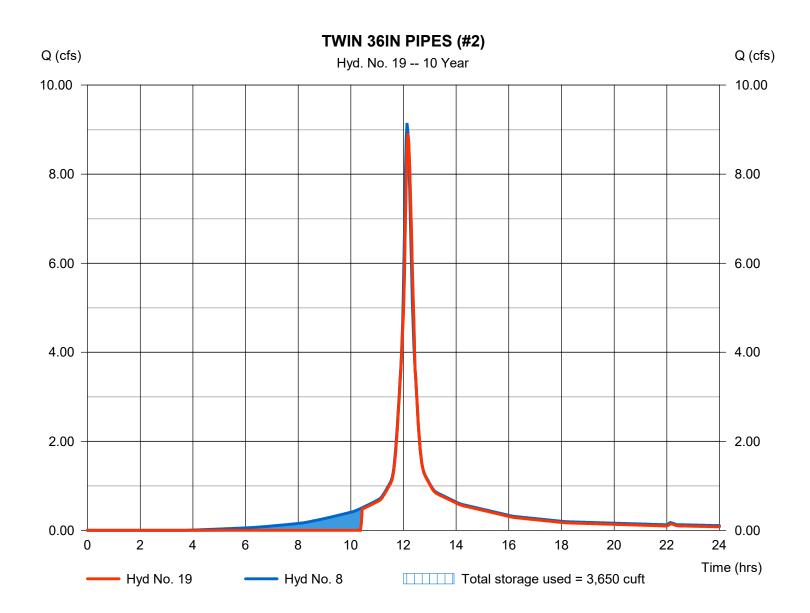
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Tuesday, 12 / 5 / 2023

Hyd. No. 19

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 8.916 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 31,682 cuft Max. Elevation = 139.12 ftInflow hyd. No. = 8 - PR WS-02D Reservoir name = Northern Twin 36IN Max. Storage = 3,650 cuft



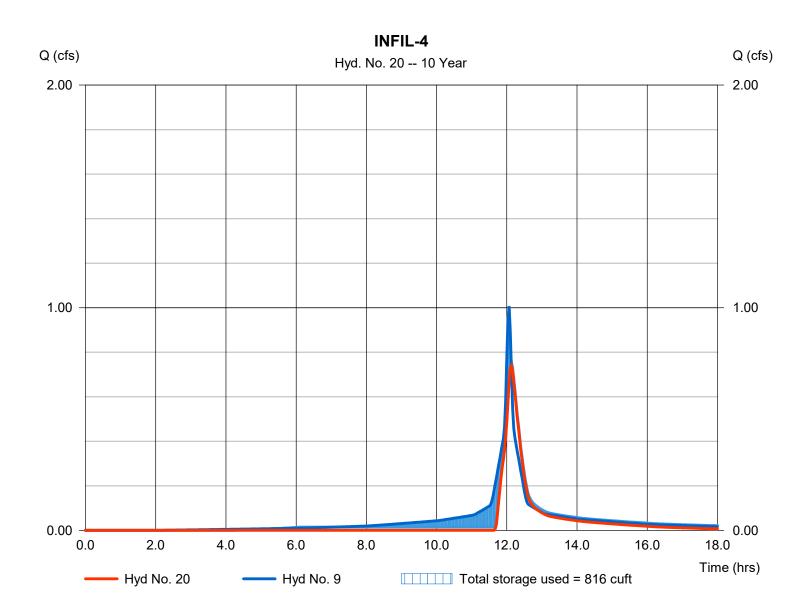
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Tuesday, 12 / 5 / 2023

Hyd. No. 20

INFIL-4

Hydrograph type = Reservoir Peak discharge = 0.739 cfsStorm frequency = 10 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 1,981 cuft Inflow hyd. No. Max. Elevation = 137.86 ft= 9 - PR WS-02E = 816 cuft Reservoir name = INFIL-4 Max. Storage



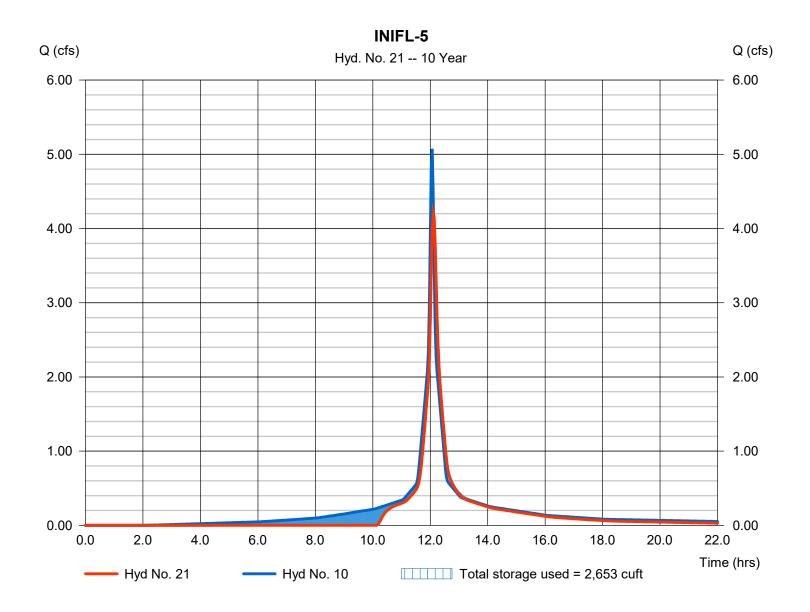
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Tuesday, 12 / 5 / 2023

Hyd. No. 21

INIFL-5

Hydrograph type Peak discharge = 4.208 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 13,323 cuft Inflow hyd. No. Max. Elevation = 10 - PR WS-02F $= 136.63 \, \text{ft}$ Reservoir name = INIFL-5 Max. Storage = 2,653 cuft



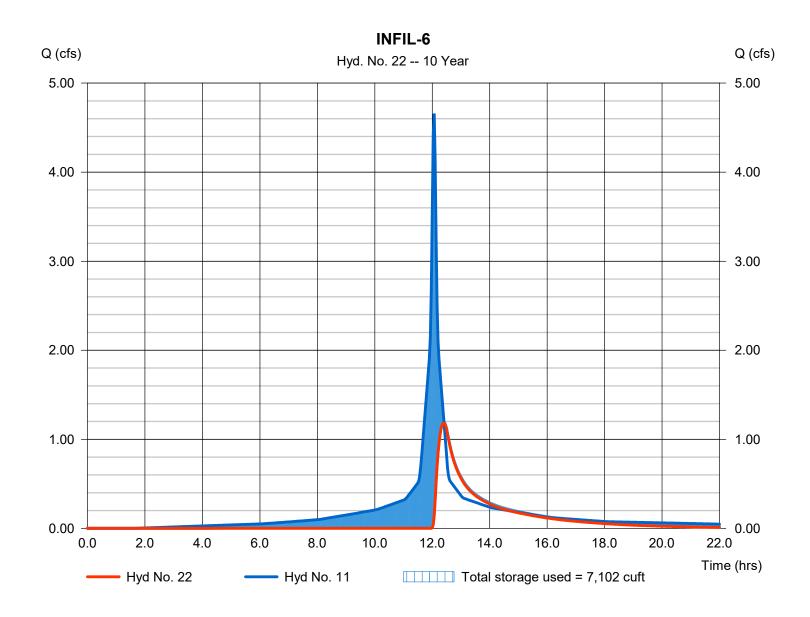
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Tuesday, 12 / 5 / 2023

Hyd. No. 22

INFIL-6

Hydrograph type Peak discharge = 1.183 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 6,554 cuftInflow hyd. No. Max. Elevation = 11 - PR WS-02G = 135.64 ftReservoir name = INFIL-6 Max. Storage = 7,102 cuft



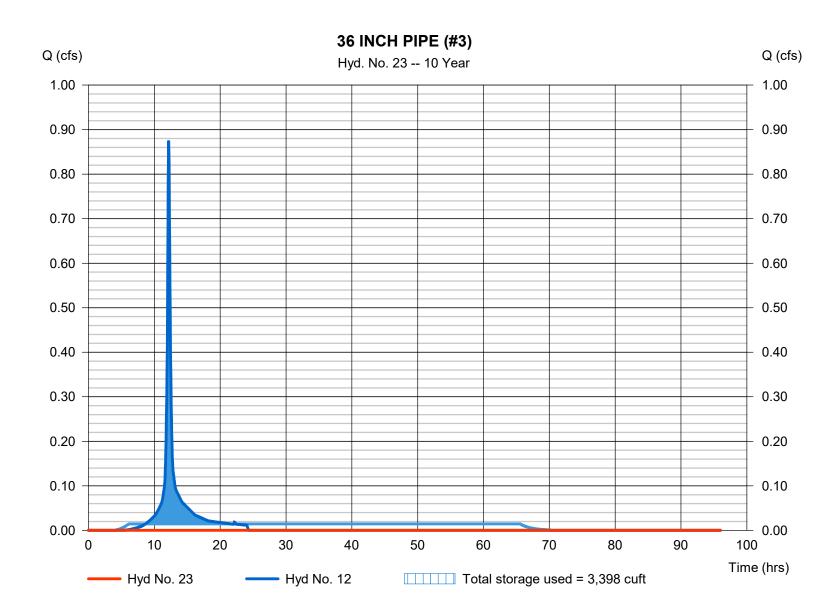
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Tuesday, 12 / 5 / 2023

Hyd. No. 23

36 INCH PIPE (#3)

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 11.27 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Max. Elevation Inflow hyd. No. = 12 - PR WS-02H = 132.37 ftReservoir name = 36IN - 3Max. Storage = 3,398 cuft



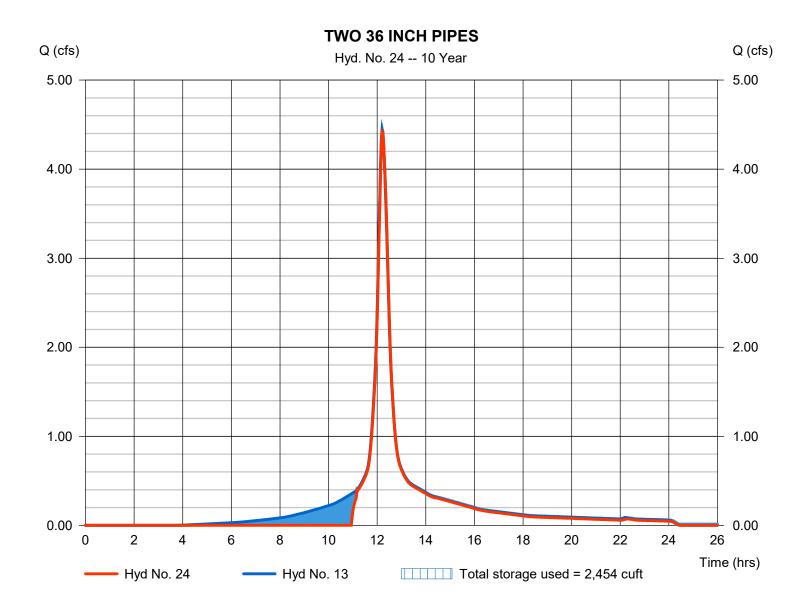
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Tuesday, 12 / 5 / 2023

Hyd. No. 24

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 4.422 cfs= Reservoir Storm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 17,270 cuftMax. Elevation Inflow hyd. No. = 13 - PR WS-02I = 135.72 ftReservoir name = TWIN 36IN Max. Storage = 2,454 cuft



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

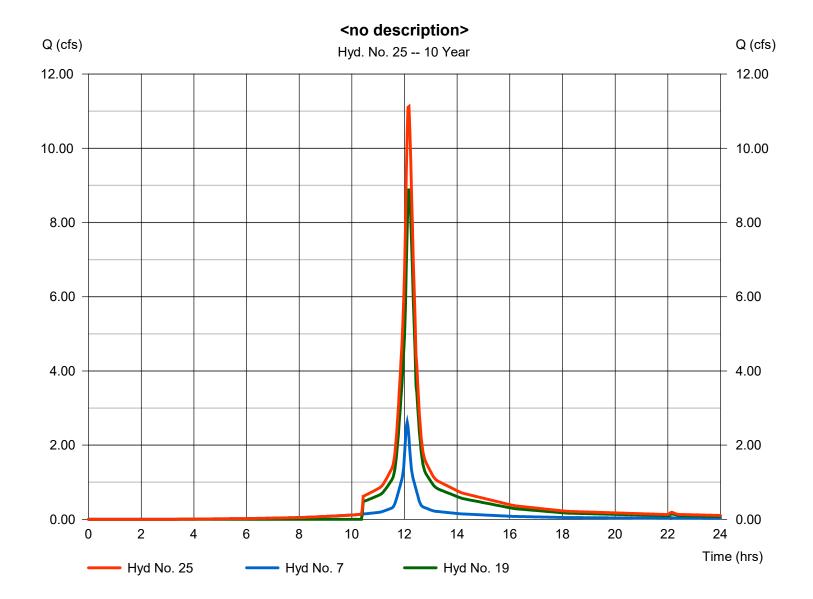
Tuesday, 12 / 5 / 2023

Hyd. No. 25

<no description>

Hydrograph type = Combine
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyds. = 7, 19

Peak discharge = 11.13 cfs
Time to peak = 12.17 hrs
Hyd. volume = 41,240 cuft
Contrib. drain. area = 0.576 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

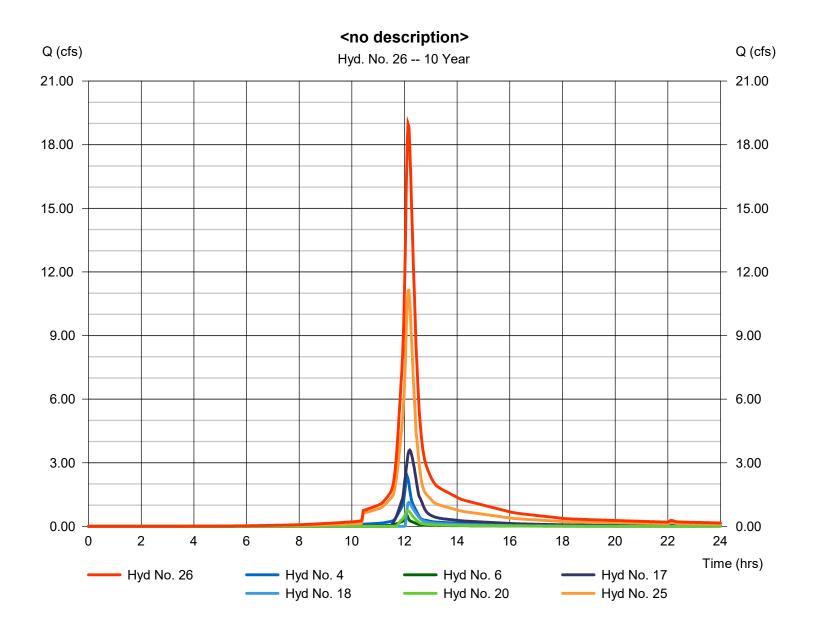
Hyd. No. 26

<no description>

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 2 min

Inflow hyds. = 4, 6, 17, 18, 20, 25

Peak discharge = 18.99 cfs
Time to peak = 12.13 hrs
Hyd. volume = 68,848 cuft
Contrib. drain. area = 0.708 ac



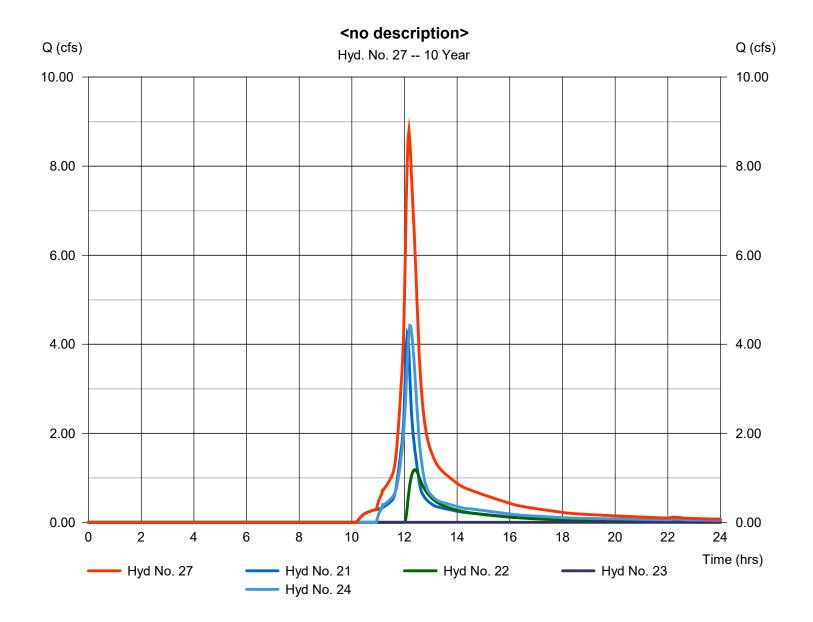
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Tuesday, 12 / 5 / 2023

Hyd. No. 27

<no description>

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 2 min Inflow hyds. = 21, 22, 23, 24 Peak discharge = 8.793 cfs
Time to peak = 12.17 hrs
Hyd. volume = 37,147 cuft
Contrib. drain. area = 0.000 ac



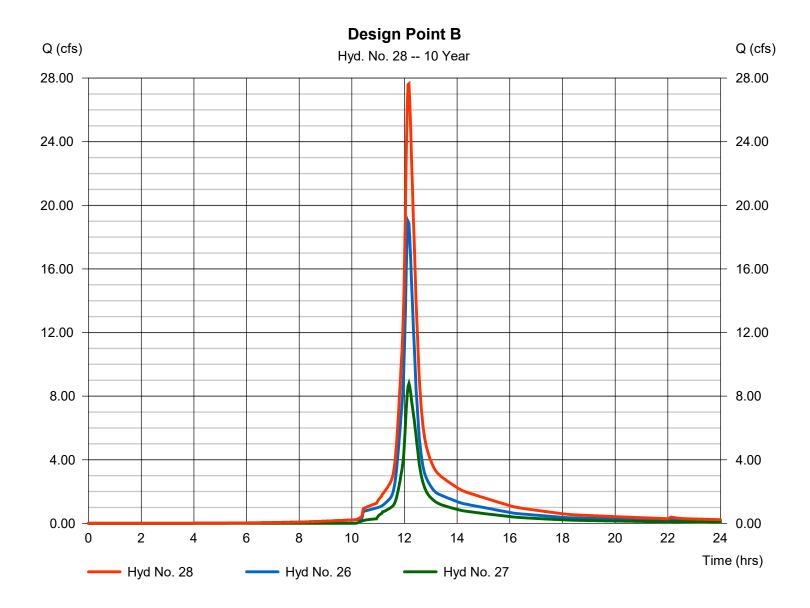
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Tuesday, 12 / 5 / 2023

Hyd. No. 28

Design Point B

Hydrograph type = Combine Peak discharge = 27.64 cfsStorm frequency Time to peak = 10 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 105,995 cuft Inflow hyds. Contrib. drain. area = 26, 27= 0.000 ac



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4.203 2.819 2.652 2.982 2.491 0.728 3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043 4.539	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	732 724 732 726 724 724 726 728 724 724 724 730 732 724	17,344 9,637 11,935 10,523 8,642 2,262 11,952 46,130 4,109 20,708 19,196 4,653 25,812				PR WS-01 PR WS-02A(I) PR WS-02A(II) PR WS-02B(II) PR WS-02B(III) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02E PR WS-02F PR WS-02G PR WS-02H
2.652 2.982 2.491 0.728 3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2 2 2 2 2 2	732 726 724 724 726 728 724 724 724 730 732	11,935 10,523 8,642 2,262 11,952 46,130 4,109 20,708 19,196 4,653				PR WS-02A(II) PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G
2.982 2.491 0.728 3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2 2 2 2 2 2	726 724 724 726 728 724 724 724 730 732	10,523 8,642 2,262 11,952 46,130 4,109 20,708 19,196 4,653				PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G
2.491 0.728 3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2 2 2 2 2	724 724 726 728 724 724 724 730 732	8,642 2,262 11,952 46,130 4,109 20,708 19,196 4,653				PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G
0.728 3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2 2 2 2	724 726 728 724 724 724 730 732	2,262 11,952 46,130 4,109 20,708 19,196 4,653				PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G
3.236 11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2 2	726 728 724 724 724 724 730 732	11,952 46,130 4,109 20,708 19,196 4,653				PR WS-02C PR WS-02D PR WS-02E PR WS-02F PR WS-02G
11.39 1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2 2	728 724 724 724 730 732	46,130 4,109 20,708 19,196 4,653				PR WS-02D PR WS-02E PR WS-02F PR WS-02G
1.234 6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2 2	724 724 724 730 732	4,109 20,708 19,196 4,653				PR WS-02E PR WS-02F PR WS-02G
6.217 5.692 1.116 5.543 0.212 2.043	2 2 2 2 2	724 724 730 732	20,708 19,196 4,653				PR WS-02F PR WS-02G
5.692 1.116 5.543 0.212 2.043	2 2 2 2	724 730 732	19,196 4,653				PR WS-02G
1.116 5.543 0.212 2.043	2 2 2	730 732	4,653				
5.543 0.212 2.043	2	732					PR WS-02H
0.212 2.043	2		25,812				1111100211
2.043		724					PR WS-02I
	2		655				PR WS-03
4.539	_	728	6,871	2	146.06	2,209	INFIL-1
	2	730	18,807	3, 15			<no description=""></no>
4.408	2	734	17,146	16	137.36	1,461	INFIL-2
1.687	2	728	4,424	5	144.88	3,070	INFIL-3
11.13	2	730	41,147	8	139.17	3,870	TWIN 36IN PIPES (#2)
0.882	2	728	2,727	9	138.12	894	INFIL-4
4.987	2	726	17,273	10	137.05	2,929	INIFL-5
2.355	2	734	9,861	11	136.11	7,919	INFIL-6
0.070	2	902	781	12	137.46	3,650	36 INCH PIPE (#3)
5.516	2	732	22,569	13	135.73	2,476	TWO 36 INCH PIPES
13.91	2	728	53,099	7, 19,			<no description=""></no>
23.97	2	728	90,181	4, 6, 17,			<no description=""></no>
12.22	2	730	50,484	21, 22, 23,			<no description=""></no>
35.87	2	728	140,665	24, 26, 27			Design Point B
	2.355 0.070 5.516 13.91 23.97 12.22	2.355 2 0.070 2 5.516 2 13.91 2 23.97 2 12.22 2	2.355 2 734 0.070 2 902 5.516 2 732 13.91 2 728 23.97 2 728 12.22 2 730	2.355 2 734 9,861 0.070 2 902 781 5.516 2 732 22,569 13.91 2 728 53,099 23.97 2 728 90,181 12.22 2 730 50,484	2.355 2 734 9,861 11 0.070 2 902 781 12 5.516 2 732 22,569 13 13.91 2 728 53,099 7, 19, 23.97 2 728 90,181 4, 6, 17, 18, 20, 25 12.22 2 730 50,484 21, 22, 23, 24, 24,	2.355 2 734 9,861 11 136.11 0.070 2 902 781 12 137.46 5.516 2 732 22,569 13 135.73 13.91 2 728 53,099 7, 19, 23.97 2 728 90,181 4, 6, 17, 12.22 2 730 50,484 21, 22, 23, 24, 24,	2.355 2 734 9,861 11 136.11 7,919 0.070 2 902 781 12 137.46 3,650 5.516 2 732 22,569 13 135.73 2,476 13.91 2 728 53,099 7, 19, 23.97 2 728 90,181 4, 6, 17, 12.22 2 730 50,484 21, 22, 23,

J:\F\F0173 Fuller\001 64 Danbury Rd\CalculatiRest\\@ndPerrivate2\Proparsed-HydrafiloTwu.egsp\nay, 12 / 5 / 2023

Hyd No. 1

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

= 24 hrs

Tuesday, 12 / 5 / 2023

= 484

Hyd. No. 1

Storm duration

PRWS-01

Hydrograph type = SCS Runoff Peak discharge = 4.203 cfsStorm frequency = 25 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 17,344 cuft Drainage area = 1.721 acCurve number = 66 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.50 min = User Total precip. = 6.54 inDistribution = Type III

Shape factor

PR WS-01 Q (cfs) Q (cfs) Hyd. No. 1 -- 25 Year 5.00 5.00 4.00 4.00 3.00 3.00 2.00 2.00 1.00 1.00 0.00 0.00 2 4 6 8 10 12 14 16 18 20 22 24 26 Time (hrs)

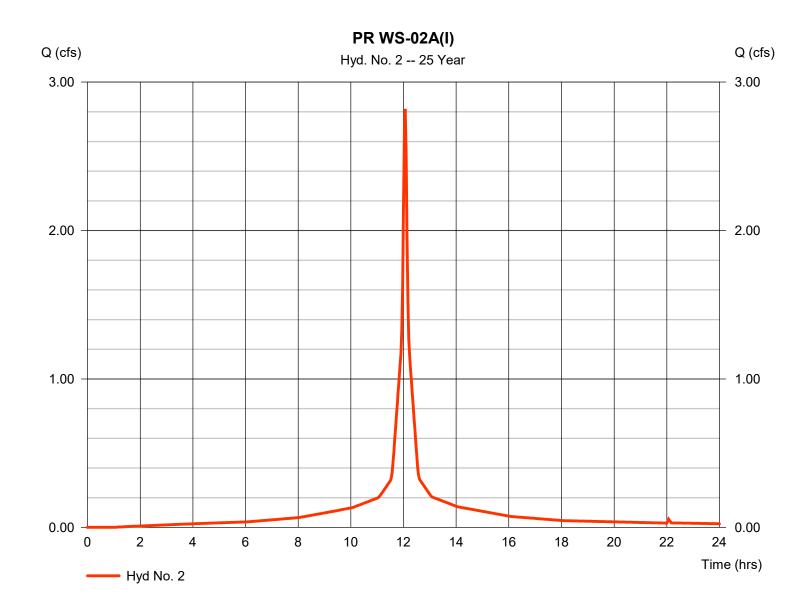
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 2

PR WS-02A(I)

Hydrograph type = SCS Runoff Peak discharge = 2.819 cfsStorm frequency = 25 yrs Time to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 9,637 cuftDrainage area Curve number = 0.458 ac= 97 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



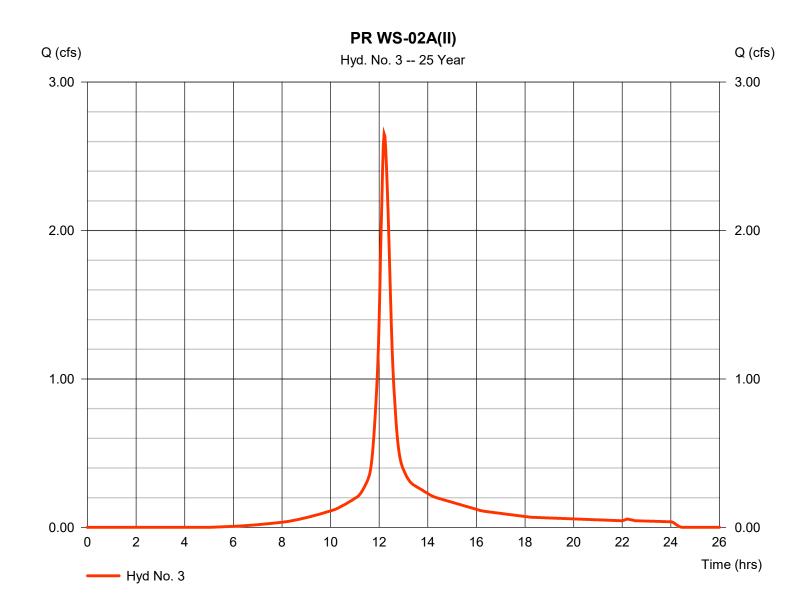
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 3

PRWS-02A(II)

Hydrograph type = SCS Runoff Peak discharge = 2.652 cfsStorm frequency = 25 yrs Time to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 11,935 cuft Drainage area Curve number = 0.683 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.10 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



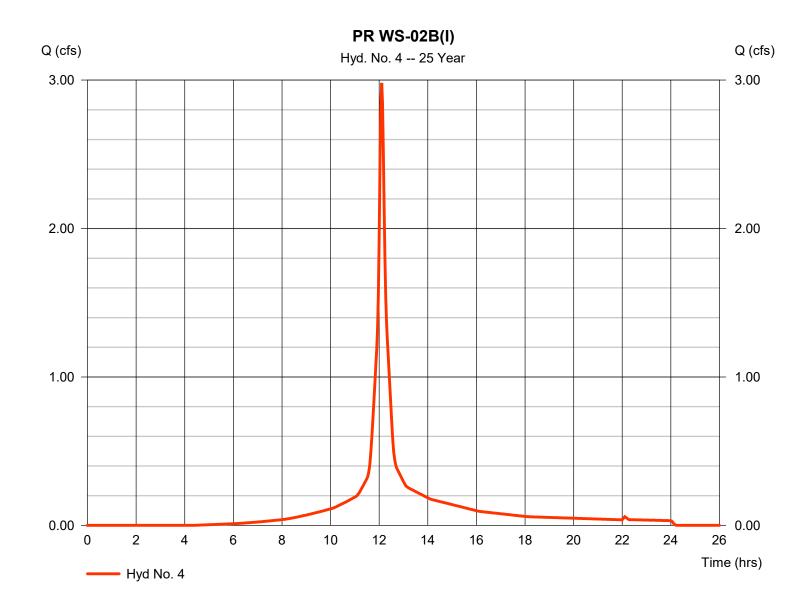
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 4

PR WS-02B(I)

Hydrograph type = SCS Runoff Peak discharge = 2.982 cfsStorm frequency = 25 yrs Time to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 10,523 cuftDrainage area Curve number = 0.576 ac= 87 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 7.40 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



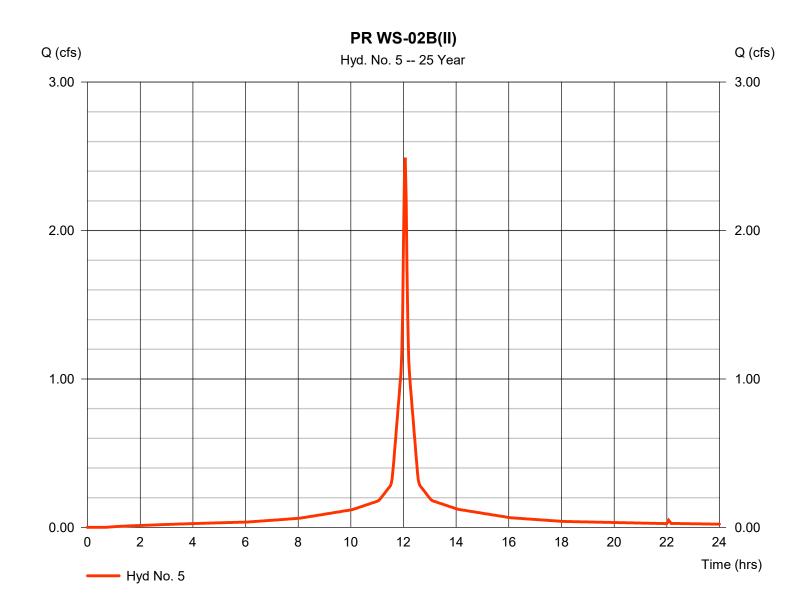
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 5

PRWS-02B(II)

Hydrograph type = SCS Runoff Peak discharge = 2.491 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 8,642 cuft Drainage area Curve number = 0.403 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



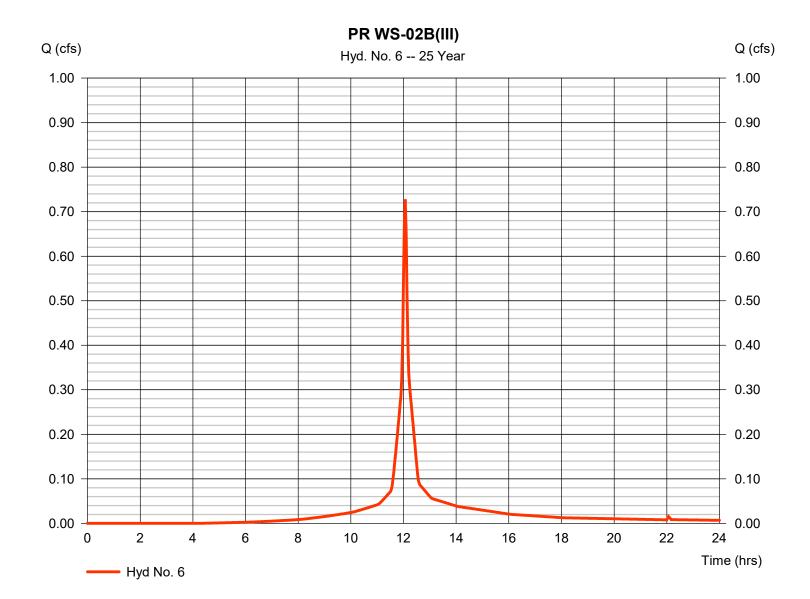
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 6

PR WS-02B(III)

Hydrograph type = SCS Runoff Peak discharge = 0.728 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2.262 cuft Drainage area Curve number = 0.132 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



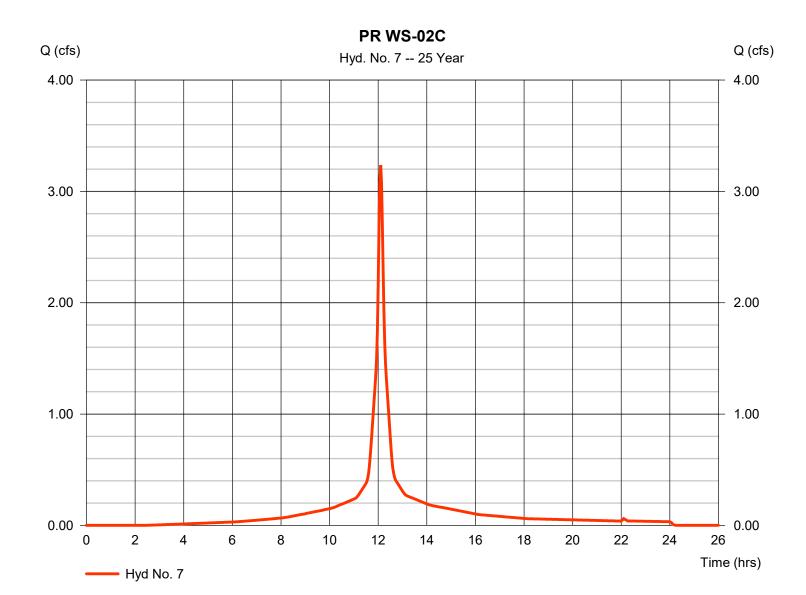
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 7

PRWS-02C

Hydrograph type = SCS Runoff Peak discharge = 3.236 cfsStorm frequency = 25 yrs Time to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 11,952 cuft Drainage area = 0.576 acCurve number = 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



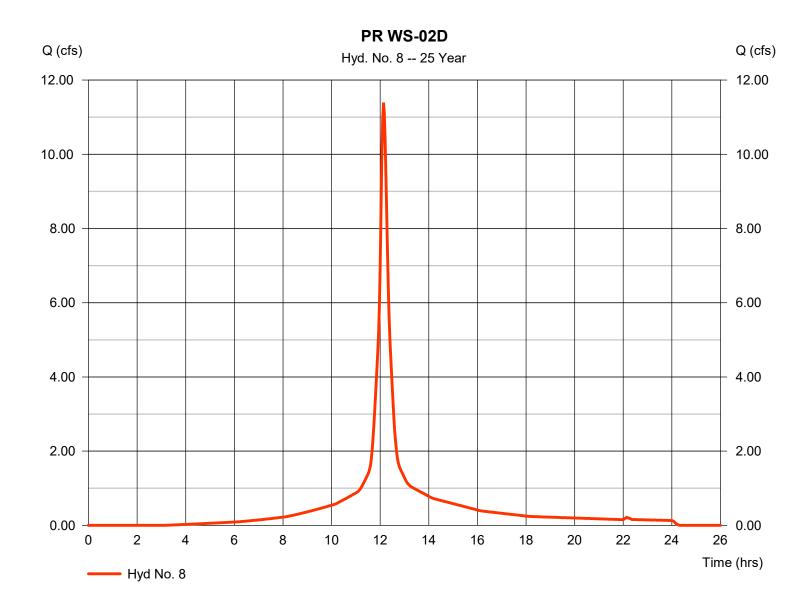
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 8

PRWS-02D

Hydrograph type = SCS Runoff Peak discharge = 11.39 cfsStorm frequency = 25 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 46,130 cuftDrainage area = 2.246 acCurve number = 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



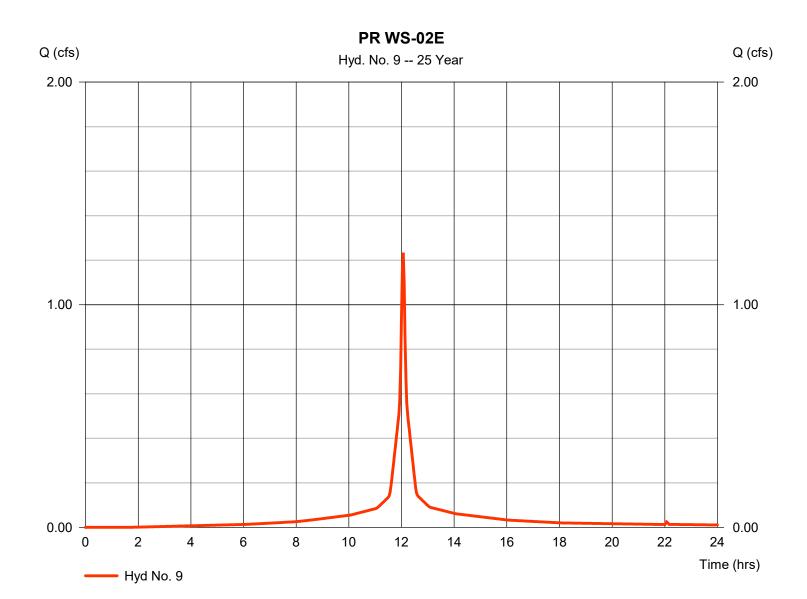
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 9

PRWS-02E

= SCS Runoff = 1.234 cfsHydrograph type Peak discharge Storm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,109 cuftDrainage area = 0.203 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

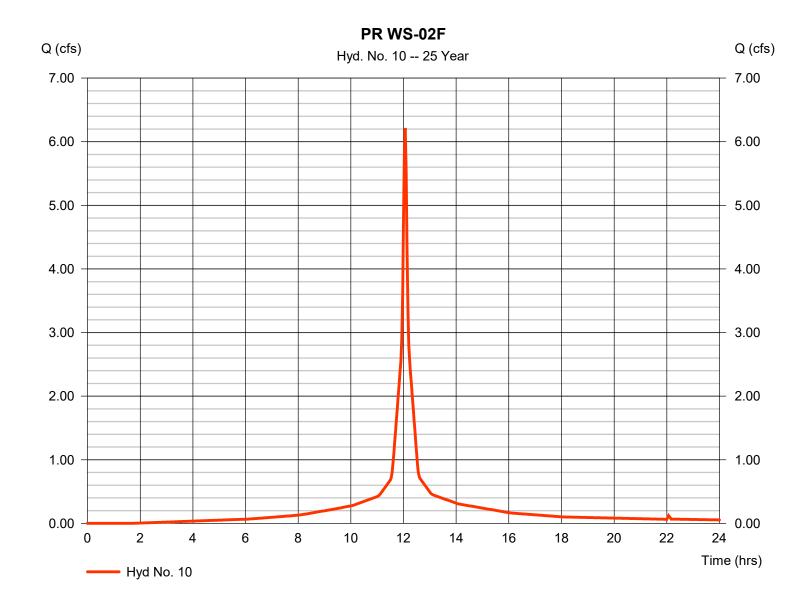
Tuesday, 12 / 5 / 2023

Hyd. No. 10

PR WS-02F

Hydrograph type = SCS Runoff Peak discharge = 6.217 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 20,708 cuft Drainage area Curve number = 1.023 ac= 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III

Storm duration = 24 hrs Shape factor = 484



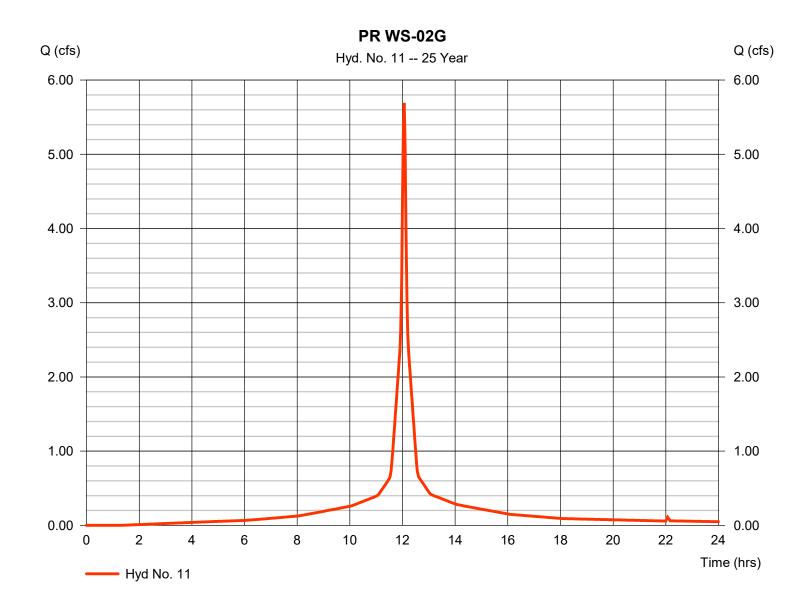
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 11

PRWS-02G

Hydrograph type = SCS Runoff Peak discharge = 5.692 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 19,196 cuft Drainage area Curve number = 96 = 0.930 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

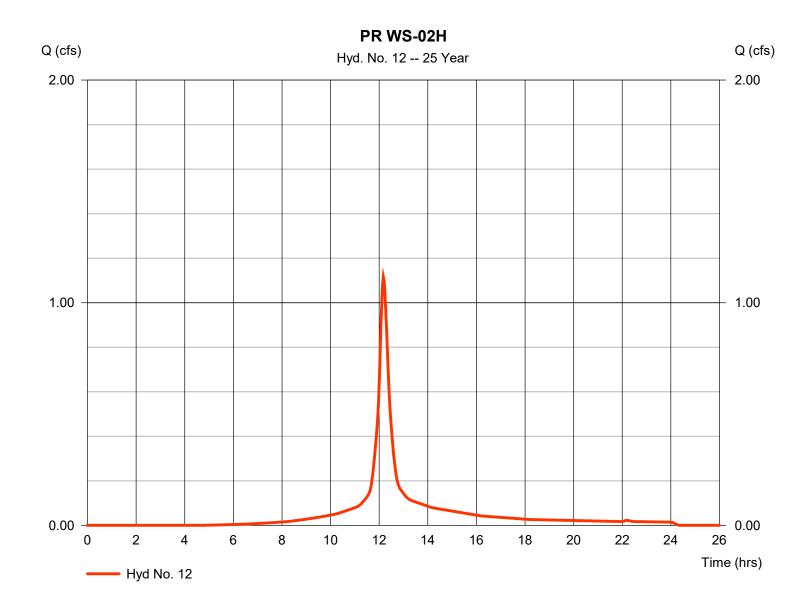
Tuesday, 12 / 5 / 2023

Hyd. No. 12

PR WS-02H

= SCS Runoff Hydrograph type Peak discharge = 1.116 cfsStorm frequency = 25 yrs Time to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 4,653 cuftDrainage area = 0.267 acCurve number = 86 Basin Slope = 0.0 %Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 13.80 min
Total precip. = 6.54 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484



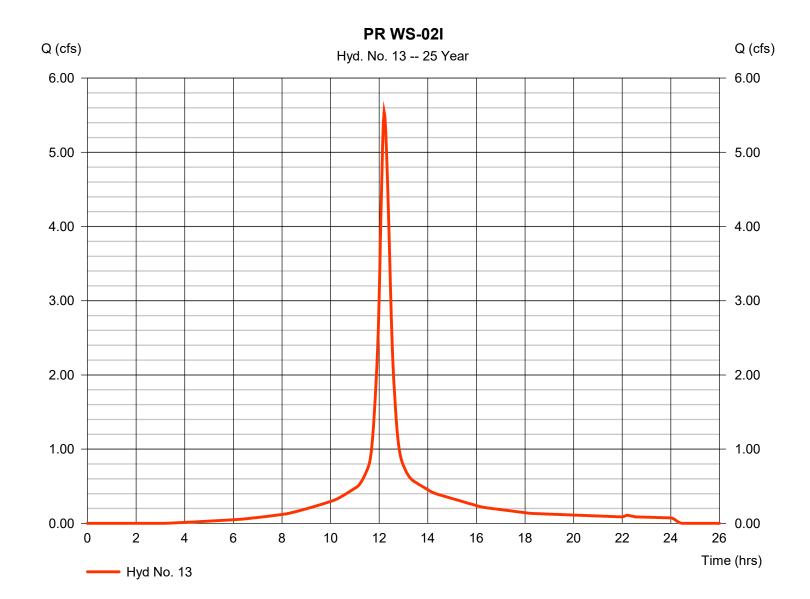
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 13

PR WS-02I

Hydrograph type = SCS Runoff Peak discharge = 5.543 cfsStorm frequency = 25 yrs Time to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 25,812 cuft Drainage area = 1.296 ac Curve number = 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



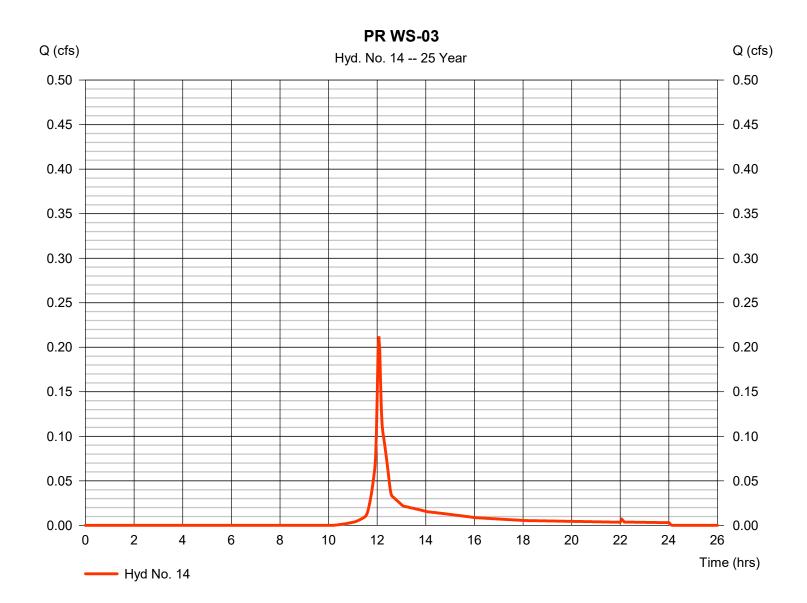
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 14

PR WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.212 cfsStorm frequency = 25 yrs Time to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 655 cuft Drainage area Curve number = 0.081 ac= 61 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.10 \, \text{min}$ = User Total precip. = 6.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



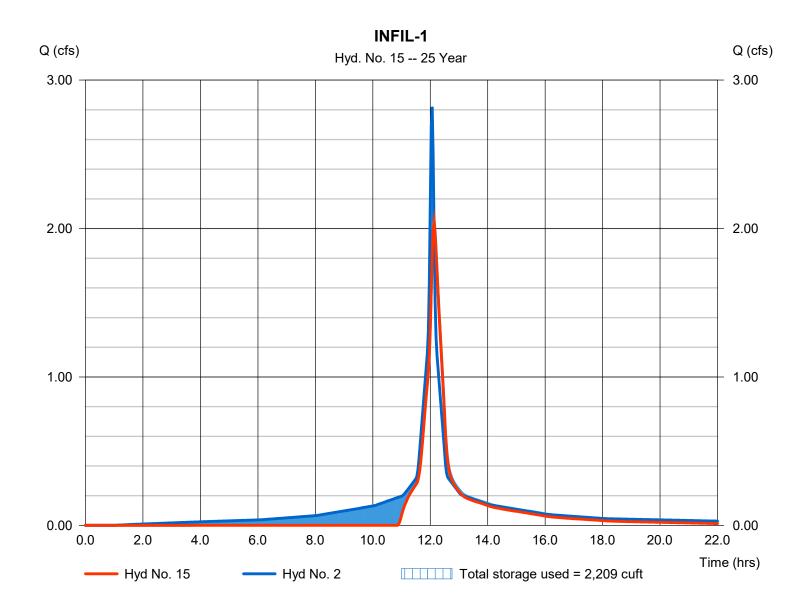
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 15

INFIL-1

Hydrograph type = Reservoir Peak discharge = 2.043 cfsStorm frequency = 25 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 6.871 cuftInflow hyd. No. Max. Elevation = 2 - PR WS-02A(I)= 146.06 ftReservoir name = INFIL-1 Max. Storage = 2,209 cuft



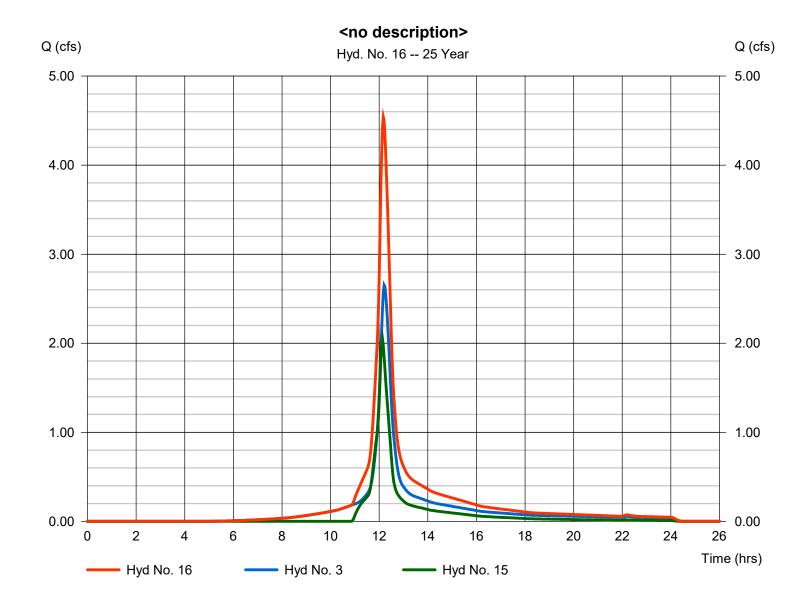
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 16

<no description>

Hydrograph type = Combine Peak discharge = 4.539 cfsStorm frequency = 25 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 18,807 cuft Inflow hyds. = 3, 15 Contrib. drain. area = 0.683 ac



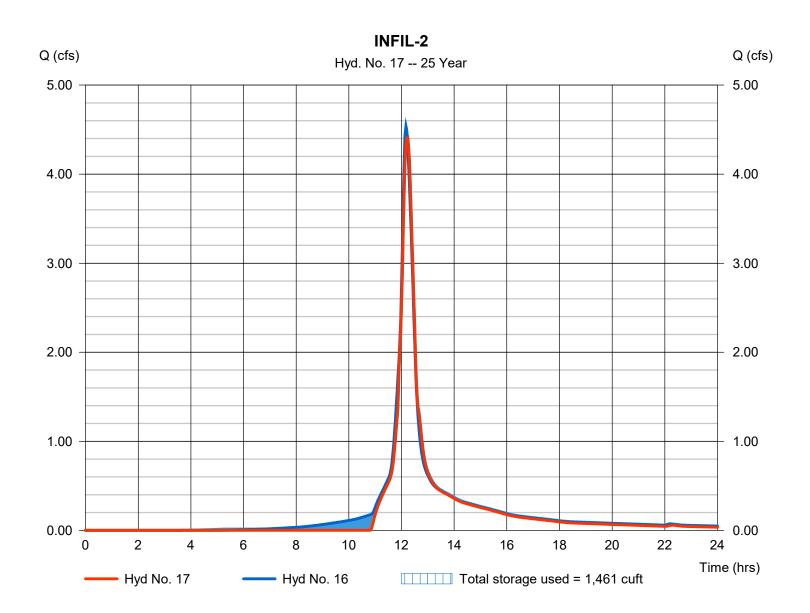
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 17

INFIL-2

Hydrograph type = Reservoir Peak discharge = 4.408 cfsStorm frequency = 25 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 17,146 cuft Max. Elevation = 137.36 ftInflow hyd. No. = 16 - <no description> Reservoir name = INFIL-2 Max. Storage = 1,461 cuft



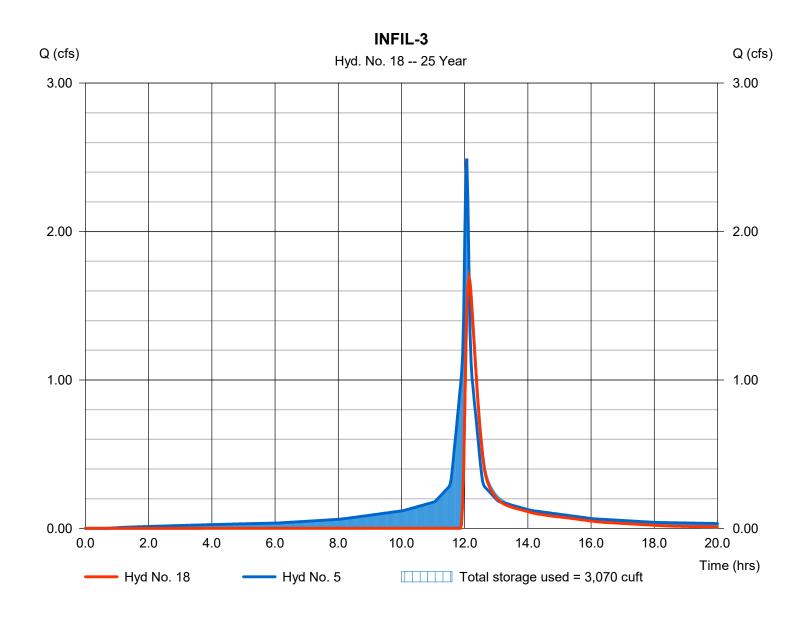
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 18

INFIL-3

Hydrograph type = Reservoir Peak discharge = 1.687 cfsStorm frequency = 25 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 4,424 cuft Inflow hyd. No. Max. Elevation = 5 - PR WS-02B(II)= 144.88 ftReservoir name = INFIL-3 Max. Storage = 3,070 cuft



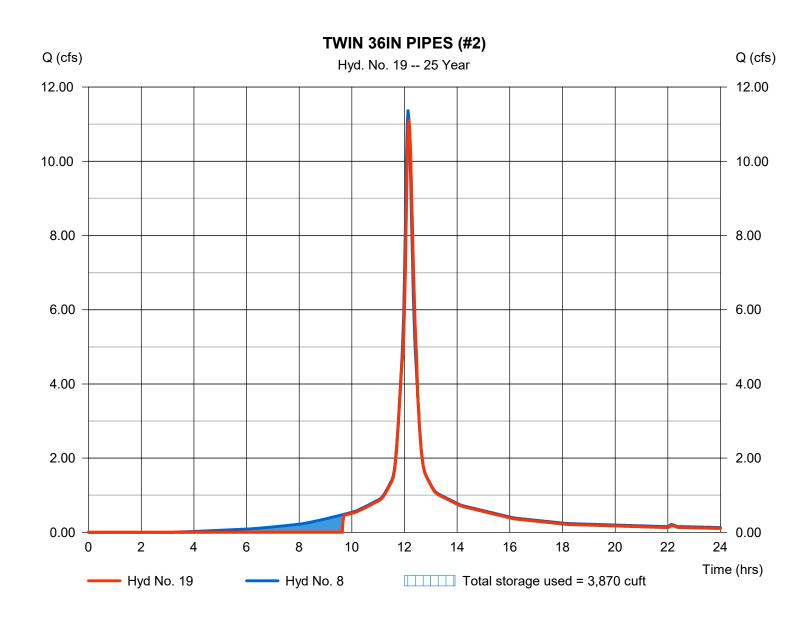
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 19

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 11.13 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 41,147 cuft Max. Elevation = 139.17 ft Inflow hyd. No. = 8 - PR WS-02D Reservoir name = Northern Twin 36IN Max. Storage = 3,870 cuft



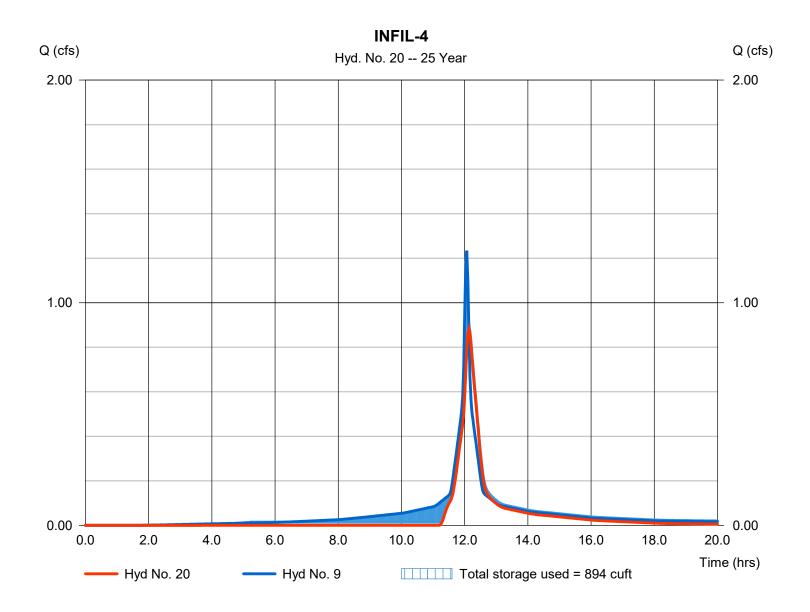
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 20

INFIL-4

Hydrograph type = Reservoir Peak discharge = 0.882 cfsStorm frequency = 25 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2,727 cuftInflow hyd. No. Max. Elevation = 9 - PR WS-02E = 138.12 ftReservoir name = INFIL-4 Max. Storage = 894 cuft



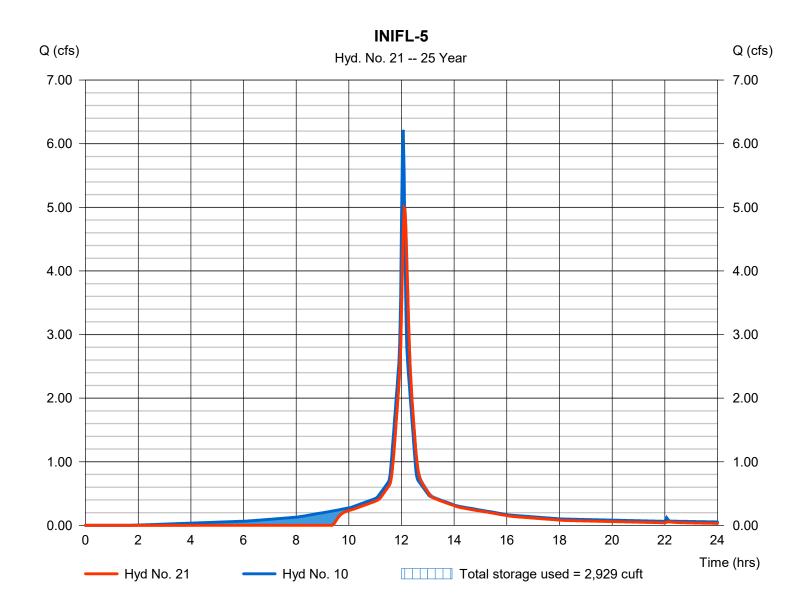
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 21

INIFL-5

Hydrograph type = Reservoir Peak discharge = 4.987 cfsStorm frequency = 25 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 17,273 cuftInflow hyd. No. Max. Elevation = 10 - PR WS-02F $= 137.05 \, \text{ft}$ Reservoir name = INIFL-5 Max. Storage = 2,929 cuft



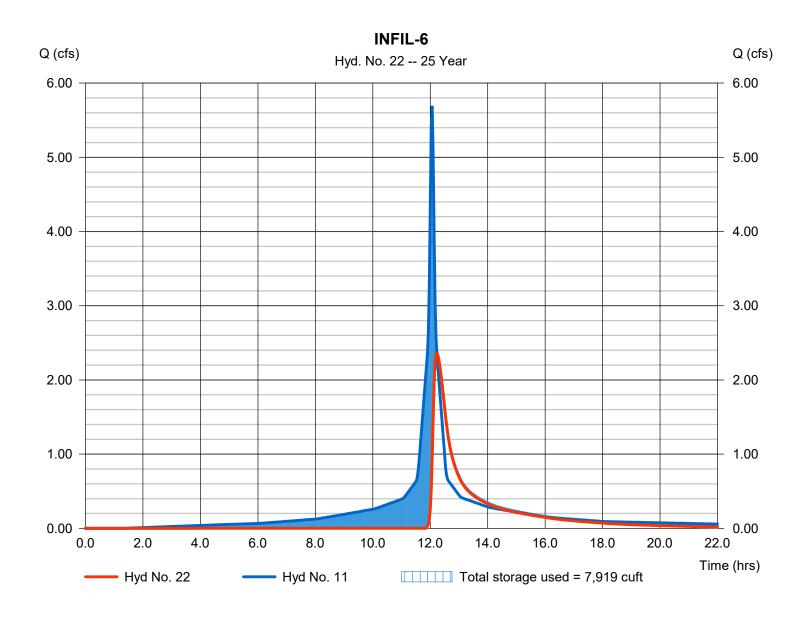
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 22

INFIL-6

Hydrograph type = Reservoir Peak discharge = 2.355 cfsStorm frequency = 25 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 9,861 cuft Inflow hyd. No. Max. Elevation = 136.11 ft = 11 - PR WS-02G Reservoir name = INFIL-6 Max. Storage = 7,919 cuft



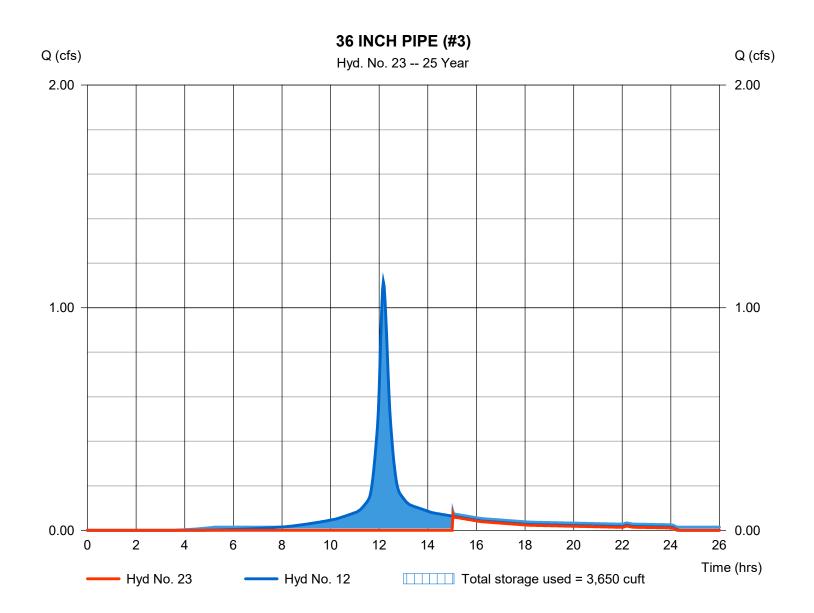
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 23

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 0.070 cfsStorm frequency = 25 yrsTime to peak $= 15.03 \, hrs$ Time interval = 2 min Hyd. volume = 781 cuft Max. Elevation Inflow hyd. No. = 12 - PR WS-02H = 137.46 ftReservoir name = 36IN - 3Max. Storage = 3,650 cuft



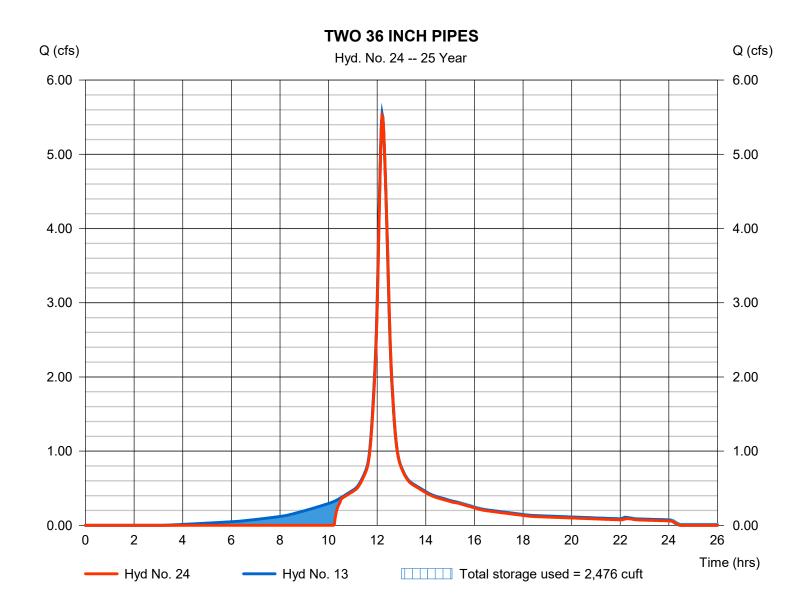
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 24

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 5.516 cfs= Reservoir Storm frequency = 25 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 22,569 cuftMax. Elevation Inflow hyd. No. = 13 - PR WS-02I = 135.73 ftReservoir name = TWIN 36IN Max. Storage = 2,476 cuft



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

= 13.91 cfs

 $= 12.13 \, hrs$

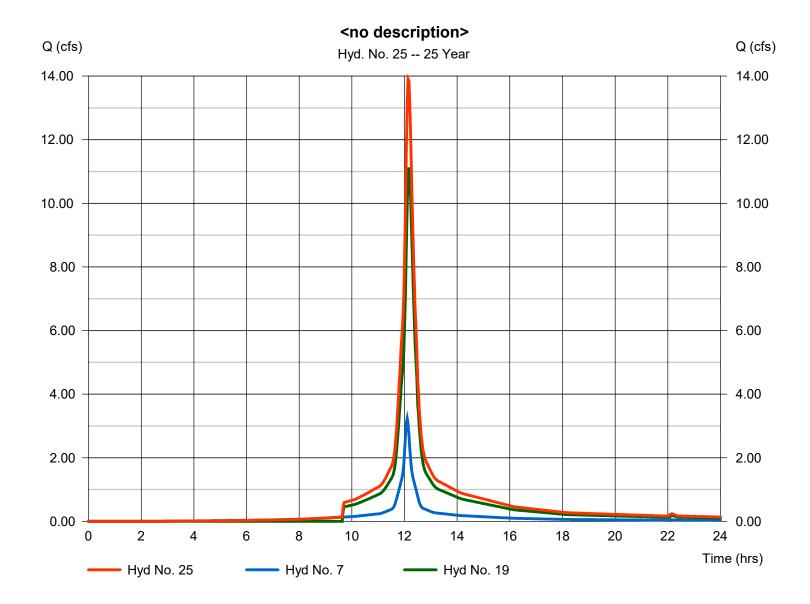
= 0.576 ac

= 53,099 cuft

Hyd. No. 25

<no description>

Hydrograph type= CombinePeak dischargeStorm frequency= 25 yrsTime to peakTime interval= 2 minHyd. volumeInflow hyds.= 7, 19Contrib. drain. area



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

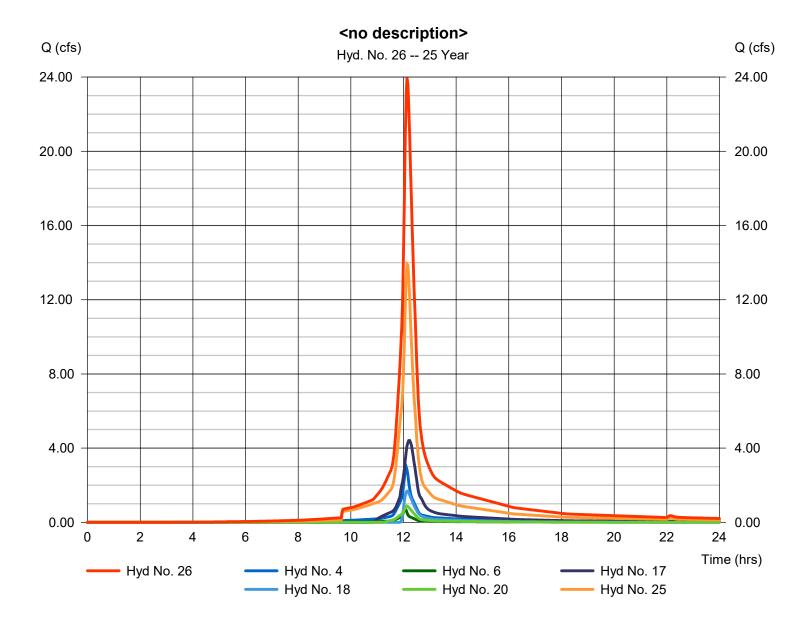
Hyd. No. 26

<no description>

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 2 min

Inflow hyds. = 4, 6, 17, 18, 20, 25

Peak discharge = 23.97 cfs
Time to peak = 12.13 hrs
Hyd. volume = 90,181 cuft
Contrib. drain. area = 0.708 ac



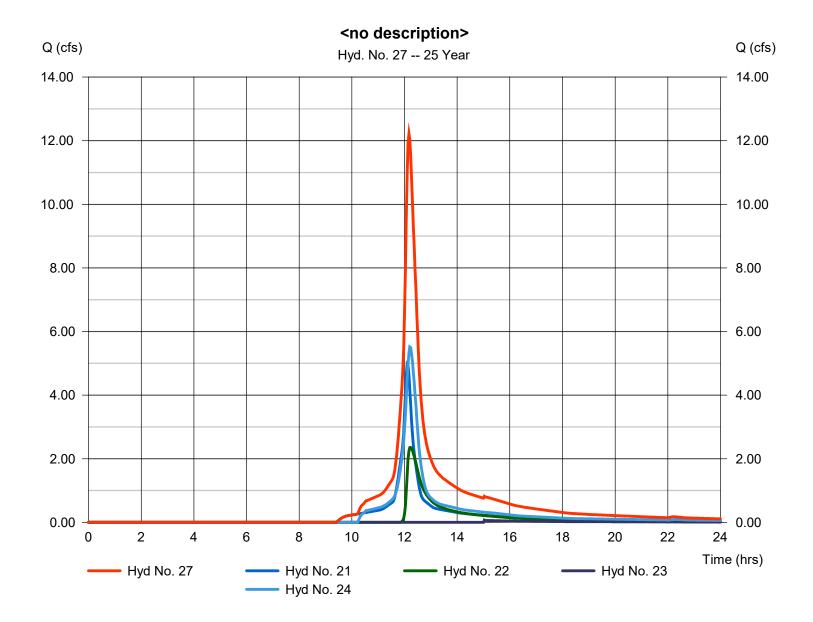
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 27

<no description>

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 2 min Inflow hyds. = 21, 22, 23, 24 Peak discharge = 12.22 cfs
Time to peak = 12.17 hrs
Hyd. volume = 50,484 cuft
Contrib. drain. area = 0.000 ac



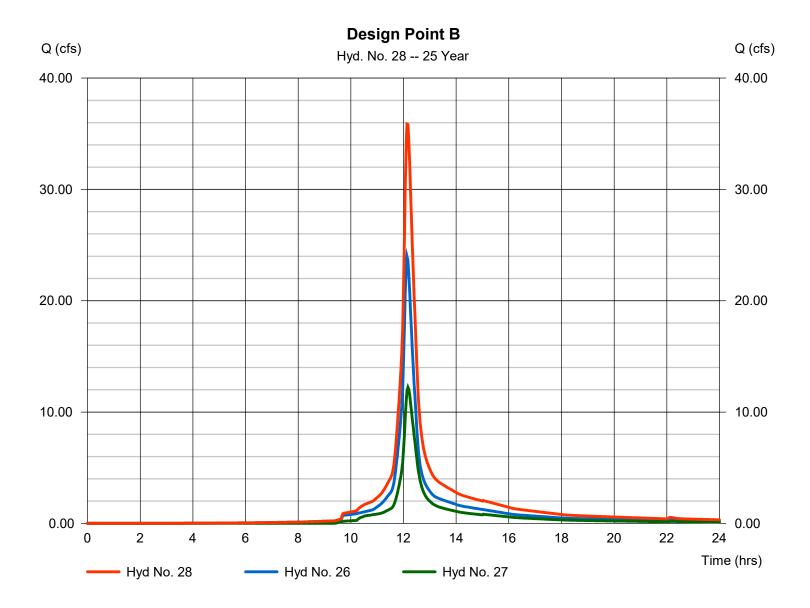
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 28

Design Point B

Hydrograph type = Combine Peak discharge = 35.87 cfsTime to peak Storm frequency = 25 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 140,665 cuft Inflow hyds. = 26, 27 Contrib. drain. area = 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

noff 5.239 noff 3.199 noff 3.089 noff 3.451 noff 2.824 noff 0.842 noff 3.695 noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358 noff 0.272	2 2 2 2 2 2 2 2 2 2 2 2 2	730 724 732 726 724 724 726 728 724 724 724	21,499 10,990 13,997 12,280 9,834 2,640 13,753 53,326 4,707 23,722 21,940				PR WS-01 PR WS-02A(I) PR WS-02A(II) PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D PR WS-02E
3.089 3.451 2.824 noff 0.842 noff 3.695 noff 13.06 noff 1.404 noff 6.467 noff 6.358	2 2 2 2 2 2 2 2 2 2 2	732 726 724 724 726 728 724 724 724	13,997 12,280 9,834 2,640 13,753 53,326 4,707 23,722				PR WS-02A(II) PR WS-02B(I) PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D
noff 3.451 2.824 noff 0.842 noff 3.695 noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2 2 2 2 2 2 2	726 724 724 726 728 724 724	12,280 9,834 2,640 13,753 53,326 4,707 23,722				PR WS-02B(II) PR WS-02B(III) PR WS-02B(III) PR WS-02C PR WS-02D
noff 2.824 noff 0.842 noff 3.695 noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2 2 2 2 2 2	724 724 726 728 724 724 724	9,834 2,640 13,753 53,326 4,707 23,722				PR WS-02B(II) PR WS-02B(III) PR WS-02C PR WS-02D
noff 0.842 3.695 noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2 2 2 2	724 726 728 724 724 724	2,640 13,753 53,326 4,707 23,722				PR WS-02B(III) PR WS-02C PR WS-02D
noff 3.695 noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2 2 2	726 728 724 724 724	13,753 53,326 4,707 23,722				PR WS-02C PR WS-02D
noff 13.06 noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2 2	728 724 724 724	53,326 4,707 23,722				PR WS-02D
noff 1.404 noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2 2	724 724 724	4,707 23,722				
noff 7.074 noff 6.467 noff 1.296 noff 6.358	2 2 2	724 724	23,722				DB WS 03E
noff 6.467 noff 1.296 noff 6.358	2 2	724			1		PR W3-02E
noff 1.296 noff 6.358	2		21 940				PR WS-02F
noff 6.358			21,010				PR WS-02G
		730	5,444				PR WS-02H
noff 0.272	2	732	29,838				PR WS-02I
	2	724	827				PR WS-03
ir 2.310	2	728	8,200	2	146.47	2,337	INFIL-1
5.234	2	730	22,197	3, 15			<no description=""></no>
ir 5.080	2	732	20,511	16	137.80	1,561	INFIL-2
ir 1.927	2	728	5,568	5	145.20	3,232	INFIL-3
ir 12.78	2	730	48,298	8	139.20	4,033	TWIN 36IN PIPES (#2)
ir 0.989	2	728	3,300	9	138.34	955	INFIL-4
ir 5.575	2	728	20,252	10	137.41	3,146	INIFL-5
ir 3.607	2	730	12,398	11	136.47	8,476	INFIL-6
ir 0.167	2	790	1,564	12	137.46	3,653	36 INCH PIPE (#3)
ir 6.332	2	732	26,572	13	135.75	2,492	TWO 36 INCH PIPES
15.96	2	728	62,051	7, 19,			<no description=""></no>
27.38	2	728	106,350	4, 6, 17,			<no description=""></no>
14.97	2	730	60,787	21, 22, 23,			<no description=""></no>
42.12	2	728	167,137	24, 26, 27			Design Point B
	1.927 12.78 12.78 10.989 10.989 10.907 10.167 10.167 10.167 10.167 10.169 10.27 10.28 10.29 10.32 10.32 10.32 10.33 10.3	1.927 2 12.78 2 12.78 2 12.78 2 12.78 2 12.78 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 12.75 2 13.75 2 14.97 2	sir 1.927 2 728 sir 12.78 2 730 sir 0.989 2 728 sir 5.575 2 728 sir 3.607 2 730 sir 0.167 2 790 sir 6.332 2 732 e 15.96 2 728 e 27.38 2 728 e 14.97 2 730	sir 1.927 2 728 5,568 sir 12.78 2 730 48,298 sir 0.989 2 728 3,300 sir 5.575 2 728 20,252 sir 3.607 2 730 12,398 sir 0.167 2 790 1,564 sir 6.332 2 732 26,572 e 15.96 2 728 62,051 e 27.38 2 728 106,350 e 14.97 2 730 60,787	1.927 2 728 5,568 5 5ir 12.78 2 730 48,298 8 6ir 0.989 2 728 3,300 9 6ir 5.575 2 728 20,252 10 70ir 3.607 2 730 12,398 11 10ir 0.167 2 790 1,564 12 10ir 6.332 2 732 26,572 13 12 728 62,051 7, 19, 15.96 2 728 62,051 7, 19, 15.96 2 728 106,350 4, 6, 17, 18, 20, 25 21, 22, 23, 24,	sir 1.927 2 728 5,568 5 145.20 sir 12.78 2 730 48,298 8 139.20 sir 0.989 2 728 3,300 9 138.34 sir 5.575 2 728 20,252 10 137.41 sir 3.607 2 730 12,398 11 136.47 sir 0.167 2 790 1,564 12 137.46 sir 6.332 2 732 26,572 13 135.75 se 15.96 2 728 62,051 7, 19, se 27.38 2 728 106,350 4, 6, 17, se 14.97 2 730 60,787 21, 22, 23, se 14.97 2 730 60,787 21, 22, 23,	bir 1.927 2 728 5,568 5 145.20 3,232 bir 12.78 2 730 48,298 8 139.20 4,033 bir 0.989 2 728 3,300 9 138.34 955 bir 5.575 2 728 20,252 10 137.41 3,146 bir 3.607 2 730 12,398 11 136.47 8,476 bir 0.167 2 790 1,564 12 137.46 3,653 bir 6.332 2 732 26,572 13 135.75 2,492 e 15.96 2 728 62,051 7, 19, e 27.38 2 728 106,350 4, 6, 17, e 14.97 2 730 60,787 21, 22, 23,

J:\F\F0173 Fuller\001 64 Danbury Rd\CalculatiRest\\@ndPerrivate5\Proparsed-HydrafiloTww.egsplray, 12 / 5 / 2023

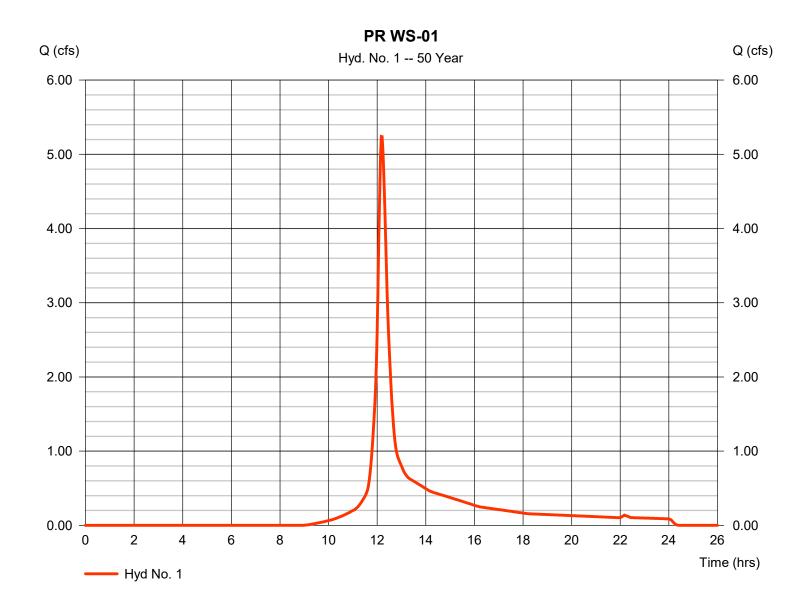
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 1

PR WS-01

Hydrograph type = SCS Runoff Peak discharge = 5.239 cfsStorm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 21,499 cuft Drainage area Curve number = 1.721 ac= 66 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.50 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



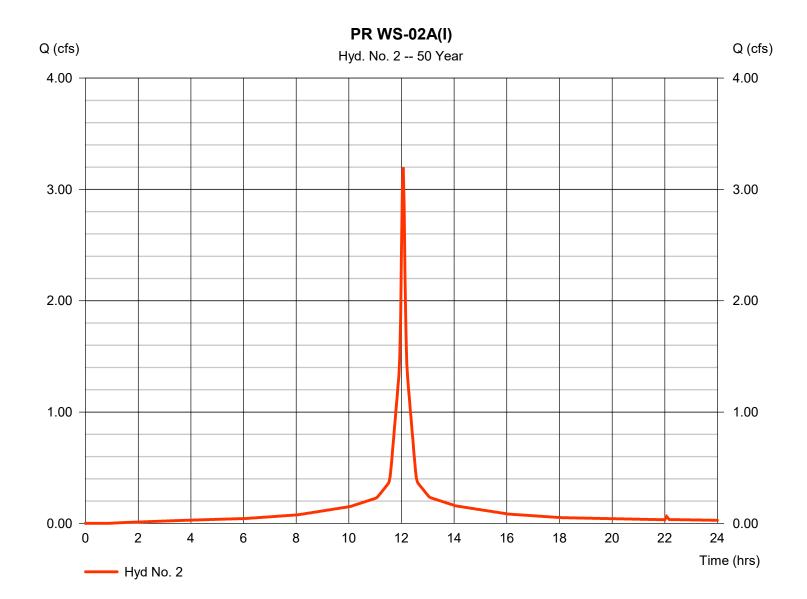
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 2

PR WS-02A(I)

Hydrograph type = SCS Runoff Peak discharge = 3.199 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 10,990 cuftDrainage area Curve number = 97 = 0.458 acHydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



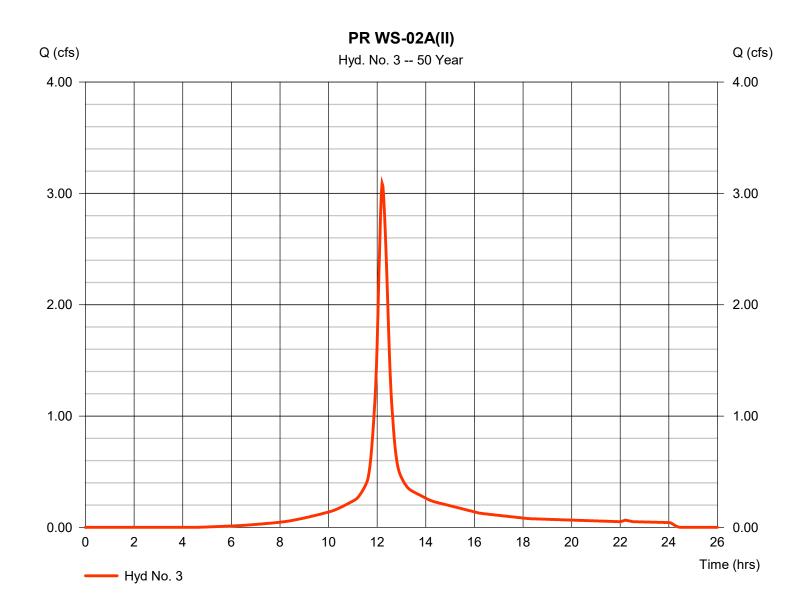
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 3

PRWS-02A(II)

Hydrograph type = SCS Runoff Peak discharge = 3.089 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 13,997 cuft Drainage area Curve number = 0.683 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.10 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



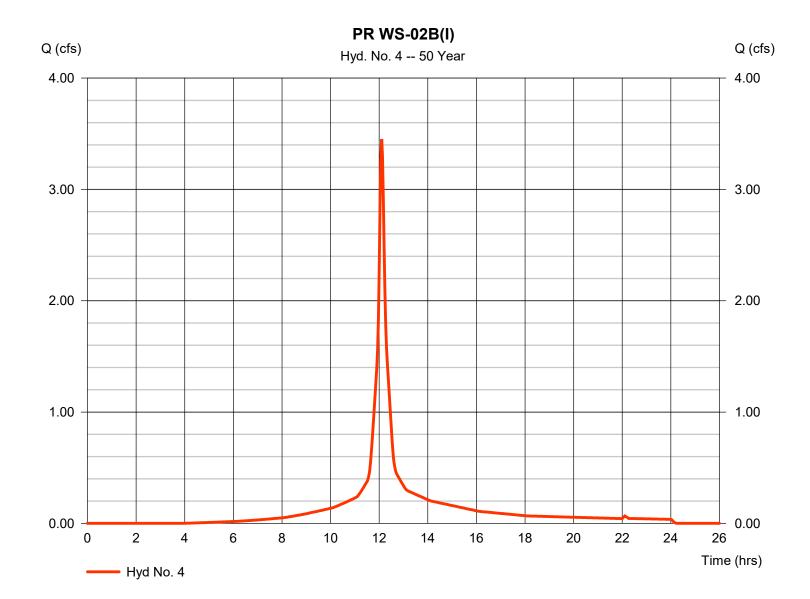
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 4

PR WS-02B(I)

Hydrograph type = SCS Runoff Peak discharge = 3.451 cfsStorm frequency = 50 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 12,280 cuftDrainage area = 0.576 acCurve number = 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 7.40 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



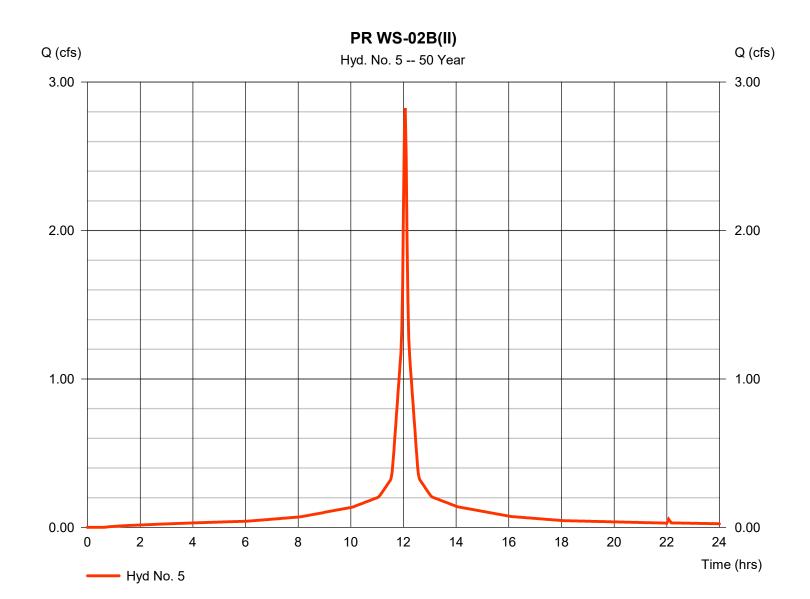
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 5

PRWS-02B(II)

Hydrograph type = SCS Runoff Peak discharge = 2.824 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 9,834 cuft Drainage area Curve number = 0.403 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



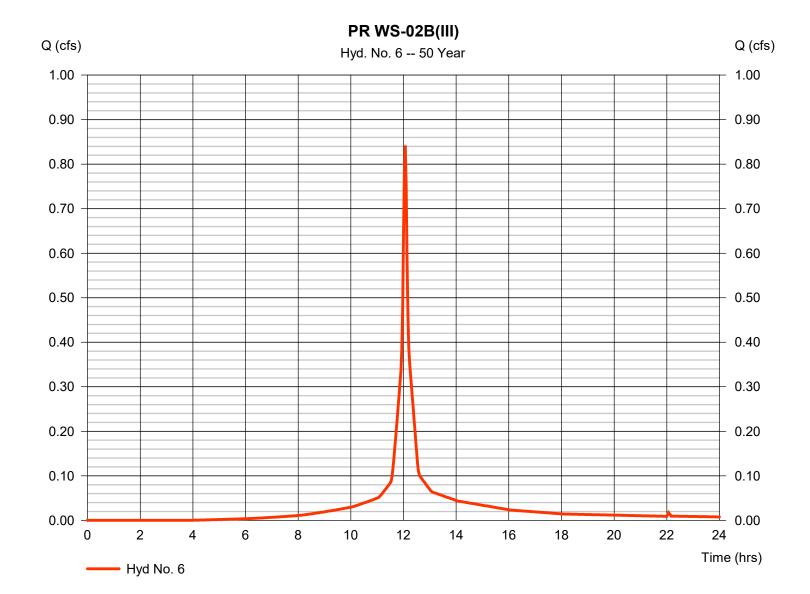
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 6

PR WS-02B(III)

Hydrograph type = SCS Runoff Peak discharge = 0.842 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,640 cuftDrainage area Curve number = 0.132 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



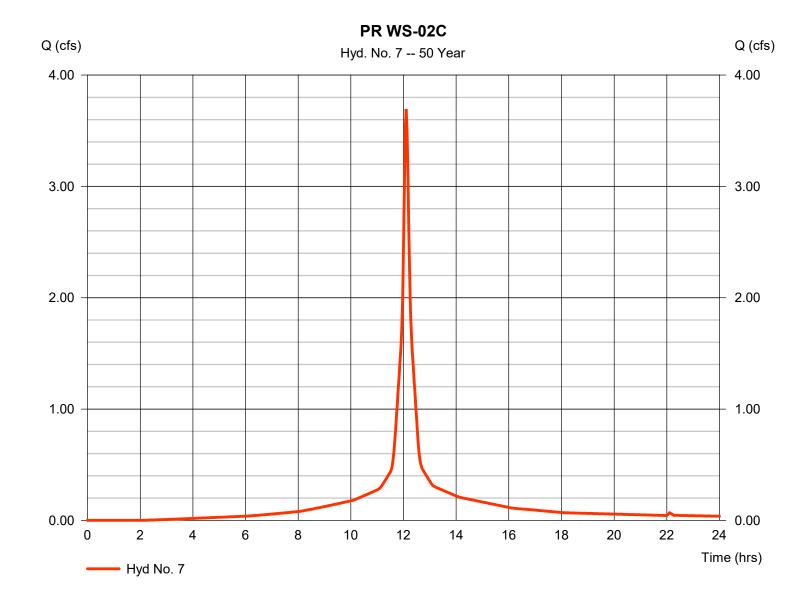
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 7

PRWS-02C

Hydrograph type = SCS Runoff Peak discharge = 3.695 cfsStorm frequency = 50 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 13,753 cuft Drainage area = 0.576 acCurve number = 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



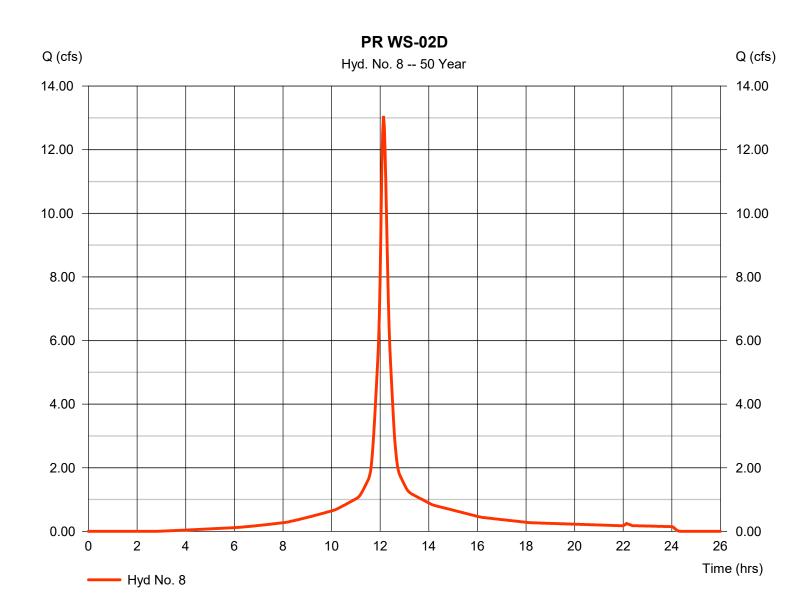
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 8

PRWS-02D

Hydrograph type = SCS Runoff Peak discharge = 13.06 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ = 53,326 cuft Time interval = 2 min Hyd. volume Drainage area = 2.246 acCurve number = 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



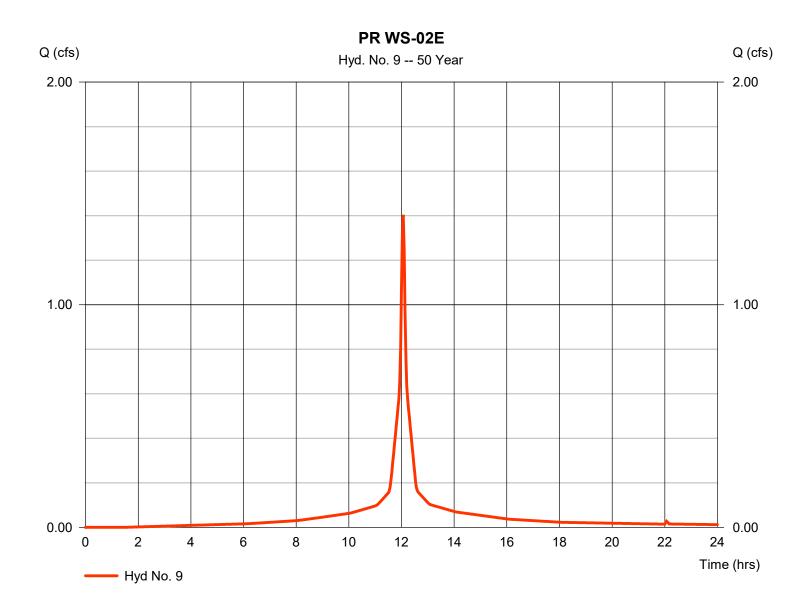
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 9

PRWS-02E

= SCS Runoff Hydrograph type Peak discharge = 1.404 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,707 cuftDrainage area = 0.203 acCurve number = 95 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



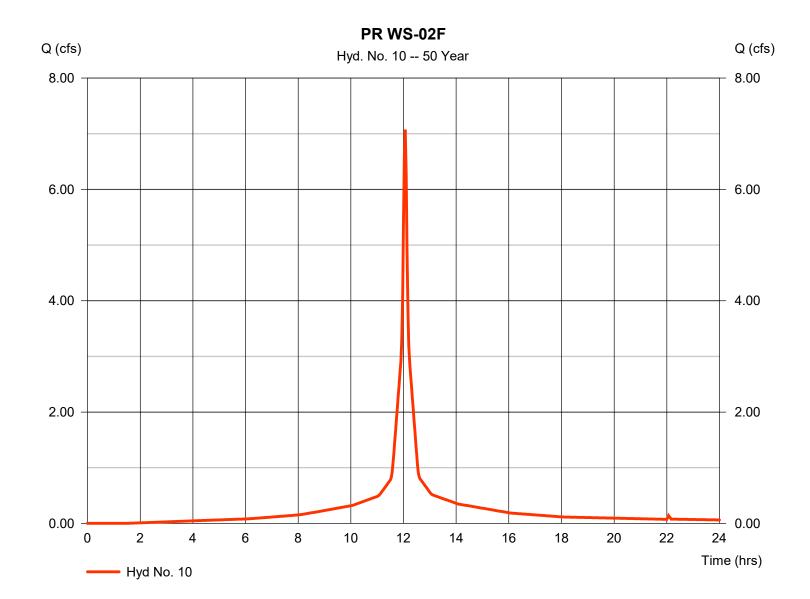
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 10

PR WS-02F

Hydrograph type = SCS Runoff Peak discharge = 7.074 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 23,722 cuft Drainage area Curve number = 1.023 ac= 95 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



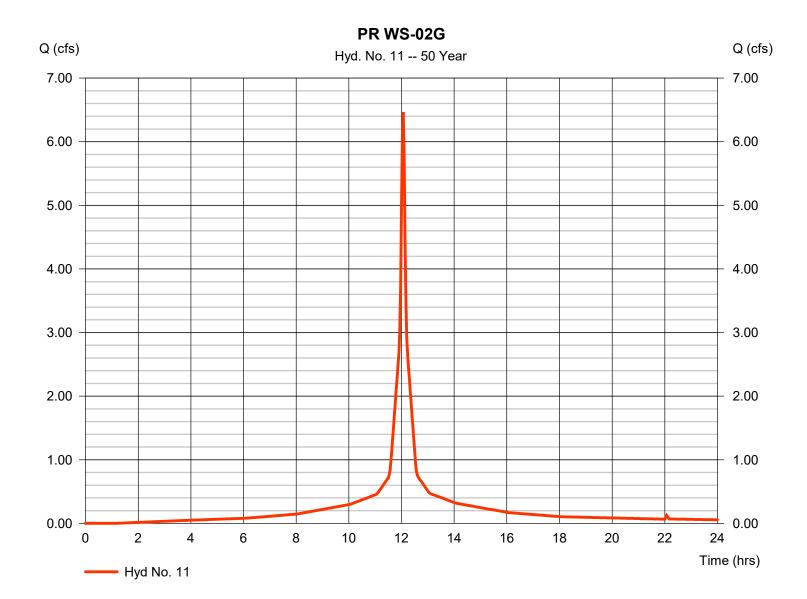
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 11

PRWS-02G

Hydrograph type = SCS Runoff Peak discharge = 6.467 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 21,940 cuftDrainage area Curve number = 0.930 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

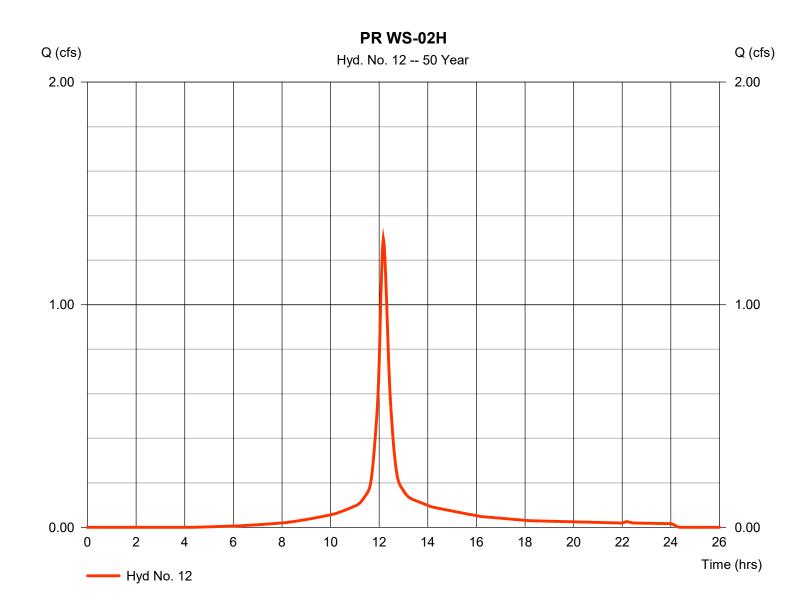
Tuesday, 12 / 5 / 2023

Hyd. No. 12

PRWS-02H

= SCS Runoff Hydrograph type Peak discharge = 1.296 cfsStorm frequency = 50 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 5,444 cuftDrainage area = 0.267 acCurve number = 86 Basin Slope = 0.0 %Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 13.80 min
Total precip. = 7.41 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484



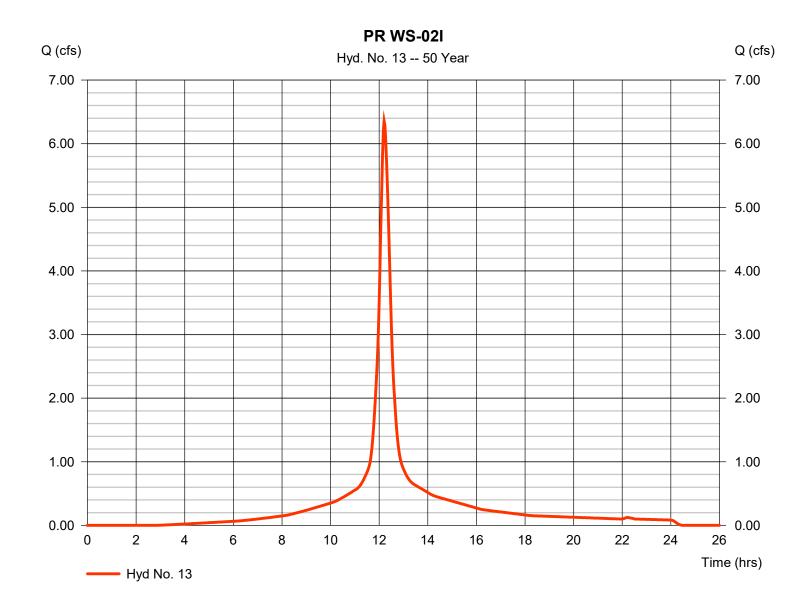
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 13

PR WS-02I

Hydrograph type = SCS Runoff Peak discharge = 6.358 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 29.838 cuft Drainage area = 1.296 ac Curve number = 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

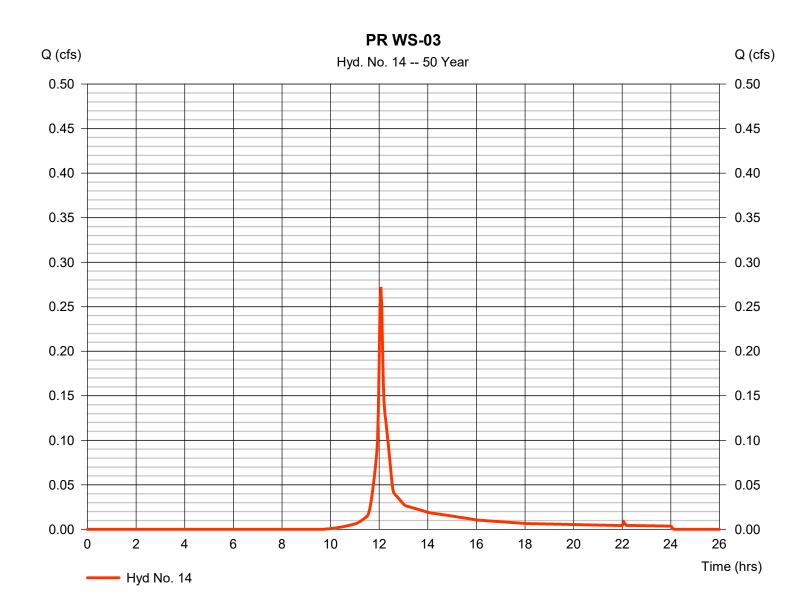


Tuesday, 12 / 5 / 2023

Hyd. No. 14

PR WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.272 cfsStorm frequency = 50 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 827 cuft Drainage area Curve number = 0.081 ac= 61 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.10 \, \text{min}$ = User Total precip. = 7.41 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



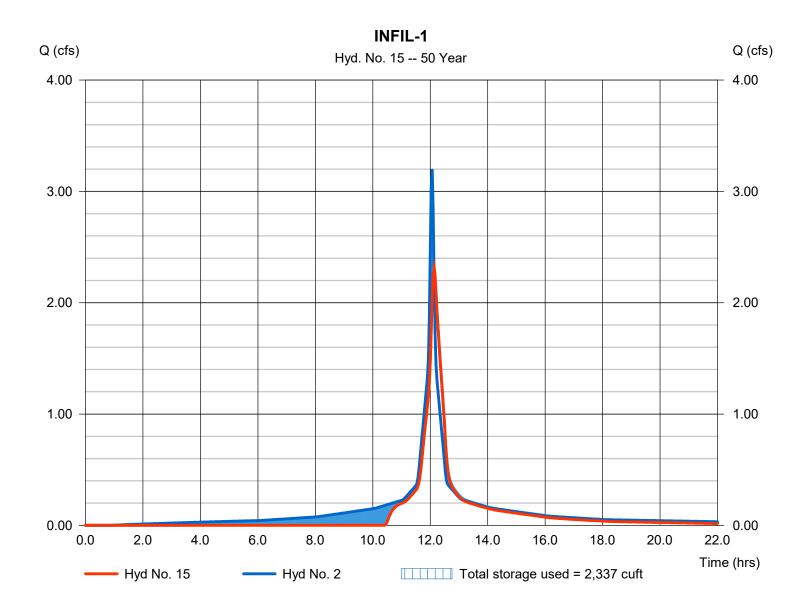
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 15

INFIL-1

Hydrograph type = Reservoir Peak discharge = 2.310 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 8,200 cuftInflow hyd. No. Max. Elevation = 2 - PR WS-02A(I)= 146.47 ftReservoir name = INFIL-1 Max. Storage = 2,337 cuft

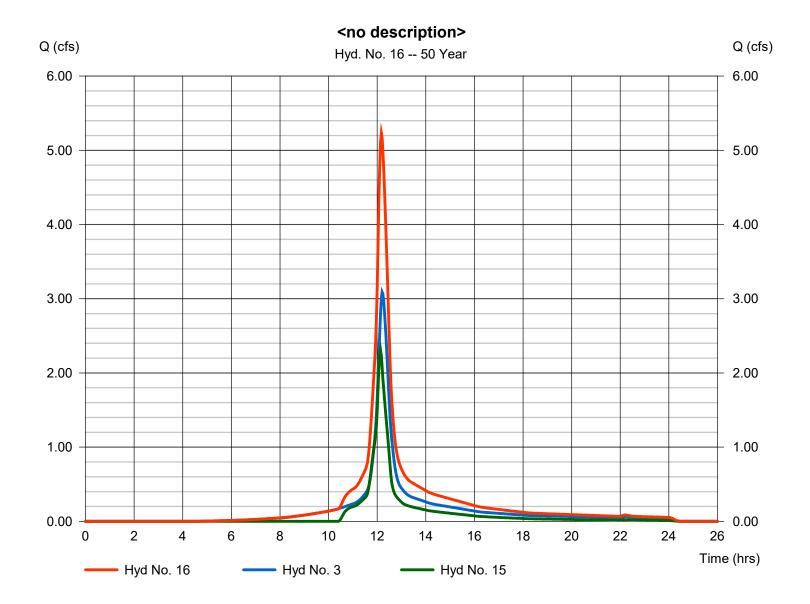


Tuesday, 12 / 5 / 2023

Hyd. No. 16

<no description>

Hydrograph type = Combine Peak discharge = 5.234 cfsTime to peak Storm frequency = 50 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 22,197 cuft Inflow hyds. Contrib. drain. area = 3, 15 = 0.683 ac



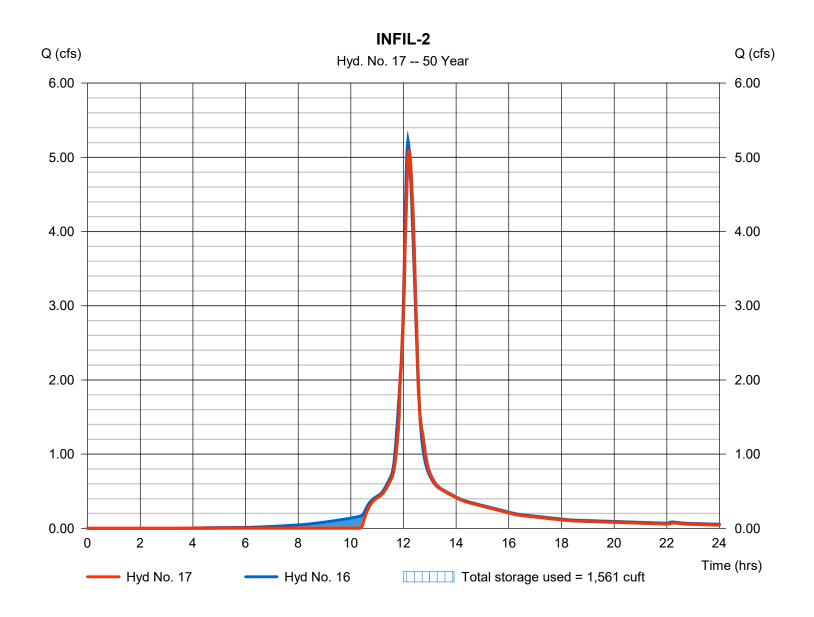
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 17

INFIL-2

Hydrograph type = Reservoir Peak discharge = 5.080 cfsStorm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 20,511 cuftMax. Elevation Inflow hyd. No. = 16 - <no description> = 137.80 ftReservoir name = INFIL-2 Max. Storage = 1,561 cuft



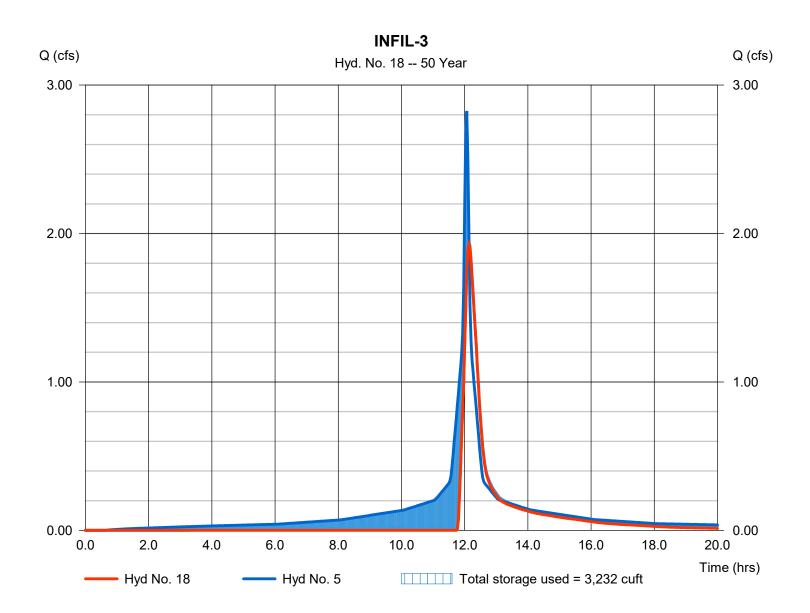
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 18

INFIL-3

Hydrograph type = Reservoir Peak discharge = 1.927 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 5,568 cuftInflow hyd. No. Max. Elevation = 5 - PR WS-02B(II)= 145.20 ftReservoir name = INFIL-3 Max. Storage = 3,232 cuft



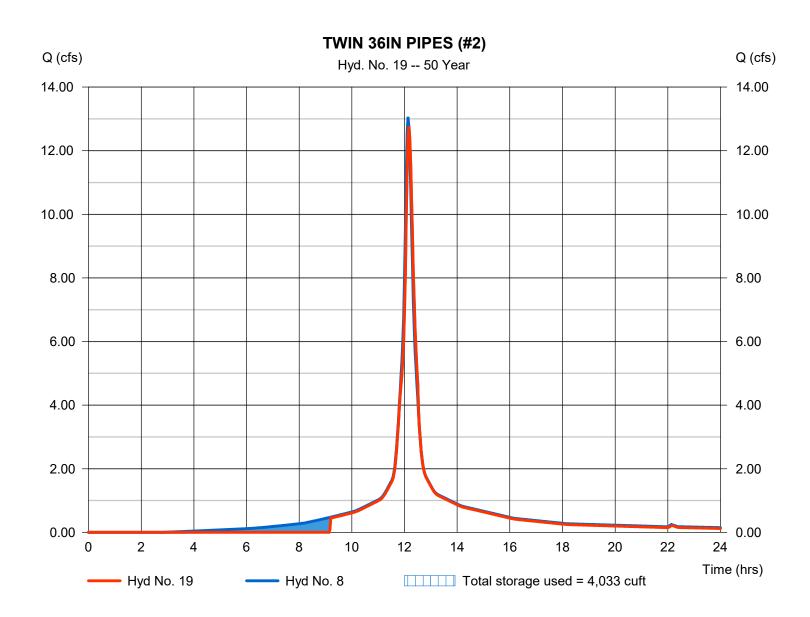
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 19

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 12.78 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 48,298 cuft Inflow hyd. No. Max. Elevation = 8 - PR WS-02D = 139.20 ft= Northern Twin 36IN Reservoir name Max. Storage = 4,033 cuft



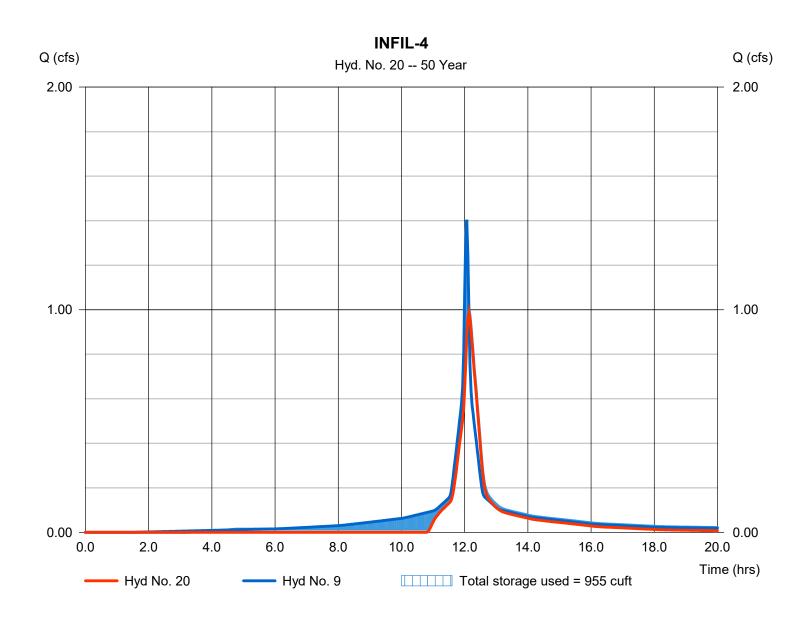
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 20

INFIL-4

Hydrograph type = Reservoir Peak discharge = 0.989 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 3,300 cuftInflow hyd. No. Max. Elevation = 9 - PR WS-02E = 138.34 ftReservoir name = INFIL-4 Max. Storage = 955 cuft



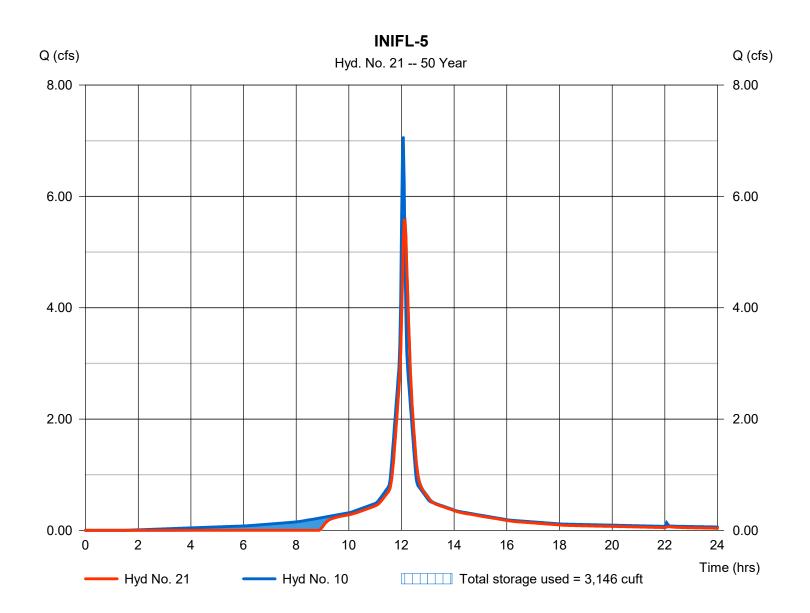
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 21

INIFL-5

Hydrograph type = Reservoir Peak discharge = 5.575 cfsStorm frequency = 50 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 20,252 cuft Inflow hyd. No. Max. Elevation = 137.41 ft= 10 - PR WS-02F Reservoir name = INIFL-5 Max. Storage = 3,146 cuft



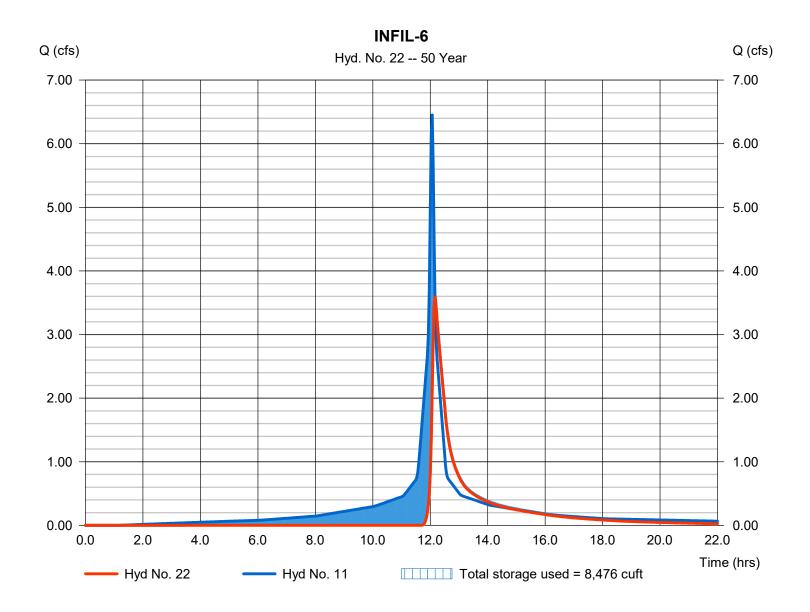
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 22

INFIL-6

Hydrograph type Peak discharge = 3.607 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 12,398 cuft Inflow hyd. No. Max. Elevation = 11 - PR WS-02G = 136.47 ftReservoir name = INFIL-6 Max. Storage = 8,476 cuft



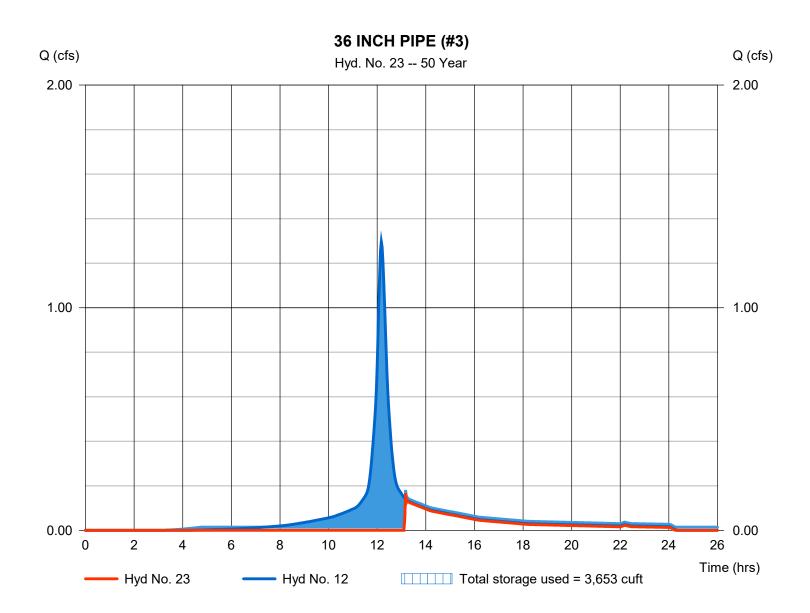
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 23

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 0.167 cfsStorm frequency = 50 yrsTime to peak $= 13.17 \, hrs$ Time interval = 2 min Hyd. volume = 1,564 cuft Max. Elevation Inflow hyd. No. = 12 - PR WS-02H = 137.46 ftReservoir name = 36IN - 3Max. Storage = 3,653 cuft



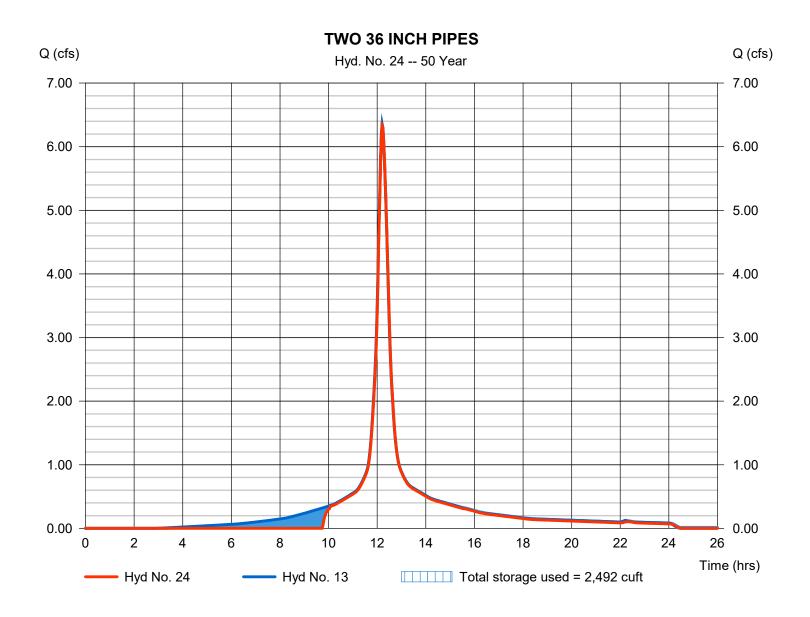
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 24

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 6.332 cfs= Reservoir Storm frequency = 50 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 26,572 cuft Inflow hyd. No. Max. Elevation = 13 - PR WS-02I $= 135.75 \, \text{ft}$ Reservoir name = TWIN 36IN Max. Storage = 2,492 cuft



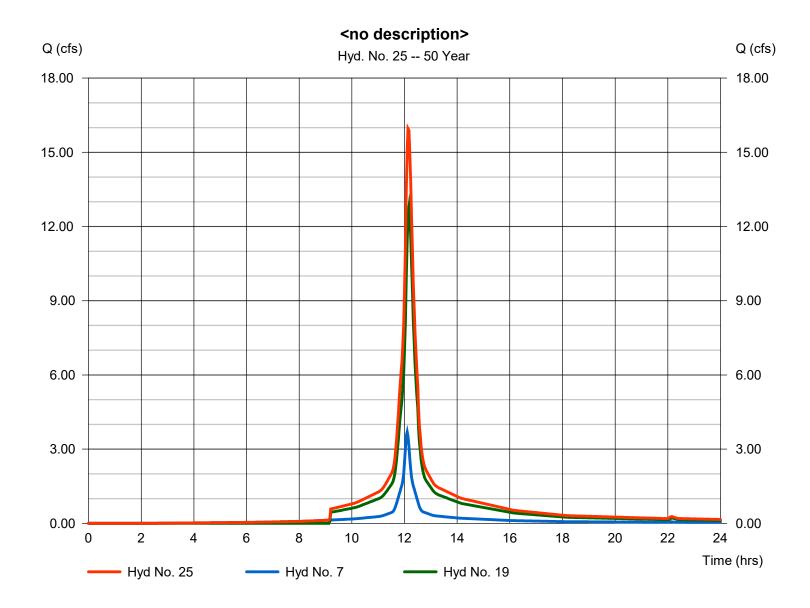
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 25

<no description>

Hydrograph type = Combine Peak discharge = 15.96 cfsStorm frequency Time to peak = 50 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 62,051 cuftInflow hyds. = 7, 19 = 0.576 acContrib. drain. area



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Tuesday, 12 / 5 / 2023

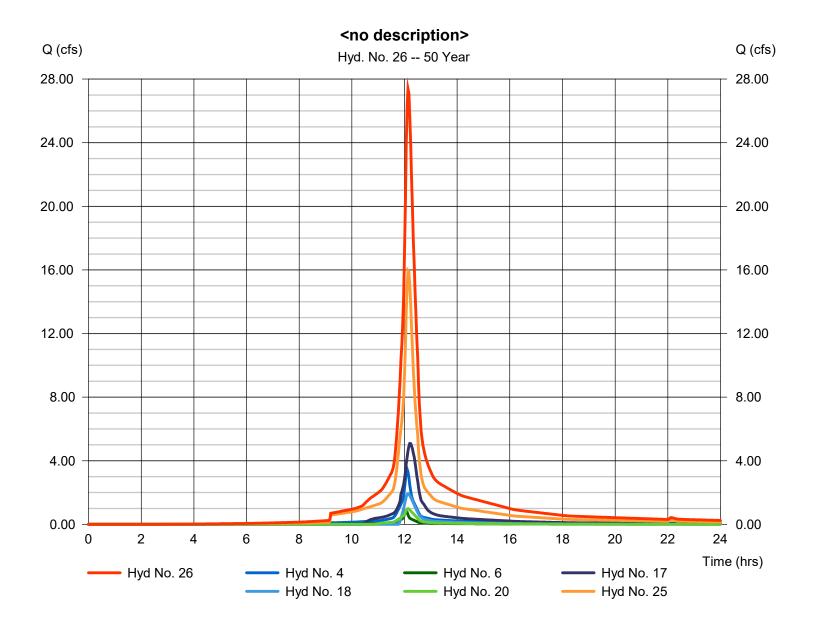
Hyd. No. 26

<no description>

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min

Inflow hyds. = 4, 6, 17, 18, 20, 25

Peak discharge = 27.38 cfs
Time to peak = 12.13 hrs
Hyd. volume = 106,350 cuft
Contrib. drain. area = 0.708 ac



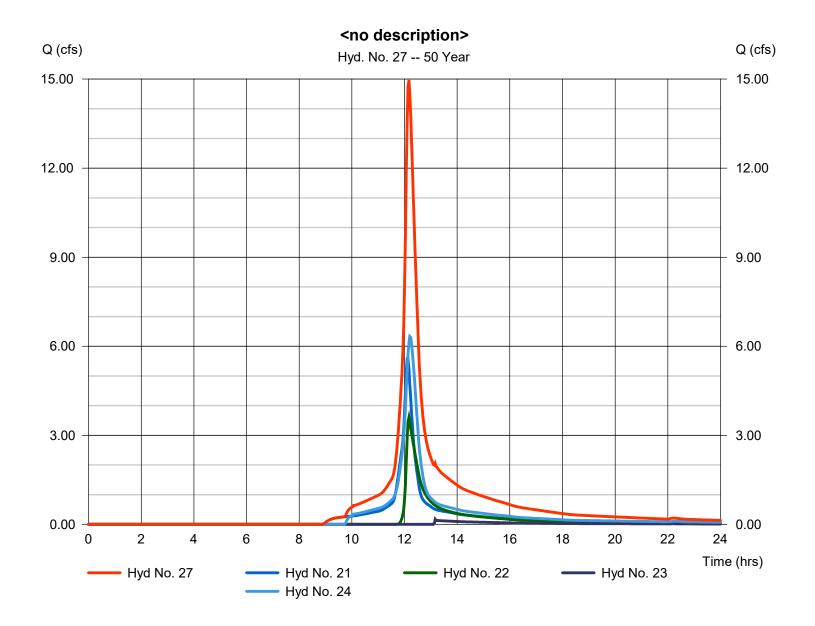
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 27

<no description>

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min Inflow hyds. = 21, 22, 23, 24 Peak discharge = 14.97 cfs
Time to peak = 12.17 hrs
Hyd. volume = 60,787 cuft
Contrib. drain. area = 0.000 ac



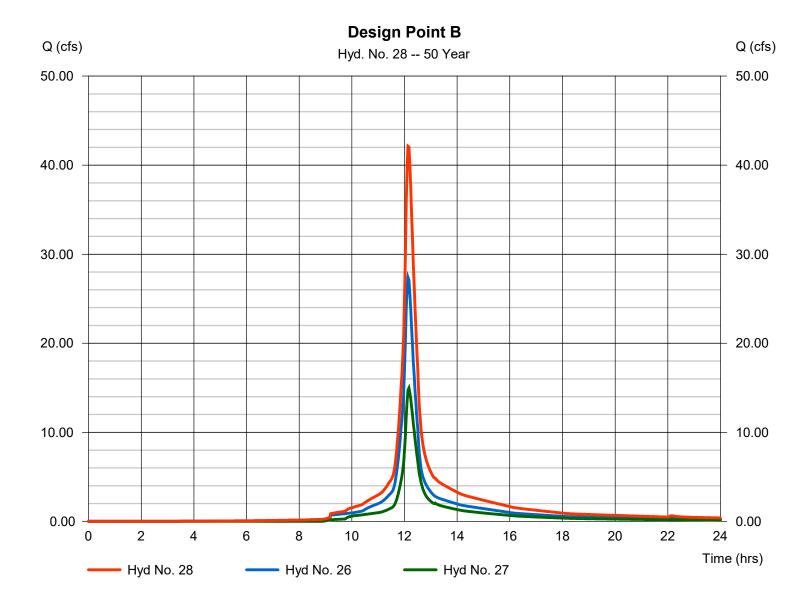
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 28

Design Point B

Hydrograph type = Combine Peak discharge = 42.12 cfsStorm frequency Time to peak = 50 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 167,137 cuft Inflow hyds. = 26, 27 Contrib. drain. area = 0.000 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

1 SC 2 SC 3 SC 4 SC 5 SC 6 SC 7 SC 8 SC	ydrograph type (origin) CS Runoff CS Runoff	Peak flow (cfs) 6.398 3.605 3.556 3.952 3.181	Time interval (min) 2 2 2 2	Time to Peak (min) 730 724 732	Hyd. volume (cuft) 26,117 12,438 16,219	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description PR WS-01 PR WS-02A(I)
2 SC 3 SC 4 SC 5 SC 6 SC 7 SC 8 SC	CS Runoff CS Runoff CS Runoff CS Runoff CS Runoff	3.605 3.556 3.952	2 2	724	12,438				
3 SC 4 SC 5 SC 6 SC 7 SC 8 SC	CS Runoff CS Runoff CS Runoff CS Runoff	3.556 3.952	2						PR WS-02A(I)
4 SC 5 SC 6 SC 7 SC 8 SC	CS Runoff CS Runoff CS Runoff	3.952		732	16,219				
5 SC 6 SC 7 SC 8 SC	CS Runoff CS Runoff		2						PR WS-02A(II)
6 SC 7 SC 8 SC	CS Runoff	3.181		726	14,171				PR WS-02B(I)
7 SC 8 SC			2	724	11,109				PR WS-02B(II)
8 SC	CS Runoff	0.964	2	724	3,046				PR WS-02B(III)
		4.184	2	726	15,682				PR WS-02C
9 SC	CS Runoff	14.84	2	728	61,043				PR WS-02D
	CS Runoff	1.585	2	724	5,347				PR WS-02E
10 SC	CS Runoff	7.986	2	724	26,946				PR WS-02F
11 SC	CS Runoff	7.294	2	724	24,876				PR WS-02G
12 SC	CS Runoff	1.488	2	730	6,295				PR WS-02H
13 SC	CS Runoff	7.225	2	732	34,156				PR WS-02I
14 SC	CS Runoff	0.339	2	724	1,022				PR WS-03
15 Re	eservoir	2.580	2	728	9,629	2	146.94	2,479	INFIL-1
16 Co	ombine	5.963	2	730	25,847	3, 15			<no description=""></no>
17 Re	eservoir	5.776	2	734	24,138	16	138.33	1,674	INFIL-2
18 Re	eservoir	2.266	2	728	6,804	5	145.49	3,366	INFIL-3
19 Re	eservoir	14.56	2	730	55,977	8	139.24	4,189	TWIN 36IN PIPES (#2)
20 Re	eservoir	1.107	2	728	3,919	9	138.62	1,020	INFIL-4
21 Re	eservoir	6.323	2	726	23,447	10	137.92	3,376	INIFL-5
22 Re	eservoir	4.990	2	728	15,158	11	136.84	8,905	INFIL-6
23 Re	eservoir	0.704	2	752	2,409	12	137.47	3,670	36 INCH PIPE (#3)
24 Re	eservoir	7.197	2	732	30,870	13	135.76	2,510	TWO 36 INCH PIPES
25 Co	ombine	18.23	2	728	71,659	7, 19,			<no description=""></no>
26 Co	ombine	31.28	2	728	123,737	4, 6, 17,			<no description=""></no>
27 Co	ombine	17.81	2	728	71,885	18, 20, 25 21, 22, 23,			<no description=""></no>
28 Co	ombine	49.08	2	728	195,622	24, 26, 27			Design Point B

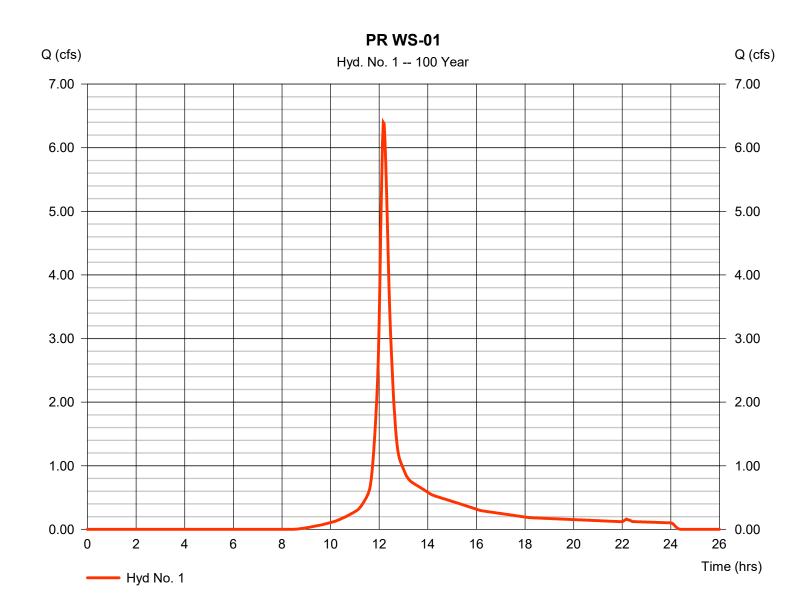
J:\F\F0173 Fuller\001 64 Danbury Rd\CalculatiRest\\@ndPerrivate/f\P00\feased-Hydra/floTwuespolvay, 12 / 5 / 2023

Tuesday, 12 / 5 / 2023

Hyd. No. 1

PRWS-01

Hydrograph type = SCS Runoff Peak discharge = 6.398 cfsStorm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 26,117 cuft Drainage area = 1.721 acCurve number = 66 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.50 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

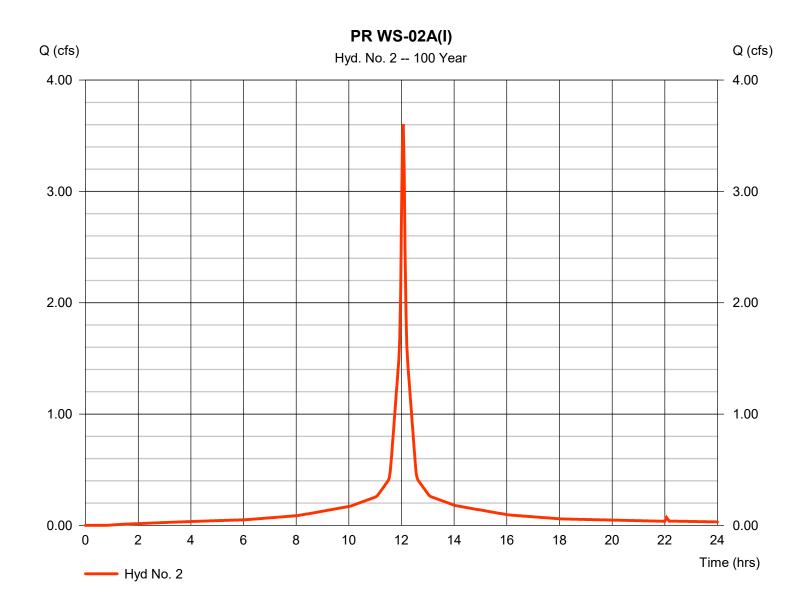


Tuesday, 12 / 5 / 2023

Hyd. No. 2

PR WS-02A(I)

Hydrograph type = SCS Runoff Peak discharge = 3.605 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 12,438 cuft Drainage area Curve number = 0.458 ac= 97 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



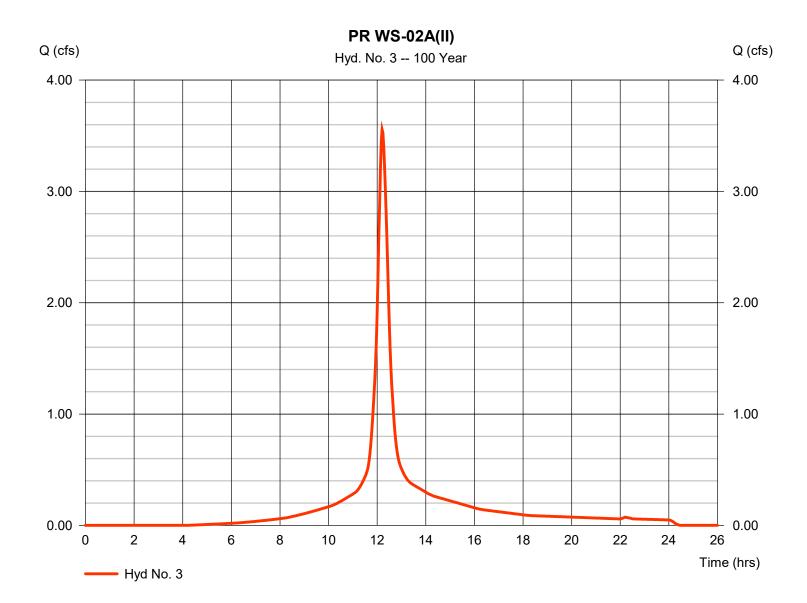
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Tuesday, 12 / 5 / 2023

Hyd. No. 3

PRWS-02A(II)

Hydrograph type = SCS Runoff Peak discharge = 3.556 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 16,219 cuftDrainage area Curve number = 0.683 ac= 85 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.10 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

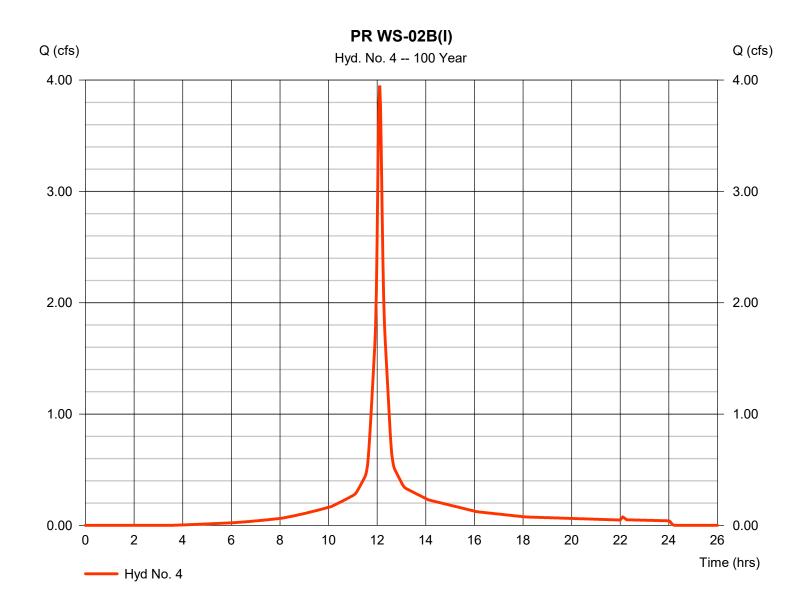


Tuesday, 12 / 5 / 2023

Hyd. No. 4

PR WS-02B(I)

Hydrograph type = SCS Runoff Peak discharge = 3.952 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 14,171 cuft Drainage area Curve number = 0.576 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 7.40 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

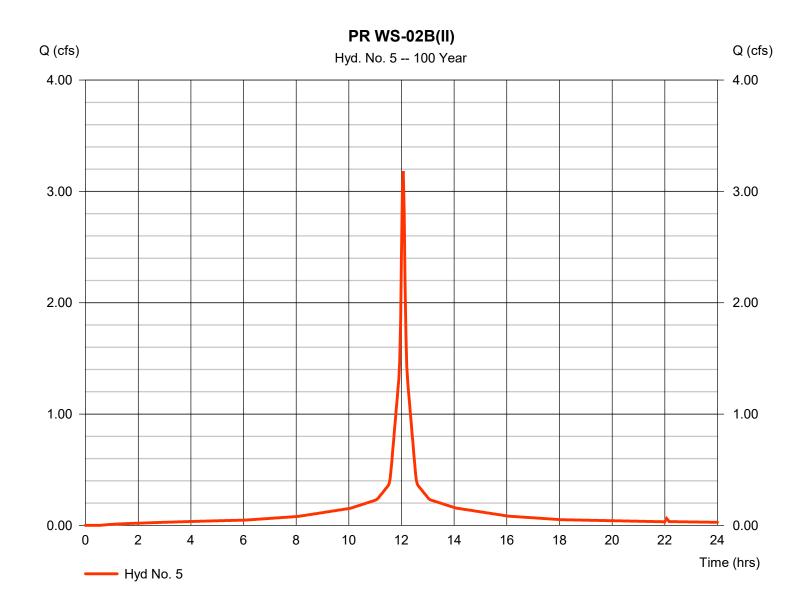


Tuesday, 12 / 5 / 2023

Hyd. No. 5

PRWS-02B(II)

Hydrograph type = SCS Runoff Peak discharge = 3.181 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 11,109 cuft Drainage area Curve number = 0.403 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

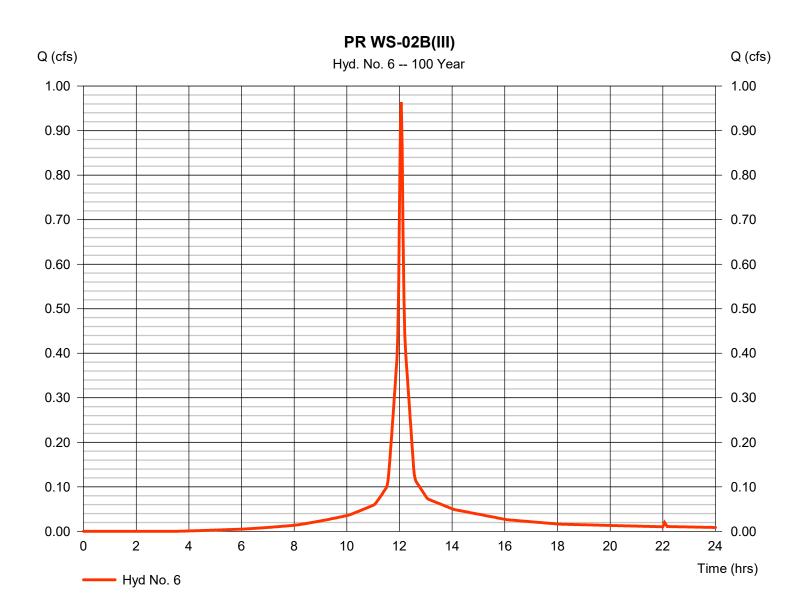


Tuesday, 12 / 5 / 2023

Hyd. No. 6

PR WS-02B(III)

Hydrograph type = SCS Runoff Peak discharge = 0.964 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,046 cuftDrainage area Curve number = 0.132 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

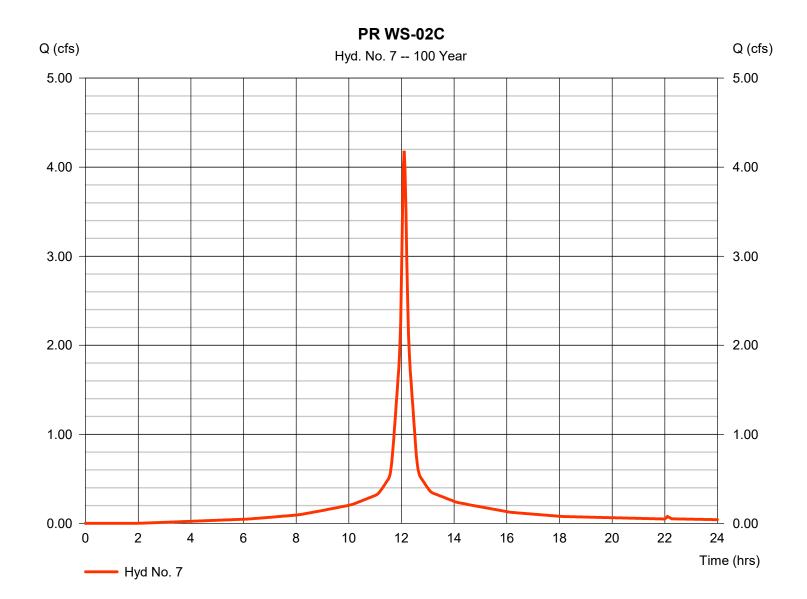


Tuesday, 12 / 5 / 2023

Hyd. No. 7

PRWS-02C

Hydrograph type = SCS Runoff Peak discharge = 4.184 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 15,682 cuft Drainage area Curve number = 0.576 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 9.40 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



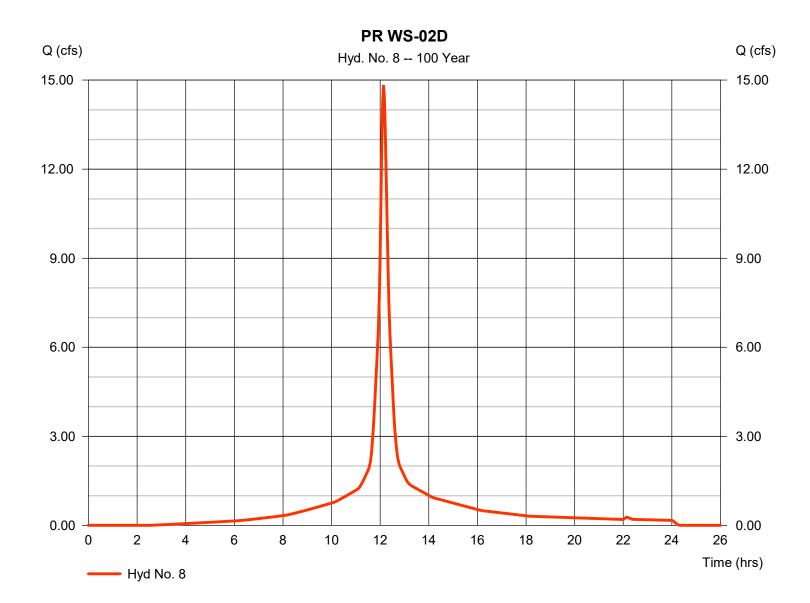
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Tuesday, 12 / 5 / 2023

Hyd. No. 8

PRWS-02D

Hydrograph type = SCS Runoff Peak discharge = 14.84 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 61,043 cuft Drainage area = 2.246 acCurve number = 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 11.10 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



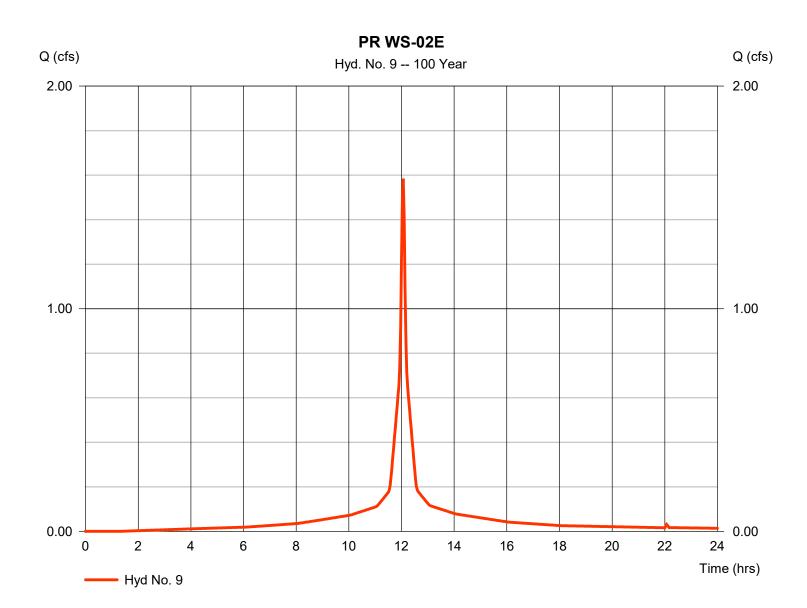
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 9

PRWS-02E

= SCS Runoff Hydrograph type Peak discharge = 1.585 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 5,347 cuftDrainage area = 0.203 acCurve number = 95 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

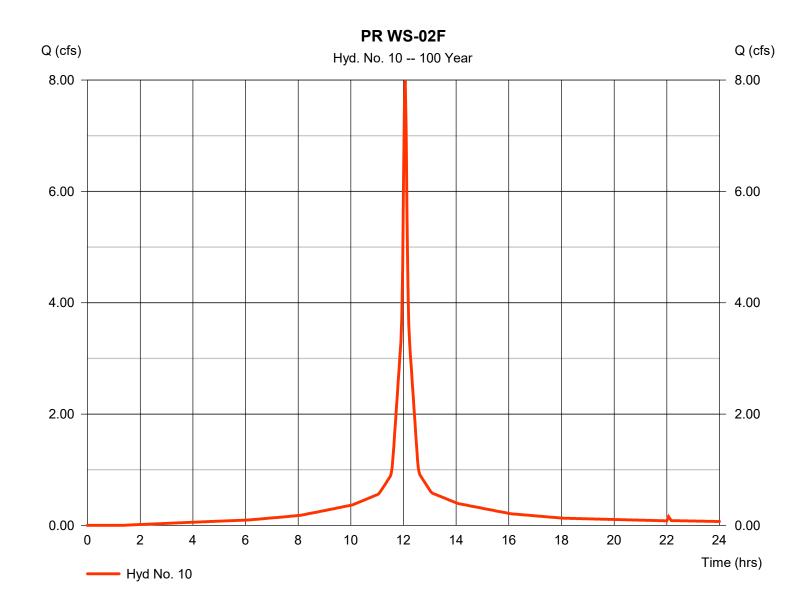


Tuesday, 12 / 5 / 2023

Hyd. No. 10

PR WS-02F

Hydrograph type = SCS Runoff Peak discharge = 7.986 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 26,946 cuft Drainage area Curve number = 1.023 ac= 95 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

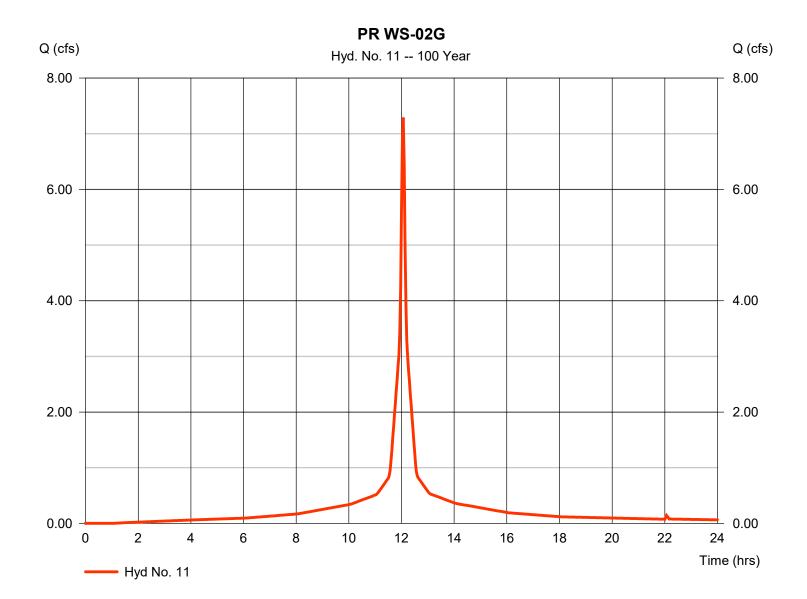


Tuesday, 12 / 5 / 2023

Hyd. No. 11

PRWS-02G

Hydrograph type = SCS Runoff Peak discharge = 7.294 cfsStorm frequency = 100 yrsTime to peak $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 24,876 cuft Drainage area Curve number = 0.930 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 5.00 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

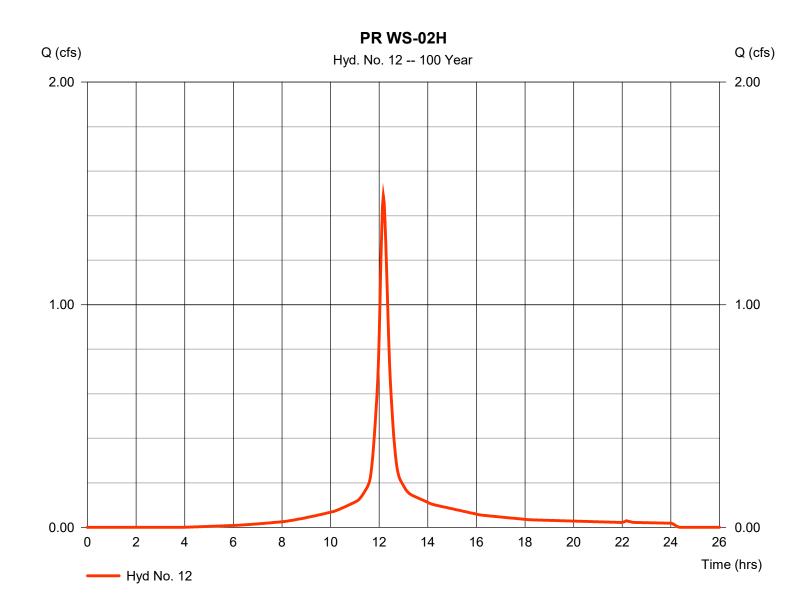


Tuesday, 12 / 5 / 2023

Hyd. No. 12

PRWS-02H

Hydrograph type = SCS Runoff Peak discharge = 1.488 cfsStorm frequency = 100 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 6,295 cuft Drainage area = 0.267 acCurve number = 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.80 min = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



Tuesday, 12 / 5 / 2023

= 7.225 cfs

 $= 12.20 \, hrs$

= 91 = 0 ft

= 34,156 cuft

= 18.60 min

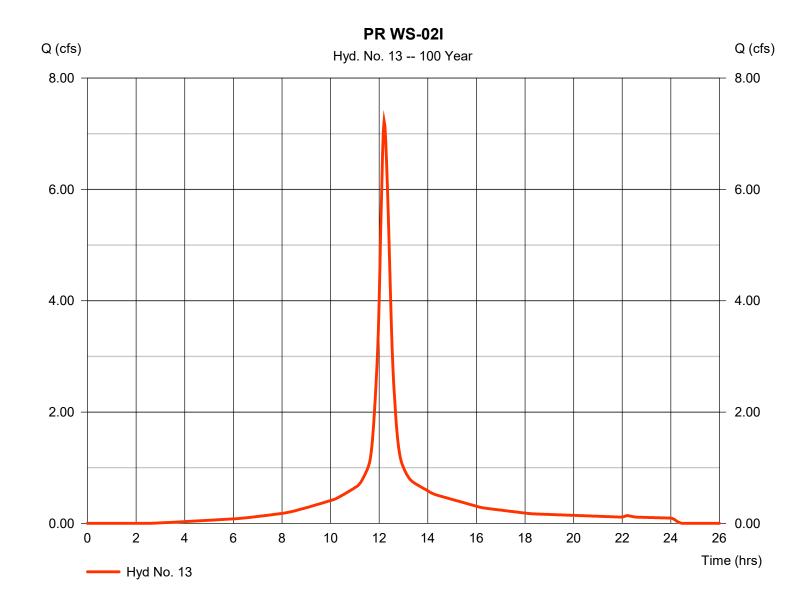
= Type III

= 484

Hyd. No. 13

PR WS-02I

Hydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak Time interval = 2 min Hyd. volume Drainage area = 1.296 ac Curve number Basin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = User Total precip. = 8.34 inDistribution Storm duration = 24 hrs Shape factor

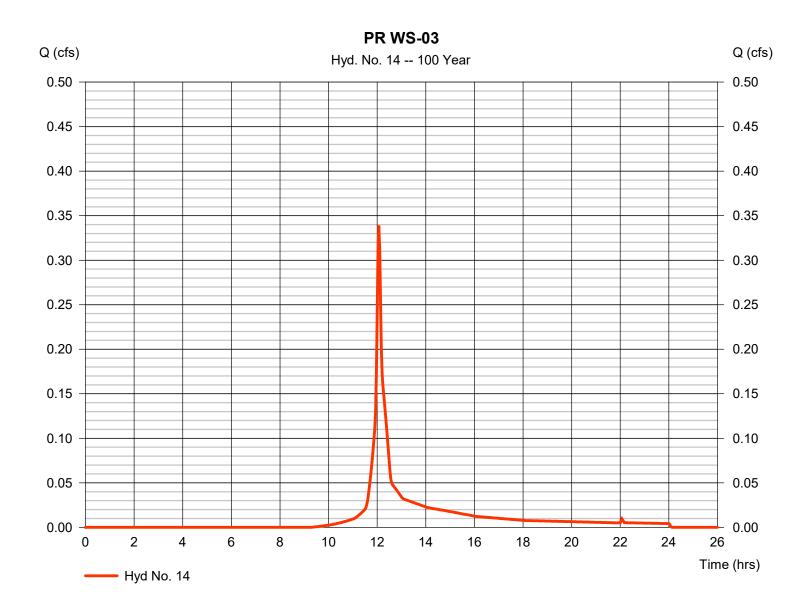


Tuesday, 12 / 5 / 2023

Hyd. No. 14

PR WS-03

Hydrograph type = SCS Runoff Peak discharge = 0.339 cfsStorm frequency = 100 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 1,022 cuft Drainage area Curve number = 61 = 0.081 acHydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.10 \, \text{min}$ = User Total precip. = 8.34 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



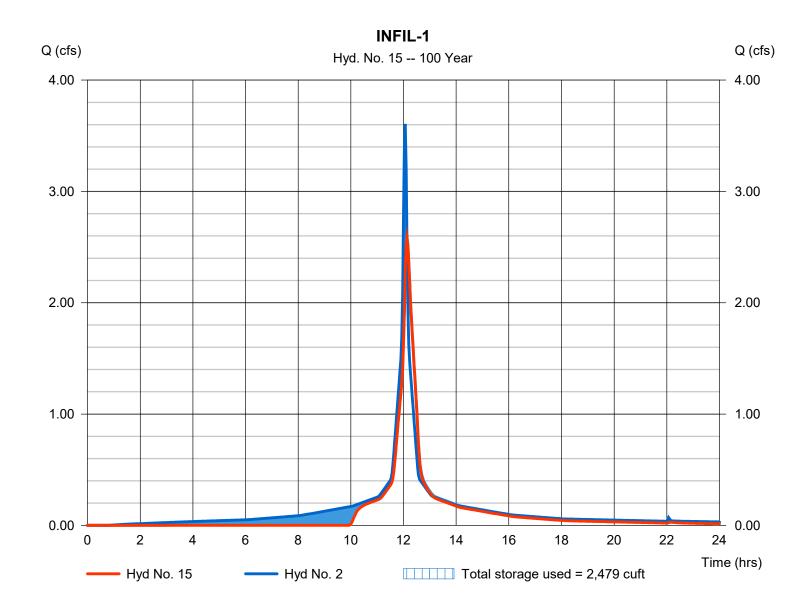
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Tuesday, 12 / 5 / 2023

Hyd. No. 15

INFIL-1

Hydrograph type = Reservoir Peak discharge = 2.580 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 9,629 cuftInflow hyd. No. Max. Elevation = 2 - PR WS-02A(I)= 146.94 ftReservoir name = INFIL-1 Max. Storage = 2,479 cuft



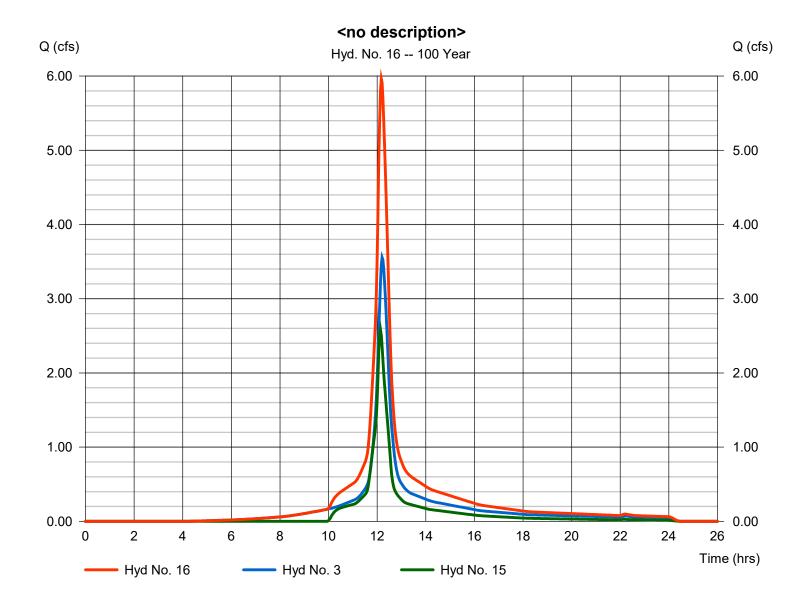
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 16

<no description>

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min Inflow hyds. = 3, 15 Peak discharge = 5.963 cfs
Time to peak = 12.17 hrs
Hyd. volume = 25,847 cuft
Contrib. drain. area = 0.683 ac



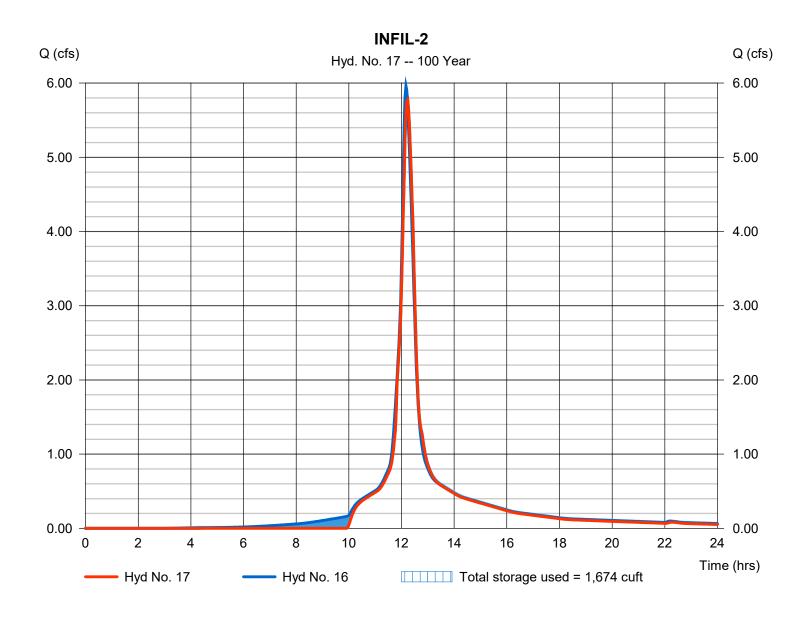
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 17

INFIL-2

Hydrograph type Peak discharge = 5.776 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 24,138 cuft Max. Elevation Inflow hyd. No. = 16 - <no description> = 138.33 ftReservoir name = INFIL-2 Max. Storage = 1,674 cuft



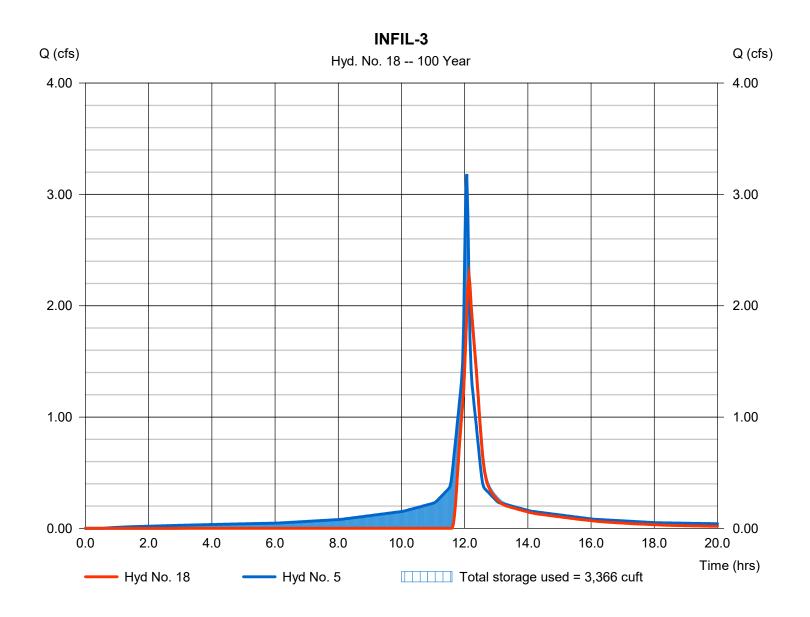
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 18

INFIL-3

Hydrograph type = Reservoir Peak discharge = 2.266 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 6.804 cuftInflow hyd. No. Max. Elevation = 5 - PR WS-02B(II)= 145.49 ftReservoir name = INFIL-3 Max. Storage = 3,366 cuft



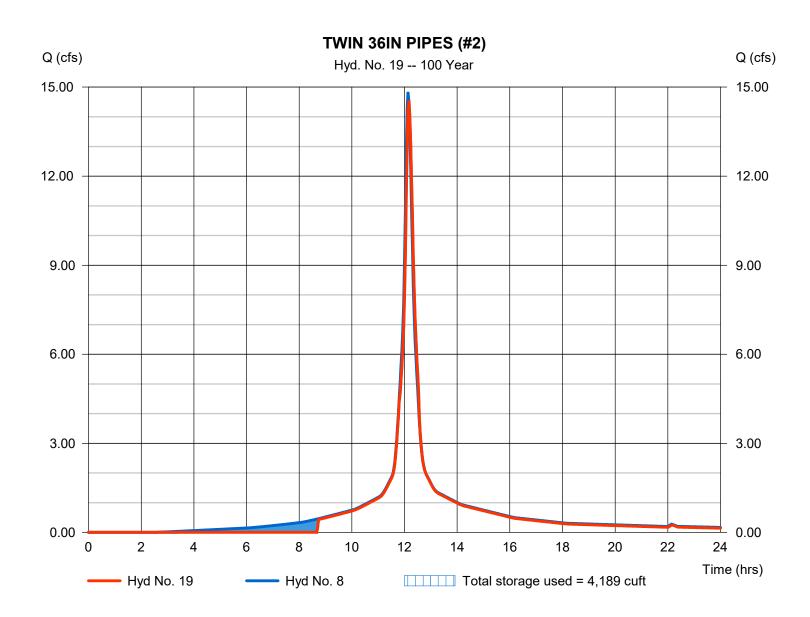
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 19

TWIN 36IN PIPES (#2)

Hydrograph type Peak discharge = 14.56 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 55,977 cuftInflow hyd. No. Max. Elevation = 8 - PR WS-02D = 139.24 ftReservoir name = Northern Twin 36IN Max. Storage = 4,189 cuft



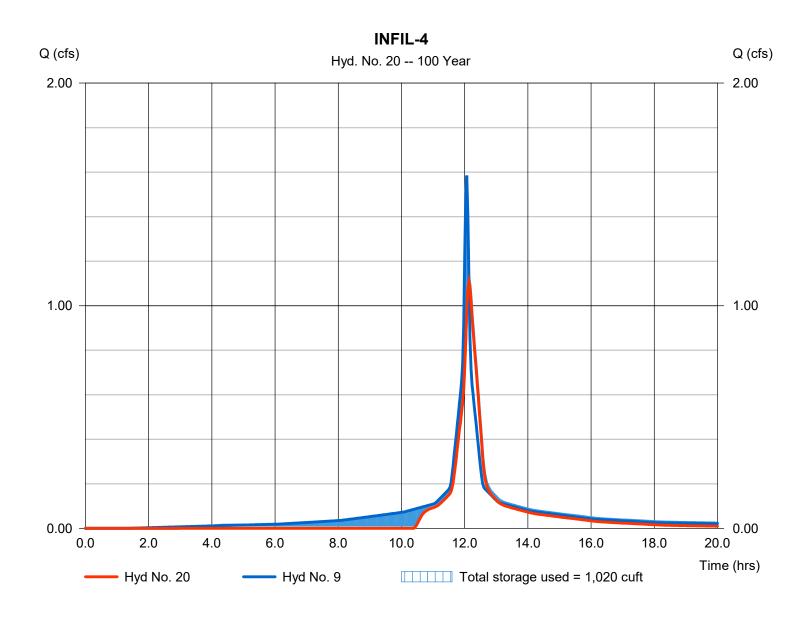
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 20

INFIL-4

Hydrograph type = Reservoir Peak discharge = 1.107 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 3,919 cuftInflow hyd. No. Max. Elevation = 9 - PR WS-02E = 138.62 ftReservoir name = INFIL-4 Max. Storage = 1,020 cuft



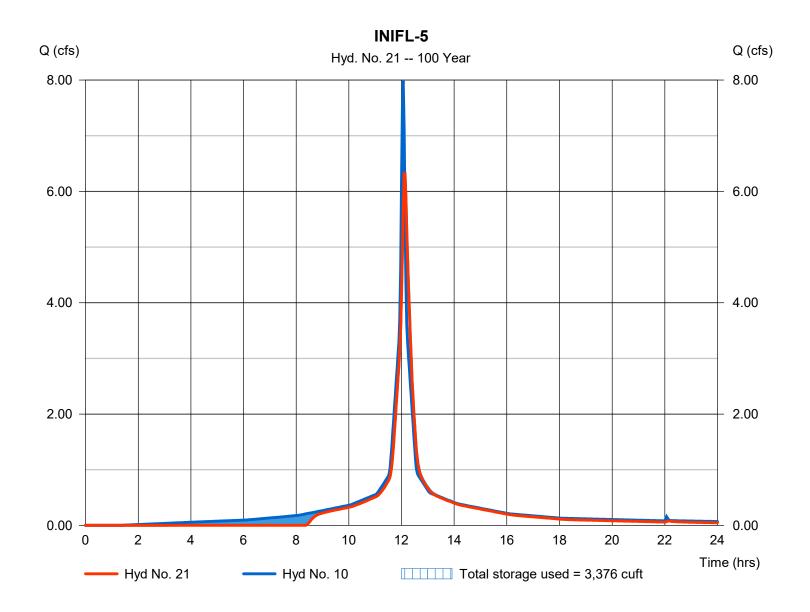
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 21

INIFL-5

Hydrograph type = Reservoir Peak discharge = 6.323 cfsStorm frequency = 100 yrsTime to peak $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 23,447 cuft Inflow hyd. No. Max. Elevation = 137.92 ft= 10 - PR WS-02F Reservoir name = INIFL-5 Max. Storage = 3,376 cuft



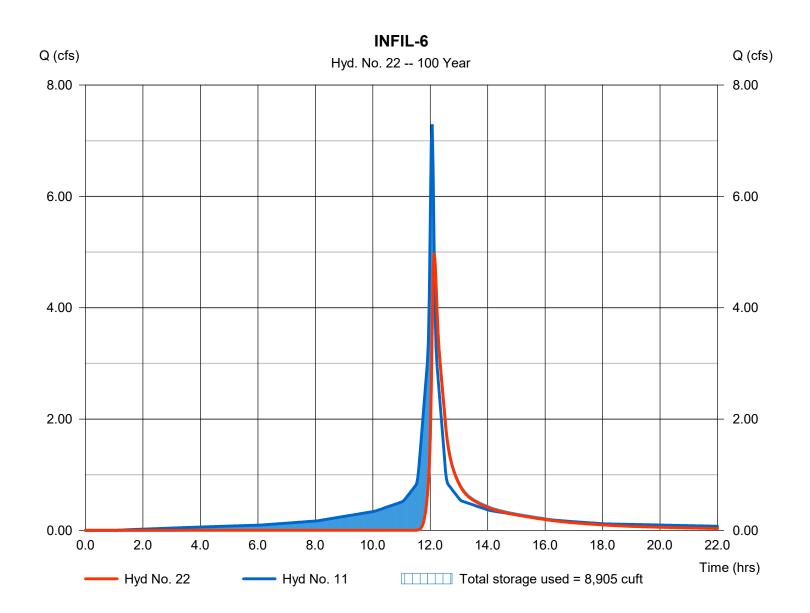
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 22

INFIL-6

Hydrograph type = Reservoir Peak discharge = 4.990 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 15,158 cuft Inflow hyd. No. Max. Elevation = 11 - PR WS-02G = 136.84 ftReservoir name = INFIL-6 Max. Storage = 8,905 cuft



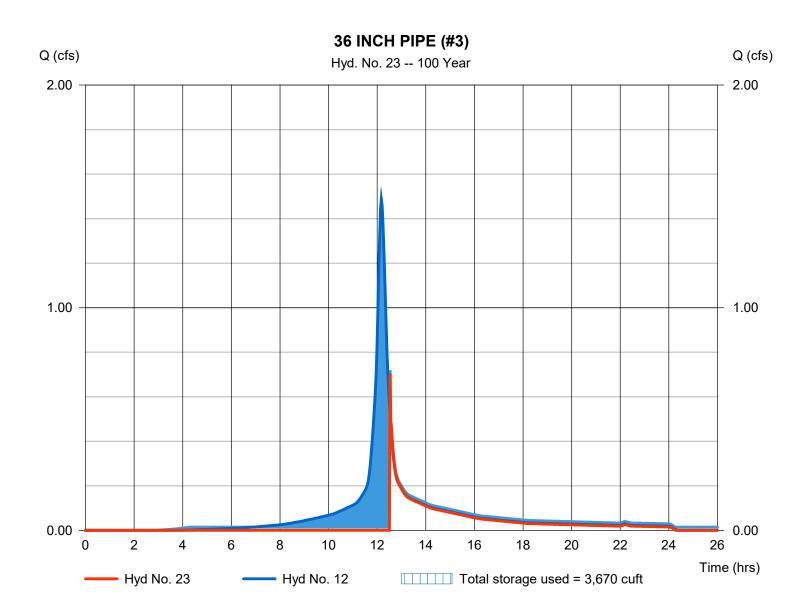
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 23

36 INCH PIPE (#3)

Hydrograph type = Reservoir Peak discharge = 0.704 cfsStorm frequency = 100 yrsTime to peak $= 12.53 \, hrs$ Time interval = 2 min Hyd. volume = 2,409 cuftMax. Elevation Inflow hyd. No. = 12 - PR WS-02H = 137.47 ftReservoir name = 36IN - 3Max. Storage = 3,670 cuft



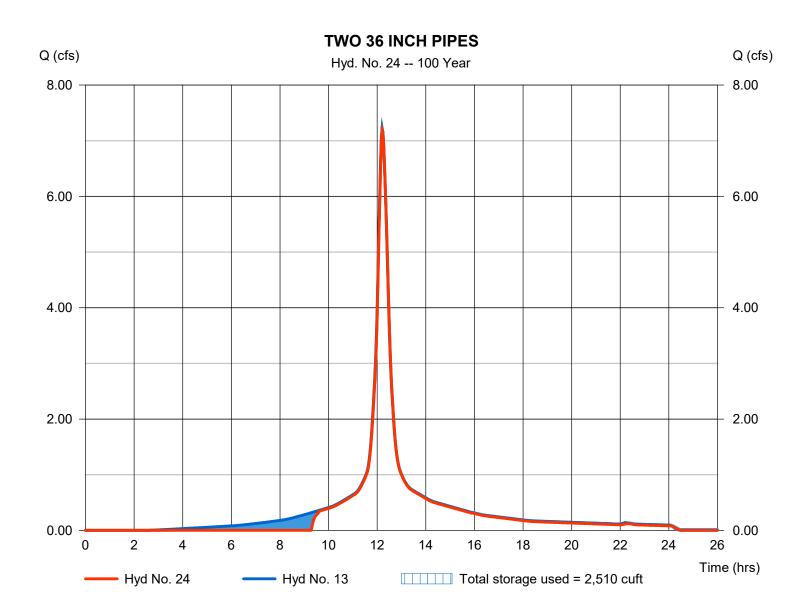
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 24

TWO 36 INCH PIPES

Hydrograph type Peak discharge = 7.197 cfs= Reservoir Storm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 30,870 cuftInflow hyd. No. Max. Elevation = 13 - PR WS-02I = 135.76 ftReservoir name = TWIN 36IN Max. Storage = 2,510 cuft



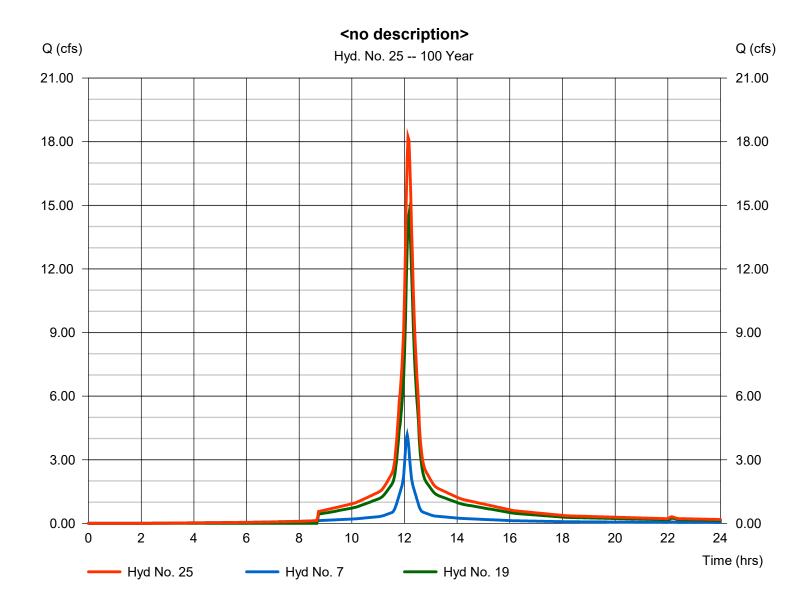
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 25

<no description>

Hydrograph type = Combine Peak discharge = 18.23 cfsStorm frequency Time to peak = 100 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 71,659 cuft Inflow hyds. = 7, 19 Contrib. drain. area = 0.576 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

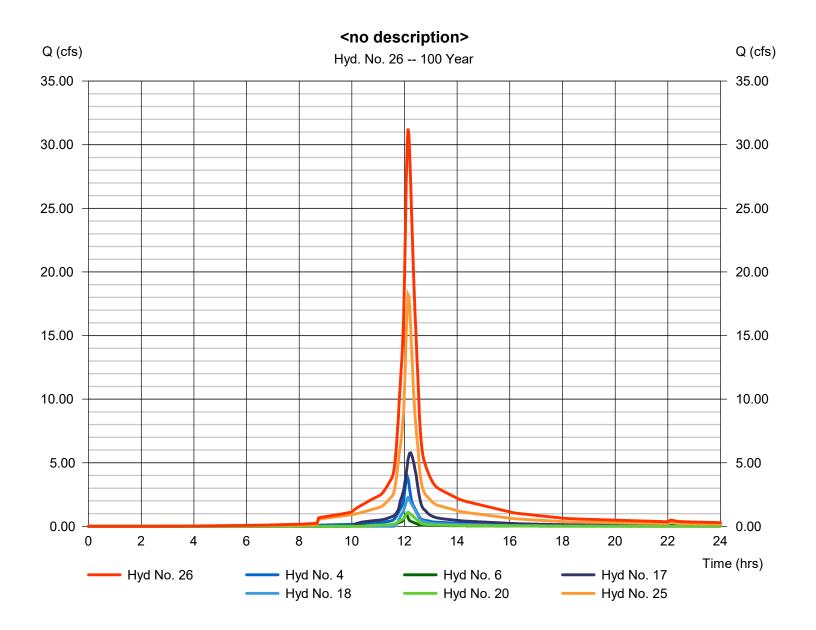
Hyd. No. 26

<no description>

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min

Inflow hyds. = 4, 6, 17, 18, 20, 25

Peak discharge = 31.28 cfs
Time to peak = 12.13 hrs
Hyd. volume = 123,737 cuft
Contrib. drain. area = 0.708 ac



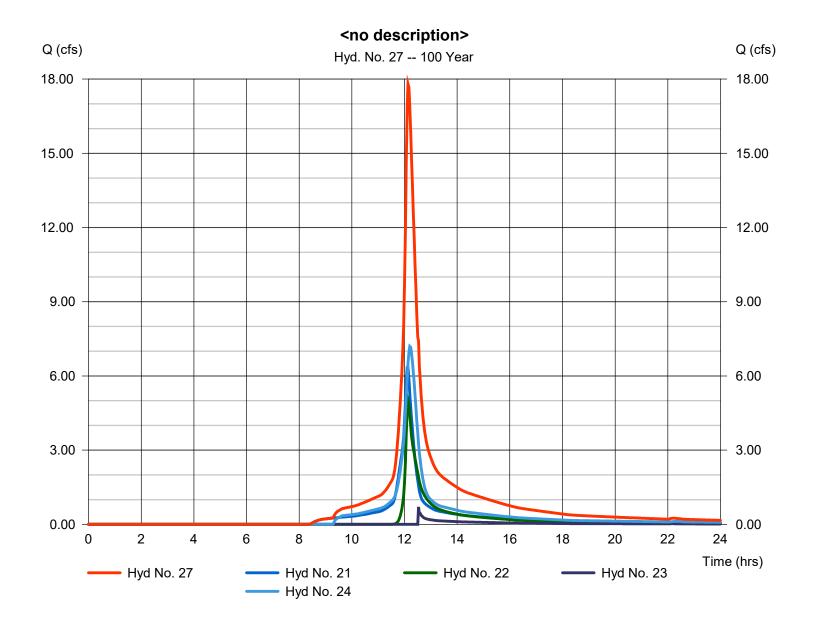
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 27

<no description>

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min Inflow hyds. = 21, 22, 23, 24 Peak discharge = 17.81 cfs
Time to peak = 12.13 hrs
Hyd. volume = 71,885 cuft
Contrib. drain. area = 0.000 ac



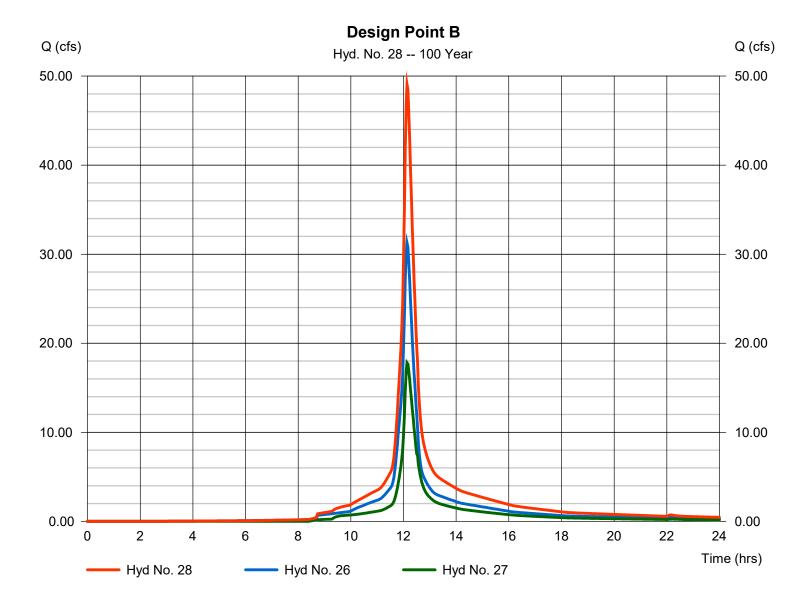
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Hyd. No. 28

Design Point B

Hydrograph type = Combine Peak discharge = 49.08 cfsStorm frequency = 100 yrsTime to peak $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 195,622 cuft Inflow hyds. = 26, 27 Contrib. drain. area = 0.000 ac



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

Return Period	Intensity-Du	Intensity-Duration-Frequency Equation Coefficients (FHA)					
(Yrs)	В	D	E	(N/A)			
1	0.0000	0.0000	0.0000				
2	23.2694	3.7000	0.7019				
3	0.0000	0.0000	0.0000				
5	28.1517	3.6000	0.6982				
10	33.4115	3.8000	0.7042				
25	38.5092	3.6000	0.6982				
50	42.7840	3.6000	0.6957				
100	48.0560	3.6000	0.6997				

File name: WILTON.IDF

Intensity = B / (Tc + D)^E

Return	·											
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5.10	3.71	2.98	2.52	2.21	1.97	1.79	1.64	1.52	1.42	1.33	1.26
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.27	4.55	3.66	3.10	2.71	2.42	2.20	2.02	1.87	1.75	1.64	1.55
10	7.22	5.26	4.23	3.58	3.13	2.80	2.54	2.33	2.16	2.02	1.90	1.79
25	8.57	6.22	5.00	4.24	3.70	3.31	3.00	2.76	2.56	2.39	2.24	2.12
50	9.57	6.96	5.60	4.74	4.15	3.71	3.37	3.09	2.87	2.68	2.52	2.38
100	10.66	7.74	6.22	5.26	4.60	4.11	3.73	3.43	3.17	2.96	2.79	2.63

Tc = time in minutes. Values may exceed 60.

 $\label{thm:precip} Precip.\ file\ name: J:$$\T\T5000\ Toll\ Brothers\012\ Woodbridge\ Village\Calculations\Stormwater\WOODBRIDGE.pcp$

		Rainfall Precipitation Table (in)						
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	2.95	3.52	0.00	4.65	5.38	6.54	7.41	8.34
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

$\textbf{Hydraflow Table of Contents} \\ \texttt{(F0173 Fuller)001 64 Danbury Rd)} \\ \texttt{Calculations} \\ \texttt{(Stormwater)Proposed-Hydraflow.gpw} \\ \texttt{(F0173 Fuller)001 64 Danbury Rd)} \\ \texttt{(F0173 Fuller$

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Tuesday, 12 / 5 / 2023

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APPENDIX E



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: CB-01

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.070	0.90	0.063
Landscaped / Lawns	0.003	0.30	0.001
	0.073		0.064

Weighted C: 0.87

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.015	75	0.020	1.2		

Total Tc = 1.2

Minimum Tc = 5.0

Designation: CB-02

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.274	0.90	0.247
Landscaped / Lawns	0.249	0.30	0.075
	0.524		0.322

Weighted C: 0.61

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland							
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)			
Segment A - B	0.4	10	0.02	3.35			
Segment B - C	0.24	84	0.02	12.22			
Segment C - D	0.015	143	0.04	1.54			

Total Tc = 17.1



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: CB-03

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.133	0.90	0.120
Landscaped / Lawns	0.033	0.30	0.010
	0.166		0.130

Weighted C: 0.78

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	10	0.02	3.35
Segment B - C	0.24	10	0.02	2.23
Segment C - D	0.015	135	0.03	1.65

Total Tc = 7.2

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: CB-04

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.113	0.90	0.102
Landscaped / Lawns	0.102	0.30	0.030
	0.214		0.132

Weighted C: 0.62

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	52	0.11	6.34
Segment B - C	0.24	3	0.11	0.43
Segment C - D	0.015	43	0.04	0.59

Total Tc = 7.4



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: CB-05

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.132	0.90	0.119
Landscaped / Lawns	0.001	0.30	0.000
	0.133		0.119

Weighted C: 0.90

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	35	0.045	0.5

Total Tc = 0.5

Minimum Tc = 5.0

Designation: CB-06

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.346	0.90	0.312
Landscaped / Lawns	0.045	0.30	0.013
	0.391		0.325

Weighted C: 0.83

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	95	0.065	0.9
Segment B - C	0.015	35	0.020	0.7

Total Tc = 1.6

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: CB-07

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.270	0.90	0.243
Landscaped / Lawns	0.001	0.30	0.000
	0.270		0.243

Weighted C: 0.90

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	35	0.020	0.7

Total Tc = 0.7

Minimum Tc = 5.0

Designation: CB-08

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.342	0.90	0.308
Landscaped / Lawns	0.004	0.30	0.001
	0.346		0.309

Weighted C: 0.89

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	60	0.020	1.0

Total Tc = 1.0 Minimum Tc = 5.0



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: CB-09

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.101	0.90	0.091
Landscaped / Lawns	0.056	0.30	0.017
	0.158		0.108

Weighted C: 0.69

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (m					
Segment A - B 0.24 20 0.05 2.69					
Segment B - C	0.015	32	0.04	0.47	

Total Tc = 3.2 Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: CB-10

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.132	0.90	0.119
Landscaped / Lawns	0.034	0.30	0.010
	0.165		0.129

Weighted C: 0.78

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.24	13	0.020	2.7	
Segment B - C	0.015	55	0.020	0.9	

Total Tc = 3.7



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **WQS-01**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.088	0.90	0.079
Landscaped / Lawns	0.003	0.30	0.001
	0.092		0.080

Weighted C: 0.88

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	105	0.025	1.5

Total Tc = 1.5

Minimum Tc = 5.0

Designation: WQS-02

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.120	0.90	0.108
Landscaped / Lawns	0.035	0.30	0.010
	0.155		0.118

Weighted C: 0.77

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	185	0.065	1.6

Total Tc = 1.6

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **WQS-03**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.271	0.90	0.244
Landscaped / Lawns	0.000	0.30	0.000
	0.271		0.244

Weighted C: 0.90

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min.)				
Segment A - B	0.015	35	0.045	0.5

Total Tc = 0.5

Minimum Tc = 5.0

Designation: WQS-04

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.178	0.90	0.160
Landscaped / Lawns	0.024	0.30	0.007
	0.203		0.168

Weighted C: 0.83

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (m					
Segment A - B	0.24	22	0.02	4.18	
Segment B - C	0.015	44	0.02	0.79	

Total Tc = 5.0



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **WQS-05**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.107	0.90	0.096
Landscaped / Lawns	0.042	0.30	0.012
	0.148		0.109

Weighted C: 0.73

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	7	0.020	1.7
Segment B - C	0.015	49	0.020	0.9

Total Tc = 2.5

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: AD-01

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.084	0.90	0.075
Landscaped / Lawns	0.005	0.30	0.002
	0.089		0.077

Weighted C: 0.87

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	13	7.600	0.3

Total Tc = 0.3



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-02

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.195	0.90	0.175
Landscaped / Lawns	0.008	0.30	0.002
	0.203		0.178

Weighted C: 0.88

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	10	0.020	2.1
Segment B - C	0.015	15	0.020	0.3
Segment C - D	0.24	6	0.020	1.5

Total Tc = 4.0

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: AD-03

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.005	0.90	0.004
Landscaped / Lawns	0.012	0.30	0.003
	0.016		0.008

Weighted C: 0.47

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min.				
Segment A - B	0.24	25	0.020	4.6

Total Tc = 4.6



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-04

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.005	0.90	0.004
Landscaped / Lawns	0.012	0.30	0.004
	0.017		0.008

Weighted C: 0.47

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	25	0.020	4.6

Total Tc = 4.6

Minimum Tc = 5.0

Designation: AD-05

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.000	0.90	0.000
Landscaped / Lawns	0.006	0.30	0.002
	0.006		0.002

Weighted C: 0.30

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	20	0.050	2.7

Total Tc = 2.7

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-06

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.015	0.90	0.013
Landscaped / Lawns	0.042	0.30	0.013
	0.057		0.026

Weighted C: 0.46

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min.)				
Segment A - B	0.24	25	0.075	2.7

Total Tc = 2.7

Minimum Tc = 5.0

Designation: AD-07

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.015	0.90	0.014
Landscaped / Lawns	0.053	0.30	0.016
	0.068		0.029

Weighted C: 0.43

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	25	0.075	2.7

Total Tc = 2.7



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-08

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.003	0.90	0.002
Landscaped / Lawns	0.011	0.30	0.003
	0.013		0.006

Weighted C: 0.42

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	18	0.020	3.6

Total Tc = 3.6

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: AD-09

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.019	0.90	0.017
Landscaped / Lawns	0.006	0.30	0.002
	0.025		0.019

Weighted C: 0.76

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.24	10	0.020	2.2	
Segment B - C	0.015	13	0.020	0.3	

Total Tc = 2.5



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-10

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.011	0.90	0.010
Landscaped / Lawns	0.008	0.30	0.002
	0.019		0.012

Weighted C: 0.65

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	13	0.020	2.7
Segment B - C	0.015	6	0.020	0.2

Total Tc = 2.9

Minimum Tc = 5.0

Designation: AD-11

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.025	0.90	0.022
Landscaped / Lawns	0.002	0.30	0.000
	0.026		0.023

Weighted C: 0.86

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	35	0.020	0.7

Total Tc = 0.7

Minimum Tc = 5.0

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-12

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.014	0.90	0.013
Landscaped / Lawns	0.006	0.30	0.002
	0.020		0.014

Weighted C: 0.72

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	14	0.020	0.3

Total Tc = 0.3 Minimum Tc = 5.0

Designation: **AD-13**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.006	0.90	0.006
Landscaped / Lawns	0.024	0.30	0.007
	0.030		0.013

Weighted C: 0.43

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	34	0.020	5.9

Total Tc = 5.9



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **AD-14**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.008	0.90	0.007
Landscaped / Lawns	0.076	0.30	0.023
	0.084		0.030

Weighted C: 0.36

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	61	0.020	9.5

Total Tc = 9.5

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation

Designation: AD-15

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.004	0.90	0.004
Landscaped / Lawns	0.033	0.30	0.010
	0.037		0.013

Weighted C: 0.37

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	21	0.020	4.0

Total Tc = 4.0



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: AD-16

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.007	0.90	0.006
Landscaped / Lawns	0.048	0.30	0.014
	0.055		0.021

Weighted C: 0.38

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	47	0.040	5.8

Total Tc = 5.8

Designation: AD-17

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.010	0.90	0.009
Landscaped / Lawns	0.035	0.30	0.010
	0.045		0.019

Weighted C: 0.43

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	50	0.020	8.1

Total Tc = 8.1

Note: Overland time of concentration computed using "Kinematic Wave" equation

Gutter and pipe time of concentration computed using Manning's equation



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **EX-CB-01**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.052	0.90	0.047
Landscaped / Lawns	0.013	0.30	0.004
	0.064		0.050

Weighted C: 0.78

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland											
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)							
Segment A - B	0.24	13	0.020	2.7							
Segment B - C	0.015	35	0.020	0.7							

Total Tc = 3.4

Minimum Tc = 5.0

Designation: EX-CB-02

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.149	0.90	0.134
Landscaped / Lawns	0.087	0.30	0.026
	0.236		0.160

Weighted C: 0.68

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland										
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)						
Segment A - B	0.24	31	0.025	5.04						

Total Tc = 5.0



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **EX-CB-03**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.010	0.90	0.009
Landscaped / Lawns	0.048	0.30	0.014
	0.058		0.023

Weighted C: 0.40

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland										
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)						
Segment A - B	0.24	45	0.133	3.48						

Total Tc = 3.5 Minimum Tc = 5.0

Designation: EX-CB-04

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.013	0.90	0.012
Landscaped / Lawns	0.070	0.30	0.021
	0.084		0.033

Weighted C: 0.40

Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland										
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)						
Segment A - B	0.24	15	0.1	1.62						

Shallow Concentrated Flow												
Segm	ent	Slope (ft/ft)	V (ft/s)	Length (ft)	Time (min.)							
Segment B - C	unpaved	0.045	3.42	125	0.6							
Segment C - D	unpaved	0.150	6.25	125	0.3							

Total Tc = 2.6 **Minimum Tc = 5.0**



Project Number: **F0173-001**Project Location: **Wilton, CT**

Description: **Proposed C & Tc Calculations**Prepared By: **AVC** Date: **December 4, 2023**

Designation: **EX-AD**

Cover Type	Area, ac	Coef.	AxC
Hardscape / Roof	0.009	0.90	0.009
Landscaped / Lawns	0.047	0.30	0.014
	0.057		0.023

Weighted C: 0.40

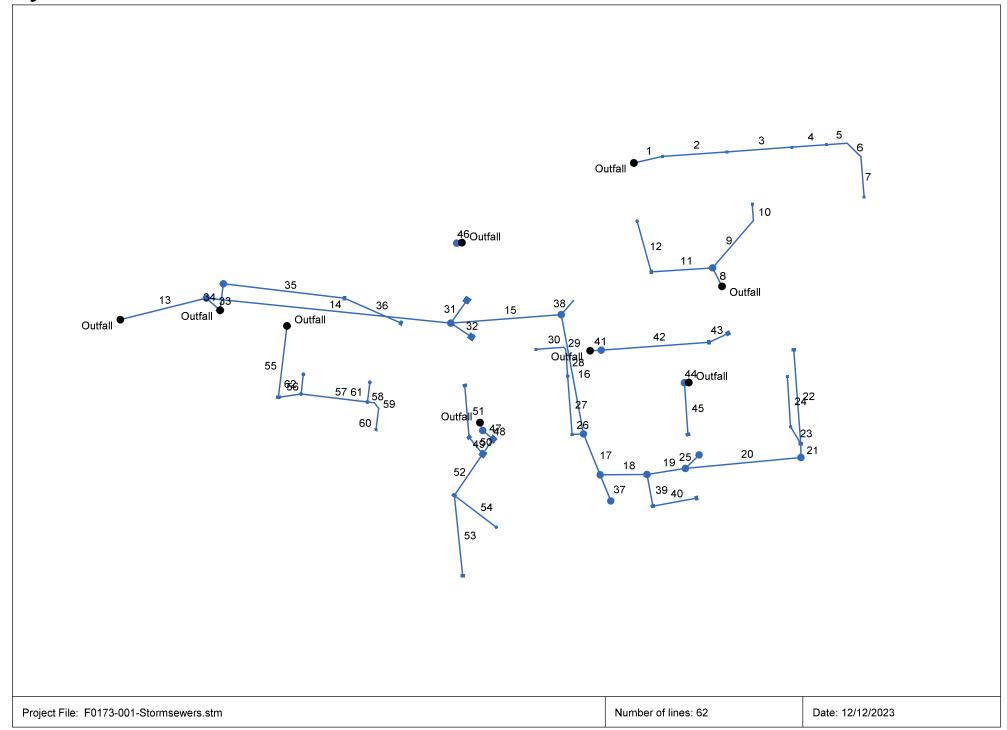
Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland										
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)						
Segment A - B	0.24	40	0.020	6.8						

Total Tc = 6.8

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	С	Тс		Rain	Total	Сар	Vel	Pipe		Invert Ele	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
Line	То		Incr	Total	coeff	Incr	Total	Inlet	Syst	(I) 	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	29.111	0.05	0.26	0.43	0.02	0.10	8.1	10.7	6.0	0.60	13.05	2.74	12	11.44	146.00	149.33	146.32	149.65	147.00	153.44	Pipe - (58)
2	1	64.080	0.06	0.21	0.38	0.02	0.08	5.8	10.3	6.1	0.48	3.86	2.38	12	1.00	149.33	149.97	149.65	150.26	153.44	154.55	Pipe - (57)
3	2	64.196	0.04	0.15	0.37	0.01	0.06	5.0	9.8	6.3	0.36	5.47	2.15	12	2.01	149.97	151.26	150.26	151.51	154.55	155.20	Pipe - (56)
4	3	34.280	0.08	0.11	0.36	0.03	0.04	9.5	9.5	6.4	0.28	3.84	2.02	12	0.99	151.26	151.60	151.51	151.82	155.20	155.54	Pipe - (55)
5	4	20.718	0.00	0.03	0.00	0.00	0.01	0.0	6.5	7.7	0.10	3.88	1.24	12	1.01	151.60	151.81	151.82	151.94	155.54	156.00	Pipe - (115)
6	5	19.047	0.00	0.03	0.00	0.00	0.01	0.0	6.3	7.8	0.10	3.85	1.70	12	1.00	151.81	152.00	151.94	152.13	156.00	156.00	Pipe - (114)
7	6	40.198	0.03	0.03	0.43	0.01	0.01	5.9	5.9	8.0	0.10	3.85	1.72	12	1.00	152.00	152.40	152.13	152.53	156.00	155.90	Pipe - (113)
8	End	20.612	0.09	0.45	0.88	0.08	0.40	5.0	5.8	8.1	3.21	11.68	4.53	12	9.17	145.00	146.89	146.29	147.66	149.67	152.40	Pipe - (06)
9	8	61.889	0.00	0.20	0.00	0.00	0.18	0.0	5.1	8.5	1.50	6.69	5.25	12	3.01	148.78	150.64	149.10	151.16	152.40	154.67	Pipe - (71)
10	9	16.371	0.20	0.20	0.88	0.18	0.18	5.0	5.0	8.6	1.51	3.81	3.66	12	0.98	150.64	150.80	151.16	151.32	154.67	154.30	Pipe - (70)
11	8	60.997	0.07	0.16	0.87	0.06	0.14	5.0	5.4	8.3	1.18	3.86	2.60	12	1.00	146.89	147.50	147.66	147.96	152.40	151.00	Pipe - (05)
12	11	52.306	0.09	0.09	0.87	0.08	0.08	5.0	5.0	8.6	0.67	7.71	2.38	12	4.00	147.50	149.59	147.96	149.93	151.00	153.10	Pipe - (04)
13	End	87.828	0.00	0.69	0.00	0.00	0.39	0.0	21.4	4.1	147.2	150.8	9.52	54	0.50	127.96	128.40	132.24	132.55	135.80	138.10	Pipe - (121)
14	13	243.249	0.00	0.69	0.00	0.00	0.39	0.0	21.0	4.1	143.4	149.6	9.02	54	0.49	128.80	130.00	133.78	134.89	138.10	139.90	Pipe - (120)
15	14	109.653	0.00	0.69	0.00	0.00	0.39	0.0	20.8	4.1	137.5	128.7	8.65	54	0.36	130.20	130.60	136.02	136.48	139.90	142.00	Pipe - (119)
16	15	120.483	0.00	0.69	0.00	0.00	0.39	0.0	19.7	4.3	17.27	108.8	1.80	42	1.00	131.80	133.00	137.64	137.67	142.00	140.19	Pipe - (118)
17	16	43.869	0.00	0.55	0.00	0.00	0.33	0.0	19.2	4.3	17.05	83.91	1.77	42	0.59	133.00	133.26	137.72	137.73	140.19	142.33	Pipe - (117)
18	17	46.296	0.00	0.55	0.00	0.00	0.33	0.0	18.5	4.4	3.17	52.06	1.01	24	4.51	133.41	135.50	137.78	137.79	142.33	145.00	Pipe - (26)
19	18	38.468	0.00	0.41	0.00	0.00	0.28	0.0	8.4	6.8	3.57	51.96	2.54	24	4.50	135.50	137.23	137.80	137.89	145.00	147.80	Pipe - (25)
20	19	115.000	0.00	0.41	0.00	0.00	0.28	0.0	7.7	7.1	1.97	51.90	2.75	24	4.49	137.23	142.39	137.89	142.88	147.80	152.20	Pipe - (24)
21	20	13.578	0.21	0.41	0.62	0.13	0.28	7.4	7.6	7.1	1.98	51.93	3.34	24	4.49	142.39	143.00	142.88	143.49	152.20	152.00	Pipe - (23)
22	21	93.648	0.17	0.17	0.78	0.13	0.13	7.2	7.2	7.3	0.95	3.87	3.60	12	1.00	147.56	148.50	147.90	148.91	152.00	152.00	Pipe - (22)
Proje	Project File: F0173-001-Stormsewers.stm										Number	of lines: 6	i2		Run Da	⊥ te: 12/12/2	2023					

NOTES:Intensity = $38.51 / (Inlet time + 3.60) ^ 0.70$; Return period =Yrs. 25; c = cir e = ellip b = box

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс		Rain	Total	Сар	Vel	Pipe		Invert Ele	ev	HGL Ele	٧	Grnd / Ri	im Elev	Line ID
Line	То	1	Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	-
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
23	21	19.814	0.02	0.03	0.47	0.01	0.02	5.0	5.7	8.1	0.13	3.88	2.03	12	1.01	144.80	145.00	144.92	145.14	152.00	149.00	Pipe - (28)
24	23	49.936	0.02	0.02	0.47	0.01	0.01	5.0	5.0	8.6	0.06	3.86	1.21	12	1.00	145.00	145.50	145.14	145.60	149.00	149.00	Pipe - (27)
25	19	19.145	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	1.69	3.84	4.27	12	0.99	143.48	143.67	143.94	144.22	147.80	148.50	Pipe - (30)
26	16	11.297	0.07	0.13	0.43	0.03	0.06	5.0	8.3	6.8	0.39	3.98	0.50	12	1.06	136.25	136.37	137.72	137.72	140.19	139.90	Pipe - (106)
27	26	58.106	0.06	0.06	0.46	0.03	0.03	5.0	6.4	7.7	0.22	4.96	0.50	12	1.65	136.37	137.33	137.73	137.73	139.90	140.90	Pipe - (59)
28	27	26.816	0.00	0.01	0.00	0.00	0.00	0.0	5.5	8.2	0.01	5.11	0.54	12	1.75	137.33	137.80	137.74	137.85	140.90	142.00	Pipe - (72)
29	28	2.804	0.00	0.01	0.00	0.00	0.00	0.0	5.5	8.2	0.01	3.99	1.04	12	1.07	137.80	137.83	137.85	137.88	142.00	142.00	Pipe - (73)
30	29	27.512	0.01	0.01	0.30	0.00	0.00	5.0	5.0	8.6	0.02	3.89	0.93	12	1.02	137.82	138.10	137.88	138.15	142.00	141.60	Pipe - (62)
31	14	27.900	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	0.88	3.86	3.53	12	1.00	136.17	136.45	136.49	136.84	139.90	140.39	Pipe - (46)
32	14	24.525	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	4.99	5.98	6.35	12	2.41	134.41	135.00	136.02	136.43	139.90	140.15	Pipe - (98)
33	13	18.166	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	1.94	6.00	2.47	12	2.42	132.06	132.50	133.78	133.83	138.10	138.50	Pipe - (86)
34	End	26.508	0.15	0.47	0.73	0.11	0.35	5.0	6.0	7.9	2.76	3.89	5.00	12	1.02	133.93	134.20	134.55	134.91	138.50	137.70	Pipe - (82)
35	34	120.556	0.17	0.32	0.78	0.13	0.24	5.0	5.4	8.3	1.97	2.72	3.64	12	0.50	134.20	134.80	134.91	135.40	137.70	138.30	Pipe - (48)
36	35	61.456	0.16	0.16	0.69	0.11	0.11	5.0	5.0	8.6	0.93	3.48	2.33	12	0.81	134.80	135.30	135.53	135.71	138.30	138.80	Pipe - (47)
37	17	27.974	0.00	0.00	0.00	0.00	0.00	5.0	5.0	0.0	13.91	77.10	1.45	42	0.50	133.26	133.40	137.78	137.78	142.33	141.20	Pipe - (116)
38	15	18.394	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	120.3	149.0	7.56	54	0.49	131.80	131.89	137.64	137.70	142.00	142.20	Pipe - (122)
39	18	32.000	0.06	0.14	0.40	0.02	0.06	5.0	15.1	5.0	0.28	14.22	0.16	18	1.56	134.50	135.00	137.80	137.80	145.00	141.00	
40 41	39 End	44.000 11.015	0.08	0.08 0.68	0.40 0.77	0.03 0.12	0.03 0.44	12.1 5.0	12.1 17.5	5.6 4.6	0.19 4.05	4.11 19.38	0.24 5.69	12 12	1.14 25.24	135.10 136.62	135.60 139.40	137.80 137.47	137.81 140.25	141.00 143.00	141.30 142.90	Pipe - (107)
42	41	107.009		0.52	0.61	0.32	0.32	17.1	17.1	4.6	3.52	6.82	5.08	12	3.12	139.40	142.74	140.25	143.54	142.90	147.90	Pipe - (12)
43	42	20.730		0.00	0.00	0.00	0.00	0.0	0.0	0.0	2.05	3.88	3.56	12	1.01	142.74	142.95	143.54	143.56	147.90	148.90	Pipe - (11)
44	End	4.387	0.27	0.40	0.90	0.24	0.36	5.0	5.4	8.3	3.03	4.12	4.81	12	1.14	143.54	143.59	144.29	144.34	148.00	147.60	Pipe - (93)
45	44	51.421		0.13	0.90	0.12	0.12	5.0	5.0	8.6	1.03	3.84	2.43	12	0.99	143.59	144.10	144.34	144.53	147.60	147.60	Pipe - (17)
73	7-7	31.721	0.15	0.15	0.30	0.12	0.12	3.0	0.0	0.0	1.00	0.04	2.73	'-	0.55	140.00	177.10	177.07	144.55	147.00	147.00	1 100 - (11)
Proje	Project File: F0173-001-Stormsewers.stm								Number of lines: 62			Run Date: 12/12/2023										

NOTES:Intensity = 38.51 / (Inlet time + 3.60) ^ 0.70; Return period =Yrs. 25; c = cir e = ellip b = box

Storm Sewer Tabulation

Statio	n	Len	Drng A	rea	Rnoff	Area x	C	Тс		Rain	Total	Сар	Vel	Pipe		Invert El	ev	HGL Ele	v	Grnd / Ri	m Elev	Line ID
_ine	То		Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	-
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
46	End	5.195	0.20	0.20	0.83	0.17	0.17	5.0	5.0	8.6	1.44	3.78	3.59	12	0.96	136.45	136.50	136.96	137.01	140.50	140.00	Pipe - (76)
47	End	8.312	0.00	1.02	0.00	0.00	0.80	0.0	8.8	6.6	5.31	6.28	7.05	12	2.65	134.20	134.42	135.10	135.35	140.00	140.00	Pipe - (128)
48	47	13.266	0.00	1.02	0.00	0.00	0.80	0.0	8.8	6.6	5.32	6.18	7.09	12	2.56	134.46	134.80	135.35	135.73	140.00	140.20	Pipe - (127)
49	48	17.753	0.00	1.02	0.00	0.00	0.80	0.0	8.7	6.7	5.34	7.64	4.64	18	0.45	134.80	134.88	135.73	135.81	140.20	140.00	Pipe - (126)
50	49	21.322	0.27	0.66	0.90	0.24	0.57	5.0	5.2	8.4	4.79	6.89	6.25	12	3.19	134.90	135.58	136.14	136.48	140.00	139.60	Pipe - (32)
51	50	51.579	0.39	0.39	0.83	0.32	0.32	5.0	5.0	8.6	2.78	3.87	4.18	12	1.01	135.58	136.10	136.48	136.81	139.60	139.60	Pipe - (31)
52	49	49.833	0.24	0.36	0.68	0.16	0.23	5.0	8.3	6.8	1.59	2.56	2.03	12	0.44	134.88	135.10	136.14	136.23	140.00	138.60	Pipe - (125)
53	52	80.288	0.06	0.06	0.78	0.05	0.05	5.0	5.0	8.6	0.43	3.60	0.77	12	0.87	135.10	135.80	136.32	136.33	138.60	138.60	Pipe - (123)
54	52	52.042	0.06	0.06	0.40	0.02	0.02	6.8	6.8	7.5	0.17	5.07	0.49	12	1.73	135.10	136.00	136.32	136.33	138.60	139.10	Pipe - (124)
55	End	71.365	0.35	0.45	0.89	0.31	0.38	5.0	6.3	7.8	2.97	3.88	4.77	12	1.01	133.20	133.92	133.94	134.66	139.40	138.00	Pipe - (38)
56	55	22.641	0.03	0.10	0.86	0.02	0.07	5.0	6.1	7.9	0.58	3.89	1.82	12	1.02	133.91	134.14	134.66	134.46	138.00	138.74	Pipe - (37)
57	56	66.235	0.03	0.06	0.76	0.02	0.04	5.0	5.5	8.3	0.30	3.85	1.85	12	1.00	134.14	134.80	134.46	135.03	138.74	138.79	Pipe - (36)
58	57	6.823	0.00	0.01	0.00	0.00	0.01	0.0	5.3	8.3	0.05	3.91	0.93	12	1.03	134.85	134.92	135.03	135.01	138.79	138.80	Pipe - (92)
59	58	7.053	0.00	0.01	0.00	0.00	0.01	0.0	5.3	8.4	0.05	3.84	1.38	12	0.99	134.92	134.99	135.01	135.08	138.80	138.80	Pipe - (91)
60	59	21.252	0.01	0.01	0.42	0.01	0.01	5.0	5.0	8.6	0.05	3.83	1.40	12	0.99	134.99	135.20	135.08	135.29	138.80	138.70	Pipe - (90)
61	57	19.655	0.02	0.02	0.65	0.01	0.01	5.0	5.0	8.6	0.11	3.89	1.25	12	1.02	134.80	135.00	135.03	135.13	138.79	138.50	Pipe - (39)
62	56	19.655	0.02	0.02	0.72	0.01	0.01	5.0	5.0	8.6	0.12	3.89	2.02	12	1.02	134.80	135.00	134.92	135.14	138.74	138.50	Pipe - (40)
Proje	ect File:	F0173-	001-Sto	rmsewer	s.stm											Numbe	r of lines: 6	62		Run Da	te: 12/12/2	2023

NOTES:Intensity = 38.51 / (Inlet time + 3.60) ^ 0.70; Return period =Yrs. 25; c = cir e = ellip b = box



Description: Riprap Apron Calculation
Prepared By: AVC Date: December 4, 2023

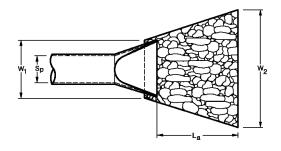
Riprap Apron

 $Invert \ Elevation = 146.00 \ ft$ $Tailwater \ Elevation = 146.33 \ ft$ $Tailwater \ Depth \ (TW) = 0.33 \ ft$ $Inside \ Pipe \ Diameter \ (S_p) = 1.00 \ ft$ $Pipe \ Discharge \ (Q) = 0.60 \ cfs \ (From \ Hydraflow \ Model)$ $Outlet \ Velocity \ (V) = 2.74 \ ft/s \ (From \ Hydraflow \ Model)$

Apron Type

Type A Riprap Apron (Minimum Tailwater Condition) TW < $0.5R_p$ Type B Riprap Apron (Maximum Tailwater Condition) TW $\geq 0.5R_p$ TW = $146.33 < 0.5R_p$

Use Type A Apron



Apron Length

Type A Riprap Apron (Minimum Tailwater Condition) TW $< 0.5R_p$

$$L_a = (1.8(Q-5.0)/Sp^{1.5})+10.0$$

Apron Width

Type A Riprap Apron (Minimum Tailwater Condition) $TW < 0.5R_p$

$$W_1 = 3*S_p$$

$$W_2 = 3*S_p + 0.7L_a$$

$W_1 =$	3.00	ft	
$W_2 =$	4.46	ft	

Riprap Specification

Outlet Velocity (V)=	0-8 ft/s	Modified
Outlet Velocity (V)=	8-10 ft/s	Intermediate
Outlet Velocity (V)=	10-14 ft/s	Standard

Outlet Velocity (V)=	2.740	ft/s	Use Modified Riprap

Outlet protection has been designed in accordance with the Section 11.13 of the ConnDOT Drainage Manual



Description: Level Spreader Calculation
Prepared By: AVC Date: December 4, 2023

Level Spreader

Flow for 10 Yr Storm= 0.6 CFS

Depth= 0.33 FT

Max Allowable Velocity **0.5** FPS

Length= **3.636364** FT

Proposed Length 10 FT

Calculated in accordence with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control Section 5-11

APPENDIX F



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-A(I)

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	0.458
Impervious Area in acres	=	0.433
Pecenct of Impervious Area (I)	=	95
Volumetric Runoff Coefficient (R)		

R = 0.05 + 0.009(I) = 0.901

WQv = (0.5")(R)(A) = 0.0172 ac*ft 12 = 749 cf

1,370 CF PROVIDED

Required Water Quality Flow (WQf)

WQv (Ac*ft)	=	0.0172	
Drainage Area (Ac)	=	0.458	
Q= WQv*12 / DA	=	0.450	in
Runoff Depth in inches (Q)	=	0.450	in
Design Precipitation in inches (P)	=	1	in
CN=1000/[10+5*P+10Q-10*(Q ² +1.25QP) ^{1/2}]	=	93	CN
From table 4-1 in chapter 4, TR-55			
$\mathbf{I_a}$	=	0.151	in
I _a / P	=	0.151	
From Exhibit 4-11 in chapter 4, TR-55			
\mathbf{q}_{u}	=	633	csm/in
Unit peak discharge in csm/in (q _u)	=	633	
Area in square miles (A)	=	0.001	
Runoff Depth in inches (Q)	=	0.450	
$WQF=q_u*A*Q$	=	0.204	cfs



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-A(II)

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	0.683
Impervious Area in acres	=	0.393
Pecenct of Impervious Area (I)	=	58
Volumetric Runoff Coefficient (R)		

R = 0.05 + 0.009(I) = 0.568

 $WQv = \frac{(0.5")(R)(A)}{12} = \frac{0.0162 \text{ ac*ft}}{704 \text{ cf}}$

1,022 CF PROVIDED

Required Water Quality Flow (WQf)

WQv (Ac*ft)	=	0.0162
Drainage Area (Ac)	=	0.683
Q= WQv*12 / DA	=	0.284 in
Runoff Depth in inches (Q)	=	0.284 in
Design Precipitation in inches (P)	=	<u>1</u> in
CN=1000/[10+5*P+10Q-10*(Q ² +1.25QP) ^{1/2}	=	89 CN
From table 4-1 in chapter 4, TR-55		
$\mathbf{I_a}$	=	0.247 in
I _a / P	=	0.247
From Exhibit 4-11 in chapter 4, TR-55		
\mathbf{q}_{u}	=	585 csm/in
Unit peak discharge in csm/in (q _u)	=	585
Area in square miles (A)	=	0.001
Runoff Depth in inches (Q)	=	0.284
$WQF=q_u*A*Q$	=	0.177 cfs



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-B (TOTAL)

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	1.092
Impervious Area in acres	=	0.714
Pecenct of Impervious Area (I)	=	65
Volumetric Runoff Coefficient (R)		

$$R = 0.05 + 0.009(I) = 0.638$$

2,240 CF PROVIDED

Required Water Quality Flow (WQf)

WQv (Ac*ft)	=	0.0291
Drainage Area (Ac)	=	1.092

$$Q = WQv*12 / DA = 0.319 in$$

Runoff Depth in inches (Q)	=	0.319 in
Design Precipitation in inches (P)	=	1 in

$$CN=1000/[10+5*P+10Q-10*(Q^2+1.25QP)^{1/2} = 90 CN$$

From table 4-1 in chapter 4, TR-55

 I_a = 0.222 in I_a/P = 0.222

From Exhibit 4-11 in chapter 4, TR-55

 $\mathbf{q}_{\mathrm{u}} = 625 \, \mathrm{csm/in}$

Unit peak discharge in csm/in (q _u)	=	625
Area in square miles (A)	=	0.002
Runoff Depth in inches (Q)	=	0.319

 $WQF=q_u*A*Q = 0.340 cfs$



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-E

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	0.203
Impervious Area in acres	=	0.177
Pecenct of Impervious Area (I)	=	87
Volumetric Runoff Coefficient (R)		

$$R = 0.05 + 0.009(I) = 0.835$$

WQv =
$$\frac{(0.5")(R)(A)}{12}$$
 = $\frac{0.0071 \text{ ac*ft}}{308 \text{ cf}}$

520 CF PROVIDED

Required Water Quality Flow (WQf)

WQv (Ac*ft)	=	0.0071	
Drainage Area (Ac)	=	0.203	
Q= WQv*12 / DA	=	0.417	in
Runoff Depth in inches (Q)	=	0.417	in
Design Precipitation in inches (P)	=	1	in
CN=1000/[10+5*P+10Q-10*(Q ² +1.25QP) ^{1/2}	=	92	CN
From table 4-1 in chapter 4, TR-55			
$\mathbf{I_a}$	=	0.174	in
I _a / P	=	0.174	
From Exhibit 4-11 in chapter 4, TR-55			
\mathbf{q}_{u}	=	630	csm/in
Unit peak discharge in csm/in (q _u)	=	630]
Area in square miles (A)	=	0.000	
Runoff Depth in inches (Q)	=	0.417	
$\mathbf{WQF} = \mathbf{q_u} \cdot \mathbf{A} \cdot \mathbf{Q}$	=	0.083	cfs
CDS 2015-4-C Treatment Capacity	=	1.2	cfs Provided



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-F

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	1.023
Impervious Area in acres	=	0.826
Pecenct of Impervious Area (I)	=	81
Volumetric Runoff Coefficient (R)		

R = 0.05 + 0.009(I) = 0.777

1,450 CF PROVIDED

Required Water Quality Flow (WQf)

Q= WQv*12 / DA	=	0.388	in
Drainage Area (Ac)	=	1.023	
WQv (Ac*ft)	=	0.0331	

Runoff Depth in inches (Q) = **0.388** in Design Precipitation in inches (P) = **1** in

 $CN=1000/[10+5*P+10Q-10*(Q^2+1.25QP)^{1/2} = 92 CN$

From table 4-1 in chapter 4, TR-55

 $I_a = 0.174 \text{ in}$ $I_a / P = 0.174$

From Exhibit 4-11 in chapter 4, TR-55

 $q_u = 630 \text{ csm/in}$

 $WQF=q_u*A*Q = 0.391 cfs$



Description: Water Quality Calculations
Prepared By: AVC Date: December 4, 2023

WQA-G

Required Water Quality Volume (WQv)

Total Area in acres (A)	=	0.930
Impervious Area in acres	=	0.774
Pecenct of Impervious Area (I)	=	83
Volumetric Runoff Coefficient (R)		

R = 0.05 + 0.009(I) = 0.799

WQv = $\frac{(0.5")(R)(A)}{12}$ = 0.0310 ac*ft 1 = 1349 cf

4,069 CF PROVIDED

1.2 cfs Provided

Required Water Quality Flow (WQf)

CDS 2015-4-C Treatment Capacity

WQv (Ac*ft)	=	0.0310]
Drainage Area (Ac)	=	0.930	
Q= WQv*12 / DA	=	0.400	in
Runoff Depth in inches (Q)	=	0.400	in
Design Precipitation in inches (P)	=	1	in
CN=1000/[10+5*P+10Q-10*(Q ² +1.25QP) ^{1/2}	=	92	CN
From table 4-1 in chapter 4, TR-55			
I _a	=	0.174	in
I _a / P	=	0.174	
From Exhibit 4-11 in chapter 4, TR-55			
\mathbf{q}_{u}	=	630	csm/in
Unit peak discharge in csm/in (q _u)	=	630]
Area in square miles (A)	=	0.001	
Runoff Depth in inches (Q)	=	0.400	
$WQF=q_u*A*Q$	=	0.366	cfs



Description: Stormwater BMP Pollutant Removal Estimate

Prepared By: **AVC** Date: **December 4, 2023**

Water Quality Area A(I)

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.170	0.034	9.041	0.013	0.003	0.012
Proposed, Post Treatment	lb/yr/1-in	0.101	0.008	0.429	0.005	0.001	0.001
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Water Quality Area A(II)

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.155	0.031	8.253	0.012	0.003	0.011
Proposed, Post Treatment	lb/yr/1-in	0.093	0.007	0.392	0.004	0.001	0.001
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Water Quality Area B

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.299	0.060	15.889	0.023	0.005	0.021
Proposed, Post Treatment	lb/yr/1-in	0.178	0.013	0.755	0.008	0.002	0.002
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Water Quality Area E

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.070	0.014	3.728	0.005	0.001	0.005
Proposed, Post Treatment	lb/yr/1-in	0.042	0.003	0.177	0.002	0.000	0.000
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Water Quality Area F

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.334	0.067	17.735	0.025	0.006	0.024
Proposed, Post Treatment	lb/yr/1-in	0.199	0.015	0.842	0.009	0.002	0.002
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Water Quality Area G

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.310	0.062	16.474	0.023	0.005	0.022
Proposed, Post Treatment	lb/yr/1-in	0.185	0.014	0.783	0.009	0.002	0.002
Reduction, Pre to Post Treat		40%	78%	95%	64%	70%	90%

Northeast Portion to Area Drains

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.035	0.007	1.853	0.003	0.001	0.002
Proposed, Post Treatment	lb/yr/1-in	0.035	0.007	1.853	0.003	0.001	0.002
Reduction, Pre to Post Treat		0%	0%	0%	0%	0%	0%

Areas to Existing Infiltration Systems

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	1.161	0.234	61.720	0.088	0.020	0.082
Proposed, Post Treatment	lb/yr/1-in	0.848	0.157	6.172	0.060	0.014	0.056
Reduction. Pre to Post Treat		27%	33%	90%	32%	32%	32%

Total Site

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	2.534	0.511	134.694	0.192	0.044	0.180
Proposed, Post Treatment	lb/yr/1-in	1.680	0.224	11.403	0.099	0.021	0.068
Reduction, Pre to Post Treat		34%	56%	92%	48%	52%	62%

Loading Calculation

Location: Area A(I) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.95 Total Area = 0.458 acres

Pollutant	Resid	<u>ential</u>	<u>Weig</u>	<u>ıhted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.458	1.900	1.900	0.170
Total Phosphorus (P)	0.458	0.383	0.383	0.034
Total Suspended Solids	0.458	101.0	101.0	9.0
Lead	0.458	0.144	0.144	0.013
Copper	0.458	0.033	0.033	0.003
Zinc	0.458	0.135	0.135	0.012
	L = 0.226	56 * EMC * [0.15 + 0.75*I] * P *A		
L	Pollution	Loading (lbs/year)		
EMC		nt Mean Concentration (mg/L)		
I		of Impervious Acres (acres)		
P		ainfall (in)		
Α	Watershe	d Area (acres)		

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Area A(I) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.95 Total Area = 0.458 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout	
	(lbs)	(105)	(%)	(IDS)	(lbs)	
Total Nitrogen (N)	0.170	0.170	0	0.00	0.170	
Total Phosphorus (P)	0.034	0.034	0	0.00	0.034	
Total Suspended Solids	9.041	9.0	5	0.45	8.6	
Lead	0.013	0.013	0	0.00	0.013	
Copper	0.003	0.003	0	0.00	0.003	
Zinc	0.012	0.012	0	0.00	0.012	
Lin 1	Pollutant Load	In				
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in	n percentage				
Lout	Pollutant Load	out of BMP				

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area A(I) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.95 Total Area = 0.458 acres

BMP: Water Quality Structure

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)	
	(103)	(103)	(/0)	(103)	(103)	
Total Nitrogen (N)	0.170	0.170	18.3	0.03	0.139	
Total Phosphorus (P)	0.034	0.034	66.9	0.02	0.011	
Total Suspended Solids	8.589	8.6	50	4.29	4.3	
Lead	0.013	0.013	46.5	0.01	0.007	
Copper	0.003	0.003	56.2	0.00	0.001	
Zinc	0.012	0.012	85.3	0.01	0.002	
Lin 1	Pollutant Load I	[n				
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in	n percentage				
Lout	Pollutant Load	out of BMP				

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area A(I) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.95 Total Area = 0.458 acres

BMP: Infiltration System

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)		
	(183)	(183)	()	(103)	(103)		
Total Nitrogen (N)	0.139	0.139	27	0.04	0.101		
Total Phosphorus (P)	0.011	0.011	33	0.00	0.008		
Total Suspended Solids	4.294	4.3	90	3.86	0.429		
Lead	0.007	0.007	32	0.00	0.005		
Copper	0.001	0.001	32	0.00	0.001		
Zinc	0.002	0.002	32	0.00	0.001		
Lin 1	Pollutant Load	In					
Sum L	Sum of Polluta	nt Load to this	BMP				
RR	Removal rate i	Removal rate in percentage					
Lout	Pollutant Load	out of BMP					

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
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Loading Calculation

Location: Area A(II) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.50 Total Area = 0.683 acres

Pollutant	Resid	<u>ential</u>		<u>Weig</u>	<u>hted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.683	1.900		1.900	0.155
Total Phosphorus (P)	0.683	0.383		0.383	0.031
Total Suspended Solids	0.683	101.0		101.0	8.3
Lead	0.683	0.144		0.144	0.012
Copper	0.683	0.033		0.033	0.003
Zinc	0.683	0.135		0.135	0.011
	L = 0.226	6 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution L	oading (l	bs/year)		
EMC	Mean Eve	nt Mean (Concentration (mg/L)		
I		•	ous Acres (acres)		
Р	Annual Ra				
A	Watershee	d Area (a	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management* by Debo & Reese

Location: Area A(II) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.50 Total Area = 0.683 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout	
	(lbs)	(lbs)	(%)	(lbs)	(lbs)	
Total Nitrogen (N)	0.155	0.155	0	0.00	0.155	
Total Phosphorus (P)	0.031	0.031	0	0.00	0.031	
Total Suspended Solids	8.253	8.3	5	0.41	7.8	
Lead	0.012	0.012	0	0.00	0.012	
Copper	0.003	0.003	0	0.00	0.003	
Zinc	0.011	0.011	0	0.00	0.011	
Lin 1	Pollutant Load I	īn				
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in	percentage				
Lout	Pollutant Load of	out of BMP				

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area A(II) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.50 Total Area = 0.683 acres

BMP: Water Quality Structure

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout	
	(lbs)	(lbs)	(%)	(lbs)	(lbs)	
Total Nitrogen (N)	0.155	0.155	18.3	0.03	0.127	
Total Phosphorus (P)	0.031	0.031	66.9	0.02	0.010	
Total Suspended Solids	7.841	7.8	50	3.92	3.9	
Lead	0.012	0.012	46.5	0.01	0.006	
Copper	0.003	0.003	56.2	0.00	0.001	
Zinc	0.011	0.011	85.3	0.01	0.002	
Lin 1	Pollutant Load In					
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in pe	rcentage				
Lout	Pollutant Load out	of BMP				

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area A(II) Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.50 Total Area = 0.683 acres

BMP: Infiltration System

Pollutant	Lin 1	Sum L	RR (-)	Lremoved	Lout	
	(lbs)	(lbs)	(-)	(lbs)	(lbs)	
Total Nitrogen (N)	0.127	0.127	27	0.03	0.093	
Total Phosphorus (P)	0.010	0.010	33	0.00	0.007	
Total Suspended Solids	3.920	3.9	90	3.53	0.4	
Lead	0.006	0.006	32	0.00	0.004	
Copper	0.001	0.001	32	0.00	0.001	
Zinc	0.002	0.002	32	0.00	0.001	
Lin 1	Pollutant Load In					
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in pe	ercentage				
Lout	Pollutant Load out	of BMP				

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Loading Calculation

Location: Area B Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.65 Total Area = 1.089 acres

Pollutant	Reside	<u>ential</u>	<u>Weig</u>	<u>ihted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	1.089	1.900	1.900	0.299
Total Phosphorus (P)	1.089	0.383	0.383	0.060
Total Suspended Solids	1.089	101.0	101.0	15.9
Lead	1.089	0.144	0.144	0.023
Copper	1.089	0.033	0.033	0.005
Zinc	1.089	0.135	0.135	0.021
L EMC I P A	Pollution L Mean Ever Fraction o Annual Ra	6 * EMC * [0.15 + 0.75*I] * P *A oading (lbs/year) nt Mean Concentration (mg/L) f Impervious Acres (acres) infall (in) d Area (acres)		

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Area B Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.65 Total Area = 1.089 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout			
	(lbs)	(lbs)	(%)	(lbs)	(lbs)			
Total Nitrogen (N)	0.299	0.299	0	0.00	0.299			
Total Phosphorus (P)	0.060	0.060	0	0.00	0.060			
Total Suspended Solids	15.889	15.9	5	0.79	15.1			
Lead	0.023	0.023	0	0.00	0.023			
Copper	0.005	0.005	0	0.00	0.005			
Zinc	0.021	0.021	0	0.00	0.021			
Lin 1	Pollutant Loa	d In						
Sum L	Sum of Pollut	Sum of Pollutant Load to this BMP						
RR	Removal rate	in percentage						
Lout	Pollutant Load	d out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area B Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.65 Total Area = 1.089 acres

BMP: Water Quality Structure

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)			
	(103)	(103)	(70)	(103)	(103)			
Total Nitrogen (N)	0.299	0.299	18.3	0.05	0.244			
Total Phosphorus (P)	0.060	0.060	66.9	0.04	0.020			
Total Suspended Solids	15.094	15.1	50	7.55	7.5			
Lead	0.023	0.023	46.5	0.01	0.012			
Copper	0.005	0.005	56.2	0.00	0.002			
Zinc	0.021	0.021	85.3	0.02	0.003			
Lin 1	Pollutant Load	In						
Sum L	Sum of Polluta	Sum of Pollutant Load to this BMP						
RR	Removal rate i	n percentage						
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area B Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.65 Total Area = 1.089 acres

BMP: Infiltration System

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)			
	(103)	(103)		(103)	(103)			
Total Nitrogen (N)	0.244	0.244	27	0.07	0.178			
Total Phosphorus (P)	0.020	0.020	33	0.01	0.013			
Total Suspended Solids	7.547	7.5	90	6.79	0.8			
Lead	0.012	0.012	32	0.00	0.008			
Copper	0.002	0.002	32	0.00	0.002			
Zinc	0.003	0.003	32	0.00	0.002			
Lin 1	Pollutant Load	l In						
Sum L	Sum of Polluta	Sum of Pollutant Load to this BMP						
RR	Removal rate	in percentage						
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Loading Calculation

Location: Area E Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.87 Total Area = 0.203 acres

Pollutant	Resid	<u>ential</u>		<u>Weig</u>	<u>hted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.203	1.900		1.900	0.070
Total Phosphorus (P)	0.203	0.383		0.383	0.014
Total Suspended Solids	0.203	101.0		101.0	3.7
Lead	0.203	0.144		0.144	0.005
Copper	0.203	0.033		0.033	0.001
Zinc	0.203	0.135		0.135	0.005
	L = 0.226	6 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution L	oading (I	bs/year)		
EMC			Concentration (mg/L)		
I		•	ous Acres (acres)		
P	Annual Ra				
A	Watershee	d Area (a	cres)		

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Area E Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.87 Total Area = 0.203 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout			
	(lbs)	(lbs)	(%)	(lbs)	(lbs)			
Total Nitrogen (N)	0.070	0.070	0	0.00	0.070			
Total Phosphorus (P)	0.014	0.014	0	0.00	0.014			
Total Suspended Solids	3.728	3.7	5	0.19	3.5			
Lead	0.005	0.005	0	0.00	0.005			
Copper	0.001	0.001	0	0.00	0.001			
Zinc	0.005	0.005	0	0.00	0.005			
Lin 1		Pollutant Load In						
Sum L		Sum of Pollutant Load to this BMP						
RR	Removal rate in							
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area E Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.87 Total Area = 0.203 acres

BMP: Water Quality Structure

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)			
	(103)	(103)	(70)	(IDS)	(103)			
Total Nitrogen (N)	0.070	0.070	18.3	0.01	0.057			
Total Phosphorus (P)	0.014	0.014	66.9	0.01	0.005			
Total Suspended Solids	3.542	3.5	50	1.77	1.8			
Lead	0.005	0.005	46.5	0.00	0.003			
Copper	0.001	0.001	56.2	0.00	0.001			
Zinc	0.005	0.005	85.3	0.00	0.001			
Lin 1	Pollutant Load In	Pollutant Load In						
Sum L	Sum of Pollutant Load to this BMP							
RR	Removal rate in pe	Removal rate in percentage						
Lout	Pollutant Load out	of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area E Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.87 Total Area = 0.203 acres

BMP: Infiltration System

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)			
Total Nitrogen (N)	0.057	0.057	27	0.02	0.042			
Total Phosphorus (P)	0.005	0.005	33	0.00	0.003			
Total Suspended Solids	1.771	1.8	90	1.59	0.2			
Lead	0.003	0.003	32	0.00	0.002			
Copper	0.001	0.001	32	0.00	0.000			
Zinc	0.001	0.001	32	0.00	0.000			
Lin 1	Pollutant Load	Pollutant Load In						
Sum L RR		Sum of Pollutant Load to this BMP						
Lout	Removal rate Pollutant Load	•						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Loading Calculation

Location: Area F Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.81 Total Area = 1.023 acres

Pollutant	Resid	<u>ntial</u>		<u>Weig</u>	<u>ıhted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	1.023	1.900		1.900	0.334
Total Phosphorus (P)	1.023	0.383		0.383	0.067
Total Suspended Solids	1.023	101.0		101.0	17.7
Lead	1.023	0.144		0.144	0.025
Copper	1.023	0.033		0.033	0.006
Zinc	1.023	0.135		0.135	0.024
	L = 0.226	5 * EMC * [0.15 + 0.	75*I] * P *A		
L	Pollution I	oading (lbs/year)			
EMC		t Mean Concentration			
I		Impervious Acres (a	cres)		
P	Annual Ra				
A	watershe	Area (acres)			

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Area F Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.81 Total Area = 1.023 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout			
	(lbs)	(lbs)	(%)	(lbs)	(lbs)			
Total Nitrogen (N)	0.334	0.334	0	0.00	0.334			
Total Phosphorus (P)	0.067	0.067	0	0.00	0.067			
Total Suspended Solids	17.735	17.7	5	0.89	16.8			
Lead	0.025	0.025	0	0.00	0.025			
Copper	0.006	0.006	0	0.00	0.006			
Zinc	0.024	0.024	0	0.00	0.024			
Lin 1		Pollutant Load In						
Sum L		Sum of Pollutant Load to this BMP						
RR	Removal rate in							
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area F Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.81 Total Area = 1.023 acres

BMP: Water Quality Structure

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout			
	(lbs)	(lbs)	(%)	(lbs)	(lbs)			
Total Nitrogen (N)	0.334	0.334	18.3	0.06	0.273			
Total Phosphorus (P)	0.067	0.067	66.9	0.04	0.022			
Total Suspended Solids	16.849	16.8	50	8.42	8.4			
Lead	0.025	0.025	46.5	0.01	0.014			
Copper	0.006	0.006	56.2	0.00	0.003			
Zinc	0.024	0.024	85.3	0.02	0.003			
Lin 1	Pollutant Load	Pollutant Load In						
Sum L	Sum of Polluta	Sum of Pollutant Load to this BMP						
RR	Removal rate i	n percentage						
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area F Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.81 Total Area = 1.023 acres

BMP: Infiltration System

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)			
	(103)	(103)		(103)	(103)			
Total Nitrogen (N)	0.273	0.273	27	0.07	0.199			
Total Phosphorus (P)	0.022	0.022	33	0.01	0.015			
Total Suspended Solids	8.424	8.4	90	7.58	0.8			
Lead	0.014	0.014	32	0.00	0.009			
Copper	0.003	0.003	32	0.00	0.002			
Zinc	0.003	0.003	32	0.00	0.002			
Lin 1	Pollutant Load	In						
Sum L	Sum of Polluta	Sum of Pollutant Load to this BMP						
RR	Removal rate i	n percentage						
Lout	Pollutant Load	out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Loading Calculation

Location: Area G Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.83 Total Area = 0.930 acres

Pollutant	<u>Residential</u>		<u>Weighted</u>		
	Α	EMC	EMC	L	
	(acres)	(mg/L)	(mg/L)	(lbs/yr)	
Total Nitrogen (N)	0.930	1.900	1.900	0.310	
Total Phosphorus (P)	0.930	0.383	0.383	0.062	
Total Suspended Solids	0.930	101.0	101.0	16.5	
Lead	0.930	0.144	0.144	0.023	
Copper	0.930	0.033	0.033	0.005	
Zinc	0.930	0.135	0.135	0.022	
L EMC I P A	L = 0.2266 * EMC * [0.15 + 0.75*I] * P *A Pollution Loading (lbs/year) Mean Event Mean Concentration (mg/L) Fraction of Impervious Acres (acres) Annual Rainfall (in) Watershed Area (acres)				

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Area G Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.83 Total Area = 0.930 acres

BMP: **Deep Sump Catch Basins**

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)		
	(105)	(105)	(70)	(IDS)	(IDS)		
Total Nitrogen (N)	0.310	0.310	0	0.00	0.310		
Total Phosphorus (P)	0.062	0.062	0	0.00	0.062		
Total Suspended Solids	16.474	16.5	5	0.82	15.7		
Lead	0.023	0.023	0	0.00	0.023		
Copper	0.005	0.005	0	0.00	0.005		
Zinc	0.022	0.022	0	0.00	0.022		
Lin 1	Pollutant Load In						
Sum L	Sum of Pollutant Load to this BMP						
RR	Removal rate in percentage						
Lout	Pollutant Load out of BMP						

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area G Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.83 Total Area = 0.930 acres

BMP: Water Quality Structure

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout
	(lbs)	(lbs)	(%)	(lbs)	(lbs)
Total Nitrogen (N)	0.310	0.310	18.3	0.06	0.253
Total Phosphorus (P)	0.062	0.062	66.9	0.04	0.021
Total Suspended Solids	15.651	15.7	50	7.83	7.8
Lead	0.023	0.023	46.5	0.01	0.013
Copper	0.005	0.005	56.2	0.00	0.002
Zinc	0.022	0.022	85.3	0.02	0.003
Lin 1	Pollutant Load I	n			
Sum L	Sum of Pollutan	t Load to this	ВМР		
RR	Removal rate in	percentage			
Lout	Pollutant Load o	ut of BMP			

Notes:

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Location: Area G Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.83 Total Area = 0.930 acres

BMP: Infiltration System

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout
	(lbs)	(lbs)	(-)	(lbs)	(lbs)
Total Nitrogen (N)	0.253	0.253	27	0.07	0.185
Total Phosphorus (P)	0.021	0.021	33	0.01	0.014
Total Suspended Solids	7.825	7.8	90	7.04	0.8
Lead	0.013	0.013	32	0.00	0.009
Copper	0.002	0.002	32	0.00	0.002
Zinc	0.003	0.003	32	0.00	0.002
Lin 1	Pollutant Load				
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in				
Lout	Pollutant Load	out of BMP			

Notes:

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Loading Calculation

Location: Northwest Portion to Area Drains Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.23 Total Area = 0.251 acres

Pollutant	Resid	<u>ential</u>		<u>Weig</u>	<u>hted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.251	1.900		1.900	0.035
Total Phosphorus (P)	0.251	0.383		0.383	0.007
Total Suspended Solids	0.251	101.0		101.0	1.9
Lead	0.251	0.144		0.144	0.003
Copper	0.251	0.033		0.033	0.001
Zinc	0.251	0.135		0.135	0.002
	L = 0.226	6 * EMC	* [0.15 + 0.75*I] * P *A		
L	Pollution L	_oading (I	bs/year)		
EMC	Mean Event Mean Concentration (mg/L)				
I	Fraction of Impervious Acres (acres)				
P	Annual Ra				
A	Watershee	d Area (a	cres)		

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management* by Debo & Reese

Loading Calculation

Location: Areas to Existing Infiltration Systems Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.62 Total Area = 4.385 acres

Pollutant	Resid	<u>ential</u>		<u>Weig</u>	<u>ihted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	4.385	1.900		1.900	1.161
Total Phosphorus (P)	4.385	0.383		0.383	0.234
Total Suspended Solids	4.385	101.0		101.0	61.7
Lead	4.385	0.144		0.144	0.088
Copper	4.385	0.033		0.033	0.020
Zinc	4.385	0.135		0.135	0.082
	L = 0.226	6 * EMC [:]	* [0.15 + 0.75*I] * P *A		
L	Pollution L	_oading (I	bs/year)		
EMC	Mean Event Mean Concentration (mg/L)				
I	Fraction of Impervious Acres (acres)				
P	Annual Ra	` ,			
Α	Watershe	d Area (ad	cres)		

Notes:

1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese

Location: Areas to Existing Infiltration Systems Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.62 Total Area = 4.385 acres

BMP: Infiltration System

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout	
	(lbs)	(lbs)	(-)	(lbs)	(lbs)	
Total Nitrogen (N)	1.161	1.161	27	0.31	0.848	
Total Phosphorus (P)	0.234	0.234	33	0.08	0.157	
Total Suspended Solids	61.720	61.7	90	55.55	6.2	
Lead	0.088	0.088	32	0.03	0.060	
Copper	0.020	0.020	32	0.01	0.014	
Zinc	0.082	0.082	32	0.03	0.056	
Lin 1	Pollutant Load	In				
Sum L	Sum of Polluta	nt Load to this I	ВМР			
RR	Removal rate i	Removal rate in percentage				
Lout	Pollutant Load	out of BMP				

Notes:

- 1. Pollution loading calculated using Municipal Stormwater Management by Debo & Reese
- 2. Pollutant removal rates for Infiltration Practices taken from *Municipal Stormwater Management* by Debo & Reese, Table 13-13
- 3. Pollutant removal rates for Contechs CDS Unit water quality structure taken from NJCAT TSS Approval letter, January 9, 2015
- 4. Pollutant removal rates for Deep Sump Catch Basins taken from MassDEP Stormwater Handbook Volume 2 Structural BMP Specifications

Available Models i

CDS Model	Treatment Capacity³ (cfs)	Maximum Sediment Storage Capacity (CF)
1515	1.0	26
w/ 1' added sump	1.0	33
w/ 2' added sump	1.0	40
w/ 3' added sump	1.0	47
2015_4	1.4	50
w/ 1' added sump	1.4	63
w/ 2' added sump	1.4	75
w/ 3' added sump	1.4	88
2015	1.4	79
w/ 1' added sump	1.4	98
w/ 2' added sump	1.4	118
2020	2.2	90
w/ 1' added sump	2.2	110
w/ 2' added sump	2.2	129
2025	3.2	97
w/ 1' added sump	3.2	117
w/ 2' added sump	3.2	136
3020	3.9	134
w/ 1' added sump	3.9	163
w/ 2' added sump	3.9	191
3030	6.1	157
w/ 1' added sump	6.1	185
w/ 2' added sump	6.1	213
4030	7.9	329
w/ 1' added sump	7.9	379
w/ 2' added sump	7.9	429
4040	12.4	381
w/ 1' added sump	12.4	431
w/ 2' added sump	12.4	482

- 1. Structure diameter represents the typical inside dimension of the concrete structure. Offline systems will require additional concrete diversion components
- 2. Depth below pipe can vary to accommodate site specific design. Depth below pipe invert represents the depth from the pipe invert to the inside bottom of concrete structure.
- 3. Treatment Capacity is based on laboratory testing using OK-110 (average d50 particle size of approximately 100 microns) and a 2400 micron screen.

Sediment Depths Indicating Required Servicing*					
CDS Model	Standard Sediment Depth (in.)	w/ 1' added Sump Sediment Depth (in.)	w/ 2' added Sump Sediment Depth (in.)		
1515	18	27	36		
2015_4	18	30	42		
2015	18	30	42		
2020	18	30	42		
2025	18	30	42		
3020	18	30	42		
3030	18	39	42		
4030	27	39	51		
4040	27	39	51		

^{*} Based on 75% capacity of isolated sump.

APPENDIX G

64 Danbury Road Wilton, Connecticut

Maintenance and Inspection Plan

December 2023

The initial inspection will be made during an intense rainfall to check the adequacy of the yard drains, catch basins, roof leaders, piping, hydrodynamic separator, infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures:</u> The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator:</u> The Contech CDS units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration:</u> The underground infiltration systems will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader:</u> The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plant species or tree saplings.

Stormwater System Outfalls: The stormwater system outfalls shall be inspected two times annually as well as after every major storm, for slope integrity, soil moisture, vegetated health, soil stability, soil compaction, soil erosion, ponding and sediment accumulation. If the rip rap has been displaced, undermined or damaged, it should be replaced immediately. The channel immediately below the outlet should be checked to see that erosion is not occurring. The downstream channel will be kept clear of obstructions, such as fallen trees, debris, leaves and sediment that could change flow patterns and/or tail water depths in pipes. Repairs must be carried out immediately to avoid additional damage to the outlet protection apron.

Drainage Structures Inspection

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand and debris from catch basins as necessary and dispose of legally.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

Hydrodynamic Separator

The Contech CDS units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

Underground Infiltration

The underground infiltration system shall be inspected annually and will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

Level Spreader

The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plant species or tree saplings.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

Stormwater System Outfalls

The stormwater system outfalls shall be inspected two times annually as well as after every major storm, for slope integrity, soil moisture, vegetated health, soil stability, soil compaction, soil erosion, ponding and sediment accumulation. If the rip rap has been displaced, undermined or damaged, it should be replaced immediately. The channel immediately below the outlet should be checked to see that erosion is not occurring. The downstream channel will be kept clear of obstructions, such as fallen trees, debris, leaves and sediment that could change flow patterns and/or tail water depths in pipes. Repairs must be carried out immediately to avoid additional damage to the outlet protection apron.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

APPENDIX H



64 Danbury Road

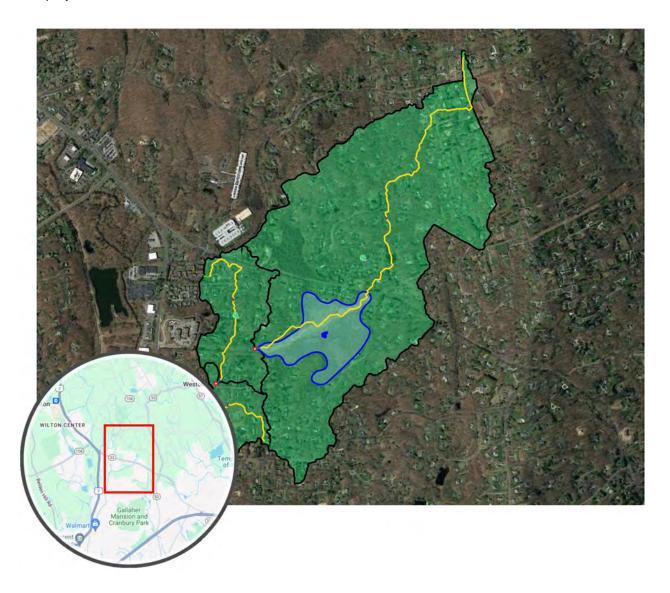
December 22, 2023

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Default Scenario	
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Project Description

The project is located at 14 Wilton Hunt Rd, Wilton, CT 06897. The site is 435.005 acres in size.



Purpose

The purpose of this hydrology study is to determine the peak runoff rates for pre-development and post-development conditions.

Methodology Used

The HEC-HMS version 4.5 computer software was used in this hydrology study. The **SCS Curve Number** infiltration (loss) method and **SCS Unit Hydrograph** runoff (transform) method was used for determining the stormwater runoff. Multiple routing method were used for routing the stormwater.

The following scenarios were analyzed in this hydrology study:

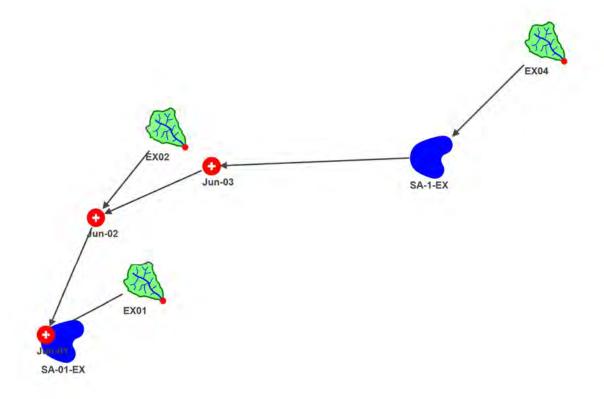
Default Scenario

This scenario contains:

- 3 delineated subbasin areas and corresponding lag time flow paths.
- 3 connecting junctions.
- 2 storage areas.

Default Scenario

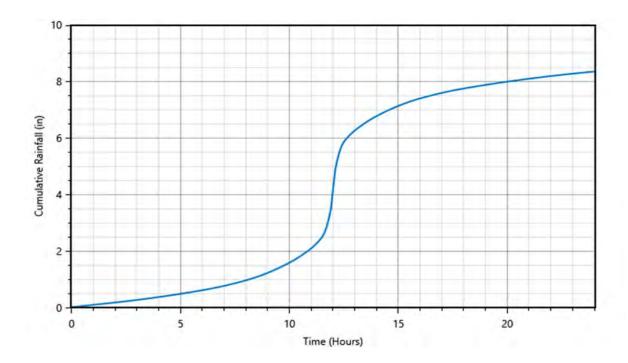
Watershed Routing Diagram



Design Storm

Precipitation type: SCS Storm SCS storm distribution: Type III

Rainfall depth: 8.35 in



Watershed Summary

Subbasin ID	Drainage Area	Initial Abstraction	Curve Number	Impervious Surface	Lag Time	Peak Discharge
	(acres)	(in)		(%)	(minutes)	(cfs)
EX01	32.493	0.65	75.53	18.32	19.01	123.43
EX02	51.222	0.74	73.10	9.77	38.76	126.93
EX04	351.290	0.68	74.63	9.77	46.12	810.02

Subbasins

Subbasin ID:		EX01			
Scenario:		Default Scenari	0	Depth	Volume
Peak discharge	::	97.2 cfs	Time of peak:	31 Oct 2023, 12:16	
Drainage area:		32.493 acres	Total rainfall:	8.35 in	22.62293 ac-ft
Initial abstract	ion:	0.65 in	Losses:	4.18 in	6.48476 ac-ft
Curve Number	:	75.53	Precip excess:	4.17 in	16.13817 ac-ft
Impervious sur	face:	18.32%	Direct runoff:	4.17 in	16.06 ac-ft
Peaking factor	:	484	Baseflow:	0.00 in	0.00 ac-ft
Lag time:		19.01 minutes	Total runoff:	4.17 in	16.06 ac-ft
Weighted Curv					
Area (acres)	Area (%)	CN	Description		
1.082	3.33	55.00	Undeveloped, Deciduous Forest		
3.723	11.46	85.83	Developed, Medium Density		
4.817	14.82	79.26	Developed, Low Density		
0.333	1.03	55.00	Undeveloped, Mixed Forest		
22.539	69.36	74.32	Developed, Open Space		
32.493	100.00	75.53	Weighted Average		
Time of Conce	ntration (TOC)	/ Lag time Calcu	lations		
TOC (min)	Length (ft)	Slope (ft/ft)	Velocity (ft/s)	Description	
18.49	100.00	0.02572	0.5958	Sheet Flow	
12.65	2,326.81	0.03610	6.2743	Shallow Concentrated	l Flow
0.54	100.00	0.00854	3.0524	Channel Flow	
	2,526.81	Total	Lag Time = 19.01 minutes		

Subbasin ID:		EX02					
Scenario:		Default Scenario		Depth	Volume		
Peak discharge: 57.7 cfs		Time of peak:	31 Oct 2023, 13:20				
Drainage area:		51.222 acres	Total rainfall:	8.35 in	35.62667 ac-f		
Initial abstract	ion:	0.74 in	Losses:	3.63 in	12.39812 ac-f		
Curve Number	:	73.10	Precip excess:	4.72 in	23.22855 ac-f		
Impervious sur	face:	9.77%	Direct runoff:	4.72 in	22.98 ac-ft		
Peaking factor	;	484	Baseflow:	0.00 in	0.00 ac-ft		
Lag time:		38.76 minutes	Total runoff:	4.72 in	22.98 ac-ft		
Weighted Curv	o Numbor Ca	lculations					
Area (acres)	Area (%)	CN	Description				
5.369	10.48	100.00	Wetlands, Forested				
4.067	7.94	56.83	Undeveloped, Deciduous Forest				
0.201	0.39	85.00	Developed, Medium Density				
7.076	13.82	76.28	Developed, Low Density				
0.024	0.05	92.00	Developed, High Density				
7.278	14.21	59.16	Undeveloped, Mixed Forest				
27.207	53.12	73.02	Developed, Open Space				
51.222	100.00	73.10	Weighted Average				
	· · · · · · · · · · · · · · · · · · ·) / Lag time Calcu					
TOC (min)	Length (ft)	Slope (ft/ft)	Velocity (ft/s)	Description			
13.98	100.00	0.05172	0.8448	Sheet Flow	d Elson		
34.69	3,047.55	0.00824	2.9982	Shallow Concentrate	a Flow		
15.92	100.00	0.00001	0.1044	Channel Flow			
64.59	3,247.55	Total	Lag Time = 38.76 minutes				

Subbasin ID:		EX04					
Scenario:		Default Scenario		Depth	Volume		
Peak discharge	ak discharge: 349.6 cfs Time of peak:		31 Oct 2023, 13:40				
Drainage area:	rainage area:		Total rainfall:	8.35 in	244.44346 ac-f		
Initial abstracti	ion:	0.68 in	Losses:	3.75 in	80.18041 ac-ft		
Curve Number	:	74.63	Precip excess:	4.60 in	164.26305 ac-1		
Impervious sur	face:	9.77%	Direct runoff:	4.54 in	162.21 ac-ft		
Peaking factor:	:	484	Baseflow:	0.00 in	0.00 ac-ft		
Lag time:		46.12 minutes	Total runoff:	4.54 in	162.21 ac-ft		
Weighted Curv	e Number Ca	lculations					
Area (acres)	Area (%)	CN	Description				
54.559	15.53	100.00	Wetlands, Forested				
67.639	19.25	57.74	Undeveloped, Deciduous Forest				
8.570	2.44	87.94	Developed, Medium Density				
0.537	0.15	74.00	Agricultural, Pasture/Hay				
0.241	0.07	100.00	Wetlands, Non-Forested				
55.533	15.81	79.00	Developed, Low Density				
30.628	8.72	58.95	Undeveloped, Mixed Forest				
133.584	38.03	73.70	Developed, Open Space				
351.290	100.00	74.63	Weighted Average				
Time of Concer	ntration (TOC)	/ Lag time Calcu	lations				
TOC (min)	Length (ft)	Slope (ft/ft)	Velocity (ft/s)	Description			
19.54	100.00	0.02239	0.5559	Sheet Flow			
56.39	8,099.02	0.02202	4.9003	4.9003 Shallow Concentrated Flow			
0.93	100.00	0.00292	1.7833 Channel Flow				
76.86	8,299.02	Total	Lag Time = 46.12 minutes				

