





141 Danbury Road Wilton, Connecticut

## **ENGINEERING REPORT**

Prepared For:

FDSPIN 141 DR, LLC 1 North Water Street, Suite 100 South Norwalk, CT 06854

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# Section 1 Introduction and Site Conditions

Tighe & Bond has prepared this report at the request of FDSPIN 141 DR LLC ( "Applicant"), to support their applications to the Town of Wilton Planning & Zoning Commission and Inlands Wetlands Commission for a proposed  $4\frac{1}{2}$  story multi-family residential building with 173 apartments.

The project site is located on a 4.28-acre parcel bounded by Danbury Road to the east, the Norwalk River to the west, and commercial properties to the north and south. The proposed development consists of the construction of a 173-unit residential building, atgrade parking, stormwater management systems, utility services, lighting, and associated landscaping. Refer to **Figure 1**, Site Location Map, in **Appendix A**.

Tighe & Bond has inspected the property and analyzed available soils, drainage, utility, wetland, and topographic information. Drainage calculations and stormwater management design have been prepared in accordance with the 2000 Connecticut Department of Transportation (CTDOT) Drainage Manual, and the Connecticut Department of Energy and Environmental (DEEP) Protection 2004 Stormwater Quality Manual. The drainage calculations include a hydrologic and hydraulic analysis of the existing conditions and the proposed development. Specifically, the calculations include an analysis of the on-site stormwater management measures and their performance in handling peak flow attenuation and pollutant removals. The report also includes a summary of the site floodplain management, the available existing and proposed utilities to serve the property, and the proposed soil erosion and sedimentation control measures incorporated during construction.

## 1.1 Existing Conditions

The existing site consists of a 47,000 square foot commercial building with at-grade parking. The 4.28-acre parcel is located within Wilton's DE-5 Design Enterprise District Zone. A significant portion of the site is impervious with paved parking areas, sidewalks, and building, with landscaping and lawns generally around the perimeter of the site. Utility services to the site include underground water, natural gas, overhead electric, and tele-data, connecting to service mains in Danbury Road.

The site is located on Danbury Road (Route 7) which is a north-south three lane State maintained major arterial roadway. The roadway is generally 40 feet wide along the frontage of the site with two lanes northbound and one lane southbound.

The topography of the site generally slopes from east to west towards the Norwalk River. Due to the lack of drainage structures within the property, stormwater runoff flows overland across the paved and landscaped surfaces. The Norwalk River runs adjacent to the western edge of the property, flowing from north to south. Approximately one third of the property lies within the Special Flood Hazard Zone AE of the Norwalk River.

## 1.2 Project Proposal

The proposed 4½ story multi-family residential building will be home to 173 apartments consisting of one-bedroom (37), two-bedroom (122), and three-bedroom (14) units. The

proposed building is situated in the central portion of the site, with driveway and parking areas along the northern and southern sides. The ground floor will include surface parking spaces (covered and uncovered) as well as utility/trash rooms and building access points. All uncovered parking will be screened from view by landscaping. The existing driveway into the property will be widened to accommodate the traffic to and from the site, with dedicated turning lanes onto Danbury Road. The western end of the property will be converted into green space with associated landscaping and walking paths along the Norwalk River. New utility services to the property are proposed including underground water, natural gas, electric, and tele-data.

Stormwater management will be accommodated on-site. Surface runoff will be collected in catch basins and inlet structures located throughout the site. Underground infiltration and porous pavement systems have been designed to reduce peak flows and provide stormwater treatment, prior to discharge into the Norwalk River. The stormwater management system has been designed to treat the water quality volume and remove a high level of pollutants.

### 1.3 Site Soils

The U.S. Department of Agriculture's National Resource Conservation Service (NRCS) Web Soil Survey indicates the following soil types are present on the site:

**Urban Land (307):** Urban land is mostly covered by streets, parking lots, buildings, and other structures of urban areas. Slopes range from 0 to 45 percent. No drainage class is assigned, and the complex does not meet hydric criteria.

**Rippowam Fine Sandy Loam (103):** This series consist of very deep, poorly drained loamy soils formed in alluvial sediments. They are nearly level soils on flood plains subject to frequent flooding. Slope ranges from 0 to 3 percent.

A copy of the NRCS Soil Resource Report is included in **Appendix B** of this report.

Soil permeability for the site was estimated to be 2 inches per hour for the design of the proposed stormwater management systems. Estimates were conservative based on the soil classifications observed in the soil exploration program previously performed on site by GZA Environmental, LLC. Permeability estimates will be confirmed in the field prior to the completion of construction documents. See **Appendix B** of this report for boring logs and observed groundwater elevations.

#### 1.4 Wetlands

Wetlands soils were delineated and flagged by William Kenny Associates LLC, William L. Kenny, soil scientist on March 15, 2021 and located in the field by D'Andrea Surveying & Engineering, P.C. Wetland flags and limits are depicted on the project drawing sheets.

# Section 2 Stormwater Management

## 2.1 Existing Site Hydrologic Analysis

To review the impact of the proposed development on the existing site, an existing conditions hydrologic analysis was performed. Under existing conditions, stormwater runoff from the site generally flows from east to west towards the Norwalk River. Since there are no catch basins or inlet structures on the existing site, runoff flows overland and discharges to the river at the western end of the site. The edge of the river along the property has been designated as the design point for the analysis. The drainage area of the existing site has been delineated into sub-watershed areas. The Existing Conditions Watershed Map (Figure WM-01) is included in **Appendix C** of this report.

Impervious and pervious areas, weighted curve number, and time of concentration were calculated for each watershed area and developed into hydrologic model to determine the project's peak flow and volume, as part of the comparative hydrology analysis. Precipitation data for the hydrologic modeling were developed from NOAA's Atlas 14 Point Precipitation Frequency Estimates online utility. The site specific precipitation depths for a 24-hour durations storm are shown in **Table 2-1**.

Table 2-1
24-hour Duration Precipitation Depth

	2-Year	10-Year	25-Year	50-Year	100-Year
Depth (in)	3.54	5.40	6.57	7.44	8.37

A breakdown of existing watershed areas, existing volumetric hydrographs, and existing watershed map are included in **Appendix C** of this report.

#### 2.1.1 Floodplain Management

The Federal Emergency Management Agency's Flood Insurance Rate Map (FIRM) for Fairfield County, effective June 18, 2010 and revised October 16, 2013 shows a portion of the site within the floodway and Zone AE of the Norwalk River, as shown in **Figure 2** in **Appendix A**. Refer to **Section 3 Floodplain Management & Hydraulics** of this report for additional information.

## 2.2 Proposed Site Hydrologic and Hydraulic Analysis

A stormwater management system has been designed for the proposed development to reduce peak flows and improve water quality for the site. The proposed drainage system consists of catch basins and inlets throughout the development site as well as water quality structures, underground infiltration systems, porous pavement systems, and outlet protection. The stormwater management system will maintain existing drainage patterns and utilize Best Management Practices for stormwater treatment.

Under proposed conditions, drainage patterns will generally remain the same, flowing in a westerly direction and ultimately discharging to the Norwalk River. Drainage structures

have been located throughout the site to collect stormwater runoff from paved and landscaped surfaces. Due to the location of the proposed building in the central portion of the site, the drainage system has been split into northern and southern systems around the building. Infiltration systems and porous pavement systems have been designed and located on either side of the proposed building, promoting infiltration and treatment of the stormwater runoff. These systems converge into a single outlet pipe located at the western end of the building, with a single outlet located at the southwestern corner of the site. A riprap apron and level spreader have been designed to reduce outlet velocities and provide erosion control prior to discharge to the Norwalk River.

#### 2.2.1 Proposed Site Hydrology

The proposed conditions hydrologic analysis consists of sub-watershed areas at each inlet structure of the development property. For each proposed watershed area, weighted curve numbers and times of concentration were calculated and utilized in the proposed conditions hydrologic model. The infiltration and porous pavement systems were also modeled to determine the effectiveness in reducing peak discharges from the site.

**Table 2-2** provides a summary of the peak discharges under existing and proposed conditions for the 2, 10, 25, 50, and 100 year storm events.

Table 2-2
Summary of Stormwater Peak Discharge (cfs)

		Storm Frequency (Years)				
Discharge Location	Condition	2	10	25	50	100
Norwalk River	Existing	7.662	13.50	17.25	20.05	23.05
	Proposed	1.636	6.762	10.69	13.64	17.35

The proposed conditions watershed map, curve number and time of concentration worksheets, and volumetric hydrographs are included in **Appendix D**.

#### 2.2.2 Water Quality Volume

The water quality volume (WQV) is equivalent to the first inch of runoff from the site that should be captured and treated in order to remove a majority of stormwater pollutants on an average annual basis. For the proposed development, the infiltration and porous pavement systems have been designed to provide the required WQV. **Table 2-3** summarizes the required and provided WQV for the site.

Table 2-3
Summary of Water Quality Volume (cu ft)

Required WQV		10,603
	North Infiltration System	2,912
Drovided WOV	South Infiltration System	4,284
Provided WQV	North Porous Pavement System	2,191
	South Porous Pavement System	1,415
Total Provided WQV		10,802

The water quality volume calculation sheets are included in **Appendix E**.

#### 2.2.3 Hydraulic Capacity and Outlet Velocity

The stormwater collection system has been designed to convey the 25-year storm event as required by the CTDOT 2000 Drainage Manual. The system was designed by analyzing sub-areas corresponding to each inlet structure and calculating weighted runoff coefficients and times of concentration. These values were entered into a storm sewers model using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3. Based upon this analysis, the proposed storm system has the capacity to convey the 25-year storm event. At the outlet of the system, a riprap apron and level spreader have been designed to reduce outlet velocities and prevent scour along slopes. Hydraulic calculation worksheets and storm sewers output results are included in **Appendix F**.

## 2.3 Method of Hydrology and Hydraulic Analysis

The following storm drainage design criteria were used for all drainage pipe systems:

- 1. Design storm rainfall data from NOAA Atlas 14 Point Precipitation Frequency Estimates
- 2. Piped storm drainage system and the outlets are designed for a 25-year storm event.
- 3. Minimum time of concentration = 5 minutes
- 4. For SCS peak flow calculations, Curve Number were as follows:
  - a. Impervious (Pavement/Roof Areas) = 98
  - b. Landscaped and Lawn Areas = 69
- 5. For rational peak flow calculations, runoff coefficients were as follows:

- a. Impervious (Pavement/Roof) areas = 0.95
- b. Landscaped and Lawn Areas = 0.30
- 6. Minimum diameter of pipes = 12 inches, excluding roof leaders, underdrains, yard drains and foundation drains
- 7. Minimum pipe slope = 0.5 percent
- 8. Watershed areas delineated using polylines in AutoCAD Civil 3D 2018.
- 9. Comparative hydrology analyzed using Hydraflow Hydrographs Extension for AutoCAD Civil 3D 2018, Version 2018.3
- 10. Storm drainage system analyzed using Hydraflow Storm Sewers Extension for AutoCAD Civil 3D 2018, Version 2018.3

## 2.4 Best Management Practices

The stormwater management plan for the proposed site uses "Best Management Practices" (BMPs) to remove a high percentage of sediments in accordance with the Connecticut Department of Energy and Environmental Protection "Stormwater General Permit Criteria".

The BMPs include:

<u>Catch Basins and Yard Drains with Sumps:</u> Catch basins and yard drains with sumps collect sediment and prevent discharge of oil and other pollutants into the storm drainage system. All new catch basins and yard drains on-site will have 24-inch sumps.

<u>Hydrodynamic Separators:</u> Hydrodynamic separators serve as pretreatment and prevent transport of oils and sediment further downstream. The proposed stormwater management system utilizes Contech CDS units prior to discharge into the underground infiltration systems. The Contech CDS units have been sized in accordance with the 2004 CTDEEP Stormwater Quality Manual. Sizing calculations are provided in **Appendix E.** 

<u>Underground Infiltration</u>: Underground Infiltration serves as a primary treatment practice, reduces peak flow rates, and promotes groundwater recharge. The proposed stormwater management system utilizes concrete chambers surrounded by stone and filter fabric and an outlet control structure designed to attenuate peak flows.

<u>Level Spreader</u>: Level Spreaders serve as a secondary treatment practice that are utilized to reduce stormwater discharge velocities to non-erosive levels.

## 2.5 Pollutant Loading Analysis

Pollutant loadings for the existing and proposed conditions were calculated using the method prescribed by Debo and Reese in "Municipal Stormwater Management", 1995. This method determines the mass of pollutant loading by inputting the fraction of

impervious area, the contributing area, the mean annual rainfall, and the event mean concentration of pollutant (EMC). The EMC is based upon the pollutant analyzed and the general characteristic of the contributing area – residential, commercial, or open space.

For the proposed conditions, the contributing area was further broken down into contributing areas to certain best management practices (BMPs). Pollutant loading reductions were taken at certain BMPs, depending upon the removal efficiency of the BMP as stated in the 2003 edition of Debo and Reese. Pollutant removal efficiencies for proprietary products were taken from a report entitled "Final Report: Stormwater Treatment Devices Section 319 Project" submitted to the Connecticut Department of Environmental Protection, Bureau of Water Management by the University of Connecticut Department of Natural Resources Management and Engineering, April 15, 2002. This report provides results of field testing for pollutant removal on different types of proprietary stormwater treatment devices installed throughout the State of Connecticut. Based upon these pollutant reductions, we have determined that pollutant loadings will be less for the proposed conditions, as shown in **Table 2-4** below. The pollutant loading calculation sheets are included in **Appendix E**.

Table 2-4
Pollutant Loading Summary

	Pollutant						
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre-Treatment	lb/yr/1-in	0.456	0.092	24.226	0.035	0.008	0.032
Proposed, Post-Treatment	lb/yr/1-in	0.284	0.037	5.121	0.015	0.003	0.009
Reduction, Pre to Post Treat		38%	59%	79%	57%	60%	71%

## 2.6 Stormwater Maintenance and Inspection Schedule

Stormwater management systems require periodic maintenance to ensure they function as designed. The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, roof leaders, piping, hydrodynamic separators, underground infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures:</u> The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment.

Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator:</u> The Contech CDS Units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand, and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration:</u> The underground infiltration system will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader:</u> The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plant species or tree saplings.

<u>Pavement:</u> Paved areas shall be swept periodically by the Owner to clean trash and other debris. The Owner will sweep paved areas on its property in the spring to remove winter accumulations of road sand.

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

Maintenance & Inspection Forms are included in **Appendix G.** 

# Section 3 Floodplain Management & Hydraulics

## 3.0 Background

The Norwalk River was studied by FEMA as a part of the Flood Insurance Study (FIS) for Fairfield County, dated June 18, 2010. The 2010 FIS updated the modeling of the Norwalk River that was originally done for the 1982 Town of Wilton Flood Insurance Study by incorporating Letters of Map Revision issued between 1982 and 2010. The river system itself was not restudied. It is important to note that the vertical datum of the two studies was changed from the National Geodetic Vertical Datum of 1929 (NGVD29, prior to 1973 also known as the Sea Level Datum of 1929) to the North American Vertical Datum of 1988 (NAVD88). The modeling data provided by FEMA is in the NGVD29 datum and the reported water surface elevations in the 2010 FIS are in the NAVD88 datum.

The National Oceanic and Atmospheric Administration (NOAA) offers an online utility, VERTCON, to calculate the difference between the two datums at a given latitude and longitude coordinate. In the area of the project, the NGVD29 datum is 1.07 feet higher than the NAVD88 datum. Refer to the VERTCON conversion in **Appendix H**.

## 3.1 Basis of Modeling

Tighe & Bond obtained a copy of the hydraulic model from FEMA for the Norwalk River. This model was used for the hydraulic analysis of the project since it is the effective FEMA model for the project area. The model was developed using the U.S. Army Corps of Engineers HEC-RAS hydraulic analysis modeling environment.

#### 3.1.1 Calibrated Model

To verify the accuracy of the modeling provided by FEMA, a model was created to replicate the data in the FIS. This is the calibrated model, also known as the duplicate effective model. The calibrated model encompasses the Norwalk River, generally spanning from Wolfpit Road to Kent Road in Wilton, corresponding with cross sections O and K of the FIS, respectively. The project site at 141 Danbury Road falls between cross sections O and N of the model. The comparison of the 100-year (1% chance) calibrated model water surface elevations with the elevations reported in the FIS Floodway Table are summarized in **Table 3-1**. The output table of the calibrated model is included in **Appendix H**.

Table 3-1
Calibrated Model Output

		Water Surface Elevation (NAVD88		
FIS Cross Section Identifier	Calibrated Model Cross Section Number	Floodway Data Table	Calibrated Model	
K	21745	123.4	123.41	
L	22765	130.6	130.57	
М	24525	138.8	138.69	
N	24597	141.2	140.19	
0	29920	153.1	152.89	

As shown in the table, the water surface elevations of the Calibrated Model closely mirror the values reported in the FIS Floodway Table. Slight variations in water surface elevations can be attributed to the differences between the HEC-2 and HEC-RAS modeling environments. The effective modeling and data provided by FEMA of the Norwalk River is in or has been developed from HEC-2 modeling. The HEC-RAS modeling environment is the successor to HEC-2 and is FEMA's current standard for flood studies. Based on the results shown, the Calibrated Model is suitable for modeling the proposed conditions of the project.

### 3.2 Flow Rates

The established flow rates for the Norwalk River are documented in Volume 1 of the FIS. Tighe & Bond is not challenging the flow rates established by the FIS and will be using the rates for modeling existing and proposed conditions. The flow rates for the river at the location of the site based on the FIS are summarized in **Table 3-2.** See **Appendix H** for a copy of the Norwalk River discharges included in the FIS.

Table 3-2
FIS Norwalk River Flow Rates at the Site

Return Frequency (years)	Annual Chance Probability	Flow Rate (cfs)
10	10%	2,980
50	2%	5,840
100	1%	7,455
500	0.2%	12,505

## 3.3 Existing Conditions Model

In order to best evaluate the impact of the proposed project, we inserted cross sections into the effective model to create an existing conditions model, also known as the corrected effective model. Due to the spacing of the sections in the effective model, the variations in floodplain topography are not accurately reflected in the vicinity of the project area. A total of four cross sections were added to the model and developed from the topographic survey of the site. Since the topographic survey is in the NAVD88 datum, the elevations of the geometry points were converted to NGVD29 before entering into the model. **Figure 3** in **Appendix A** shows the locations of the cross sections through the project site. **Table 3-3** summarizes the resulting water surface elevations of the added sections in the existing conditions model.

Table 3-3
Existing Conditions 100-Year Water Surface Elevations (NAVD88)

Existing Conditions Model Added Sections	100-year Water Surface Elevation (NAVD88)
28020	146.48
27930	146.47
27830	146.46
27790	146.46

Refer to **Appendix H** for the model output table of the existing conditions model.

## 3.4 Proposed Conditions Model

The next step in the modeling process is to determine the resultant water surface elevations of the project, including the proposed building and grading changes. We modified the appropriate sections in the Existing Conditions model accordingly. **Table 3-4a** and **3-4b** compare the proposed conditions results to the existing conditions for the 100-year and 10-year events, respectively.

Table 3-4a
100-Year Water Surface Elevation Comparison (NAVD88)

	100-year V	Vater Surface Elevation	(NAVD88)
Section	Existing	Proposed	Difference
28020	146.48	146.48	0.00
27930	146.47	146.47	0.00
27830	146.46	146.46	0.00
27790	146.46	146.46	0.00

Table 3-4b
10-Year Water Surface Elevation Comparison (NAVD88)

	10-year W	ater Surface Elevation	(NAVD88)
Section	Existing	Proposed	Difference
28020	144.93	144.93	0.00
27930	144.93	144.93	0.00
27830	144.92	144.92	0.00
27790	144.92	144.92	0.00

Based upon the hydraulic analysis, the proposed construction will not adversely impact 100-year and 10-year flood elevations along the Norwalk River.

## 3.5 Compliance with Local Floodplain Regulations

Section 29-9.F.7 of the Wilton Zoning Regulations requires the following:

- k. Equal Conveyance: Within the floodplain, except those areas which are tidally influenced, as designated on the Flood Insurance Rate Map (FIRM) for the community, encroachments resulting from filling, new construction or substantial improvements involving an increase in footprint of the structure, are prohibited unless the applicant provides certification by a registered professional engineer demonstrating, with supporting hydrologic and hydraulic analyses performed in accordance with standard engineering practice, that such encroachments shall not result in any (0.00 feet) increase in flood levels (base flood elevation). Work within the floodplain and the land adjacent to the floodplain, including work to provide compensatory storage shall not be constructed in such a way so as to cause an increase in flood stage or flood velocity.
- I. Compensatory Storage: The water holding capacity of the floodplain, except those areas which are tidally influenced, shall not be reduced. Any reduction caused by filling, new construction or substantial improvements involving an increase in footprint to the structure, shall be compensated for by deepening and/or widening of the floodplain, storage shall be provided on-site, unless easements have been gained from adjacent property owners; it shall be provided within the same hydraulic reach and a volume not previously used for flood storage; it shall be hydraulically comparable and incrementally equal to the theoretical volume of flood water at each elevation, up to and including the 100-year flood elevation, which would be displaced by the proposed project. Such compensatory volume shall have an unrestricted hydraulic connection to the same waterway or water body. Compensatory storage can be provided off-site if approved by the municipality.

#### 3.5.1 Equal Conveyance

As shown in Table 3-4a, there are no increases in the base flood elevation as a result of the project, so the equal conveyance requirement has been met.

#### 3.5.2 Compensatory Storage

The placement of the building columns and stairways within the floodplain would result in a loss of floodplain storage. Therefore, we propose revised grading to mitigate against the loss of flood storage volume. The grading as proposed results in a net cut of approximately 440 CY within the floodplain boundary, compensating for the approximate 40 CY occupied by the columns and stairways of the proposed building. The project as proposed would not decrease floodplain storage on-site.

## **Section 4 Site Utility Services**

#### 4.1 Water and Fire Protection Services

Water and fire protection services to the site will be provided by The Aquarion Water Company (Aquarion). Services to the proposed buildings will be fed from the reported 12-inch main located in Danbury Road. Existing hydrants are located in the vicinity of the project site on the west and east sides of Danbury Road.

The estimated daily water demand for the proposed residential development is approximately 48,450 gallons per day (GPD). The estimated peak hour demand is 101 gallons per minute (GPM), determined using a maximum-to-average-day ratio of 3.0.

#### 4.2 Electric Service

Electric service to the site is provided by Eversource Electric Company. Overhead primary service lines are located on the west side of Danbury Road and enter the site from the north.

### 4.3 Gas Service

Eversource Gas Company provides natural gas service to the project area. Eversource Gas Company maintains a 12-inch gas main located in Danbury Road.

Once the estimated peak demand for the total project is determined, Eversource Gas Company will provide a letter of service availability.

#### 4.4 Tele-Data and Cable TV Services

Frontier Communications provides local and long-distance telephone service to the project area and also offers high speed internet and business data services. The existing network in this area is composed of a combination of overhead lines and underground ductbanks. The existing service is provided overhead on the north side of the building. There is also an existing utility pole on the project site along the southerly property line that provides overhead services for 131 Danbury Road. These overhead wires and the routing for this building will need to be relocated in order to accommodate the proposed site improvements. Easements are not identified on the record documents for this utility pole or the service lines.

Telephone service to the proposed development would be provided underground from a utility pole in the adjacent street. The exact location of the service connections will be coordinated with the utility owner during the final design process.

Altice USA provides cable service as well as high speed internet access to the project area. The majority of the existing network runs overhead and follows the same alignment as the telephone service.

## **4.5 Sanitary Sewer Service**

The project site is located within the Wilton WPCA Sewershed.

Based on available Town maps, there is a 24-inch gravity sanitary sewer located in Danbury Road. The proposed building will connect to the existing sewage system by constructing a manhole over the existing sewer pipe in the adjacent street frontage. WPCA approval will be required for all sewer connections.

The projected wastewater flows associated with the proposed development were calculated based on the 173 residential units with 323 total bedrooms and a flow rate of 150 gallons per day (GPD) per bedroom. A peaking factor of 4 was applied to the average daily flows to estimate peak flows. **Table 4-1** below summarizes the projected average and peak daily sanitary sewer flows for the site. Refer to **Appendix J** for a full breakdown of the sanitary sewer flow calculations.

**Table 4-1 - Projected Average and Peak Daily Sanitary Sewer Flows** 

Wastewater Requirements					
Develo	pment	oment Design Criteria		Average	Peak Flow
Use	Units / Bedrooms	GPD	Unit	Daily Flow (GPD)	(GPM)*
Residential	173 / 323	150	Per Bedroom	48,450	135

<sup>\*</sup> Peak factor of 4 was applied to average daily flows to estimate peak flows; New England Interstate Water Pollution Control Commission, 2011.

# Section 5 Soil Erosion and Sedimentation Control

#### **5.1 SESC Narrative**

#### General

The proposed development is entitled "141 Danbury Road" in Wilton, Connecticut.

Estimated:

Project Start: Fall 2021

Project Completion: Spring 2022

Erosion Control Narrative refers to drawings C-501 through C-503.

The proposed site development will consist of building demolition, clearing and grubbing the existing site, excavation, construction of sedimentation/detention basins, and rough grading of building, parking areas, sidewalks and curbing.

The development is located in Wilton, Connecticut and is located on Danbury Road.

The stormwater management measures will address the stormwater quality once the site has been constructed and stabilized. Sedimentation and erosion control measures will be installed during construction which will minimize adverse impacts from construction activities.

All sedimentation and erosion control measures proposed for this development have been designed in accordance with the "2002 Connecticut Guidelines for Soil Erosion and Sedimentation Control" as published by the Connecticut Council on Soil Erosion and Water Conservation. Additional guidelines have also been followed that are available from the Connecticut Department of Environmental Protection as recommended for sedimentation control during construction activities.

#### Construction Sequence – Initial Phase

- 1. Conduct a pre-construction meeting with the Owner or Owner's Representative, Town Engineer, Design Engineer, Site Engineer, Contractor and Site Superintendent to establish the limits of construction, construction procedures and material stockpile areas.
- 2. Field stake the limits of construction.
- 3. Install all applicable soil and erosion control measures around the perimeter of the site to the extent possible. this will include siltation fence around the project as shown on the plans.
- 4. Install construction access road and anti-tracking pavement in the areas as shown on the plans. All construction access shall be into the site through the anti-tracking pads.

- 5. Establish temporary staging area.
- 6. Begin building demolition and pavement removal.
- 7. Construct the initial storm drainage and sedimentation trap as shown on the plans.
- 8. Install water quality systems and associated drainage network to the maximum extent practicable. Grade the area around the storm drainage system as necessary.
- 9. Begin rough roadway grading.
- 10. Install remaining drainage system to the extent necessary to provide positive drainage.
- 11. Begin installation of sanitary sewer system, water, and other utilities to extent necessary.
- 12. Provide silt fence/haybale barrier around soil stockpile area. Provide temporary vegetative cover (defined in erosion control notes) on all exposed surfaces.
- 13. Begin building construction.
- 14. Pave binder course on parking and driveways for non-porous pavement areas.
- 15. Establish temporary vegetative cover.
- Construct drainage and subbase for porous pavement and place porous pavement course

#### Construction Sequence – Final Phase

- 1. Repair perimeter sediment & erosion controls as needed.
- 2. Clean/replace controls from previous phase as needed.
- 3. Fine grade site.
- 4. Continue construction of building.
- 5. Complete construction of sidewalks.
- 6. Establish final vegetative cover and landscaping.
- 7. Pave surface course on roadways.
- 8. Remove erosion controls when site is stabilized.

### 5.2 Soil Erosion and Sedimentation Control Notes

- All sedimentation and erosion control measures shall be constructed in accordance with the standards and specifications of the "2002 Connecticut Guidelines for Soil Erosion and Sediment Control", DEP Bulletin No. 34, and all amendments and addenda thereto as published by the Connecticut Department of Environmental Protection.
- 2. Land disturbance shall be kept to the minimum necessary for construction operations.
- 3. All erosion control measures shall be installed as shown on the plan and elsewhere as ordered by the engineer.
- 4. All catch basins shall be protected with a silt sacks, haybale ring, silt fence or block and stone inlet protection throughout the construction period and until all disturbed areas are thoroughly stabilized.
- 5. Whenever possible, erosion and sediment control measures shall be installed prior to construction. See "Erosion Control Narrative".
- 6. Additional control measures shall be installed during the construction period as ordered by the engineer.
- 7. All sedimentation and erosion control measures shall be maintained in effective condition throughout the construction period.
- 8. Sediment removed shall be disposed of offsite or in a manner as required by the Engineer.
- 9. The construction contractor shall be responsible for construction and maintenance of all control measures throughout the construction period.
- 10. All disturbed areas to be left exposed for more than 30 days shall be protected with a temporary vegetative cover. Seed these areas with perennial ryegrass at the rate of 40 lbs. per acre (1 lb. per 1,000 sq. ft). Apply soil amendments and mulch as required to establish a uniform stand of vegetation over all disturbed areas.
- 11. The construction contractor shall utilize approved methods/materials for preventing the blowing and movement of dust from exposed soil surfaces onto adjacent properties and site areas.
- 12. The construction contractor shall maintain a supply of silt fence/haybales and antitracking crushed stone on site for emergency repairs.
- 13. All drainage structures shall be periodically inspected weekly by the construction contractor and cleaned to prevent the build-up of silt.
- 14. The construction contractor shall carefully coordinate the placement of erosion control measures with the phasing of construction.
- 15. Keep all paved surfaces clean. Sweep and scrape before forecasted storms.

- 16. Treat all unpaved surface with 4" minimum of topsoil prior to final stabilization.
- 17. Haybale barriers and silt fencing shall be installed along the toe of critical cut and fill slopes.
- 18. The contractor shall notify the Town officials prior to the installation of erosion controls, cutting of trees, or any excavation.
- 19. All trucks leaving the site must be covered.
- 20. Some control measures are permanent. These structures shall be cleaned and replenished at the end of construction. locations of the permanent control structures are shown on the drainage plans.
- 21. All sedimentation and erosion controls shall be checked weekly and/or after each rain fall event. Necessary repairs shall be made without delay.
- 22. Prior to any forecasted rainfall, erosion and sediment controls shall be inspected and repaired as necessary.
- 23. After all disturbed areas have been stabilized, erosion controls may be removed once authorization to do so has been secured from the Owner. Disturbed areas shall be seeded and mulched.
- 24. All embankment slopes 3:1 or greater to be stabilized with erosion control blanket, North American Green SC150BN or approved equivalent, unless otherwise noted on plans.

**APPENDIX A** 





141 DANBURY ROAD WILTON, CONNECTICUT

SITE LOCATION MAP

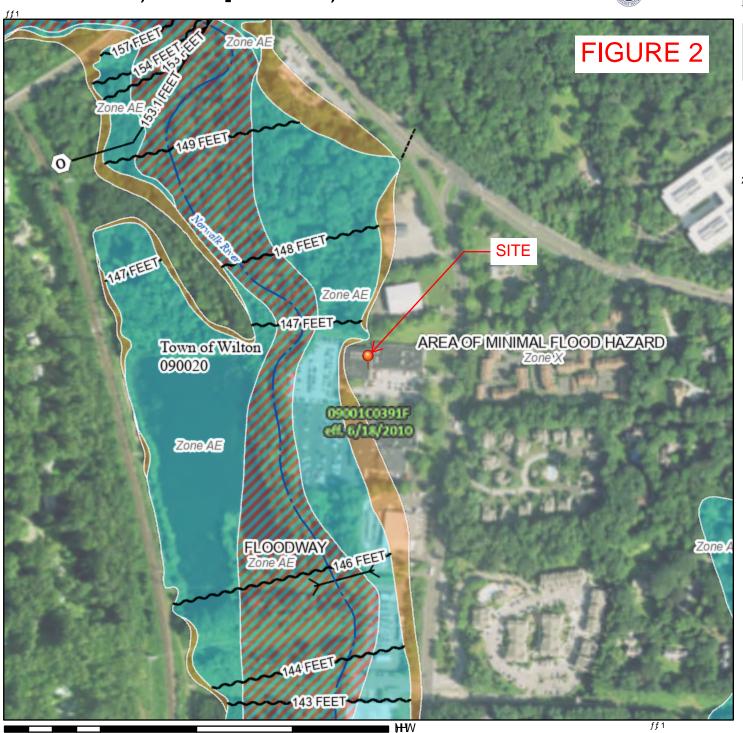


FIGURE 1



## 1DWLRODO (DRRG-EDUGIDHU) (SIWWH







74LVESFREDLH/ZWK)ØVWDQEDJG/IRU WKHXHR G.JWDO IORRGEB/LI LW LV QRW YR GD/GH/RULEHGEHORZ 7KHED/HES WRQETHEDLH/ZWK)ØVED/HES DFXUFXWDQEDJG/

74LVBSLBHLVYR.GLI WKHRQHRU RUHRI WKHIROORZQJES HOHDQWVGRQW DSB-DU EDMESLBHUN IORRGJRQHODHOV OHHOG VFDOHEDU BSFUHDWLRQGDWH FFRQLWN.LG-QWLILHUV JSBQCHO QQHU DQG)SHIHFWLYHGDWH DSLBHVIRU XDBSGGCQXRQ-UQLJGDUHDVFDQRW EHXMGIRU UHXODWRU\SUSRMV

**APPENDIX B** 



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:12.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails <del>. . .</del> Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: State of Connecticut Survey Area Data: Version 20, Jun 9, 2020 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Dec 31, 2009—Oct 5. 2016 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

## **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
103	Rippowam fine sandy loam	B/D	0.7	13.8%
307	Urban land	D	4.4	83.3%
W	Water		0.2	2.8%
Totals for Area of Interest			5.3	100.0%

## **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

GZA GEOENVIRONMENTAL, INC. BORING NO. MW-4 Engineers and Scientists 141 Danbury Road PAGE 1 OF 1 FILE NO. 50642 CHKD. BY: JMB 204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808 Wilton, Connecticut CASING 4 1/4" SAMPLER GROUNDWATER READINGS Boring Co. GZA Drilling Type HSA Split Spoon Foreman Al Augustine I.D./O.D. 1 3/8"/ 2" Date Time Depth Casing Stab. Time GZA Rep. ClareAnn Watsh Hammer Wt. 140 lbs. 5/30/92 1610 9.31 10.04 0 hrs. Date Start 5/30/92 End 5/30/92 Hammer Fall 30 in. GS.Elev. \_\_ Datum\_\_ Other Location C Sample Information Equipment Installed ASNG S SAMPLE Stratum Field Testing DESCRIPTION & CLASSIFICATION T Pen./ No. Depth (Ft.) Blows/6" Description H Rec. (ppm) Steel Casing 8-1 24/12 Top 2": TOPSOIL and grey-brown, fine to coarse SAND. 0-2.0 5-10-10-5 ND TOPSOIL - Concrete 0.21 FINE TO Auger COARSE Spoils 8-2 24/16 4.0-6.0 2-3-2-2 ND\* Loose, brown, fine SAND grading to black SILT. 4.01 Bentonite Seat AND Loose black SILT grading to brown fine Sand grading back to black Silt. 8-3 24/20 6.0-8.0 3-3-3-3 ND\* SAND Riser 5-4 24/22 8.0-10.0 6-5-8-9 Medium dense, grey-brown, fine to coarse SAND, some fine rounded Gravel, trace Rock Fragments. ND 8.04 Screen 10 8-5 24/16 10.0-12.0 8-10-12-12 ND Medium dense, grey, fine to coarse SAND, trace fine Gravel. FINE TO COARSE Sand 15 8-6 24/22 15.0-17.0 5-1-2-3 Very loose, grey, fine SAND, finer towards tip of spoon. ND 15.01 FINE 5-7 24/22 17.0-19.0 11-14-18-20 ND Medium dense, grey, fine SAND. 19.01 150 E.O.B. 25 Soil samples field screened with a 10.2 eV portable HNu photoionization detector for volatile organic compounds (VOCs). "\*" Indicates sample sent to laboratory for additional analysis. Sample wet.

Sample wet.

10 feet of 2-inch, schedule 40, threaded, flush-jointed, 10-slot PVC screen set at approximately 17 feet below grade. Well completed to ground surface with 2-inch, schedule 40, threaded, flush-jointed, solid PVC riser. Filter sand placed in annulus around well from 17 to 5 feet below grade. Bentonite seal placed from 5 to 4 feet below grade. Annulus around well backfilled with auger spoils from 4 to 0 feet below grade. Well capped with steel stick-up casing cemented in place.

E.O.B. = End of Boring. tratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings ave been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made. BORING NO. MW-4

G	ZA GE	OENVI	RONMENTA nd Scien	AL, INC. htists			141 Dan	bury Road		_			ORING NO.	- A
1 2	04 Sp rumbu 203)	ring ill c 268-0	Hill Ros onnectio 808	ad out 06611			Wilton, C	onnecticut		-		F	TLE NO.	50642
Во	ring	Co.	GZA Dr	illing	Тур	oe .	CASING 4 1/4" HSA	SAMPLER Split Spoon		GROUN	DWATER	RE	ADINGS .	
٠,	remar	1	AL Aug	ustine	1.0	./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. Time
, uZ	A Rep		ClareA	nn Walsh	Har	mer Wt.		140 lbs.	5/30/92	1745	9.0		10.0'	0 hrs.
Da	te St	art	5/30/	92 End 5/	/30/92 Han	mer Fat		30 in.						
1	.Elev			Datum		ner								
ILo	catio	n												
,	-		Sc	ample Inform	ation							RE	Equ	ipment talled
Įń.	CASNG	No.	Pen./	Depth (Ft.)	Blows/6"	Field Testing (ppm)		SAMPLE IPTION & CLASSII	FICATION	Descri	7777	EXX	Ins	
۳	-	8-1	24/8	0.5-2.5	1-2-4-6	ND	Loose, dark brown SILT, some fine Sand, trace coarse Sand.		TOPSO	IL	1		Flush mount	
1	_						Sand, trace	coarse Sand.		0.5'				- Auger Spoils
5		8-2	24/6	4.0-6.0	16-22-24-25	0.2*	Medium der SAND and gr little find	nse, brown, fine rey ROCK FRAGMEN rounded Grave	e to medium NTS,			П		- Riser - Bentonit
T		8-3	24/12	6.0-8.0	27-24-28-31	ND	Dense ROCK to coarse : Gravel.	FRAGMENTS and to	fine rounded				Ш	Seal
J.	F	s-4	24/20	8.0-10.0	8-20-30-13	ND	Dense, brow SAND, some trace Rock	en, fine to coar fine rounded Gr Fragments.	rse ravel,	FINE COAL SAL	RSE ND			Screen
1.10		8-5	24/14	10.0-12.0	7-9-18-20	ND	Medium den: coarse SAND trace fine	e, brown, fine and ROCK FRAGE rounded Gravel.	TO MENTS,	GRA			E	
ľ	_													- Sand
15		8-6	24/18	15.0-17.0	WOR-12-18	ND	Brown, fine	s SAND, 2" lens se Sand, return Sand below len	of dark	16.0'		$\ $		-
di Gr	_	5-7	24/12	18.0-20.0	6-12-13-10	ND		ie, brown, fine trace fine rour		FI	NE ND		Ħ.	
20							FRAGMENTS,	trace fine rour	nded Gravel.	20.0'		3		-
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129														_
`I														
,I. -														
SEME CALOR	1.	comp	ounds (	VOCs). "W"	Indicates sam	ple sent	to laborat	photoionization ory for addition , 10-slot PVC sench, schedule 4 18 to 6 feet bed with drill cuce.	nat anatysis.					
St	rati	ficati en ma	on line	s represent imes and unc	approximate b	oundarie stated.	s between s Fluctuati	oil types, tran	sitions may b ter may occur	e gradua due to	l. Wa factor	ter s o	level re ther than	radings 1
L.	ose	reser	t at the	e time measu	rements were	made.							ORING NO.	

GZA	GEOENV	IRON	MENTAL,	INC.
			Scient	

141 Danbury Road

BORING NO. MW-6

204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808

Wilton, Connecticut

PAGE 1 OF 1 FILE NO. 50642 CHKD. BY: JMB

Во	ring	Co.	GZA Dr	illing	ту	ре	CASING 4" HSA	GROUNDWATER READINGS						
oreman		Al Augustine I.			D./O.D.		Split Spoon 1 3/8"/ 2"	Date	Time	Dept	th Casin		Stab. Time	
, 3Z	3ZA Rep.				mmer Wt.		140 lbs.	5/30/92	1715	11.1	,	out	4 hrs.	
Da	te S	art	5/30/	92 End 5	/30/92 Ha	mmer Fal		30 in.						
35	.Ele	<b>/</b> .		Datum	Ot	her								
Lo	catio	n												
Dave	CBAL		Se	ample Inform	nation							R	Eq	uipment stalled
H	SNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIF	SAMPLE TION & CLASSIF	ICATION	Stra Descri		MXS	In	Steel Casing
		8-1	24/8	0-2.0	4-12-27-50	ND	Top 4": TOPS	OIL.		TOPSO	IL	1		- Concret
							Bottom 4": F trace Rock F	OIL. ine to coarse ragments.	SAND,	0.25		П		****
										10000000		П		- Auger Spoils
												П		
5		s-2	24/16	4.0-6.0	4-5-6-4	ND*	Medium dense	, dark brown T race Brick Fra	OPSOIL,	FIL	L	П		Riser
-							CEILLY			1		П		
		8-3	24/19	6.0-8.0	4-4-8-16	ND	some Silt, t	, dark brown T race Brick Fra ng to grey-bro	gments			l		Bentoní Seal
	_						fine Sand.	ing to grey-oro	MII,					
		8-4	24/10	8.0-10.0	10-15-18-21	ND	Medium dense	grey, fine t	o coarse	8.0'				
10	_						orano, ana no	on inagmenta.				2		Screen
		\$-5	24/8	10.0-12.0	20-24-16-12	ND	Dense, grey, SAND and ROC	fine to coars	e	FINE	то		H	44
-				-						COAR	SE		H	
i	_		_							(80)			H	- Sand
	_	_											H	
15	_	8-6	24/0	15.0-17.0	4-4-5-4	ND.		#1 A110		40.0			H	-
	_	5-0	24/0	15.0-17.0	4-4-3-4	ND	Loose, grey,	fine SAND.		15.0'		8	H	
		_									.	8	H	
	_	_								FIN	5	3		
		s-7	24/8	19.0-21.0	5-6-10-8	ND	Medium dense	gray fina s	ND			1		_
":0			4.70	1710 2110	20100	ND	trace fine,	grey, fine S/ counded Gravel.				4		-
-		_								21.0'		1		
	_										"			
											- 1	1		
25														-
EM	1.	Soil	samples	field scree	ned with a 11	7 eV po	rtable MNu ph	otoionization for addition	detector for	volatíl	e organ	nic		

3. Soil sample screened with a 10.2 eV portable MNu.
4. 10 feet of 2-inch, schedule 40, threaded, flush-jointed, 10-slot PVC screen set at approximately 19 feet below grade. Well completed to ground surface with 2-inch, schedule 40, threaded, flush-jointed, solid PVC riser. Filter sand placed in annulus around well from 19 to 7 feet below grade. Bentonite seal placed from 7 to 6 feet below grade. Annulus around well backfilled with auger spoils from 6 to 0 feet below grade. Well capped with stick-up casing cemented in place.

tratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings and been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

BORING NO. MW-6

E	ngin	eers a	and Scie				141 Danbury Road						HW-7
270	04 s rumb 203)	268-0	Hill Ro Connecti 0808	oad cut 06611			Wilton, Connecticut		_			AGE 1 ILE NO. HKD. BYT	OF 1 50642 JMB
Во	ring	Co.	GZA D	rilling	ту	'pe	CASING SAMPLER 4 174" HSA Split Speen		GROUN	DWATER	RE	AD I NGS	
0	remai	n		gustine	1.	D./O.D.	1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. Time
	A Rej		4 0272	Ann Walsh	and the second	mmer Wt.	140 lbs. 5	/30/92	1715	9.4	,	out	6 hrs.
	te S		5/30/	92 End _5	No. of the last of	mmer Fat	30 in.						
	.Elev			Datum	Ot	her							
,	_	_	s	ample Infor	mation			-			10		
	CASWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIPTION & CLASSIFICAT	ION	Strat Descrip	T.	REEKO	Ins	steel Casing
		s-1	24/8	0-2.0	4-8-9-10	0.9	Top 4": TOPSOIL.		TOPSO	)IL	1		- Auger
							Top 4": TOPSOIL. Bottom 4": Red-brown, fine to coarse SAND, trace fine Gravel.	. [	0.25'		1		Spoils
	_	_									l		Bentoni Seal
١	_	s-2	24/12	1010	7.5.4			- 1			П		Riser
5	-	2.4	24/12	4.0-6.0	7-5-5-6	0.9*	Loose, red-brown, medium SAND, trace Silt.						
		8-3	24/18	6.0-8.0	12-15-15-19	0.3	Medium dense, red-brown, fine t coarse SAND, trace fine Gravel.	to	FINE COAR: SAN	SE.	-	Ħ	
		s-4	24/8	8.0-10.0	14-24-17-24	0.1	Dense, brown-black, coarse SAND, some medium Sand, little fine Gravel.				2	I	
0		8-5	24/18	10.0-12.0	9-7-6-8	ND		-	10.01			H	Screen _
		-	24/10	1010-1210	7-7-0-0	NO.	Medium dense, grey, fine SAND.		10.0'		8	B	
												В	
								1	FINE			Ħ	- Sand
5												E	
1	_	8-6	24/12	15.0-17.0	4-3-3-3	ND	Loose, grey, fine SAND.						
ł	_		-					-	17.01		3		
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	1.	Soil s comport Sample 10 fee below riser, 3 to 2	amples unds (VC wet. t of 2- grade. Filte feet b	field scree DCs). "*" inch, sched Well compl er sand plac pelow grade.	ned with a 11 Indicates sam ule 40, thread eted to grounded in annulus Annulus are stick-up cas	.7 eV po ple sent ded, flu d surfac around und well ing ceme	table HNu photoionization detecto laboratory for additional arch-jointed, 10-slot PVC screen services of the control of the co	ctor for nalysis. set at appeaded, fl ade. Ben rom 2 to	volatile proximat ush-join tonite s 1 feet b	organ ely 15 ted, s eal pl elow g	fe ioli ace	et d PVC d from e.	
ra	tifi	cation	lines	represent a		undaries	backfilled with auger spoils fracted in place.  between soil types, transitions Fluctuations of groundwater may						dings

BORING NO. MW-7

G:	ZA GE	OENVI	RONMENTA nd Scien	AL, INC.			141 Danbury Road	_			ORING NO.	
20   Ti	04 Sp rumb( 203)	ring ill c 268-0	Hill Ros onnection 808	ad cut 06611		_	Wilton, Connecticut	_		F	TLE NO.	50642
Boi	ring	Co.	GZA Dr	illing	ту	pe	CASING SAMPLER 4 1/4" HSA Split Speen	GROUN	DWATER	RE	AD I NGS	
701	remar	1	AL Aug	ustine	1.	D./O.D.	1 3/8"/ 2" Date	Time	Depti	h	Casing	Stab. Time
IZ/	A Rep		ClareA	nn Walsh	На	mmer Wt.	140 lbs. 5/30/92	***	7.8		15.0'	0 hrs.
Da	te St	art	5/30/	92 End 5	/30/92 Ha	mmer Fat	30 in.					
18	.Elev			_ Datum	Ot	her						
.00	catio	n								П		
D.	СВ		St	ample Inform	nation			04		R	Equ	ipment
H	CASSG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	SAMPLE DESCRIPTION & CLASSIFICATION	Stra Descri		REEKO		talled ount cover
		S-1	24/0	0-2.0	6-10-14-11	0.7	Medium dense, brown, fine to coarse SAND (auger spoils).	FINE	то	1		Auger
							coarse SAND (auger spoits).	.COA		П		Spoils
								2,0'		П	-	Bentonit Seal
										П		
		8-2	24/8	4.0-6.0	2-2-3-4	0.8	Loose, black-brown, fine SAND and SILT, trace Clay.	£11		П		Riser
- 5							SILT, trace Clay.	SAI	ID	П	Н	
		8-3	24/8	6.0-8.0	2-2-2-3	0.9*	Loose, black, fine SAND and SILT, little Clay, trace coarse Sand.			П	H	
										2	H	
		s-4	24/8	8.0-10.0	5-5-1-10	0.8	Loose, black, fine SAND and SILT, little Clay, trace coarse Sand.			П	=	
1							SILT, little Clay, trace coarse Sand.			П	· H	Screen
10		8-5	24/10	10.0-12.0	8-11-15-3	0.8	Medium dense, black-brown, fine to coarse SAND, trace fine rounded	10.0'	2.	11	$ \Box$	7
							Gravel.			П	H	8
								FINE		П	H	M
1.								COAR		П	H	- Sand
										П	H	0
.5		s-6	24/10 15.0-17.	15.0-17.0	5.0-17.0 8-15-12-10	0.7	Medium dense, brown, fine to coarse SAND, trace fine rounded Gravel,			١٢		
							trace Organic matter.			إرا		
								17.0		3		
								E.O.	в.	П		
										Н		
30										П		_
										П		
										П		
								1		Н		
										П		
25	_									П		-
		-								П		
										П		
										Н		
-	1.	Soil	samples	field scre	ened with a	11.7eV p	ortable MNu photoionization detector fo	or volatí	e orga	nic	1	
E M	35.5						ortable NNu photoionization detector for to laboratory for additional analysis					
٨	3:	10 fe	et of 2	-inch, sche-	dule 40, thre	aded, flo nd surfa	ush-jointed, 10-slot PVC screen set at ce with 2-inch, schedule 40, threaded, well from 15 to 3 feet below grade. I l backfilled with auger spoils from 2 cemented in place.	flush-jo	inted,	50	lid PVC	
J		riser	. Filt	er sand pla below grade	ced in annulu	s around	well from 15 to 3 feet below grade. I backfilled with auger spoils from 2	Bentonite to 1 feet	seal p	gra	ed from	
		Well	capped	with a flus	h-mounted wel	l cover	cemented in place.				776	
tr	atif	icatio	n lines	represent	approximate h	oundarie	s between soil types, transitions may	be gradua	l. Was	ter	level re	adings
the	e be	en mac	e at ti	mes and und	ler conditions	stated.	s between soil types, transitions may Fluctuations of groundwater may occu	r due to	factors			
4110	rae p	esen	ac che	. cime measu	i cinerica were	marer :				B	ORING NO.	MW-8

				AL INC.			141 Danbury Road	_		DAGE 1	10A-1	
204 Trun (20:	Spr nbul 3)	11 c	fill Ro onnecti 808	ad cut 06611			Wilton, Connecticut			FILE NO. CHKD. BY	50642 :JMB	
orir oren ZA F	man Rep.		Al Aug ClareA	illing Justine Junn Walsh 192 End 5	I.I	pe D./O.D. mmer Wt. mmer Fal	CASING 2 3/4" Split Spoon  1 3/8"/ 2" Date  140 lbs.  30 in.	GROUND	WATER Depth	Casing		
	lev. tior			Datum	Oth	her						
CASS	BLOX	No.	Pen./	ample Inform	Blows/6"	Field Testing	SAMPLE DESCRIPTION & CLASSIFICATION	Stratu	um tion	R E	Equipment Installed	
G	8	8-1	Rec. (Ft.) (ppm		(ppm) ND*	Top 3": TOPSOIL. Bottom 5": Brown, medium to fine SAND, some Rock Fragments.	TOPSOI 0.25' FINE T MEDIU SAND	IL TO	8			
		s-2 8-3	24/6	4.0-6.0	2-5-6-6 4-5-7-15	ND*	Loose brown, fine SAND, trace fine Gravel.	4.0' FINE SAND				
		s-4	24/4	8.0-10.0	11-13-26-26		Medium dense, brown, fine to coarse SAND, trace Silt, trace fine Gravel. Dense, brown, fine to coarse SAND, little fine Gravel, trace Rock Fragments.	FINE T COARSI SAND	ti l	2		
								Ĕ.O.8				
1.		Soil compo Sampl E.O.B	samples unds (V e wet. . = End	field screen (OCs). "*"	ened with a 10 Indicates same	1.2 eV po ole sent	rtable HNu photoionization detector f to laboratory for additional analysis	or volatile	organ	ic		
at /e	ifi	catio n mad	n lines e at ti	represent mes and und	approximate boler conditions	oundarie stated. made.	s between soil types, transitions may fluctuations of groundwater may occu	be gradual. ur due to fa	Wate	other the	eadings in	

		100000000000000000000000000000000000000	TAL, INC. entists			141 Danbury Road				BORING NO	
204 : Trumi (203	Spring bull 268-	Hill Re Connect 0808	oad icut 06611		_	Wilton, Connecticut		_		PAGE 1 FILE NO. CHKD. BY:	OF 1 50642 JMB
oring	g Co.		rilling		/pe .D./O.D.	CASING SAMPLER 4 1/4" HSA Split Spoon 1 3/8"/ 2"	Date	GROUN	DWATER R	Casing	Stab. Ti
ZA Re ate S S.Ele ocati	Start ev.	The Wilder	Ann Walsh /92 End _ Datum_	3/31/92 Ha	ommer Wt. ommer Fal	140 Ubs.			Veptii	ustrig	etab. 11
-		S	ample Infor	mation				+	- Io	f.e.	.l.
CASS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	SAMPLE DESCRIPTION & CLASSIFIC	CATION	Stra Descri	M	Ins	ripment stalled
	S-1	24/8	0-2.0	6-13-13-12	ND	Top 4": TOPSOIL. Bottom 4": Brown, medium SAM ROCK FRAGMENTS.	ID and	0.3'	OIL 1		
	8-2	24/6	4.0-6.0	2-6-4-8	ND*	Loose, brown, medium to fine SAND, little Silt, trace coa Sand.	rse	FINE MEDIU SANG	JM		
H	8-3	24/10	6.0-8.0	2-4-5-4	ND	No recovery.			- 11		
	S-4	24/10	8.0-10.0	20-4-19-15	1.4*	Top 4": Black CLAY and SILT. Middle 1": WOOD FIBER. Bottom 5": ROCK FRAGMENTS.		8.0' ORGANIC	SILT 2		
	8-5	24/8	10.0-12.0	22-16-15-14	1.9	Dense, grey, medium to fine SAND and ROCK FRAGHENTS.		10.0' FINE MEDIUM SA 12.0' E.O.B	IND		
										,	
1. :	Soil s compou Sample E.O.B.	amples inds (VO wet. = End (	field screer Cs). "*" of Boring.	ned with a 10. Indicates samp	2 eV por le sent	table HNu photoionization det to laboratory for additional	tector for analysis.	volatile	organic		
tífí bee	cation n made	lines at time	represent ages and under	pproximate bou conditions s	ndaries tated.	between soil types, transition fluctuations of groundwater m	ons may be	gradual. due to fac	Water le	evel read	ings
					775				BOR	NG NO.	A-2

A	GEOEN	IRON	Scient:	INC.
93	neers	and	Scient	sts

141 Danbury Road

BORING NO. B-3

PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB

204 Spring Hill Road Trumbull, Connecticut 06611 03) 268-0808

Wilton, Connecticut

		00	674 De-	Illing	ту	De.	CASING 2%" HSA	SAMPLER Split Spoon		GROUN	DWATER	RE/	DINGS	,
	ing eman			illing Lman		D./O.D.	EA HAA	1 3/8"/ 2"	Date	Time	Depth	T	Casing	Stab. Time
				e, P. Crox		mmer Wt.		140 lbs.	6/13/92		8.0'	7	8.0'	0 hrs.
	Rep			22 End _6		mmer Fall		30 in.						
1 ,	e St Elev		0/10/1	_ Datum		her								
1	atio		See Pla											
_			POLICE STATE OF THE PARTY OF TH	mple Infor	mation			CAMPI E		Stra	tim	REM	Equ	uipment stalled
	BLOWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSII	FICATION	100000	iption	MK8		None
1		s-1	24/14	0-2.0	3-2-7-15	1/0.8	Loose, brow and fine to Silt.	n, fine to coar coarse GRAVEL	se SAND , little	0.3'	OIL	1		
	_													
١,		8-2	24/10	2.0-4.0	12-19-24-29	0.4/0.6	Dense, brow and fine to Silt.	n, fine to coa coarse GRAVEL	rse SAND , little	COA	ND			-
-										GRA	VEL			
4	_	s-3	24/16	4.0-6.0	16-20-44-66	0.2/0.6	Very dense, SAND and fi little Silt	brown, fine to ne to coarse G	o coarse RAVEL,					
;							10.000					Ш		
5		s-4	24/21	6.0-8.0	29-26-26-40	0.4/0.6		own, fine to co coarse GRAVEL		6.3'		1		
. 7							Bottom 18": SAND, Littl	Brown, fine to le Silt.	o medium	MED	E TO IUM ND			
8		s-5	24/15	8.0-10.0	20-19-16-13	0.2/0.6	Dense, brow and fine to Silt.	n, fine to coa coarse GRAVEL	rse SAND , little		E TO	2		•
?										SAND	RSE AND VEL			
Ö										10.0′ E.C		3		
11														
12														
3														
14														
1										- UU M-	dal OI-	104		

Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101 photoionization detector. 1/0.8 = meter response of sample/meter reponse of background conditions. ppm = parts per million.
Sample wet at approximately 8 feet below grade.

2.

Boring ended at approximately 10 feet below grade. E.O.B. = End of Boring.

Stratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

·'A	GEOEN	/IRO	MENTAL,	INC.
19	neers	and	Scient:	sts

141 Danbury Road

BORING NO. B-4

PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB

204 Spring Hill Road umbull, Connecticut 06611 :03) 268-0808

Wilton, Connecticut

CASING SAMPLER GROUNDWATER READINGS GZA Drilling Type 2%" HSA Split Spoon Boring Co. Stab. Time Time Depth Casing Date I.D./O.D. 1 3/8"/ 2" f 'eman Ron Holman 140 lbs. L. McKee, P. Crowell Hammer Wt. GZA Rep. 30 in. :e Start 6/13/92 End 6/13/92 Hammer Fall \_\_\_\_ Datum\_\_\_\_ Other " .Elev.

ati		See Pla	_ Datum_		circi			$\neg$	
		A Comment of the last	mple Infor	mation				R	Equipment Installed
C B A C N G	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)		Stratum Description	REMKS	None
	s-1	24/16	0-2.0	3-16-18-21	0.6/0.6	Top 6": Brown to black TOPSOIL.	TOPSOIL	1	
						Top 6": Brown to black TOPSOIL. Bottom 10": Brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt.	0.5'		
							FINE TO COARSE SAND AND GRAVEL		
_	s-2	6/6	4.0-4.5	64-10/0"	NS	Very dense, fine to coarse SAND and fine to coarse GRAVEL, little Silt.			
	8-3	0/0	5.0	10/0"	NS	No recovery.	5.0' E.O.B.	2	
									•
	-								
	-								
_	-								
F									
_	+	+							

Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101 photoionization detector. 1/0.8 = meter response of sample/meter reponse of background conditions. ppm = parts per million.

Boring ended at approximately 5 feet below grade due to auger and spoon refusal. E.O.B. = End of Boring. NS = No sample

2.

Atratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

Ť	04 8	pring ull,	Hill R	oad icut 06611	1		Wilton, Connecticut				PAGE 1 FILE NO. CHKD. BYT	0F 1 50642
(	203)	268-	808				#Itton, Connecticut				CHKD. BYI	ЈМВ
01	ring	Co.	GZA D	rilling	1	Гуре	CASING SAMPLER		GROUN	DWATER RE	ADINGS	
	emar		Ron H			I.D./O.D.	1 3/8"/ 2"	Date	T +1	Danet.		I
Z	Rep	٥.		Kee, P. Cro		lammer Wt.	THE RESERVE OF THE PARTY OF THE	6/13/92	Time	Depth 8.0'	Casing	Stab. Ti
1	e St	tart	No. of DOI 10	/92 End _		lammer Fat	177 1881	0/13/72		8.0	8.0'	0 hrs.
;,	Elev	/·		Datum_		other						
1	atio	n	See p	an (4 feet	east of B-4)							
Ī	C B		S	ample Info	rmation					R	Equ	ipment
	BLOWS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRIPTION & CLASSIF	ICATION	Stra Descri	M		vipment stalled None
									SEE B-4	1		
		8-1	24/14	4.0-6.0	22-27-42-22	0.4/0.4	Very dense, brown, fine to SAND and fine to coarse GR little Silt.	coarse AVEL,				
-		8-2	24/18	6.0-8.0	18-16-15-16	0.6/0.4	Dense, brown, fine to coars and fine GRAVEL, little Si	e SAND	FINE COARS SAND AND GRAVE	E		
		s-3	24/14	8.0-10.0	14-15-21-30		Dense, brown, fine to coars and fine to coarse GRAVEL, Silt, trace Organics.	e SAND little		2		
									10.0' E.O.B	. 3		
	+											
Ī										- 11		
7 200							nic compounds with an 11.7 onse of sample/meter repons ade. E.O.B. = End of Boris		Nu Model und condi	PI-101 tions.		

BORING NO. B-4A

GZA GEOENVIRONMENTAL, INC.

ingin	EOENVI	RONMENT/ nd Scien	AL, INC.			141 Danbury Road	_		BORING NO	200
204 S Trumb (203)	pring ull c 268-0	Hill Roa onnectio BOB	nd cut 06611		_	Wilton, Connecticut	_		FILE NO. CHKD. BY:	OF 1 50642 JMB
oring	Co	67A De	(III)			CASING SAMPLER	GROUND	WATER R	EAD INGS	
oring orema			illing lman		ype .D./O.D.	2%" HSA Split Spoon 1 3/8"/ 2" Date	Time	Depth	Casing	Stab. Tim
ZA Re	р.	L. McK	ee, P. Cro	0.60	ammer Wt.	140 lbs. 6/13/92		8.0'	8.0'	0 hrs.
ate S	tart		92 End _		ammer Fal	30 in.				
S.Ele	9/20	The state of the state of	Datum	0	ther		+			
cati	_	See pl	an Imple Infor	mation				I R	Ear	ipment
CASS	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	SAMPLE DESCRIPTION & CLASSIFICATION	Descrip	l M		ipment stalled None
	8-1	24/4	0-2.0	1-2-14-24	0.4/0.4	Top 2": Brown to black TOPSOIL.	TOPSO	IL 1		
1	-					Top 2": Brown to black TOPSOIL. Bottom 2": Brown, medium to coarse SAND and fine to coarse GRAVEL, trace Silt.	0.2'			
$\vdash$	-									
2	8-2	12/12	2.0-3.0	13-56	0.4/0.4	Very dense, brown, fine to coarse				
, _						Very dense, brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt.				
_							FINE	E		
-	s-3	24/14	4.0-6.0	16-30-34-34	0.4/0.4	Very dense, brown, fine to coarse	SAND AND GRAVE			
						Very dense, brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt.				
-	5-4	24/19	6.0-8.0	32-28-60-53	0.4/0.4	Many dance bears flow to seems				
$\vdash$	3-4	64/17	0.0-0.0	32-20-00-33	0.4/0.4	Very dense, brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt.				
								2		
-	8-5	24/14	8.0-10.0	12-17-19-18	0.2/0.2	Dense, brown, fine to medium SAND, little fine to coarse Gravel, little Silt.	8.0'	,		
$\vdash$	_					treete arte.	COARS	E		
								3		
							10.0' E.O.B	.		
-	-									
5										
-	_									
-										
1. 2. 3.	ppm = Sampl Borin	parts e wet a g ended	per millio t approxim at approx	n. ately 8 feet b imately 10 fee	elow grad t below s	nic compounds with an 11.7 eV portable conse of sample/meter reponse of backge. e. rade. E.O.B. = End of Boring.				
THE PERSON NAMED IN	Hentic	n Lines	represent	approximate	ooundarie:	between soil types, transitions may Fluctuations of groundwater may occu	be gradual.	Water	level re	adings

BORING NO. B-5

G	ZA G	EOENVI	RONMENT	AL, INC.			141 Danbury Road					ORING NO	
7	04 s rumb 203)	268-0	Hill Ro connecti 808	ad cut 06611		_	Wilton, Connecticut		_		-	PAGE 1 TLE NO.	OF 1 50642 JMB
Во	ring	Co.				ype	CASING SAMPLER 2%" HSA Split Spoon		GROUN	DWATER	RE	ADINGS	
	remai		Ron Ho			.D./O.D.	1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. Time
	A Re		THE STREET	ee, P. Cro		ammer Wt.		6/13/92	***	8.5		8.0'	0 hrs.
		tart	6/13/	92 End		ammer Fal	. 30 in.						
	.Ele	399			0	ther					_		
_	catio	_	See pl					L	-		-		
E	AL	_	T -	ample Info I	rmation	Field	SAMPLE		Stra	tum	RE	Equ	ipment talled
DEPTH	CASNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Testing (ppm)		- 10-000	Descri	ption	NXX.		None
		8-1	24/15	0-2.0	6-13-15-27	0.6/0.6	Top 4": Brown to black TO	PSOIL.	TOPS	DIL	1		
1		_					Top 4": Brown to black TO Bottom 11": Brown, fine to SAND and fine to coarse G little Silt.	RAVEL,	0.3'		П		
	_	_									П		
2	_	-									П		
	_	-									П		
3	$\vdash$										П		
	_	-									П		
4	_	s-2	24/15	4.0-6.0	22-27-61-61	0.4/0.8	Vanu dance brown fine to		FINE	то	П		
	_	9-6	64/15	4.0-0.0	10-10-12-22	0.4/0.8	Very dense, brown, fine to SAND and fine to coarse GR little Silt.	AVEL,	SAN	D	П		
5							tittle sitt.		GRAV	EL	П		-
	_										П		
6	_	s-3	24/20	6.0-8.0	50-34-44-46	0.6/0.8	Very dense, brown, fine to	coarse			Н		
							Very dense, brown, fine to SAND and fine to coarse GR little Silt.	AVEL,					
7													
													-
В		8-4	24/16	8.0-10.0	26-50-41-19	0.6/0.8	Very dense, brown, fine to	coarse			2		
9							SAND and fine to coarse GR little Silt.	AVEL,					
10											3		_
									10.0' E.O.I	.	1		
11									21011	"	1		
	_									- 1	1		
12										- 1	1		
	_												_
13	_	_											
1	_			-							1		
14	_									- 1			
1	_												
R	1.	Soil	eamplee	field ecr	sened for vols	tile orga	nic compounds with an 11 7	eV postable	WWW Mode	DI-10			
Ë	٠.	photo	ionizat	ion detect	or. 1/0.8 = m	eter resp	nic compounds with an 11.7 conse of sample/meter repon	se of backgro	ound cond	itions.			
REMARKS	3:	Sample	wet a	approximat approx	stely 8.5 feet	below gr	ade. rade. E.O.B. = End of Bor	ina.					
Š			, chaed	at approx		. paron 9	LIVIDI - EIM OF BOI						
Str	ntif	icatio	n lines	represent	approximate b	oundaries	between soil types, trans	itions may be	graduat	. Wate	er	level rea	dings
have	bee	en mad	e at ti	mes and un	der conditions	stated.	between soil types, trans Fluctuations of groundwat	er may occur	due to f	actors	ot	her than	

BORING NO. B-6

GZA GEOENVIRONMENTAL, INC. Engineers and Scientists BORING NO.\_B-7 141 Danbury Road PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB 204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808 Wilton, Connecticut CASING SAMPLER GROUNDWATER READINGS Boring Co. GZA Drilling Type Z¼" HSA Split Spoon Foreman Ron Holman I.D./O.D. 1 3/8"/ 2" Date Time Casing Depth Stab. Time GZA Rep. L. McKee, P. Crowell Hammer Wt. 140 lbs. 6/13/92 ... 8.54 8.0 0 hrs. Date Start 6/13/92 End 6/13/92 Hammer Fall \_\_\_\_\_30 in. GS.Elev. \_\_\_ Datum\_\_ Other Location See plan В Sample Information REMKS Equipment ASS S DESCRIPTION & CLASSIFICATION Stratum Installed Field H No. Pen./ Depth (Ft.) Blows/6" Testing Description Rec. (ppm) None Top 10": Brown to black TOPSOIL, little fine to coarse Gravel. Bottom 6": Brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt. 8-1 24/16 0-2.0 6-10-18-27 0.8/0.8 TOPSOIL 0.8 8-2 24/18 0.8/0.8 Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt. 4.0-6.0 20-26-23-25 FINE TO COARSE GRAVEL 5-3 24/15 6.0-8.0 25-31-38-39 0.8/1.0 Very dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt. 5-4 24/15 8.0-10.0 21-15-13-24 Medium dense, brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt. 0.8/1.0 10 10.04 E.O.B. 12 1 13 14 Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101 photoionization detector. 1/0.8 = meter response of sample/meter reponse of background conditions. ppm = parts per million.

Sample wet at approximately 8.5 feet below grade.

Boring ended at approximately 10 feet below grade. E.O.B. = End of Boring. 3: CRKS

Stratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

GZA.	GEOEN'	IRON	MENTAL	, INC.
Engi	neers	and	Scient	ists

141 Danbury Road

BORING NO. B-8

BORING NO. B-8

204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808

Wilton, Connecticut

PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB

ring	Co.	GZA D	rilling		Туре	2%" HSA	Split Spoon		GROUP	DWATER	RE	ADINGS	
rema	n	Ron H	olman		I.D./O.D.		1 3/8"/ 2"	Date	Time	Dept	h	Casing	Stab. T
Re	p.	L. Mc	Cee, P. Cr	owell	Hammer Wt.		140 lbs.	6/13/92		10.0		8.0'	0 hrs
e S	tart	6/13/	/92 End	6/13/92	dammer Fat		30 in.						0 111 8
Ele	٧.		Datum_		Other						$\dashv$		
ati	on	See pl	an								$\dashv$		
C E		8	ample Info	rmation					_		T <sub>o</sub>	For	irmant
CASNG	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing	DESCRIP	SAMPLE TION & CLASSIF	ICATION	Stra Descri		REMKS	Ins	ipment
-	8-1	24/12	The same of the sa	4-8-26-24	(ppm)	W (W					8	!	lone
_	-	E-4/ 1E	0-2.0	4-0-20-24	0.8/0.8	Top 4": Brown ORGANICS.	TOPSOIL and		TOPS	DIL	1		
_	-	-				fine to coars	ght grey, tan e SAND, some , little Silt	ine to	0.8		П		
-	_					coarse Gravet	, little Silt.				П		
-	-	_									П		
-	-	_											
_	-	_											
_	_									**			
_									FINE	SE			
	8-2	24/10	4.0-6.0	26-48-49-37	0.8/0.8	Very dense, b	rown, grey, or	ange,	SAN		1		
						coarse GRAVEL	rown, grey, or e SAND and fin , trace Silt.	e to	GRAV	EL	1		
											1		
											1		
	8-3	24/17	6.0-8.0	37-22-50-34	0.8/0.8	Top 9": Brown	, fine to coar	se SAND			1		
						XIII.	, fine to coar parse GRAVEL,		6.8'	-	1		
						Bottom 8": Ord	ange to brown, fine to coarse silt.	fine	FINE	. 1	1		
					-	Gravel, little	Silt.		SANC				
	8-4	24/18	8.0-10.0	14-9-9-15	0.8/0.8	dedium dense	brown fine to		8.0'				
					010,010	oarse SAND ar	brown, fine to d fine to coa silt.	rse	12000	.	2		
_	_					MAVEL, LILLIE	, sitt.		COARS	E			
									SAND A GRAVE		1		
											3		
-	-								10.0' E.O.B	. 1			
-	_										1		
_													
-	_												
_													
_													
_													
	Soil s	amples onizati	field scre	ened for vola	tile organ	ic compounds	with an 11.7 e /meter reponse	V portable i	HNu Model	PI-10	1		
: 1	ppm =	parts p	er million	tely 10 feet i	- Teopo	or adilpre	, mater reponse	or package	una condi	cions.			

tratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings gave been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

GZA GEOENVIRONMENTAL, INC. Engineers and Scientists BORING NO. 8-9 141 Danbury Road PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB 204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808 Wilton, Connecticut CASING SAMPLER GROUNDWATER READINGS Boring Co. GZA Drilling Type 2%" HSA Split Spoon Foreman Ron Holman I.D./O.D. Depth 1 3/8"/ 2" Date Time Casing Stab. Time GZA Rep. L. McKee, P. Crowell Hammer Wt. \_\_\_\_140 lbs. 6/13/92 ... 9.01 8.0 0 hrs. Date Start \_\_6/13/92\_\_ End \_6/13/92 Hammer Fall \_\_\_\_\_\_30 in. GS.Elev. \_\_ Datum\_\_ Other Location See plan CASSG Sample Information Equipment Installed DESCRIPTION & CLASSIFICATION Stratum Field No. Pen./ (Ft.) Blows/6" Testing Description H Rec. (ppm) None Top 4": Brown to black TOPSOIL. Bottom 12": Brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt. 5-1 24/16 0-2.0 3-6-8-12 0.6/0.6 TOPSOIL 0.37 8-2 24/16 Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt. 2.0-4.0 16-20-17-17 0.6/0.6 FINE TO COARSE SAND Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt. 8-3 24/18 4.0-6.0 23-22-29-30 0.6/0.6 AND GRAVEL Very dense, brown, fine to coarse SAND and fine to coarse GRAVEL, trace Silt. 5-4 24/16 6.0-8.0 44-37-54-50 0.6/0.6 Top 6": Grey, fine SAND, some fine to coarse Gravel, little Sitt. Bottom 12": Brown, fine to coarse SAND, trace Silt. 5=5 24/18 8.0-10.0 21-13-12-12 0.2/0.6 8.0' FINE SAND 0.4/0.6 FINE TO COARSE SAND 10.0' E.O.B. 12 13 14 Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101 photoionization detector. 1/0.8 = meter response of sample/meter reponse of background conditions. ppm = parts per million.
Sample wet at approximately 9 feet below grade.
Boring ended at approximately 10 feet below grade. E.O.B. = End of Boring. 3: ARKS Stratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

BORING NO. B-9

GZA GEOENVIRONMENTAL, INC. Engineers and Scientists BORING NO. B-10 141 Danbury Road PAGE 1 OF FILE NO. 50642 CHKD. BY: JMB 204 Spring Hill Road Trumbull, Connecticut 06611 (203) 268-0808 Wilton, Connecticut CASING SAMPLER GROUNDWATER READINGS \_GZA Drilling Boring Co. Type 2%" NSA Split Spoon Foreman Ron Holman I.D./O.D. 1 3/8"/ 2" Date Time Depth Casing Stab. Time L. McKee, P. Crowell GZA Rep. Hammer Wt. 140 lbs. 6/13/92 ---6.5 4.01 0 hrs. Date Start \_\_6/13/92 End \_6/13/92 Hammer Fall 30 in. GS.Elev. \_\_\_ Datum\_\_\_\_ Other Location See plan CASWS Sample Information Equipment Installed DESCRIPTION & CLASSIFICATION Stratum Field No. Pen./ Depth (Ft.) Blows/6" Testing Description Rec. (ppm) None 8-1 24/7 0-2.0 4-7-3-3 Top 4": Brown to black TOPSOIL. Bottom 3": Brown, fine to coarse SAND and fine to coarse GRAVEL, little Silt. 0.6/0.6 TOPSOIL 0.37 8-1A 24/3 2.0-4.0 0.6/0.6 7-8-7-7 Medium dense, brown, fine SAND, some fine to coarse Gravel, little Silt. 3 SAND (ORGANICS FROM 4-6') 5-2 24/2 4.0-6.0 Loose, brown to black, fine SAND, little fine Gravel, little organic Silt. 1-3-4-7 0.8/0.6 5-3 24/10 6.0-8.0 14-17-14-27 0.6/0.6 Dense, brown, fine to coarse SAND and fine to coarse GRAVEL, some Silt. 6.01 FINE TO COARSE SAND 8 8.0 E.O.B. Soil samples field screened for volatile organic compounds with an 11.7 eV portable HNu Model PI-101 photoionization detector. 1/0.8 = meter response of sample/meter reponse of background conditions. ppm = parts per million.
Sample wet at approximately 6.5 feet below grade.
Boring ended at approximately 8 feet below grade. E.O.B. = End of Boring. R 3:

tratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings ave been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

				TAL, INC. entists		-	141 Dant	oury Road		_			0. <u>8-11</u>
270	04 S rumb 203)	pring ull, 268-	Hill Re Connect 0808	oad icut 0661	1		Wilton, Co	nnecticut				PAGE 1 FILE NO. CHKD. BY	50642 JMB
30	ring	co.	1	rilling		Гуре	CASING 2%" HSA	SAMPLER Split Spoon		GROUN	DWATER R	EADINGS	
0	remar	n		olman		.D./O.D.		1 3/8"/ 2"	Date	Time	Depth	Casing	Stab. T
Z	A Rep	٥.	L. Mc	Kee, P. Cr	owell 1	lammer Wt.	_	140 lbs.	6/13/92	***	10.0'	8.0'	0 hrs
a	te Si	tart	6/13	/92_ End .	6/13/92	dammer Fat		30 in.					
s	.Elev	/.		Datum_		other							
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	СВ		8	ample Info	rmation			201000000			R	East	uipment
	C A L O W S	No.	Pen./ Rec.	Depth (Ft.)	Blows/6"	Field Testing (ppm)	DESCRI	SAMPLE PTION & CLASSIF	ICATION	Stra Descri	M		uipment stalled None
Ī		S-1	24/12	0.3-2.3	16-13-7-5	0.6/0.6	Medium dense	, brown, fine S	SAND.	ASPH	_		
							Some fine Gr (Black Organ	e, brown, fine s ravel, trace Sil nic Silt in tip	t.	0.3'			
1							spoon).		15.5				
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١		8-2	24/2	4.0-6.0	17-14-21-19	0.640.4	Dance bee			GRAV	EL		
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ŀ		8-3	24/14	6.0-8.0	22-31-30-27	0.740.7			Automa -		- 11		
ŀ		0-3	24/14	0.0-0.0	22-31-30-27	0.0/0.6	SAND and fin	brown, fine to e to coarse GRA	coarse VEL,		- 11		
ŀ		_	_				trace Silt.				- 11		
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ŀ	-	0.1	7/ /4/	0.0.40.0							2		
ŀ	$\rightarrow$	8-4	24/16	8.0-10.0	42-45-30-20	0.4/0.6	GRAVEL, some	fine to coarse	e		"		
ŀ	-						SILT.						
ŀ	-						to coarse SAN	range to brown, ND, some fine Gr	avel,				
ŀ	_										3		
ŀ										10.0' E.O.B	"		
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Sample wet at approximately 10 feet below grade.
Boring ended at approximately 10 feet below grade. E.O.B. = End of Boring.

Stratification lines represent approximate boundaries between soil types, transitions may be gradual. Water level readings have been made at times and under conditions stated. Fluctuations of groundwater may occur due to factors other than those present at the time measurements were made.

TABLE 1
GROUNDWATER ELEVATION DATA: 11/2/93
141 DANBURY ROAD
WILTON, CONNECTICUT

LOCATION	REFERENCE ELEVATION	DEPTH TO WATER (FT)	WATER TABLE ELEVATION
MW-1	99.14	12.60	86.54
MW-2	100.57	14.33	86.24
MW-3	98.56	12.18	86.38
MW-4	96.24	10.51	85.73
MW-5	94.53	9.24	85.29
MW-6	96.43	11.35	85.08
MW-7	94.73	9.75	84.98
MW-8	88.89	4.00	84.89

#### NOTES:

 Reference elevation: are top of PVC monitor wells based on relative difference to an arbitrary benchmark established on center of a manhole cover along the eastern property line which was assumed to be 100 feet above mean sea level.

**APPENDIX C** 

Project No. **F0173-002** 

Date: **05/07/21**Prepared By: **TAS** 

# 141 Danbury Road Wilton, CT Existing CN & Tc Worksheet



Name: EX-WS-01
Location: Southern Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	1.932	98	189.314
Landscaped and Lawns	0.872	69	60.183
			249.497

Total Area: \_\_\_\_\_2.804 CN: \_\_\_\_\_89

#### Time of Concentration:

Sheet-Flow Travel Time								
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)								
A-B	0.24	3.54 100 0.015 15.2						

Shallow Concentrated Flow Travel Time								
Segment ID	Cover Flow Length (ft) Slope (ft/ft) V (ft/s) Time (min)							
B-C	Paved	580	2.87	3.4				

Total Tc (min) = \_\_\_\_18.6

Name: EX-WS-02
Location: Northern Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.059	98	5.739
Landscaped and Lawns	1.040	69	71.728
			77.467

Total Area: 1.098 CN: 71

#### Time of Concentration:

Sheet-Flow Travel Time							
Segment ID	Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)						
A-B 0.24 3.54 130 0.035 13.4							

Shallow Concentrated Flow Travel Time								
Segment ID	gment ID Cover Flow Length (ft) Slope (ft/ft) V (ft/s) Time (min)							
B-C	Unpaved	410	0.020	2.28	3.0			

Total Tc (min) = \_\_\_\_\_16.4

References: NRCS Technical Release 55 ConnDOT Drainage Manual, Chapter 6 Project No. **F0173-002** Date: **05/07/21** 

Prepared By: TAS

#### 141 Danbury Road Wilton, CT Existing CN & Tc Worksheet



Name: EX-RF-01
Location: Existing Building

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.775	98	75.932
Landscaped and Lawns	0.000	69	0.000
			75.932

Total Area: 0.775 CN: 98

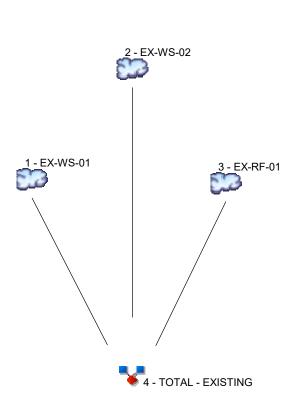
#### Time of Concentration:

Sheet-Flow Travel Time								
Segment ID	Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)							
A-B	0.015	3.54	60	0.015	1.1			

Total Tc (min) = 1.1

Minimum Tc = 5.0

## Watershed Model Schematic, Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3



#### **Legend**

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	SCS Runoff	EX-WS-01
2	SCS Runoff	EX-WS-02
3	SCS Runoff	EX-RF-01
4	Combine	TOTAL - FXISTING

Project: F0173-02 Hydrographs - Existing.gpw

Monday, 05 / 24 / 2021

# Hydrograph Return Period Recap Hydraffow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.		Inflow		Peak Outflow (cfs)							Hydrograph
No.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			5.474			9.316	11.72	13.50	15.39	EX-WS-01
2	SCS Runoff			0.975			2.287	3.202	3.910	4.680	EX-WS-02
3	SCS Runoff			2.573			3.949	4.812	5.454	6.139	EX-RF-01
4	Combine	1, 2, 3		7.662			13.50	17.25	20.05	23.05	TOTAL - EXISTING

Proj. file: F0173-02 Hydrographs - Existing.gpw

Monday, 05 / 24 / 2021

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	5.474	2	732	24,369				EX-WS-01
2	SCS Runoff	0.975	2	732	4,233				EX-WS-02
3	SCS Runoff	2.573	2	724	8,720				EX-RF-01
4	Combine	7.662	2	730	37,453	1, 2, 3			TOTAL - EXISTING
F01	F0173-02 Hydrographs - Existing.gpw					eriod: 2 Ye	ear	Monday, 05	5 / 24 / 2021

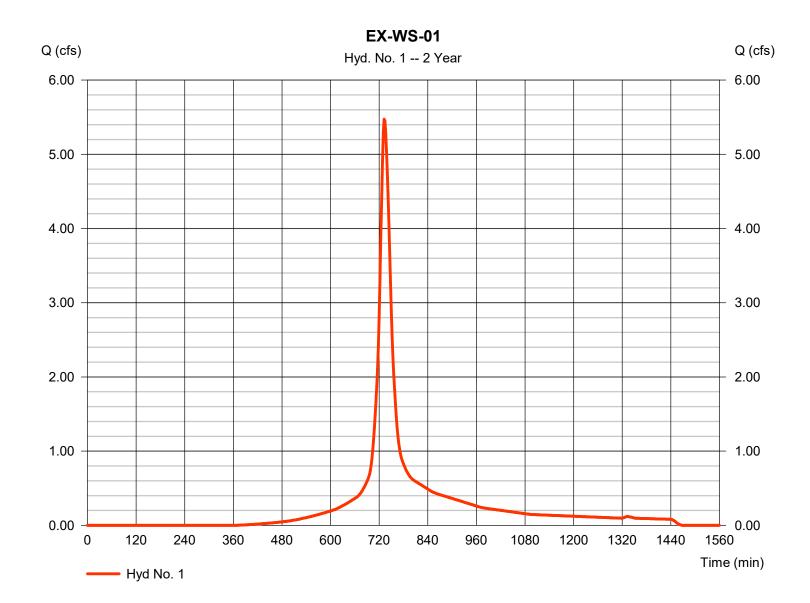
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 1

EX-WS-01

Hydrograph type = SCS Runoff Peak discharge = 5.474 cfsStorm frequency = 2 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 24,369 cuftDrainage area Curve number = 2.804 ac= 89 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



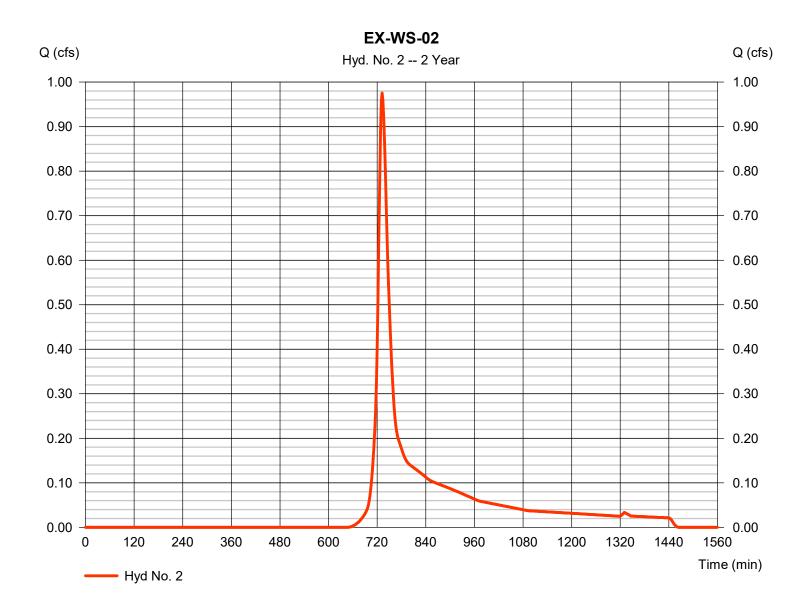
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 2

EX-WS-02

Hydrograph type = SCS Runoff Peak discharge = 0.975 cfsStorm frequency = 2 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 4,233 cuftDrainage area Curve number = 71 = 1.098 acHydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 16.40 min = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



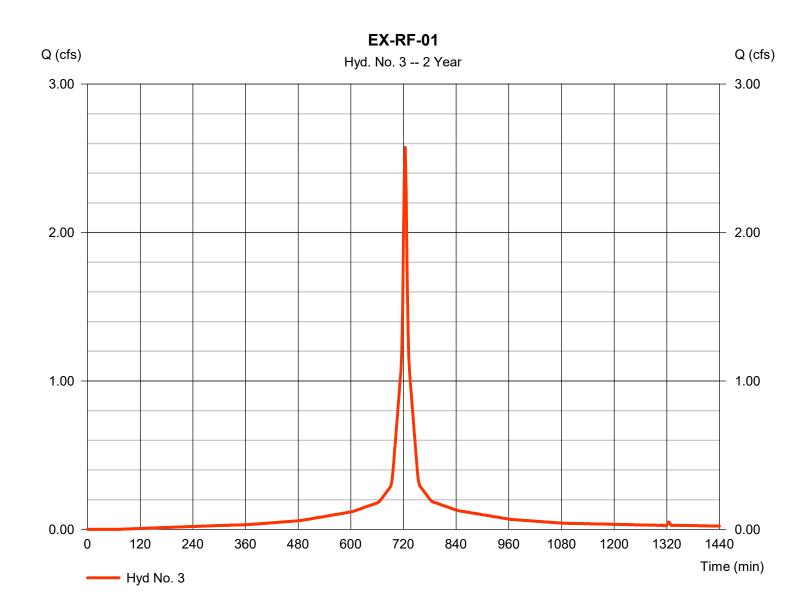
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 3

EX-RF-01

Hydrograph type = SCS Runoff Peak discharge = 2.573 cfsStorm frequency = 2 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 8,720 cuftDrainage area = 0.775 acCurve number = 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



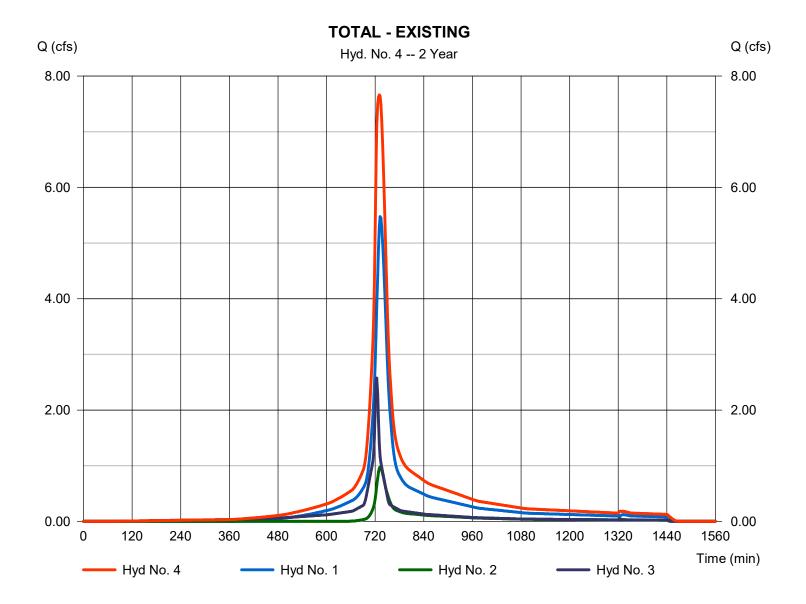
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type = Combine Peak discharge = 7.662 cfsStorm frequency Time to peak = 2 yrs= 730 min Time interval = 2 min Hyd. volume = 37,453 cuftInflow hyds. = 1, 2, 3Contrib. drain. area = 4.677 ac



## Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	9.316	2	732	42,301				EX-WS-01
2	SCS Runoff	2.287	2	732	9,417				EX-WS-02
3	SCS Runoff	3.949	2	724	13,616				EX-RF-01
4	Combine	13.50	2	730	65,561	1, 2, 3			TOTAL - EXISTING
F01	173-02 Hydro	graphs - I	Existing.	gpw	Return F	Period: 10 Y	'ear	Monday, 05	5 / 24 / 2021

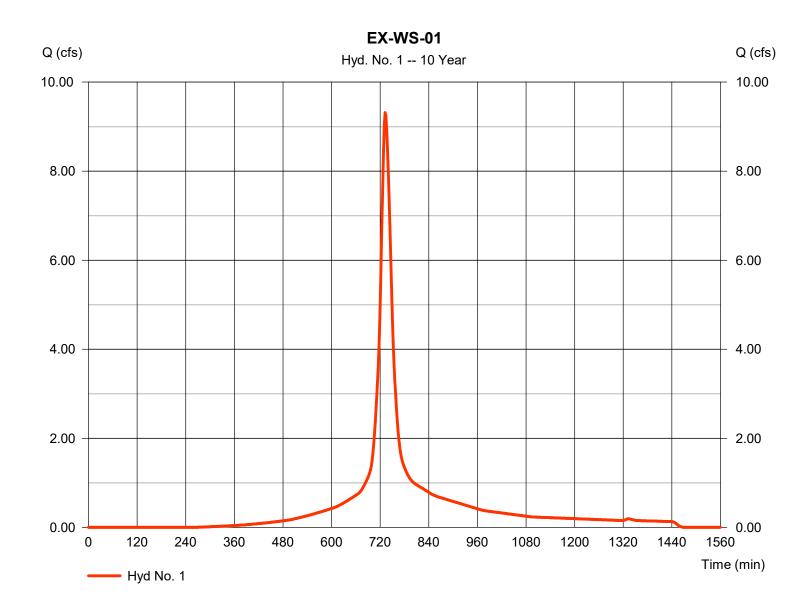
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 1

EX-WS-01

Hydrograph type = SCS Runoff Peak discharge = 9.316 cfsStorm frequency = 10 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 42,301 cuftDrainage area Curve number = 2.804 ac= 89 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



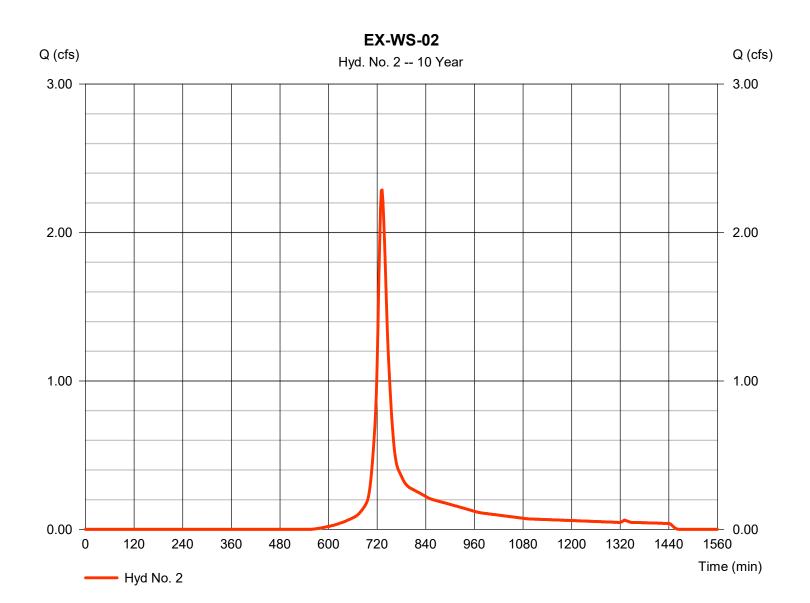
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 2

EX-WS-02

Hydrograph type = SCS Runoff Peak discharge = 2.287 cfsStorm frequency = 10 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 9.417 cuft Drainage area Curve number = 71 = 1.098 ac= 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 16.40 min = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



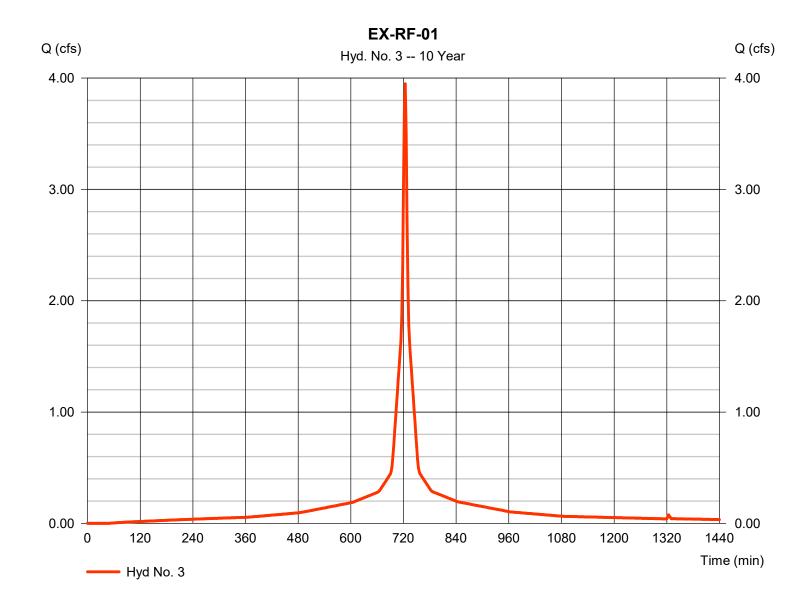
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 3

EX-RF-01

Hydrograph type = SCS Runoff Peak discharge = 3.949 cfsStorm frequency = 10 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 13,616 cuft Drainage area Curve number = 0.775 ac= 98 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



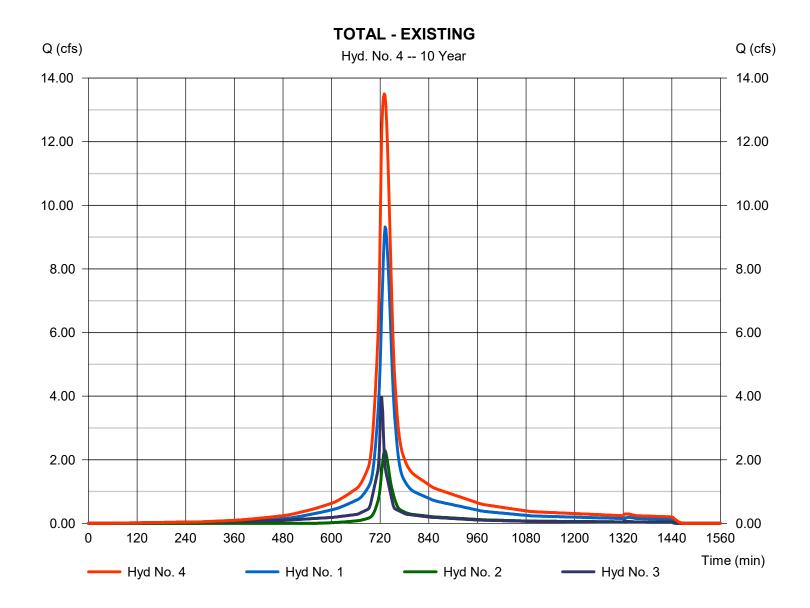
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type = Combine Peak discharge = 13.50 cfsStorm frequency Time to peak = 10 yrs= 730 min Time interval = 2 min Hyd. volume = 65,561 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 4.677 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	11.72	2	732	53,834				EX-WS-01
2	SCS Runoff	3.202	2	730	13,075				EX-WS-02
3	SCS Runoff	4.812	2	724	16,698				EX-RF-01
4	Combine	17.25	2	730	83,894	1, 2, 3			TOTAL - EXISTING
F01	73-02 Hydro	granhe - <sup>1</sup>	= xieting o	npw.	Return 5	Period: 25 Y	/ear	Monday, 05	5 / 24 / 2021

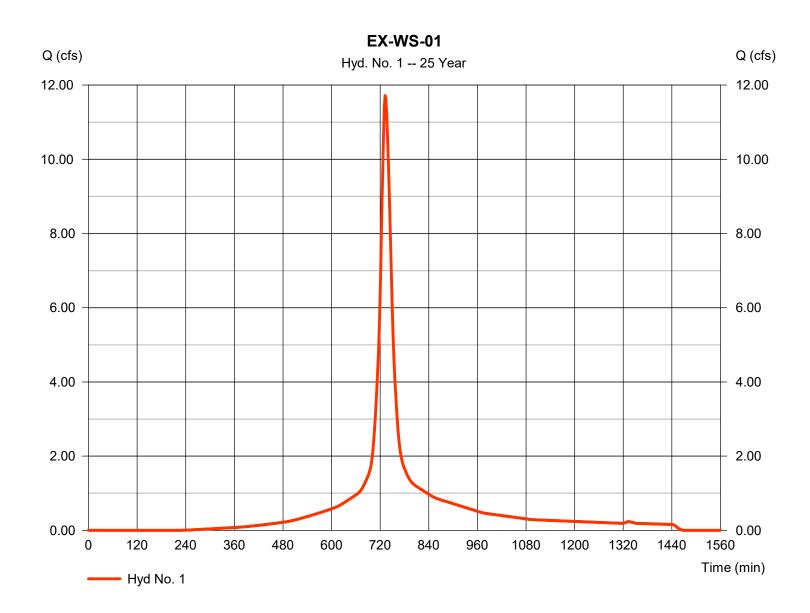
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 1

EX-WS-01

Hydrograph type = SCS Runoff Peak discharge = 11.72 cfsStorm frequency = 25 yrs Time to peak = 732 min Time interval = 2 min Hyd. volume = 53,834 cuft Drainage area Curve number = 2.804 ac= 89 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



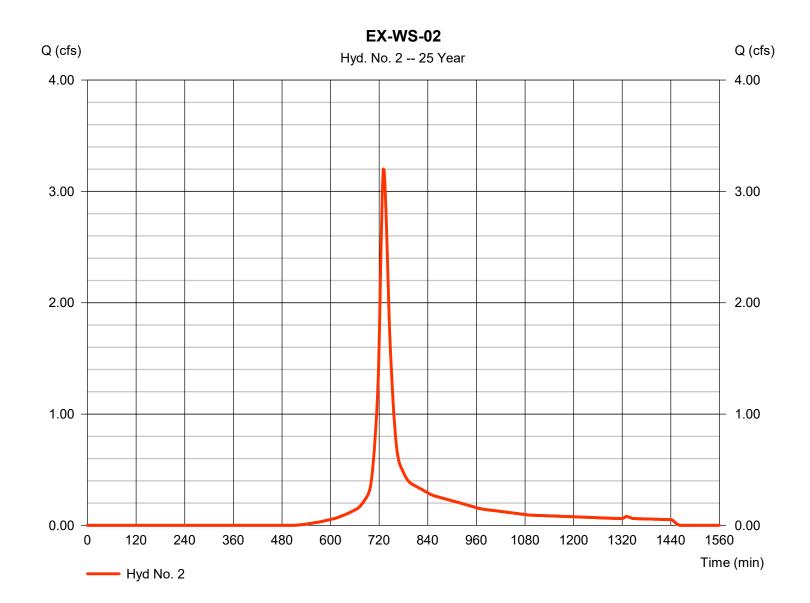
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 2

EX-WS-02

Hydrograph type = SCS Runoff Peak discharge = 3.202 cfsStorm frequency = 25 yrs Time to peak = 730 min Time interval = 2 min Hyd. volume = 13,075 cuftDrainage area Curve number = 1.098 ac= 71 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 16.40 min = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



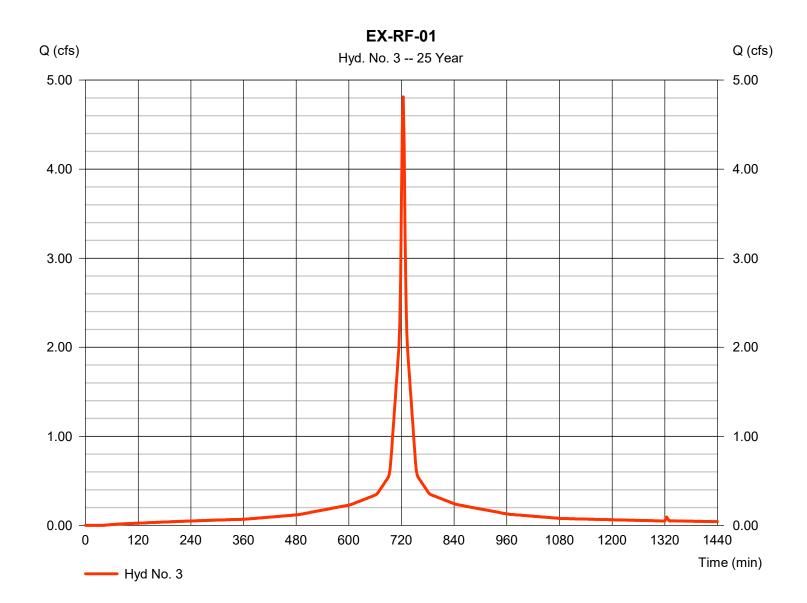
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 3

EX-RF-01

Hydrograph type = SCS Runoff Peak discharge = 4.812 cfsStorm frequency = 25 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 16,698 cuft Drainage area Curve number = 0.775 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



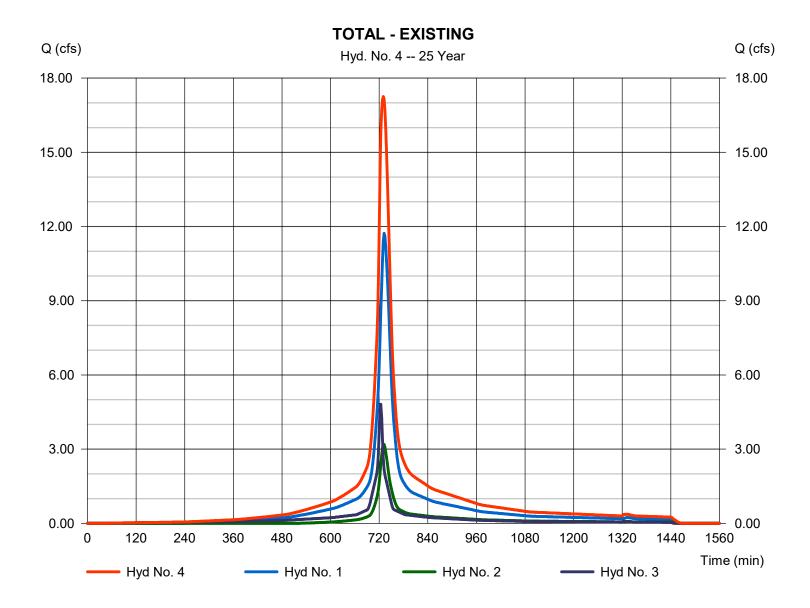
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 4

**TOTAL - EXISTING** 

= 17.25 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 25 yrs= 730 min Time interval = 2 min Hyd. volume = 83,894 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 4.677 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	13.50	2	732	62,477				EX-WS-01
2	SCS Runoff	3.910	2	730	15,920				EX-WS-02
3	SCS Runoff	5.454	2	724	18,991				EX-RF-01
	SCS Runoff Combine	5.454 20.05	2 2	724 730	18,991 97,722	1, 2, 3			EX-RF-01 TOTAL - EXISTING
F0173-02 Hydrographs - Existing.gpw				Return Period: 50 Year			Monday, 05 / 24 / 2021		

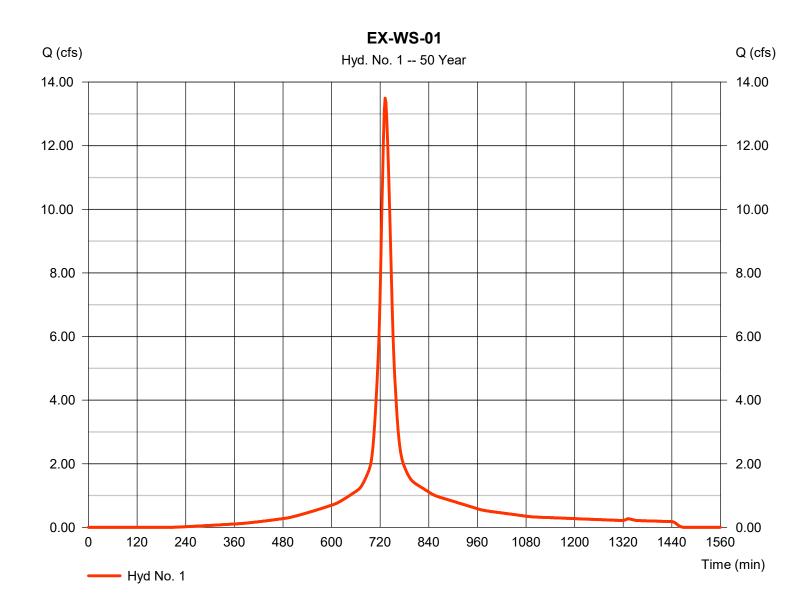
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

### Hyd. No. 1

EX-WS-01

Hydrograph type = SCS Runoff Peak discharge = 13.50 cfsStorm frequency = 50 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 62,477 cuft Drainage area Curve number = 2.804 ac= 89 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



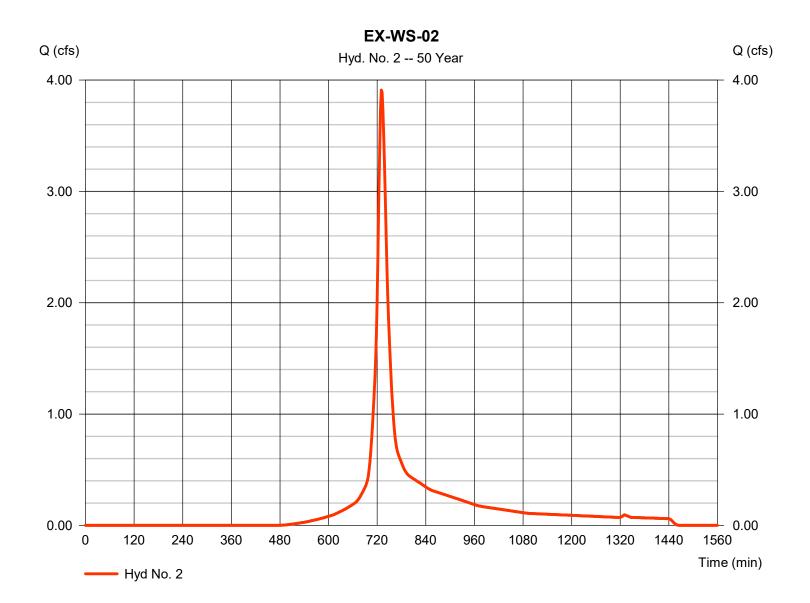
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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### Hyd. No. 2

EX-WS-02

Hydrograph type = SCS Runoff Peak discharge = 3.910 cfsStorm frequency = 50 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 15,920 cuftDrainage area Curve number = 1.098 ac= 71 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 16.40 min = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



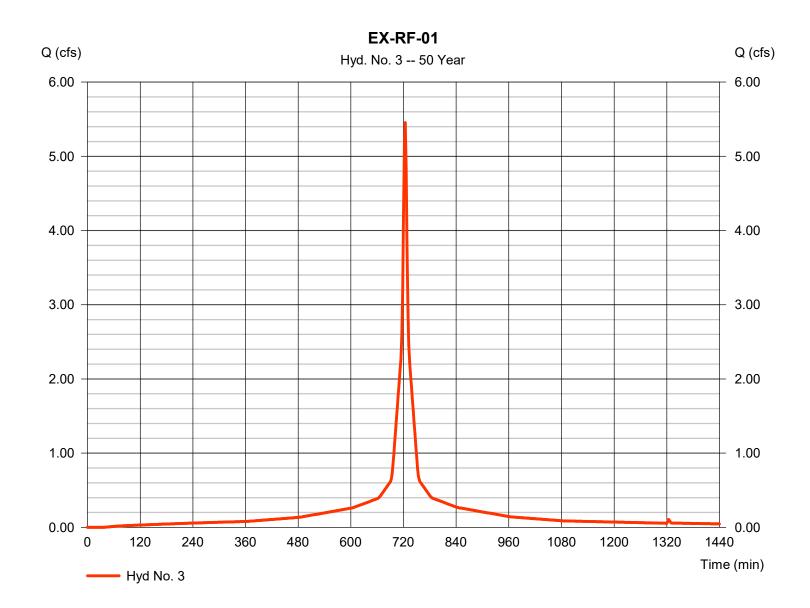
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 3

EX-RF-01

Hydrograph type = SCS Runoff Peak discharge = 5.454 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 18,991 cuft Drainage area Curve number = 0.775 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



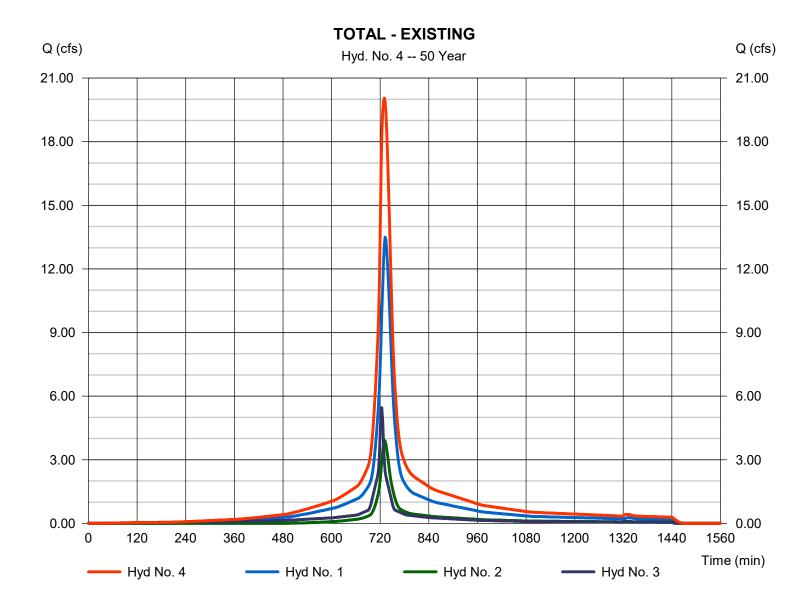
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type = Combine Peak discharge = 20.05 cfsStorm frequency Time to peak = 50 yrs= 730 min Time interval = 2 min Hyd. volume = 97,722 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 4.677 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	15.39	2	732	71,759				EX-WS-01
2	SCS Runoff	4.680	2	730	19,050				EX-WS-02
3	SCS Runoff	6.139	2	724	21,442				EX-RF-01
3 4	SCS Runoff Combine	6.139 23.05	2 2	724 730	21,442 112,636	1, 2, 3			EX-RF-01 TOTAL - EXISTING
	173-02 Hydro					Period: 100			5 / 24 / 2021

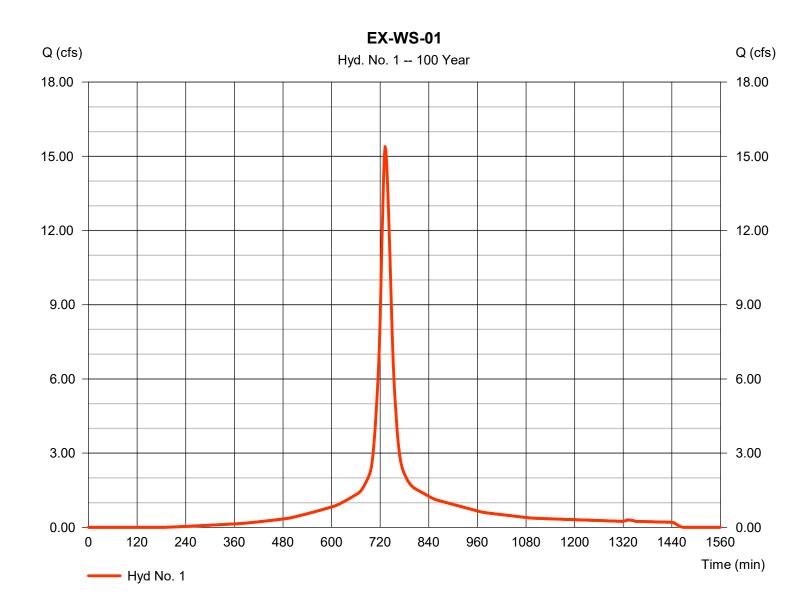
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 1

EX-WS-01

Hydrograph type = SCS Runoff Peak discharge = 15.39 cfsStorm frequency = 100 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 71,759 cuft Drainage area Curve number = 2.804 ac= 89 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 18.60 min = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



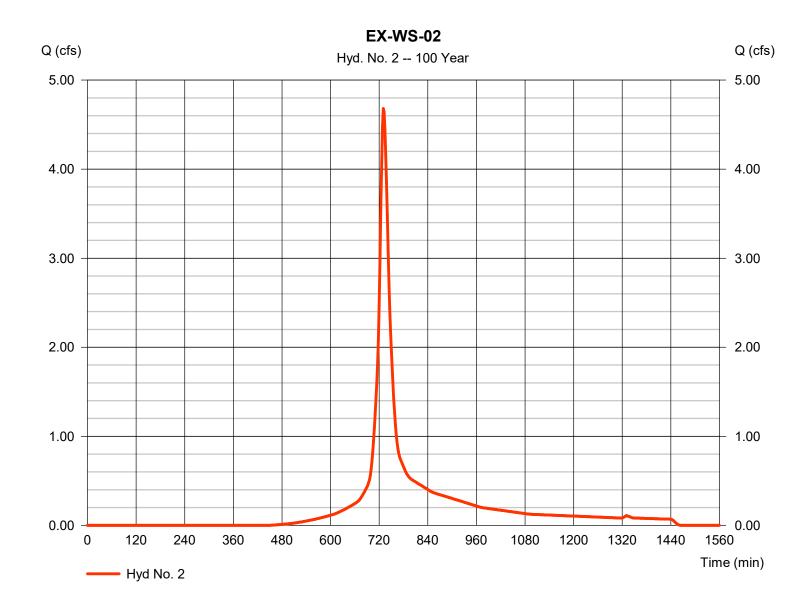
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 2

EX-WS-02

Hydrograph type = SCS Runoff Peak discharge = 4.680 cfsStorm frequency = 100 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 19,050 cuftCurve number Drainage area = 1.098 ac= 71 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 16.40 min = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



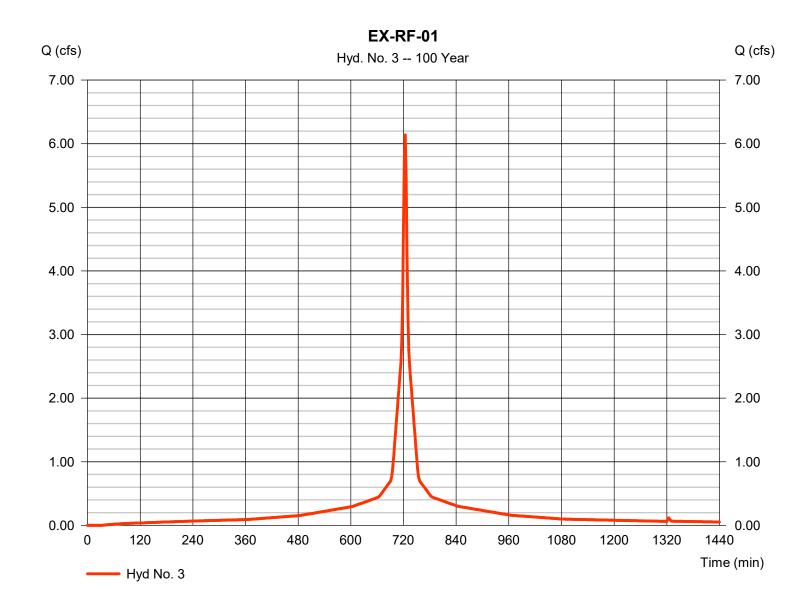
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 3

EX-RF-01

Hydrograph type = SCS Runoff Peak discharge = 6.139 cfsStorm frequency = 100 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 21,442 cuft Drainage area Curve number = 0.775 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



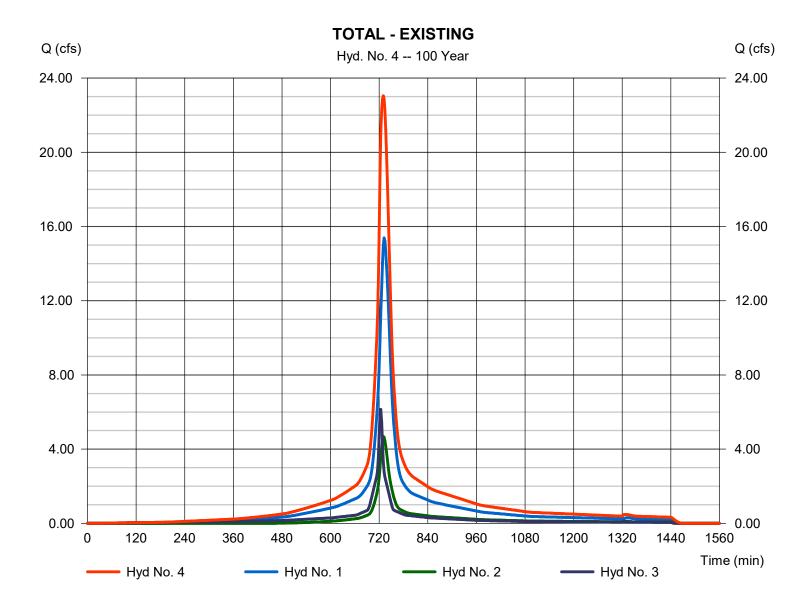
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Monday, 05 / 24 / 2021

## Hyd. No. 4

**TOTAL - EXISTING** 

Hydrograph type = Combine Peak discharge = 23.05 cfsStorm frequency Time to peak = 100 yrs= 730 min Time interval = 2 min Hyd. volume = 112,636 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 4.677 ac



**APPENDIX D** 

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-01

Location: Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.025	98	2.470
Landscaped and Lawns	0.082	69	5.682
	_		8.152

Total Area: 0.108 CN: 76

#### **Time of Concentration:**

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	130	0.030	14.2	

Total Tc (min) = 14.2

Name: CB-01A

**Location:** Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.008	98	0.778
Landscaped and Lawns	0.186	69	12.827
			13.606

Total Area: 0.194 CN: 70

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	50	0.020	7.8	

Total Tc (min) = \_\_\_\_ 7.8

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-02

Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.043	98	4.252
Landscaped and Lawns	0.010	69	0.719
			4.971

Total Area: 0.054 CN: 92

#### **Time of Concentration:**

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.015	3.54	98	0.050	1.0	

Total Tc (min) = 1.0

Minimum Tc = 5.0

Name: CB-03

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.057	98	5.620
Landscaped and Lawns	0.016	69	1.137
			6.757

Total Area: 0.074 CN: 92

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	60	0.033	0.8	

Total Tc (min) = 4.5

Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-04

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.044	98	4.320
Landscaped and Lawns	0.009	69	0.604
_			4.923

Total Area: 0.053 CN: 93

#### **Time of Concentration:**

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	55	0.045	0.7	

Total Tc (min) = 4.4
Minimum Tc = 5.0

Name: CB-05

Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.076	98	7.451
Landscaped and Lawns	0.039	69	2.706
			10.157

Total Area: 0.115 CN: 88

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	65	0.040	0.8

Total Tc (min) = 4.5

Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-06

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.047	98	4.628
Landscaped and Lawns	0.015	69	1.006
			5.634

Total Area: 0.062 CN: 91

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	22	0.020	4.0
B-C	0.015	3.54	58	0.025	0.9

Total Tc (min) = 4.9
Minimum Tc = 5.0

Name: CB-07

**Location:** Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.081	98	7.915
Landscaped and Lawns	0.018	69	1.243
			9.158

Total Area: 0.099 CN: 93

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	15	0.020	3.0
B-C	0.015	3.54	115	0.035	1.3

Total Tc (min) = 4.3

Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-08

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.094	98	9.249
Landscaped and Lawns	0.017	69	1.180
			10.429

Total Area: 0.111 CN: 94

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	30	0.040	3.9
B-C	0.015	3.54	140	0.035	1.5

Total Tc (min) = 5.5

Name: CB-09

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.117	98	11.445
Landscaped and Lawns	0.020	69	1.375
			12.820

Total Area: 0.137 CN: 94

#### Time of Concentration:

Sheet-Flow Travel Time						
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)	
A-B	0.24	3.54	20	0.020	3.7	
B-C	0.015	3.54	120	1.000	0.4	

Total Tc (min) = 4.1
Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: CB-10

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.104	98	10.153
Landscaped and Lawns	0.029	69	2.020
			12.173

Total Area: 0.133 CN: 92

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	30	0.040	3.9
B-C	0.015	3.54	135	1.000	0.4

Total Tc (min) = 4.3
Minimum Tc = 5.0

Name: CB-11

Location: Proposed Yard Drain - Southeast Corner Site

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.010	98	0.990
Landscaped and Lawns	0.217	69	14.945
			15.935

Total Area: 0.227 CN: 70

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	120	0.050	10.9

Total Tc (min) = 10.9

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: PP-01

Location: Proposed Porous Pavement - Southwest Parking Area

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.266	98	26.077
Landscaped and Lawns	0.005	69	0.317
		<u> </u>	26.394

Total Area: 0.271 CN: 98

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	100	0.020	1.5

Total Tc (min) = 1.5

Minimum Tc = 5.0

Name: PP-02

Location: Proposed Porous Pavement - Northwest Parking Area

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.393	98	38.505
Landscaped and Lawns	0.026	69	1.777
			40.282

Total Area: 0.419 CN: 96

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	40	0.040	4.9
B-C	0.015	3.54	60	0.016	1.1

Total Tc (min) = 6.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: RF-01

Location: Proposed Building - North

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.668	98	65.466
Landscaped and Lawns	0.000	69	0.000
			65.466

Total Area: 0.668 CN: 98

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = 1.0
Minimum Tc = 5.0

Name: RF-02

Location: Proposed Building - South

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.653	98	63.954
Landscaped and Lawns	0.000	69	0.000
			63.954

Total Area: 0.653 CN: 98

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = 1.0

Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: RF-03

**Location:** Proposed Building - Northwest

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.120	98	11.807
Landscaped and Lawns	0.000	69	0.000
			11.807

Total Area: 0.120 CN: 98

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = 1.0

Minimum Tc = 5.0

Name: RF-04

**Location:** Proposed Building - Southwest

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.115	98	11.274
Landscaped and Lawns	0.000	69	0.000
			11.274

Total Area: 0.115 CN: 98

#### Time of Concentration:

Sheet-Flow Travel Time								
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)			
A-B	0.015	3.54	50	0.015	1.0			

Total Tc (min) = 1.0
Minimum Tc = 5.0

### 141 Danbury Road Wilton, CT Proposed CN & Tc Worksheet



Name: PR-WS-01 Location: Site - West

Cover Type	Area (ac)	CN	A x CN
Pavement / Impervious	0.065	98	6.412
Landscaped and Lawns	0.975	69	67.267
			73.679

Total Area: 1.040 CN: 71

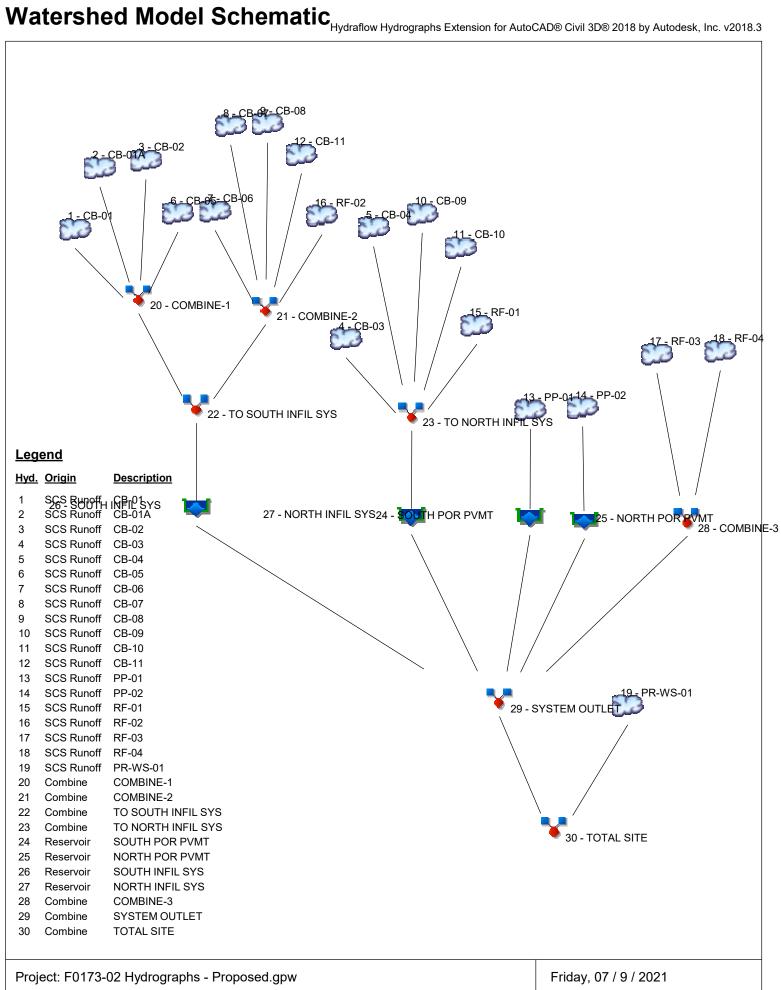
Time of Concentration: 71

Sheet-Flow Travel Time								
Segment ID	"n"	P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)						
A-B	0.24	3.54	130	0.008	24.1			

Shallow Concentrated Flow Travel Time										
Segment ID	Cover Flow Length (ft) Slope (ft/ft) V (ft/s) Time									
B-C	Unpaved	240	0.013	1.80	2.2					
C-D	Paved	165	0.013	2.27	1.2					

Total Tc (min) = 27.6

References: NRCS Technical Release 55 ConnDOT Drainage Manual, Chapter 6



# Hydrograph Return Period Recap Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd.	Hydrograph	ype hyd(s)	Peak Outflow (cfs)								Hydrograph
No.	type (origin)		1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			0.128			0.269	0.364	0.436	0.514	CB-01
2	SCS Runoff			0.195			0.475	0.671	0.822	0.987	CB-01A
3	SCS Runoff			0.159			0.259	0.321	0.366	0.415	CB-02
4	SCS Runoff			0.218			0.354	0.439	0.502	0.569	CB-03
5	SCS Runoff			0.160			0.257	0.318	0.363	0.410	CB-04
6	SCS Runoff			0.299			0.513	0.648	0.747	0.852	CB-05
7	SCS Runoff			0.177			0.292	0.364	0.417	0.473	CB-06
8	SCS Runoff			0.299			0.481	0.594	0.678	0.767	CB-07
9	SCS Runoff			0.344			0.546	0.672	0.766	0.865	CB-08
10	SCS Runoff			0.424			0.674	0.830	0.945	1.068	CB-09
11	SCS Runoff			0.392			0.637	0.790	0.902	1.023	CB-10
12	SCS Runoff			0.212			0.510	0.720	0.883	1.061	CB-11
13	SCS Runoff			0.900			1.381	1.683	1.907	2.147	PP-01
14	SCS Runoff			1.352			2.106	2.577	2.926	3.298	PP-02
15	SCS Runoff			2.218			3.404	4.148	4.701	5.291	RF-01
16	SCS Runoff			2.168			3.327	4.055	4.595	5.172	RF-02
17	SCS Runoff			0.398			0.611	0.745	0.844	0.951	RF-03
18	SCS Runoff			0.382			0.586	0.714	0.809	0.911	RF-04
19	SCS Runoff			0.734			1.726	2.421	2.955	3.537	PR-WS-01
20	Combine	1, 2, 3,		0.722			1.409	1.865	2.210	2.583	COMBINE-1
21	Combine	6, 7, 8, 9,		3.147			5.059	6.276	7.186	8.161	COMBINE-2
22	Combine	12, 16, 20, 21		3.869			6.468	8.142	9.396	10.74	TO SOUTH INFIL SYS
23	Combine	4, 5, 10,		3.412			5.327	6.525	7.413	8.361	TO NORTH INFIL SYS
24	Reservoir	11, 15, 13		0.000			0.000	0.036	0.106	0.191	SOUTH POR PVMT
25	Reservoir	14		0.000			0.000	0.031	0.105	0.200	NORTH POR PVMT
26	Reservoir	22		0.241			2.347	3.888	5.328	7.056	SOUTH INFIL SYS
27	Reservoir	23		0.583			2.771	4.442	5.575	6.513	NORTH INFIL SYS
28	Combine	17, 18,		0.780			1.197	1.459	1.654	1.861	COMBINE-3
29	Combine	24, 25, 26,		0.917			5.271	8.975	11.51	14.90	SYSTEM OUTLET
30	Combine	27, 28 19, 29		1.636			6.762	10.69	13.64	17.35	TOTAL SITE

Proj. file: F0173-02 Hydrographs - Proposed.gpw

Friday, 07 / 9 / 2021

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.128	2	732	533				CB-01
2	SCS Runoff	0.195	2	728	727				CB-01A
3	SCS Runoff	0.159	2	724	492				CB-02
4	SCS Runoff	0.218	2	724	674				CB-03
5	SCS Runoff	0.160	2	724	500				CB-04
6	SCS Runoff	0.299	2	724	902				CB-05
7	SCS Runoff	0.177	2	724	544				CB-06
8	SCS Runoff	0.299	2	724	934				CB-07
9	SCS Runoff	0.344	2	724	1,086				CB-08
10	SCS Runoff	0.424	2	724	1,340				CB-09
11	SCS Runoff	0.392	2	724	1,211				CB-10
12	SCS Runoff	0.212	2	730	878				CB-11
13	SCS Runoff	0.900	2	724	3,049				PP-01
14	SCS Runoff	1.352	2	724	4,399				PP-02
15	SCS Runoff	2.218	2	724	7,516				RF-01
16	SCS Runoff	2.168	2	724	7,347				RF-02
17	SCS Runoff	0.398	2	724	1,350				RF-03
18	SCS Runoff	0.382	2	724	1,294				RF-04
19	SCS Runoff	0.734	2	742	4,104				PR-WS-01
20	Combine	0.722	2	724	2,654	1, 2, 3,			COMBINE-1
21	Combine	3.147	2	724	10,790	6, 7, 8, 9,			COMBINE-2
22	Combine	3.869	2	724	13,444	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	3.412	2	724	11,241	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.000	2	760	0	11, 15, 13	141.82	897	SOUTH POR PVMT
25	Reservoir	0.000	2	732	0	14	141.31	1,336	NORTH POR PVMT
26	Reservoir	0.241	2	760	1,021	22	143.05	5,230	SOUTH INFIL SYS
27	Reservoir	0.583	2	746	1,717	23	143.36	4,356	NORTH INFIL SYS
28	Combine	0.780	2	724	2,644	17, 18,			COMBINE-3
29	Combine	0.917	2	748	5,382	24, 25, 26,			SYSTEM OUTLET
30	Combine	1.636	2	746	9,487	27, 28 19, 29			TOTAL SITE
F01	F0173-02 Hydrographs - Proposed.gpw			Return F	Period: 2 Ye	ear	Friday, 07 / 9 / 2021		

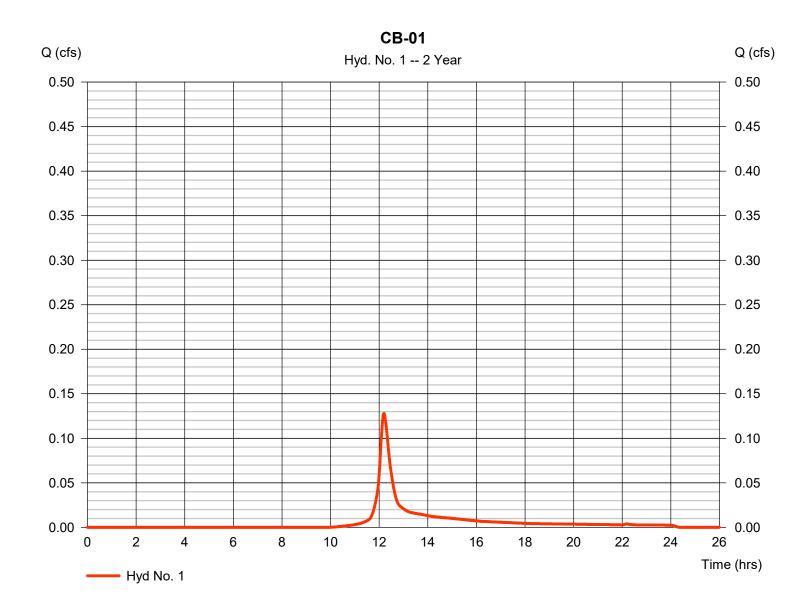
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 1

CB-01

Hydrograph type = SCS Runoff Peak discharge = 0.128 cfsStorm frequency = 2 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 533 cuft Drainage area Curve number = 0.108 ac= 76 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 14.20 min = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



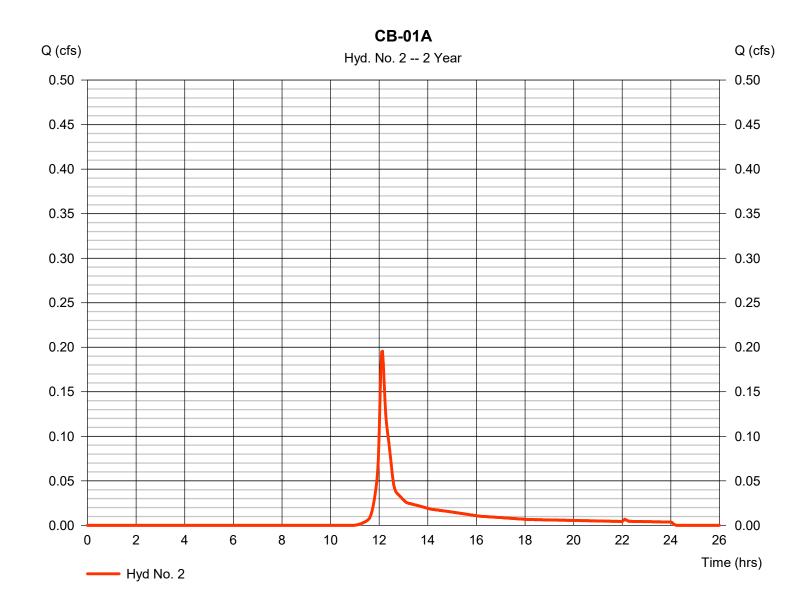
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 2

**CB-01A** 

Hydrograph type = SCS Runoff Peak discharge = 0.195 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 727 cuft Drainage area Curve number = 0.194 ac= 70 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 7.80 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



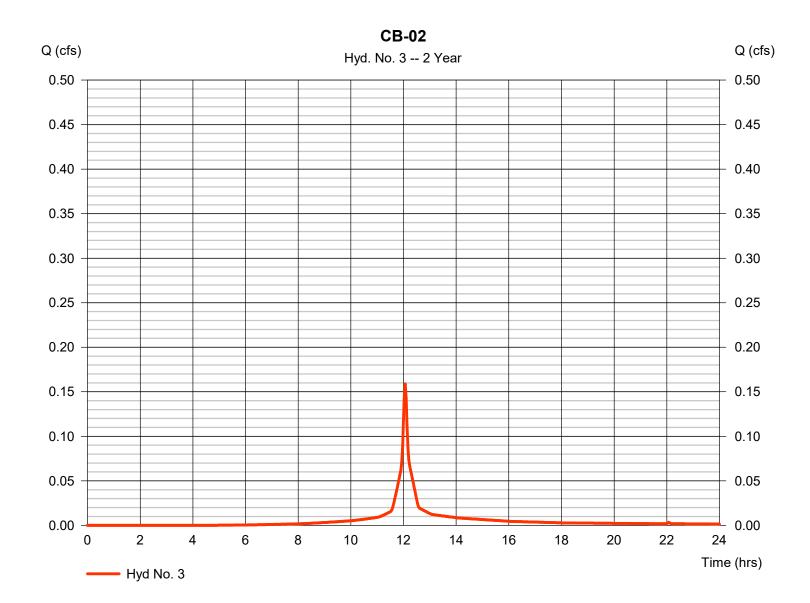
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 3

**CB-02** 

Hydrograph type = SCS Runoff Peak discharge = 0.159 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 492 cuft Drainage area Curve number = 0.054 ac= 92 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



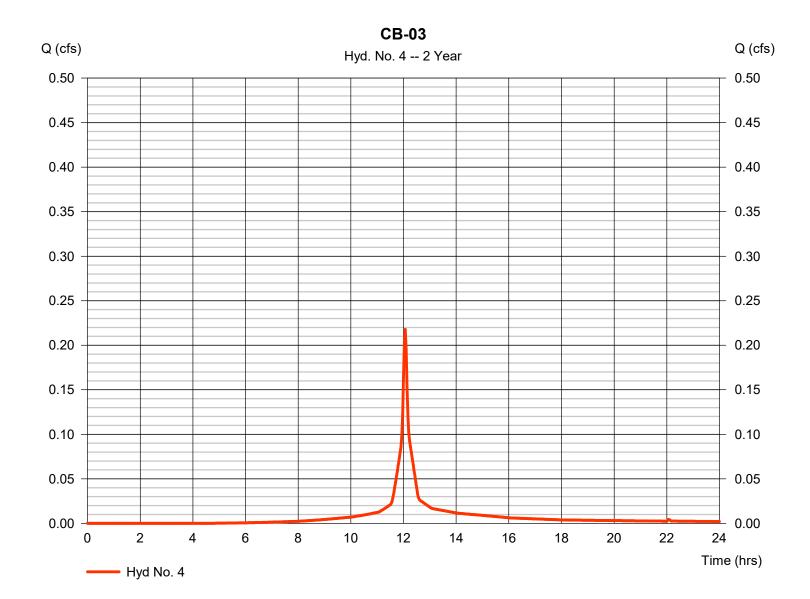
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 4

**CB-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.218 cfsStorm frequency Time to peak = 2 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 674 cuft Drainage area = 0.074 acCurve number = 92 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



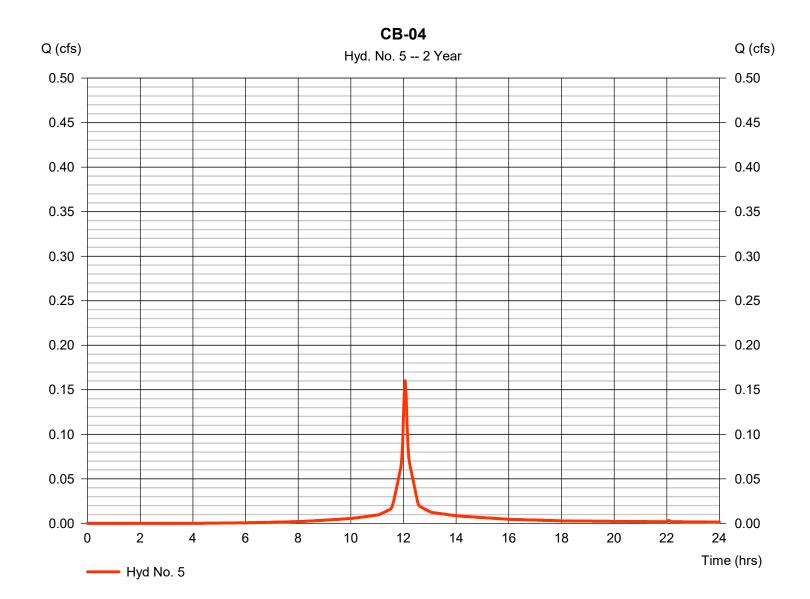
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 5

**CB-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.160 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 500 cuft Drainage area Curve number = 0.053 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



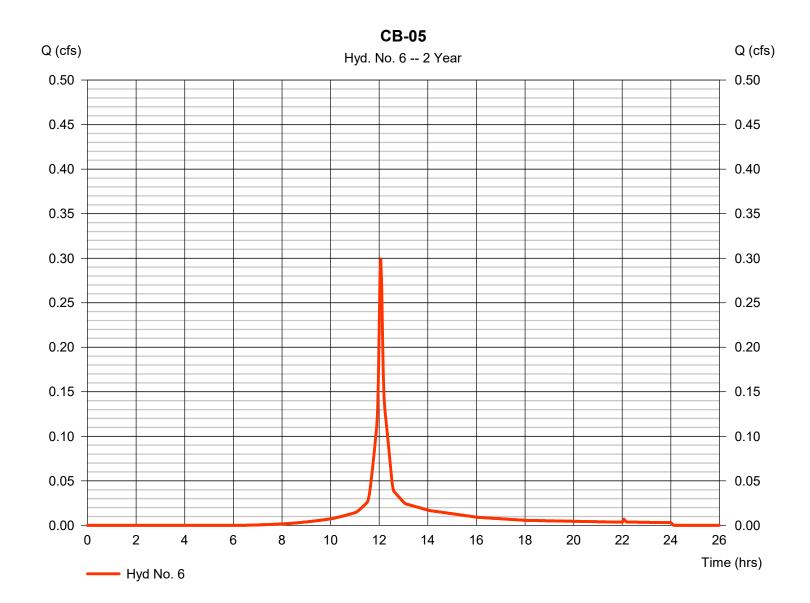
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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### Hyd. No. 6

**CB-05** 

Hydrograph type = SCS Runoff Peak discharge = 0.299 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 902 cuft Drainage area = 0.115 acCurve number = 88 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



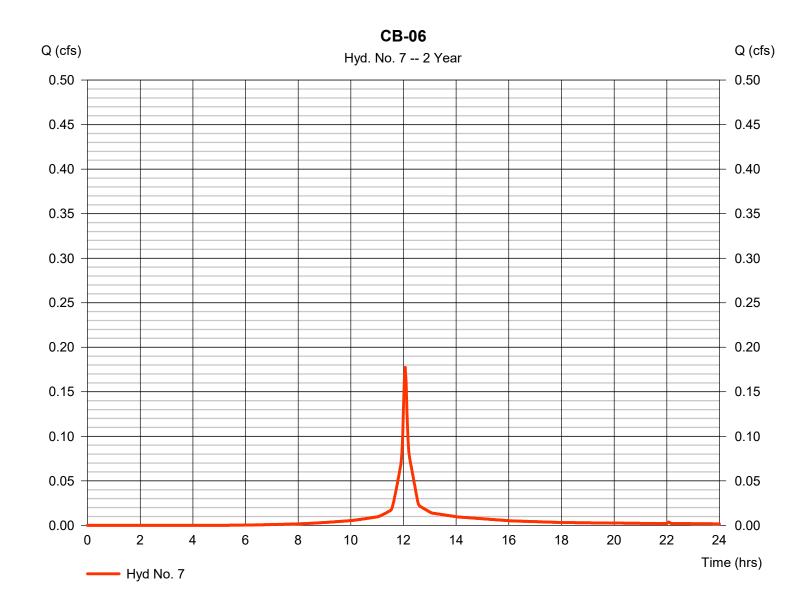
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 7

**CB-06** 

Hydrograph type = SCS Runoff Peak discharge = 0.177 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 544 cuft Drainage area Curve number = 0.062 ac= 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



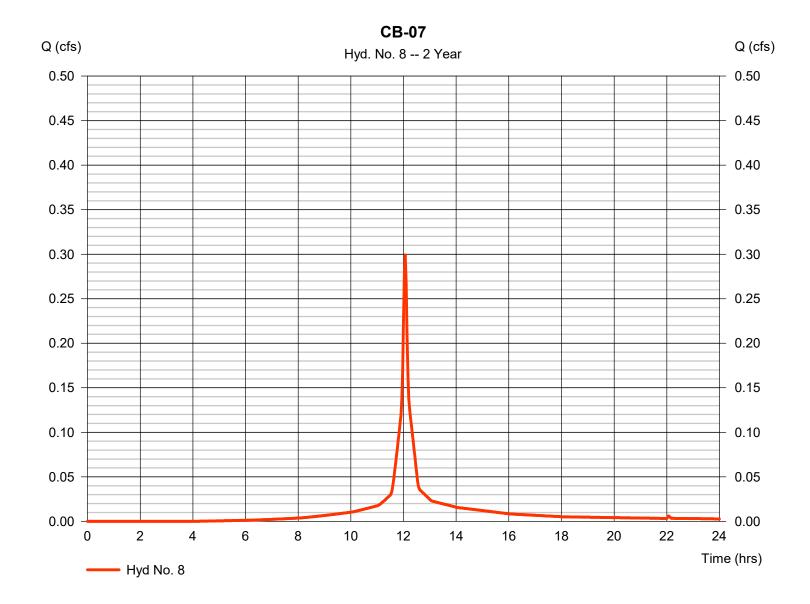
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Friday, 07 / 9 / 2021

## Hyd. No. 8

**CB-07** 

Hydrograph type = SCS Runoff Peak discharge = 0.299 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 934 cuft Drainage area Curve number = 0.099 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



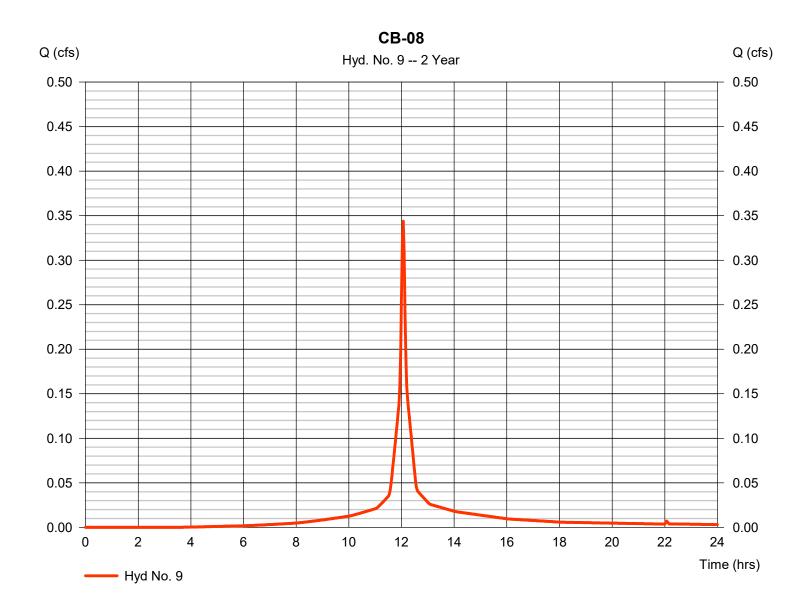
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 9

**CB-08** 

Hydrograph type = SCS Runoff Peak discharge = 0.344 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 1,086 cuftDrainage area Curve number = 0.111 ac= 94 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.50 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



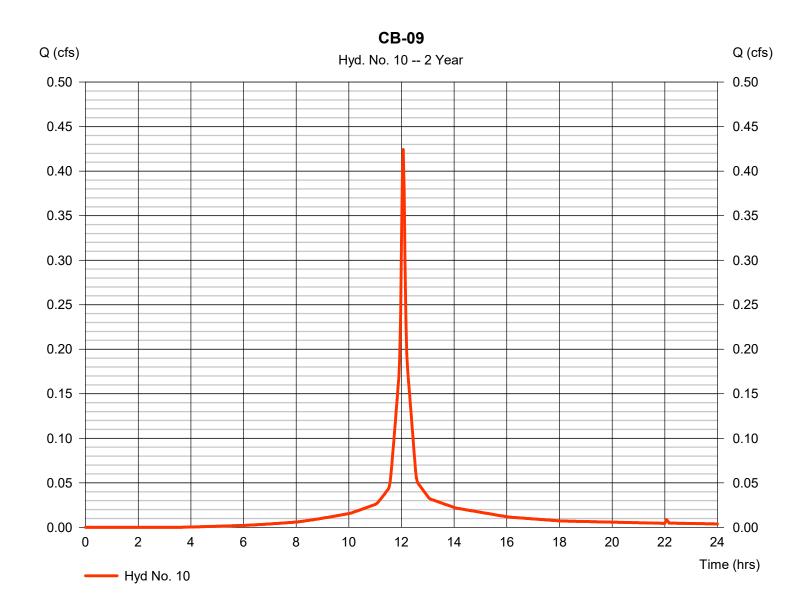
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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## Hyd. No. 10

**CB-09** 

Hydrograph type = SCS Runoff Peak discharge = 0.424 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 1,340 cuftDrainage area Curve number = 0.137 ac= 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



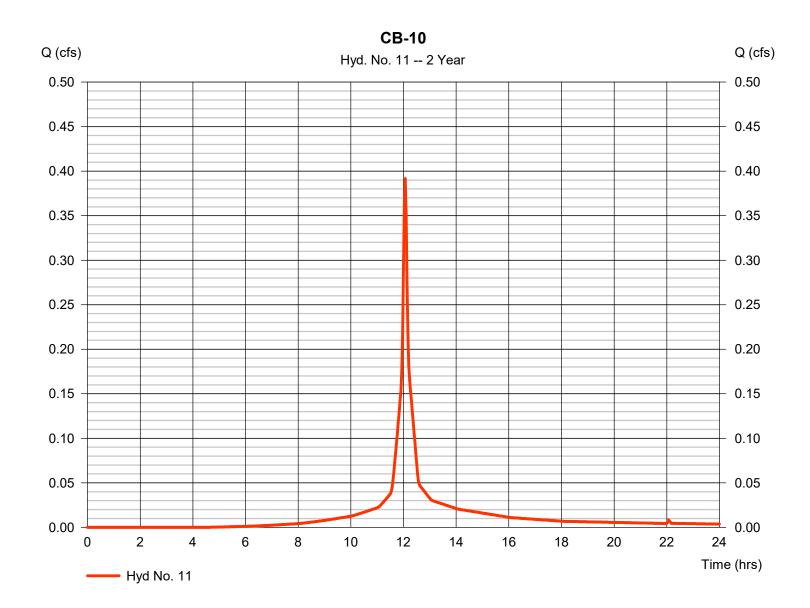
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

## Hyd. No. 11

**CB-10** 

Hydrograph type = SCS Runoff Peak discharge = 0.392 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,211 cuft Drainage area Curve number = 0.133 ac= 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



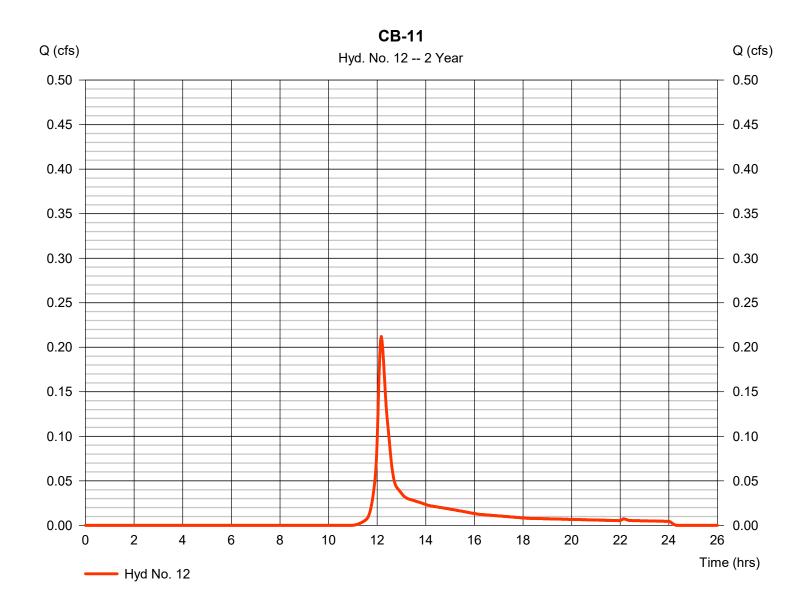
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## Hyd. No. 12

**CB-11** 

Hydrograph type = SCS Runoff Peak discharge = 0.212 cfsStorm frequency = 2 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 878 cuft Drainage area = 70 = 0.227 acCurve number Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 10.90 min = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



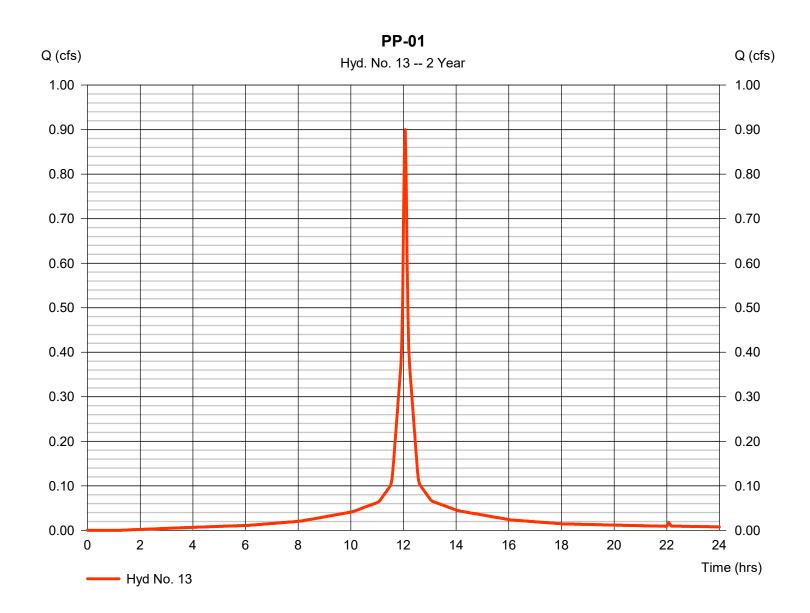
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## **Hyd. No. 13**

PP-01

Hydrograph type = SCS Runoff Peak discharge = 0.900 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,049 cuftDrainage area = 0.271 acCurve number = 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



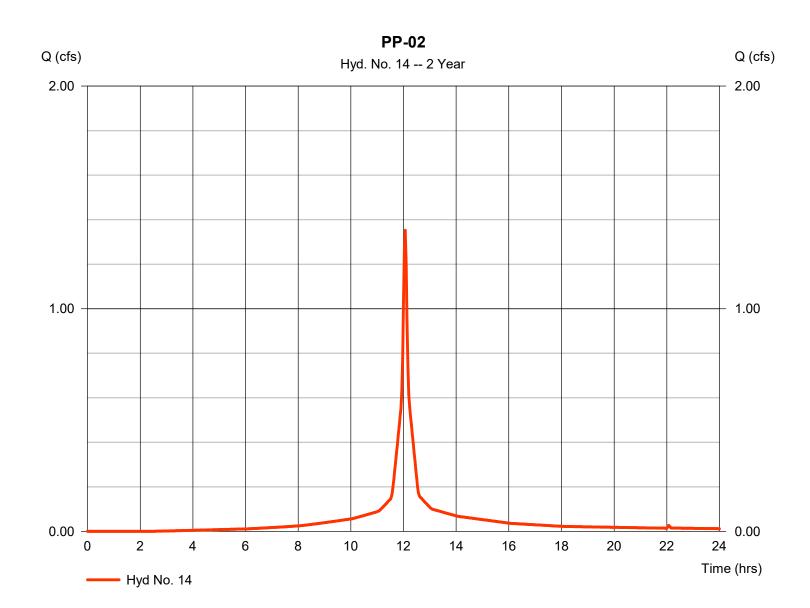
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## Hyd. No. 14

PP-02

Hydrograph type = SCS Runoff Peak discharge = 1.352 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,399 cuftDrainage area = 0.419 acCurve number = 96 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 6.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



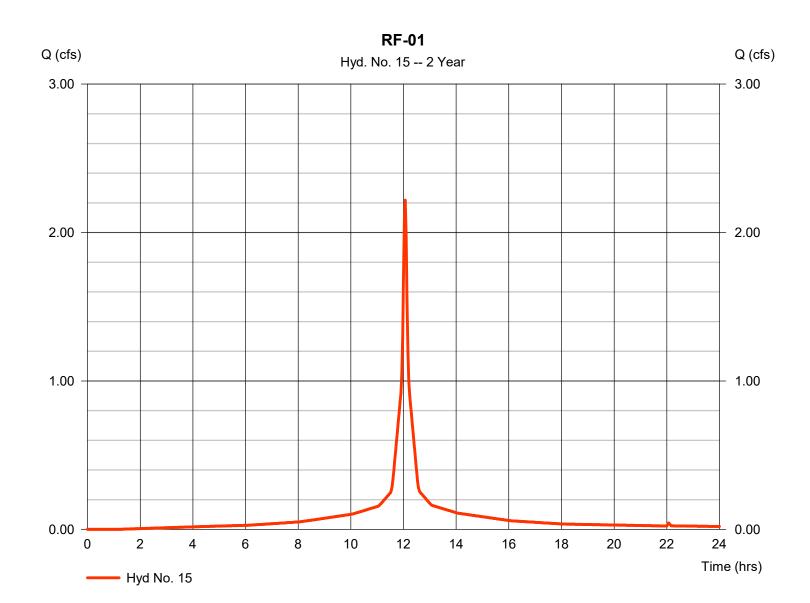
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#### Hyd. No. 15

**RF-01** 

Hydrograph type = SCS Runoff Peak discharge = 2.218 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 7,516 cuft Drainage area = 0.668 acCurve number = 98 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



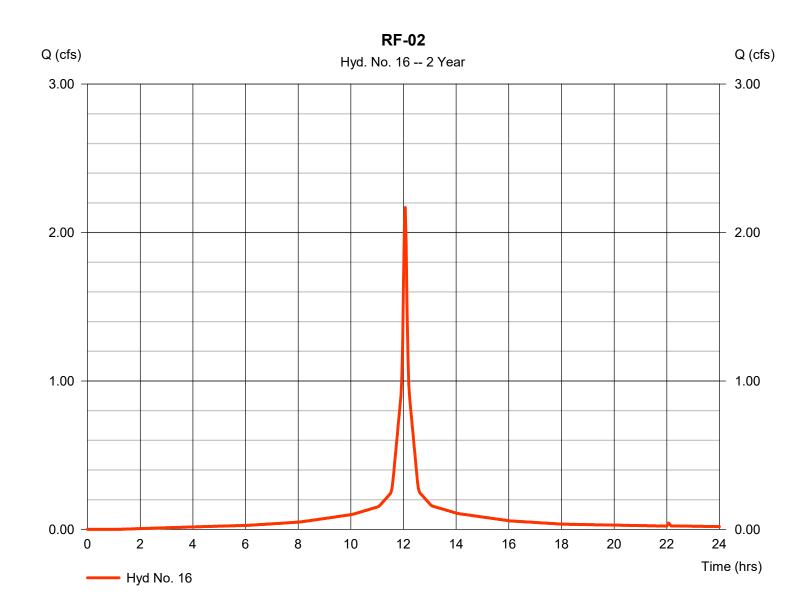
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#### Hyd. No. 16

**RF-02** 

Hydrograph type = SCS Runoff Peak discharge = 2.168 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7,347 cuftDrainage area Curve number = 0.653 ac= 98 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



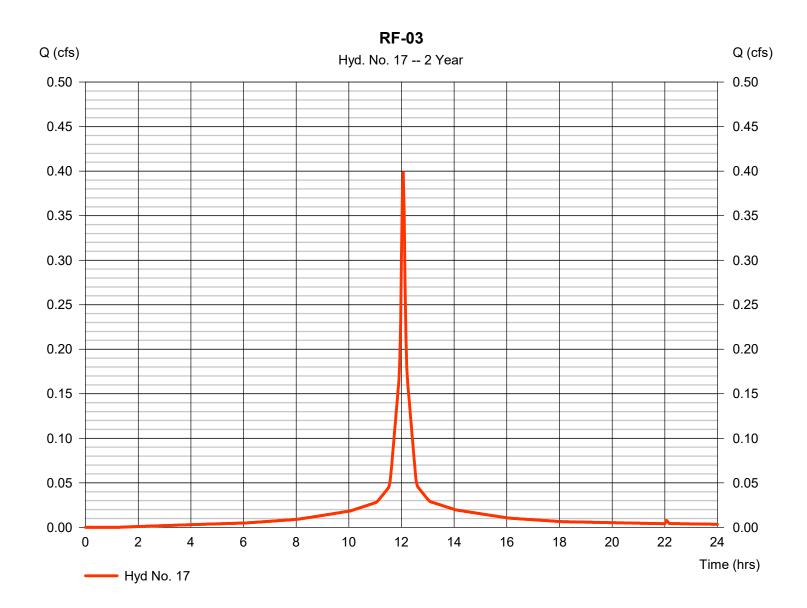
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#### Hyd. No. 17

**RF-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.398 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,350 cuftDrainage area = 0.120 acCurve number = 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



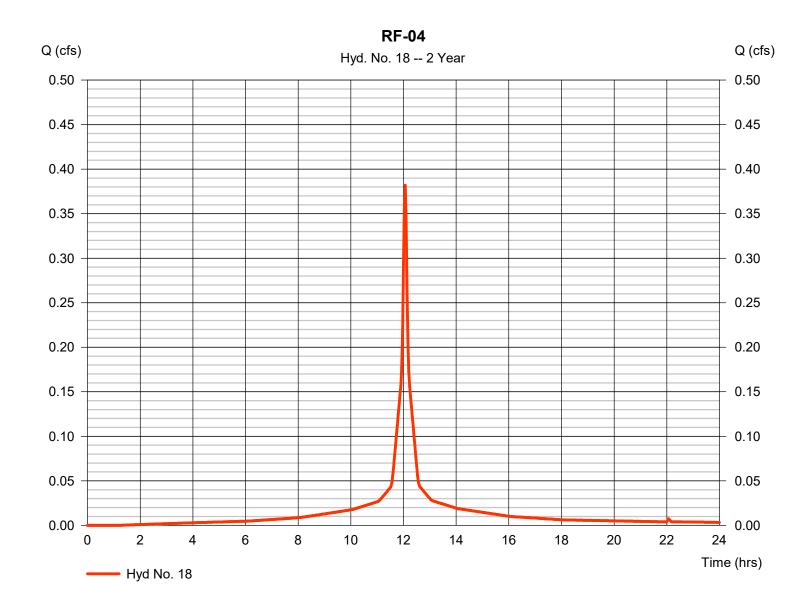
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#### Hyd. No. 18

**RF-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.382 cfsStorm frequency = 2 yrsTime to peak  $= 12.07 \, hrs$ = 1,294 cuft Time interval = 2 min Hyd. volume Drainage area = 0.115 acCurve number = 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



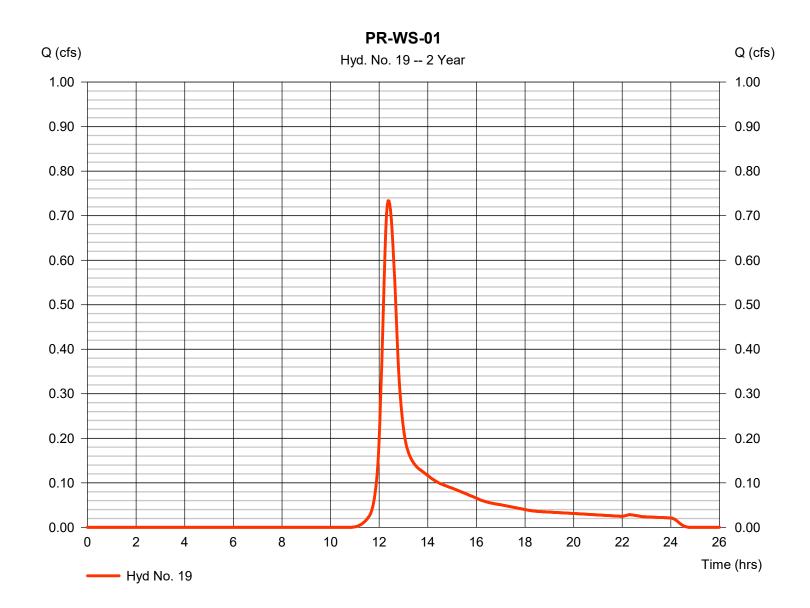
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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### Hyd. No. 19

PR-WS-01

Hydrograph type = SCS Runoff Peak discharge = 0.734 cfsStorm frequency = 2 yrsTime to peak  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 4,104 cuftDrainage area Curve number = 71 = 1.038 acHydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 27.60 min = User Total precip. = 3.54 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



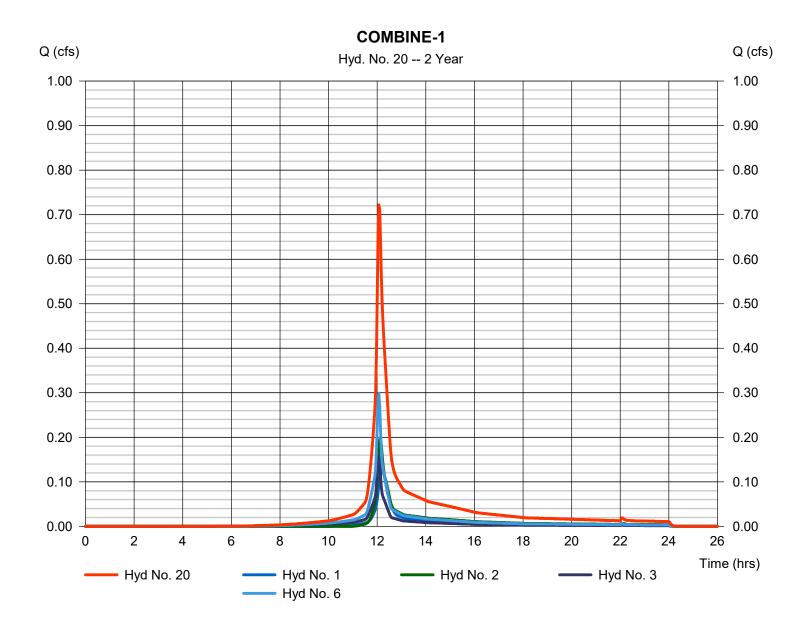
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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### Hyd. No. 20

**COMBINE-1** 

Hydrograph type = Combine Peak discharge = 0.722 cfsStorm frequency Time to peak = 2 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,654 cuft Inflow hyds. = 1, 2, 3, 6Contrib. drain. area = 0.471 ac



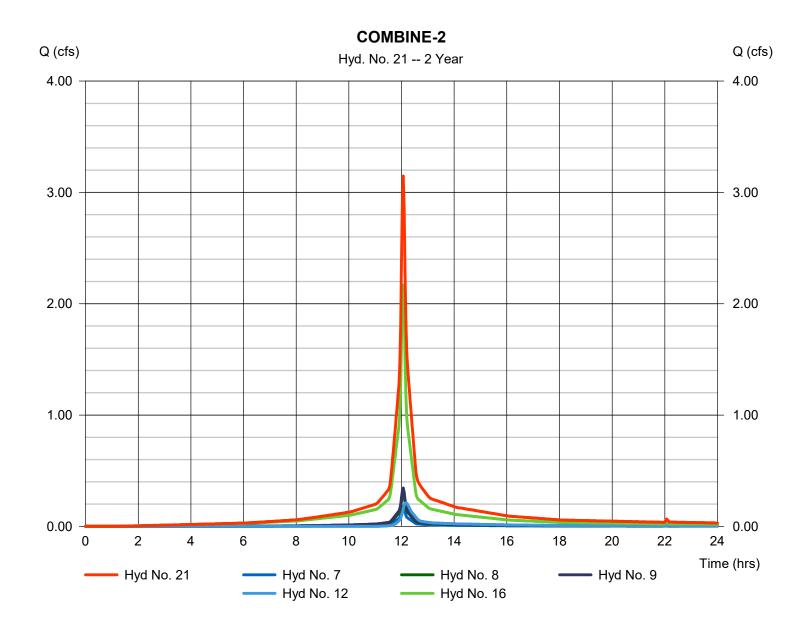
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### Hyd. No. 21

**COMBINE-2** 

Hydrograph type = Combine Peak discharge = 3.147 cfsStorm frequency Time to peak = 2 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 10,790 cuftInflow hyds. = 7, 8, 9, 12, 16 Contrib. drain. area = 1.152 ac



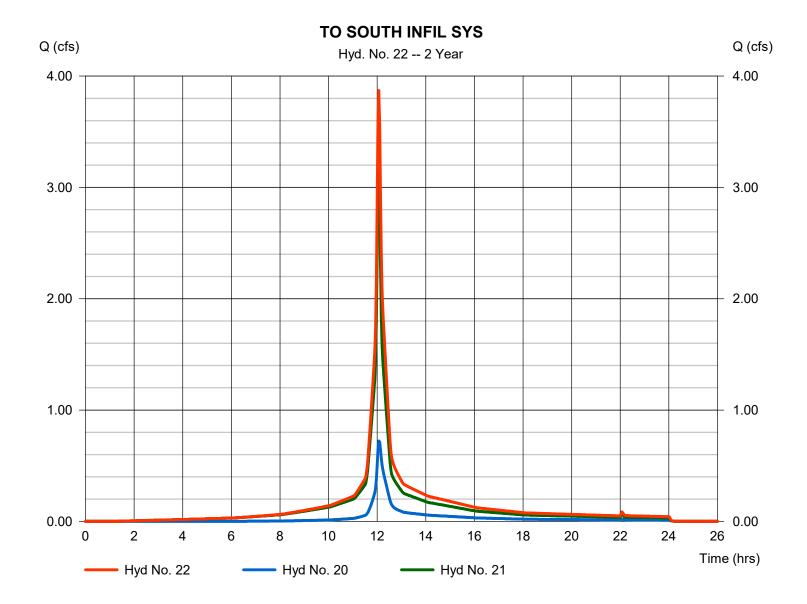
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#### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type = Combine Peak discharge = 3.869 cfsTime to peak Storm frequency = 2 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 13,444 cuft Inflow hyds. = 20, 21 Contrib. drain. area = 0.000 ac



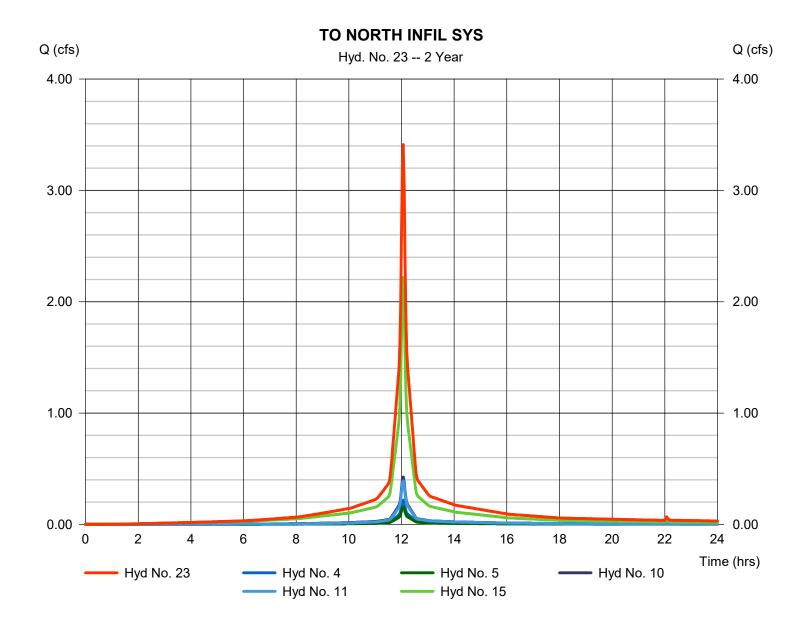
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### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type = Combine Peak discharge = 3.412 cfsStorm frequency Time to peak = 2 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 11,241 cuft Inflow hyds. = 4, 5, 10, 11, 15 Contrib. drain. area = 1.065 ac



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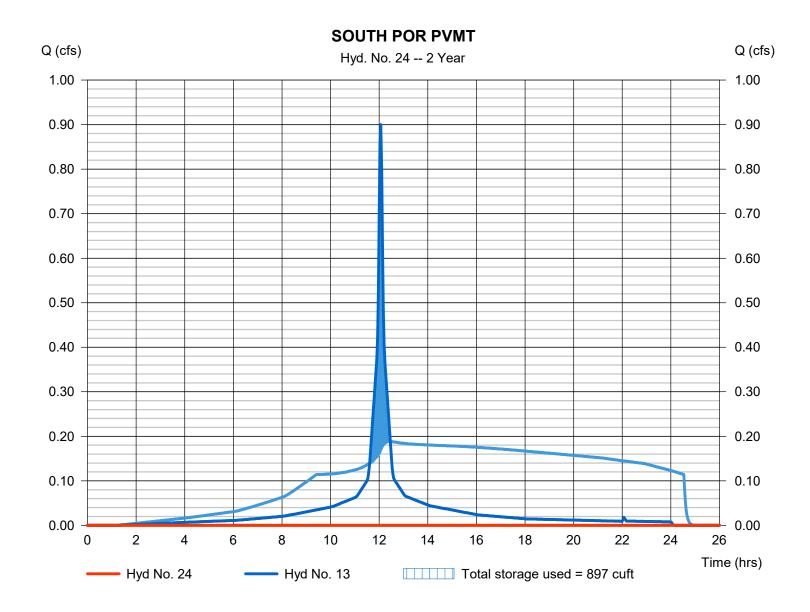
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#### Hyd. No. 24

#### SOUTH POR PVMT

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 12.67 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. Max. Elevation = 13 - PP-01 = 141.82 ft= SOUTH POROUS PVMT Reservoir name Max. Storage = 897 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Pond No. 3 - SOUTH POROUS PVMT

#### **Pond Data**

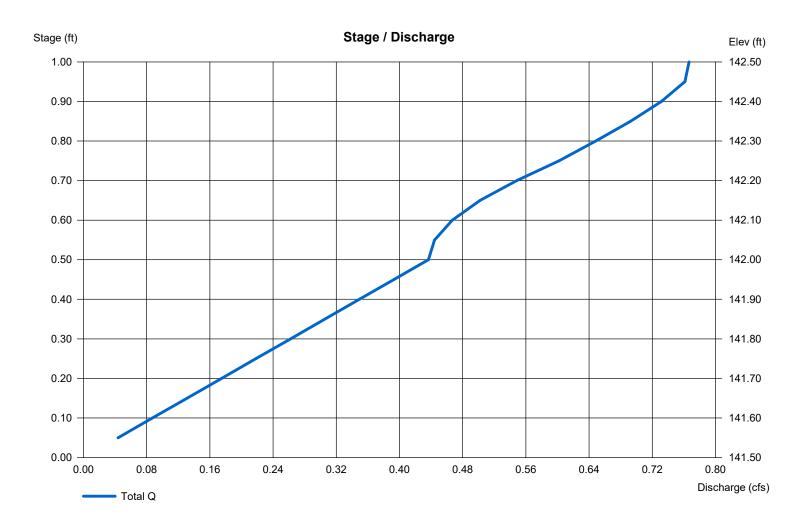
Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 141.50 ft. Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.50	9,430	0	0
0.50	142.00	9,430	1,414	1,414
1.00	142.50	9,430	1,414	2,829

Culvert / Orifice Structures					Weir Structures					
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 6.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00	
Span (in)	= 6.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00	
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33	
Invert El. (ft)	= 142.00	0.00	0.00	0.00	Weir Type	=				
Length (ft)	= 10.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 1.00	0.00	0.00	n/a						
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by	(Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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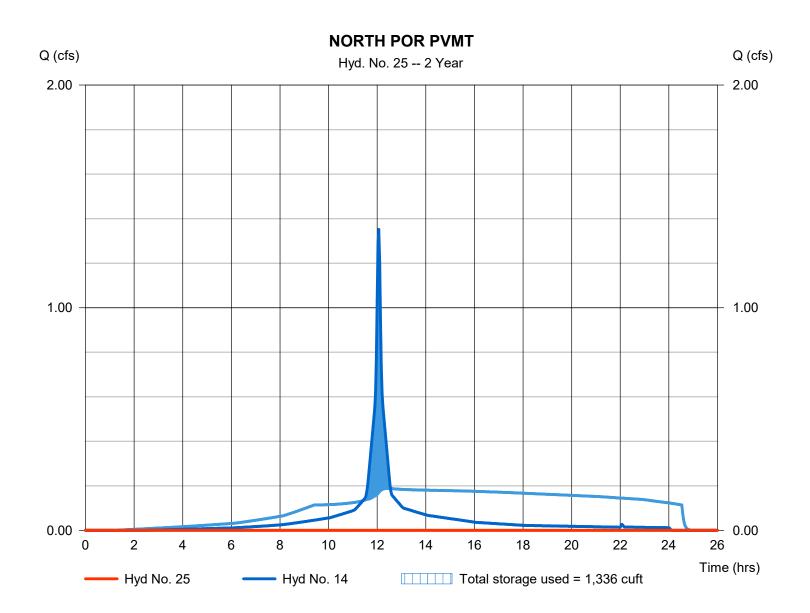
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### Hyd. No. 25

#### NORTH POR PVMT

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Max. Elevation Inflow hyd. No. = 14 - PP-02  $= 141.31 \, \text{ft}$ = NORTH POROUS PVMT Reservoir name Max. Storage = 1,336 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Pond No. 4 - NORTH POROUS PVMT

#### **Pond Data**

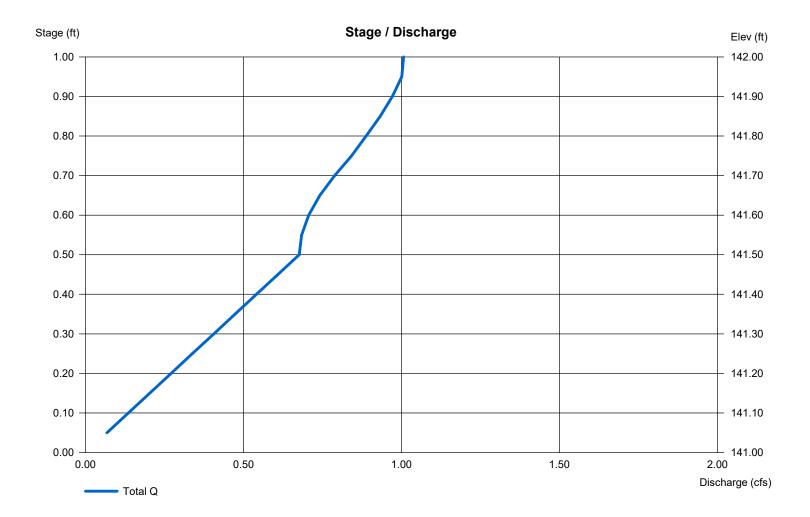
Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 141.00 ft. Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	14,607	0	0
0.50	141.50	14,607	2,191	2,191
1.00	142.00	14,607	2,191	4,382

Culvert / Ori	fice Structur	Weir Structures							
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 6.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 6.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 141.50	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 10.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a	_				
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by	(Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00	•		

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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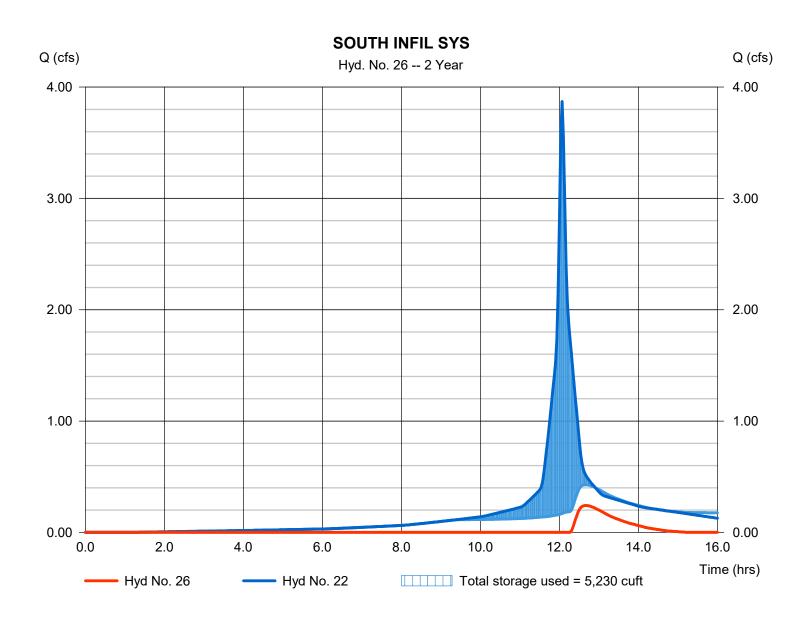
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#### Hyd. No. 26

**SOUTH INFIL SYS** 

Hydrograph type = Reservoir Peak discharge = 0.241 cfsStorm frequency = 2 yrsTime to peak  $= 12.67 \, hrs$ Time interval = 2 min Hyd. volume = 1,021 cuftMax. Elevation Inflow hyd. No. = 22 - TO SOUTH INFIL SYS  $= 143.05 \, \text{ft}$ = SOUTH INFIL SYS Reservoir name Max. Storage = 5,230 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Pond No. 1 - SOUTH INFIL SYS

#### **Pond Data**

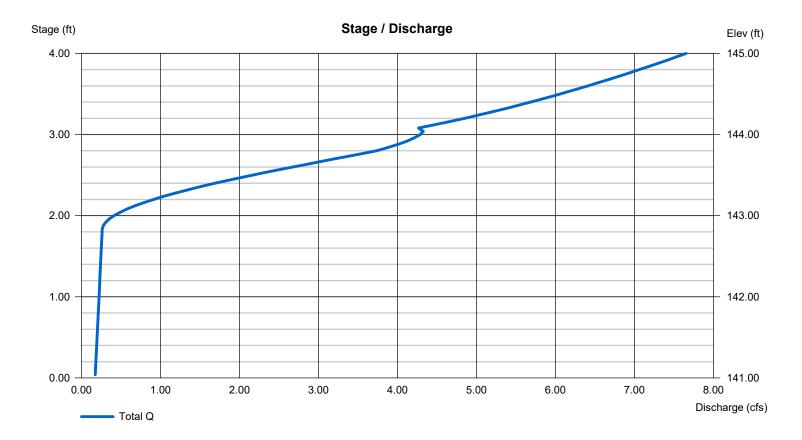
**UG Chambers** -Invert elev. = 142.00 ft, Rise x Span = 2.00 x 7.00 ft, Barrel Len = 170.00 ft, No. Barrels = 3, Slope = 0.00%, Headers = Yes **Encasement** -Invert elev. = 141.00 ft, Width = 7.00 ft, Height = 4.00 ft, Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	n/a	0	0
0.40	141.40	n/a	464	464
0.80	141.80	n/a	464	928
1.20	142.20	n/a	1,005	1,932
1.60	142.60	n/a	1,546	3,478
2.00	143.00	n/a	1,546	5,024
2.40	143.40	n/a	1,546	6,570
2.80	143.80	n/a	1,546	8,116
3.20	144.20	n/a	1,005	9,121
3.60	144.60	n/a	464	9,584
4.00	145.00	n/a	464	10,048

#### **Culvert / Orifice Structures Weir Structures** [B] [PrfRsr] [A] [A] [C] [B] [C] [D] = 15.00 0.00 0.00 0.00 Inactive 0.00 Inactive 0.00 Rise (in) Crest Len (ft) Span (in) = 15.000.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 142.83 0.00 0.00 0.00 Weir Type = Rect = 38.00 0.00 0.00 0.00 Multi-Stage = Yes No No No Length (ft) 0.00 0.00 n/a = 1.00 Slope (%) = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 2.000 (by Wet area) No No Multi-Stage = n/aNo TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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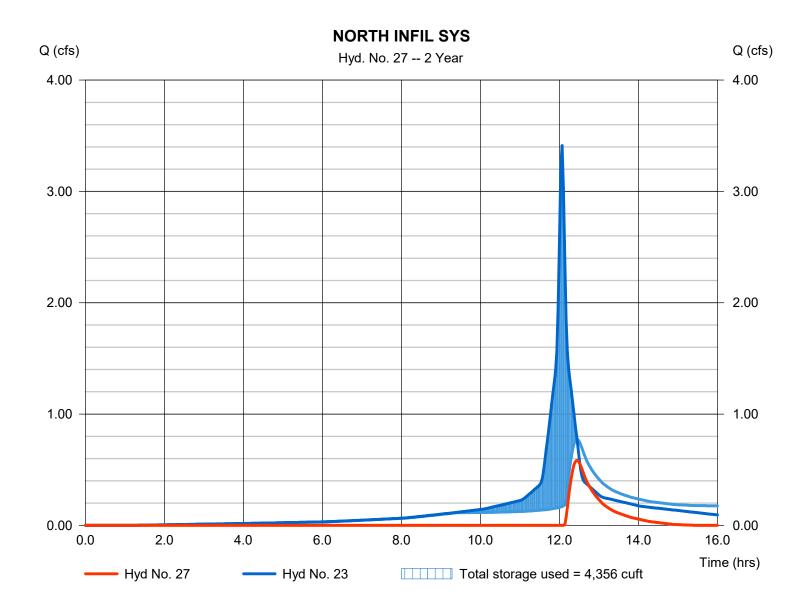
Friday, 07 / 9 / 2021

### Hyd. No. 27

**NORTH INFIL SYS** 

Hydrograph type Peak discharge = 0.583 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 12.43 \, hrs$ Time interval = 2 min Hyd. volume = 1,717 cuftMax. Elevation Inflow hyd. No. = 23 - TO NORTH INFIL SYS = 143.36 ft= NORTH INFIL SYS Reservoir name Max. Storage = 4,356 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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#### Pond No. 2 - NORTH INFIL SYS

#### **Pond Data**

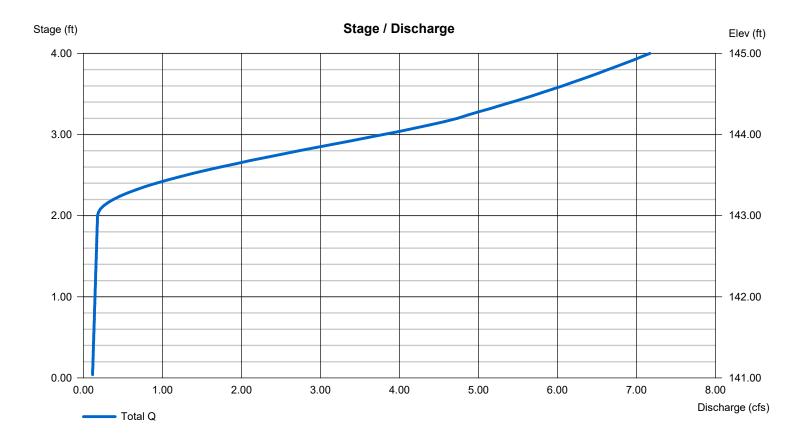
**UG Chambers** -Invert elev. = 142.00 ft, Rise x Span = 2.00 x 7.00 ft, Barrel Len = 80.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = Yes **Encasement** -Invert elev. = 141.00 ft, Width = 7.00 ft, Height = 4.00 ft, Voids = 30.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	141.00	n/a	0	0
0.40	141.40	n/a	316	316
0.80	141.80	n/a	316	632
1.20	142.20	n/a	684	1,316
1.60	142.60	n/a	1,053	2,369
2.00	143.00	n/a	1,053	3,422
2.40	143.40	n/a	1,053	4,475
2.80	143.80	n/a	1,053	5,528
3.20	144.20	n/a	684	6,213
3.60	144.60	n/a	316	6,528
4.00	145.00	n/a	316	6,844

#### **Culvert / Orifice Structures Weir Structures** [B] [PrfRsr] [A] [A] [C] [B] [C] [D] = 15.00 0.00 0.00 0.00 Inactive 0.00 Inactive 0.00 Rise (in) Crest Len (ft) Span (in) = 15.000.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 1 0 0 Weir Coeff. = 3.333.33 3.33 3.33 Invert El. (ft) = 143.000.00 0.00 0.00 Weir Type = Rect = 50.00 0.00 0.00 0.00 Multi-Stage = Yes No No No Length (ft) 0.00 0.00 n/a = 1.50 Slope (%) = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 2.000 (by Wet area) No Multi-Stage = n/aYes No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



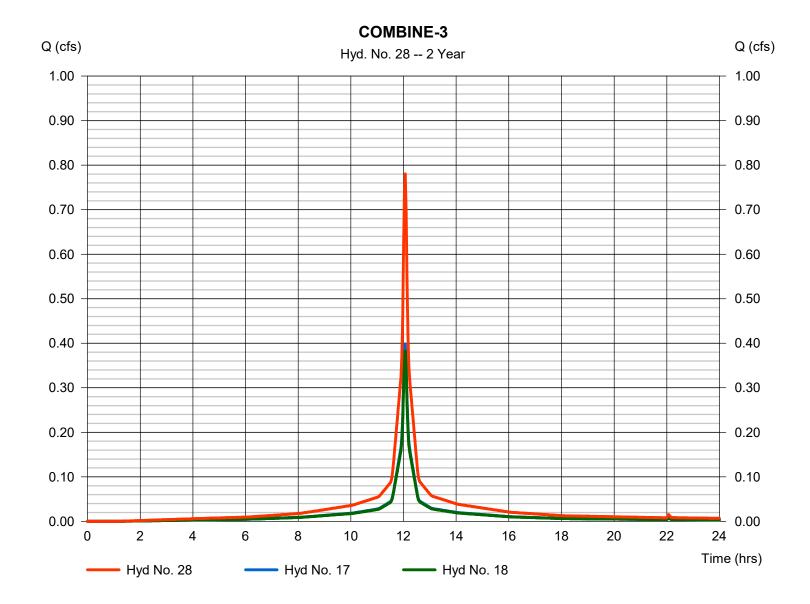
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### Hyd. No. 28

**COMBINE-3** 

Hydrograph type = Combine Peak discharge = 0.780 cfsStorm frequency Time to peak = 2 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,644 cuft Inflow hyds. = 17, 18 Contrib. drain. area = 0.235 ac



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= 0.917 cfs

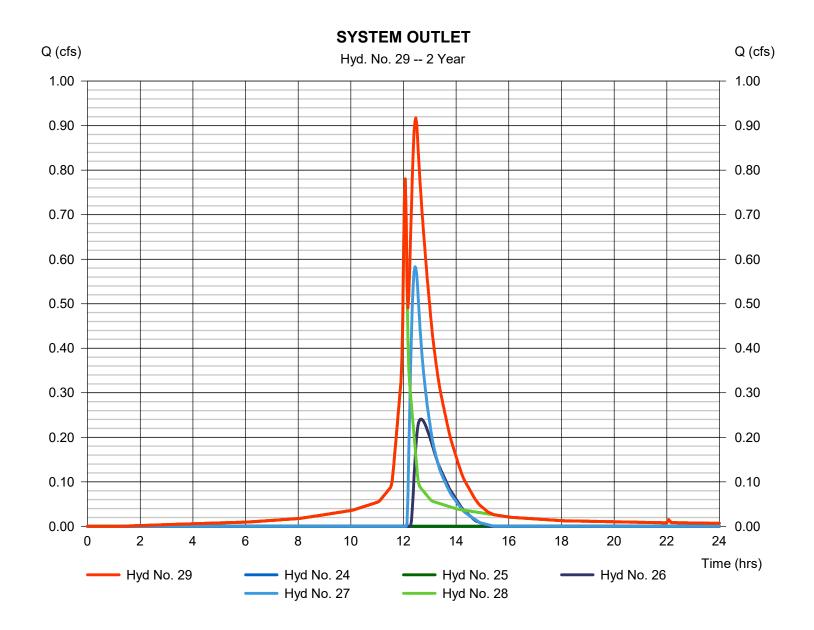
 $= 12.47 \, hrs$ 

#### Hyd. No. 29

SYSTEM OUTLET

Hydrograph type = Combine Peak discharge Storm frequency Time to peak = 2 yrsTime interval = 2 min Hyd. volume

= 5,382 cuft Inflow hyds. Contrib. drain. area = 24, 25, 26, 27, 28 = 0.000 ac



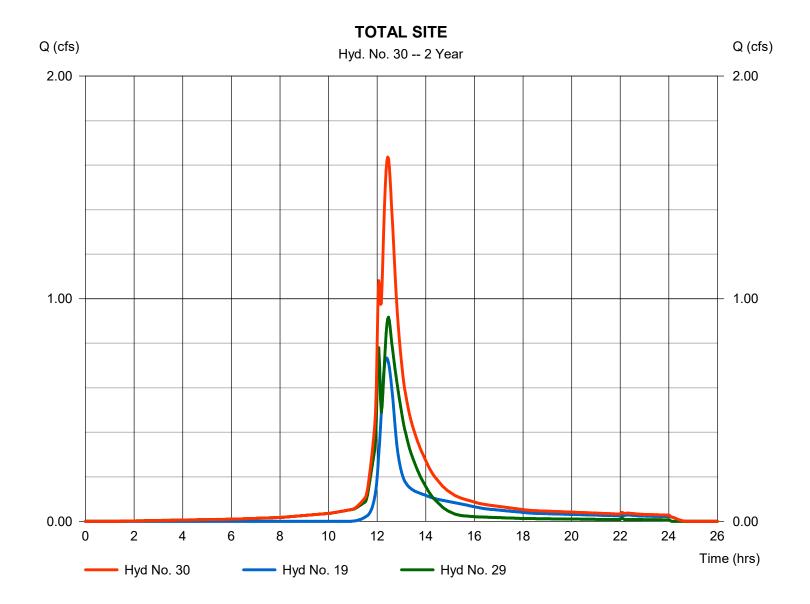
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### Hyd. No. 30

**TOTAL SITE** 

Hydrograph type = Combine Peak discharge = 1.636 cfsTime to peak Storm frequency = 2 yrs $= 12.43 \, hrs$ Time interval = 2 min Hyd. volume = 9,487 cuftInflow hyds. = 19, 29 Contrib. drain. area = 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.269	2	730	1,097				CB-01
2	SCS Runoff	0.475	2	726	1,646				CB-01A
3	SCS Runoff	0.259	2	724	823				CB-02
4	SCS Runoff	0.354	2	724	1,128				CB-03
5	SCS Runoff	0.257	2	724	828				CB-04
6	SCS Runoff	0.513	2	724	1,585				CB-05
7	SCS Runoff	0.292	2	724	922				CB-06
8	SCS Runoff	0.481	2	724	1,547				CB-07
9	SCS Runoff	0.546	2	724	1,777				CB-08
10	SCS Runoff	0.674	2	724	2,193				CB-09
11	SCS Runoff	0.637	2	724	2,028				CB-10
12	SCS Runoff	0.510	2	730	1,986				CB-11
13	SCS Runoff	1.381	2	724	4,761				PP-01
14	SCS Runoff	2.106	2	724	7,030				PP-02
15	SCS Runoff	3.404	2	724	11,736				RF-01
16	SCS Runoff	3.327	2	724	11,473				RF-02
17	SCS Runoff	0.611	2	724	2,108				RF-03
18	SCS Runoff	0.586	2	724	2,020				RF-04
19	SCS Runoff	1.726	2	740	9,131				PR-WS-01
20	Combine	1.409	2	724	5,151	1, 2, 3,			COMBINE-1
21	Combine	5.059	2	724	17,705	6, 7, 8, 9,			COMBINE-2
22	Combine	6.468	2	724	22,856	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	5.327	2	724	17,913	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.000	2	806	0	11, 15, 13	141.99	1,380	SOUTH POR PVMT
25	Reservoir	0.000	2	720	0	14	141.48	2,094	NORTH POR PVMT
26	Reservoir	2.347	2	738	7,350	22	143.60	7,323	SOUTH INFIL SYS
27	Reservoir	2.771	2	730	6,391	23	143.85	5,607	NORTH INFIL SYS
28	Combine	1.197	2	724	4,129	17, 18,			COMBINE-3
29	Combine	5.271	2	732	17,870	24, 25, 26,			SYSTEM OUTLET
30	Combine	6.762	2	736	27,001	27, 28 19, 29			TOTAL SITE
F01	F0173-02 Hydrographs - Proposed.gpw			Return F	Period: 10 Y	'ear	Friday, 07 /	9 / 2021	

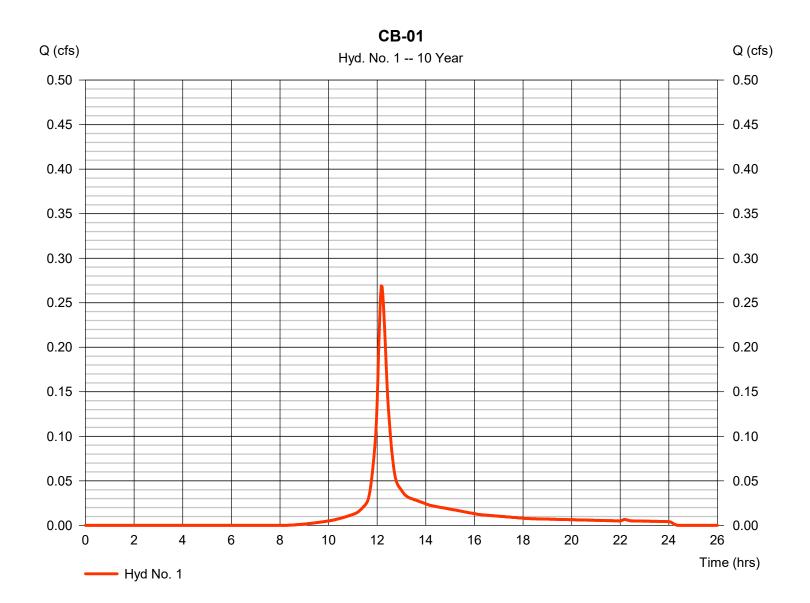
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#### Hyd. No. 1

CB-01

Hydrograph type = SCS Runoff Peak discharge = 0.269 cfsStorm frequency = 10 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 1,097 cuftDrainage area Curve number = 0.108 ac= 76 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 14.20 min = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



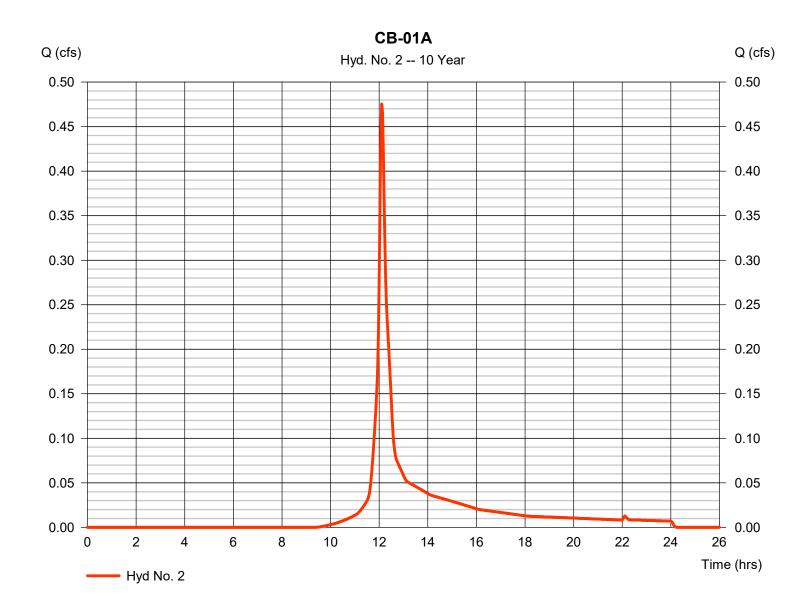
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#### Hyd. No. 2

CB-01A

Hydrograph type = SCS Runoff Peak discharge = 0.475 cfsStorm frequency = 10 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 1,646 cuft Drainage area Curve number = 0.194 ac= 70 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 7.80 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



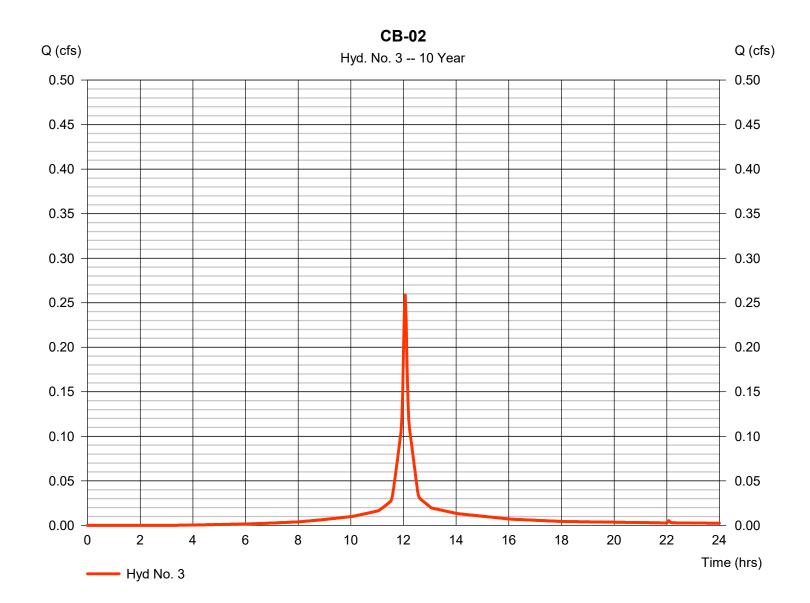
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#### Hyd. No. 3

**CB-02** 

Hydrograph type = SCS Runoff Peak discharge = 0.259 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 823 cuft Drainage area Curve number = 0.054 ac= 92 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



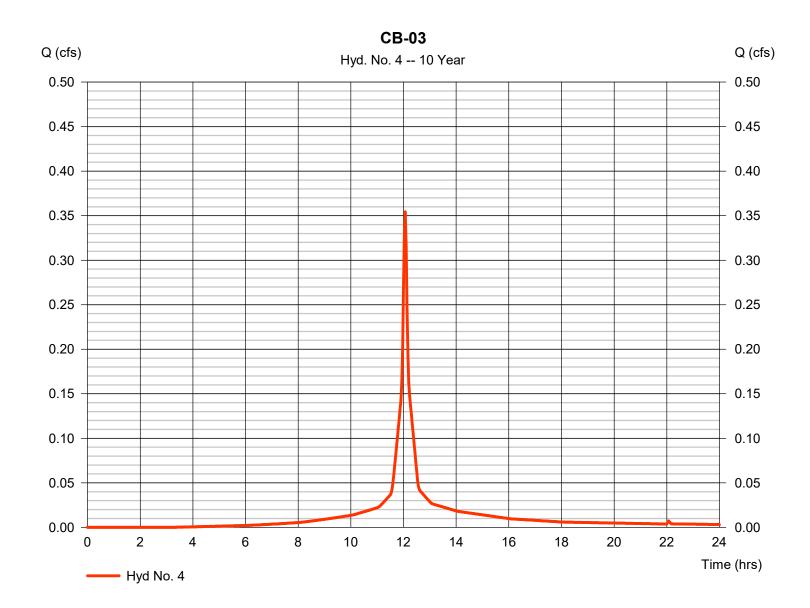
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#### Hyd. No. 4

**CB-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.354 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,128 cuft Drainage area Curve number = 0.074 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



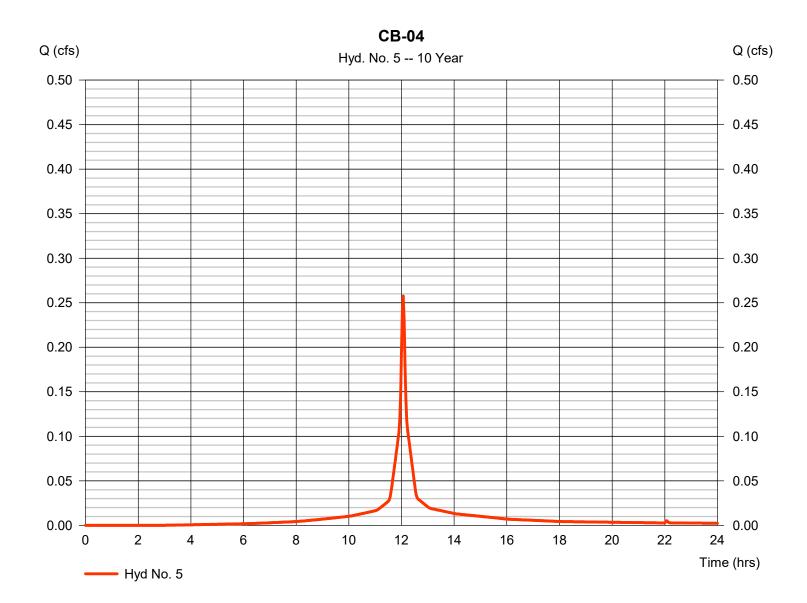
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#### Hyd. No. 5

**CB-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.257 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 828 cuft Drainage area Curve number = 0.053 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



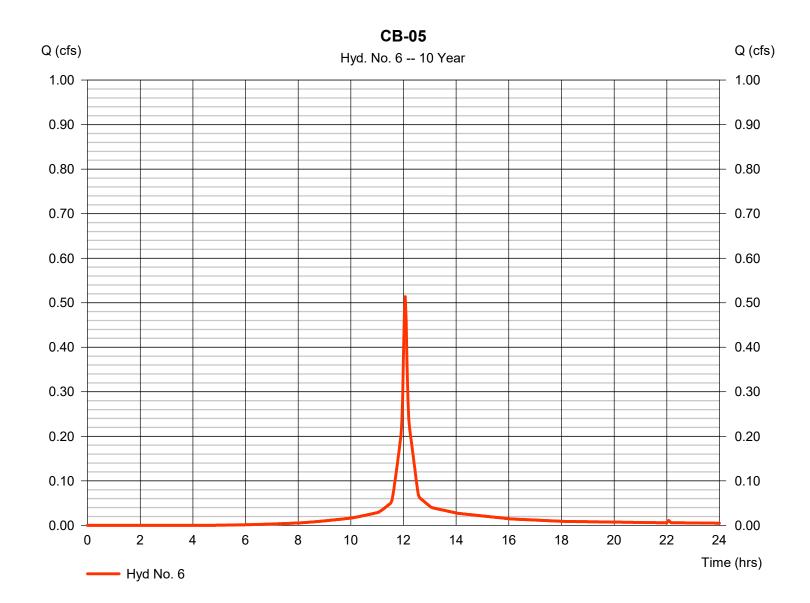
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#### Hyd. No. 6

**CB-05** 

Hydrograph type = SCS Runoff Peak discharge = 0.513 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,585 cuft Drainage area Curve number = 0.115 ac= 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



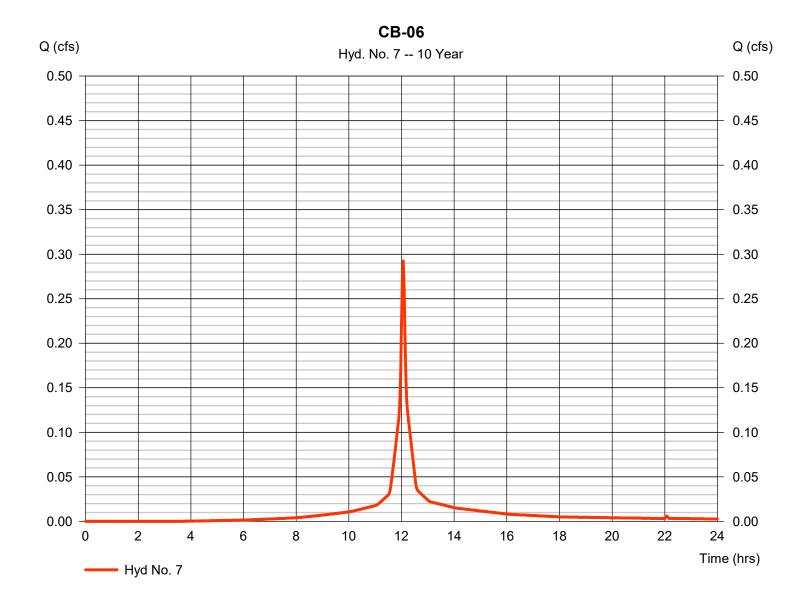
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#### Hyd. No. 7

**CB-06** 

Hydrograph type = SCS Runoff Peak discharge = 0.292 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 922 cuft Drainage area Curve number = 0.062 ac= 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



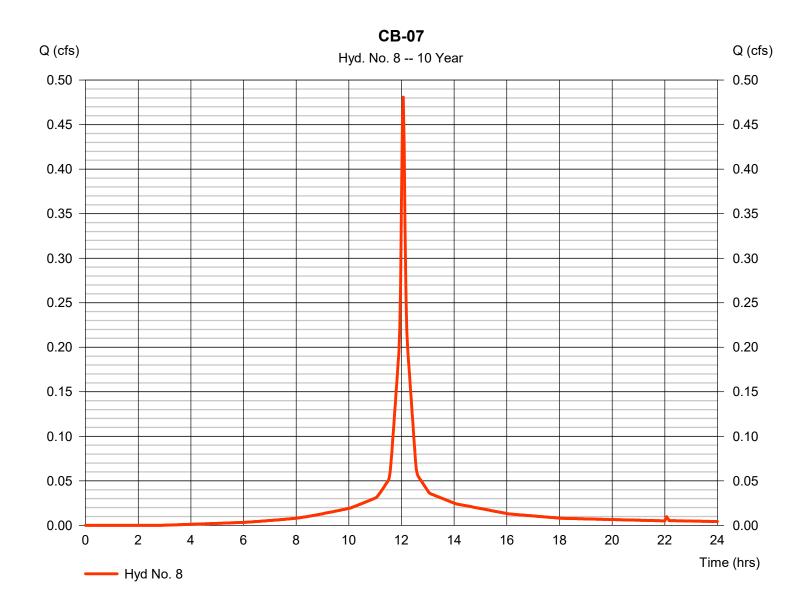
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#### Hyd. No. 8

**CB-07** 

Hydrograph type = SCS Runoff Peak discharge = 0.481 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,547 cuftDrainage area Curve number = 0.099 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



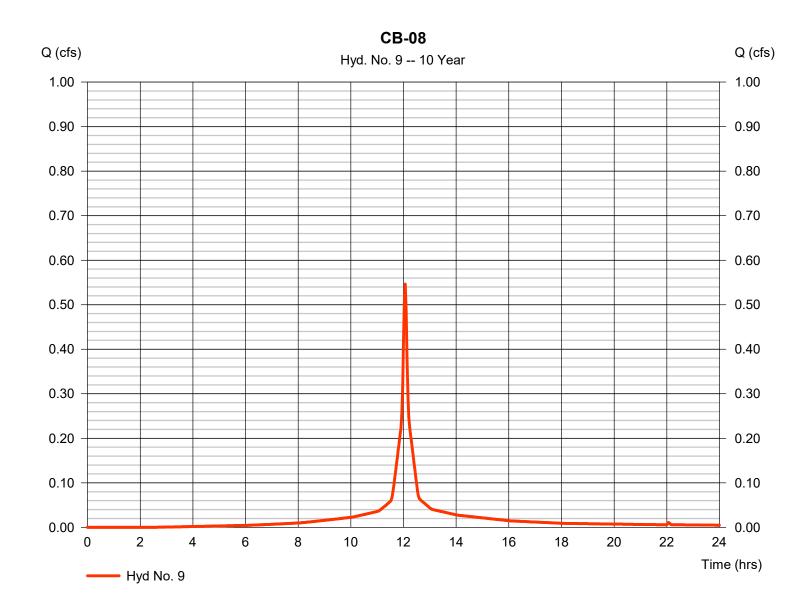
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#### Hyd. No. 9

**CB-08** 

Hydrograph type = SCS Runoff Peak discharge = 0.546 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,777 cuft Drainage area = 0.111 acCurve number = 94 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.50 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



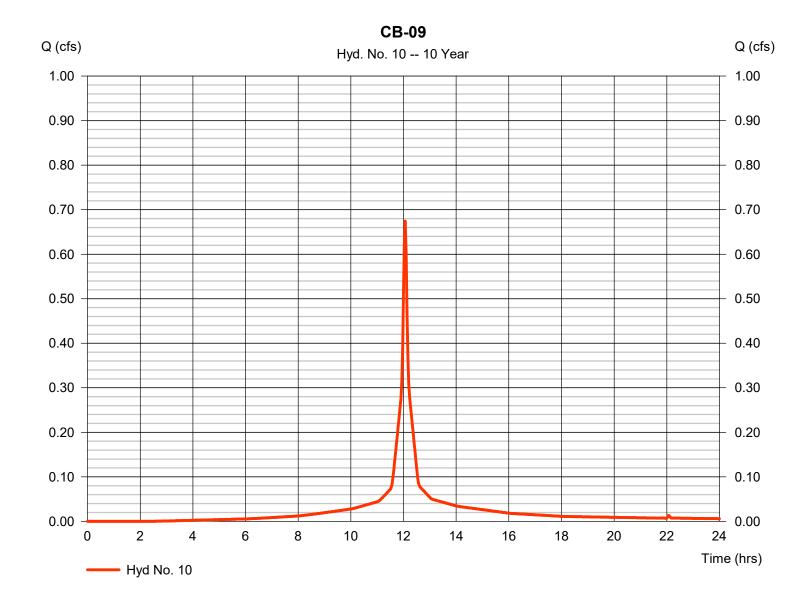
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#### Hyd. No. 10

**CB-09** 

Hydrograph type = SCS Runoff Peak discharge = 0.674 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,193 cuftDrainage area Curve number = 0.137 ac= 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



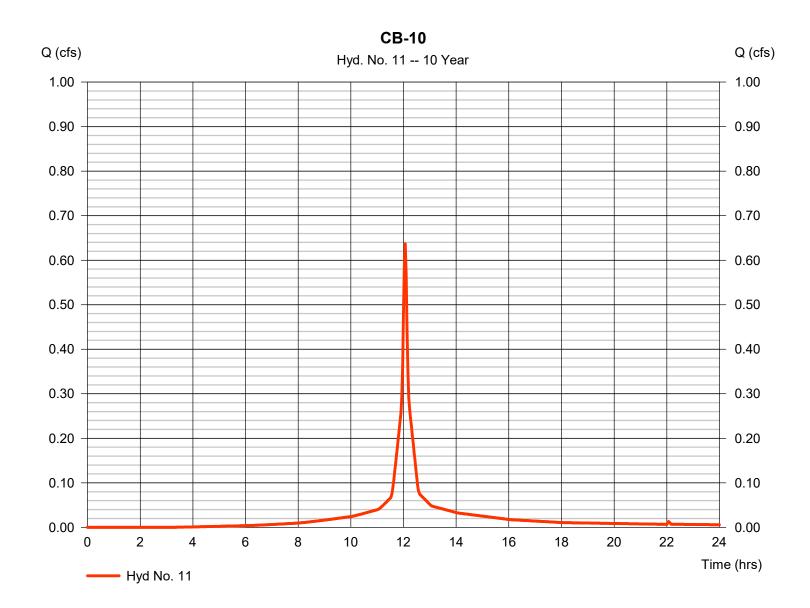
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#### Hyd. No. 11

**CB-10** 

Hydrograph type = SCS Runoff Peak discharge = 0.637 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,028 cuft Drainage area Curve number = 0.133 ac= 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



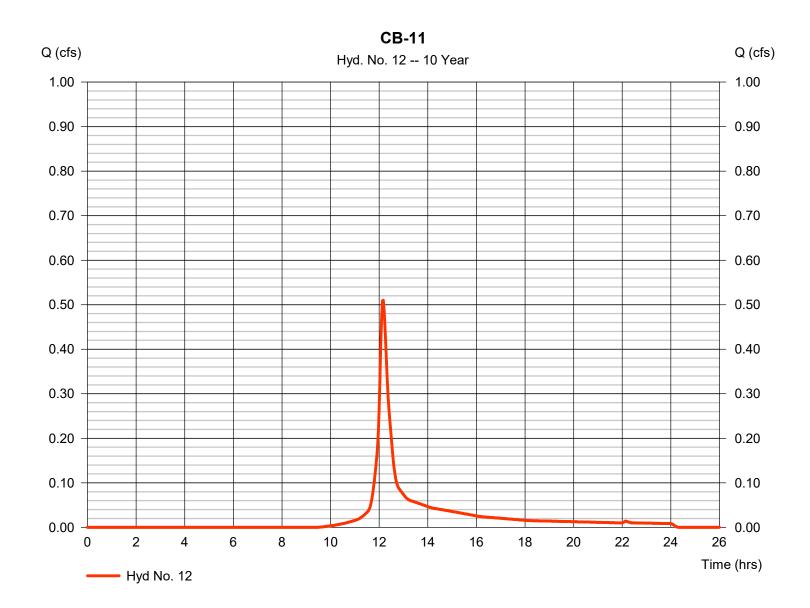
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#### Hyd. No. 12

**CB-11** 

Hydrograph type = SCS Runoff Peak discharge = 0.510 cfsStorm frequency = 10 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1,986 cuft Drainage area = 0.227 acCurve number = 70 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.90 min = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



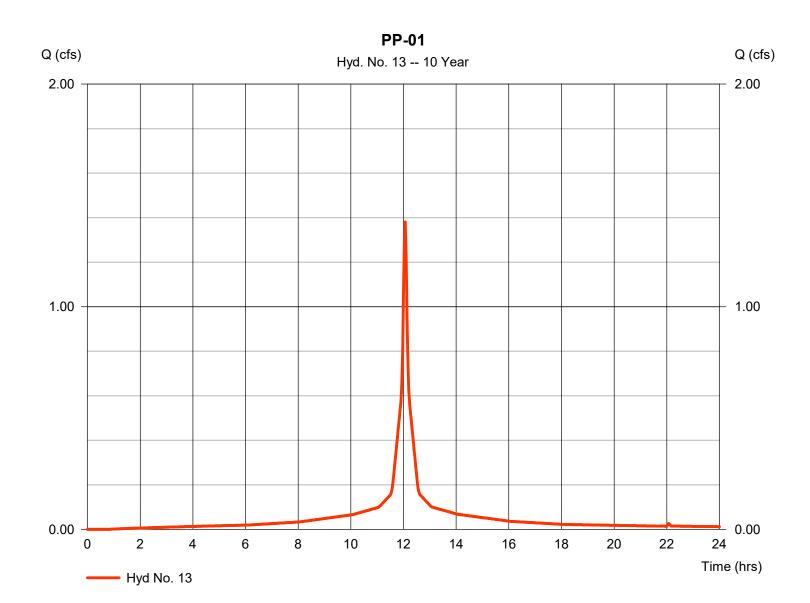
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#### **Hyd. No. 13**

PP-01

Hydrograph type = SCS Runoff Peak discharge = 1.381 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,761 cuftDrainage area = 0.271 acCurve number = 98 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



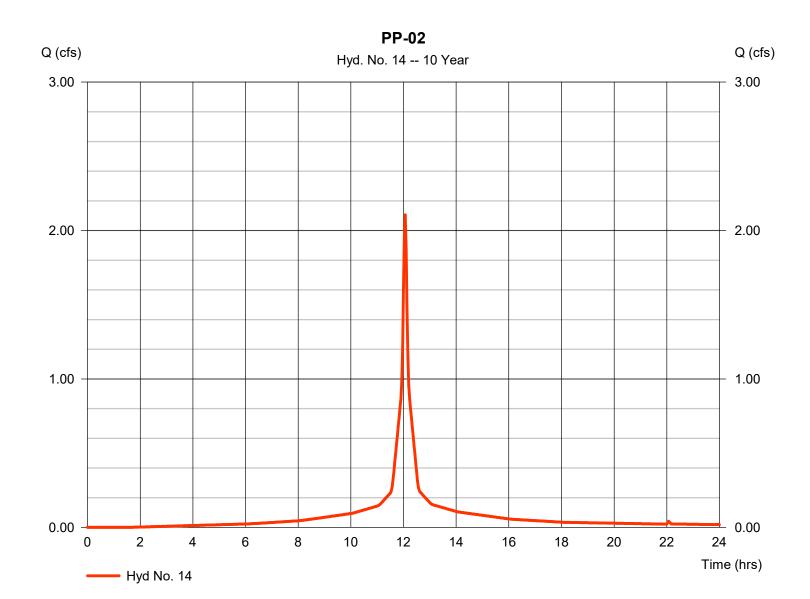
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## Hyd. No. 14

PP-02

Hydrograph type = SCS Runoff Peak discharge = 2.106 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7,030 cuftDrainage area Curve number = 0.419 ac= 96 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 6.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



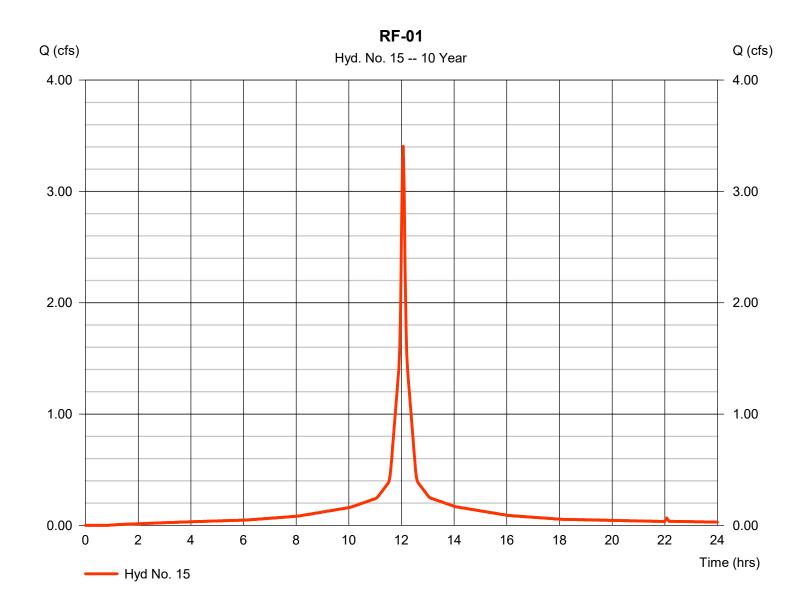
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#### Hyd. No. 15

**RF-01** 

Hydrograph type = SCS Runoff Peak discharge = 3.404 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 11,736 cuft Drainage area Curve number = 0.668 ac= 98 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



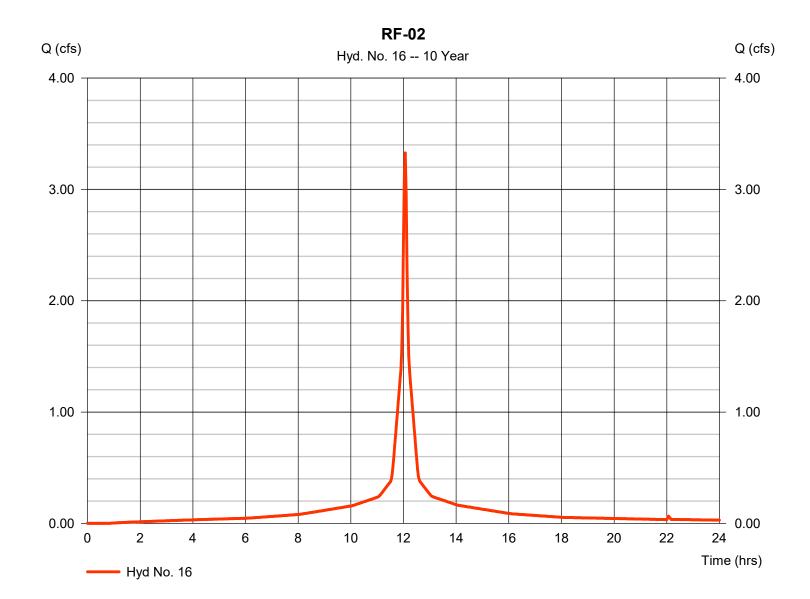
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#### Hyd. No. 16

**RF-02** 

Hydrograph type = SCS Runoff Peak discharge = 3.327 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 11,473 cuft Drainage area Curve number = 0.653 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



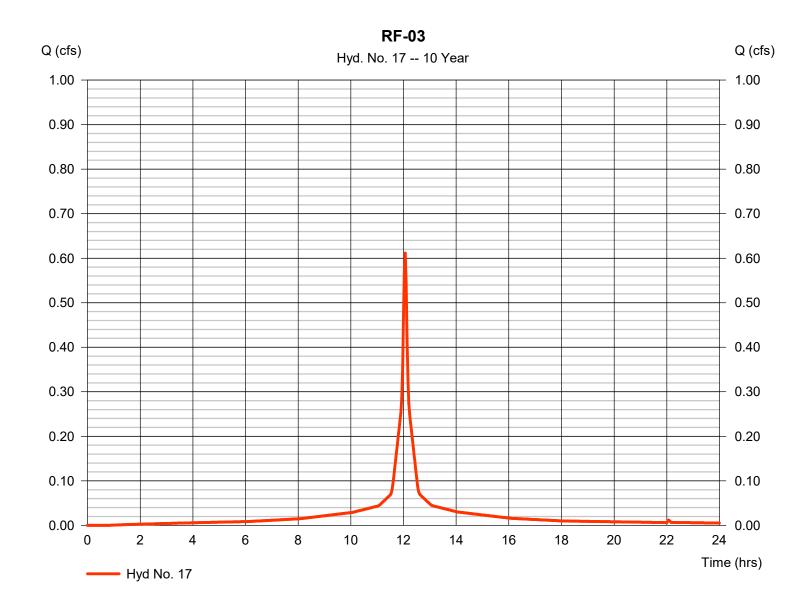
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#### Hyd. No. 17

**RF-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.611 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,108 cuftDrainage area Curve number = 0.120 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



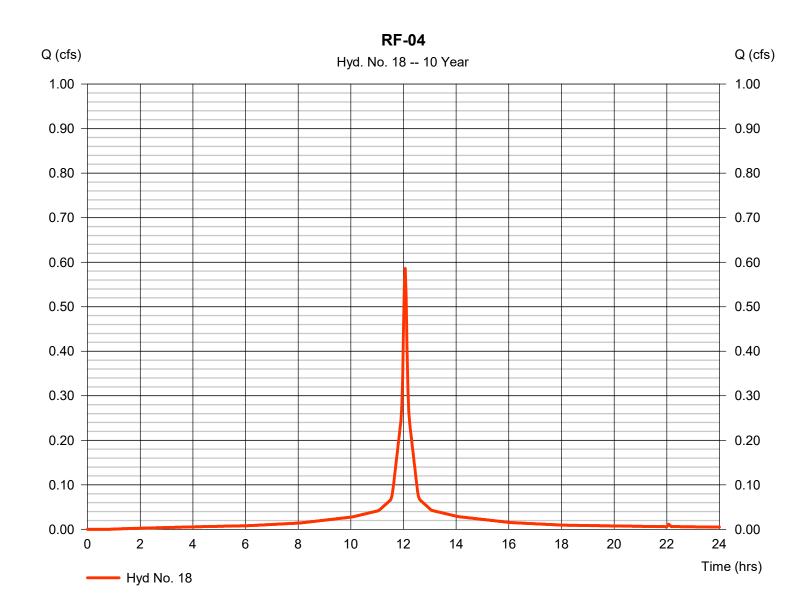
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#### **Hyd. No. 18**

**RF-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.586 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,020 cuftDrainage area Curve number = 0.115 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



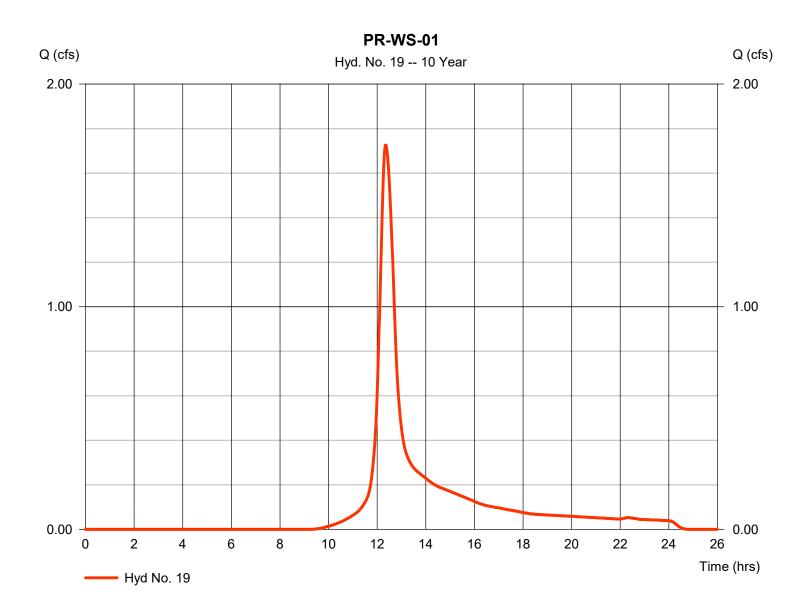
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### Hyd. No. 19

PR-WS-01

= SCS Runoff Hydrograph type Peak discharge = 1.726 cfsStorm frequency = 10 yrsTime to peak  $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 9,131 cuftDrainage area Curve number = 71 = 1.038 acHydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 27.60 min = User Total precip. = 5.40 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



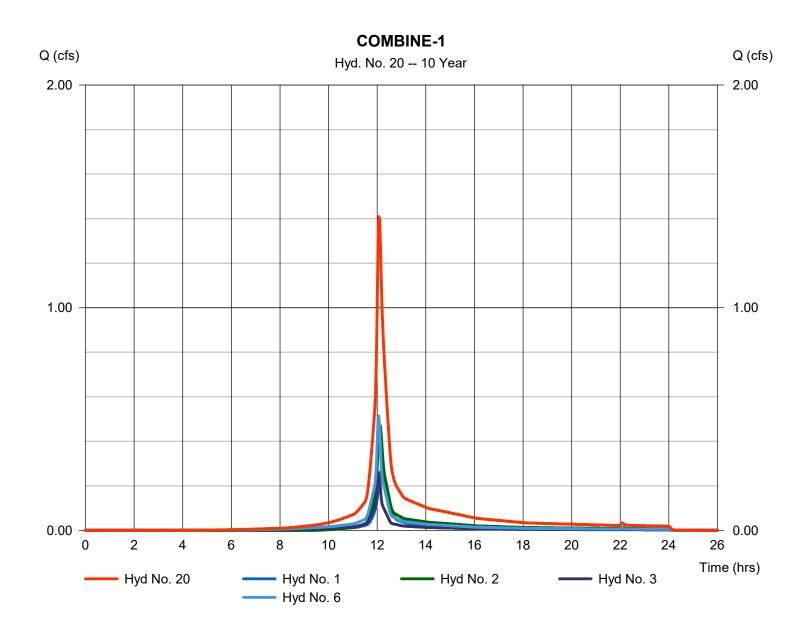
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### Hyd. No. 20

**COMBINE-1** 

Hydrograph type = Combine Peak discharge = 1.409 cfsStorm frequency = 10 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 5,151 cuftInflow hyds. = 1, 2, 3, 6Contrib. drain. area = 0.471 ac



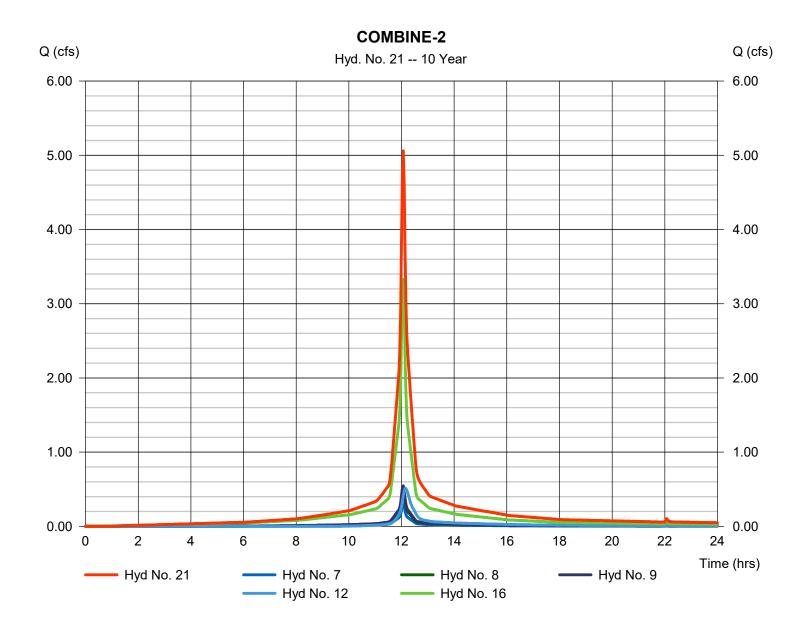
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#### Hyd. No. 21

**COMBINE-2** 

Hydrograph type = Combine Peak discharge = 5.059 cfsStorm frequency = 10 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 17,705 cuftInflow hyds. Contrib. drain. area = 1.152 ac= 7, 8, 9, 12, 16



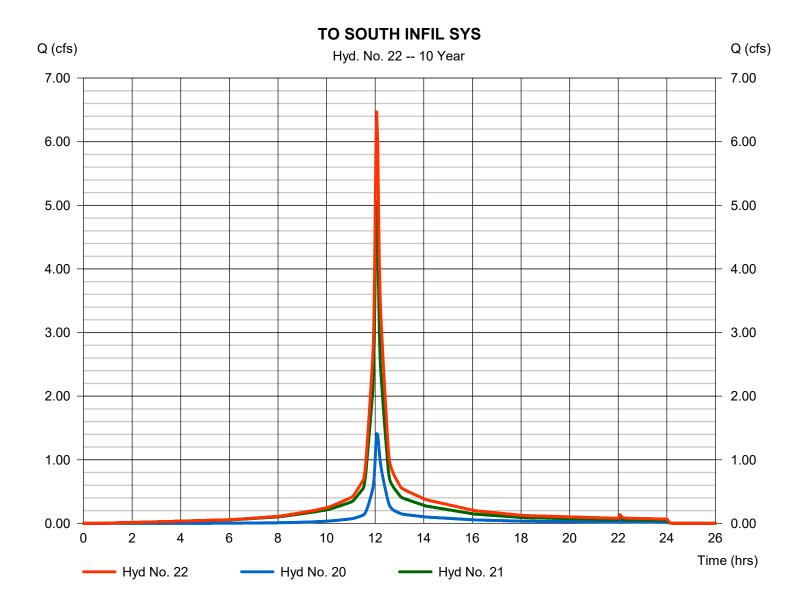
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#### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type = Combine Peak discharge = 6.468 cfsStorm frequency Time to peak = 10 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 22,856 cuft Inflow hyds. Contrib. drain. area = 20, 21= 0.000 ac



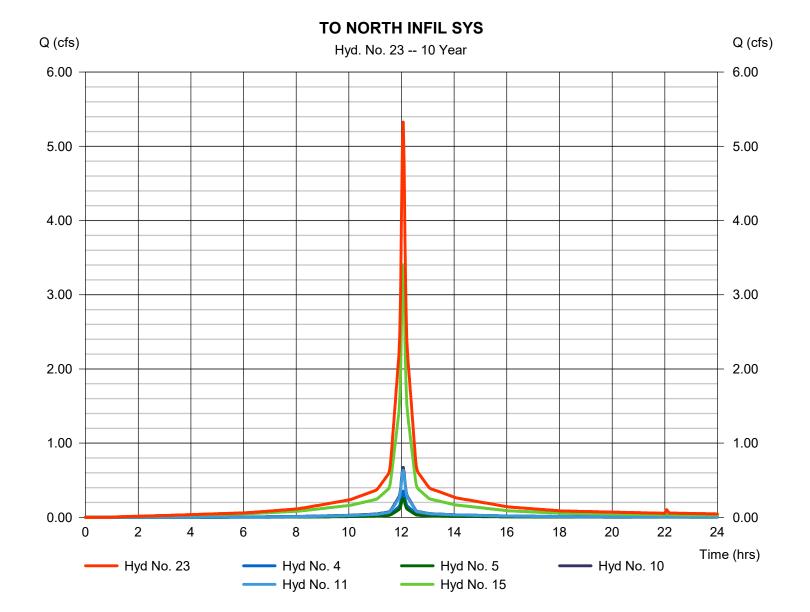
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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#### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type = Combine Peak discharge = 5.327 cfsStorm frequency = 10 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 17,913 cuft Inflow hyds. Contrib. drain. area = 1.065 ac= 4, 5, 10, 11, 15



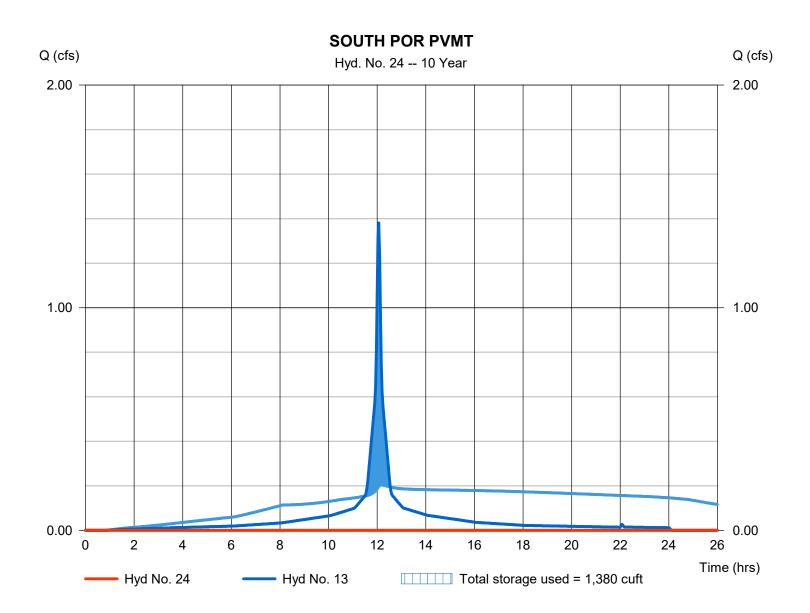
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#### Hyd. No. 24

#### SOUTH POR PVMT

Hydrograph type = Reservoir Peak discharge = 0.000 cfsStorm frequency = 10 yrsTime to peak  $= 13.43 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. = 13 - PP-01 Max. Elevation = 141.99 ft= SOUTH POROUS PVMT Reservoir name Max. Storage = 1,380 cuft



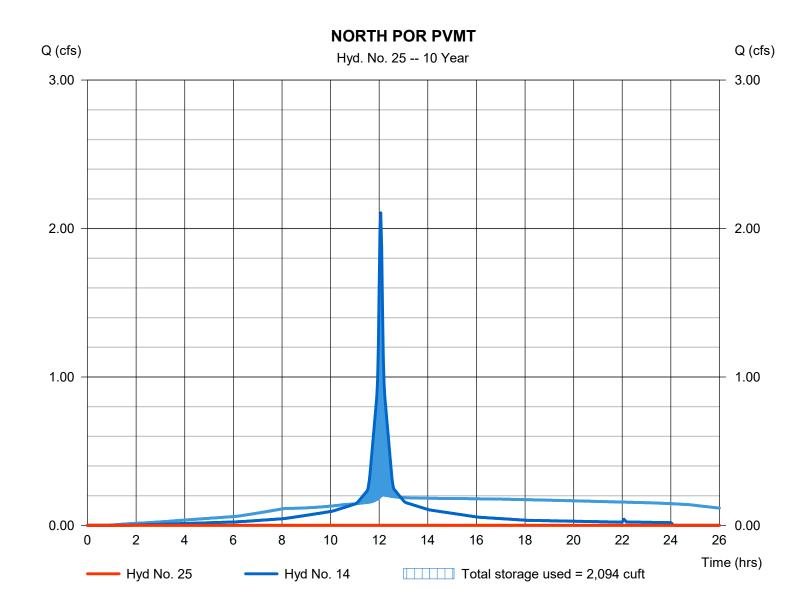
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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#### Hyd. No. 25

#### NORTH POR PVMT

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 10 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. Max. Elevation = 14 - PP-02 = 141.48 ftReservoir name = NORTH POROUS PVMT Max. Storage = 2,094 cuft



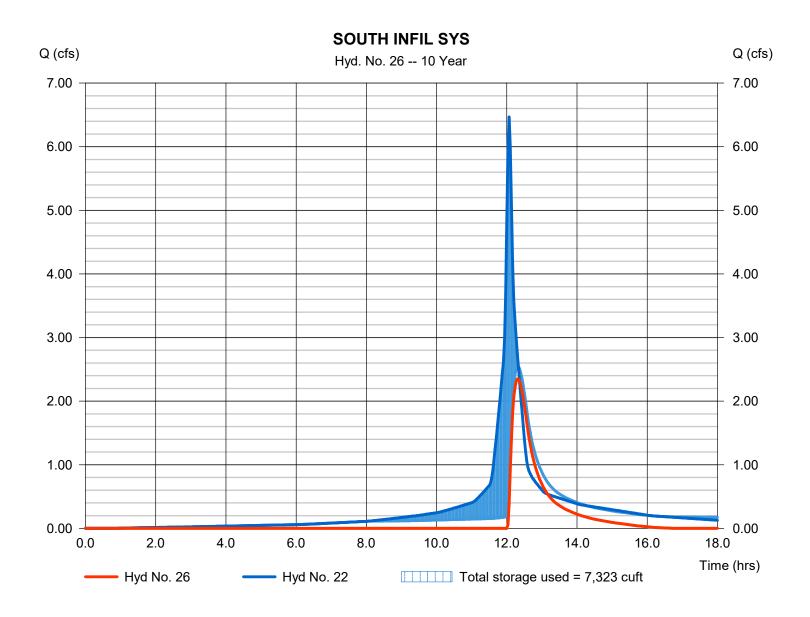
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#### Hyd. No. 26

**SOUTH INFIL SYS** 

Hydrograph type Peak discharge = 2.347 cfs= Reservoir Storm frequency = 10 yrsTime to peak  $= 12.30 \, hrs$ Time interval = 2 min Hyd. volume = 7,350 cuftMax. Elevation Inflow hyd. No. = 22 - TO SOUTH INFIL SYS  $= 143.60 \, \text{ft}$ = SOUTH INFIL SYS Reservoir name Max. Storage = 7,323 cuft



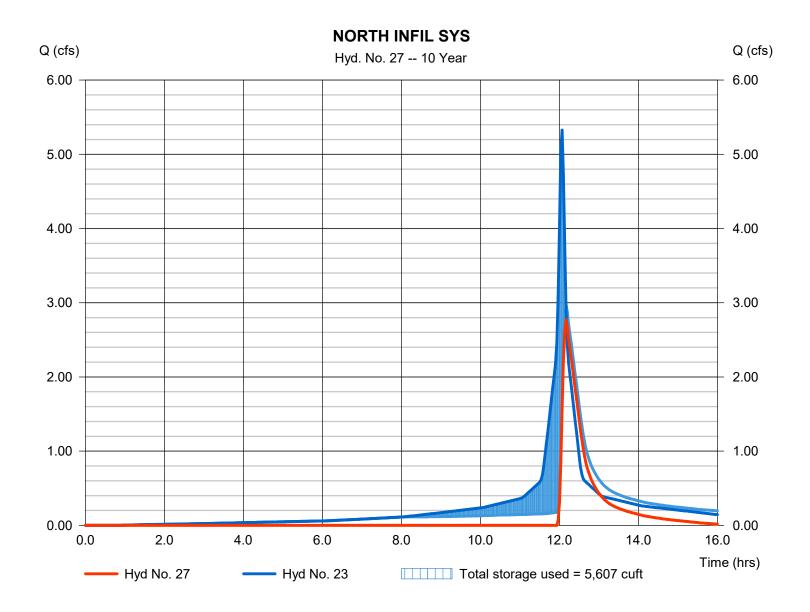
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#### Hyd. No. 27

**NORTH INFIL SYS** 

Hydrograph type Peak discharge = 2.771 cfs= Reservoir Storm frequency = 10 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 6.391 cuft= 23 - TO NORTH INFIL SYS Max. Elevation Inflow hyd. No.  $= 143.85 \, \text{ft}$ = NORTH INFIL SYS Reservoir name Max. Storage = 5,607 cuft



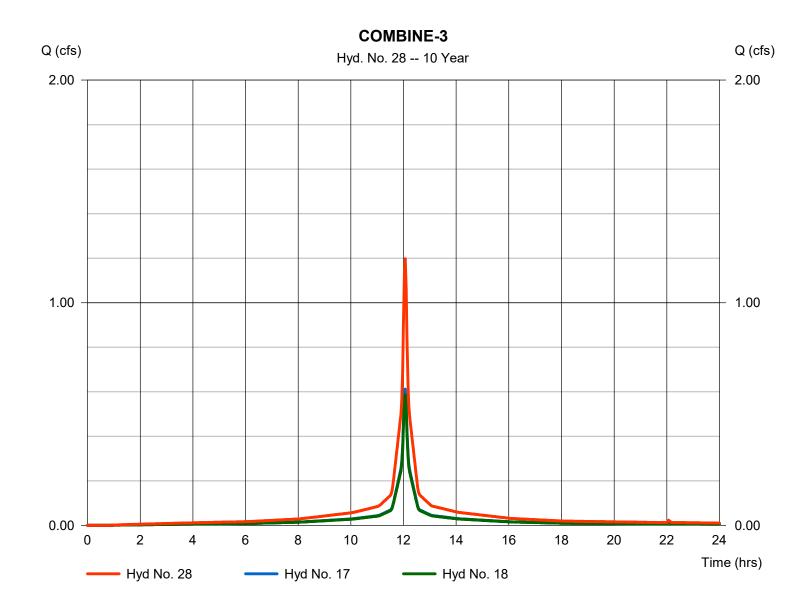
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#### Hyd. No. 28

**COMBINE-3** 

Hydrograph type = Combine Peak discharge = 1.197 cfsTime to peak Storm frequency = 10 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,129 cuft Inflow hyds. = 17, 18 Contrib. drain. area = 0.235 ac



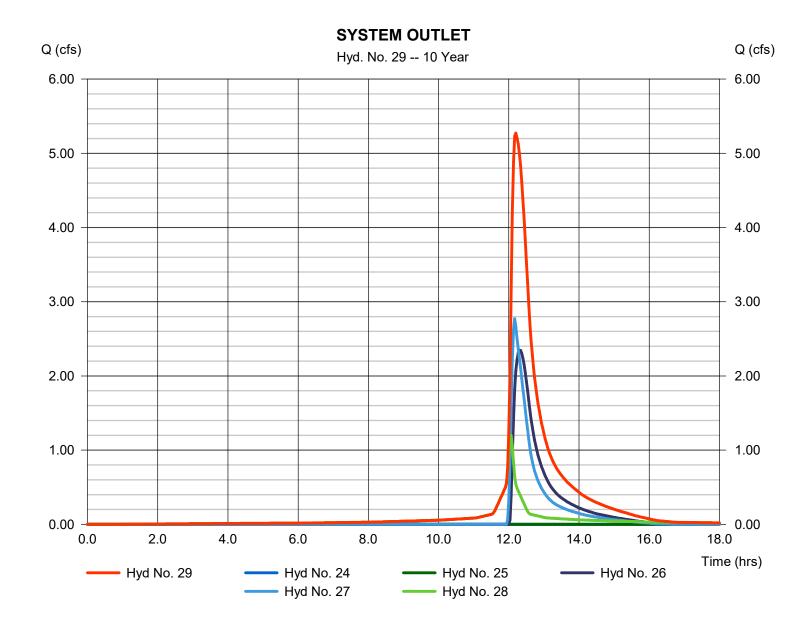
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#### Hyd. No. 29

SYSTEM OUTLET

Hydrograph type = Combine Peak discharge = 5.271 cfsStorm frequency Time to peak = 10 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 17,870 cuft Inflow hyds. Contrib. drain. area = 24, 25, 26, 27, 28 = 0.000 ac



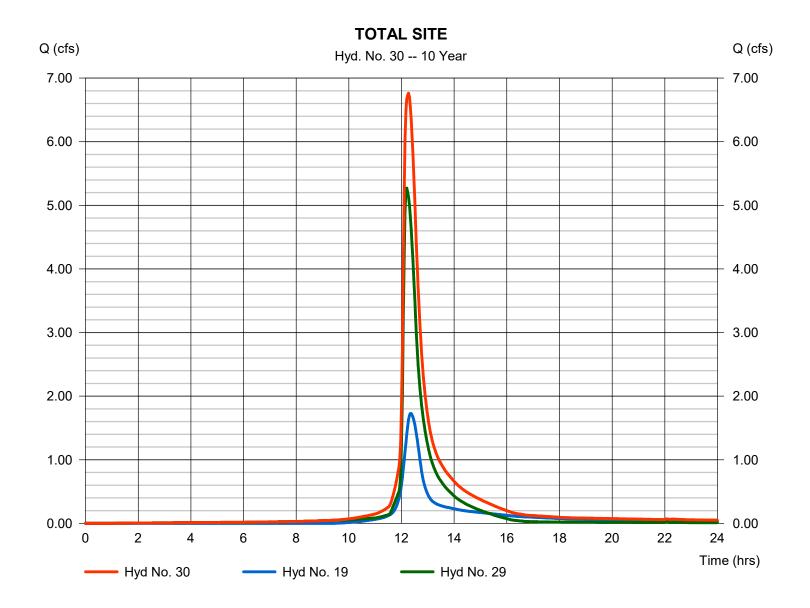
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### Hyd. No. 30

**TOTAL SITE** 

Hydrograph type = Combine Peak discharge = 6.762 cfsStorm frequency Time to peak = 10 yrs $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 27,001 cuftInflow hyds. = 19, 29 Contrib. drain. area = 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.364	2	730	1,482				CB-01
2	SCS Runoff	0.671	2	726	2,299				CB-01A
3	SCS Runoff	0.321	2	724	1,035				CB-02
4	SCS Runoff	0.439	2	724	1,418				CB-03
5	SCS Runoff	0.318	2	724	1,036				CB-04
6	SCS Runoff	0.648	2	724	2,026				CB-05
7	SCS Runoff	0.364	2	724	1,164				CB-06
8	SCS Runoff	0.594	2	724	1,936				CB-07
9	SCS Runoff	0.672	2	724	2,214				CB-08
10	SCS Runoff	0.830	2	724	2,733				CB-09
11	SCS Runoff	0.790	2	724	2,548				CB-10
12	SCS Runoff	0.720	2	728	2,774				CB-11
13	SCS Runoff	1.683	2	724	5,839				PP-01
14	SCS Runoff	2.577	2	724	8,691				PP-02
15	SCS Runoff	4.148	2	724	14,393				RF-01
16	SCS Runoff	4.055	2	724	14,070				RF-02
17	SCS Runoff	0.745	2	724	2,586				RF-03
18	SCS Runoff	0.714	2	724	2,478				RF-04
19	SCS Runoff	2.421	2	740	12,677				PR-WS-01
20	Combine	1.865	2	724	6,841	1, 2, 3,			COMBINE-1
21	Combine	6.276	2	724	22,157	6, 7, 8, 9,			COMBINE-2
22	Combine	8.142	2	724	28,998	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	6.525	2	724	22,128	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.036	2	742	49	11, 15, 13	142.11	1,721	SOUTH POR PVMT
25	Reservoir	0.031	2	744	42	14	141.60	2,632	NORTH POR PVMT
26	Reservoir	3.888	2	734	11,946	22	143.96	8,508	SOUTH INFIL SYS
27	Reservoir	4.442	2	728	9,585	23	144.19	6,181	NORTH INFIL SYS
28	Combine	1.459	2	724	5,063	17, 18,			COMBINE-3
29	Combine	8.975	2	728	26,685	24, 25, 26,			SYSTEM OUTLET
30	Combine	10.69	2	730	39,362	27, 28 19, 29			TOTAL SITE
F0173-02 Hydrographs - Proposed.gpw					Return Period: 25 Year			Friday, 07 / 9 / 2021	

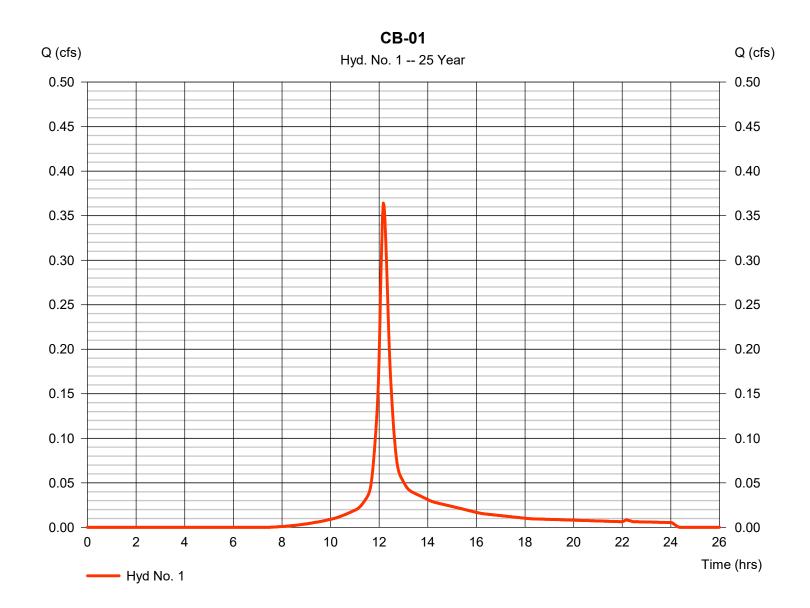
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#### Hyd. No. 1

CB-01

Hydrograph type = SCS Runoff Peak discharge = 0.364 cfsStorm frequency = 25 yrs Time to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1,482 cuft Drainage area Curve number = 0.108 ac= 76 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 14.20 min = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



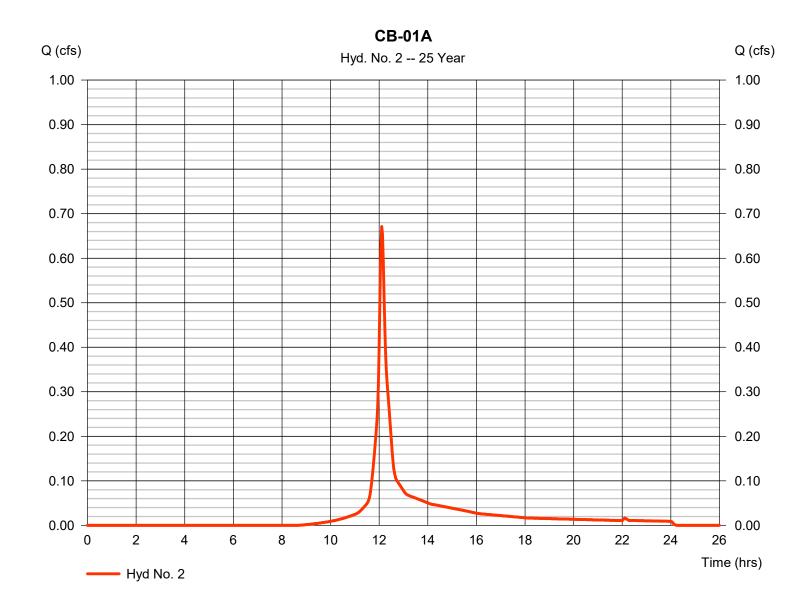
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#### Hyd. No. 2

**CB-01A** 

Hydrograph type = SCS Runoff Peak discharge = 0.671 cfsStorm frequency = 25 yrs Time to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 2.299 cuft Drainage area Curve number = 0.194 ac= 70 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 7.80 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



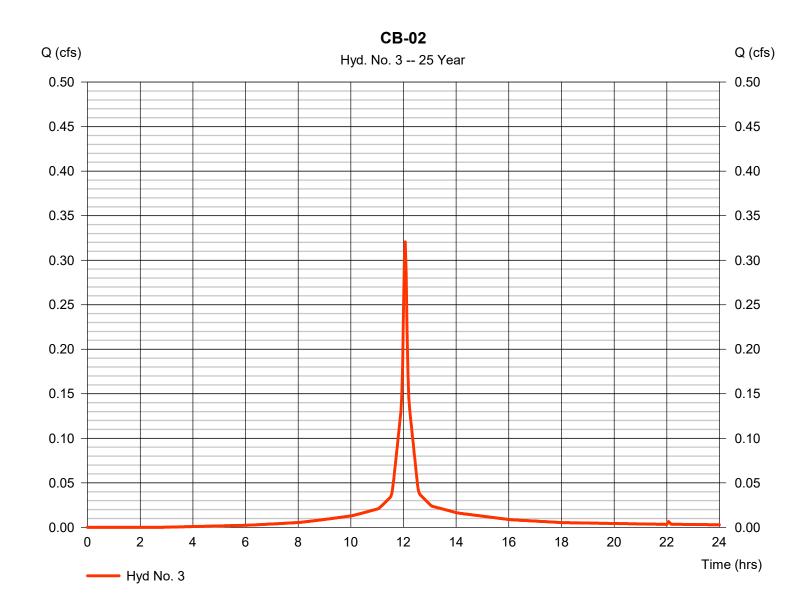
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#### Hyd. No. 3

**CB-02** 

Hydrograph type = SCS Runoff Peak discharge = 0.321 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,035 cuftDrainage area Curve number = 0.054 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



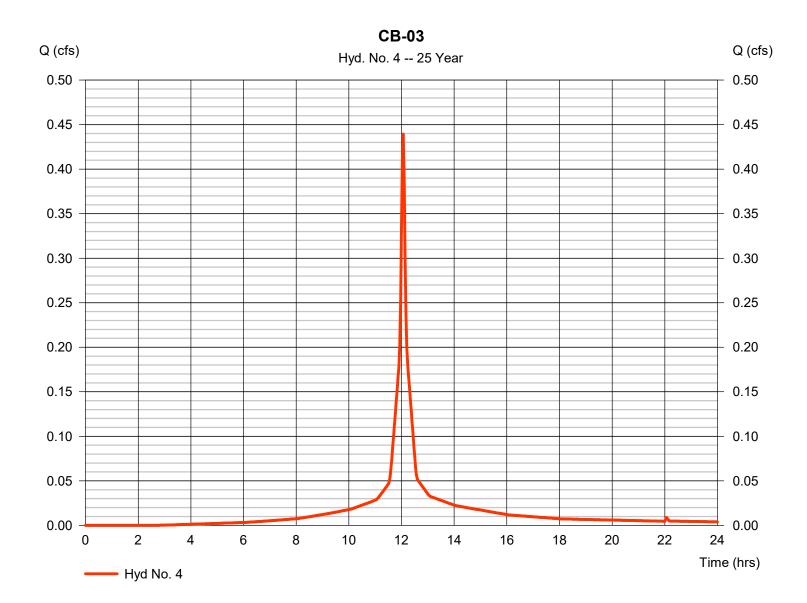
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#### Hyd. No. 4

**CB-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.439 cfsStorm frequency = 25 yrs Time to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 1,418 cuft Drainage area Curve number = 0.074 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



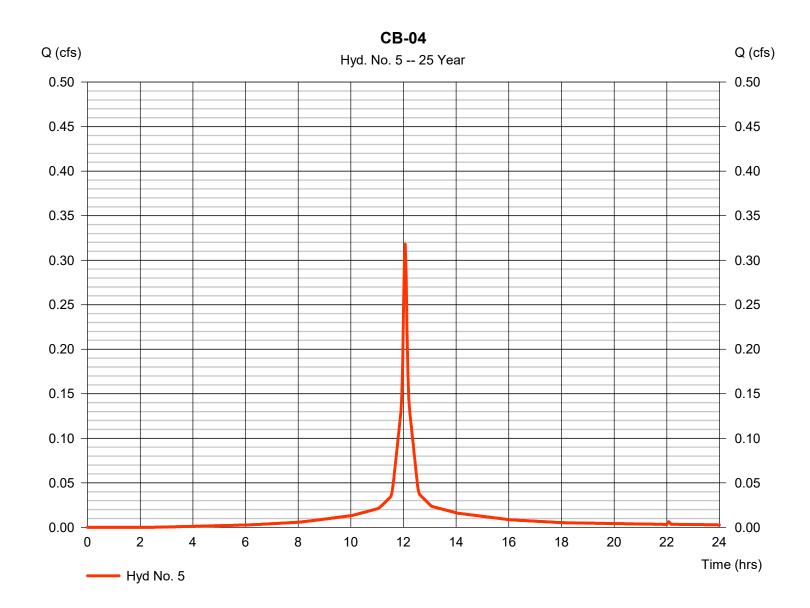
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#### Hyd. No. 5

**CB-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.318 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,036 cuftDrainage area Curve number = 0.053 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



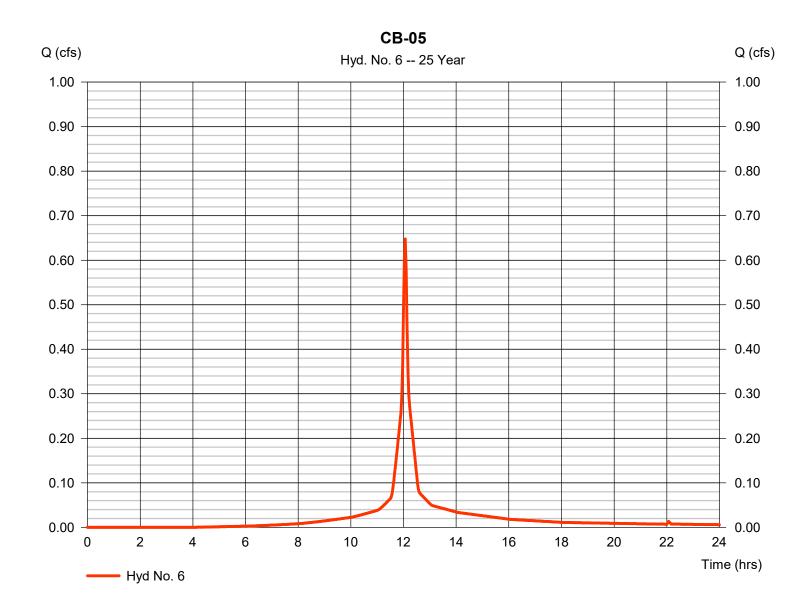
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#### Hyd. No. 6

**CB-05** 

Hydrograph type = SCS Runoff Peak discharge = 0.648 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,026 cuftDrainage area Curve number = 0.115 ac= 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



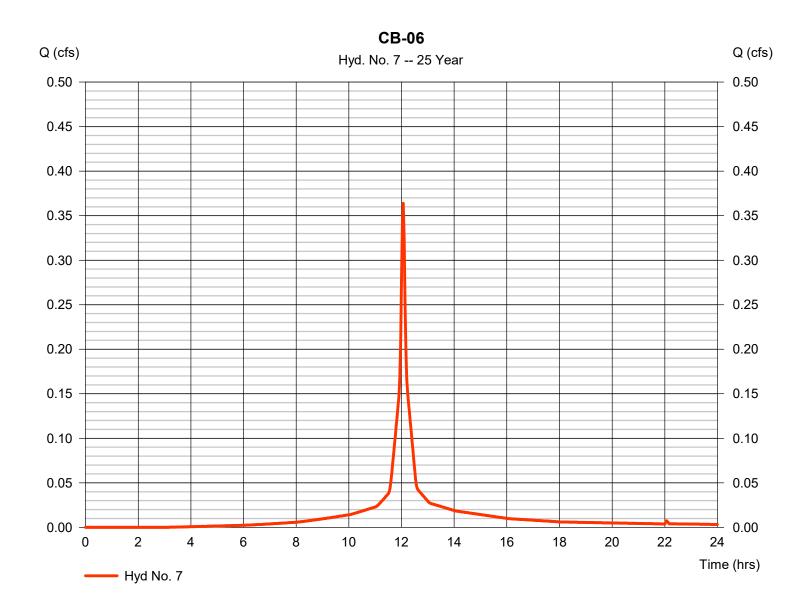
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#### Hyd. No. 7

**CB-06** 

Hydrograph type = SCS Runoff Peak discharge = 0.364 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,164 cuft Drainage area Curve number = 0.062 ac= 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



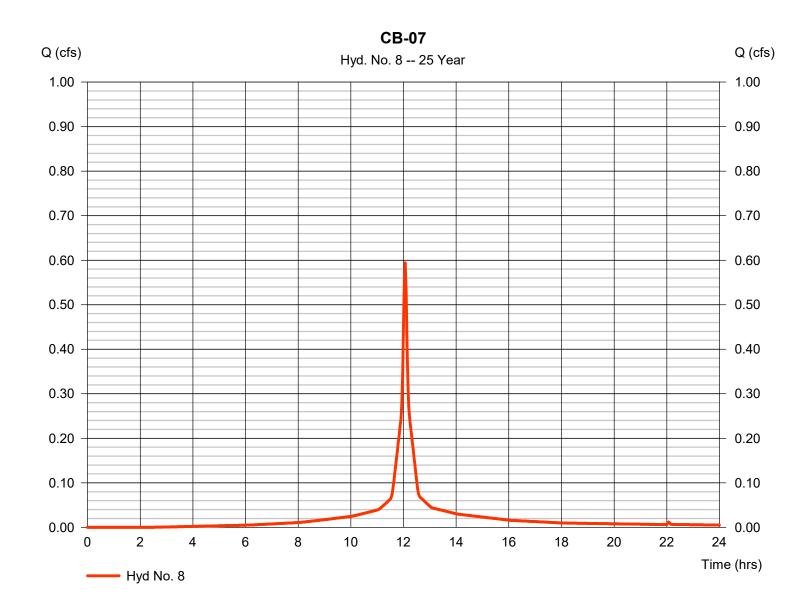
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#### Hyd. No. 8

**CB-07** 

Hydrograph type = SCS Runoff Peak discharge = 0.594 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,936 cuft Drainage area Curve number = 0.099 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



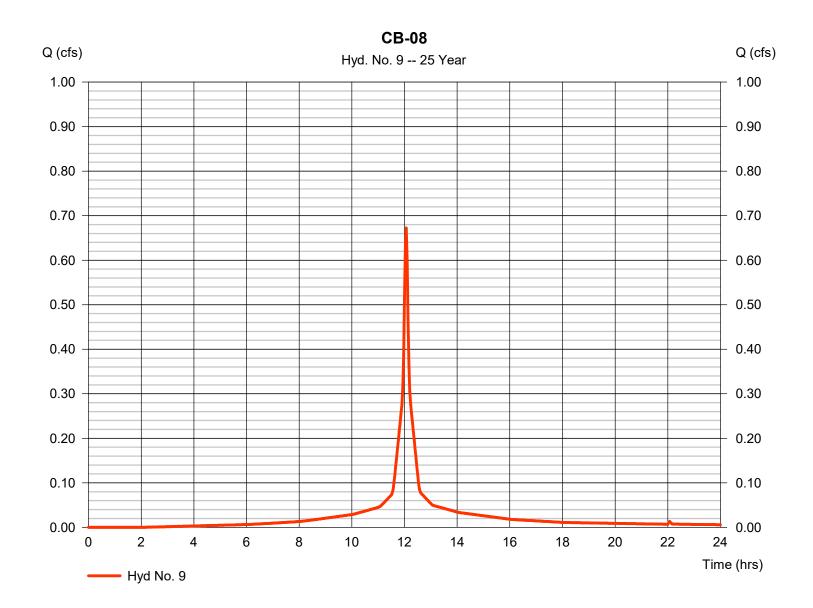
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#### Hyd. No. 9

**CB-08** 

Hydrograph type = SCS Runoff Peak discharge = 0.672 cfsStorm frequency = 25 yrs Time to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 2,214 cuft Drainage area = 0.111 acCurve number = 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.50 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



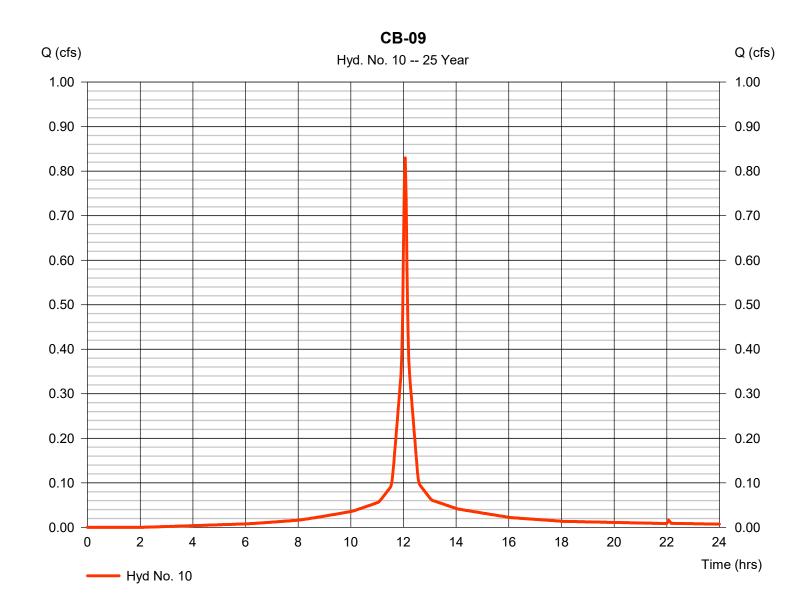
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#### Hyd. No. 10

**CB-09** 

Hydrograph type = SCS Runoff Peak discharge = 0.830 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,733 cuftDrainage area Curve number = 0.137 ac= 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



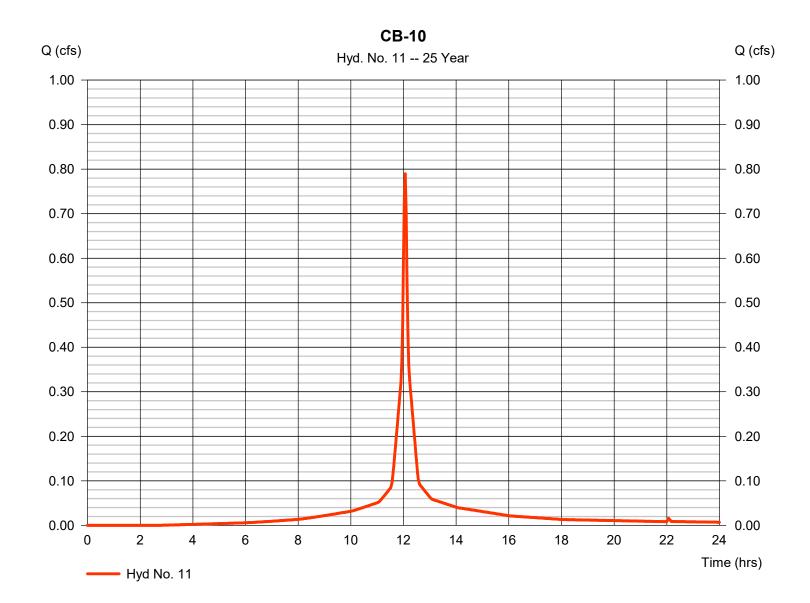
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#### Hyd. No. 11

**CB-10** 

Hydrograph type = SCS Runoff Peak discharge = 0.790 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,548 cuftDrainage area Curve number = 0.133 ac= 92 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



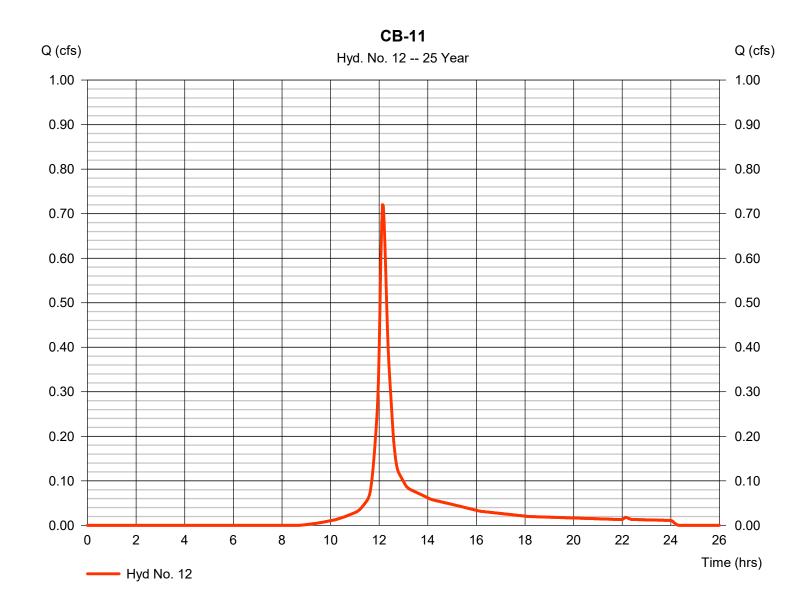
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#### Hyd. No. 12

**CB-11** 

Hydrograph type = SCS Runoff Peak discharge = 0.720 cfsStorm frequency = 25 yrs Time to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2.774 cuftDrainage area = 0.227 acCurve number = 70 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.90 min = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



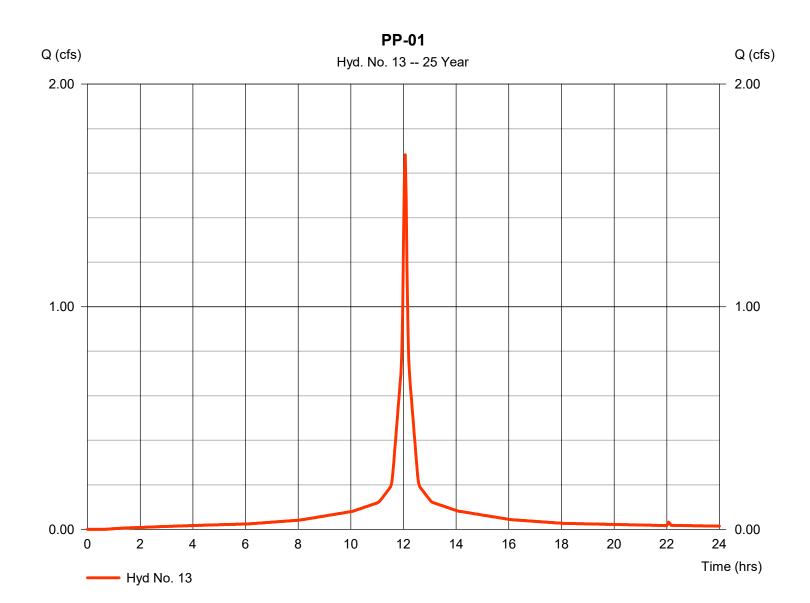
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#### **Hyd. No. 13**

PP-01

= SCS Runoff Hydrograph type Peak discharge = 1.683 cfsStorm frequency = 25 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 5.839 cuftDrainage area = 0.271 acCurve number = 98 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



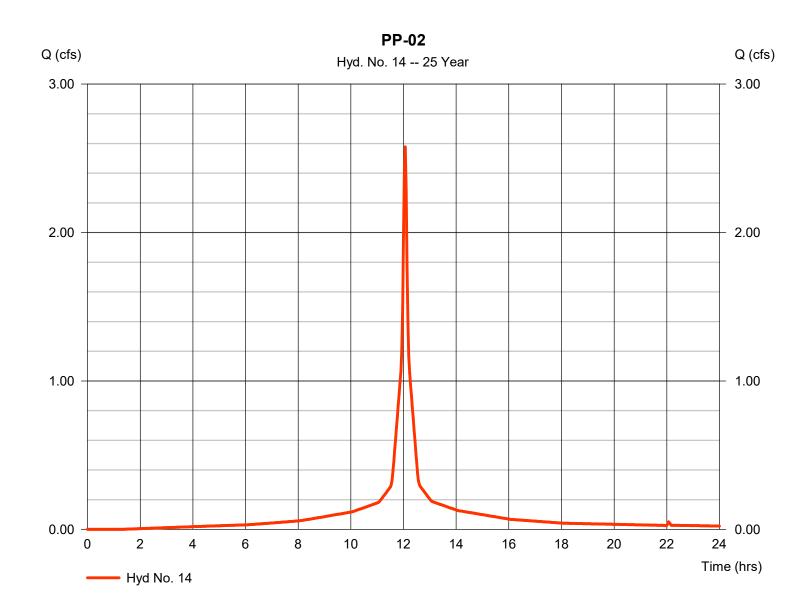
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### Hyd. No. 14

PP-02

= SCS Runoff Hydrograph type Peak discharge = 2.577 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 8,691 cuft Drainage area = 0.419 acCurve number = 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 6.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



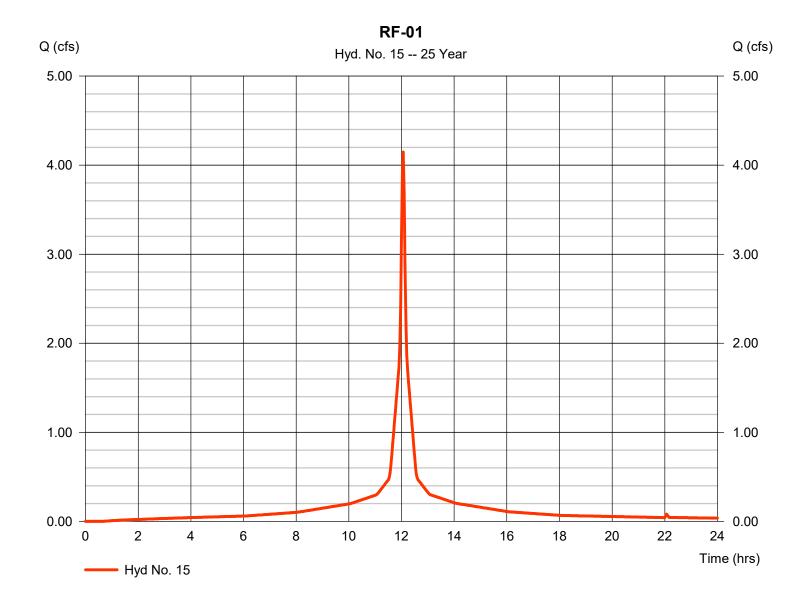
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#### Hyd. No. 15

**RF-01** 

Hydrograph type = SCS Runoff Peak discharge = 4.148 cfsStorm frequency = 25 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 14,393 cuft Curve number Drainage area = 0.668 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



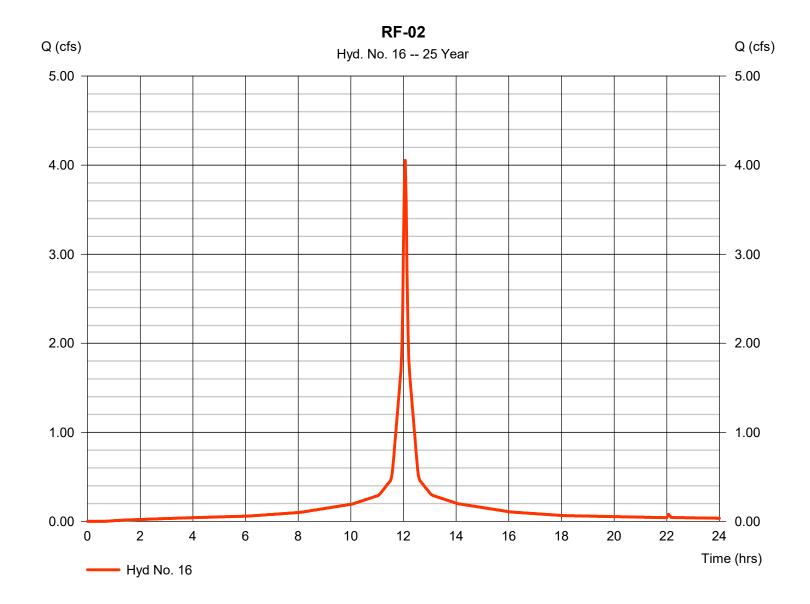
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#### Hyd. No. 16

**RF-02** 

Hydrograph type = SCS Runoff Peak discharge = 4.055 cfsStorm frequency = 25 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 14,070 cuftDrainage area Curve number = 0.653 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



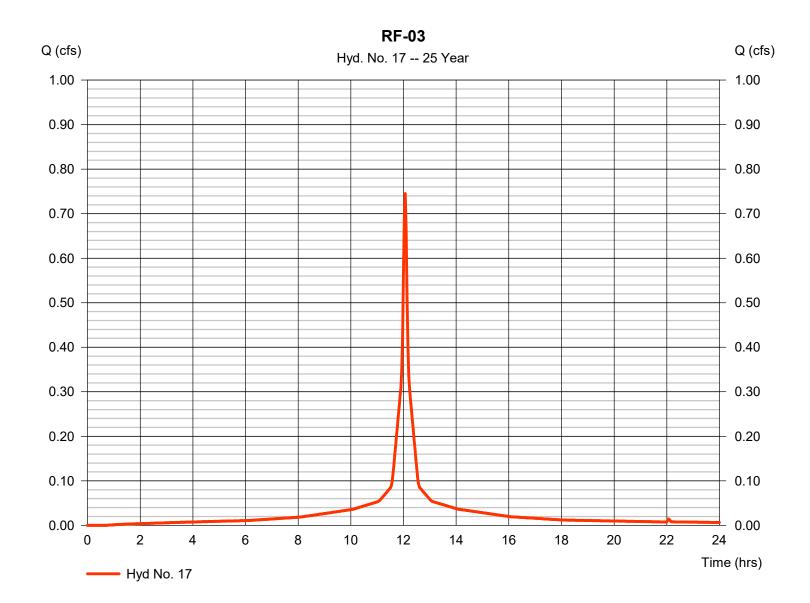
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#### Hyd. No. 17

**RF-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.745 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,586 cuftDrainage area Curve number = 0.120 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



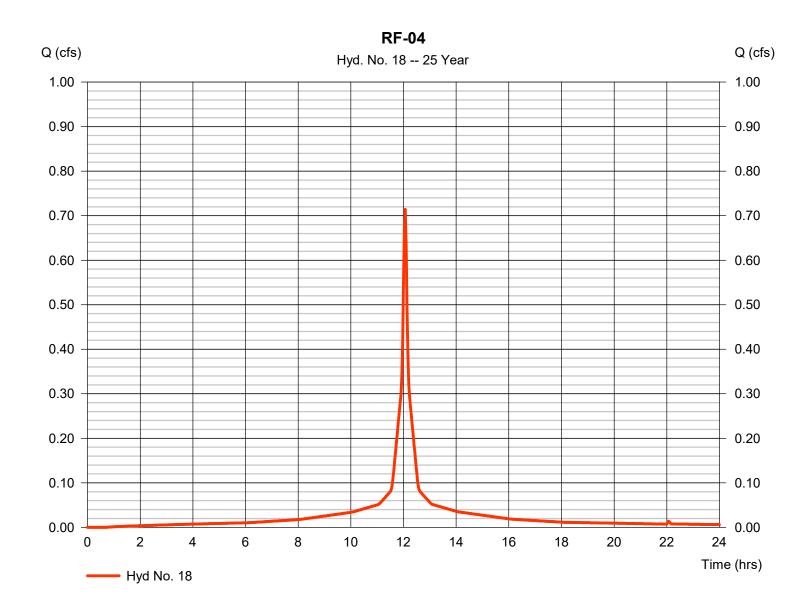
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#### **Hyd. No. 18**

**RF-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.714 cfsStorm frequency = 25 yrs Time to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,478 cuftDrainage area Curve number = 0.115 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



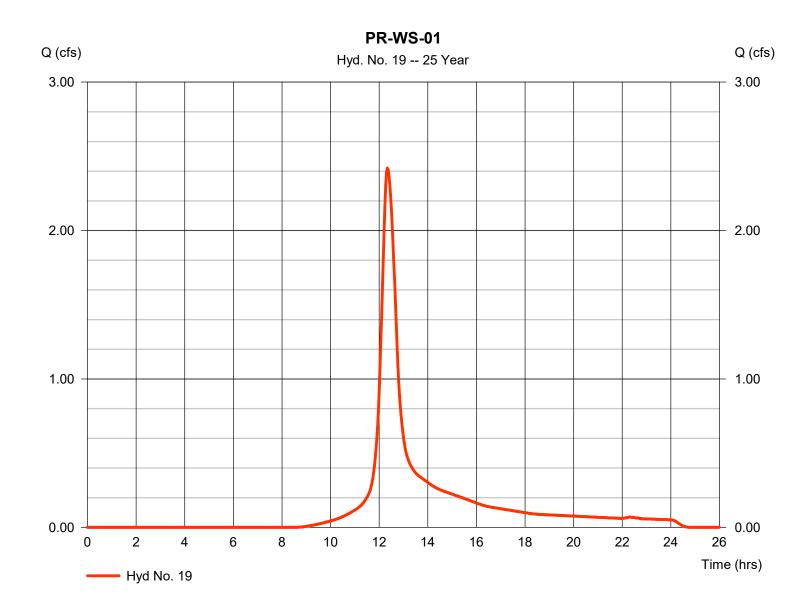
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### Hyd. No. 19

PR-WS-01

= SCS Runoff Hydrograph type Peak discharge = 2.421 cfsStorm frequency = 25 yrs Time to peak  $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 12,677 cuft Drainage area Curve number = 1.038 ac= 71 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 27.60 min = User Total precip. = 6.57 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



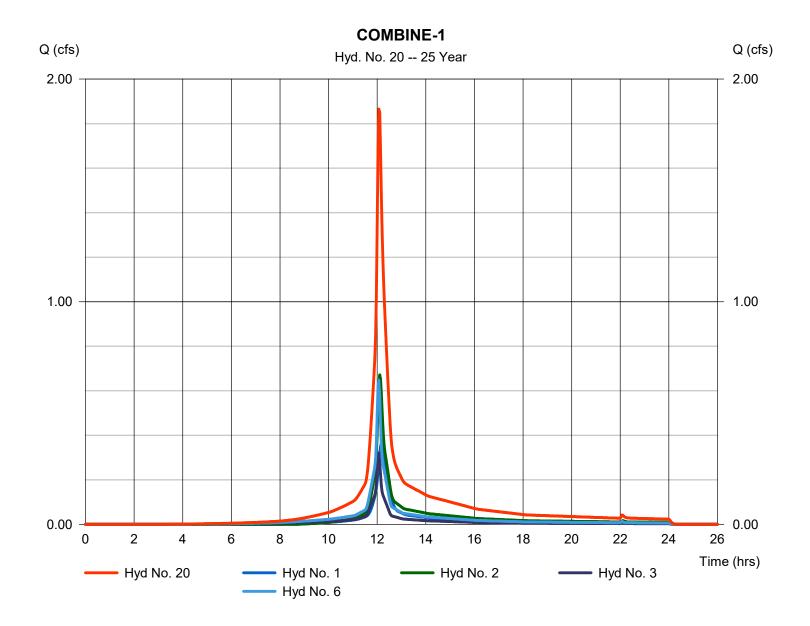
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### Hyd. No. 20

**COMBINE-1** 

Hydrograph type = Combine Peak discharge = 1.865 cfsStorm frequency = 25 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 6,841 cuft Inflow hyds. = 1, 2, 3, 6Contrib. drain. area = 0.471 ac



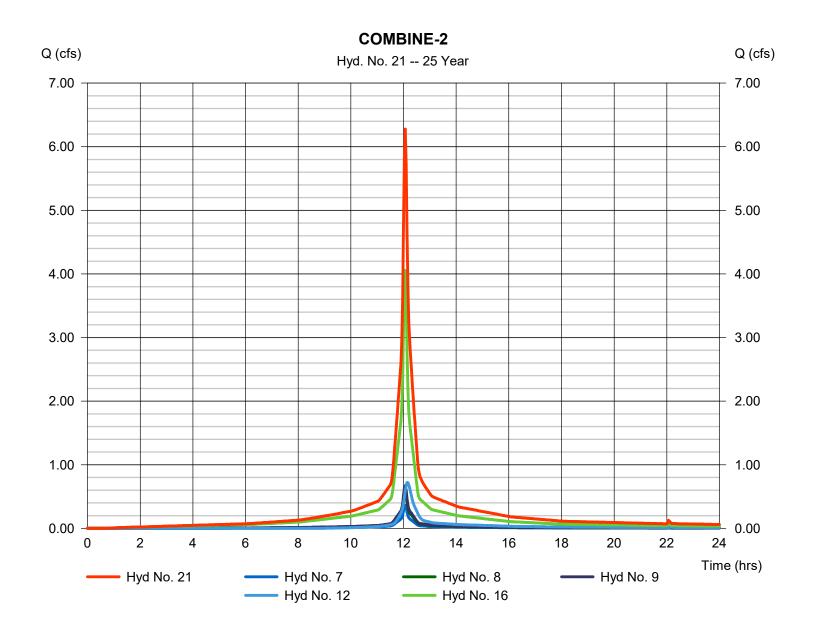
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### Hyd. No. 21

**COMBINE-2** 

Hydrograph type = Combine Peak discharge = 6.276 cfsStorm frequency Time to peak = 25 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 22,157 cuft Inflow hyds. = 7, 8, 9, 12, 16 Contrib. drain. area = 1.152 ac



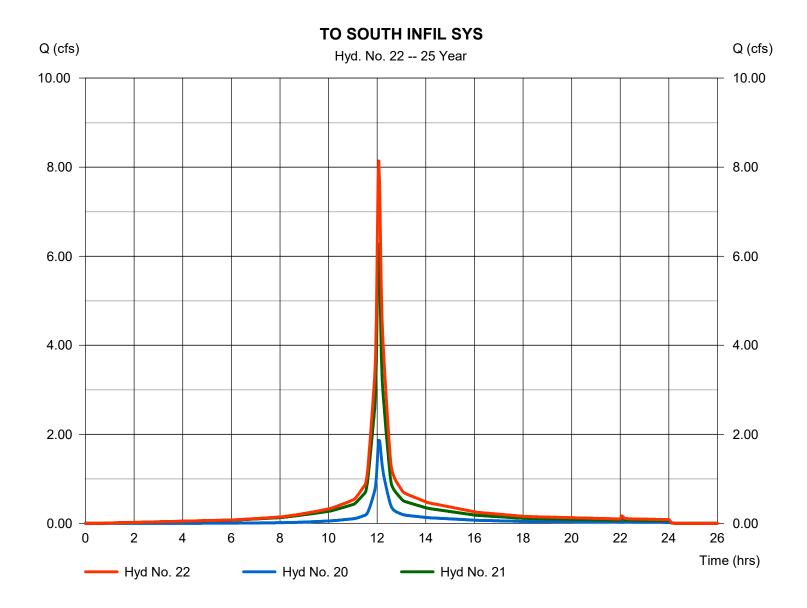
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### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type = Combine Peak discharge = 8.142 cfsStorm frequency Time to peak = 25 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 28,998 cuft Inflow hyds. = 20, 21 Contrib. drain. area = 0.000 ac



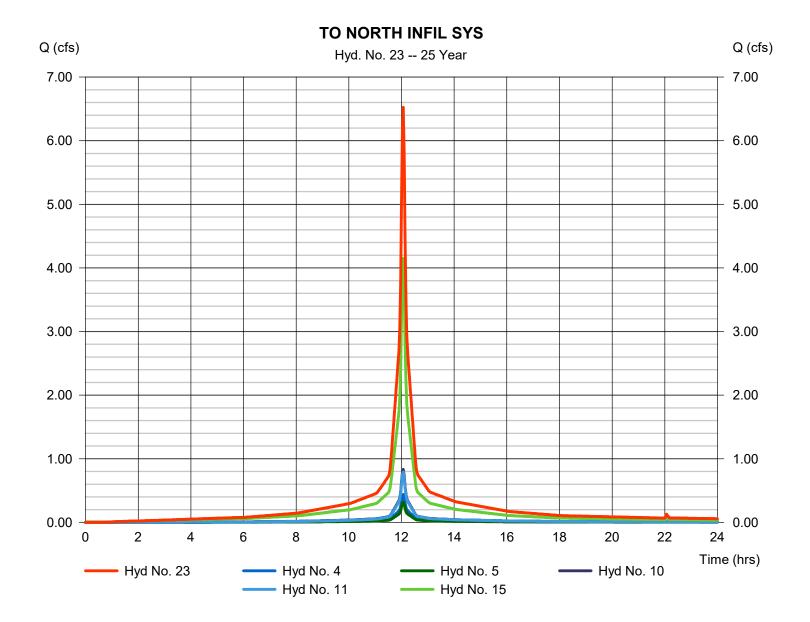
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### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type = Combine Peak discharge = 6.525 cfsStorm frequency Time to peak = 25 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 22,128 cuft Inflow hyds. = 4, 5, 10, 11, 15 Contrib. drain. area = 1.065 ac



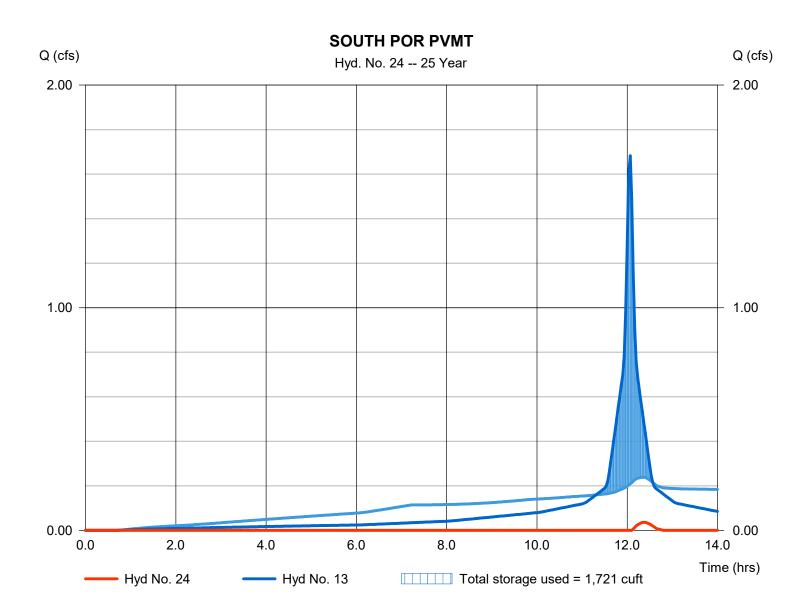
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### Hyd. No. 24

#### **SOUTH POR PVMT**

Hydrograph type = Reservoir Peak discharge = 0.036 cfsStorm frequency = 25 yrsTime to peak  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 49 cuft = 13 - PP-01 Max. Elevation Inflow hyd. No.  $= 142.11 \, \text{ft}$ = SOUTH POROUS PVMT Reservoir name Max. Storage = 1,721 cuft



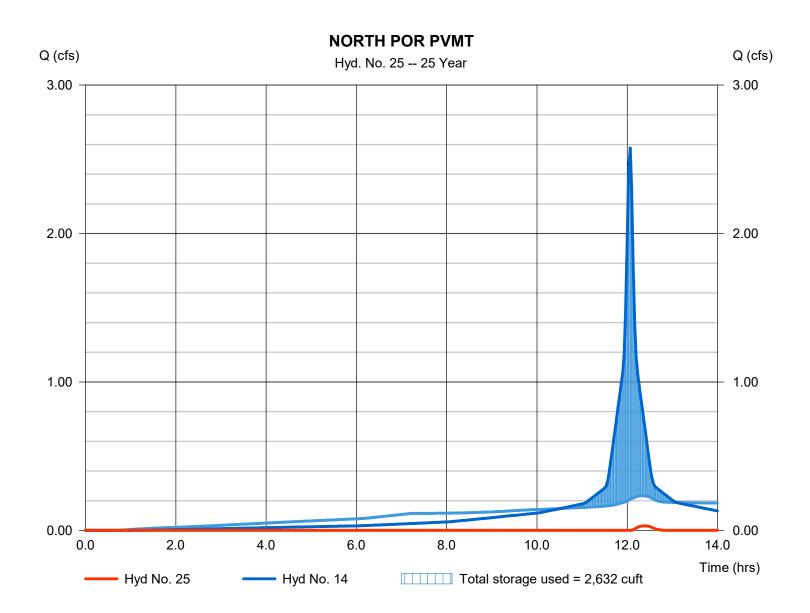
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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### Hyd. No. 25

#### NORTH POR PVMT

Hydrograph type Peak discharge = 0.031 cfs= Reservoir Storm frequency = 25 yrsTime to peak  $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 42 cuft Max. Elevation = 141.60 ftInflow hyd. No. = 14 - PP-02 Reservoir name = NORTH POROUS PVMT Max. Storage = 2,632 cuft



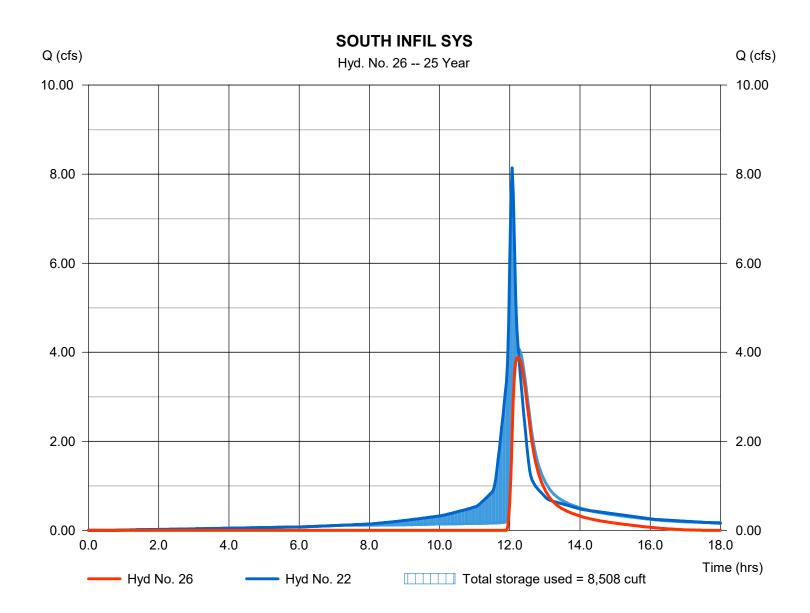
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### Hyd. No. 26

**SOUTH INFIL SYS** 

Hydrograph type = Reservoir Peak discharge = 3.888 cfsStorm frequency = 25 yrsTime to peak  $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 11,946 cuft Inflow hyd. No. Max. Elevation = 22 - TO SOUTH INFIL SYS = 143.96 ft= SOUTH INFIL SYS Reservoir name Max. Storage = 8,508 cuft



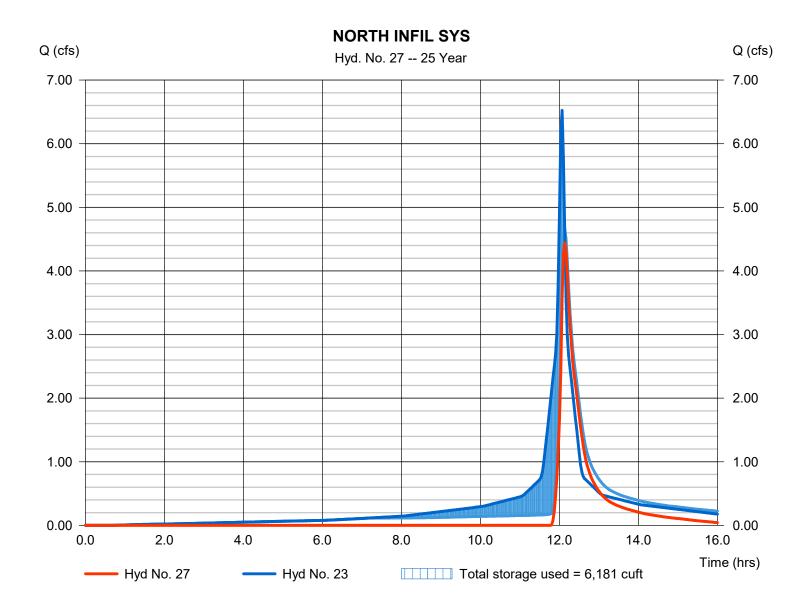
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### Hyd. No. 27

**NORTH INFIL SYS** 

Hydrograph type Peak discharge = 4.442 cfs= Reservoir Storm frequency = 25 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 9,585 cuft = 23 - TO NORTH INFIL SYS Max. Elevation Inflow hyd. No. = 144.19 ft= NORTH INFIL SYS Reservoir name Max. Storage = 6,181 cuft



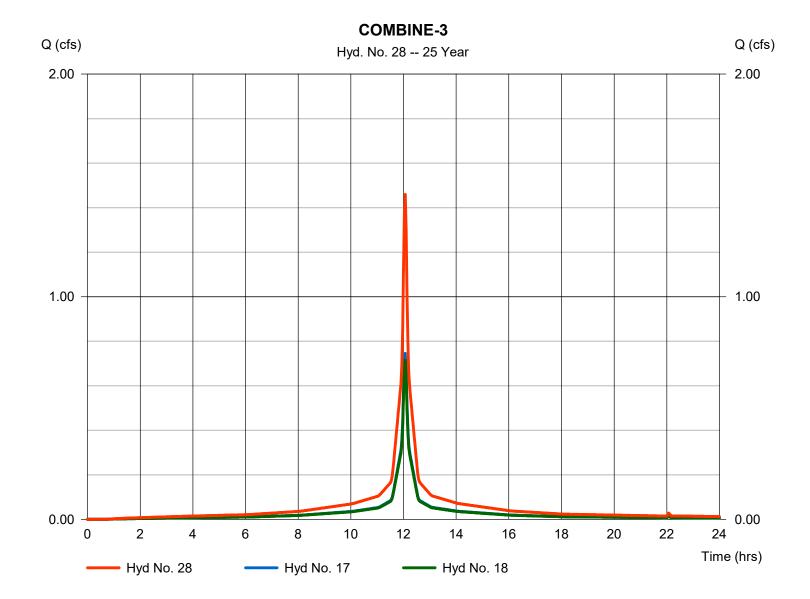
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### Hyd. No. 28

**COMBINE-3** 

Hydrograph type = Combine Peak discharge = 1.459 cfsTime to peak Storm frequency = 25 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 5,063 cuftInflow hyds. = 17, 18 Contrib. drain. area = 0.235 ac



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= 8.975 cfs

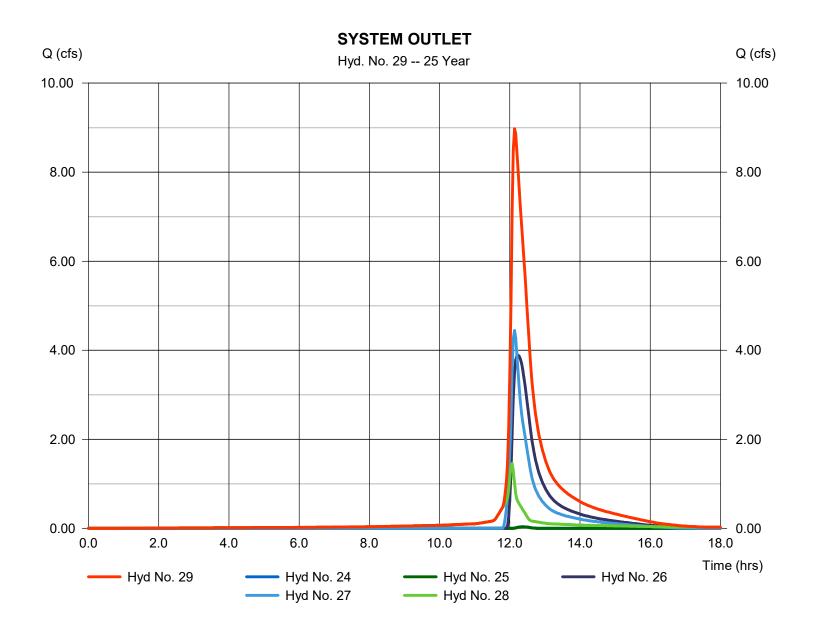
 $= 12.13 \, hrs$ 

### Hyd. No. 29

SYSTEM OUTLET

Hydrograph type= CombinePeak dischargeStorm frequency= 25 yrsTime to peakTime interval= 2 minHyd. volume

Time interval = 2 min Hyd. volume = 26,685 cuft Inflow hyds. = 24, 25, 26, 27, 28 Contrib. drain. area = 0.000 ac



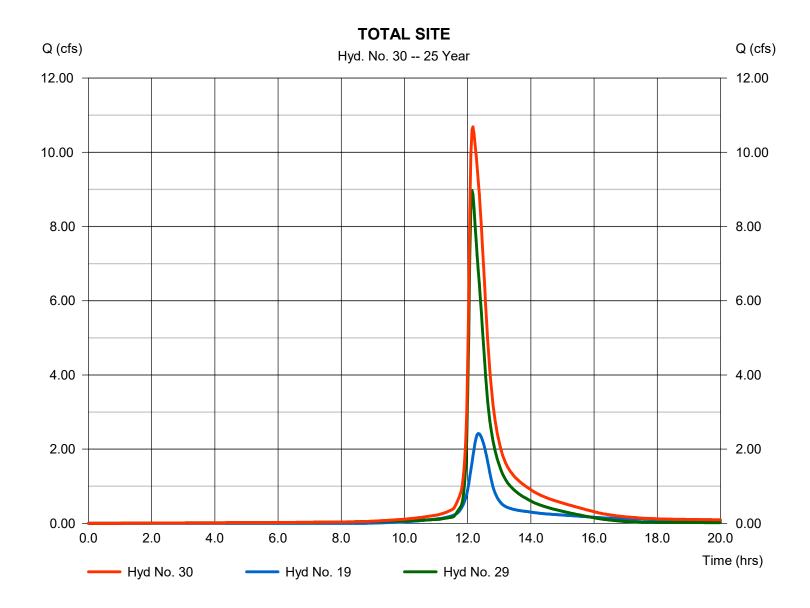
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### Hyd. No. 30

**TOTAL SITE** 

Hydrograph type = Combine Peak discharge = 10.69 cfsStorm frequency Time to peak = 25 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 39,362 cuft Inflow hyds. = 19, 29Contrib. drain. area = 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	0.436	2	730	1,778				CB-01	
2	SCS Runoff	0.822	2	726	2,808				CB-01A	
3	SCS Runoff	0.366	2	724	1,193				CB-02	
4	SCS Runoff	0.502	2	724	1,634				CB-03	
5	SCS Runoff	0.363	2	724	1,192				CB-04	
6	SCS Runoff	0.747	2	724	2,357				CB-05	
7	SCS Runoff	0.417	2	724	1,344				CB-06	
8	SCS Runoff	0.678	2	724	2,226				CB-07	
9	SCS Runoff	0.766	2	724	2,540				CB-08	
10	SCS Runoff	0.945	2	724	3,136				CB-09	
11	SCS Runoff	0.902	2	724	2,937				CB-10	
12	SCS Runoff	0.883	2	728	3,388				CB-11	
13	SCS Runoff	1.907	2	724	6,641				PP-01	
14	SCS Runoff	2.926	2	724	9,928				PP-02	
15	SCS Runoff	4.701	2	724	16,369				RF-01	
16	SCS Runoff	4.595	2	724	16,001				RF-02	
17	SCS Runoff	0.844	2	724	2,941				RF-03	
18	SCS Runoff	0.809	2	724	2,818				RF-04	
19	SCS Runoff	2.955	2	740	15,436				PR-WS-01	
20	Combine	2.210	2	724	8,135	1, 2, 3,			COMBINE-1	
21	Combine	7.186	2	724	25,500	6, 7, 8, 9,			COMBINE-2	
22	Combine	9.396	2	724	33,635	12, 16, 20, 21			TO SOUTH INFIL SYS	
23	Combine	7.413	2	724	25,268	4, 5, 10,			TO NORTH INFIL SYS	
24	Reservoir	0.106	2	742	184	11, 15, 13	142.19	1,961	SOUTH POR PVMT	
25	Reservoir	0.105	2	744	188	14	141.69	3,036	NORTH POR PVMT	
26	Reservoir	5.328	2	732	15,547	22	144.41	9,347	SOUTH INFIL SYS	
27	Reservoir	5.575	2	728	12,049	23	144.56	6,462	NORTH INFIL SYS	
28	Combine	1.654	2	724	5,759	17, 18,			COMBINE-3	
29	Combine	11.51	2	728	33,726	24, 25, 26,			SYSTEM OUTLET	
30	Combine	13.64	2	730	49,162	27, 28 19, 29			TOTAL SITE	
F0173-02 Hydrographs - Proposed.gpw					Return	Return Period: 50 Year			Friday, 07 / 9 / 2021	

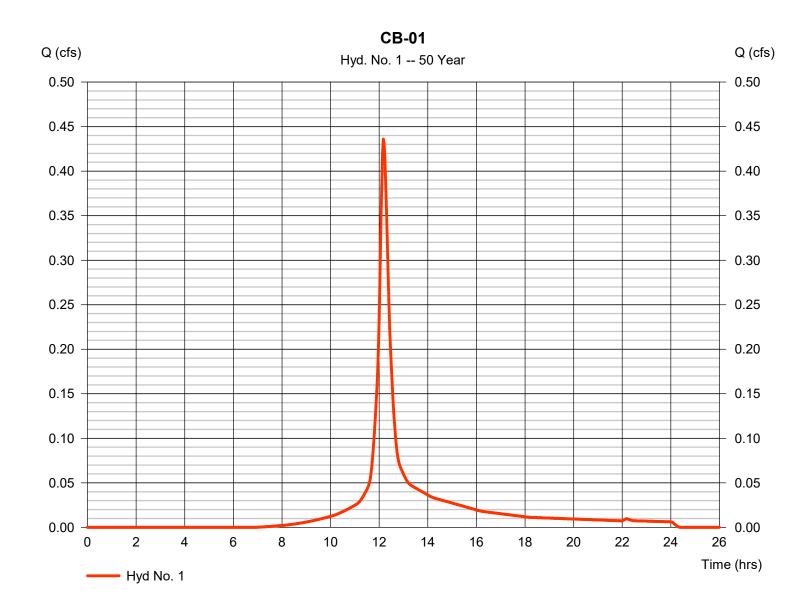
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### Hyd. No. 1

CB-01

Hydrograph type = SCS Runoff Peak discharge = 0.436 cfsStorm frequency = 50 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 1,778 cuft Drainage area Curve number = 0.108 ac= 76 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 14.20 min = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

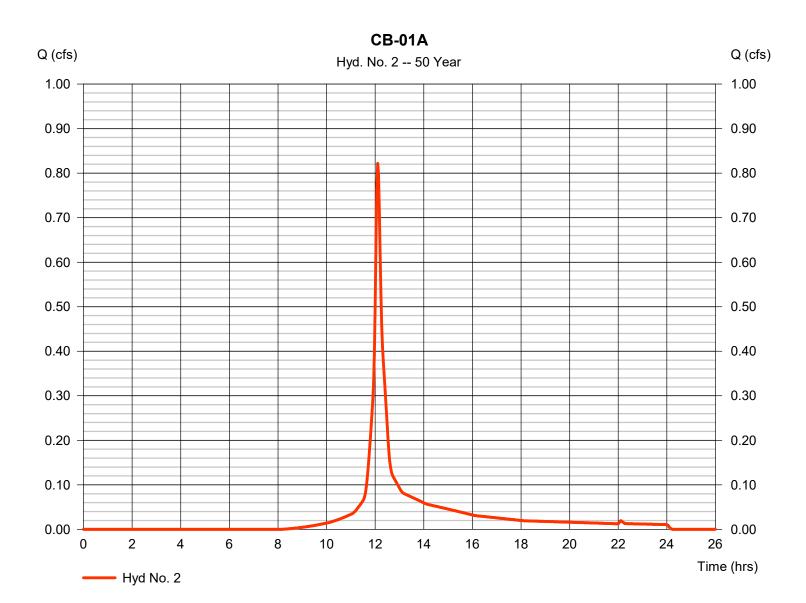


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### Hyd. No. 2

**CB-01A** 

Hydrograph type = SCS Runoff Peak discharge = 0.822 cfsStorm frequency = 50 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 2.808 cuft Drainage area Curve number = 0.194 ac= 70 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 7.80 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



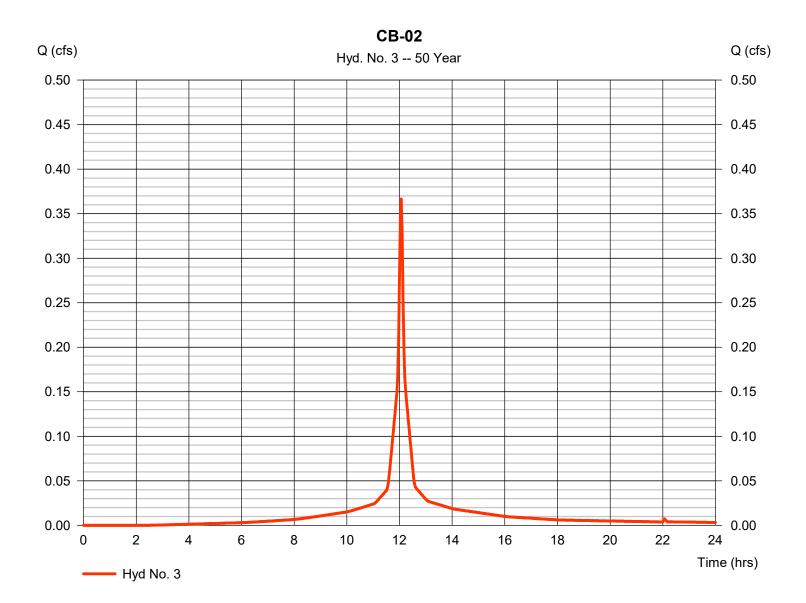
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### Hyd. No. 3

**CB-02** 

Hydrograph type = SCS Runoff Peak discharge = 0.366 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,193 cuft Drainage area Curve number = 0.054 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

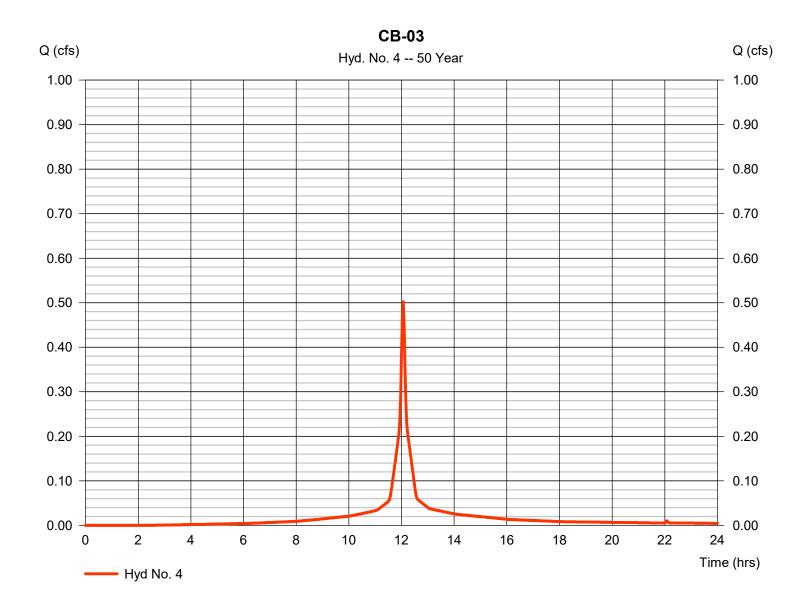


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### Hyd. No. 4

**CB-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.502 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 1,634 cuft Drainage area Curve number = 0.074 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

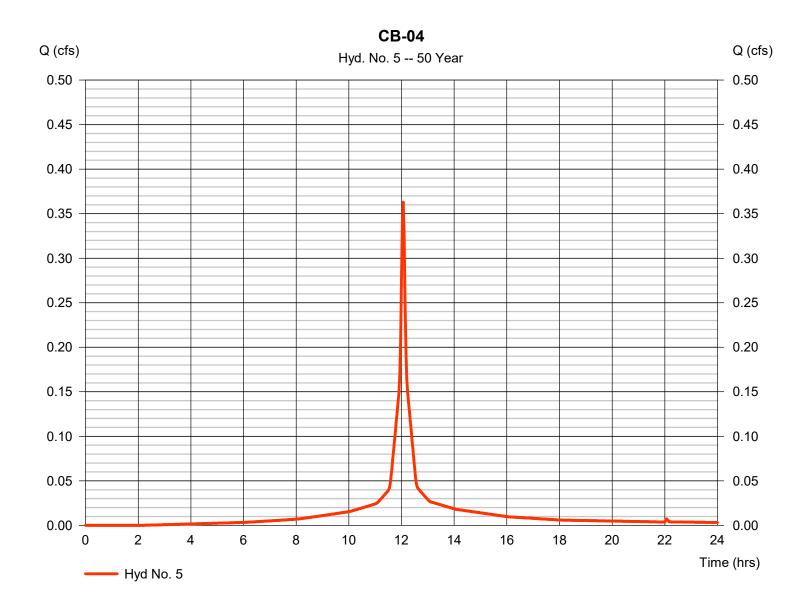


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### Hyd. No. 5

**CB-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.363 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,192 cuft Drainage area Curve number = 0.053 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

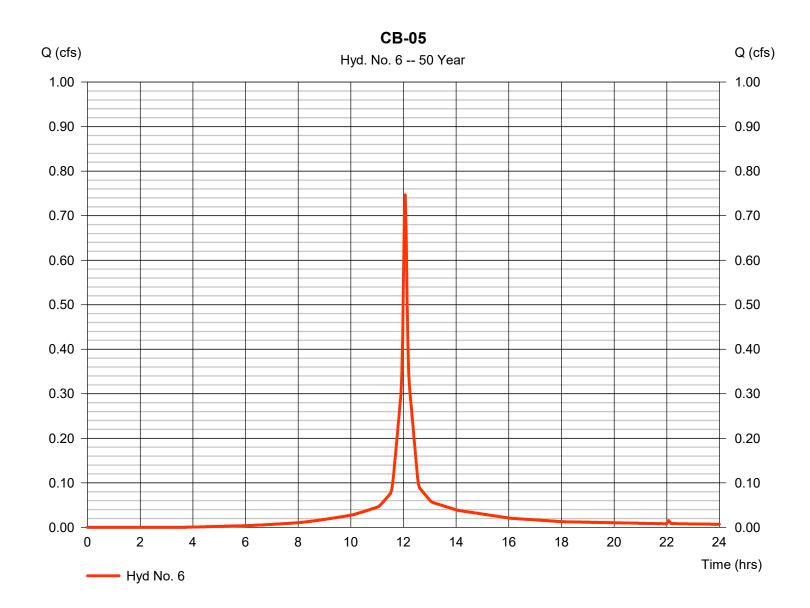


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### Hyd. No. 6

**CB-05** 

Hydrograph type = SCS Runoff Peak discharge = 0.747 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 2,357 cuftDrainage area Curve number = 0.115 ac= 88 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



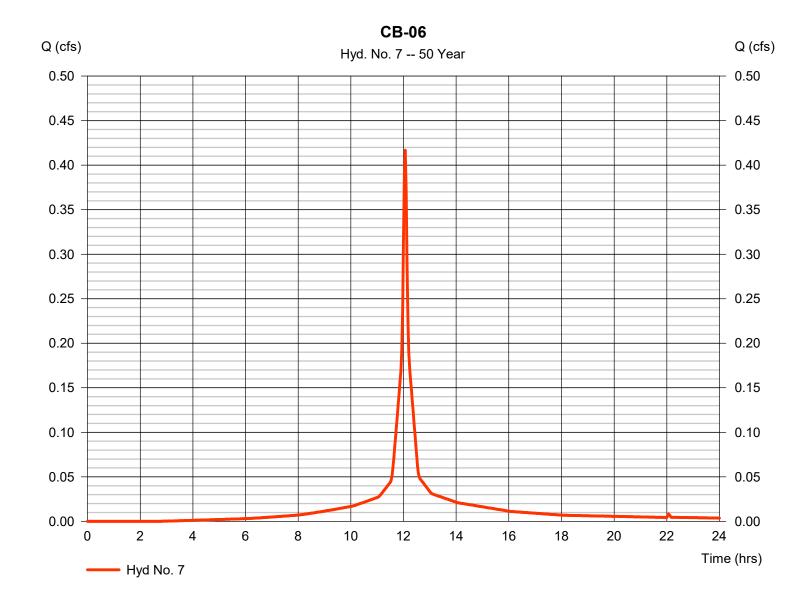
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#### Hyd. No. 7

**CB-06** 

Hydrograph type = SCS Runoff Peak discharge = 0.417 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,344 cuft Drainage area Curve number = 0.062 ac= 91 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



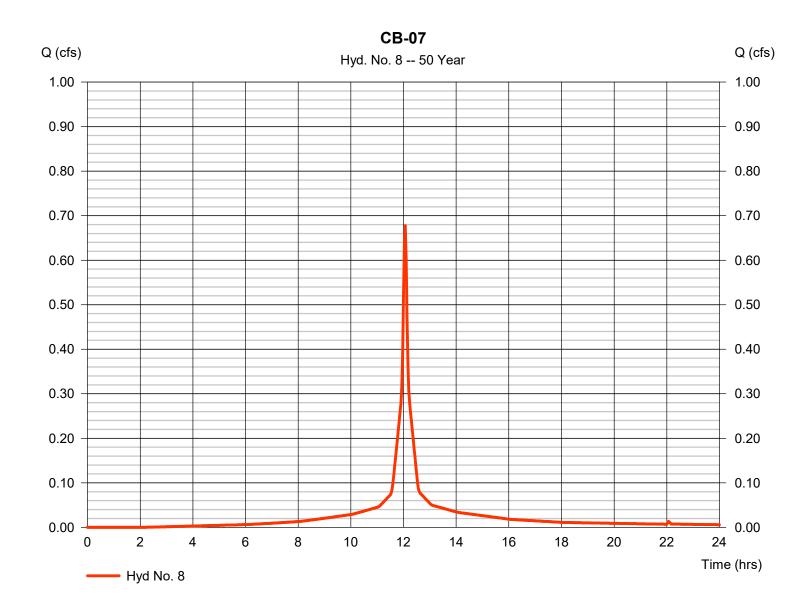
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### Hyd. No. 8

**CB-07** 

Hydrograph type = SCS Runoff Peak discharge = 0.678 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,226 cuft Drainage area Curve number = 0.099 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



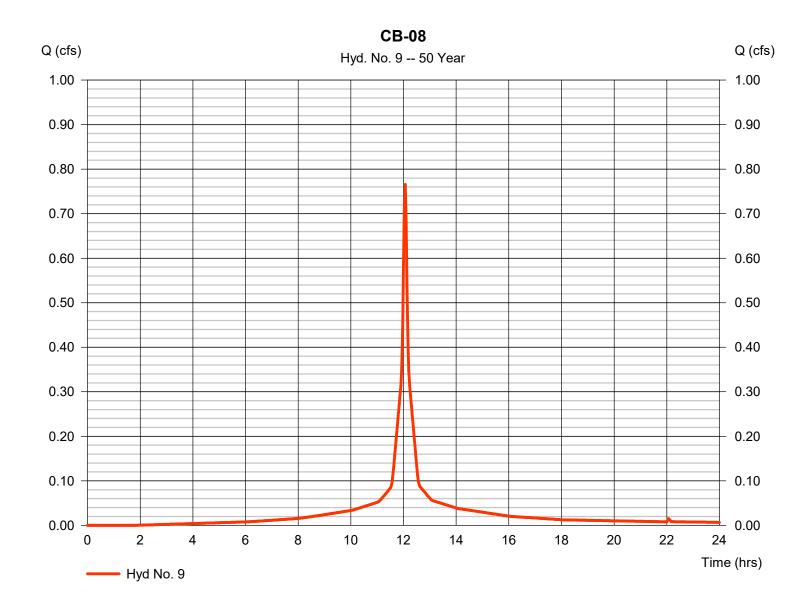
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### Hyd. No. 9

**CB-08** 

Hydrograph type = SCS Runoff Peak discharge = 0.766 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 2,540 cuftDrainage area = 0.111 acCurve number = 94 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.50 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

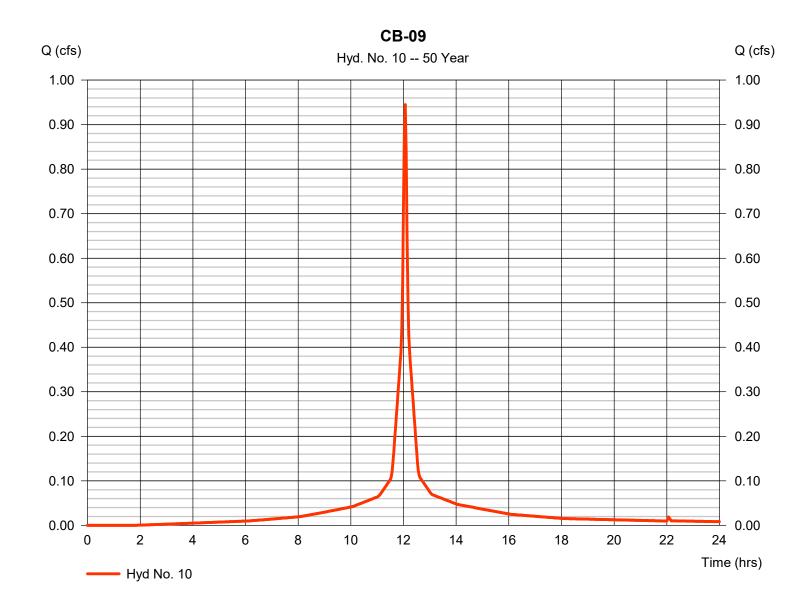


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### Hyd. No. 10

**CB-09** 

Hydrograph type = SCS Runoff Peak discharge = 0.945 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 3,136 cuftDrainage area Curve number = 0.137 ac= 94 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

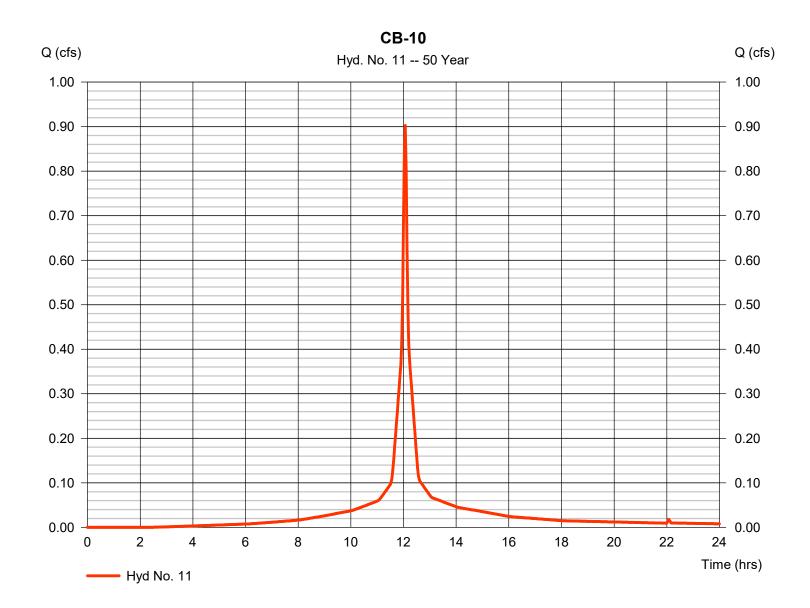


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#### Hyd. No. 11

**CB-10** 

Hydrograph type = SCS Runoff Peak discharge = 0.902 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,937 cuftDrainage area = 0.133 acCurve number = 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



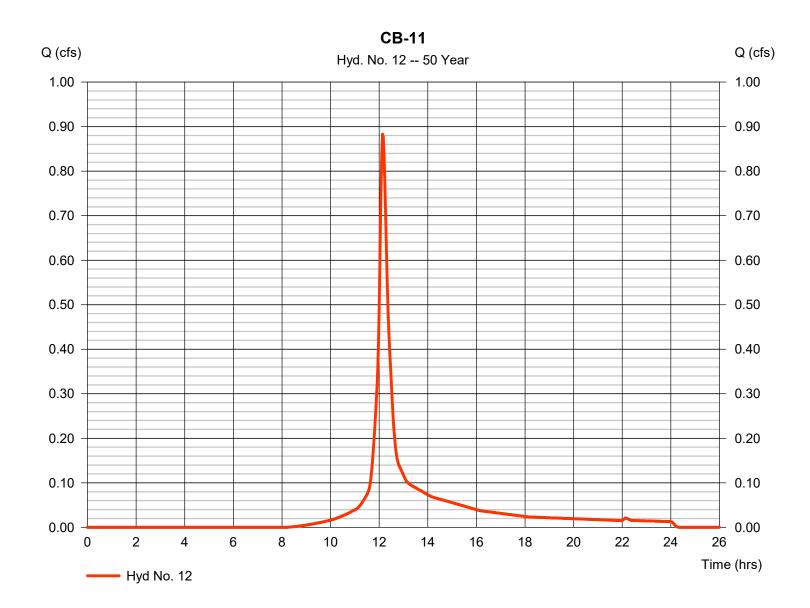
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### Hyd. No. 12

**CB-11** 

Hydrograph type = SCS Runoff Peak discharge = 0.883 cfsStorm frequency = 50 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 3,388 cuft Drainage area = 0.227 acCurve number = 70 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 10.90 min = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

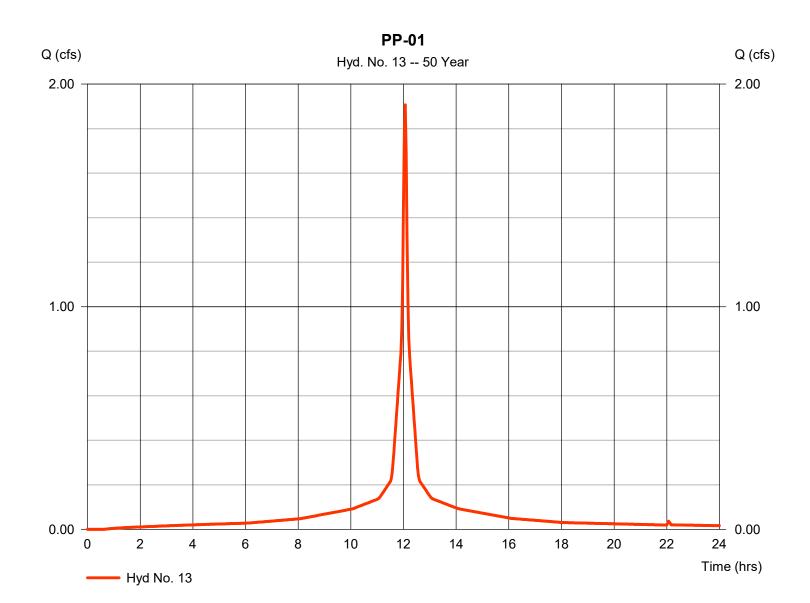


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### **Hyd. No. 13**

PP-01

= SCS Runoff Hydrograph type Peak discharge = 1.907 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 6,641 cuftDrainage area = 0.271 acCurve number = 98 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method = User Time of conc. (Tc)  $= 5.00 \, \text{min}$ Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



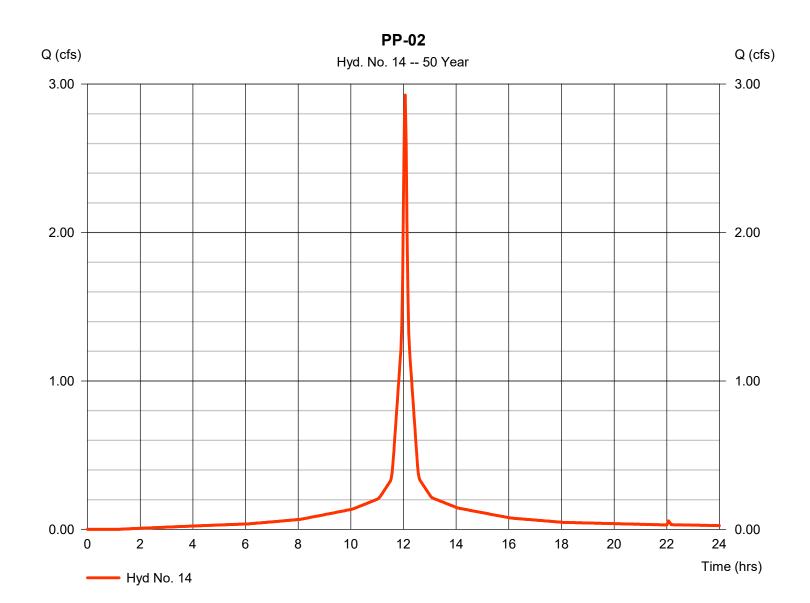
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### Hyd. No. 14

PP-02

= SCS Runoff Hydrograph type Peak discharge = 2.926 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 9,928 cuft Drainage area Curve number = 0.419 ac= 96 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 6.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



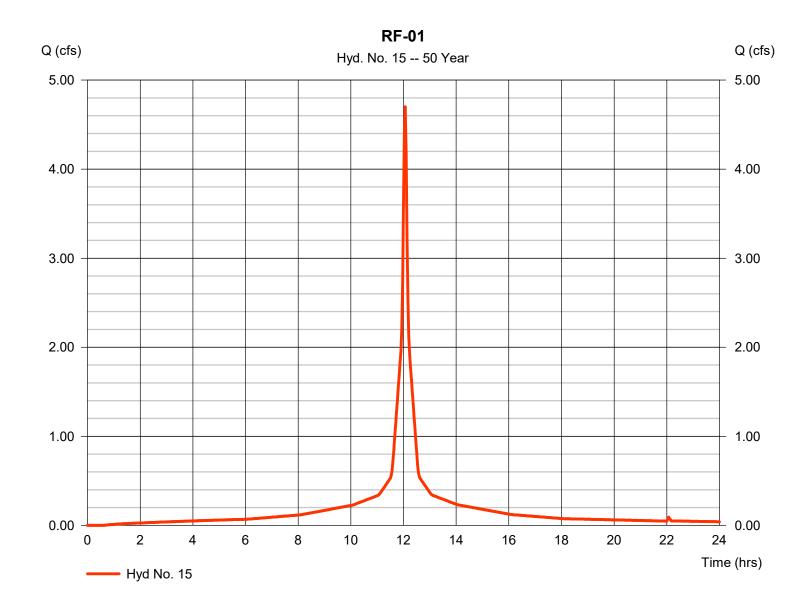
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### Hyd. No. 15

**RF-01** 

Hydrograph type = SCS Runoff Peak discharge = 4.701 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 16,369 cuftDrainage area Curve number = 0.668 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

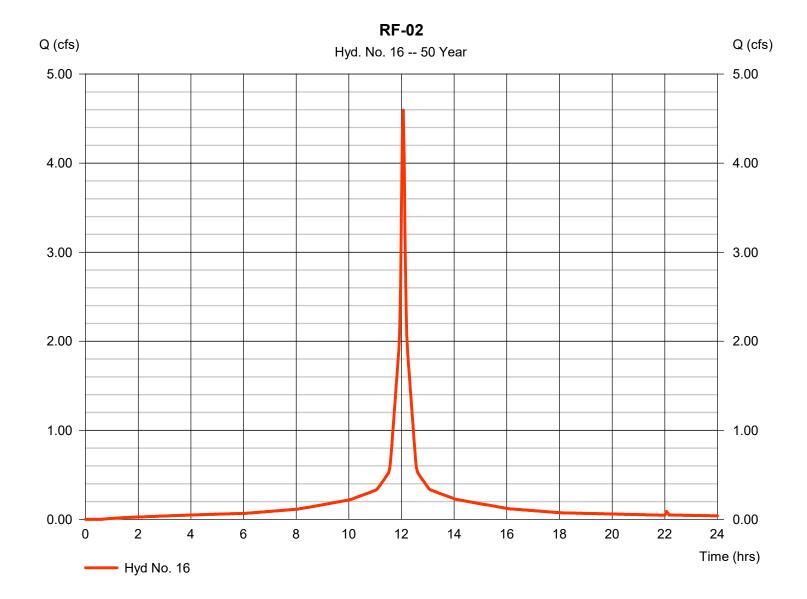


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### Hyd. No. 16

**RF-02** 

Hydrograph type = SCS Runoff Peak discharge = 4.595 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 16,001 cuftDrainage area Curve number = 0.653 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

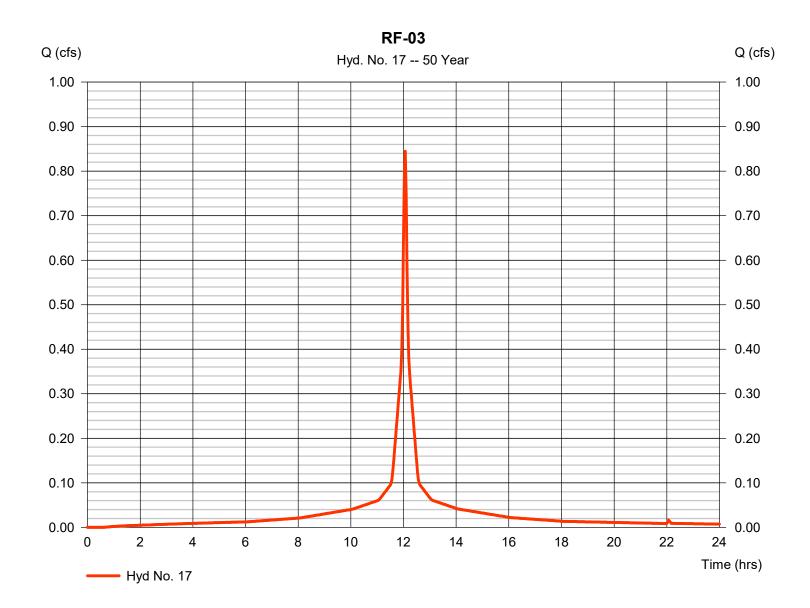


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### Hyd. No. 17

**RF-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.844 cfsStorm frequency = 50 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 2,941 cuftDrainage area = 0.120 acCurve number = 98 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

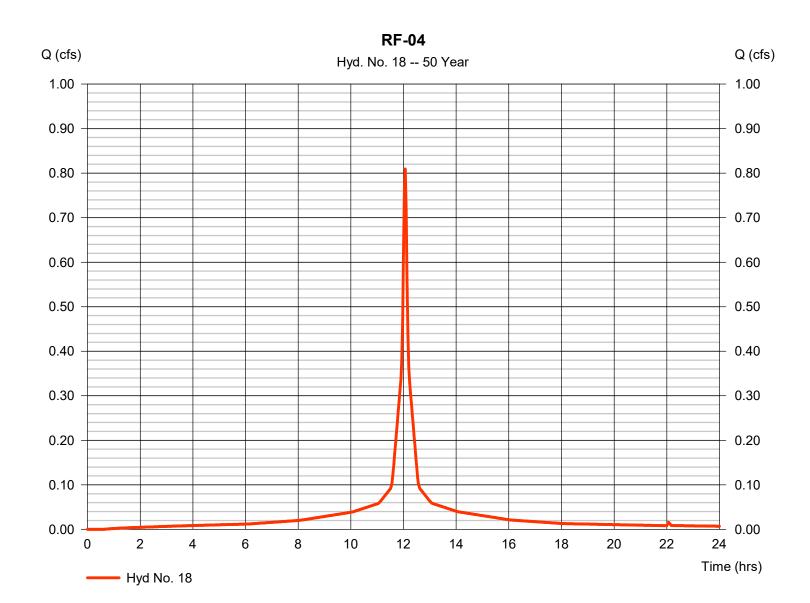


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### **Hyd. No. 18**

**RF-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.809 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,818 cuft Drainage area Curve number = 0.115 ac= 98 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

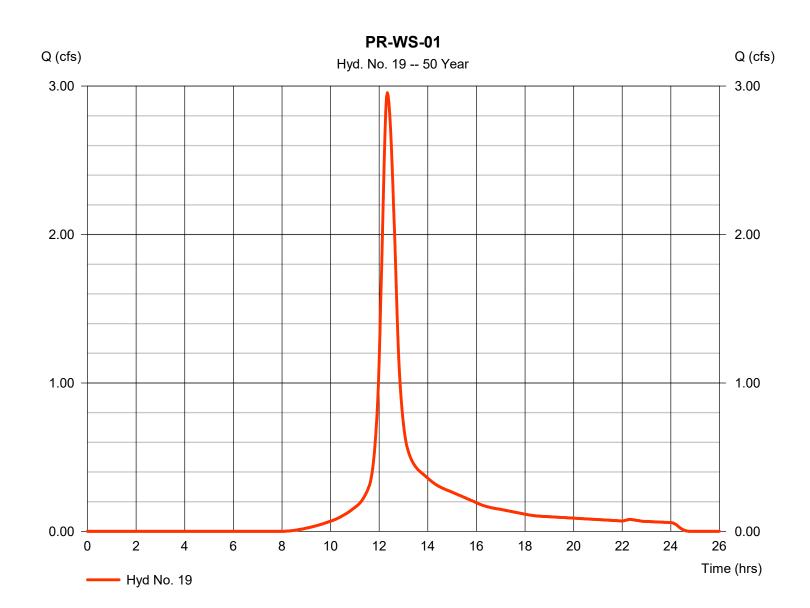


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### Hyd. No. 19

PR-WS-01

= SCS Runoff Hydrograph type Peak discharge = 2.955 cfsStorm frequency = 50 yrsTime to peak  $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 15,436 cuft Drainage area Curve number = 1.038 ac= 71 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 27.60 min = User Total precip. = 7.44 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

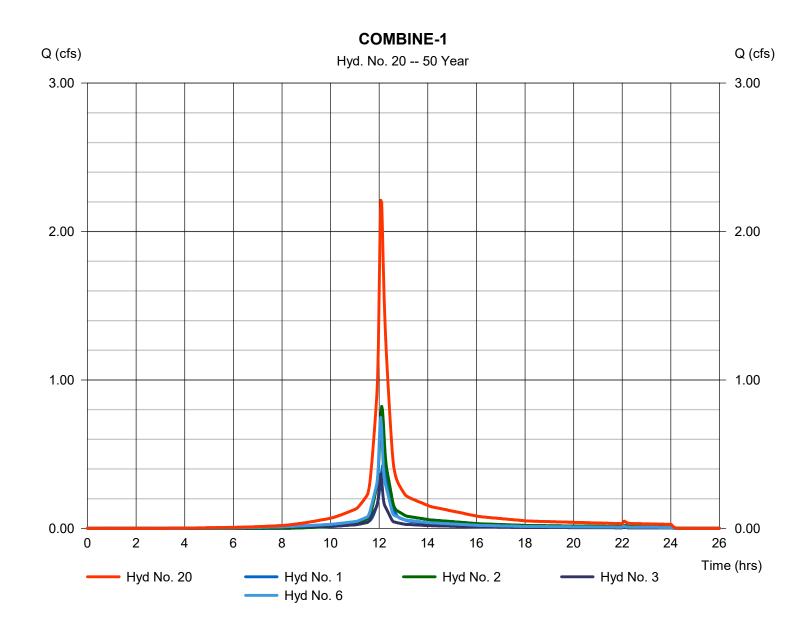


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### Hyd. No. 20

**COMBINE-1** 

Hydrograph type = Combine Peak discharge = 2.210 cfsStorm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 8,135 cuft Inflow hyds. = 1, 2, 3, 6Contrib. drain. area = 0.471 ac

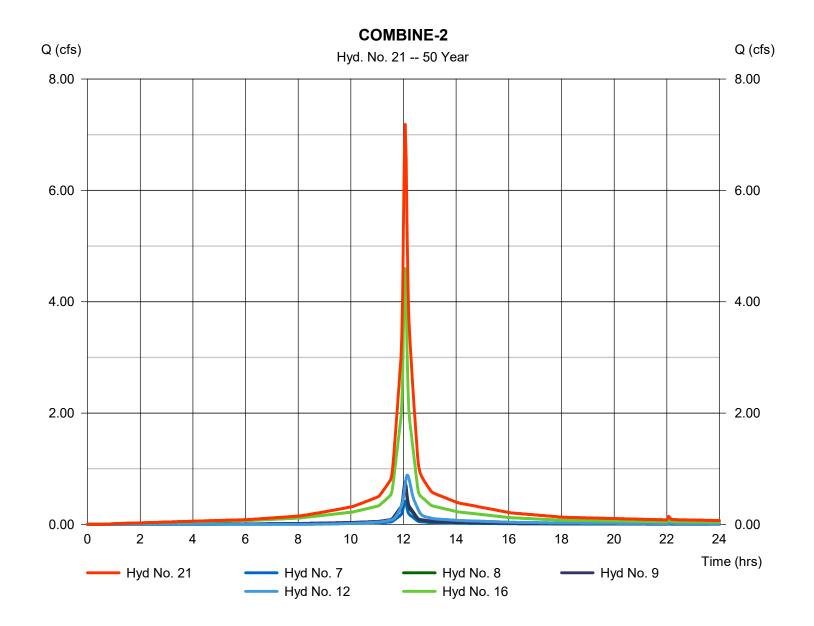


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### Hyd. No. 21

**COMBINE-2** 

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min Inflow hyds. = 7, 8, 9, 12, 16 Peak discharge = 7.186 cfs
Time to peak = 12.07 hrs
Hyd. volume = 25,500 cuft
Contrib. drain. area = 1.152 ac



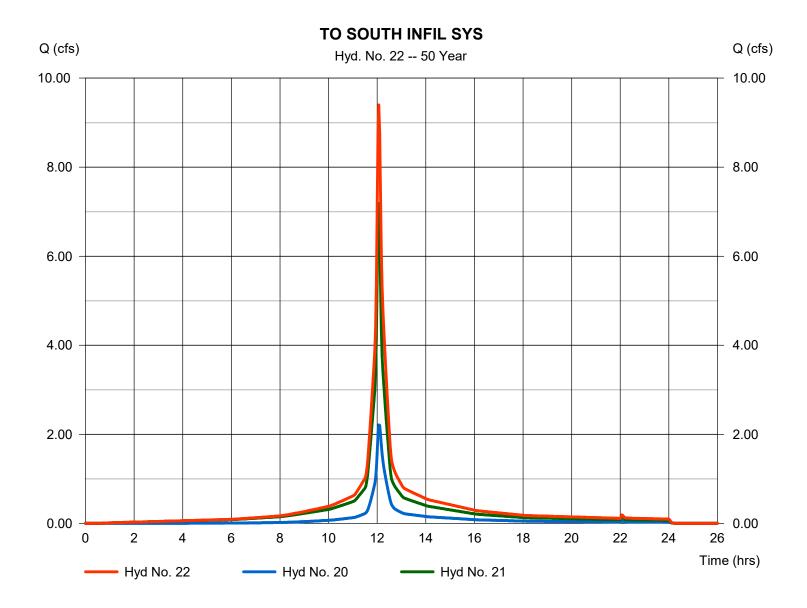
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### Hyd. No. 22

TO SOUTH INFIL SYS

Peak discharge Hydrograph type = Combine = 9.396 cfsStorm frequency Time to peak = 50 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 33,635 cuft Inflow hyds. = 20, 21 Contrib. drain. area = 0.000 ac



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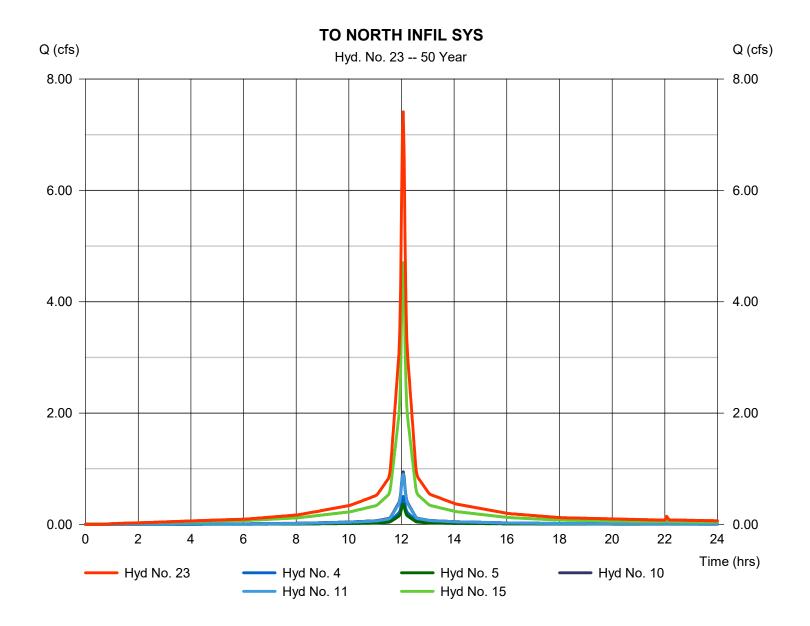
### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type = Combine Storm frequency = 50 yrs Time interval = 2 min

Inflow hyds. = 4, 5, 10, 11, 15

Peak discharge = 7.413 cfs
Time to peak = 12.07 hrs
Hyd. volume = 25,268 cuft
Contrib. drain. area = 1.065 ac



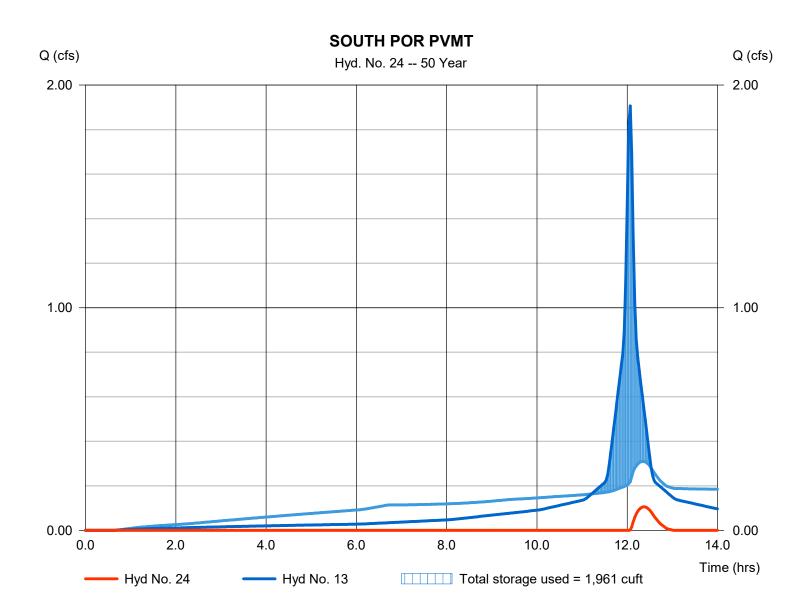
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### Hyd. No. 24

#### **SOUTH POR PVMT**

Hydrograph type = Reservoir Peak discharge = 0.106 cfsStorm frequency = 50 yrsTime to peak  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 184 cuft Inflow hyd. No. = 13 - PP-01 Max. Elevation = 142.19 ft= SOUTH POROUS PVMT Reservoir name Max. Storage = 1,961 cuft



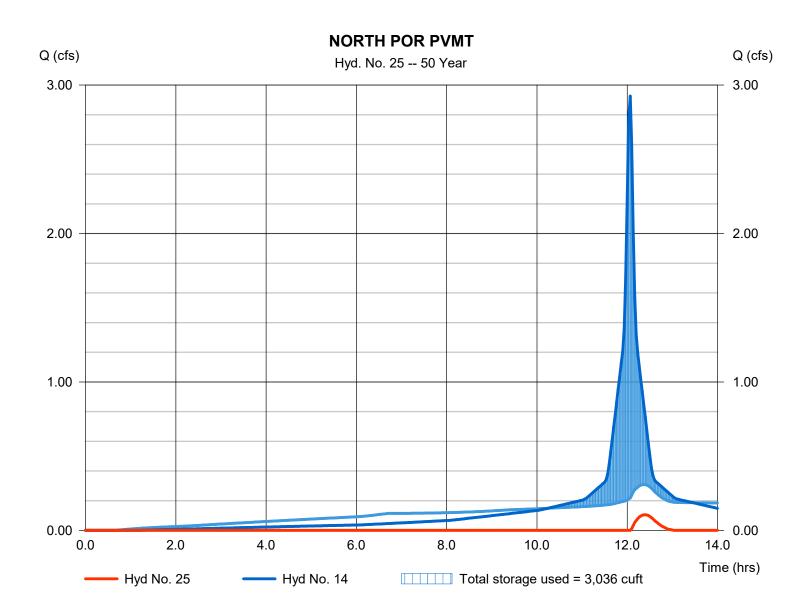
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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#### Hyd. No. 25

#### NORTH POR PVMT

Hydrograph type = Reservoir Peak discharge = 0.105 cfsStorm frequency = 50 yrsTime to peak  $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 188 cuft Inflow hyd. No. = 14 - PP-02 Max. Elevation = 141.69 ftReservoir name = NORTH POROUS PVMT Max. Storage = 3,036 cuft



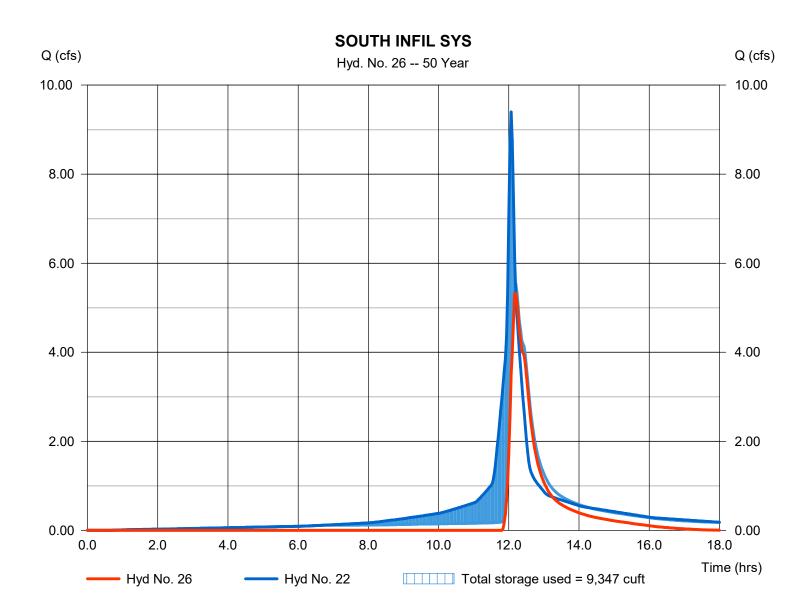
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#### Hyd. No. 26

**SOUTH INFIL SYS** 

Hydrograph type = Reservoir Peak discharge = 5.328 cfsStorm frequency = 50 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 15,547 cuft Inflow hyd. No. Max. Elevation = 22 - TO SOUTH INFIL SYS = 144.41 ft= SOUTH INFIL SYS Reservoir name Max. Storage = 9,347 cuft



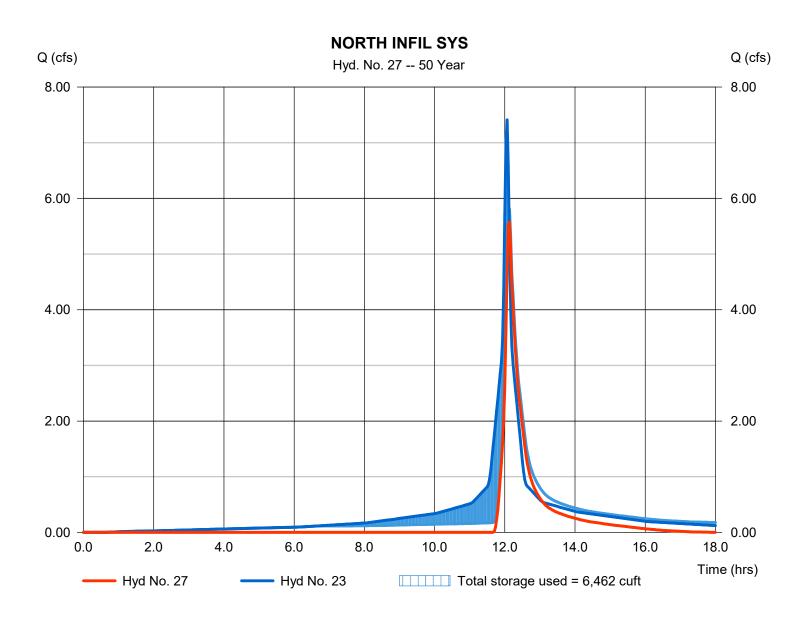
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#### Hyd. No. 27

**NORTH INFIL SYS** 

Hydrograph type = Reservoir Peak discharge = 5.575 cfsStorm frequency = 50 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 12,049 cuftInflow hyd. No. Max. Elevation = 144.56 ft= 23 - TO NORTH INFIL SYS = NORTH INFIL SYS Reservoir name Max. Storage = 6,462 cuft

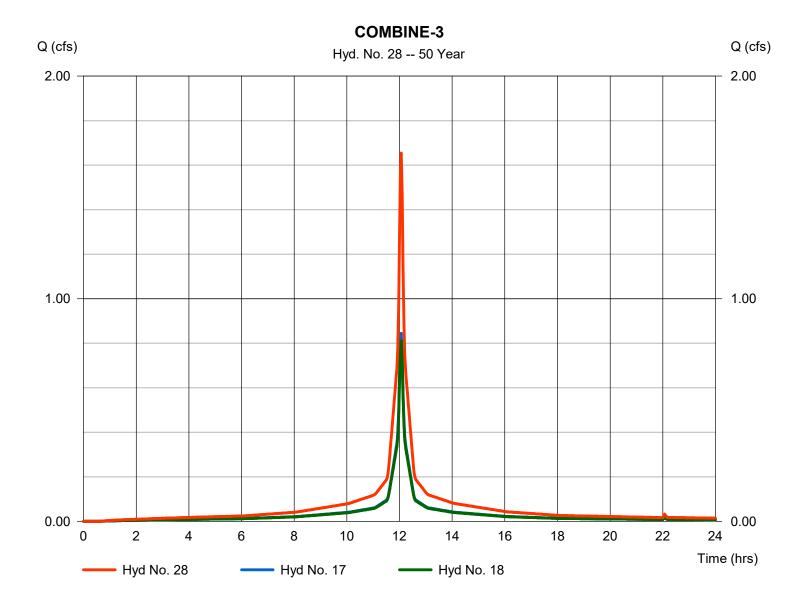


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#### Hyd. No. 28

**COMBINE-3** 

Hydrograph type = Combine Peak discharge = 1.654 cfsTime to peak Storm frequency = 50 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 5,759 cuftInflow hyds. = 17, 18 Contrib. drain. area = 0.235 ac

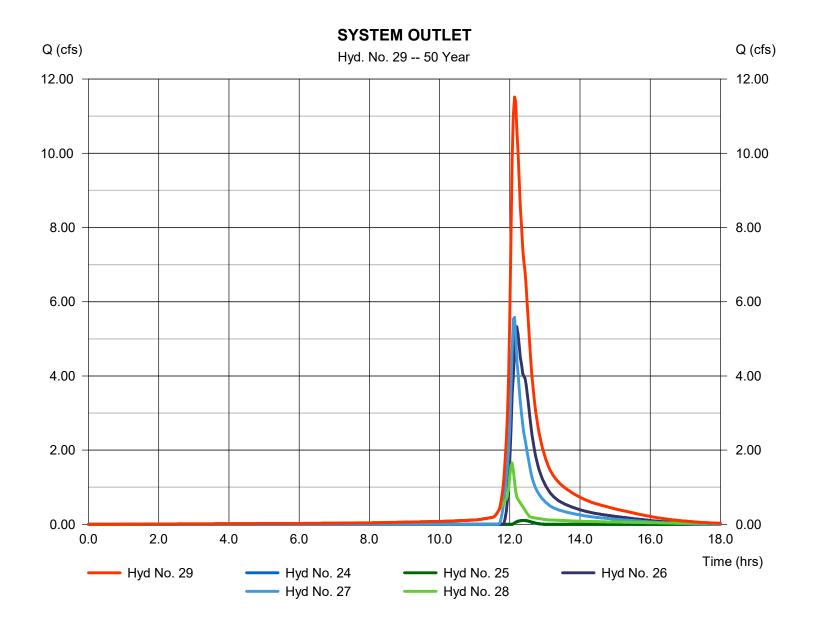


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#### Hyd. No. 29

SYSTEM OUTLET

Hydrograph type = Combine Peak discharge = 11.51 cfsStorm frequency Time to peak = 50 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 33,726 cuft Inflow hyds. = 24, 25, 26, 27, 28 Contrib. drain. area = 0.000 ac

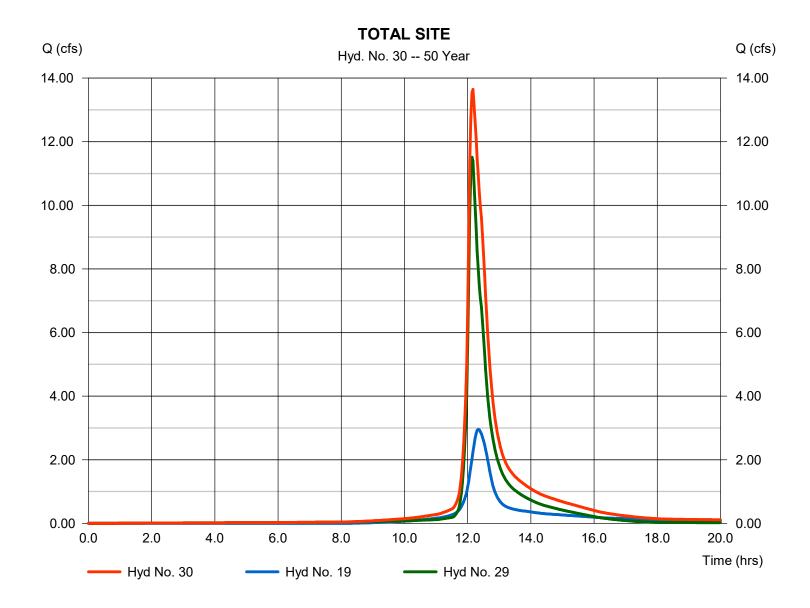


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#### Hyd. No. 30

**TOTAL SITE** 

Hydrograph type = Combine Peak discharge = 13.64 cfsStorm frequency Time to peak = 50 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 49,162 cuft Inflow hyds. = 19, 29Contrib. drain. area = 1.038 ac



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

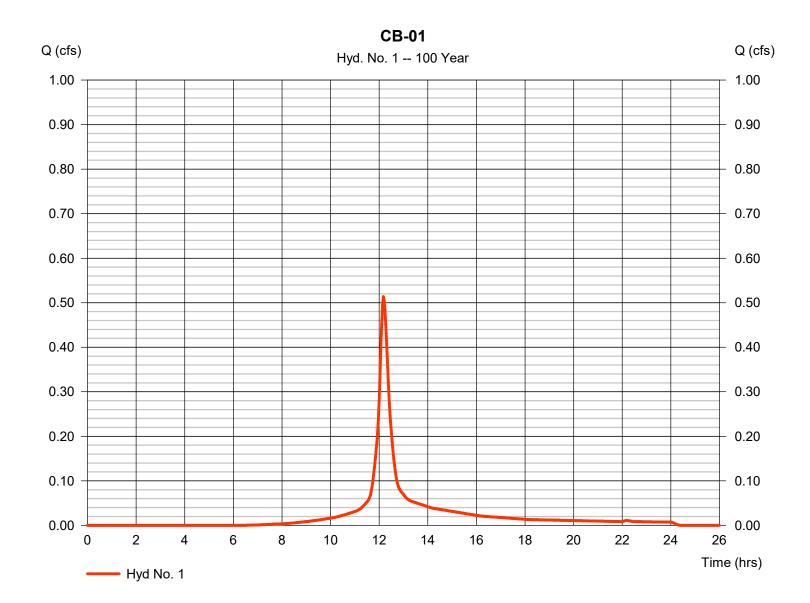
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.514	2	730	2,101				CB-01
2	SCS Runoff	0.987	2	726	3,369				CB-01A
3	SCS Runoff	0.415	2	724	1,362				CB-02
4	SCS Runoff	0.569	2	724	1,866				CB-03
5	SCS Runoff	0.410	2	724	1,358				CB-04
6	SCS Runoff	0.852	2	724	2,712				CB-05
7	SCS Runoff	0.473	2	724	1,538				CB-06
8	SCS Runoff	0.767	2	724	2,537				CB-07
9	SCS Runoff	0.865	2	724	2,890				CB-08
10	SCS Runoff	1.068	2	724	3,567				CB-09
11	SCS Runoff	1.023	2	724	3,354				CB-10
12	SCS Runoff	1.061	2	728	4,065				CB-11
13	SCS Runoff	2.147	2	724	7,498				PP-01
14	SCS Runoff	3.298	2	724	11,250				PP-02
15	SCS Runoff	5.291	2	724	18,482				RF-01
16	SCS Runoff	5.172	2	724	18,067				RF-02
17	SCS Runoff	0.951	2	724	3,320				RF-03
18	SCS Runoff	0.911	2	724	3,182				RF-04
19	SCS Runoff	3.537	2	740	18,471				PR-WS-01
20	Combine	2.583	2	724	9,543	1, 2, 3,			COMBINE-1
21	Combine	8.161	2	724	29,097	6, 7, 8, 9,			COMBINE-2
22	Combine	10.74	2	724	38,640	12, 16, 20, 21			TO SOUTH INFIL SYS
23	Combine	8.361	2	724	28,626	4, 5, 10,			TO NORTH INFIL SYS
24	Reservoir	0.191	2	742	397	11, 15, 13	142.28	2,200	SOUTH POR PVMT
25	Reservoir	0.200	2	744	446	14	141.79	3,450	NORTH POR PVMT
26	Reservoir	7.056	2	730	19,539	22	144.94	9,955	SOUTH INFIL SYS
27	Reservoir	6.513	2	726	14,748	23	144.89	6,718	NORTH INFIL SYS
28	Combine	1.861	2	724	6,502	17, 18,			COMBINE-3
29	Combine	14.90	2	728	41,632	24, 25, 26,			SYSTEM OUTLET
30	Combine	17.35	2	728	60,103	27, 28 19, 29			TOTAL SITE
F0173-02 Hydrographs - Proposed.gpw					Return Period: 100 Year			Friday, 07 / 9 / 2021	

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#### Hyd. No. 1

CB-01

Hydrograph type = SCS Runoff Peak discharge = 0.514 cfsStorm frequency = 100 yrsTime to peak = 12.17 hrsTime interval = 2 min Hyd. volume = 2.101 cuftDrainage area Curve number = 0.108 ac= 76 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 14.20 min = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

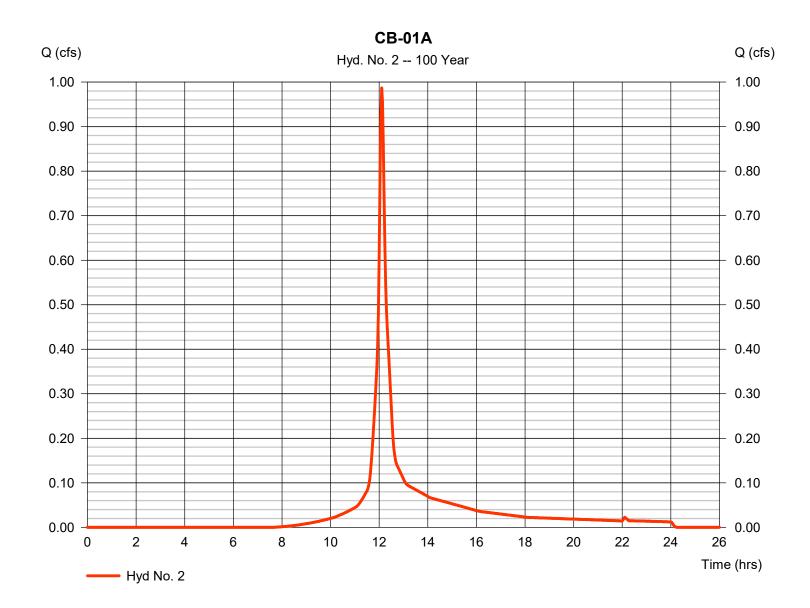


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#### Hyd. No. 2

**CB-01A** 

Hydrograph type = SCS Runoff Peak discharge = 0.987 cfsStorm frequency = 100 yrsTime to peak = 12.10 hrsTime interval = 2 min Hyd. volume = 3,369 cuftDrainage area Curve number = 0.194 ac= 70 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.80 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

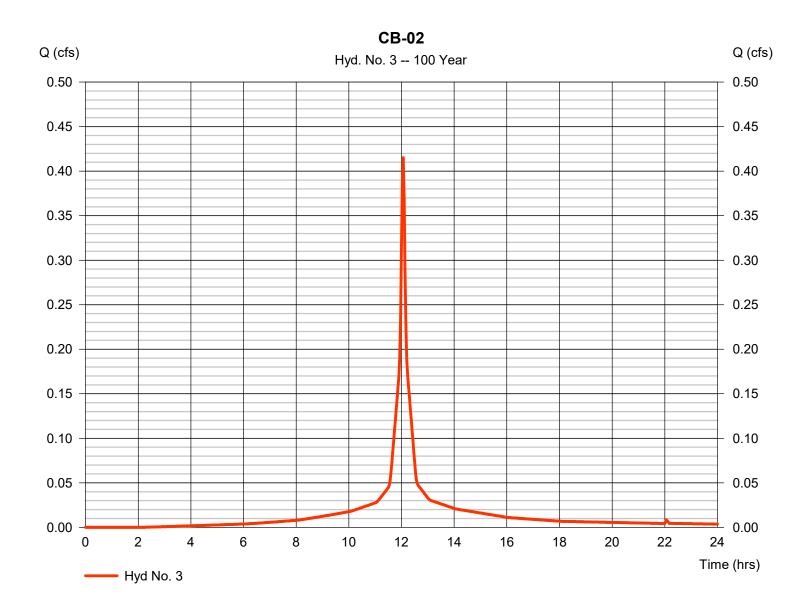


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#### Hyd. No. 3

**CB-02** 

Hydrograph type = SCS Runoff Peak discharge = 0.415 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,362 cuftDrainage area Curve number = 0.054 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

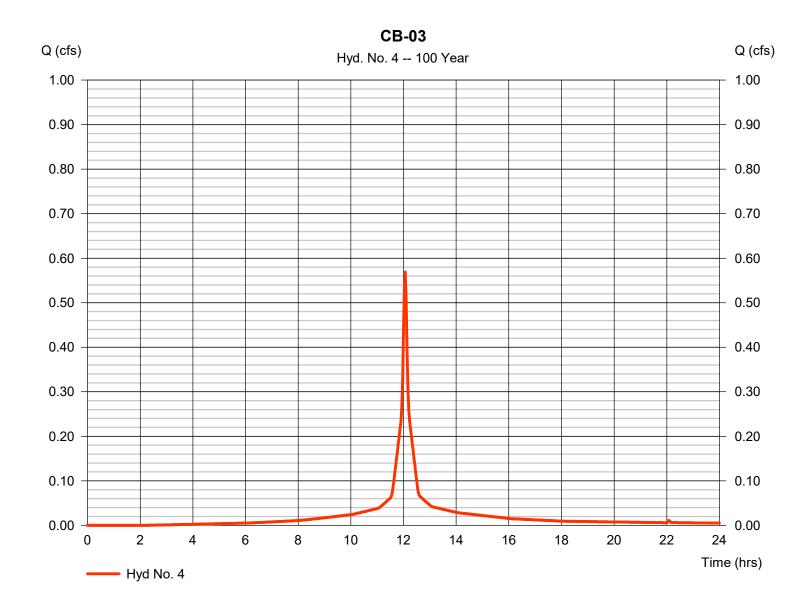


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#### Hyd. No. 4

**CB-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.569 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,866 cuft Drainage area Curve number = 0.074 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

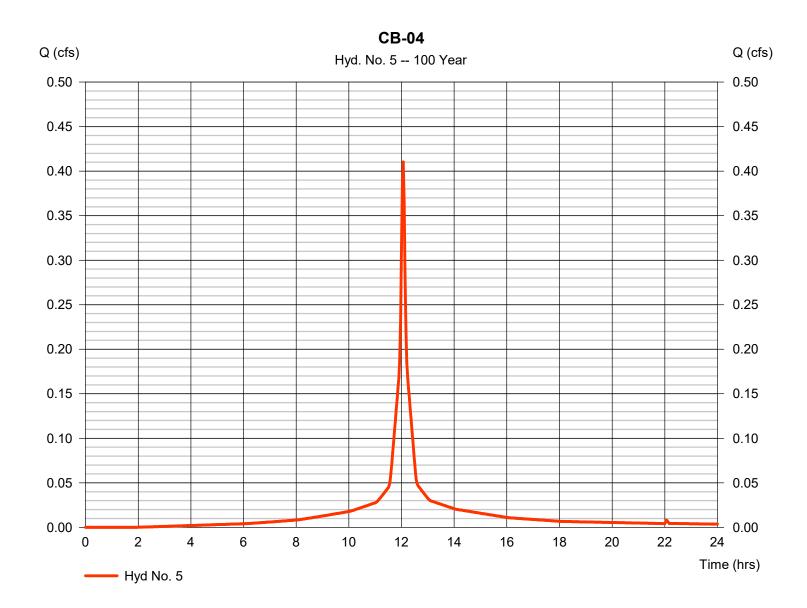


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#### Hyd. No. 5

**CB-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.410 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,358 cuft Drainage area Curve number = 0.053 ac= 93 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

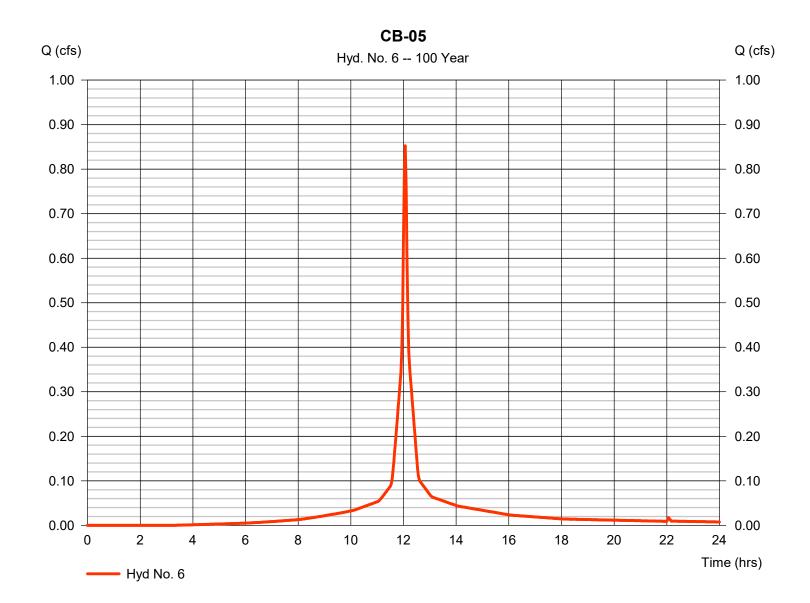


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#### Hyd. No. 6

**CB-05** 

Hydrograph type = SCS Runoff Peak discharge = 0.852 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,712 cuftDrainage area Curve number = 0.115 ac= 88 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



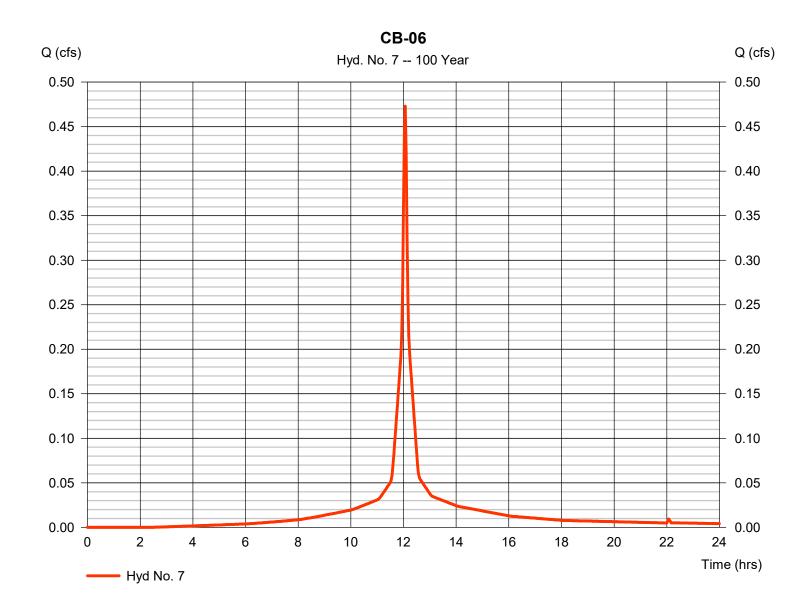
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#### Hyd. No. 7

**CB-06** 

Hydrograph type = SCS Runoff Peak discharge = 0.473 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 1,538 cuft Drainage area Curve number = 0.062 ac= 91 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

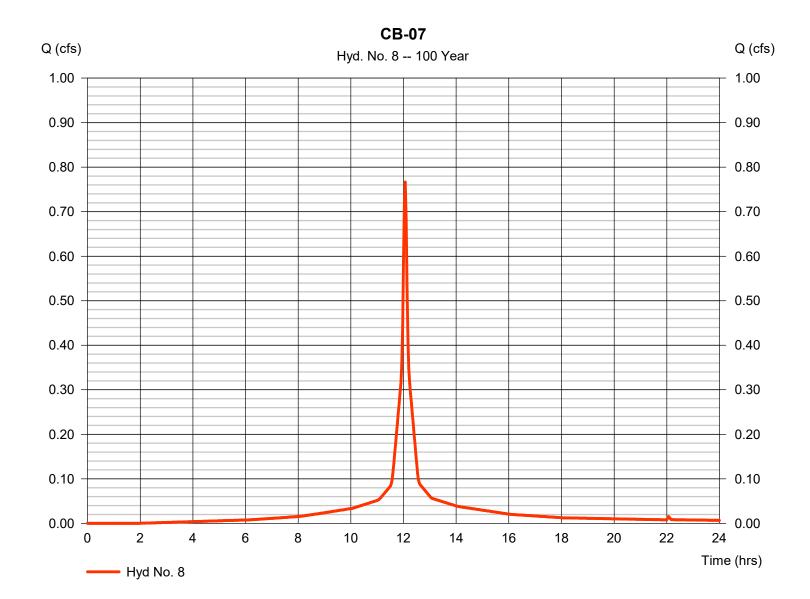


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#### Hyd. No. 8

**CB-07** 

Hydrograph type = SCS Runoff Peak discharge = 0.767 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,537 cuftDrainage area Curve number = 0.099 ac= 93 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

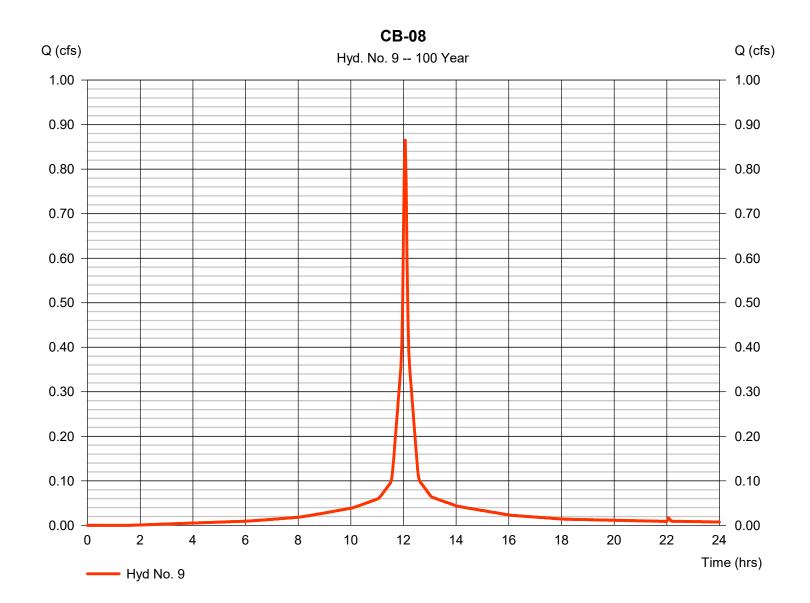


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#### Hyd. No. 9

**CB-08** 

Hydrograph type = SCS Runoff Peak discharge = 0.865 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 2,890 cuftDrainage area Curve number = 0.111 ac= 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.50 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



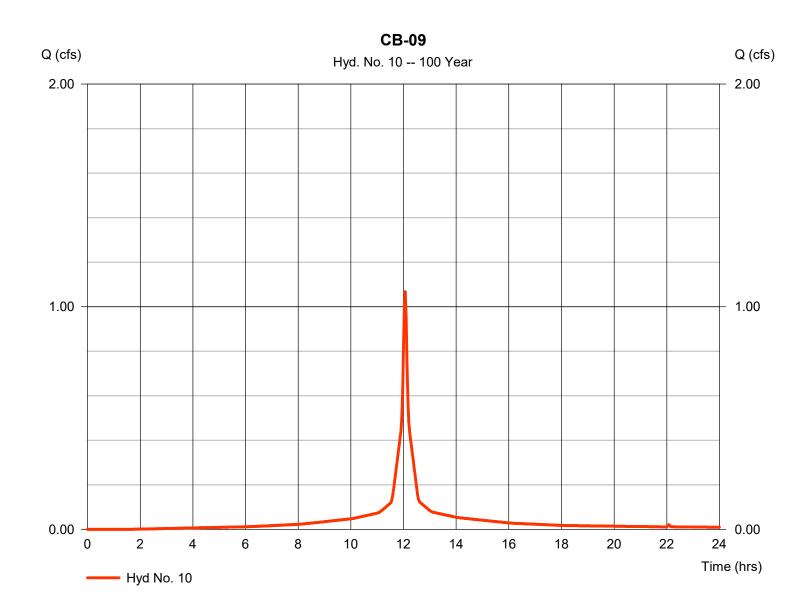
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### Hyd. No. 10

**CB-09** 

Hydrograph type = SCS Runoff Peak discharge = 1.068 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,567 cuftDrainage area Curve number = 0.137 ac= 94 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



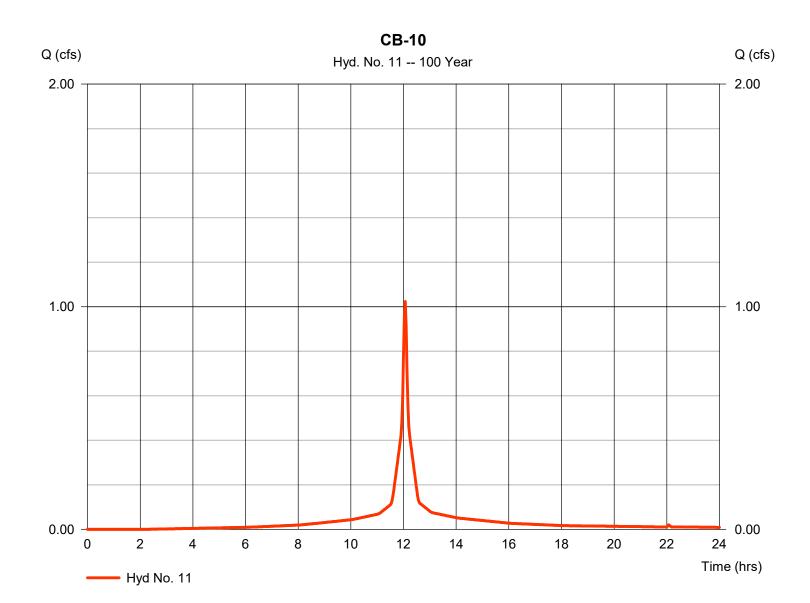
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### Hyd. No. 11

**CB-10** 

Hydrograph type = SCS Runoff Peak discharge = 1.023 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,354 cuftDrainage area Curve number = 0.133 ac= 92 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



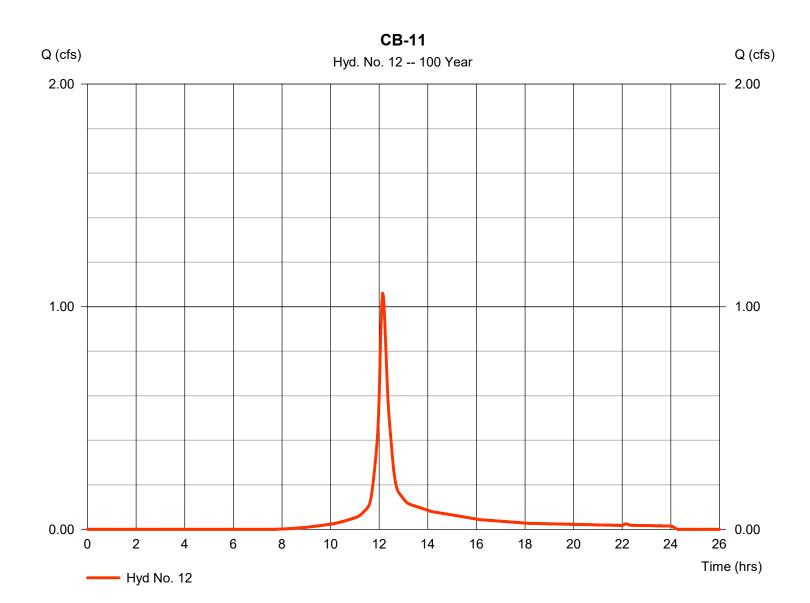
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#### Hyd. No. 12

**CB-11** 

Hydrograph type = SCS Runoff Peak discharge = 1.061 cfsStorm frequency = 100 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 4,065 cuftDrainage area = 0.227 acCurve number = 70 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 10.90 min = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



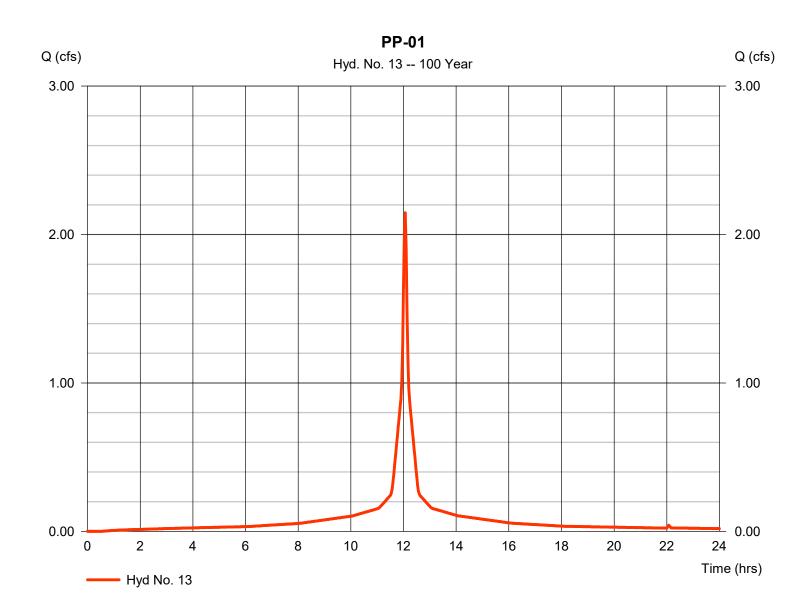
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#### Hyd. No. 13

PP-01

= 2.147 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 7,498 cuft Drainage area = 0.271 acCurve number = 98 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

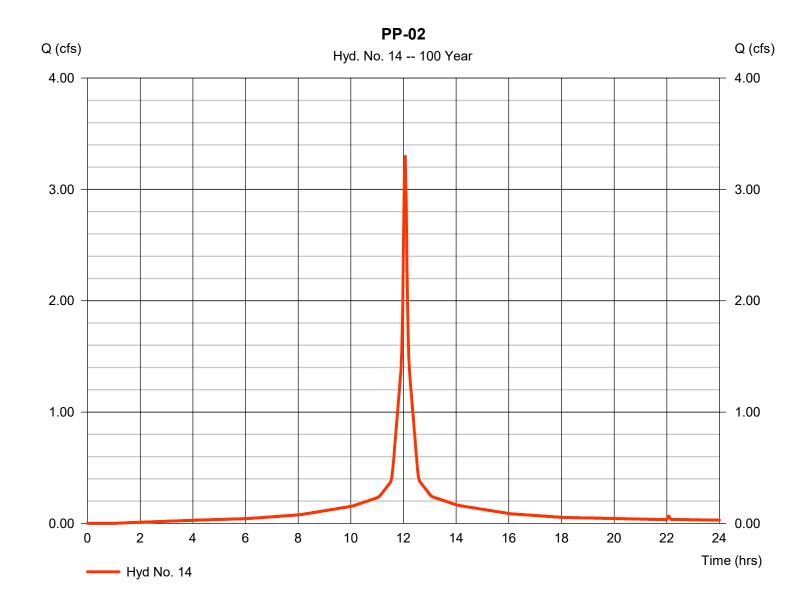


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#### Hyd. No. 14

PP-02

Hydrograph type = SCS Runoff Peak discharge = 3.298 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 11,250 cuft Drainage area Curve number = 0.419 ac= 96 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc)  $= 6.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

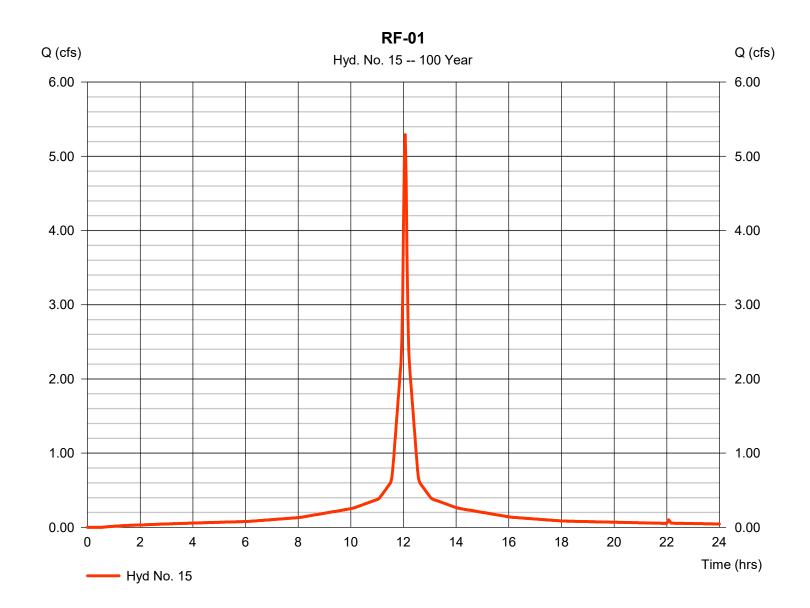


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#### **Hyd. No. 15**

**RF-01** 

Hydrograph type = SCS Runoff Peak discharge = 5.291 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 18,482 cuft Drainage area Curve number = 0.668 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

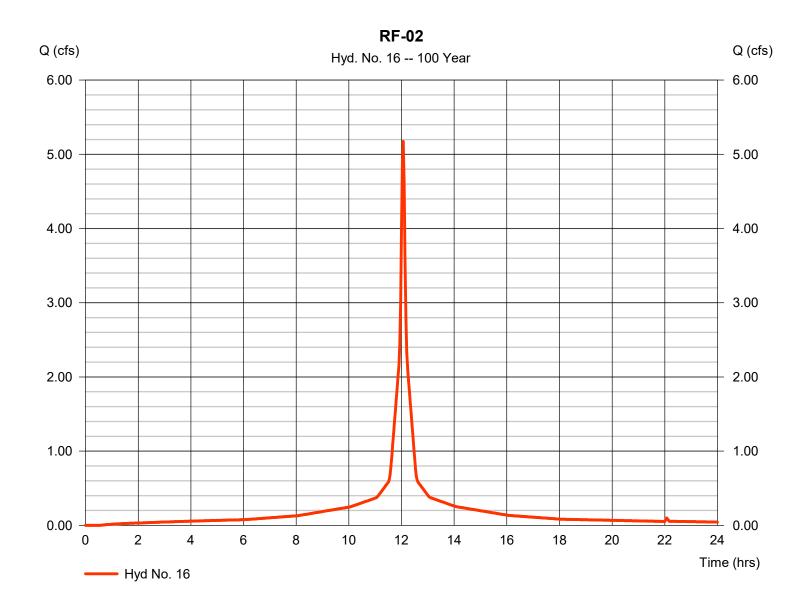


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#### Hyd. No. 16

**RF-02** 

Hydrograph type = SCS Runoff Peak discharge = 5.172 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 18,067 cuft Drainage area Curve number = 0.653 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

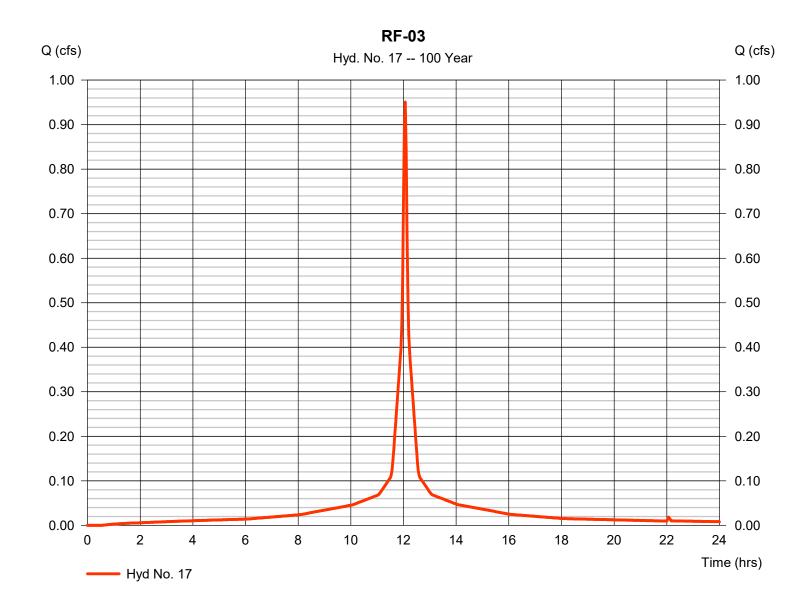


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#### Hyd. No. 17

**RF-03** 

Hydrograph type = SCS Runoff Peak discharge = 0.951 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,320 cuftDrainage area Curve number = 0.120 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

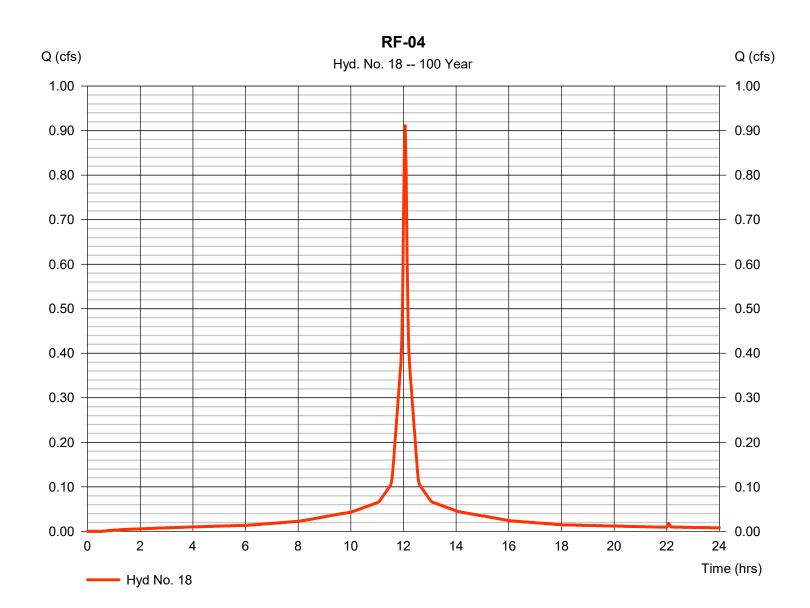


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#### Hyd. No. 18

**RF-04** 

Hydrograph type = SCS Runoff Peak discharge = 0.911 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,182 cuftDrainage area Curve number = 0.115 ac= 98 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

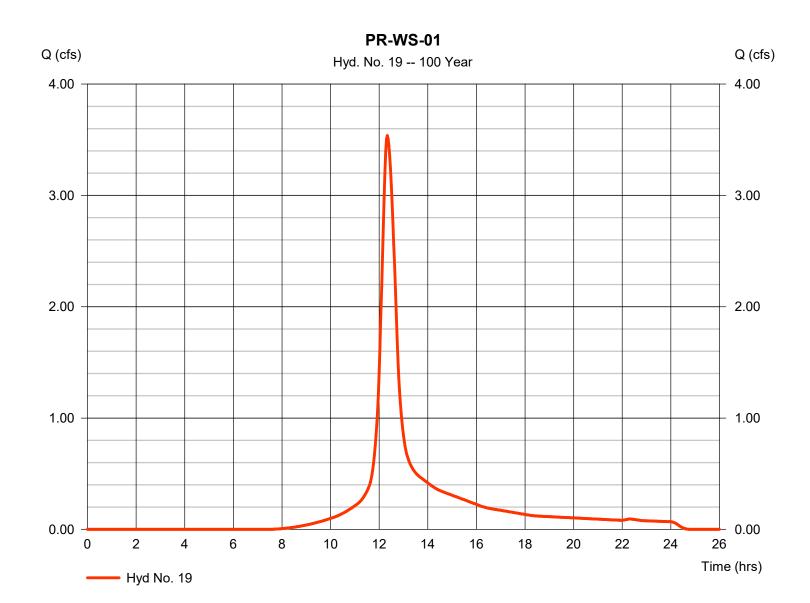


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#### Hyd. No. 19

PR-WS-01

Hydrograph type = SCS Runoff Peak discharge = 3.537 cfsStorm frequency = 100 yrsTime to peak  $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 18,471 cuft Drainage area Curve number = 1.038 ac= 71 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) = 27.60 min = User Total precip. = 8.37 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



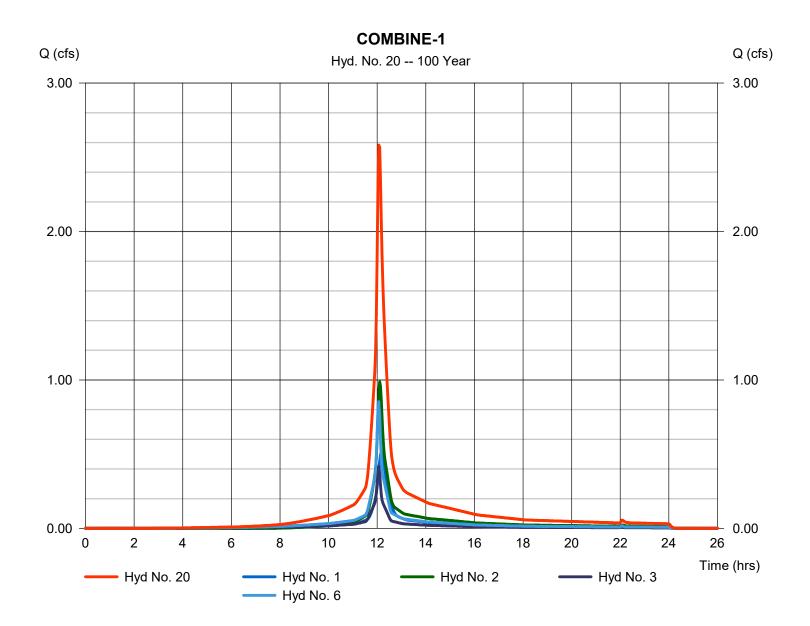
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#### Hyd. No. 20

**COMBINE-1** 

Hydrograph type = Combine Peak discharge = 2.583 cfsStorm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 9,543 cuft Inflow hyds. = 1, 2, 3, 6Contrib. drain. area = 0.471 ac

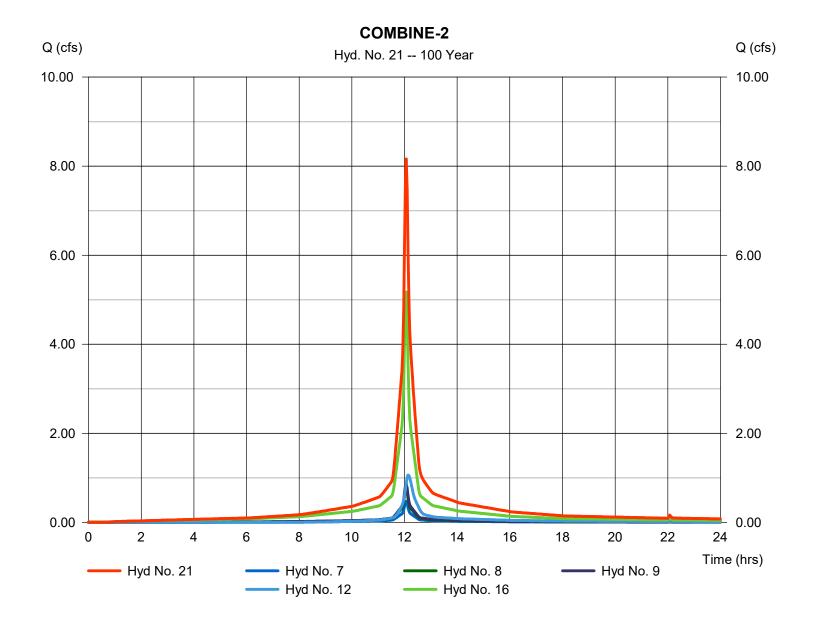


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#### Hyd. No. 21

**COMBINE-2** 

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min Inflow hyds. = 7, 8, 9, 12, 16 Peak discharge = 8.161 cfs
Time to peak = 12.07 hrs
Hyd. volume = 29,097 cuft
Contrib. drain. area = 1.152 ac

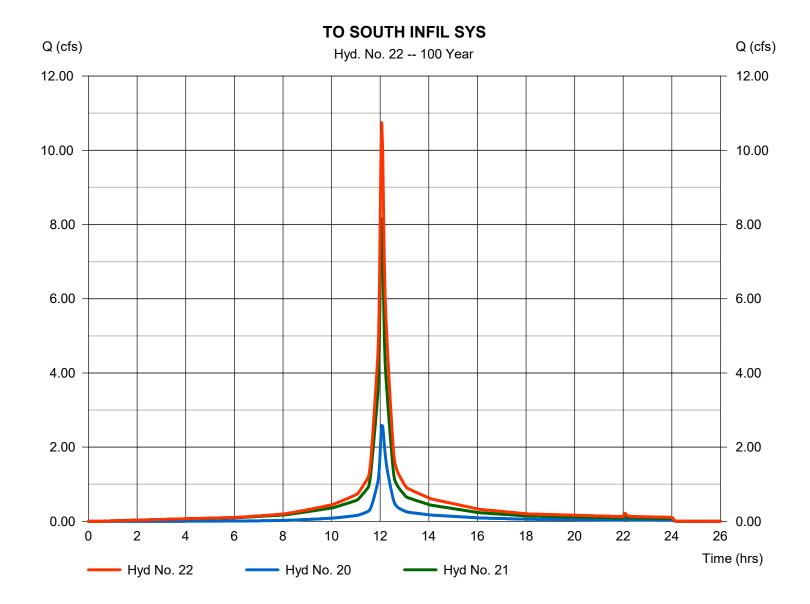


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#### Hyd. No. 22

TO SOUTH INFIL SYS

Hydrograph type = Combine Peak discharge = 10.74 cfsStorm frequency Time to peak = 100 yrs= 12.07 hrsTime interval = 2 min Hyd. volume = 38,640 cuftInflow hyds. = 20, 21 Contrib. drain. area = 0.000 ac



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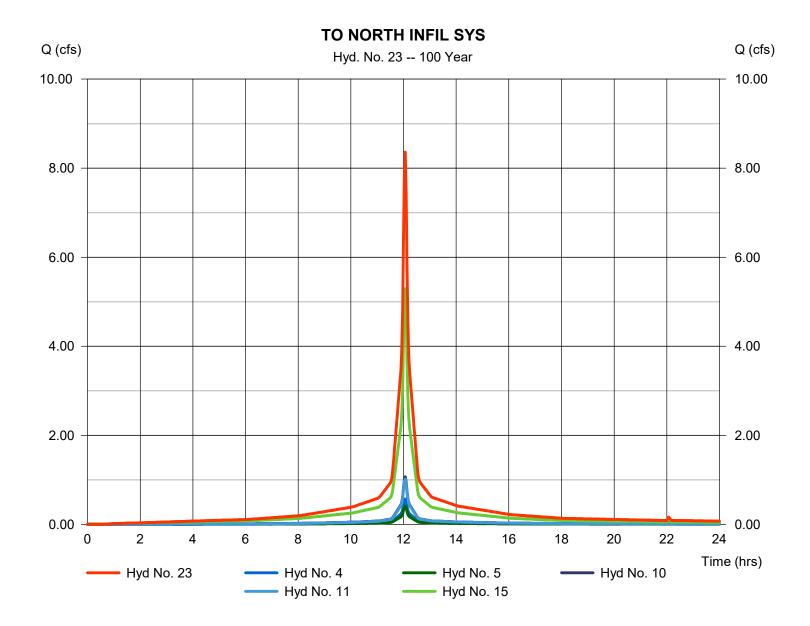
#### Hyd. No. 23

TO NORTH INFIL SYS

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 2 min

Inflow hyds. = 4, 5, 10, 11, 15

Peak discharge = 8.361 cfs
Time to peak = 12.07 hrs
Hyd. volume = 28,626 cuft
Contrib. drain. area = 1.065 ac



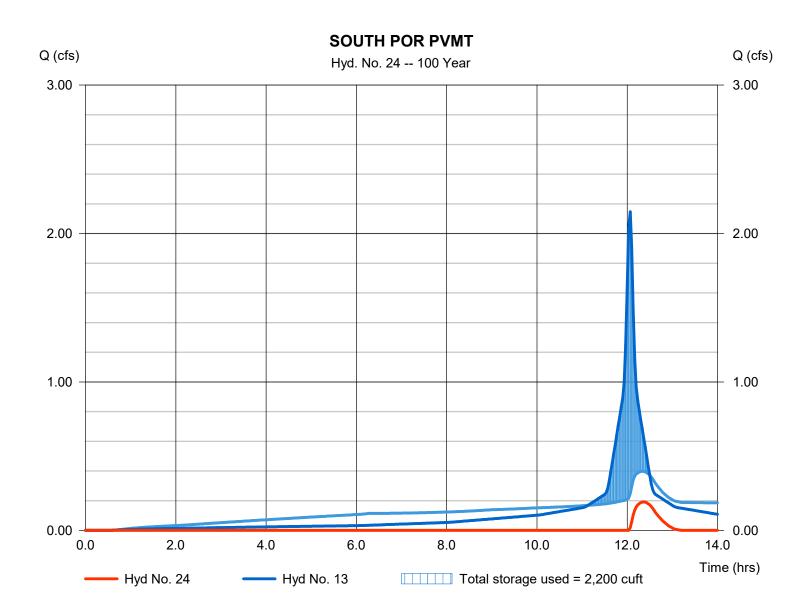
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#### Hyd. No. 24

#### **SOUTH POR PVMT**

= Reservoir Hydrograph type Peak discharge = 0.191 cfsStorm frequency = 100 yrsTime to peak  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 397 cuft Inflow hyd. No. Max. Elevation = 142.28 ft= 13 - PP-01 = SOUTH POROUS PVMT Reservoir name Max. Storage = 2,200 cuft



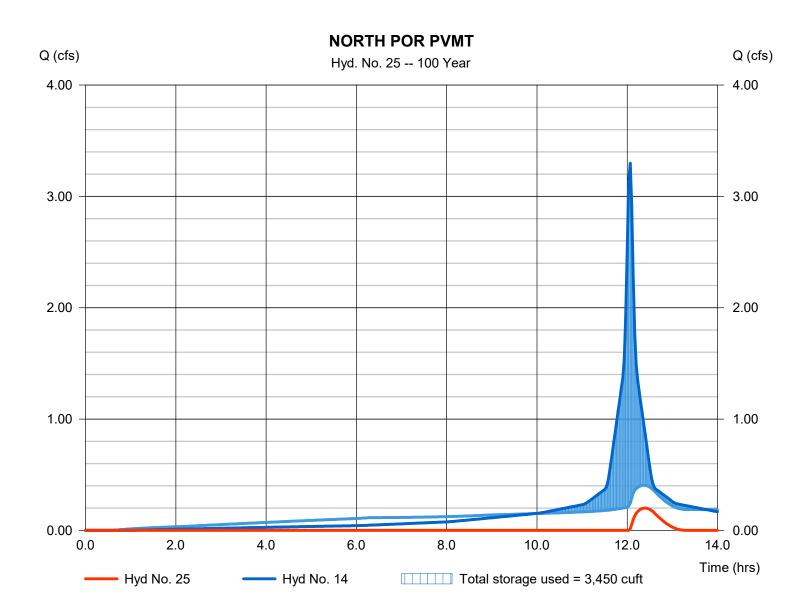
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#### Hyd. No. 25

#### NORTH POR PVMT

Hydrograph type Peak discharge = 0.200 cfs= Reservoir Storm frequency = 100 yrsTime to peak  $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 446 cuft Inflow hyd. No. Max. Elevation = 14 - PP-02 = 141.79 ftReservoir name = NORTH POROUS PVMT Max. Storage = 3,450 cuft



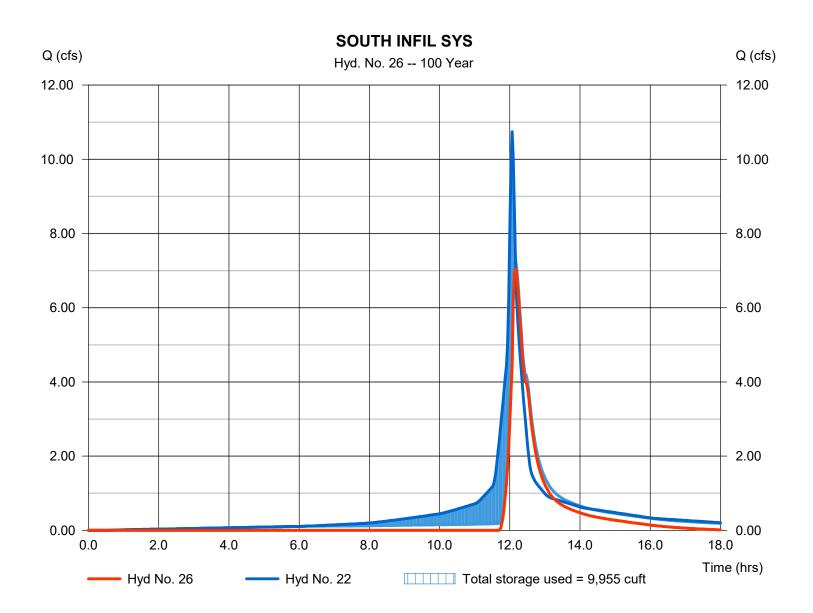
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

#### Hyd. No. 26

**SOUTH INFIL SYS** 

= Reservoir Hydrograph type Peak discharge = 7.056 cfsStorm frequency = 100 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 19,539 cuftInflow hyd. No. Max. Elevation = 22 - TO SOUTH INFIL SYS = 144.94 ft= SOUTH INFIL SYS Reservoir name Max. Storage = 9,955 cuft



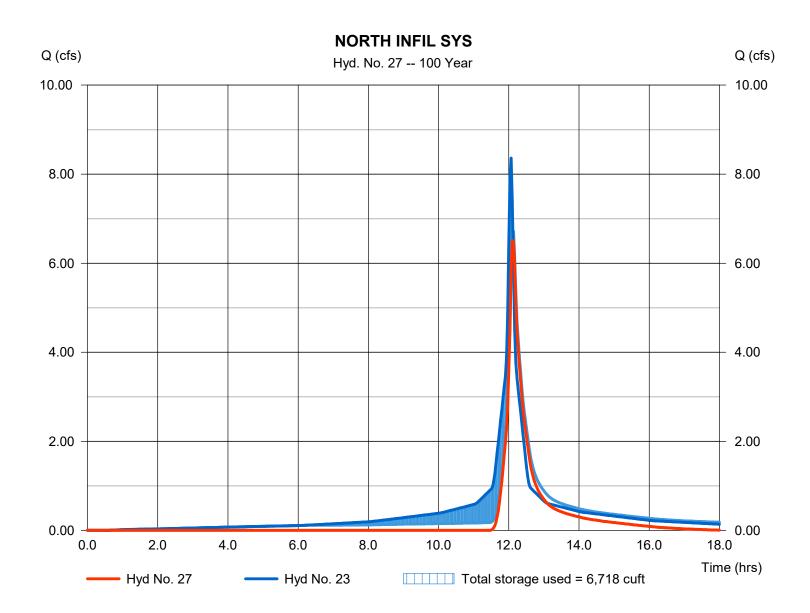
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

#### Hyd. No. 27

**NORTH INFIL SYS** 

= Reservoir Hydrograph type Peak discharge = 6.513 cfsStorm frequency = 100 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 14,748 cuft Inflow hyd. No. Max. Elevation = 144.89 ft= 23 - TO NORTH INFIL SYS = NORTH INFIL SYS Reservoir name Max. Storage = 6,718 cuft



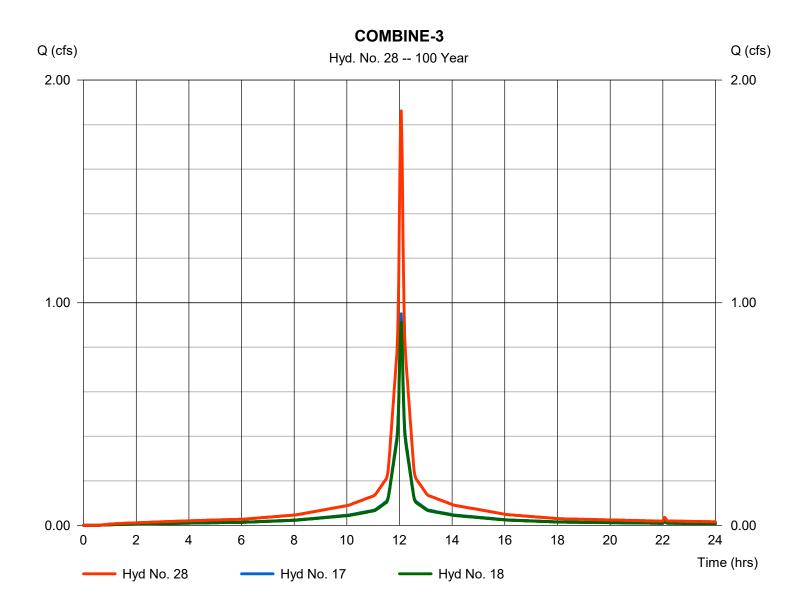
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Friday, 07 / 9 / 2021

#### Hyd. No. 28

**COMBINE-3** 

Hydrograph type = Combine Peak discharge = 1.861 cfsTime to peak Storm frequency = 100 yrs $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 6,502 cuft Inflow hyds. = 17, 18 Contrib. drain. area = 0.235 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

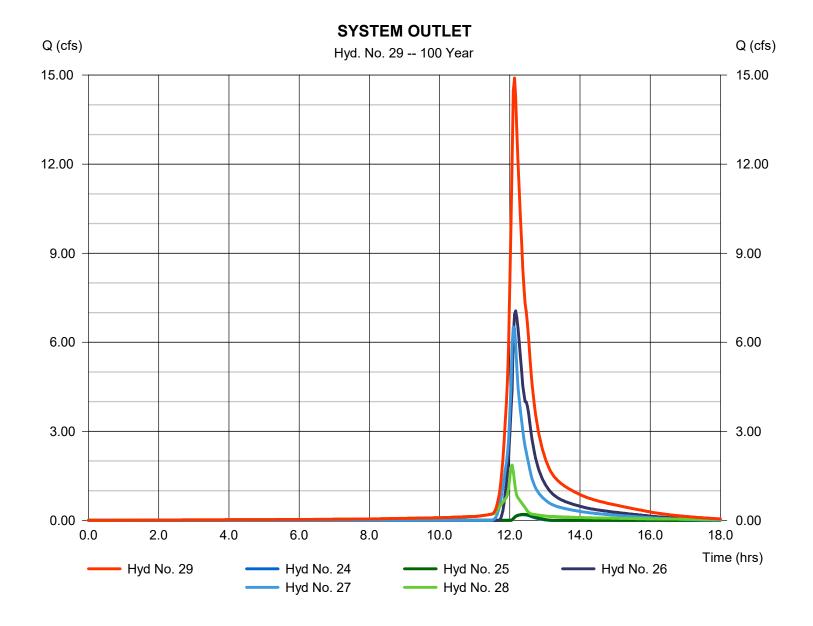
Friday, 07 / 9 / 2021

#### Hyd. No. 29

SYSTEM OUTLET

Hydrograph type = Combine Peak discharge = 14.90 cfsStorm frequency Time to peak = 100 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 41,632 cuft

Inflow hyds. Contrib. drain. area = 0.000 ac= 24, 25, 26, 27, 28



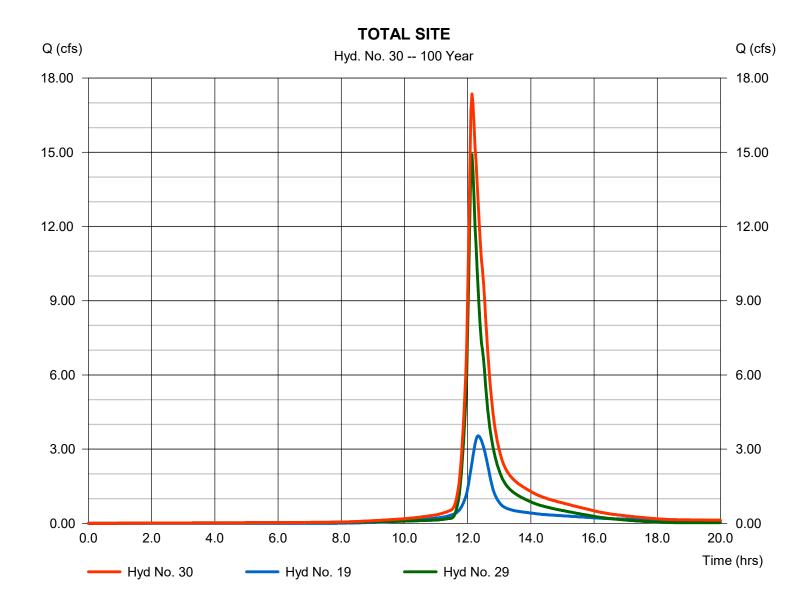
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

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#### Hyd. No. 30

**TOTAL SITE** 

Hydrograph type = Combine Peak discharge = 17.35 cfsStorm frequency Time to peak = 100 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 60,103 cuftInflow hyds. = 19, 29Contrib. drain. area = 1.038 ac



**APPENDIX E** 

Date: 07/09/21
Prepared By: TAS

141 Danbury Road Wilton, CT WQV Worksheet



#### **Required Water Quality Volume (WQV)**

#### 141 Danbury Road

Site Area in Acres, A	=	4.651	ac
Impervious Area in Acres	=	2.987	ac
Percent Impervious Cover, I	=	64.2	%
Volumetric Runoff Coefficient, R			
R = 0.05 + 0.009(I)	=	0.628	

#### Water Quality Volume (WQV)

$$WQV = \frac{(1'')(R)(A)}{12}$$
 = 0.243 ac·ft = 10,603 cf

#### **Provided Water Quality Volume**

	=	10,802	cf
South Porous Pavement System	=	1,415	cf
North Porous Pavement System	=	2,191	cf
South Infiltration System	=	4,284	cf
North Infiltration System	=	2,912	cf

Date: **07/09/2021**Prepared By: **TAS** 

141 Danbury Road Wilton, CT WQF Worksheet



#### **Required Water Quality Flow (WQF)**

Water Quality Volume, WQV = 0.243 ac·ft Drainage Area, A = 4.651 ac

Runoff Depth in Watershed inches, Q

$$Q = \frac{WQV \times 12}{A} = 0.628$$
 in

Design Precipitation in inches, P = 1 in

Runoff Curve Number, CN

$$CN = \frac{1000}{[10 + 5P + 10Q - 10(Q^2 + 1.25QP)^{\frac{1}{2}}]} = 96$$

From Table 4-1 in Chapter 4 of TR-55

Initial Abstraction,  $I_a$  = 0.083 in  $I_a / P$  = 0.083

u .

From Exhibit 4-III in Chapter 4 of TR-55  $q_u =$  Unit Peak Discharge = 650 csm/in

Water Quality Flow (WQF)

 $WQF = (q_u)(A)(Q)$  = 2.97 cfs



Project Name: **141 Danbury Road** Project Number: **F0173-002** 

Project Location: Wilton, CT

Description: Stormwater BMP Pollutant Removal Estimate

Prepared By: **TAS** Date: **July 9, 2021** 

#### Water Quality Area 1

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.067	0.013	3.550	0.005	0.001	0.005
Proposed, Post Treatment	lb/yr/1-in	0.040	0.003	0.359	0.002	0.000	0.000
Reduction, Pre to Post Treat		40%	78%	90%	64%	70%	90%

#### **Water Quality Area 2**

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.183	0.037	9.715	0.014	0.003	0.013
Proposed, Post Treatment	lb/yr/1-in	0.109	0.008	0.983	0.005	0.001	0.001
Reduction, Pre to Post Treat		40%	78%	90%	64%	70%	90%

#### **Water Quality Area 3**

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.043	0.009	2.293	0.003	0.001	0.003
Proposed, Post Treatment	lb/yr/1-in	0.031	0.006	1.261	0.002	0.001	0.002
Reduction, Pre to Post Treat		27%	33%	45%	32%	32%	32%

#### **Water Quality Area 4**

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.042	0.008	2.240	0.003	0.001	0.003
Proposed, Post Treatment	lb/yr/1-in	0.031	0.006	1.232	0.002	0.000	0.002
Reduction, Pre to Post Treat		27%	33%	45%	32%	32%	32%

#### **Water Quality Area 5**

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.080	0.016	4.261	0.006	0.001	0.006
Proposed, Post Treatment	lb/yr/1-in	0.048	0.010	0.852	0.002	0.001	0.002
Reduction, Pre to Post Treat		40%	40%	80%	60%	60%	60%

#### **Water Quality Area 6**

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Proposed, Post Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Reduction, Pre to Post Treat							

#### **Water Quality Area 7**

		Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Proposed, Post Treatment	lb/yr/1-in	0.000	0.000	0.000	0.000	0.000	0.000
Reduction, Pre to Post Treat							

#### **Water Quality Area 8**

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.041	0.008	2.165	0.003	0.001	0.003
Proposed, Post Treatment	lb/yr/1-in	0.024	0.005	0.433	0.001	0.000	0.001
Reduction, Pre to Post Treat		40%	40%	80%	60%	60%	60%

#### **Total Site**

		Pollutant					
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr/1-in	0.456	0.092	24.226	0.035	0.008	0.032
Proposed, Post Treatment	lb/yr/1-in	0.284	0.037	5.121	0.015	0.003	0.009
Reduction, Pre to Post Treat		38%	59%	79%	57%	60%	71%

#### **Loading Calculation**

Location: Area 1 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.32 Total Area = 0.396 acres

Pollutant	<u>Reside</u>	<u>ential</u>	<u>Weig</u>	<u>ihted</u>			
	Α	EMC	EMC	L			
	(acres)	(mg/L)	(mg/L)	(lbs/yr)			
Total Nitrogen (N)	0.396	1.900	1.900	0.067			
Total Phosphorus (P)	0.396	0.383	0.383	0.013			
Total Suspended Solids	0.396	101.0	101.0	3.6			
Lead	0.396	0.144	0.144	0.005			
Copper	0.396	0.033	0.033	0.001			
Zinc	0.396	0.135	0.135	0.005			
L EMC	L = 0.2266 * EMC * [0.15 + 0.75*I] * P *A  Pollution Loading (lbs/year)						
I EMC		nt Mean Concentration (mg/L) f Impervious Acres (acres)					
P	Annual Ra						
A		d Area (acres)					

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 1 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.32 Total Area = 0.396 acres

BMP: **Deep Sump Catch Basins** 

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)		
Total Nitrogen (N)	0.067	0.067	0	0.00	0.067		
Total Phosphorus (P)	0.013	0.013	0	0.00	0.013		
Total Suspended Solids	3.550	3.6	20	0.71	2.8		
Lead	0.005	0.005	0	0.00	0.005		
Copper	0.001	0.001	0	0.00	0.001		
Zinc	0.005	0.005	0	0.00	0.005		
Lin 1	Pollutant Load Ar	Pollutant Load Area 1					
Sum L RR	Sum of Pollutant Removal rate in		BMP				
Lout	Pollutant Load ou						

#### Notes

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location: Area 1 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.32 Total Area = 0.396 acres

BMP: Water Quality Structure

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)		
Total Nitrogen (N)	0.067	0.067	18.3	0.01	0.055		
Total Phosphorus (P)	0.013	0.013	66.9	0.01	0.004		
Total Suspended Solids	2.840	2.8	77	2.19	0.7		
Lead	0.005	0.005	46.5	0.00	0.003		
Copper	0.001	0.001	56.2	0.00	0.001		
Zinc	0.005	0.005	85.3	0.00	0.001		
Lin 1	Pollutant Load Out of Deep Sump Catch Basins BMP						
Sum L RR		Sum of Pollutant Load to this BMP Removal rate in percentage					
Lout	Pollutant Load out	_					

#### Notes

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location: Area 1 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.32 Total Area = 0.396 acres

BMP: Infiltration System

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout	
	(lbs)	(lbs)	(-)	(lbs)	(lbs)	
Total Nitrogen (N)	0.055	0.055	27	0.01	0.040	
Total Phosphorus (P)	0.004	0.004	33	0.00	0.003	
Total Suspended Solids	0.653	0.7	45	0.29	0.359	
Lead	0.003	0.003	32	0.00	0.002	
Copper	0.001	0.001	32	0.00	0.000	
Zinc	0.001	0.001	32	0.00	0.000	
Lin 1	Pollutant Load o	ut from WQS				
Sum L		Sum of Pollutant Load to this BMP				
RR	Removal rate in	percentage				
Lout	Pollutant Load o	ut of BMP				

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location: Area 2 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.38 Total Area = 0.969 acres

Pollutant	Reside	<u>ential</u>	<u>Weig</u>	<u>ghted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.969	1.900	1.900	0.183
Total Phosphorus (P)	0.969	0.383	0.383	0.037
Total Suspended Solids	0.969	101.0	101.0	9.7
Lead	0.969	0.144	0.144	0.014
Copper	0.969	0.033	0.033	0.003
Zinc	0.969	0.135	0.135	0.013
L EMC I P A	Pollution L Mean Ever Fraction of Annual Ra	6 * EMC * [0.15 + 0.75*I] * P *A  oading (lbs/year)  nt Mean Concentration (mg/L)  f Impervious Acres (acres)  infall (in) d Area (acres)		

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 2 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.38 Total Area = 0.969 acres

BMP: **Deep Sump Catch Basins** 

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (lbs)	Lout (lbs)		
Total Nitrogen (N)	0.183	0.183	0	0.00	0.183		
Total Phosphorus (P)	0.037	0.037	0	0.00	0.037		
Total Suspended Solids	9.715	9.7	20	1.94	7.8		
Lead	0.014	0.014	0	0.00	0.014		
Copper	0.003	0.003	0	0.00	0.003		
Zinc	0.013	0.013	0	0.00	0.013		
Lin 1	Pollutant Load Are	Pollutant Load Area 1					
Sum L RR	Sum of Pollutant I Removal rate in p		BMP				
Lout	Pollutant Load out	-					

#### Notes

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location: Area 2 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.38 Total Area = 0.969 acres

BMP: Water Quality Structure

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout
	(lbs)	(lbs)	(%)	(lbs)	(lbs)
Total Nitrogen (N)	0.183	0.183	18.3	0.03	0.149
Total Phosphorus (P)	0.037	0.037	66.9	0.02	0.012
Total Suspended Solids	7.772	7.8	77	5.98	1.8
Lead	0.014	0.014	46.5	0.01	0.007
Copper	0.003	0.003	56.2	0.00	0.001
Zinc	0.013	0.013	85.3	0.01	0.002
Lin 1	Pollutant Load Out	of Deep S	ump Cat	ch Basins E	ЗМР
Sum L	Sum of Pollutant Lo				
RR	Removal rate in pe	rcentage			
Lout	Pollutant Load out	of BMP			

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

Location: Area 2 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.38 Total Area = 0.969 acres

BMP: Infiltration System

Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)	
T						
Total Nitrogen (N)	0.149	0.149	27	0.04	0.109	
Total Phosphorus (P)	0.012	0.012	33	0.00	0.008	
Total Suspended Solids	1.788	1.8	45	0.80	1.0	
Lead	0.007	0.007	32	0.00	0.005	
Copper	0.001	0.001	32	0.00	0.001	
Zinc	0.002	0.002	32	0.00	0.001	
Lin 1	Pollutant Load out	-				
Sum L		Sum of Pollutant Load to this BMP				
RR	Removal rate in p	_				
Lout	Pollutant Load out	t of BMP				

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location: Area 3 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.00 Total Area = 0.668 acres

Pollutant	Reside	<u>ential</u>	<u>Weig</u>	<u>ıhted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.668	1.900	1.900	0.043
Total Phosphorus (P)	0.668	0.383	0.383	0.009
Total Suspended Solids	0.668	101.0	101.0	2.3
Lead	0.668	0.144	0.144	0.003
Copper	0.668	0.033	0.033	0.001
Zinc	0.668	0.135	0.135	0.003
		6 * EMC * [0.15 + 0.75*I] * P *A		
L		oading (lbs/year)		
EMC		nt Mean Concentration (mg/L)		
I		f Impervious Acres (acres)		
P	Annual Ra	· ·		
A	watersne	d Area (acres)		

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 3 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.00 Total Area = 0.668 acres

BMP: Infiltration System

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)
Total Nitrogen (N)	0.043	0.043	27	0.01	0.031
Total Phosphorus (P)	0.009	0.009	33	0.00	0.006
Total Suspended Solids	2.293	2.3	45	1.03	1.3
Lead	0.003	0.003	32	0.00	0.002
Copper	0.001	0.001	32	0.00	0.001
Zinc	0.003	0.003	32	0.00	0.002
Lin 1 Sum L RR Lout	Pollutant Load out from WQS Sum of Pollutant Load to this BMP Removal rate in percentage Pollutant Load out of BMP				

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location: Area 4 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.00 Total Area = 0.653 acres

Pollutant	Reside	<u>ential</u>	<u>Weig</u>	<u>lhted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.653	1.900	1.900	0.042
Total Phosphorus (P)	0.653	0.383	0.383	0.008
Total Suspended Solids	0.653	101.0	101.0	2.2
Lead	0.653	0.144	0.144	0.003
Copper	0.653	0.033	0.033	0.001
Zinc	0.653	0.135	0.135	0.003
L EMC I P A	Pollution L Mean Ever Fraction of Annual Ra	6 * EMC * [0.15 + 0.75*I] * P *A  oading (lbs/year)  nt Mean Concentration (mg/L)  f Impervious Acres (acres)  infall (in) d Area (acres)		

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 4 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.00 Total Area = 0.653 acres

BMP: Infiltration System

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout
	(lbs)	(lbs)	(-)	(lbs)	(lbs)
Total Nitrogen (N)	0.042	0.042	27	0.01	0.031
Total Phosphorus (P)	0.008	0.008	33	0.00	0.006
Total Suspended Solids	2.240	2.2	45	1.01	1.2
Lead	0.003	0.003	32	0.00	0.002
Copper	0.001	0.001	32	0.00	0.000
Zinc	0.003	0.003	32	0.00	0.002
Lin 1	Pollutant Load out	from WQS			
Sum L	Sum of Pollutant Load to this BMP				
RR	Removal rate in p	ercentage			
Lout	Pollutant Load out	of BMP			

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location: Area 5 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.39 Total Area = 0.419 acres

Pollutant	Reside	<u>ential</u>		<u>Weig</u>	<u>ıhted</u>
	Α	EMC		EMC	L
	(acres)	(mg/L)		(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.419	1.900		1.900	0.080
Total Phosphorus (P)	0.419	0.383		0.383	0.016
Total Suspended Solids	0.419	101.0		101.0	4.3
Lead	0.419	0.144		0.144	0.006
Copper	0.419	0.033		0.033	0.001
Zinc	0.419	0.135		0.135	0.006
			* [0.15 + 0.75*I] * P *A		
L	Pollution L				
			·		
		•			
•					
L EMC I P A	L = 0.226  Pollution L  Mean Eve	6 * EMC Loading ( nt Mean ( f Imperv infall (in)	lbs/year) Concentration (mg/L) ious Acres (acres) )	0.133	

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 5 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.39 Total Area = 0.419 acres

BMP: **Porous Pavement** 

Pollutant	Lin 1 (lbs)	Sum L (lbs)	RR (-)	Lremoved (lbs)	Lout (lbs)	
	(183)	(103)	( )	(103)	(103)	
Total Nitrogen (N)	0.080	0.080	40	0.03	0.048	
Total Phosphorus (P)	0.016	0.016	40	0.01	0.010	
Total Suspended Solids	4.261	4.3	80	3.41	0.9	
Lead	0.006	0.006	60	0.00	0.002	
Copper	0.001	0.001	60	0.00	0.001	
Zinc	0.006	0.006	60	0.00	0.002	
Lin 1	Pollutant Load out from WQS					
Sum L	Sum of Pollutant Load to this BMP					
RR	Removal rate in percentage					
Lout	Pollutant Load	out of BMP				

#### Notes

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

#### **Loading Calculation**

Location: Area 8 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.27 Total Area = 0.271 acres

Pollutant	Reside	<u>ential</u>	<u>Weig</u>	<u>ihted</u>
	Α	EMC	EMC	L
	(acres)	(mg/L)	(mg/L)	(lbs/yr)
Total Nitrogen (N)	0.271	1.900	1.900	0.041
Total Phosphorus (P)	0.271	0.383	0.383	0.008
Total Suspended Solids	0.271	101.0	101.0	2.2
Lead	0.271	0.144	0.144	0.003
Copper	0.271	0.033	0.033	0.001
Zinc	0.271	0.135	0.135	0.003
L	Pollution L	6 * EMC * [0.15 + 0.75*I] * P *A .oading (lbs/year)		
EMC		nt Mean Concentration (mg/L)		
I		f Impervious Acres (acres)		
P	Annual Ra			
A	watersne	d Area (acres)		

#### Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition* by Debo & Reese, pgs. 193-195

Location: Area 8 Condition: Proposed

Rainfall: 1 inches

Impervious Fraction: 0.27 Total Area = 0.271 acres

BMP: **Porous Pavement** 

Pollutant	Lin 1	Sum L	RR	Lremoved	Lout		
	(lbs)	(lbs)	(-)	(lbs)	(lbs)		
Total Nitrogen (N)	0.041	0.041	40	0.02	0.024		
Total Phosphorus (P)	0.008	0.008	40	0.00	0.005		
Total Suspended Solids	2.165	2.2	80	1.73	0.4		
Lead	0.003	0.003	60	0.00	0.001		
Copper	0.001	0.001	60	0.00	0.000		
Zinc	0.003	0.003	60	0.00	0.001		
Lin 1	Pollutant Load out from WQS						
Sum L	Sum of Pollutant Load to this BMP						
RR	Removal rate in p	Removal rate in percentage					
Lout	Pollutant Load ou	t of BMP					

#### Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project #99-07*, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report:* Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests, Submitted by Stan Galicki, Ph.D., Millsaps College December 9th, 2009.

**APPENDIX F** 

#### 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: CB-01

**Location:** Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.025	0.95	0.024
Landscaped and Lawns	0.082	0.30	0.025
			0.049

Total Area: 0.108 C: 0.45

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	130	0.030	14.2

Total Tc (min) = 14.2

Name: CB-01A

**Location:** Proposed Yard Drain - Front Lawn

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.008	0.95	0.008
Landscaped and Lawns	0.186	0.30	0.056
			0.063

Total Area: 0.194 C: 0.33

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	50	0.020	7.8

Total Tc (min) = 7.8

#### 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: CB-02

Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.043	0.95	0.041
Landscaped and Lawns	0.010	0.30	0.003
			0.044

Total Area: 0.054 C: 0.82

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	98	0.050	1.0

Total Tc (min) = 1.0

Minimum Tc = 5.0

Name: CB-03

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.057	0.95	0.054
Landscaped and Lawns	0.016	0.30	0.005
			0.059

Total Area: 0.074 C: 0.80

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	60	0.033	0.8

Total Tc (min) = 4.5
Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: CB-04

Location: Proposed Catch Basin - Parking Area East

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.044	0.95	0.042
Landscaped and Lawns	0.009	0.30	0.003
			0.044

Total Area: 0.053 C: 0.84

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	55	0.045	0.7

Total Tc (min) = 4.4
Minimum Tc = 5.0

Name: CB-05

Location: Proposed Catch Basin - Driveway

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.076	0.95	0.072
Landscaped and Lawns	0.039	0.30	0.012
			0.084

Total Area: 0.115 C: 0.73

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	65	0.040	0.8

Total Tc (min) = 4.5

Minimum Tc = 5.0

# 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: CB-06

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.047	0.95	0.045
Landscaped and Lawns	0.015	0.30	0.004
			0.049

Total Area: 0.062 C: 0.80

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (m					
A-B	0.24	3.54	22	0.020	4.0
B-C	0.015	3.54	58	0.025	0.9

Total Tc (min) = 4.9
Minimum Tc = 5.0

Name: CB-07

**Location:** Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.081	0.95	0.077
Landscaped and Lawns	0.018	0.30	0.005
			0.082

Total Area: 0.099 C: 0.83

#### **Time of Concentration:**

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (mi					
A-B	0.24	3.54	15	0.020	3.0
B-C	0.015	3.54	115	0.035	1.3

Total Tc (min) = 4.3

Minimum Tc = 5.0

#### 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: CB-08

Location: Proposed Catch Basin - Parking Area South

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.094	0.95	0.090
Landscaped and Lawns	0.017	0.30	0.005
			0.095

Total Area: 0.111 C: 0.85

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (m					Time (min)
A-B	0.24	3.54	30	0.040	3.9
B-C	0.015	3.54	140	0.035	1.5

Total Tc (min) = 5.5

Name: CB-09

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.117	0.95	0.111
Landscaped and Lawns	0.020	0.30	0.006
			0.117

Total Area: 0.137 C: 0.86

#### Time of Concentration:

Sheet-Flow Travel Time					
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (m					Time (min)
A-B	0.24	3.54	20	0.020	3.7
B-C	0.015	3.54	120	1.000	0.4

Total Tc (min) = 4.1

Minimum Tc = 5.0

Project No. **F0173-002** Date: 07/09/21

**141 Danbury Road** Wilton, CT Prepared By: TAS **Proposed C & Tc Worksheet** 



**CB-10** Name:

Location: Proposed Catch Basin - Parking Area North

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.104	0.95	0.098
Landscaped and Lawns	0.029	0.30	0.009
			0.107

0.81 Total Area: 0.133

#### **Time of Concentration:**

		Shee	et-Flow Travel Time					
Segment ID	Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) 1							
A-B	0.24	3.54	30	0.040	Time (min) 3.9			
B-C	0.015	3.54	135	1.000	0.4			

Total Tc (min) = 4.3 Minimum Tc =

Name: **CB-11** 

Location: Proposed Yard Drain - Southeast Corner Site

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.010	0.95	0.010
Landscaped and Lawns	0.217	0.30	0.065
			0.075

Total Area: 0.227 0.33

#### **Time of Concentration:**

	Sheet-Flow Travel Time									
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)					
A-B	0.24	3.54	120	0.050	10.9					

Total Tc (min) = 10.9

#### 141 Danbury Road Wilton, CT Proposed C & Tc Worksheet



Name: RF-01

Location: Proposed Building - North

Cover Type	Area (ac)	C	AxC
Pavement / Impervious	0.668	0.95	0.635
Landscaped and Lawns	0.000	0.30	0.000
			0.635

Total Area: 0.668 C: 0.95

#### **Time of Concentration:**

		Shee	et-Flow Travel Time								
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)											
A-B	0.015	3.54	50	0.015	1.0						

Total Tc (min) = 1.0

Minimum Tc = 5.0

Name: RF-02

Location: Proposed Building - South

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.653	0.95	0.620
Landscaped and Lawns	0.000	0.30	0.000
			0.620

Total Area: 0.653 C: 0.95

#### Time of Concentration:

Sheet-Flow Travel Time										
Sheet-Flow Travel Time           Segment ID         "n"         P2 (in)         Flow Length (ft)         Slope (ft/ft)         Time (min)           A-B         0.015         3.54         50         0.015         1.0										
A-B	0.015	3.54	50	0.015	1.0					

Total Tc (min) = 1.0

Minimum Tc = 5.0

Project No. **F0173-002** Date: 07/09/21

**141 Danbury Road** Wilton, CT Prepared By: TAS **Proposed C & Tc Worksheet** 



RF-03 Name:

Location: Proposed Building - Northwest

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.120	0.95	0.114
Landscaped and Lawns	0.000	0.30	0.000
			0.114

Total Area: 0.120 0.95

#### **Time of Concentration:**

		Shee	et-Flow Travel Time								
Segment ID "n" P <sub>2</sub> (in) Flow Length (ft) Slope (ft/ft) Time (min)											
A-B	0.015	3.54	50	0.015	1.0						

Total Tc (min) = 1.0 Minimum Tc = 5.0

Name: **RF-04** 

Location: Proposed Building - Southwest

Cover Type	Area (ac)	С	AxC
Pavement / Impervious	0.115	0.95	0.109
Landscaped and Lawns	0.000	0.30	0.000
			0.109

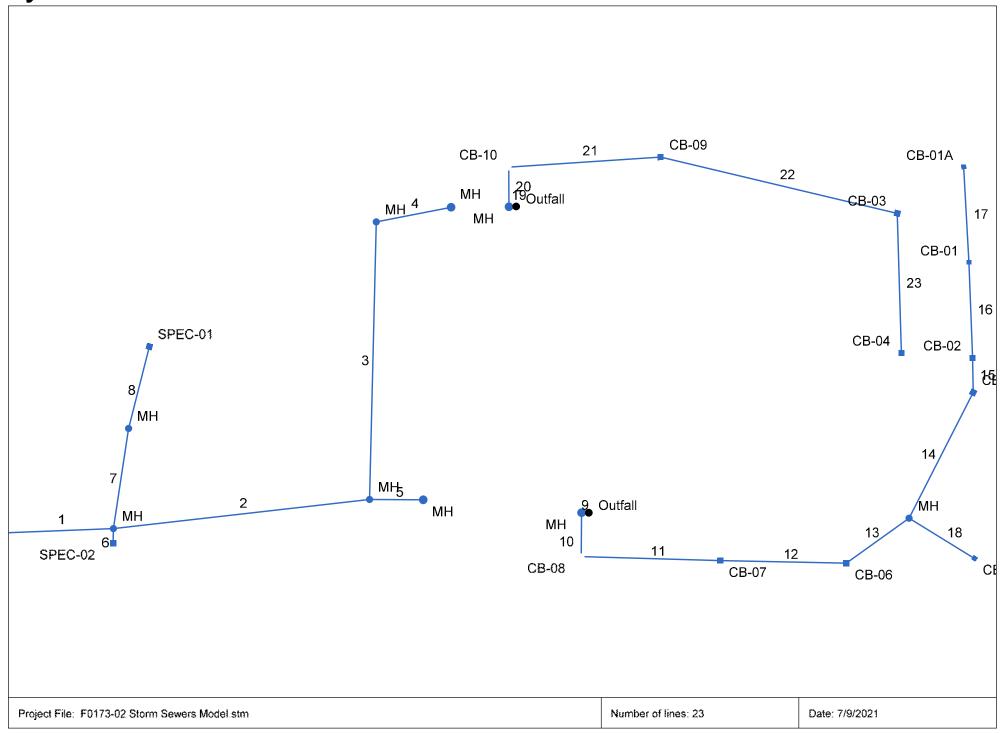
Total Area: 0.115 0.95

#### Time of Concentration:

		Shee	et-Flow Travel Time		
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A-B	0.015	3.54	50	0.015	1.0

Total Tc (min) = \_\_\_\_ 1.0 Minimum Tc = 5.0

## Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



### **Storm Sewer Tabulation**

Station	L	Len	Drng A	Area	Rnoff	Area x C		Тс			Total	Cap	Vel	Pipe		Invert El	ev	HGL Ele	•v	Grnd / Ri	m Elev	Line ID
ine To			Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
Line		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1 En 2 1 3 2 4 3 5 6 1 7 1 8 7 9 En 10 9 11 10 11 13 12 14 13 15 14 16 15 17 16 18 13 19 En 20 21 20 21 22 21 23 22	nd 7 1 1 1 5 3 1 7 7 5 9 8 8 5 9 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	76.000 178.000 192.000 52.600 37.000 10.000 70.000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.24 0.00 0.11 0.10 0.06 0.00 0.12 0.05 0.11 0.12 0.05 0.14	0.24 0.00 0.00 0.00 0.00 0.00 0.24 0.00 0.97 0.97 0.86 0.76 0.70 0.47 0.36 0.30 0.19 0.23 0.40 0.26 0.13 0.05	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.22 0.00 0.00 0.00 0.00 0.00 0.54 0.54 0.45 0.37 0.32 0.24 0.16 0.11 0.07 0.33 0.22 0.10 0.04	0.0 0.0 0.0 0.0 0.0 0.0 5.0 5.0 5.0 5.0	27.9 1.2 0.2 0.0 0.0 25.5 0.0 16.6 15.3 14.9 14.7 14.2 7.8 10.9 7.6 7.5 7.0 5.8 5.0	3.5 0.0 0.0 0.0 0.0 0.0 3.7 0.0 4.7 4.7 4.8 4.9 5.0 5.1 5.2 7.0 6.0 7.1 7.2 7.4 8.0 8.6	9.14 8.30 4.40 4.40 3.90 0.04 0.85 0.03 2.56 2.57 2.17 1.79 0.58 0.45 0.45 0.45 2.34 2.36 1.64 0.83 0.38	8.04 11.05 9.85 9.65 7.00 14.07 8.04 2.72 0.00 2.80 3.32 3.33 3.34 3.85 3.87 2.38 2.39 1.69 0.00 3.38 6.36 6.09 4.71	5.17	18 18 18 15 15 12 12 12 12 12 12 12 12 12 12 12 12 12	0.50 0.94 0.75 1.90 1.00 13.30 0.50 0.50 0.50 0.75 0.75 0.75 0.75 0.99 1.00 1.01 1.02 0.51 0.00 0.77 2.72 2.50 1.49	138.50 138.88 140.56 142.00 142.63	138.88 140.56 142.00 143.00 143.00 140.21 139.23 139.52 142.00 143.16 145.03 145.43 147.36 147.60 148.03 148.70 145.70 142.00 143.21 146.07 150.26 151.70	140.44 141.35 142.63 143.15 143.30 141.35 141.35 143.84 144.03 144.41 144.90 145.60 146.78 147.82 147.87 148.36 145.96 143.79 143.87 146.61 150.64	140.93 142.29 142.93 143.85 143.80 141.35 141.35 143.86 144.68 145.60 145.96 147.97 148.36 148.99 146.02 143.81 143.87 146.61 150.64 151.95	141.50 142.82 145.79 145.79 145.79 142.82 142.82 143.80 146.33 146.10 148.30 151.60 153.50 0.00 152.50 146.50 146.50 146.50 146.50 146.70	142.82 145.79 145.97 146.50 146.33 144.30 143.80 146.10 148.30 151.60 153.50 0.00 152.50 150.70 147.70 146.50 149.70 154.70	

Number of lines: 23

NOTES:Intensity = 38.51 / (Inlet time + 3.60) ^ 0.70; Return period =Yrs. 25 ; c = cir e = ellip b = box

Project File: F0173-02 Storm Sewers Model.stm

Run Date: 7/9/2021

**APPENDIX G** 

# 141 Danbury Road Residential Development Wilton, Connecticut

## **Maintenance and Inspection Plan**

**July 2021** 

The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, roof leaders, piping, hydrodynamic separators, underground infiltration systems, and system outlet.

The following is a checklist of items that will be checked and maintained during scheduled maintenance operations.

<u>Drainage Structures:</u> The Owner will be responsible for cleaning the catch basins, yard drains, manholes, piping, and outlet protection on their property. A Connecticut licensed hauler shall clean the sumps, and legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed.

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

<u>Hydrodynamic Separator:</u> The Contech CDS units (hydrodynamic separator) will be skimmed and oil and scum removed. In a separate operation, silt, sand, and sediment will be removed. Once the structure is cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.

<u>Underground Infiltration:</u> The underground infiltration system will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

<u>Level Spreader:</u> The level spreader shall be inspected two times annually. Regular maintenance includes removing accumulated debris and sediment, checking for erosion, vegetative bare spots, and removing invasive plan species or tree saplings.

<u>Pavement:</u> Paved areas shall be swept periodically by the Owner to clean trash and other debris. The Owner will sweep paved areas on its property in the spring to remove winter accumulations of road sand.

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

## **Drainage Structures Inspection**

Each catch basin and yard drain shall be inspected every four months, with one inspection occurring during the month of April. Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment. Maintain a log of inspections. Remove organic matter, sand, and debris from catch basins as necessary and dispose of legally.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

## **Underground Infiltration**

The underground infiltration system shall be inspected annually and will be cleaned of all silt, debris and sediment from the inlet structure, outlet structure and the chamber lengths. The outlet control structure will be inspected and cleaned to make sure nothing is clogging the discharge pipe.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments
		_	

#### Pavement Inspection

Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Sweep accumulated sediment and debris from the paved areas. Clean paved areas as necessary during the remainder of the year.

Date (MM/DD/YY)	Company/Person	Supervising Team Member	Comments

**APPENDIX H** 

Questions concerning the VERTCON process may be mailed to  $\underline{\mbox{NGS}}$ 

Latitude: 41.179

Longitude: 073.417

NGVD 29 height:

Datum shift(NAVD 88 minus NGVD 29): -0.329 meter = -1.07 feet

 $\underline{\textbf{TABLE 5-SUMMARY OF DISCHARGES}} \text{-} \text{continued}$ 

		10		CHARGES (cfs)	0.2
FLOODING SOURCE AND LOCATION	DRAINAGE AREA (sq. miles)	10- PERCENT- ANNUAL- <u>CHANCE</u>	2- PERCENT- ANNUAL- <u>CHANCE</u>	1- PERCENT- ANNUAL- <u>CHANCE</u>	0.2- PERCENT- ANNUAL- <u>CHANCE</u>
NOROTON RIVER -					
continued	4.20	500	000	1.000	1.000
At Jelliff Mill Road	4.38	520	890	1,080	1,900
Upstream of Mead Park	1.90	220	390	460	820
Upstream of Wahackne Road	0.79	90	160	200	340
Upstream of Greenley	0.79	90	100	200	340
Road	0.43	50	90	110	190
NORTH FARRAR					
BROOK					
At the confluence with					
the Pequonnock River					
(Upper Reach)	0.46	100	245	350	780
At the Trumbull-Monroe					
corporate limits	0.03	10	25	35	80
NORWALK RIVER					
Upstream of confluence					
of Betts Pond Brook	57.6	4,100	9,500	14,000	16,250
Upstream of confluence	22.0	2 (00	c 200	0.100	20,000
of Silvermine River	32.8	2,600	6,300	9,100	20,000
At Kent Road  Downstream of	30.0	2,980	5,840	7,455	12,505
confluence of					
Comstock Brook	25.7	2,680	5,280	6,735	11,295
Upstream of confluence	23.7	2,000	3,200	0,733	11,275
of Comstock Brook	18.4	1,845	3,660	4,675	7,840
Downstream of		,	-,	7	, , -
confluence of Gilbert					
and Bennett Brooks	13.8	1,425	2,865	3,655	6,135
Upstream of confluence					
of Gilbert and Bennett					
Brooks	12.3	1,205	2,445	3,125	5,240
Downstream of the					
confluence of Cooper					
Pond Brook	11.13	1,010	2,085	2,665	4,475
Upstream of the					
confluence of Cooper	0.72	((5	1.250	1 505	2 (00
Pond Brook	8.73	665	1,250	1,595	2,680

## Norwalk River Calibrated (Duplicate Effective) Model Output Table

HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1

	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
D 1.4	00000	100/	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.75
Reach-1	29920	10%	2980.00	147.00	152.32	152.32	153.29	0.004454	9.23	671.47	438.66	0.75
Reach-1	29920	2%	5840.00	147.00	153.56	153.56	154.60	0.004481	10.83	1400.71	673.09	0.79
Reach-1	29920	1%	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86	1676.50	693.44	0.83
Reach-1	29920	0.2%	12505.00	147.00	154.99	154.99	156.40	0.005722	14.14	2414.85	738.35	0.92
Reach-1	29760	10%	2980.00	142.20	148.53		149.01	0.001498	5.62	583.13	179.68	0.44
Reach-1	29760	2%	5840.00	142.20	151.31		151.93	0.001165	6.63	1125.96	211.79	0.42
Reach-1	29760	1%	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	29760	0.2%	12505.00	142.20	154.28		155.51	0.001589	9.59	1814.00	255.42	0.51
11000111	20700	0.270	12000.00	1 12.20	101.20		100.01	0.001000	0.00	1011.00	200.12	0.01
Reach-1	28240	10%	2980.00	138.00	145.34		146.30	0.002090	7.99	445.85	151.41	0.55
Reach-1	28240	2%	5840.00	138.00	146.52	146.52	148.75	0.004139	12.55	696.60	258.98	0.79
Reach-1	28240	1%	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	28240	0.2%	12505.00	138.00	149.76	149.76	151.98	0.003397	14.32	1979.91	552.23	0.76
Reach-1	27468	10%	2980.00	132.10	145.99		145.99	0.000005	0.60	9140.64	793.45	0.03
Reach-1	27468	2%	5840.00	132.10	146.99		146.99	0.000017	1.11	9943.03	813.12	0.05
Reach-1	27468	1%	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	27468	0.2%	12505.00	132.10	148.85		148.88	0.000052	2.13	11529.28	890.79	0.10
Decel 4	07440	400/	2000.00	400.00	445.07		445.00	0.000004	4.74	4705 50	000.40	0.40
Reach-1	27110	10%	2980.00	136.60 136.60	145.97		145.99	0.000064	1.74	4765.52 5707.19	962.48 991.44	0.10
Reach-1	27110 27110	1%	5840.00 7455.00	136.60 136.60	146.94 147.46		146.97	0.000148 0.000187	2.83 3.29	5707.19 6234.70	991.44 1005.58	0.16
Reach-1	27110	0.2%	12505.00	136.60	147.46		147.51 148.82	0.000187	4.52	7518.38	1005.58	0.18
reach-l	2/110	0.270	12005.00	130.00	148.74		148.82	0.000304	4.52	1518.38	1009.50	0.23
Reach-1	27025	10%	2980.00	135.50	145.63	141.84	145.90	0.000562	5.28	1759.35	880.05	0.30
Reach-1	27025	2%	5840.00	135.50	145.63	145.59	146.68	0.000362	9.96	1855.68	883.55	0.56
Reach-1	27025	1%	7455.00	135.50	146.24	146.03	147.20	0.001303	10.68	2304.78	899.67	0.59
Reach-1	27025	0.2%	12505.00	135.50	147.33	147.10	148.46	0.002112	12.81	3304.65	934.56	0.67
TCGGII-1	21020	0.270	12000.00	100.00	147.00	147.10	140.40	0.002004	12.01	0004.00	304.00	0.07
Reach-1	27020		Bridge									
Reach-1	27015	10%	2980.00	135.50	141.85	141.85	144.38	0.006857	13.22	278.63	62.97	0.97
Reach-1	27015	2%	5840.00	135.50	145.62	145.62	146.66	0.002172	10.38	1752.24	879.80	0.59
Reach-1	27015	1%	7455.00	135.50	146.08	146.08	147.18	0.002399	11.26	2163.67	894.64	0.63
Reach-1	27015	0.2%	12505.00	135.50	147.11	147.11	148.43	0.003090	13.64	3099.86	927.52	0.72
Reach-1	26680	10%	2980.00	134.00	140.31	140.08	141.21	0.004091	9.97	762.74	365.85	0.74
Reach-1	26680	2%	5840.00	134.00	142.16		142.88	0.003007	10.34	1642.26	560.63	0.67
Reach-1	26680	1%	7455.00	134.00	142.90		143.58	0.002777	10.58	2066.21	590.20	0.65
Reach-1	26680	0.2%	12505.00	134.00	145.35		145.79	0.001646	9.70	3857.15	759.13	0.52
Reach-1	26209	10%	2980.00	133.40	140.62		140.66	0.000240	1.93	2591.95	867.42	0.17
Reach-1	26209	2%	5840.00	133.40	142.35		142.41	0.000238	2.43	4170.98	944.15	0.18
Reach-1	26209	1%	7455.00	133.40	143.05		143.12	0.000251	2.70	4830.47	949.47	0.19
Reach-1	26209	0.2%	12505.00	133.40	145.37		145.47	0.000223	3.12	7059.39	967.22	0.19
Reach-1	26136	10%	2980.00	130.20	139.77	136.89	140.44	0.001214	7.36	865.42	504.59	0.44
Reach-1	26136	2%	5840.00	130.20	141.38	140.68	142.16	0.001214	9.14	1847.21	666.49	0.50
Reach-1	26136	1%	7455.00	130.20	141.30	141.28	142.16	0.001499	9.14	2353.38	704.50	0.50
Reach-1	26136	0.2%	12505.00	130.20	144.86	142.59	145.33	0.001499	8.76	4394.50	760.00	0.30
		1		.00.20		2.55		2.000000	5.70	.001.00	, 55.56	5.41
Reach-1	26127.5		Bridge									
Reach-1	26119	10%	2980.00	131.30	138.62	136.96	138.86	0.001012	5.17	1356.28	541.45	0.36
Reach-1	26119	2%	5840.00	131.30	141.25	138.61	141.42	0.000572	4.88	3054.77	719.80	0.28
Reach-1	26119	1%	7455.00	131.30	142.26	138.86	142.42	0.000529	5.03	3791.17	742.95	0.28
Reach-1	26119	0.2%	12505.00	131.30	144.97	140.05	145.13	0.000437	5.35	5865.51	778.00	0.26
Reach-1	26058	10%	2980.00	131.30	138.53		138.79	0.001092	5.33	1309.05	531.38	0.37
Reach-1	26058	2%	5840.00	131.30	141.22		141.38	0.000586	4.92	3026.55	717.66	0.29
Reach-1	26058	1%	7455.00	131.30	142.22		142.38	0.000539	5.06	3764.56	742.33	0.28
Reach-1	26058	0.2%	12505.00	131.30	144.94		145.10	0.000442	5.37	5843.13	778.00	0.26
Decel 1	05050	400/	0000.55	101.55	107.65		100.15	0.000765	4.5.	4504.55	100 5 1	
Reach-1	25358	10%	2980.00	131.00	137.99		138.13	0.000739	4.81	1594.08	436.94	0.33
Reach-1	25358	2%	5840.00	131.00	140.85		140.99	0.000527	5.13	2885.35	468.88	0.29
Reach-1	25358	1%	7455.00	131.00	141.84		142.00	0.000548	5.59	3368.25	501.77	0.30
Reach-1	25358	0.2%	12505.00	131.00	144.56		144.76	0.000543	6.48	5013.74	635.86	0.31
Reach-1	24597	10%	2980.00	127.90	137.54		137.72	0.000415	3.74	908.33	167.21	0.22
Reach-1	24597	2%	5840.00	127.90	140.33		140.60	0.000415	4.72	1477.03	282.08	0.24
	24597	1%	7455.00	127.90 127.90						1477.03		
Reach-1	24597	0.2%	12505.00	127.90	141.26 143.91		141.58 144.30	0.000532 0.000614	5.33 6.50	3259.65	487.39 576.34	0.26
1.00011-1	24331	0.270	12303.00	121.30	143.81		144.30	0.000014	0.30	3239.03	310.34	0.28
		10%	2980.00	127.90	137.15	132.79	137.67	0.001052	5.78	515.90	160.44	0.35
Reach-1	24560											

HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	24560	1%	7455.00	127.90	141.24	136.38	141.56	0.000537	5.35	1773.46	485.12	0.26
Reach-1	24560	0.2%	12505.00	127.90	143.88	139.30	144.28	0.000619	6.52	3245.22	576.17	0.29
Reach-1	24542.5		Bridge									
Reach-1	24525	10%	2980.00	127.20	135.27	133.49	136.46	0.003361	9.08	507.48	212.95	0.60
Reach-1	24525	2%	5840.00	127.20	138.57	136.74	139.62	0.002188	9.45	1358.71	342.03	0.52
Reach-1	24525	1%	7455.00	127.20	139.76	137.71	140.91	0.002189	10.16	1844.44	449.44	0.53
Reach-1	24525	0.2%	12505.00	127.20	142.35	139.79	143.79	0.002461	12.32	3395.84	811.45	0.58
												<b>.</b>
Reach-1	24457	10%	2980.00	127.20	133.42	133.42	136.00	0.007504	12.96	249.76	64.13	1.00
Reach-1	24457	2%	5840.00	127.20	136.74	136.74	139.26	0.004358	13.68	858.70	241.86	0.82
Reach-1	24457	1%	7455.00	127.20	137.78	137.78	140.54	0.004328	14.71	1121.20	262.63	0.84
Reach-1	24457	0.2%	12505.00	127.20	140.59	140.59	143.45	0.003743	16.22	2228.03	492.18	0.81
D 1.4	04405	100/	2000.00	404.00	100.05	100.00	100.11	2 222224	7.40	447.00	70.00	0.55
Reach-1	24105	10%	2980.00	124.80	132.65	130.63	133.44	0.002381	7.13	417.66	78.83	0.55
Reach-1	24105	2%	5840.00	124.80	134.63	132.93	136.19	0.003492	10.03	582.32	262.38	0.69
Reach-1	24105 24105	1% 0.2%	7455.00 12505.00	124.80 124.80	135.37	134.00 137.57	137.42 139.49	0.004065 0.001714	11.49 9.47	665.70	391.75 1520.09	0.75 0.52
Reach-1	24105	0.2%	12505.00	124.00	138.50	137.57	139.49	0.001714	9.47	3845.46	1520.09	0.52
Ponch 1	23805	10%	2090 00	124.00	122.20		122 07	0.001170	6.13	997.32	221.22	0.41
Reach-1	23805	2%	2980.00 5840.00	124.00 124.00	132.38 134.65		132.87 135.32	0.001170 0.001300	7.78	1933.43	331.23 474.68	0.41
Reach-1	23805	1%	7455.00	124.00	134.65		135.32	0.001300	8.38	2427.76	508.37	0.45
Reach-1	23805	0.2%	12505.00	124.00	138.18		138.99	0.001310	9.55	4409.49	1582.59	0.46
	20000	J.2 70	12303.00	124.00	130.10		130.33	5.001276	3.33	-400.48	1002.09	0.47
Reach-1	23415	10%	2980.00	123.00	129.81	129.81	131.82	0.006096	11.90	404.45	161.55	0.89
Reach-1	23415	2%	5840.00	123.00	132.27	132.27	134.30	0.000096	13.19	1159.47	343.43	0.89
Reach-1	23415	1%	7455.00	123.00	133.11	133.11	135.33	0.004719	14.27	1451.84	358.59	0.84
Reach-1	23415	0.2%	12505.00	123.00	135.13	135.13	137.89	0.005069	16.96	2245.13	422.31	0.91
TCGGIT-1	20410	0.270	12000.00	120.00	100.10	100.10	107.00	0.000000	10.50	2240.10	422.01	0.51
Reach-1	23171	10%	2980.00	120.30	128.75		129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2%	5840.00	120.30	129.79	129.12	131.57	0.005575	10.79	599.24	177.93	0.81
Reach-1	23171	1%	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23171	0.2%	12505.00	120.30	134.35	100.00	135.16	0.001732	7.84	1880.08	333.29	0.44
rtouoii i	120111	10.270	12000.00	120.00	101.00		100.10	0.001702	7.01	1000.00	000.20	i
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	1%	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	23036	0.2%	12505.00	121.70	134.55		134.98	0.000237	3.32	2572.37	391.51	0.18
Reach-1	22916	10%	2980.00	121.00	128.01	126.93	128.88	0.002603	8.01	570.82	302.03	0.57
Reach-1	22916	2%	5840.00	121.00	130.41		130.84	0.000999	6.20	1483.60	430.42	0.38
Reach-1	22916	1%	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Reach-1	22765	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	2%	5840.00	114.20	130.48		130.70	0.000299	3.96	2020.14	395.39	0.19
Reach-1	22765	1%	7455.00	114.20	131.64		131.87	0.000301	4.19	2548.37	511.91	0.19
Reach-1	22765	0.2%	12505.00	114.20	134.64		134.84	0.000240	4.22	4324.67	669.64	0.17
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27		130.51	0.001575	4.56	1791.09	483.52	0.26
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
Reach-1	22140	10%	2980.00	117.00	124.05	124.05	126.26	0.006734	12.84	391.36	132.65	0.95
Reach-1	22140	2%	5840.00	117.00	126.77	126.77	129.42	0.005440	14.96	889.23	205.48	0.91
Reach-1	22140	1%	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
		1.00/										L
Reach-1	21825	10%	2980.00	115.90	121.80	121.75	123.65	0.007981	11.17	314.54	84.21	0.97
Reach-1	21825	2%	5840.00	115.90	124.12	124.12	126.73	0.006551	13.42	604.08	179.14	0.94
Reach-1	21825	1%	7455.00	115.90	125.26	125.26	128.03	0.005781	14.07	847.23	239.90	0.91
Reach-1	21825	0.2%	12505.00	115.90	131.24	127.79	132.45	0.001436	10.39	3430.35	1045.30	0.50
Dec 1 1	04770	4001	2057.7	44	100.00	100.00	100.00	0.000:		000 0	100.00	
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.97	0.002174	7.62	390.83	103.38	0.55
Reach-1	21770	2%	5840.00	115.40	124.17	122.36	126.07	0.003067	11.07	527.79	119.93	0.68
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Desert 1	04757.5		5									
Reach-1	21757.5		Bridge									
Decel 1	04745	400/	0000 55	415.10	404.0-	400.00	400.05	0.0000::		202 5-	100 55	2 ==
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach-1	21745	1%	7455.00	115.40	124.48	123.47	127.36	0.004410	13.60	547.97	122.37	0.83
Reach-1	21745	0.2%	12505.00	115.40	126.94	126.53	131.79	0.005288	17.67	707.72	141.67	0.94

HEC-RAS Plan: DE River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21695	10%	2980.00	114.20	121.74	120.15	122.74	0.003025	8.01	371.94	69.60	0.61
Reach-1	21695	2%	5840.00	114.20	123.69	122.46	125.72	0.004430	11.42	511.32	74.77	0.76
Reach-1	21695	1%	7455.00	114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1	21695	0.2%	12505.00	114.20	127.45	127.45	130.78	0.004531	14.98	1124.07	292.57	0.82
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

# Norwalk River Existing Conditions (Corrected Effective) Model Output Table

1150 540	DI EVIOT	D: D: /ED 4	
			Reach: Reach-1

Reach   1900   1901				Reach. Reach-									
	Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
				(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
	Reach-1	29920	10%	2980.00	147.00	152.32	152.32	153.29	0.004454	9.23	671.47	438.66	0.75
Seages   19800   95		29920	2%							10.83			0.79
Seaght   98900   25%   120500   147.00   154.50   154.50   154.50   0.000722   154.51   254.50   799.30   0.1													
Reach   S7780													0.83
Seach   SWIND   26,   Seach   20   19.   19.   26.00   19.   26.00   19.   26.00   19.   26.00   19.   26.00   2	Reach-1	29920	0.2%	12505.00	147.00	154.99	154.99	156.40	0.005722	14.14	2414.85	738.35	0.92
Seach   SWIND   26,   Seach   20   19.   19.   26.00   19.   26.00   19.   26.00   19.   26.00   19.   26.00   2													ĺ
Respiration   Process	Reach-1	29760	10%	2980.00	142.20	148.53		149.01	0.001498	5.62	583.07	179.68	0.44
Seach   19700   16													0.42
Research   20200													
Respired 1 202-00 10% 206-00 130-00 146-39 146-32 0.00239 7.02 452-97 156.57 0.0 Respired 1 202-00 2% 560-00 130-00 146-50 146-52 146-52 146-52 0.00239 12.55 56-60 258-56 7.0 Respired 1 202-00 1% 202-00 130-00 146-71 147-71 440-00 0.00396 12.55 56-60 258-56 7.0 Respired 1 202-00 10% 202-00 130-00 147-71 147-71 440-70 151-80 0.00396 12.55 56-60 258-56 7.0 Respired 1 202-00 10% 202-00 130-00 147-71 147-71 440-70 0.00396 12.55 56-60 258-77 0.0 Respired 1 202-00 10% 202-00 130-30 146-00 147-70 140-70 0.00396 14.2 151-50 56-70 56-0 1.0 Respired 202-00 10% 202-00 130-30 146-00 147-70 0.00035 14.2 151-50 56-70 56-0 1.0 Respired 202-00 1% 745-50 130-30 146-00 147-70 0.00035 12.5 151-50 76-70 0.0 Respired 202-00 1% 745-50 130-30 147-70 147-70 0.00035 12.5 151-50 745-70 0.0 Respired 202-00 1% 122-00 130-30 147-70 147-70 0.00035 12.5 151-50 745-70 0.0 Respired 202-00 1% 122-00 130-30 147-70 147-70 0.00035 12.5 151-50 745-70 0.0 Respired 202-00 1% 122-00 130-30 148-80 144-80 144-80 0.00035 12.5 151-50 80-74-73 0.0 Respired 202-00 10% 202-00 130-50 148-80 144-80 0.00035 147-50 0.00035 12.5 151-50 80-72-71 0.0 Respired 279-00 20% 56-00 0.0 136-50 144-09 147-72 0.00000 1.2 20 58-90 23 77-6.6 0.00035 12.5 151-50 80-72-71 0.0 Respired 279-00 20% 152-00 0.0 130-50 144-09 147-72 0.00000 12.2 20 58-90 23 77-6.5 0.0 Respired 279-00 20% 152-00 0.0 130-50 144-09 147-72 0.000000 12.2 20 58-90 23 77-6.5 0.0 Respired 279-00 20% 152-00 0.0 130-50 144-09 147-72 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.000000 12.2 0.0000000 12.2 0.0000000 12.2 0.0000000 12.2 0.0000000 12.2 0.0000000 12.2 0.0000000 12.2 0.0000000000													0.44
Reacht   28240	Reach-1	29760	0.2%	12505.00	142.20	154.28		155.51	0.001589	9.59	1814.00	255.42	0.51
Reacht   28240													ĺ
Reacht   28240	Reach-1	28240	10%	2980.00	138.00	145.39		146.32	0.002036	7.92	452.97	156.57	0.54
Reach-1   28240   15							146 52						0.79
Reacht   28840													
Reach   20020   19%   290.00   136.33   146.00   146.01   0.000055   1.53   4394.50   676.05   0.746.73   0.866.01   120.00   156.73   147.00   0.001131   2.54   5105.56   745.73   0.866.01   120.00   156.73   147.00   0.001131   2.54   5105.56   745.73   0.866.01   120.00   156.73   147.00   0.001131   2.54   5105.56   745.73   0.866.01   120.00   156.73   147.00   0.001131   2.54   5105.56   745.73   0.866.01   120.00   156.73   147.00   0.001131   2.54   5105.56   745.73   0.866.01   147.00   0.001131   2.54   5105.56   745.73   0.866.01   148.00   148.00   0.000006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   140.00   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   1.60   0.00006   0.60   0.00006   0.60   0.00006   0.0													0.75
Reach+1   20020   2%   Seq.00   15.633   147.00   147.03   0.000143   2.45   516.566   74.873   0.000148   0.0000148   0.000148   0.000148   0.000148   0.000148   0.000148	Reach-1	28240	0.2%	12505.00	138.00	149.76	149.76	151.98	0.003397	14.32	1979.91	552.23	0.76
Reach+1   20020   2%   Seq.00   15.633   147.00   147.03   0.000143   2.45   516.566   74.873   0.000148   0.0000148   0.000148   0.000148   0.000148   0.000148   0.000148													ĺ
Reach-1   20020   2%   594.00   19.33   147.00   147.03   0.00113   2.4   510.56   74.73   0.0018   Reach-1   20020   7%   749.50   19.33   147.05   147.95   0.00192   2.77   501.07   769.77   0.00   769.77   769.77   0.00   769.77   0.00   769.77   0.00   769.77   769.7	Reach-1	28020	10%	2980.00	136.33	146.00		146.01	0.000055	1.53	4394.50	676.05	0.09
Reach   20020													0.14
Reach-1   2020   0.2%   1205.00   19.0.33   148.88   148.87   0.002035   4.08   6569.85   69.3.73   0.1													
Reach-1   27930   10%   298.00   133.65   146.00   146.01   0.000066   1.46   4590.10   7721.01   0.00066   1.46   4590.10   7721.01   0.00066   1.46   4590.10   774.68   0.000132   2.76   5775.37   778.50   0.00066   1.46   774.68   0.000132   2.76   5775.37   778.50   0.00066   778.50   0.00067   774.68   0.000712   2.76   5775.37   778.50   0.00067   0.00067   0.00067   0.00067   0.00067   0.00067   0.00067   0.00067   0.00067   0.00067   0.													0.16
Reacht   27930   2%   594.00   135.66   145.69   147.02   0.000100   2.38   5340.23   774.68   0.0	Reach-1	28020	0.2%	12505.00	136.33	148.88		148.97	0.000263	4.06	6569.85	803.73	0.21
Reach+1   27930   2%   594.00   135.65   146.99   147.22   0.000100   2.78   579.63   774.65   0.0   Reach+1   27930   1%   745.00   135.65   147.54   147.58   0.000132   2.76   576.37   785.30   0.0   Reach+1   27930   0.2%   12500.00   135.65   148.86   148.86   0.000207   3.72   6803.94   778.82   0.0   1.													
Reach+1   27930   2%   594.00   135.65   146.99   147.22   0.000100   2.78   579.63   774.65   0.0   Reach+1   27930   1%   745.00   135.65   147.54   147.58   0.000132   2.76   576.37   785.30   0.0   Reach+1   27930   0.2%   12500.00   135.65   148.86   148.86   0.000207   3.72   6803.94   778.82   0.0   1.	Reach-1	27930	10%	2980 00	135.65	146 00		146 01	0 000046	1 46	4590 10	721 ∩1	0.08
Reach-1   27930   1%   74550   135.65   147.54   147.58   0.000132   2.76   576.37   765.36   0.000132   0.2%   12590.00   134.60   145.59   146.00   0.000037   1.37   4838.61   785.83   0.000132   0.2%   1.00000000000000000000000000000000000													
Reach-1   27390   0.2%   12590.00   13.5.65   148.66   148.95   0.000027   3.72   8893.94   7783.2   0.0													0.13
Reach-1   2780   19%   298.00   134.60   146.99   146.00   0.00037   1.7	Reach-1	27930	1%	7455.00	135.65	147.54		147.58	0.000132	2.76	5765.37	785.36	0.15
Reach-1   27830   10%   2980.00   134.60   145.90   146.00   0.000337   1.37   4838.61   785.83   0.0	Reach-1	27930	0.2%	12505.00	135.65	148.86		148.95	0.000207	3.72	6803.94	788.32	0.19
Reacht   27830   2%   \$840.00   134.80   146.98   147.01   0.000084   2.20   \$692.42   869.13   0.													
Reacht   27830   2%   \$840.00   134.80   146.98   147.01   0.000084   2.20   \$692.42   869.13   0.	Doort 1	27922	100/	2002.22	404.00	4/5 00		440.00	0.00000	1.0-	4000 0:	705.00	2.55
Reach-1   27830   1%   7455.00   134.60   147.53   147.57   0.000104   2.52   6148.13   990.10   0.													0.08
Reach-1   2780   0.2%   12505.00   134.00   148.85   148.82   0.000153   3.20   7437.92   1023.96   0.	Reach-1	27830		5840.00	134.60	146.98		147.01	0.000084	2.20	5662.42	869.13	0.12
Reach   27890   0.2%   12505.00   134.00   148.85   148.82   0.000153   3.29   7437.02   1023.96   0.	Reach-1	27830	1%	7455.00	134.60	147.53		147.57	0.000104	2.52	6148.13	920.10	0.13
Reach-1 27790 10% 2890.00 134.00 146.59 146.00 0.000035 1.33 4920.00 803.92 0.0 Reach-1 27790 29% 5840.00 134.00 146.98 147.01 0.000079 2.13 5783.83 928.44 0.0 Reach-1 27790 15% 27455.00 134.00 146.98 147.01 0.000079 2.43 6290.40 0.0 Reach-1 27790 10% 29% 12505.00 134.00 146.85 142.55 0.000079 2.43 6290.40 0.0 Reach-1 27780 10% 2980.00 134.00 148.85 148.85 148.92 0.000139 3.14 7665.44 1110.26 0.0 Reach-1 27488 10% 29% 5840.00 132.10 146.59 0.000070 0.000070 1.11 9943.03 813.12 0.0 Reach-1 27488 17% 7455.00 132.10 146.59 146.89 146.99 0.000005 0.60 9140.64 7793.45 0.0 Reach-1 27488 17% 7455.00 132.10 146.59 146.89 146.99 0.000005 0.60 9140.64 7793.45 0.0 Reach-1 27488 17% 7455.00 132.10 146.59 146.89 146.99 0.000005 0.60 9140.64 7793.45 0.0 Reach-1 27488 17% 5745.00 132.10 144.55 1475.46 0.000027 1.11 9943.03 813.12 0.0 Reach-1 27408 0.2% 12505.00 132.10 146.59 146.59 0.000027 1.11 9943.03 813.12 0.0 Reach-1 2710 10% 2980.00 138.00 146.97 146.89 146.99 0.000006 0.00002	Reach-1	27830	0.2%	12505.00	134 60	148 85		148 92	0.000153	3 29	7437 92	1023 96	0.16
Reach-1   27790   2%   5840.00   134.60   144.89   147.01   0.000079   2.13   5783.83   0.24.4   0.0		27.000	0.270	12000.00	101.00	1 10.00		110.02	0.000100	0.20	7 107.02	1020.00	0.10
Reach-1   27790   2%   5840.00   134.60   144.89   147.01   0.000079   2.13   5783.83   0.24.4   0.0													
Reach-1   27790   1%   7455.00   134.60   147.55   147.56   0.00097   2.43   6299.40   970.45   0.0													80.0
Reach-1   27790   0.2%   12505.00   134.60   148.85   148.92   0.000139   3.14   7665.44   1110.26   0.0	Reach-1	27790	2%	5840.00	134.60	146.98		147.01	0.000079	2.13	5783.83	928.44	0.11
Reach-1   27790   0.2%   12505.00   134.60   148.86   148.92   0.000139   3.14   7665.44   1110.26   0.0	Reach-1	27790	1%	7455.00	134.60	147.53		147.56	0.000097	2.43	6299.40	970.45	0.13
Reach-1 27468 19% 2980 00 132.10 146.99 0.000005 0.60 9140.64 733.45 0.0 Reach-1 27468 2% 5840.00 132.10 146.99 146.99 0.000017 1.11 9943.03 813.12 0.0 Reach-1 27468 0.22% 1555.00 132.10 147.53 147.54 0.000024 1.37 10389.13 832.33 0.0 Reach-1 27468 0.22% 12555.00 132.10 147.53 147.54 0.000024 1.37 10389.13 832.33 0.0 Reach-1 2710 10% 2980.00 136.60 145.97 145.99 0.000064 1.74 4765.52 982.48 0.0 Reach-1 2710 10% 2980.00 136.60 145.97 145.99 0.000064 1.74 4765.52 982.48 0.0 Reach-1 2710 10% 745.00 136.60 145.97 145.99 0.000164 1.74 4765.52 982.48 0.0 Reach-1 2710 10% 745.00 136.60 146.94 146.97 0.000148 2.83 5707.19 991.44 0.0 Reach-1 2710 10% 125.00 136.60 147.48 147.71 0.000187 3.29 623.47 0.005.89 0.0 Reach-1 2710 0.2% 12505.00 136.60 148.74 148.82 0.000304 4.52 7518.38 1008.50 0.0 Reach-1 2710 0.2% 12505.00 136.60 148.74 145.90 0.000662 5.28 1759.35 880.05 0.0 Reach-1 27025 2% 5840.00 135.50 145.83 141.84 145.90 0.000662 5.28 1759.35 880.05 0.0 Reach-1 27025 10% 2980.00 135.50 145.74 145.50 146.83 0.000862 5.28 1759.35 880.05 0.0 Reach-1 27025 10 840.00 135.50 146.24 146.03 147.20 0.002112 10.66 2304.78 8967 0.0 Reach-1 27025 15% 7455.00 135.50 146.24 146.03 147.20 0.002112 10.66 2304.78 8967 0.0 Reach-1 27015 10% 2980.00 135.50 145.83 141.85 144.88 0.008687 13.22 278.63 829.78 8967 0.0 Reach-1 27015 10% 2860.00 135.50 145.60 146.60 146.08 147.18 0.002399 11.26 278.60 62.97 Reach-1 27015 10% 7455.00 135.50 145.83 141.85 144.83 0.008687 13.22 278.63 82.97 0.0 Reach-1 27015 10% 7455.00 135.50 145.80 144.80 145.80 144.80 0.002172 10.66 2304.78 8967 0.0 Reach-1 27015 10% 7455.00 135.50 145.80 144.80 144.80 0.002172 10.66 2304.78 8967 0.0 Reach-1 27015 10% 2860.00 133.50 144.80 144.80 144.80 0.002172 10.60 2304.78 8967 0.0 Reach-1 27015 10% 2860.00 133.50 144.80 144.80 144.80 0.002172 10.60 2304.78 8967 0.0 Reach-1 27015 10% 7455.00 1355.00 1355.00 145.62 145.60 0.002172 10.60 2304.78 8964.00 0.0 Reach-1 27015 10% 7455.00 133.00 142.80 144.80 144.80 0.002472 10.30 302.07 755.51 0.0 Reach-1 28080 10% 2980.00 133.40													0.16
Reach   27468   2%   5840.00   132.10   146.99   146.99   0.000017   1.11   9943.03   813.12   0.0	Tteach-1	21130	0.270	12303.00	134.00	140.00		140.32	0.000133	3.14	7005.44	1110.20	0.10
Reach   27468   2%   5840.00   132.10   146.99   146.99   0.000017   1.11   9943.03   813.12   0.0													
Reach-1   27468   1%   7455.00   132.10   147.53   147.54   0.000024   1.37   10389.13   832.33   0.0	Reach-1	27468	10%	2980.00	132.10	145.99		145.99	0.000005	0.60	9140.64	793.45	0.03
Reach-1   27468   0.2%   12505.00   132.10   148.85   148.88   0.000052   2.13   11529.28   890.79   0.0	Reach-1	27468	2%	5840.00	132.10	146.99		146.99	0.000017	1.11	9943.03	813.12	0.05
Reach-1   27468   0.2%   12505.00   132.10   148.85   148.88   0.000052   2.13   11529.28   890.79   0.0	Reach-1	27468	1%	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1   27110   10%   2980.00   136.60   145.97   145.99   0.000064   1.74   4765.52   962.48   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00064   0.00065   0.000664   0.000665   0.000666   0.00													0.10
Reach-1   27110   2%   5840.00   136.60   146.94   146.97   0.000148   2.83   5707.19   991.44   0.0	Neacii-i	27400	0.2 /6	12303.00	132.10	140.00		140.00	0.000032	2.13	11329.20	090.79	0.10
Reach-1   27110   2%   5840.00   136.60   146.94   146.97   0.000148   2.83   5707.19   991.44   0.0													
Reach-1   27110	Reach-1	27110	10%	2980.00	136.60	145.97		145.99	0.000064	1.74	4765.52	962.48	0.10
Reach-1   27110	Reach-1	27110	2%	5840.00	136.60	146.94		146.97	0.000148	2.83	5707.19	991.44	0.16
Reach-1   27110   0.2%   12505.00   136.60   148.74   148.82   0.000304   4.52   7518.38   1009.50   0.0005666   0.000566   0.000566   0.000566   0.000566   0.0005666   0.000		27110	1%		136.60					3 20		1005 58	0.18
Reach-1   27025   10%   2980.00   135.50   145.63   141.84   145.99   0.000562   5.28   1759.35   880.05   0.000562   0													0.23
Reach-1   27025   2%   5840.00   135.50   145.74   145.59   146.68   0.001965   9.96   1855.68   883.55   0.001965   174.50   145.50   145.74   145.59   146.68   0.002102   10.68   2304.78   899.67   0.001965   0.002102   10.68   2304.78   899.67   0.002102   10.68   2304.78   2304.65   0.002602   0.00260	Reacti-1	2/110	0.276	12505.00	130.00	140.74		140.02	0.000304	4.52	7510.36	1009.50	0.23
Reach-1   27025   2%   5840.00   135.50   145.74   145.59   146.68   0.001965   9.96   1855.68   883.55   0.001965   174.50   145.50   145.74   145.59   146.68   0.002102   10.68   2304.78   899.67   0.001965   0.002102   10.68   2304.78   899.67   0.002102   10.68   2304.78   2304.65   0.002602   0.00260													
Reach-1         27025         1%         7455.00         135.50         146.24         146.03         147.20         0.002112         10.68         2304.78         899.67         0.0           Reach-1         27025         0.2%         12505.00         135.50         147.33         147.10         148.46         0.002654         12.81         3304.65         934.56         0.0           Reach-1         27020         Bridge         2980.00         135.50         141.85         144.83         0.008857         13.22         278.63         62.97         0.0           Reach-1         27015         10%         2980.00         135.50         145.62         145.62         146.66         0.002172         10.38         1752.24         879.80         0.3           Reach-1         27015         1%         7455.00         135.50         146.08         146.08         147.11         147.18         0.002399         11.26         2183.67         894.64         0.0           Reach-1         27015         1%         7455.00         135.50         140.08         140.08         147.11         147.11         147.11         147.11         147.11         147.11         147.11         147.11         147.11         1	Reach-1	27025	10%	2980.00	135.50	145.63	141.84	145.90	0.000562	5.28	1759.35	880.05	0.30
Reach-1         27025         1%         7455.00         135.50         146.24         146.03         147.20         0.002112         10.68         2304.78         899.67         0.0           Reach-1         27025         0.2%         12505.00         135.50         147.33         147.10         148.46         0.002654         12.81         3304.65         934.56         0.0           Reach-1         27020         Bridge         2980.00         135.50         141.85         144.83         0.008857         13.22         278.63         62.97         0.0           Reach-1         27015         10%         2980.00         135.50         145.62         145.62         146.66         0.002172         10.38         1752.24         879.80         0.3           Reach-1         27015         1%         7455.00         135.50         146.08         146.08         147.11         147.18         0.002399         11.26         2183.67         894.64         0.0           Reach-1         27015         1%         7455.00         135.50         140.08         140.08         147.11         147.11         147.11         147.11         147.11         147.11         147.11         147.11         147.11         1	Reach-1	27025	2%	5840.00	135.50	145.74	145.59	146.68	0.001965	9.96	1855.68	883.55	0.56
Reach-1         27025         0.2%         12505.00         135.50         147.33         147.10         148.46         0.002654         12.81         3304.65         934.56         0.0           Reach-1         27020         Bridge   <													0.59
Reach-1         27020         Bridge           Reach-1         27015         10%         2980.00         135.50         141.85         144.38         0.006857         13.22         278.63         62.97         0.1           Reach-1         27015         2%         5840.00         135.50         145.62         145.62         146.66         0.002172         10.38         1752.24         879.80         0.0           Reach-1         27015         1%         7455.00         135.50         145.62         145.62         146.08         147.18         0.002399         11.26         218.367         894.64         0.0           Reach-1         27015         0.2%         12505.00         135.50         147.11         147.11         148.43         0.003090         113.64         3099.86         927.52         0.0           Reach-1         26680         10%         2980.00         134.00         142.26         140.08         141.20         0.004316         10.17         742.52         359.88         0.           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0													
Reach-1 27015 10% 298.00 135.50 141.85 141.85 144.38 0.008857 13.22 278.63 62.97 0.0 Reach-1 27015 2% 5840.00 135.50 145.62 145.62 146.66 0.002172 10.38 1752.24 879.80 0.0 Reach-1 27015 1% 7455.00 135.50 146.08 146.08 147.18 0.002399 11.26 2163.67 894.64 0.0 Reach-1 27015 0.2% 12505.00 135.50 147.11 147.11 148.43 0.003090 13.64 3099.86 927.52 0.0 Reach-1 26800 10% 2980.00 134.00 140.25 140.08 141.20 0.004316 10.17 742.52 359.88 0.0 Reach-1 26680 2% 5840.00 134.00 142.16 142.88 0.003007 10.34 1642.30 560.63 0.0 Reach-1 26680 1% 7455.00 134.00 142.89 143.57 0.002787 10.60 2063.23 590.00 0.0 Reach-1 26680 0.2% 12505.00 134.00 145.43 145.86 0.001574 9.53 3920.70 759.51 0.0 Reach-1 266209 10% 2980.00 133.40 140.59 140.59 140.63 0.000247 1.94 2566.09 865.64 0.0 Reach-1 26209 10% 2980.00 133.40 142.35 142.41 0.000238 2.43 4171.02 944.15 0.0 Reach-1 26209 1% 7455.00 133.40 143.04 143.12 0.000252 2.70 4826.43 949.44 0.0 Reach-1 26209 1.6 2980.00 130.20 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 144.97 142.59 145.41 0.000283 8.59 4476.35 760.00 0.0 Reach-1 26136 0.2% 12505.00 130.20 144.17 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 2980.00 130.20 144.97 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0	Reacn-1	27025	0.2%	12505.00	135.50	147.33	147.10	148.46	0.002654	12.81	3304.65	934.56	0.67
Reach-1 27015 10% 298.00 135.50 141.85 141.85 144.38 0.008857 13.22 278.63 62.97 0.0 Reach-1 27015 2% 5840.00 135.50 145.62 145.62 146.66 0.002172 10.38 1752.24 879.80 0.0 Reach-1 27015 1% 7455.00 135.50 146.08 146.08 147.18 0.002399 11.26 2163.67 894.64 0.0 Reach-1 27015 0.2% 12505.00 135.50 147.11 147.11 148.43 0.003090 13.64 3099.86 927.52 0.0 Reach-1 26800 10% 2980.00 134.00 140.25 140.08 141.20 0.004316 10.17 742.52 359.88 0.0 Reach-1 26680 2% 5840.00 134.00 142.16 142.88 0.003007 10.34 1642.30 560.63 0.0 Reach-1 26680 1% 7455.00 134.00 142.89 143.57 0.002787 10.60 2063.23 590.00 0.0 Reach-1 26680 0.2% 12505.00 134.00 145.43 145.86 0.001574 9.53 3920.70 759.51 0.0 Reach-1 266209 10% 2980.00 133.40 140.59 140.59 140.63 0.000247 1.94 2566.09 865.64 0.0 Reach-1 26209 10% 2980.00 133.40 142.35 142.41 0.000238 2.43 4171.02 944.15 0.0 Reach-1 26209 1% 7455.00 133.40 143.04 143.12 0.000252 2.70 4826.43 949.44 0.0 Reach-1 26209 1.6 2980.00 130.20 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 144.97 142.59 145.41 0.000283 8.59 4476.35 760.00 0.0 Reach-1 26136 0.2% 12505.00 130.20 144.17 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 2980.00 130.20 144.97 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0													
Reach-1 27015 10% 298.00 135.50 141.85 141.85 144.38 0.008857 13.22 278.63 62.97 0.0 Reach-1 27015 2% 5840.00 135.50 145.62 145.62 146.66 0.002172 10.38 1752.24 879.80 0.0 Reach-1 27015 1% 7455.00 135.50 146.08 146.08 147.18 0.002399 11.26 2163.67 894.64 0.0 Reach-1 27015 0.2% 12505.00 135.50 147.11 147.11 148.43 0.003090 13.64 3099.86 927.52 0.0 Reach-1 26680 10% 2980.00 134.00 140.25 140.08 141.20 0.004316 10.17 742.52 359.88 0.0 Reach-1 26680 2% 5840.00 134.00 142.16 142.88 0.003007 10.34 1642.30 560.63 0.0 Reach-1 26680 1% 7455.00 134.00 142.89 143.57 0.002787 10.60 2063.23 590.00 0.0 Reach-1 26680 0.2% 12505.00 134.00 145.43 145.86 0.001574 9.53 3920.70 759.51 0.0 Reach-1 26680 0.2% 5840.00 133.40 144.59 140.69 140.63 0.000247 1.94 2566.09 865.64 0.0 Reach-1 26209 10% 2980.00 133.40 142.35 142.41 0.000238 2.43 4171.02 944.15 0.0 Reach-1 26209 1% 7455.00 133.40 143.04 143.12 0.000252 2.70 4826.43 949.44 0.0 Reach-1 26209 12% 5840.00 133.40 145.45 145.54 0.000216 3.09 7137.65 967.83 0.0 Reach-1 26209 1.0% 2980.00 133.40 143.04 143.12 0.000252 2.70 4826.43 949.44 0.0 Reach-1 26209 1.0% 2980.00 130.20 143.04 143.65 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 2980.00 130.20 141.38 140.68 142.16 0.001499 9.14 1847.30 666.49 0.0 Reach-1 26136 10% 7455.00 130.20 144.17 142.59 145.41 0.000283 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 2980.00 130.20 144.19 142.59 145.41 0.000283 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 7455.00 130.20 144.19 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 2980.00 130.20 144.19 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 7455.00 130.20 144.19 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 7455.00 130.20 144.19 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0 Reach-1 26136 10% 7455.00 130.20 144.19 142.59 145.41 0.000893 8.59 4476.35 760.00 0.0	Reach-1	27020		Bridge									1
Reach-1         27015         2%         5840.00         135.50         145.62         145.62         146.66         0.002172         10.38         1752.24         879.80         0.3           Reach-1         27015         1%         7455.00         135.50         146.08         147.18         0.002399         11.26         2163.67         894.64         0.0           Reach-1         27015         0.2%         12505.00         135.50         147.11         147.11         147.11         148.43         0.003090         13.64         3099.86         927.52         0.0           Reach-1         26880         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.0           Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         0.2%         12505.00         134.00         145.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26209         10%         2980.00         133.40 <td></td>													
Reach-1         27015         2%         5840.00         135.50         145.62         145.62         146.66         0.002172         10.38         1752.24         879.80         0.3           Reach-1         27015         1%         7455.00         135.50         146.08         147.18         0.002399         11.26         2163.67         894.64         0.0           Reach-1         27015         0.2%         12505.00         135.50         147.11         147.11         147.11         148.43         0.003090         13.64         3099.86         927.52         0.0           Reach-1         26880         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.0           Reach-1         26880         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         0.2%         12505.00         133.40 <td>Peach 1</td> <td>27015</td> <td>10%</td> <td>2000.00</td> <td>125 FA</td> <td>1/1 05</td> <td>1/1 05</td> <td>144 20</td> <td>0.006057</td> <td>12.22</td> <td>270 62</td> <td>62.07</td> <td>0.97</td>	Peach 1	27015	10%	2000.00	125 FA	1/1 05	1/1 05	144 20	0.006057	12.22	270 62	62.07	0.97
Reach-1         27015         1%         7455.00         135.50         146.08         147.18         0.002399         11.26         2163.67         894.64         0.1           Reach-1         27015         0.2%         12505.00         135.50         147.11         147.11         148.43         0.003090         13.64         3099.86         927.52         0.1           Reach-1         26680         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.1           Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.1           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         10%         7455.00         133.40         140.59         140.63         0.00247         1.94         2566.09         865.64         0.           Reach-1         26209         1%         5840.00         133.40         142.55         142.41													
Reach-1         27015         0.2%         12505.00         135.50         147.11         147.11         148.43         0.003090         13.64         3099.86         927.52         0.00000           Reach-1         26680         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.00000           Reach-1         26680         2%         5840.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.00000           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.00000           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.00000           Reach-1         26209         10%         2980.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.00000           Reach-1         26209         1%         7455.00         133.40         145.45													0.59
Reach-1         26680         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.7           Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.           Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.           Reach-1         26209         1%         7455.00         133.40         145.45         145.54         0.000252	Reach-1					146.08		147.18		11.26	2163.67		0.63
Reach-1         26680         10%         2980.00         134.00         140.25         140.08         141.20         0.004316         10.17         742.52         359.88         0.7           Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.           Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.           Reach-1         26209         1%         7455.00         133.40         145.45         145.54         0.000252	Reach-1	27015	0.2%	12505.00	135.50	147.11	147.11	148.43	0.003090	13.64	3099.86	927.52	0.72
Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.0           Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.0           Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09													
Reach-1         26680         2%         5840.00         134.00         142.16         142.88         0.003007         10.34         1642.30         560.63         0.0           Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.0           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.0           Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.0           Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09	Peach 1	26680	10%	2000.00	124.00	140.05	140.00	141 20	0.004346	10 17	7/10 FO	250.00	0.76
Reach-1         26680         1%         7455.00         134.00         142.89         143.57         0.002787         10.60         2063.23         590.00         0.01           Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.           Reach-1         26209         2%         5840.00         133.40         143.04         143.12         0.000238         2.43         4171.02         944.15         0.           Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.           Reach-1         26136         10%         2980.00         130.20         141.38         140.68         142.16         0.001499							140.08						
Reach-1         26680         0.2%         12505.00         134.00         145.43         145.86         0.001574         9.53         3920.70         759.51         0.0           Reach-1         26209         10%         2980.00         133.40         140.59         140.63         0.000247         1.94         2566.09         865.64         0.0           Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         1%         7455.00         133.40         145.45         145.54         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.0           Reach-1         26136         10%         2980.00         130.20         141.38         140.40         0.001266         7.48         832.78         483.49         0.0           Reach-1         26136         1%         7455.00         130.20         141.38         140.68         142.16         0.001499													0.67
Reach-1       26209       10%       2980.00       133.40       140.59       140.63       0.000247       1.94       2566.09       865.64       0.         Reach-1       26209       2%       5840.00       133.40       142.35       142.41       0.000238       2.43       4171.02       944.15       0.         Reach-1       26209       1%       7455.00       133.40       143.04       143.12       0.000252       2.70       4826.43       949.44       0.         Reach-1       26209       0.2%       12505.00       133.40       145.45       145.54       0.000216       3.09       7137.65       967.83       0.         Reach-1       26136       10%       2980.00       130.20       139.70       136.89       140.40       0.001266       7.48       832.78       483.49       0.         Reach-1       26136       2%       5840.00       130.20       141.38       140.68       142.16       0.001499       9.14       1847.30       666.49       0.3         Reach-1       26136       1%       7455.00       130.20       142.10       141.28       142.87       0.001511       9.59       2344.50       703.85       0.0         Reac	Reach-1	26680	1%	7455.00	134.00	142.89		143.57	0.002787	10.60	2063.23	590.00	0.65
Reach-1       26209       10%       2980.00       133.40       140.59       140.63       0.000247       1.94       2566.09       865.64       0.         Reach-1       26209       2%       5840.00       133.40       142.35       142.41       0.000238       2.43       4171.02       944.15       0.         Reach-1       26209       1%       7455.00       133.40       143.04       143.12       0.000252       2.70       4826.43       949.44       0.         Reach-1       26209       0.2%       12505.00       133.40       145.45       145.54       0.000216       3.09       7137.65       967.83       0.         Reach-1       26136       10%       2980.00       130.20       139.70       136.89       140.40       0.001266       7.48       832.78       483.49       0.         Reach-1       26136       2%       5840.00       130.20       141.38       140.68       142.16       0.001499       9.14       1847.30       666.49       0.3         Reach-1       26136       1%       7455.00       130.20       142.10       141.28       142.87       0.001511       9.59       2344.50       703.85       0.0         Reac	Reach-1	26680	0.2%	12505.00	134.00	145.43		145.86	0.001574	9.53	3920.70	759.51	0.51
Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.0           Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.           Reach-1         26136         10%         2980.00         130.20         139.70         136.89         140.40         0.001266         7.48         832.78         483.49         0.           Reach-1         26136         2%         5840.00         130.20         141.38         140.68         142.16         0.001499         9.14         1847.30         666.49         0.3           Reach-1         26136         1%         7455.00         130.20         142.10         141.28         142.87         0.001511         9.59         2344.50         703.85         0.3           Reach-1         26136         0.2%         12505.00         130.20         144.97													
Reach-1         26209         2%         5840.00         133.40         142.35         142.41         0.000238         2.43         4171.02         944.15         0.0           Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.0           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.           Reach-1         26136         10%         2980.00         130.20         139.70         136.89         140.40         0.001266         7.48         832.78         483.49         0.           Reach-1         26136         2%         5840.00         130.20         141.38         140.68         142.16         0.001499         9.14         1847.30         666.49         0.3           Reach-1         26136         1%         7455.00         130.20         142.10         141.28         142.87         0.001511         9.59         2344.50         703.85         0.3           Reach-1         26136         0.2%         12505.00         130.20         144.97	Peach 1	26200	10%	2000.00	122.40	140 50		140.60	0.000047	1.04	2566.00	00E 04	0.47
Reach-1         26209         1%         7455.00         133.40         143.04         143.12         0.000252         2.70         4826.43         949.44         0.           Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.           Reach-1         26136         10%         2980.00         130.20         139.70         136.89         140.40         0.001266         7.48         832.78         483.49         0.           Reach-1         26136         2%         5840.00         130.20         141.38         140.68         142.16         0.001499         9.14         1847.30         666.49         0.           Reach-1         26136         1%         7455.00         130.20         142.10         141.28         142.87         0.001511         9.59         2344.50         703.85         0.           Reach-1         26136         0.2%         12505.00         130.20         144.97         142.59         145.41         0.000893         8.59         4476.35         760.00         0.           Reach-1         26127.5         Bridge         8         139.43 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.17</td></t<>													0.17
Reach-1         26209         0.2%         12505.00         133.40         145.45         145.54         0.000216         3.09         7137.65         967.83         0.           Reach-1         26136         10%         2980.00         130.20         139.70         136.89         140.40         0.001266         7.48         832.78         483.49         0.           Reach-1         26136         2%         5840.00         130.20         141.38         140.68         142.16         0.001499         9.14         1847.30         666.49         0.           Reach-1         26136         1%         7455.00         130.20         142.10         141.28         142.87         0.001511         9.59         2344.50         703.85         0.           Reach-1         26136         0.2%         12505.00         130.20         144.97         142.59         145.41         0.000893         8.59         4476.35         760.00         0.           Reach-1         26127.5         Bridge         8         139.43         0.004828         10.33         305.18         444.27         0.													0.18
Reach-1     26136     10%     2980.00     130.20     139.70     136.89     140.40     0.001266     7.48     832.78     483.49     0.2       Reach-1     26136     2%     5840.00     130.20     141.38     140.68     142.16     0.001499     9.14     1847.30     666.49     0.2       Reach-1     26136     1%     7455.00     130.20     142.10     141.28     142.87     0.001511     9.59     2344.50     703.85     0.3       Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     87.48     832.78     444.27     444.27     0.0       Reach-1     26119     10%     2980.00     131.30     137.79     136.96     139.43     0.004828     10.33     305.18     444.27     0.0	Reach-1	26209	1%	7455.00	133.40	143.04		143.12	0.000252	2.70	4826.43	949.44	0.19
Reach-1     26136     10%     2980.00     130.20     139.70     136.89     140.40     0.001266     7.48     832.78     483.49     0.2       Reach-1     26136     2%     5840.00     130.20     141.38     140.68     142.16     0.001499     9.14     1847.30     666.49     0.2       Reach-1     26136     1%     7455.00     130.20     142.10     141.28     142.87     0.001511     9.59     2344.50     703.85     0.3       Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     87.48     832.78     444.27     444.27     0.0       Reach-1     26119     10%     2980.00     131.30     137.79     136.96     139.43     0.004828     10.33     305.18     444.27     0.0	Reach-1	26209	0.2%	12505.00	133.40	145.45		145.54	0.000216	3.09	7137.65	967.83	0.18
Reach-1     26136     2%     5840.00     130.20     141.38     140.68     142.16     0.001499     9.14     1847.30     666.49     0.0       Reach-1     26136     1%     7455.00     130.20     142.10     141.28     142.87     0.001511     9.59     2344.50     703.85     0.0       Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     Bridge     130.20     130.20     130.20     130.20     130.20     130.20     130.20     130.20     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     130.20     130.20     130.96     130.43     0.004828     10.33     305.18     444.27     0.0										. ,,			
Reach-1     26136     2%     5840.00     130.20     141.38     140.68     142.16     0.001499     9.14     1847.30     666.49     0.0       Reach-1     26136     1%     7455.00     130.20     142.10     141.28     142.87     0.001511     9.59     2344.50     703.85     0.0       Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     Bridge     130.20     130.20     130.20     130.20     130.20     130.20     130.20     130.20     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     130.20     130.20     130.96     130.43     0.004828     10.33     305.18     444.27     0.0	Doort 1	26422	100/	2002.22	400.00	400 70	400.00	440.40	0.001005	- 1-	000 70	400.45	
Reach-1     26136     1%     7455.00     130.20     142.10     141.28     142.87     0.001511     9.59     2344.50     703.85     0.0       Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge       Reach-1     26119     10%     2980.00     131.30     137.79     136.96     139.43     0.004828     10.33     305.18     444.27     0.0													0.44
Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge	Reach-1	26136	2%	5840.00	130.20	141.38		142.16	0.001499	9.14	1847.30	666.49	0.50
Reach-1     26136     0.2%     12505.00     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     8.59     8.59     130.20     130.20     130.20     130.20     144.97     142.59     145.41     0.000893     8.59     4476.35     760.00     0.0       Reach-1     26127.5     Bridge     130.20     130	Reach-1	26136	1%	7455.00	130.20	142.10	141.28	142.87	0.001511	9.59	2344.50	703.85	0.51
Reach-1 26127.5 Bridge Reach-1 26119 10% 2980.00 131.30 137.79 136.96 139.43 0.004828 10.33 305.18 444.27 0.004828 10.30 10.004828 10.00				12505.00						8.59			0.40
Reach-1 26119 10% 2980.00 131.30 137.79 136.96 139.43 0.004828 10.33 305.18 444.27 0.004828		1		000.00	.00.20		2.55		2.000000	3.55		. 55.50	5.40
Reach-1 26119 10% 2980.00 131.30 137.79 136.96 139.43 0.004828 10.33 305.18 444.27 0.004828	Description of	00407.5		5									
	Reach-1	26127.5		Bridge									1
	Reach-1	26119	10%	2980.00	131.30	137.79	136.96	139.43	0.004828	10.33	305.18	444.27	0.76

Reach-1	26119 26119 26058 26058 26058 26058	1% 0.2% 10% 2%	(cfs) 7455.00 12505.00	(ft) 131.30 131.30	(ft) 142.25	(ft) 138.86	(ft)	(ft/ft)	(ft/s) 5.04	(sq ft) 3781.94	(ft) 742.73	2
Reach-1	26058 26058 26058 26058 26058	0.2% 10% 2%			142.25	138.86	440 44	0.000533	5.04	3781 94	742 73	
Reach-1	26058 26058 26058 26058	10%	12505.00	131.30			142.41	0.000532				0.28
Reach-1	26058 26058 26058	2%			145.07	140.05	145.23	0.000420	5.27	5944.93	778.00	0.26
Reach-1	26058 26058 26058	2%										
Reach-1	26058 26058		2980.00	131.30	138.31		138.63	0.001328	5.74	1195.20	506.31	0.41
Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1	26058		5840.00	131.30	141.19		141.36	0.000594	4.95	3010.05	716.41	0.29
Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1		1%	7455.00	131.30	142.21		142.37	0.000543	5.08	3755.15	742.11	0.28
Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1	05050	0.2%	12505.00	131.30	145.04		145.20	0.000425	5.29	5923.49	778.00	0.26
Reach-1 Reach-1 Reach-1 Reach-1 Reach-1 Reach-1		400/	2000.00	404.00	407.00		407.70	0.000000	F 07	4404.40	400.70	0.00
Reach-1 Reach-1 Reach-1 Reach-1 Reach-1	25358 25358	10%	2980.00 5840.00	131.00 131.00	137.60 140.82		137.79 140.96	0.000999	5.37 5.16	1424.10 2872.39	432.76 468.02	0.38 0.29
Reach-1 Reach-1 Reach-1	25358	1%	7455.00	131.00	141.83		141.99	0.000552	5.61	3360.84	499.89	0.30
Reach-1 Reach-1 Reach-1	25358	0.2%	12505.00	131.00	144.68		144.87	0.000522	6.39	5088.72	636.70	0.31
Reach-1 Reach-1	20000	0.270	12000.00	101.00				0.000022	0.00	0000.72	000.70	0.01
Reach-1 Reach-1	25340	10%	2980.00	128.10	137.58		137.77	0.000473	4.58	1994.04	375.83	0.27
	25340	2%	5840.00	128.10	140.68		140.94	0.000504	5.76	3250.24	506.40	0.29
Reach-1	25340	1%	7455.00	128.10	141.64		141.96	0.000587	6.55	3740.65	512.66	0.32
1 todon 1	25340	0.2%	12505.00	128.10	144.36		144.83	0.000718	8.22	5237.84	696.11	0.37
Reach-1	25334	10%	2980.00	130.31	137.63		137.75	0.000522	3.87	1572.58	347.27	0.27
Reach-1	25334	2%	5840.00	130.31	140.75		140.90	0.000405	4.43	2715.70	411.08	0.25
Reach-1	25334	1%	7455.00	130.31	141.74		141.92	0.000444	4.96	3149.10	457.22	0.27
Reach-1	25334	0.2%	12505.00	130.31	144.51		144.76	0.000483	6.04	4441.00	475.13	0.29
			$\vdash$									
Reach-1	24975	10%	2980.00	129.20	135.57	135.57	137.16	0.005532	10.62	402.65	172.24	0.83
Reach-1	24975	2%	5840.00	129.20	139.83		140.59	0.001521	8.36	1283.40	362.15	0.48
Reach-1	24975	1%	7455.00	129.20	140.90		141.61	0.001359	8.49	1683.39	414.42	0.46
Reach-1	24975	0.2%	12505.00	129.20	144.14		144.54	0.000656	7.07	3094.75	445.51	0.34
Decel 4	04000	400/	2000.00	407.00	405 50		400.00	0.000404	7.70	550.70	455.00	0.55
Reach-1	24922 24922	10%	2980.00 5840.00	127.89	135.50 139.90		136.32 140.47	0.002194	7.76 7.14	556.72	155.93 374.77	0.55 0.38
Reach-1	24922	1%	7455.00	127.89 127.89	140.97		141.50	0.000917 0.000829	7.14	1431.97 1850.23	441.04	0.36
Reach-1	24922	0.2%	12505.00	127.89	144.18		144.49	0.000829	6.01	3438.02	506.44	0.37
TCGCII-1	24322	0.270	12303.00	127.03	144.10		144.45	0.000413	0.01	3430.02	300.44	0.27
Reach-1	24677	10%	2980.00	127.87	135.59		135.88	0.000688	4.52	855.68	167.98	0.31
Reach-1	24677	2%	5840.00	127.87	139.95		140.24	0.000405	4.83	1817.72	331.75	0.25
Reach-1	24677	1%	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24677	0.2%	12505.00	127.87	143.91		144.36	0.000485	6.46	3377.85	405.00	0.29
Reach-1	24620	10%	2980.00	128.90	134.41	133.97	135.69	0.005035	9.23	402.42	166.53	0.77
Reach-1	24620	2%	5840.00	128.90	139.56		140.17	0.001035	6.96	1443.21	273.89	0.40
Reach-1	24620	1%	7455.00	128.90	140.48		141.22	0.001143	7.78	1737.87	369.05	0.42
Reach-1	24620	0.2%	12505.00	128.90	143.60		144.30	0.000901	8.22	3001.58	410.00	0.39
Reach-1	24597	10%	2980.00	127.30	134.90		135.41	0.001279	5.88	709.79	201.22	0.40
Reach-1	24597	2%	5840.00	127.30	139.69		140.09	0.000572	5.66	1863.48	322.73	0.30
Reach-1	24597	1%	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-1	24597	0.2%	12505.00	127.30	143.74		144.22	0.000567	6.91	3499.24	421.00	0.31
Reach-1	24570	10%	2980.00	127.60	134.33	132.31	135.31	0.002228	7.94	375.39	104.89	0.56
Reach-1	24570	2%	5840.00	127.60	138.87	134.73	140.00	0.001290	8.69	958.27	316.33	0.47
Reach-1	24570	1%	7455.00	127.60	139.43	135.90	140.99	0.001698 0.001176	10.31	1145.22	348.43	0.54 0.47
Reach-1	24570	0.2%	12505.00	127.60	142.91	140.91	144.13	0.001170	10.26	3114.93	807.05	0.47
Reach-1	24542.5		Bridge									
	2.0.2.0		Dilage									
Reach-1	24540	10%	2980.00	127.60	134.18		135.21	0.002423	8.14	366.09	101.22	0.58
Reach-1	24540	2%	5840.00	127.60	137.37	134.72	139.01	0.002223	10.32	679.47	187.99	0.60
Reach-1	24540	1%	7455.00	127.60	138.19	135.88	140.32	0.002630	11.88	844.91	232.45	0.66
Reach-1	24540	0.2%	12505.00	127.60	142.97	140.68	144.09	0.001107	9.98	3240.15	809.73	0.46
Reach-1	24485	10%	2980.00	126.30	133.05		134.80	0.004960	10.97	339.74	65.99	0.79
Reach-1	24485	2%	5840.00	126.30	135.42	135.42	138.41	0.006522	14.55	576.27	136.90	0.94
Reach-1	24485	1%	7455.00	126.30	136.91	136.91	139.86	0.005771	14.75	837.67	207.98	0.90
Reach-1	24485	0.2%	12505.00	126.30	139.57	139.57	143.21	0.005456	17.09	1473.62	250.14	0.92
Reach-1	24430	10%	2980.00	126.60	133.65		134.19	0.004131	5.91	504.51	89.39	0.44
Reach-1	24430	2%	5840.00	126.60	136.49		137.13	0.003507	6.76	1121.38	251.35	0.41
Reach-1	24430	1%	7455.00	126.60	137.85		138.46	0.002969	6.88	1464.10	254.64	0.39
Reach-1	24430	0.2%	12505.00	126.60	140.49		141.28	0.002984	8.11	2145.07	261.05	0.41
				,	,							
Reach-1	24401	10%	2980.00	124.66	133.66		134.04	0.003118	4.88	610.18	102.03	0.35
Reach-1	24401	2%	5840.00	124.66	136.40		137.02	0.003389	6.39	985.38	198.56	0.39
Reach-1	24401	1%	7455.00	124.66	137.67		138.37	0.003234	6.86	1278.84	257.49	0.39
Reach-1	24401	0.2%	12505.00	124.66	140.31		141.18	0.003245	8.07	2049.16	332.83	0.41
	0.405.	100/										
Reach-1	24381	10%	2980.00	124.66	133.34		133.96	0.001781	7.05	527.73	91.46	0.49

Reach	River Sta	Profile	Q Total	1 (Continued) Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	24381	2%	5840.00	124.66	135.78		136.91	0.002413	9.59	770.10	118.58	0.59
Reach-1	24381	1%	7455.00	124.66	136.85		138.24	0.002563	10.71	931.57	185.57	0.62
Reach-1	24381	0.2%	12505.00	124.66	139.22	137.46	141.03	0.002745	12.89	1531.13	330.29	0.66
Reach-1	24180	10%	2980.00	124.70	133.06		133.61	0.001495	5.98	502.38	92.91	0.44
Reach-1	24180	2%	5840.00	124.70	135.48		136.44	0.001803	7.95	844.89	259.49	0.51
Reach-1	24180	1%	7455.00	124.70	136.78	133.49	137.70	0.001560	8.02	1209.32	290.98	0.48
Reach-1	24180	0.2%	12505.00	124.70	139.53	136.93	140.38	0.001281	8.35	2316.16	451.50	0.45
Reach-1	24105	10%	2980.00	124.80	132.53		133.42	0.003018	7.59	392.78	80.10	0.60
Reach-1	24105	2%	5840.00	124.80	134.54		136.18	0.004147	10.27	570.55	100.04	0.73
Reach-1	24105	1%	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reach-1	24105	0.2%	12505.00	124.80	137.64	137.25	140.07	0.003869	12.93	1098.93	201.62	0.76
Reach-1	23805	10%	2980.00	124.00	132.40		132.79	0.001004	5.69	1165.28	312.50	0.38
Reach-1	23805	2%	5840.00	124.00	134.69		135.27	0.001156	7.36	2038.14	469.70	0.42
Reach-1	23805	1%	7455.00	124.00	135.70		136.34	0.001191	7.99	2548.56	544.98	0.44
Reach-1	23805	0.2%	12505.00	124.00	138.21		138.97	0.001211	9.31	4063.59	641.58	0.46
Doosh 1	22445	100/	2000.00	122.00	120.01	120.01	121.02	0.006006	11.00	404.45	161 55	0.00
Reach-1	23415 23415	10%	2980.00 5840.00	123.00 123.00	129.81 132.27	129.81 132.27	131.82 134.30	0.006096 0.004596	11.90 13.19	404.45 1159.47	161.55 343.43	0.89
Reach-1	23415	1%	7455.00	123.00	133.11	133.11	135.33	0.004390	14.27	1451.84	358.59	0.84
Reach-1	23415	0.2%	12505.00	123.00	135.11	135.11	137.89	0.005069	16.96	2245.13	422.31	0.04
Reach-1	23171	10%	2980.00	120.30	128.75		129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2%	5840.00	120.30	129.79	129.12	131.57	0.005575	10.79	599.24	177.93	0.81
Reach-1	23171	1%	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23171	0.2%	12505.00	120.30	134.35		135.16	0.001732	7.84	1880.08	333.29	0.44
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	1%	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	23036	0.2%	12505.00	121.70	134.55		134.98	0.000237	3.32	2572.37	391.51	0.18
Reach-1	22916	10%	2980.00	121.00	128.01	126.93	128.88	0.002603	8.01	570.82	302.03	0.57
Reach-1	22916	2%	5840.00	121.00	130.41		130.84	0.000999	6.20	1483.60	430.42	0.38
Reach-1	22916	1%	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Reach-1	22765	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	2%	5840.00	114.20	130.48		130.70	0.000299	3.96	2020.14	395.39	0.19
Reach-1	22765	1%	7455.00	114.20	131.64		131.87	0.000301	4.19	2548.37	511.91	0.19
Reach-1	22765	0.2%	12505.00	114.20	134.64		134.84	0.000240	4.22	4324.67	669.64	0.17
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27	124.70	130.51	0.000142	4.56	1791.09	483.52	0.46
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
Reach-1	22140	10%	2980.00	117.00	124.05	124.05	126.26	0.006734	12.84	391.36	132.65	0.95
Reach-1	22140	2%	5840.00	117.00	126.77	126.77	129.42	0.005440	14.96	889.23	205.48	0.91
Reach-1	22140	1%	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
Reach-1	21825	10%	2980.00	115.90	121.80	121.75	123.65	0.007981	11.17	314.54	84.21	0.97
Reach-1	21825	2%	5840.00	115.90	121.60	121.75	126.73	0.007961	13.42	604.08	179.14	0.97
Reach-1	21825	1%	7455.00	115.90	125.26	125.26	128.03	0.005781	14.07	847.23	239.90	0.91
Reach-1	21825	0.2%	12505.00	115.90	131.24	127.79	132.45	0.001436	10.39	3430.35	1045.30	0.50
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.97	0.002174	7.62	390.83	103.38	0.55
Reach-1	21770	2%	5840.00	115.40	124.17	120.06	126.07	0.002174	11.07	527.79	119.93	0.53
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Reach-1	21757.5		Bridge									
cuon-1	21101.3		Bridge									
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach-1	21745	1%	7455.00	115.40	124.48	123.47	127.36	0.004410	13.60	547.97	122.37	0.83
Reach-1	21745	0.2%	12505.00	115.40	126.94	126.53	131.79	0.005288	17.67	707.72	141.67	0.94
Reach-1	21695	10%	2980.00	114.20	121.74	120.15	122.74	0.003025	8.01	371.94	69.60	0.61
Reach-1	21695	2%	5840.00	114.20	123.69	122.46	125.72	0.004430	11.42	511.32	74.77	0.76
Reach-1	21695	1%	7455.00	114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1	21695	0.2%						0.004531	14.98	1124.07		0.82

HEC-RAS Plan: EXIST River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

# Norwalk River Proposed Conditions Model Output Table

HEC-RAS Plan: PROPOSED River: RIVER-1 Reach: Reach-1

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
D 1.4	20000	100/	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.75
Reach-1	29920	10%	2980.00	147.00	152.32	152.32	153.29	0.004454	9.23	671.47	438.66	0.75
Reach-1	29920	2%	5840.00	147.00	153.56	153.56	154.60	0.004481	10.83	1400.71	673.09	0.79
Reach-1	29920	1%	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86	1676.50	693.44	0.83
Reach-1	29920	0.2%	12505.00	147.00	154.99	154.99	156.40	0.005722	14.14	2414.85	738.35	0.92
Reach-1	29760	10%	2980.00	142.20	148.53		149.01	0.001498	5.62	583.07	179.68	0.44
Reach-1	29760	2%	5840.00	142.20	151.31		151.93	0.001498	6.63	1125.96	211.79	0.44
Reach-1	29760	1%	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	29760	0.2%	12505.00	142.20	154.28		155.51	0.001589	9.59	1814.00	255.42	0.51
Decel 4	00040	400/	2000.00	400.00	445.00		440.00	0.000005	7.00	450.44	450.00	0.54
Reach-1	28240	10%	2980.00	138.00	145.39	110.50	146.33	0.002035	7.92	453.14	156.69	0.54
Reach-1	28240	2%	5840.00	138.00	146.52	146.52	148.75	0.004139	12.55	696.60	258.98	0.79
Reach-1	28240	1%	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	28240	0.2%	12505.00	138.00	149.76	149.76	151.98	0.003397	14.32	1979.91	552.23	0.76
Decel 4	20000	400/	2000.00	400.00	440.00		440.04	0.000055	4.50	4440.00	705 50	0.00
Reach-1	28020	10%	2980.00	136.33	146.00		146.01	0.000055	1.53	4419.69	705.50	0.09
Reach-1	28020	2%	5840.00	136.33	147.00		147.04	0.000130	2.53	5181.72	802.47	0.14
Reach-1	28020	1%	7455.00	136.33	147.55		147.59	0.000163	2.94	5632.11	838.83	0.16
Reach-1	28020	0.2%	12505.00	136.33	148.89		148.97	0.000246	3.92	6797.17	892.67	0.20
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Reach-1	27930	10%	2980.00	135.65	146.00		146.01	0.000049	1.51	4606.87	734.08	0.09
Reach-1	27930	2%	5840.00	135.65	146.99		147.02	0.000116	2.50	5386.72	818.88	0.14
Reach-1	27930	1%	7455.00	135.65	147.54		147.58	0.000146	2.90	5847.71	863.80	0.16
Reach-1	27930	0.2%	12505.00	135.65	148.87		148.94	0.000221	3.85	7100.18	1055.04	0.20
Reach-1	27830	10%	2980.00	134.60	145.99		146.00	0.000041	1.44	4845.93	788.10	0.08
Reach-1	27830	2%	5840.00	134.60	146.99		147.01	0.000096	2.34	5676.92	876.39	0.13
Reach-1	27830	1%	7455.00	134.60	147.53		147.57	0.000120	2.70	6166.04	914.94	0.14
Reach-1	27830	0.2%	12505.00	134.60	148.86		148.92	0.000180	3.57	7478.45	1102.15	0.18
Reach-1	27790	10%	2980.00	134.60	145.99		146.00	0.000039	1.40	4934.34	818.72	0.08
Reach-1	27790	2%	5840.00	134.60	146.98		147.01	0.000089	2.25	5799.61	916.21	0.12
Reach-1	27790	1%	7455.00	134.60	147.53		147.56	0.000109	2.58	6306.18	946.93	0.14
Reach-1	27790	0.2%	12505.00	134.60	148.85		148.92	0.000161	3.38	7600.04	999.96	0.17
Reach-1	21190	0.276	12303.00	134.00	140.03		140.92	0.000101	3.30	7000.04	999.90	0.17
Reach-1	27468	10%	2980.00	132.10	145.99		145.99	0.000005	0.60	9140.64	793.45	0.03
	_	2%						0.000017				
Reach-1	27468		5840.00	132.10	146.99		146.99		1.11	9943.03	813.12	0.05
Reach-1	27468	1%	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	27468	0.2%	12505.00	132.10	148.85		148.88	0.000052	2.13	11529.28	890.79	0.10
D 1.4	07440	100/	2000.00	400.00	115.07		445.00	2 222224	4.74	1705 50	000.40	0.40
Reach-1	27110	10%	2980.00	136.60	145.97		145.99	0.000064	1.74	4765.52	962.48	0.10
Reach-1	27110	2%	5840.00	136.60	146.94		146.97	0.000148	2.83	5707.19	991.44	0.16
Reach-1	27110	1%	7455.00	136.60	147.46		147.51	0.000187	3.29	6234.70	1005.58	0.18
Reach-1	27110	0.2%	12505.00	136.60	148.74		148.82	0.000304	4.52	7518.38	1009.50	0.23
Reach-1	27025	10%	2980.00	135.50	145.63	141.84	145.90	0.000562	5.28	1759.35	880.05	0.30
Reach-1	27025	2%	5840.00	135.50	145.74	145.59	146.68	0.001965	9.96	1855.68	883.55	0.56
Reach-1	27025	1%	7455.00	135.50	146.24	146.03	147.20	0.002112	10.68	2304.78	899.67	0.59
Reach-1	27025	0.2%	12505.00	135.50	147.33	147.10	148.46	0.002654	12.81	3304.65	934.56	0.67
Reach-1	27020		Bridge									
												<u> </u>
Reach-1	27015	10%	2980.00	135.50	141.85	141.85	144.38	0.006857	13.22	278.63	62.97	0.97
Reach-1	27015	2%	5840.00	135.50	145.62	145.62	146.66	0.002172	10.38	1752.24	879.80	0.59
Reach-1	27015	1%	7455.00	135.50	146.08	146.08	147.18	0.002399	11.26	2163.67	894.64	0.63
Reach-1	27015	0.2%	12505.00	135.50	147.11	147.11	148.43	0.003090	13.64	3099.86	927.52	0.72
Reach-1	26680	10%	2980.00	134.00	140.25	140.08	141.20	0.004316	10.17	742.52	359.88	0.76
Reach-1	26680	2%	5840.00	134.00	142.16		142.88	0.003007	10.34	1642.30	560.63	0.67
Reach-1	26680	1%	7455.00	134.00	142.89		143.57	0.002787	10.60	2063.23	590.00	0.65
Reach-1	26680	0.2%	12505.00	134.00	145.43		145.86	0.001574	9.53	3920.70	759.51	0.51
Reach-1	26209	10%	2980.00	133.40	140.59		140.63	0.000247	1.94	2566.09	865.64	0.17
Reach-1	26209	2%	5840.00	133.40	142.35		142.41	0.000238	2.43	4171.02	944.15	0.18
Reach-1	26209	1%	7455.00	133.40	143.04		143.12	0.000252	2.70	4826.43	949.44	0.19
Reach-1	26209	0.2%	12505.00	133.40	145.45		145.54	0.000232	3.09	7137.65	967.83	0.18
ouoii i		0.2,3	.2000.00	100.40	1-1010		140.04	5.500£10	0.00	. 107.00	507.55	0.10
Reach-1	26136	10%	2980.00	130.20	139.70	136.89	140.40	0.001266	7.48	832.78	483.49	0.44
Reach-1	26136	2%	5840.00	130.20	141.38	140.68	142.16	0.001266	9.14	1847.30	666.49	0.44
Reach-1	26136	1%	7455.00						9.14			
				130.20	142.10	141.28	142.87	0.001511		2344.50	703.85	0.51
Reach-1	26136	0.2%	12505.00	130.20	144.97	142.59	145.41	0.000893	8.59	4476.35	760.00	0.40
Deart 1	26407.5		B.:									
Reach-1	26127.5		Bridge									
												-
Reach-1	26119	10%	2980.00	131.30	137.79	136.96	139.43	0.004828	10.33	305.18	444.27	0.76
Reach-1	26119	2%	5840.00	131.30	141.23	138.61	141.40	0.000580	4.90	3038.66	718.58	0.29

HEC-RAS Plan: PROPOSED River: RIVER-1 Reach: Reach-1 (Continued)

			ER-1 Reach: F									
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
		101	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	26119	1%	7455.00	131.30	142.25	138.86	142.41	0.000532	5.04	3781.94	742.73	0.28
Reach-1	26119	0.2%	12505.00	131.30	145.07	140.05	145.23	0.000420	5.27	5944.93	778.00	0.26
D 1.4	00050	100/	2000.00	101.00	100.01		100.00	0.004000	5.74	1105.00	500.04	0.44
Reach-1	26058	10%	2980.00	131.30	138.31		138.63	0.001328	5.74	1195.20	506.31	0.41
Reach-1	26058	2%	5840.00	131.30	141.19		141.36	0.000594 0.000543	4.95	3010.05	716.41	0.29
Reach-1	26058	1%	7455.00	131.30	142.21		142.37		5.08	3755.15	742.11	0.28
Reach-1	26058	0.2%	12505.00	131.30	145.04		145.20	0.000425	5.29	5923.49	778.00	0.26
D 1.4	05050	100/	2000.00	101.00	107.00		107.70	0.00000	5.07	110110	400.70	2.00
Reach-1	25358	10%	2980.00	131.00	137.60		137.79	0.000999	5.37	1424.10	432.76	0.38
Reach-1	25358	2%	5840.00	131.00	140.82		140.96	0.000534	5.16	2872.39	468.02	0.29
Reach-1	25358	1%	7455.00	131.00	141.83		141.99	0.000552	5.61	3360.84	499.89	0.30
Reach-1	25358	0.2%	12505.00	131.00	144.68		144.87	0.000522	6.39	5088.72	636.70	0.31
D 1.4	05040	100/	2000.00	100.10	107.50		107.77	0.000470	4.50	100101	075.00	2.00
Reach-1	25340	10%	2980.00	128.10	137.58		137.77	0.000473	4.58	1994.04	375.83	0.27
Reach-1	25340	2%	5840.00	128.10	140.68		140.94	0.000504	5.76	3250.24	506.40	0.29
Reach-1	25340	1%	7455.00	128.10	141.64		141.96	0.000587	6.55	3740.65	512.66	0.32
Reach-1	25340	0.2%	12505.00	128.10	144.36		144.83	0.000718	8.22	5237.84	696.11	0.37
Decel 4	05004	400/	2000.00	400.04	407.00		407.75	0.000500	0.07	4570.50	0.47.07	0.07
Reach-1	25334	10%	2980.00	130.31	137.63		137.75	0.000522	3.87	1572.58	347.27	0.27
Reach-1	25334	2%	5840.00	130.31	140.75		140.90	0.000405	4.43	2715.70	411.08	0.25
Reach-1	25334	1%	7455.00	130.31	141.74		141.92	0.000444	4.96	3149.10	457.22	0.27
Reach-1	25334	0.2%	12505.00	130.31	144.51		144.76	0.000483	6.04	4441.00	475.13	0.29
Dec 1 1	04075	400/	2005	40	10	10	40	0.00====		100.0-		
Reach-1	24975	10%	2980.00	129.20	135.57	135.57	137.16	0.005532	10.62	402.65	172.24	0.83
Reach-1	24975	2%	5840.00	129.20	139.83		140.59	0.001521	8.36	1283.40	362.15	0.48
Reach-1	24975	1%	7455.00	129.20	140.90		141.61	0.001359	8.49	1683.39	414.42	0.46
Reach-1	24975	0.2%	12505.00	129.20	144.14		144.54	0.000656	7.07	3094.75	445.51	0.34
D	04005	100/										
Reach-1	24922	10%	2980.00	127.89	135.50		136.32	0.002194	7.76	556.72	155.93	0.55
Reach-1	24922	2%	5840.00	127.89	139.90		140.47	0.000917	7.14	1431.97	374.77	0.38
Reach-1	24922	1%	7455.00	127.89	140.97		141.50	0.000829	7.23	1850.23	441.04	0.37
Reach-1	24922	0.2%	12505.00	127.89	144.18		144.49	0.000415	6.01	3438.02	506.44	0.27
Reach-1	24677	10%	2980.00	127.87	135.59		135.88	0.000688	4.52	855.68	167.98	0.31
Reach-1	24677	2%	5840.00	127.87	139.95		140.24	0.000405	4.83	1817.72	331.75	0.25
Reach-1	24677	1%	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24677	0.2%	12505.00	127.87	143.91		144.36	0.000485	6.46	3377.85	405.00	0.29
Reach-1	24620	10%	2980.00	128.90	134.41	133.97	135.69	0.005035	9.23	402.42	166.53	0.77
Reach-1	24620	2%	5840.00	128.90	139.56		140.17	0.001035	6.96	1443.21	273.89	0.40
Reach-1	24620	1%	7455.00	128.90	140.48		141.22	0.001143	7.78	1737.87	369.05	0.42
Reach-1	24620	0.2%	12505.00	128.90	143.60		144.30	0.000901	8.22	3001.58	410.00	0.39
Reach-1	24597	10%	2980.00	127.30	134.90		135.41	0.001279	5.88	709.79	201.22	0.40
Reach-1	24597	2%	5840.00	127.30	139.69		140.09	0.000572	5.66	1863.48	322.73	0.30
Reach-1	24597	1%	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-1	24597	0.2%	12505.00	127.30	143.74		144.22	0.000567	6.91	3499.24	421.00	0.31
Reach-1	24570	10%	2980.00	127.60	134.33	132.31	135.31	0.002228	7.94	375.39	104.89	0.56
Reach-1	24570	2%	5840.00	127.60	138.87	134.73	140.00	0.001290	8.69	958.27	316.33	0.47
Reach-1	24570	1%	7455.00	127.60	139.43	135.90	140.99	0.001698	10.31	1145.22	348.43	0.54
Reach-1	24570	0.2%	12505.00	127.60	142.91	140.91	144.13	0.001176	10.26	3114.93	807.05	0.47
Pooch 4	24542.5		D-: -I-									
Reach-1	24542.5		Bridge									
Reach-1	24540	10%	2980.00	127.60	134.18		135.21	0.002423	8.14	366.09	101.22	0.58
Reach-1	24540	2%	5840.00	127.60	134.18	134.72	135.21	0.002423	10.32	679.47	187.99	0.60
Reach-1	24540	1%	7455.00	127.60	137.37	134.72	140.32	0.002223	11.88	844.91	232.45	0.66
Reach-1	24540	0.2%	12505.00	127.60	138.19	135.88	144.09	0.002630	9.98	3240.15	809.73	0.46
rveatti-1	24340	U.Z /0	12005.00	127.00	142.97	140.08	144.09	0.001107	9.98	3∠40.15	609.73	0.46
Reach-1	24485	10%	2980.00	126.30	133.05		134.80	0.004960	10.97	339.74	65.99	0.79
Reach-1	24485	2%	5840.00	126.30		135.42	134.80	0.004960				0.79
Reach-1		1%			135.42				14.55	576.27	136.90	0.94
Reach-1	24485 24485	0.2%	7455.00 12505.00	126.30 126.30	136.91 139.57	136.91 139.57	139.86 143.21	0.005771 0.005456	14.75 17.09	837.67 1473.62	207.98 250.14	0.90
reach-1	24400	U.Z /0	12303.00	120.30	139.57	138.37	143.21	0.005456	17.09	14/3.02	200.14	0.92
Reach-1	24430	10%	2980.00	126.60	133.65		134.19	0.004131	5.91	504.51	89.39	0.44
Reach-1	24430	2%	5840.00	126.60	133.65		134.19	0.004131	6.76	1121.38	251.35	0.44
Reach-1	24430	1%	7455.00	126.60	136.49		137.13	0.003507	6.88	1464.10	251.35	0.41
Reach-1	24430	0.2%	12505.00	126.60	140.49		141.28	0.002989	8.11	2145.07	261.05	0.39
r (cacil-I	24430	J.Z /0	12303.00	120.00	140.49		141.20	0.002904	0.11	≥ 140.07	201.03	0.41
Reach-1	24401	10%	2980.00	124.66	133.66		134.04	0.003118	4.88	610.18	102.03	0.35
Reach-1		2%	5840.00	124.66	133.66		134.04	0.003118	6.39	985.38	102.03	0.39
Reach-1	24401 24401	1%	7455.00	124.66	136.40		137.02	0.003389	6.86	985.38 1278.84	198.56 257.49	0.39
Reach-1	24401	0.2%			140.31				8.07	2049.16	332.83	0.39
reach-1	24401	U.Z /0	12505.00	124.66	140.31		141.18	0.003245	8.07	∠049.16	ა3∠.83	0.41
Donah 4	24204	100/	2000.00	404.00	400.04		400.00	0.004704	7.05	507.70	04.40	0.10
Reach-1	24381	10%	2980.00	124.66	133.34		133.96	0.001781	7.05	527.73	91.46	0.49

HEC-RAS Plan: PROPOSED River: RIVER-1 Reach: Reach-1 (Continued)

			ER-1 Reach: F									
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
Reach-1	24381	2%	(cfs) 5840.00	(ft) 124.66	(ft)	(ft)	(ft) 136.91	(ft/ft) 0.002413	(ft/s) 9.59	(sq ft)	(ft) 118.58	0.59
Reach-1	24381	1%	7455.00	124.66	135.78 136.85		138.24	0.002413	10.71	770.10 931.57	185.57	0.62
Reach-1	24381	0.2%	12505.00	124.66	139.22	137.46	141.03	0.002303	12.89	1531.13	330.29	0.66
i teacii-i	24301	0.270	12303.00	124.00	133.22	137.40	141.03	0.002743	12.03	1331.13	330.23	0.00
Reach-1	24180	10%	2980.00	124.70	133.06		133.61	0.001495	5.98	502.38	92.91	0.44
Reach-1	24180	2%	5840.00	124.70	135.48		136.44	0.001803	7.95	844.89	259.49	0.51
Reach-1	24180	1%	7455.00	124.70	136.78	133.49	137.70	0.001560	8.02	1209.32	290.98	0.48
Reach-1	24180	0.2%	12505.00	124.70	139.53	136.93	140.38	0.001281	8.35	2316.16	451.50	0.45
Reach-1	24105	10%	2980.00	124.80	132.53		133.42	0.003018	7.59	392.78	80.10	0.60
Reach-1	24105	2%	5840.00	124.80	134.54		136.18	0.004147	10.27	570.55	100.04	0.73
Reach-1	24105	1%	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reach-1	24105	0.2%	12505.00	124.80	137.64	137.25	140.07	0.003869	12.93	1098.93	201.62	0.76
Reach-1	23805	10%	2980.00	124.00	132.40		132.79	0.001004	5.69	1105.00	312.50	0.38
Reach-1	23805	2%	5840.00	124.00	134.69		135.27	0.001004	7.36	1165.28 2038.14	469.70	0.42
Reach-1	23805	1%	7455.00	124.00	135.70		136.34	0.001130	7.99	2548.56	544.98	0.44
Reach-1	23805	0.2%	12505.00	124.00	138.21		138.97	0.001191	9.31	4063.59	641.58	0.44
Neach-1	23603	0.276	12303.00	124.00	130.21		130.97	0.001211	9.51	4003.39	041.30	0.40
Reach-1	23415	10%	2980.00	123.00	129.81	129.81	131.82	0.006096	11.90	404.45	161.55	0.89
Reach-1	23415	2%	5840.00	123.00	132.27	132.27	134.30	0.004596	13.19	1159.47	343.43	0.82
Reach-1	23415	1%	7455.00	123.00	133.11	133.11	135.33	0.004719	14.27	1451.84	358.59	0.84
Reach-1	23415	0.2%	12505.00	123.00	135.13	135.13	137.89	0.005069	16.96	2245.13	422.31	0.91
											7.	
Reach-1	23171	10%	2980.00	120.30	128.75		129.48	0.002604	6.87	455.76	121.38	0.57
Reach-1	23171	2%	5840.00	120.30	129.79	129.12	131.57	0.005575	10.79	599.24	177.93	0.81
Reach-1	23171	1%	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23171	0.2%	12505.00	120.30	134.35		135.16	0.001732	7.84	1880.08	333.29	0.44
Reach-1	23036	10%	2980.00	121.70	128.65		129.15	0.001483	5.59	564.12	284.35	0.43
Reach-1	23036	2%	5840.00	121.70	130.47		130.96	0.000752	4.61	1111.41	319.70	0.31
Reach-1	23036	1%	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	23036	0.2%	12505.00	121.70	134.55		134.98	0.000237	3.32	2572.37	391.51	0.18
D 1.4	00040	100/	2000 00	101.00	100.01	400.00	400.00		0.04	570.00	222.22	0.55
Reach-1	22916	10%	2980.00	121.00	128.01	126.93	128.88	0.002603	8.01	570.82	302.03	0.57
Reach-1	22916 22916	1%	5840.00	121.00	130.41		130.84	0.000999	6.20 5.38	1483.60	430.42	0.38
Reach-1			7455.00	121.00	131.63		131.97	0.000628		2037.14	480.80	0.31 0.21
Reach-1	22916	0.2%	12505.00	121.00	134.63		134.90	0.000281	4.31	3712.15	632.31	0.21
Reach-1	22765	10%	2980.00	114.20	128.49		128.58	0.000149	2.53	1428.22	234.62	0.13
Reach-1	22765	2%	5840.00	114.20	130.48		130.70	0.000149	3.96	2020.14	395.39	0.19
Reach-1	22765	1%	7455.00	114.20	131.64		131.87	0.000301	4.19	2548.37	511.91	0.19
Reach-1	22765	0.2%	12505.00	114.20	134.64		134.84	0.000240	4.22	4324.67	669.64	0.17
								0.0000				
Reach-1	22450	10%	2980.00	116.90	127.63	124.78	128.38	0.006142	7.39	605.20	384.22	0.48
Reach-1	22450	2%	5840.00	116.90	130.27		130.51	0.001575	4.56	1791.09	483.52	0.26
Reach-1	22450	1%	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21
Reach-1	22450	0.2%	12505.00	116.90	134.54		134.71	0.000615	3.62	4362.75	1054.32	0.17
Reach-1	22140	10%	2980.00	117.00	124.05	124.05	126.26	0.006734	12.84	391.36	132.65	0.95
Reach-1	22140	2%	5840.00	117.00	126.77	126.77	129.42	0.005440	14.96	889.23	205.48	0.91
Reach-1	22140	1%	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	22140	0.2%	12505.00	117.00	131.26	131.26	134.04	0.003953	16.95	2349.42	658.06	0.83
Reach-1	21825	10%	2980.00	115.90	121.80	121.75	123.65	0.007981	11.17	314.54	84.21	0.97
Reach-1	21825	2%	5840.00	115.90	121.80	121.75	123.65	0.007981	11.17	604.08	179.14	0.97
Reach-1	21825	1%	7455.00	115.90	124.12	125.26	128.03	0.005551	14.07	847.23	239.90	0.94
Reach-1	21825	0.2%	12505.00	115.90	131.24	127.79	132.45	0.003781	10.39	3430.35	1045.30	0.50
00011 1	2.320	5.2.0	12000.00	110.00	131.24	121.13	102.40	0.001400	10.08	0-00.00	10-10.00	0.50
Reach-1	21770	10%	2980.00	115.40	122.06	120.08	122.97	0.002174	7.62	390.83	103.38	0.55
Reach-1	21770	2%	5840.00	115.40	124.17	122.36	126.07	0.003067	11.07	527.79	119.93	0.68
Reach-1	21770	1%	7455.00	115.40	125.08	123.47	127.59	0.003503	12.70	587.15	127.10	0.74
Reach-1	21770	0.2%	12505.00	115.40	130.39	126.53	132.19	0.001574	11.58	2432.53	932.61	0.54
Reach-1	21757.5		Bridge									
												<u> </u>
Reach-1	21745	10%	2980.00	115.40	121.95	120.08	122.89	0.002314	7.77	383.57	102.50	0.56
Reach-1	21745	2%	5840.00	115.40	123.88	122.36	125.93	0.003470	11.48	508.60	117.61	0.72
Reach-1	21745	1%	7455.00	115.40	124.48	123.47	127.36	0.004410	13.60	547.97	122.37	0.83
Reach-1	21745	0.2%	12505.00	115.40	126.94	126.53	131.79	0.005288	17.67	707.72	141.67	0.94
Reach-1	21695	10%	2980.00	114.20	121.74	120.15	122.74	0.003025	8.01	371.94	69.60	0.61
Reach-1	21695	2%	5840.00	114.20	123.69	122.46	125.72	0.004430	11.42	511.32	74.77	0.76
				114.20	124.27	123.52	127.08	0.005624	13.46	557.56	87.09	0.87
Reach-1 Reach-1	21695 21695	0.2%	7455.00 12505.00	114.20	127.45	127.45	130.78	0.004531	14.98	1124.07	292.57	0.82

HEC-RAS Plan: PROPOSED River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21285	10%	2980.00	114.30	119.50	119.17	120.92	0.006772	9.55	312.25	87.08	0.88
Reach-1	21285	2%	5840.00	114.30	121.70	121.16	123.70	0.005436	11.42	567.01	229.63	0.85
Reach-1	21285	1%	7455.00	114.30	122.75	122.75	124.74	0.004638	11.68	907.52	396.78	0.80
Reach-1	21285	0.2%	12505.00	114.30	124.70	124.69	126.86	0.004103	13.05	1782.33	518.61	0.79

**APPENDIX I** 



Project Name: 141 Danbury Road

Project Number: **F0173-02**Project Location: **Wilton, CT** 

Description: Riprap Apron Calculation
Prepared By: TAS Date: July 9, 2021

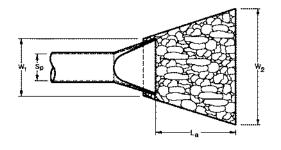
### **Riprap Apron**

 $Invert \ Elevation = 138.50 \ ft$   $Tailwater \ Elevation = 140.44 \ ft$   $Tailwater \ Depth \ (TW) = 1.94 \ ft$   $Inside \ Pipe \ Diameter \ (S_p) = 1.50 \ ft$   $Pipe \ Discharge \ (Q) = 9.14 \ cfs$   $Outlet \ Velocity \ (V) = 5.17 \ ft/s$ 

#### **Apron Type**

Type A Riprap Apron (Minimum Tailwater Condition) TW <  $0.5R_p$ Type B Riprap Apron (Maximum Tailwater Condition) TW  $\geq 0.5R_p$ TW =  $1.94 > 0.5R_p$ 

#### Use Type B Apron



#### **Apron Length**

Type B Riprap Apron (Maximum Tailwater Condition) TW ≥ 0.5R<sub>p</sub>

$$L_a = (3.0(Q-5)/Sp^{1.5})+10.0$$

#### **Apron Width**

#### Type B Riprap Apron (Maximum Tailwater Condition) TW $\geq 0.5R_p$

$$W_1 = 3*S_p$$
  
 $W_2 = 3*S_p + 0.4L_a$ 

W <sub>1</sub> =	4.50	ft	
$W_2 =$	11.20	ft	

#### **Riprap Specification**

Outlet Velocity (V)=	0-8 ft/s	Modified
Outlet Velocity (V)=	8-10 ft/s	Intermediate
Outlet Velocity (V)=	10-14 ft/s	Standard

Outlet Velocity (V)=	5.170	ft/s	Use Modified Riprap
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Outlet protection has been designed in accordance with the Section 11.13 of the ConnDOT Drainage Manual



Project Name: 141 Danbury Road

Project Number: **F0173-02**Project Location: **Wilton, CT** 

Description: Temporary Sediment Trap Sizing Calculation

Prepared By: **TAS** Date: **May 20, 2021** 

## **Temporary Sediment Trap 01**

## **Sediment Storage Volume**

Drainage Area	=	2.4	acres
Initial Storage Volume	=	134	cy/ac
Required Storage	=	322	су
	=	8,683	cf
Min Wet Storage (1/2 Required Storage)	=	4,342	cf

## **Wet Storage Volume**

$$V_{w} = 0.85*A_{w}*D_{w}$$

V <sub>w</sub> , Wet Storage Volume	=	7064	cf
D <sub>w</sub> , Maximum Depth (Low Point in Trap to Base of Outlet)	=	3	ft
A <sub>w</sub> , Surface Area of the Flooded Area at	_	2770	sf
the Base of the Outlet	_	2//0	SI

## **Dry Storage Volume**

$$V_d = [(A_w + A_d) / 2] * D_d$$

V., Dry Storage Volume	=	3004	cf
D <sub>d</sub> , Depth (Base to the top of the Outlet)	=	1	ft
the Top of the Outlet	=	3237	SI
A <sub>d</sub> , Surface Area of the Flooded Area at	_	3237	sf
A <sub>w</sub> , Surface Area of the Flooded Area at the Base of the Outlet	=	2770	sf
A Curfoco Aron of the Flooded Aron at			

## **Provided Storage Volume**

Wet Storage  Dry Storage	= = =	7064 262 3004 111	cf cy cf cy
Total Provided Storage	=	10067 373	cf cy

Calculated in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control Section 5-11

**APPENDIX J** 



Project Name: 141 Danbury Road

Project Number: **F0173-02**Project Location: **Wilton, CT** 

Description: Sanitary Sewer Flow Calculation
Prepared By: TAS Date: July 14, 2021

#### 141 Danbury Road

#### **Total Bedrooms**

			Bedrooms
1 Bedroom Units =	37	x 1	37
2 Bedroom Units =	122	x 2	244
3 Bedroom Units =	14	x 3	42

Total Residential Units = 173

323 Total Bedrooms

#### **Average Daily & Peak Flow**

Average Flow = 
$$323 \times 150$$
  
Average Flow =  $48,450$  GPD

Peak Flow Factor = 4

#### **Sanitary Sewer Lateral Capactity**

6" PVC Gravity Lateral

Capacity = 668,400 GPD