# GREGORY AND ADAMS, P.C.

PAUL H. BURNHAM DANIEL L. CONANT SUSAN L. GOLDMAN J. VANCE HANCOCK J. CASEY HEALY MICHAEL LAMAGNA\* DERREL M. MASON\* MATTHEW C. MASON\* JAMES D'ALTON MURPHY\* KATHLEEN L. ROYLE \* RALPH E. SLATER ROGER R. VALKENBURGH \* ATTORNEYS AT LAW 190 Old Ridgefield Road Wilton, CT 06897 (203) 762-9000 FAX: (203) 834-1628

# ESTABLISHED 1964

NEW YORK OFFICE: 399 KNOLLWOOD ROAD - SUITE 201 WHITE PLAINS, NY 10603 (914) 848-5000

WWW.GREGORYANDADAMS.COM

JULIAN A. GREGORY (1912 - 2002)

THOMAS T. ADAMS (1929 - 2015)

PLEASE REPLY TO SENDER: JAMES D'ALTON MURPHY DIRECT DIAL: 203-571-6309 jmurphy@gregoryandadams.com

\* Also Admitted in New York ② Also Admitted in Vermont

May 25, 2022

## By E-mail and Hand Delivery

Planning and Zoning Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897 Attn: Mr. Michael E. Wrinn – Director of Planning and Land Use Management

# Re: ASML US, LLC – Applications for Special Permit and Site Plan Review Premises: <u>77 Danbury Road</u>, Wilton, Connecticut

Dear Mr. Chairman and Members of the Commission:

This firm represents ASML US, LLC ("ASML"). Our client is the owner of the 28.6425-acre parcel at 77 Danbury Road.

In recent years, and in light of this Commission's recent approval of a revamped cafeteria and logistics area, and the Commission's informal review of this access road proposal, the evolution of certain on-site traffic circulation design deficiencies has become readily apparent. At present, almost all of the employee and visitor trips, as well as delivery truck and forklift trips, use the same two-lane access road which runs from the westerly side of the entrance bridge in a clockwise direction around the southern side of the main building. That road travels through a series of pedestrian crosswalks and also through three active loading dock and logistics areas before reaching the parking garage in the northwest corner of the property.

The daily interaction of hundreds of employee and visitor cars, with the many trucks maneuvering on the site, is less than optimum from a traffic flow safety viewpoint. To improve this situation, ASML proposes to construct a second access road running in a counterclockwise direction from the end of the entry bridge and running generally northwest to create direct access to the 4th level of the existing parking garage.

The proposed new access road will require a Special Permit and Site Plan Review. In addition, ASML's engineers at Tighe & Bond, Inc. ("**T&B**") have determined that the only feasible route for this new access road will require a cut and fill excavation which exceeds the 15,000 square foot limitation under the zoning regulations. Therefore, under separate cover, our client is also requesting the simultaneous text

# Planning and Zoning Commission May 25, 2022 Page 2 of 4

change which would provide relief from the town-wide 15,000 square foot limitation in recognition of the relatively large 28.6425-acre size of the ASML parcel, which is more than 280% of the minimum lot size in the DE-10 zone.

As attorneys for ASML, we hereby submit an application for special permit and site plan review to allow the construction of a new access road.

- 1. Authorization letter signed by ASML authorizing Gregory and Adams to act as its Agent in connection with this matter.
- 2. Application for Special Permit with Form B Zoning Data and Statement of Compliance with Town Plan attached.
- 3. Location Map and Vicinity Sketch prepared by Arthur H. Howland Associates ("AHH") dated November 11, 2021.
- 4. Property Survey & As-Built Map (BDY.1) prepared by AHH dated July 1, 2021 and revised November 11, 2021.
- 5. Campus Traffic Flow Safety Improvements Drawings prepared by T&B dated May 24, 2022.
  - a. Cover Sheet with Location Map
  - b. General Notes, Legend and Abbreviations (C-000)
  - c. Existing Conditions Plan (C-100)
  - d. Roadway Typical Sections (C-200)
  - e. Alignment Plan (C-210)
  - f. Driveway Profile (C-220)
  - g. Site Plan (C-300)
  - h. Site Plan Enlargement (C-310)
  - i. Grading Plan (C-400)
  - j. Grading Plan Enlargement (C-410)
  - k. Drainage and Utility Plan (C-500)
  - 1. Drainage and Utility Plan Enlargement (C-510)
  - m. Sediment and Erosion Control Plan Phase I (C-601)
  - n. Sediment and Erosion Control Plan Phase 2 (C-602)
  - o. Sediment and Erosion Control Plan Phase 3 (C-603)
  - p. Sediment and Erosion Control Plan Phase 4 (C-604)
  - q. Sediment and Erosion Control Plan Phase 5 (C-605)
  - r. Sediment and Erosion Control Notes, Narrative and Details (C-610)
  - s. Sediment and Erosion Control Details (C-611)
  - t. Sediment and Erosion Control Details (C-612)
  - u. Cross Sections (C-700)
  - v. Cross Sections (C-701)
  - w. Cross Sections (C-702)
  - x. Cross Sections (C-703)
  - y. Cross Sections (C-704)
  - z. Cross Sections (C-705)

Planning and Zoning Commission May 25, 2022 Page 3 of 4

> aa. Cross Sections (C-706) bb. Cross Sections (C-707) cc. Cross Sections (C-708) dd. Traffic Operations Plan (C-800) ee. Site Details (C-900) ff. Site Details (C-901) gg. Site Details (C-902) hh. Site Details (C-903) ii. Site Details (C-904) ij. Site Details (C-905) kk. Site Details (C-906) II. Drainage Details (C-910) Drainage Details (C-911) mm. nn. Drainage Details (C-912) oo. Drainage Details (C-913) pp. Drainage Details (C-914) qq. Drainage Details (C-915) rr. Drainage Details (C-916) ss. Planting Plan -1 (L-100) tt. Planting Plan -2 (L-101) uu. Planting Plan – Details (L-102)

- 6. Inland Wetland and Watercourses Significant Activity Permit Application prepared by T&B dated May 24, 2022.
- 7. Engineering Report prepared by T&B dated May 24, 2022.
- 8. Preliminary View Studies prepared by T&B dated April 12, 2022.
  - a. View Line Study Locations (V-100)
  - b. View Line Study Locations (Aerial Imagery) (V-101)
  - c. View Line Cross Sections -1 (V-200)
  - d. View Line Cross Sections 2 (V-201)
  - e. View Line Photos (V-300)
- 9. Photography of the Premises taken from Danbury Road by Gregory and Adams on May 23, 2022.
- 10. Environmental Impact Statement prepared by Gregory and Adams.
- 11. Title Certification Letter prepared by Gregory and Adams.
- 12. List of Owners within 500' of the Premises.
- 13. List of Project Professionals

Planning and Zoning Commission May 25, 2022 Page 4 of 4

I also enclose:

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- 1. Gregory and Adams check in the amount of \$460.00 in payment of the application fee.
- 2. Two (2) envelopes addressed to ASML US, LLC c/o Gregory and Adams.

We look forward to presenting testimony and evidence at the hearing.

Respectfully submitted, Gregory and Adams, P.C.

James D'Alton Murphy

By:

James D'Alton Murphy

JD'AM/ko

Enclosures

cc: Mr. Jason Domena and Mr. Patrick van den Bogaard – ASML John W. Block, P.E. and Joseph A. Canas, P.E. – Tighe & Bond, Inc. Ms. Marilee Beebe - WSP Kathleen L. Royle, Esq. Daniel L. Conant, Esq.

M:\Clients\ASML\2022 Driveway Extension\Application to PZC-SP and SDP\Formal Review 05-25-22\PZC submission ltr.05-25-22 (4).doc

# GREGORY AND ADAMS, P.C.

PAUL H. BURNHAM SUSAN L. GOLDMAN J. VANCE HANCOCK J. CASEY HEALY MICHAEL LAMAONA\* DERREL M. MASON\* MATTHEW C. MASON\* JAMES D'ALTON MURPHY\* (2) KATHLEEN L. ROYLE \* RALPH E, SLATER RODER R. VALKENBURGH \*

ALSO ADMITTED IN NEW YORK

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PLEASE REPLY TO SENDER: JAMES D'ALTON MURPHY DIRECT DIAL: 203-571-6309 jmurphy@gregoryandadams.com

# October 28, 2021

### By E-Mail Only ASML US, LLC

Attn: Mr. Jason Domena, Senior Project Leader AM CRE Facility Management

Rei ASML US, LLC-Land Use Applications Premises: 77 Danbury Road, Wilton, Connecticut

Dear Mr. Domena:

As you know, we are in the process of preparing land use applications to various Town of Wilton and State of Gonnecticut and other government agencies, if applicable. These agencies require written authorization from the applicant and the property owner authorizing Gregory and Adams, P.C to act as its agent in connection with any and all land use matters involving the subject property. Please sign a copy of this letter as applicant and owner and return it to me by email.

Very truly yours,

James D'Alton Murphy James D'Alton Murphy

JD'AM/ko

The undersigned hereby authorizes Gregory and Adams, P.O. to act as its agent in connection with the above-referenced matters.

. By:

ASML US, LLC Jason Domenta

Its: Senior Project Leader AM CRE Facility Management Duly Authorized .

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**SPECIAL PERMIT DESCRIPTION:** Cite specific section(s) of the Zoning Regulations and provide a detailed description of the proposed development. Attach additional sheets as required. Section 29-

ASML US, LLC		c/o	Gregory	and A	dams,	P.C.,	190	01d	Ridgef	Eield	Road,	Wilton
APPLICANT'S NAME			ADDR	ESS								
ASML US, LLC		c/o	Gregory	and A	dams,	P.C.,	190	01d	Ridgef	Eield	Road,	Wilton
OWNER'S NAME			ADDR	ESS								
77 Danbury Road							DI	E-10				
PROPERTY LOCATION							ZO	NIN	G DIS	<b>FRIC</b>	CT	
5250	2494	293		69	9		18		28	3.642	5 acre	<u>s</u>
WLR	VOLUME	PAGE		TAX	K MA	P #	LO	Γ#	A	CRE	AGE	

# THE FOLLOWING MATERIALS ARE REQUIRED:

* Please see SPECIAL INSTRUCTIONS FOR SUBMISSION DURING COVID at:
Application Forms / Materials   Wilton CT
* All submitted plans and documents shall bear an original signature, seal, and license number of the
professional responsible for preparing each item. Maps should be folded, not rolled.
<b>VICINITY SKETCH</b> at a scale of 1"=100' or 1"=200'. Said map shall show all existing zone boundaries, existing
buildings and parcels, labeled by their corresponding Tax Map and Lot Number, within 500' of the subject property.
<b>X</b> CLASS A-2 SURVEY MAP of the subject property
<b>SITE DEVELOPMENT PLAN</b> pursuant to Section 29-11 of the Zoning Regulations
<b>X</b> FORM B – ZONING DATA
X LIST OF PROJECT PROFESSIONALS including name, firm, address and telephone
<b>X</b> LETTER OF TITLE certifying owner of record as of date of the application
X PROOF OF APPLICANT'S LEGAL INTEREST in property
<b>X</b> LIST OF OWNERS WITHIN 500' of any portion of subject property, sorted by Tax Map and Lot #
[See online GIS instructions at: owner list 500 ft gis directions.pdf (wiltonct.org)]
X. ANY OTHER PLAN OR DOCUMENT as required by Zoning Regulations
<b>X</b> ONE COPY OF THE DEED
<b>X</b> ELECTRONIC SUBMISSION of all materials, consolidated into 1 or 2 PDFs maximum, emailed to
michael.wrinn@wiltonct.org and daphne.white@wiltonct.org
X \$460 FILING FEE + \$50/Unit or \$50/2000 sq. ft. (Accessory Apartment - \$260) payable to: Town of Wilton
<b>ENVELOPES, a</b> ddressed to each property owner within 500' of any portion of subject property.
[See "Envelopes Instructions" at: envelopes instructions 0.pdf (wiltonct.org)]

# X IS THE SUBJECT PROPERTY LOCATED WITHIN THE WATERSHED BOUNDARY? NO X IS THE SUBJECT PROPERTY WITHIN THE FLOOD ZONE? NO

THE APPLICANT understands that this application is to be considered complete only when all information and documents required by the Commission have been submitted and is responsible for the payment of all legal notices incurred.

THE UNDERSIGNED WARRANTS the truth of all statements contained herein and in all supporting documents according to the best of his or her knowledge and belief; and hereby grants visitation and inspection of the subject property as described herein.

ASML US, LLC by its Agent Gregory	and Adams,	P.C.
By: James D'Alton Murphy	May 25,	2022 jmurphy@gregoryandadams.com 203-762-9000
APPLICANT'S SIGNATURE )	DATE	EMAIL ADDRESS TELEPHONE
ASML US, LLC by its Agent Gregory	and Adams,	P.C.
By: James D'Alton Murphy	May 25,	2022 jmurphy@gregoryandadams.com 203-762-9000
OWNER'& SIGNATURE	DATE	EMAIL ADDRESS TELEPHONE
$\Box$		

# For Planning and Zoning Department Use Only:

Mandatory Referrals - Jurisdiction/Age	ncy	
	Yes	No
Village District Design Advisory Committee (VDDAC):		
Architectural Review Board (ARB):		
Western Connecticut Council of Governments (WestCOG):		
South Norwalk Electric and Water Company (SNEW) Designated Public Watershed:		
First Taxing District Water Department Designated Public Watershed:		
State-Designated Aquifer Protection Area:		
Adjoining Community Notification:		

WILTON PLANNING AND ZONING COMMISSION

FORM B - ZONING DATA

Include the following data on the required Site Development Plan, as well.

### 77 Danbury Road, Wilton, CT

#### PROPERTY ADDRESS

1,247,668 sf (28,6425 acres)

AGE

1.065.12 feet

LOT FRONTAGE

	PER ZONING REGS (MAX OR MIN ALLOWED)	EXISTING	PROPOSED	TOTAL
GROSS FLOOR AREA [SF]		375,789 sf	0 sf	375,789 sf
BUILDING FOOTPRINT [SF]		292,585 sf	0 sf	292,585 sf
BUILDING COVERAGE [SF/%] (round up)	25%	24%	0%	24%
BUILDING HEIGHT [FT - Story]	55 ft / 4 story	51'-6" / 2 story	0	51'-6" / 2 story
FLOOR AREA RATIO (F.A.R.)	N/A	N/A	N/A	N/A
PARKING SPACES (round up)	1 per 400 sf of GFA 1 per 1,000 sf of outdoor storage	1,193	(- 66)	1,127
LOADING SPACES	29-8B.7 - 17 required	17	0	17
SITE COVERAGE [SF/%]	50%	526,600 sf 42.2%	+ 14,788 sf + 1.1%	541,388 sf 43.3%

### OFF-STREET PARKING AND LOADING CALCULATIONS

Please provide the specific calculation used to determine the minimum required off-street parking and loading spaces pursuant to the Zoning Regulations.

**PARKING CALCULATION** (Use separate page, if necessary)

LOADING CALCULATION (Use separate page, if necessary)

### PLAN OF CONSERVATION AND DEVELOPMENT

Please indicate on separate page how this proposal complies with the Plan of Conservation and Development.

THE UNDERSIGNED WARRANTS the truth of all statement's contained herein: ASML US, LLC by its Agent Gregory and Adams, P.C.

By: James D'Alton Murphy

APPLICANT'S SIGNATURE

May 25, 2022 DATE

LOT	ACRE

**DE-10** 

ZONING DISTRICT

# ASML US, LLC.

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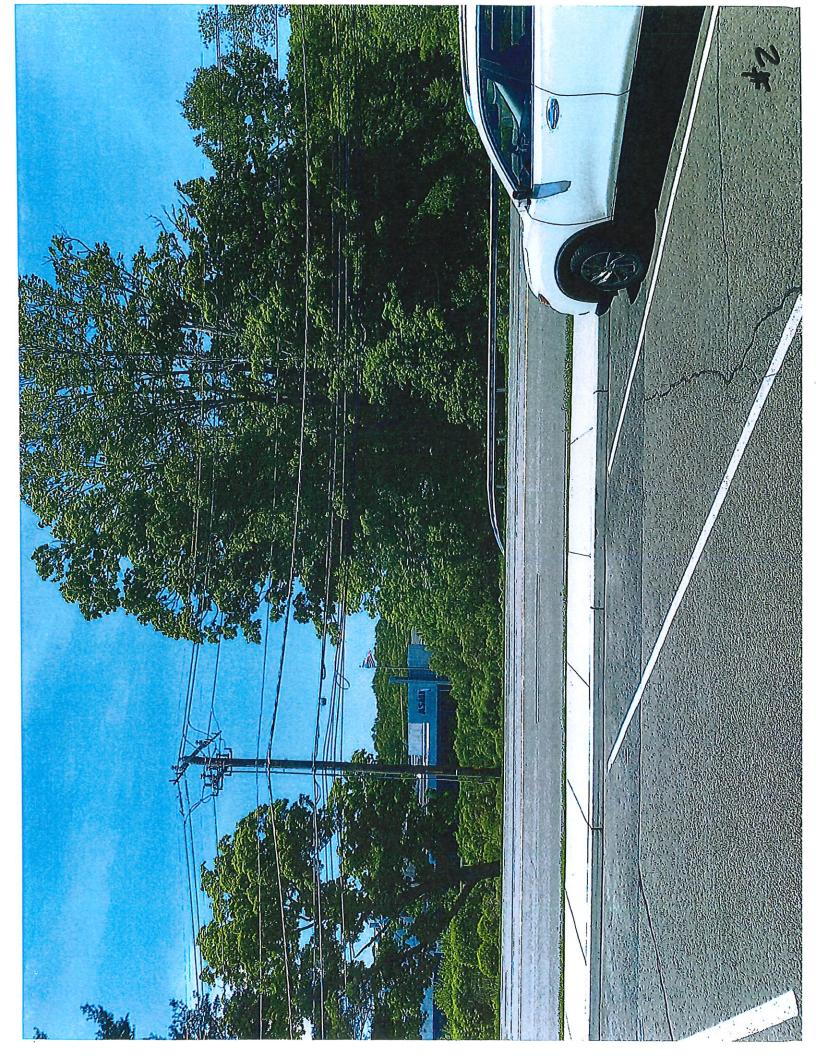
# **Application for Special Permit**

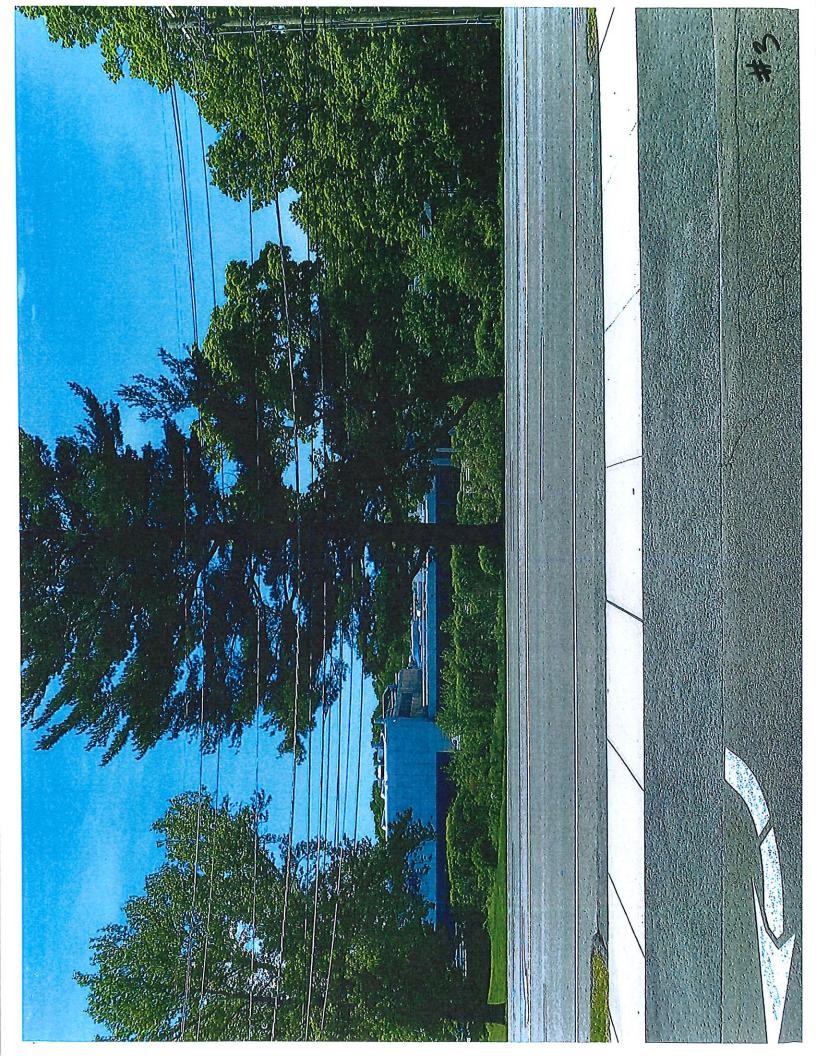
# Premises: 77 Danbury Road, Wilton Connecticut

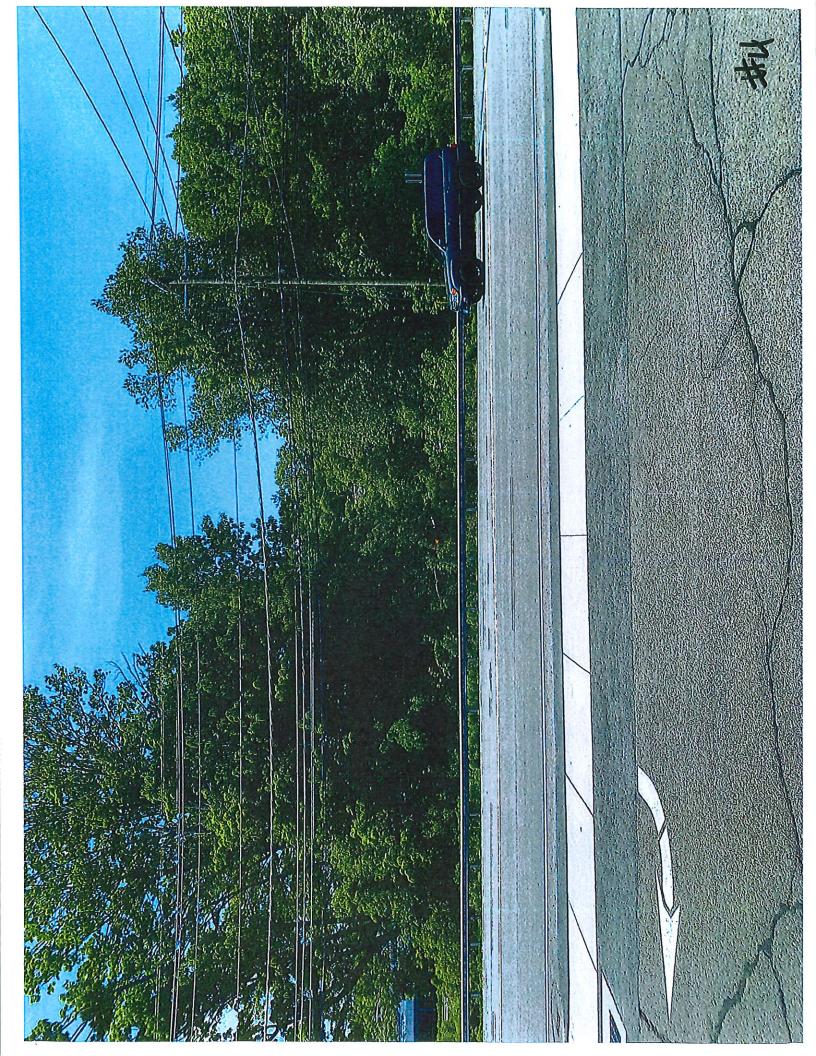
### Statement of Compliance with Plan of Conservation and Development

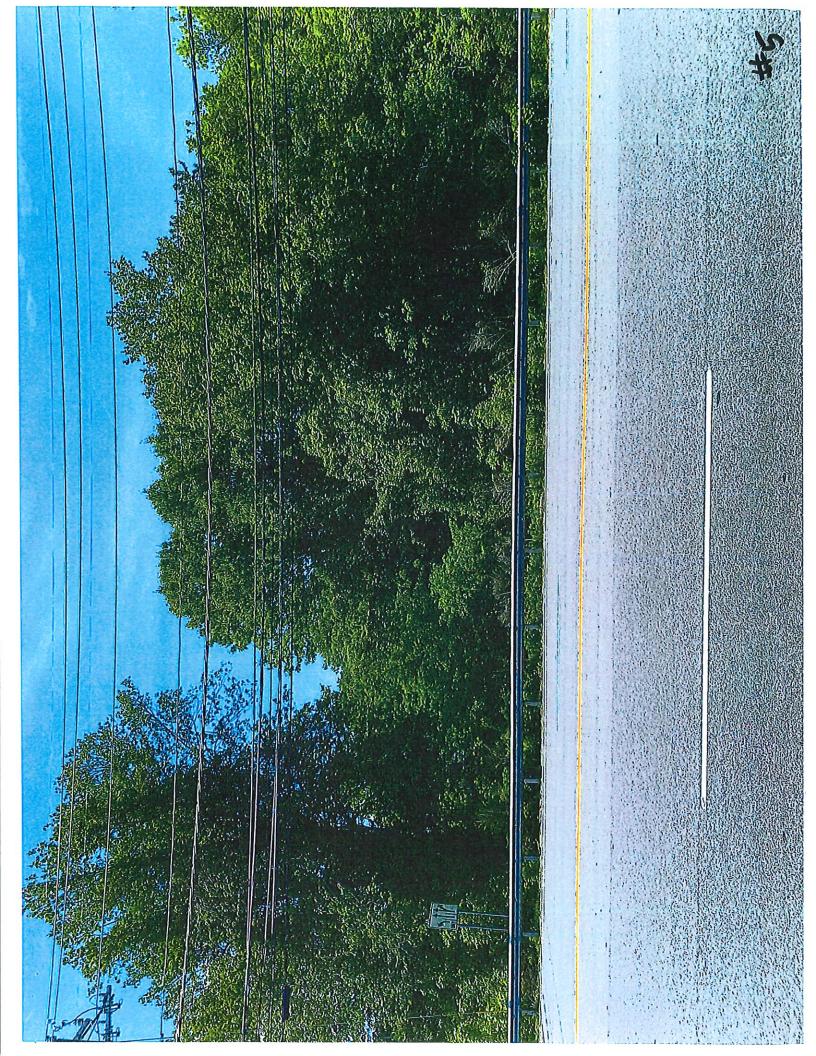
The above-referenced Premises consists of 28.6425± acres of land located in a DE-10 Design Enterprise District and is improved with a research, manufacturing, and business offices facility. ASML wishes to amend its existing special permit to allow the construction of an access road to the 4th floor of the existing parking garage in order to address safety concerns about the on-site traffic patterns. This use is compatible with the Town's Plan of Conservation and Development adopted on September 23, 2019, and effective October 1, 2019 (the "Town Plan"). The Town Plan states that a goal is supporting existing commercial development in this area, which extends from the Norwalk town line to Wolfpit Road (reference made to page 67 of the Town Plan under section six, titled "Built Environment").

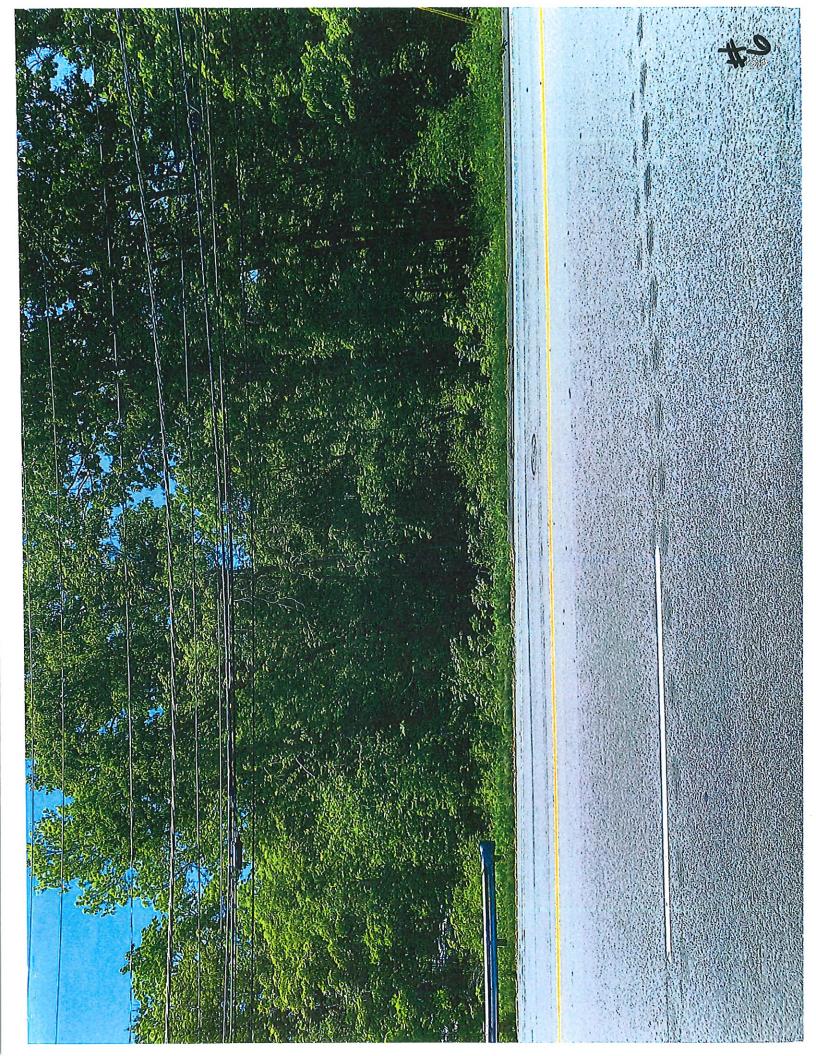


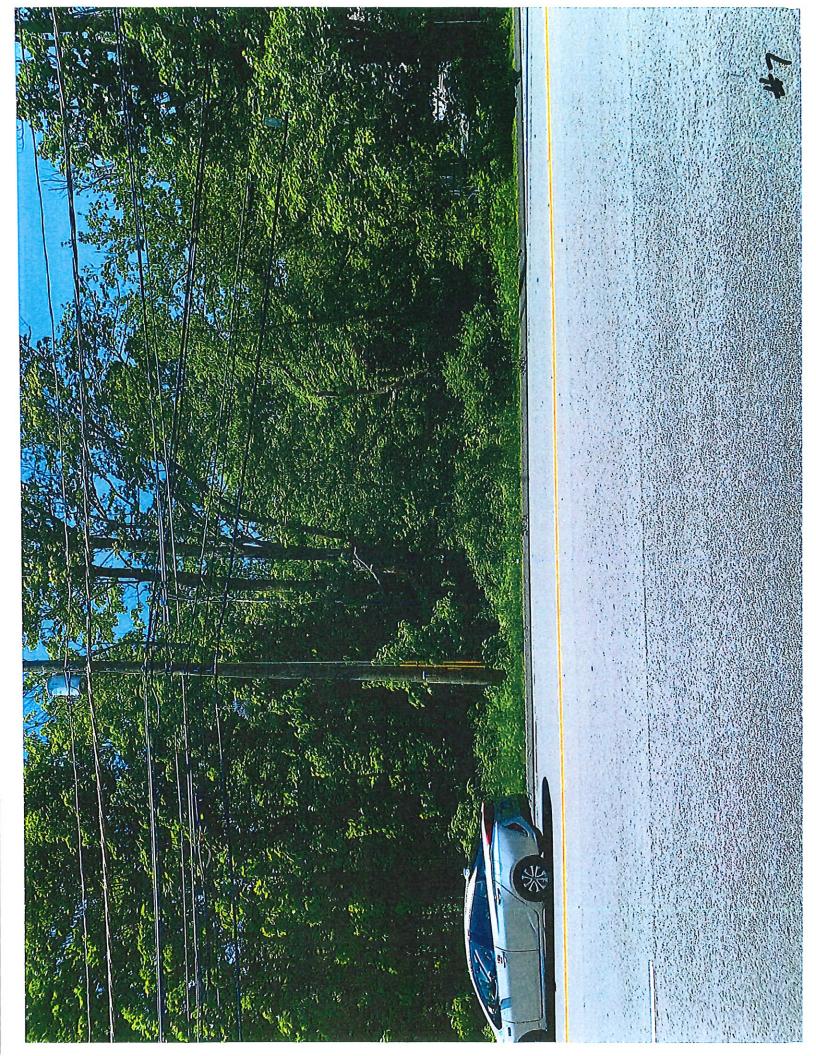


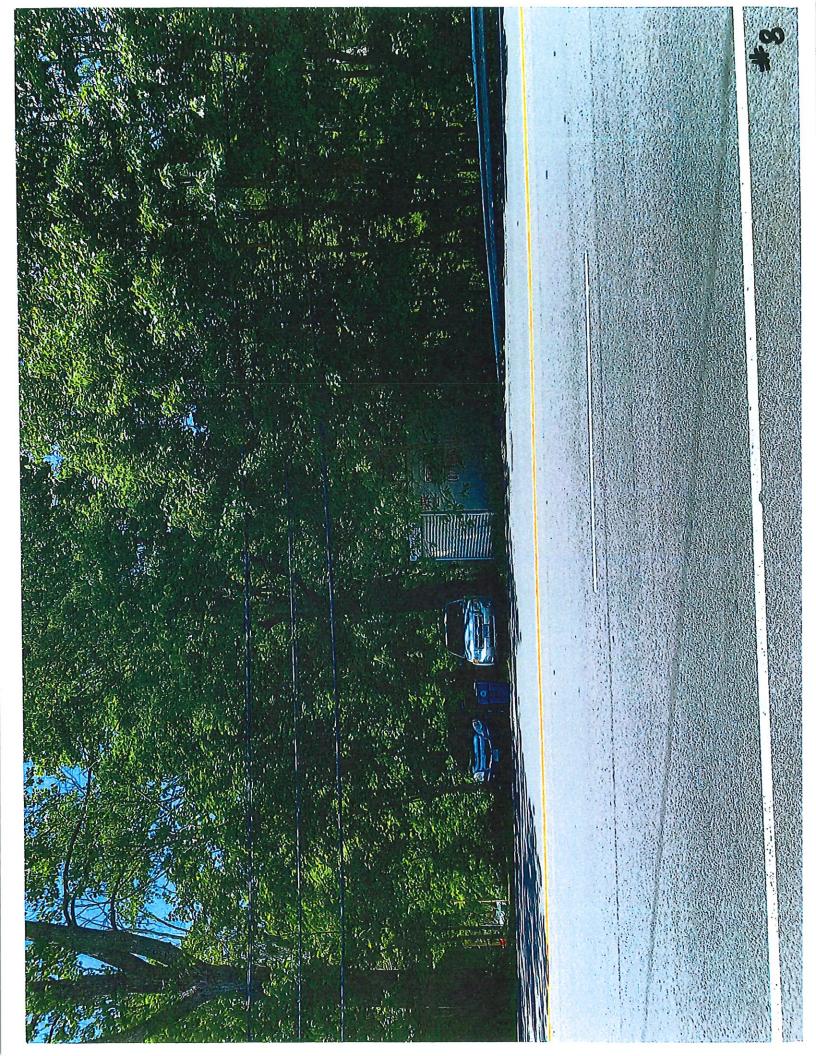


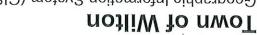






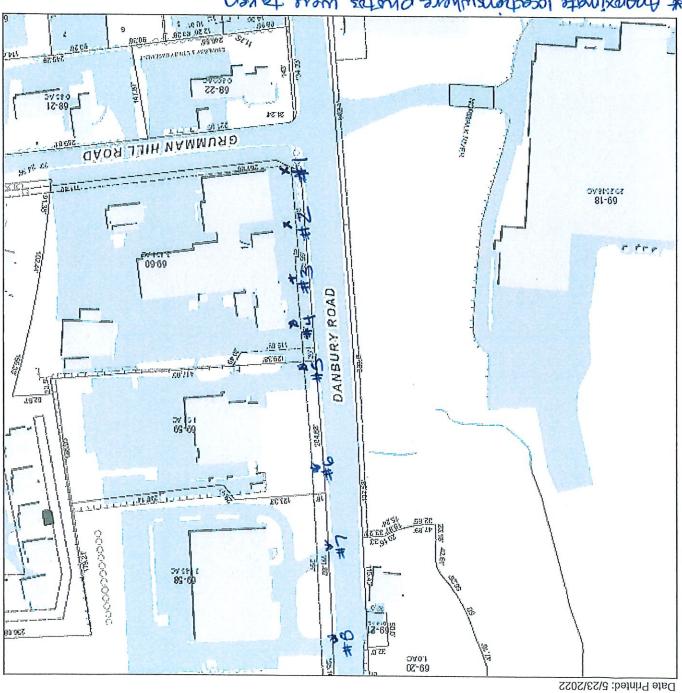






Geographic Information System (GIS)





\* Approximete locations where photos were NAUET

# MAP DISCLAIMER - NOTICE OF LIABILITY

This map is for assessment properties only. It is not for legal description or conveyances. All information is subject to verification by any user. The Town of Wilton and its mapping contractors assume no legal responsibility for the information confacted herein.



Planimetrics Updated: 2014 Zoning Effective: July 28, 2017

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# **GREGORY AND ADAMS, P.C.**

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May 25, 2022

# Via Email and Hand Delivery

Planning and Zoning Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897 Attn: Mr. Michael E. Wrinn – Director of Planning and Land Use Management

> Re: ASML US, LLC. – Application for Special Permit/Environmental Impact Statement Premises: <u>77 Danbury Road, Wilton, CT</u>

Dear Mr. Chairman and Members of the Commission:

Set forth below is ASML's Environmental Impact Statement in satisfaction of the requirements of Section 29-10.A.5 of the Zoning Regulations of the Town of Wilton (the "**Regulations**"):

a. <u>Compatibility with Town's Plan of Development</u>

The above-referenced Premises consists of 28.6425± acres of land located in a DE-10 Design Enterprise District and is improved with a research, manufacturing, and business offices facility. ASML wishes to amend its existing special permit to allow the construction of an access road to the 4th floor of the existing parking garage in order to address safety concerns about the on-site traffic patterns. This use is compatible with the Town's Plan of Conservation and Development adopted on September 23, 2019, and effective October 1, 2019 (the "Town Plan"). The Town Plan states that a goal is supporting existing commercial development in this area, which extends from the Norwalk town line to Wolfpit Road (reference made to page 67 of the Town Plan under section six, titled "Built Environment"). Planning and Zoning Commission May 25, 2022 Page 2 of 3

# b. <u>Sensitive Environmental Features</u>

There are wetlands and watercourses located on and adjacent to the Property, and the proposed project also involves construction of a driveway on a hillside on the northern portion of the Property. The area proposed for the access road is near a previously reviewed and approved underground piped watercourse and storm drainage system. A forested wetland and perennial watercourses are located east of the proposed project area, within the Town's 100-Foot Review Area. Neither the wetlands, open watercourses, nor the piped watercourse will be disturbed during construction.

During the construction process, erosion control barriers and other control measures will be installed along the work areas. Further, the proposed project includes numerous mitigation and protective measures, which include improvements to the existing stormwater management systems and planting of additional vegetation.

The stormwater management systems will be improved with a network of catch basins and storm drains, increase of the average distance from impervious cover to wetlands, improved water quality discharged to the river, and the installation of infiltration chambers beneath the parking area to recharge ground water and decrease peak volume and flow discharge to the Norwalk River. Additional vegetation will be planted within the riparian buffer west of the Norwalk River and east of the driveway, and water and drought tolerant vegetation will be added to the rain gardens and bioswale for stormwater management and biodiversity.

# c. Impact on Water, Sewer and Storm Drainage

The Premises is served by public water and sewer infrastructure, and the proposed project will not impact the aforementioned or the storm drainage system of the Town.

# d. Traffic Impact

The proposed project will not increase the current employee and trucking/delivery traffic and will improve the on-site traffic patterns and address safety concerns.

# e. <u>Impact on Town Services</u> The proposed project will not have a significant impact on Town services,

# f. Alternatives to mitigate adverse impacts

The proposed project will not have adverse impacts on the premises, but four alternatives were considered for the design of the project. These alternatives were No Build, Conducting Activity in a Different Location, Conducting an Activity of a Different Nature, and Alternate Grades. The project and current proposal evolved through several iterations and was ultimately selected by ASML. For additional details concerning the aforementioned alternatives, please refer to Section 4.7 of the Engineering Report.

Planning and Zoning Commission May 25, 2022 Page 3 of 3

If you have any questions, please contact me.

Respectfully submitted, Gregory and Adams, P.C.

James D'Alton Murphy

By:

James D'Alton Murphy

JD'AM/dc

Cc: Mr. Patrick van den Bogaard and Mr. Jason Domena – ASML Mr. Joe Canas and Mr. John Block – Tighe & Bond Ms. Marilee Beebe and Ms. Monique Bland – WSP

M:\Clients\ASML\2022 Driveway Extension\Application to PZC-SP and SDP\Formal Review 05-25-22\Environmental Impact Statement (1) (5.25.22).doc

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May 25, 2022

# **By E-mail and Hand Delivery**

Planning and Zoning Commission Town Hall Annex 238 Danbury Road Wilton, CT 06897 Attn: Mr. Michael E. Wrinn – Director of Planning and Land Use Management

# Re: ASML US, LLC – Application for Special Permit and Site Plan Review Premises: <u>77 Danbury Road</u>, Wilton, Connecticut

Dear Mr. Chairman and Members of the Commission:

As attorneys for ASML US, LLC, we hereby certify that title to the above-referenced Premises is vested in ASML US, LLC by virtue of the following documents:

- 1. Warranty Deed from The Perkin-Elmer Corporation to SVG Lithography Systems, Inc. dated August 1, 1996 and recorded on August 2, 1996 in Volume 1002 of the Wilton Land Records at Page 329; and
- Certificate of Change of Name by which SVG Lithography Systems Inc. changed its name to ASML US, Inc., which Certificate is dated January 17, 2002 and was recorded on January 17, 2002 in Volume 1348 of the Wilton Land Records at Page 202.
- 3. Certificate of Change of Name by which ASML US, Inc. changed its name to ASML US, LLC, which Certificate is dated January 30, 2019 and was recorded on February 5, 2019 in Volume 2494 of the Wilton Land Records at Page 293.

Planning and Zoning Commission May 25, 2022 Page 2 of 2

Copies of the Warranty Deed and the Certificates of Change of Name are enclosed for the Commission's file.

Respectfully submitted,

Gregory and Adams, P.C.

James D'Alton Murphy

By:

James D'Alton Murphy

JD'AM/ko

15

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Enclosures

cc: Mr. Jason Domena and Mr. Patrick Van Den Bogaard – ASML
 Mr. Paul Szymanski, P.E and Mr. Jim McTigue, PLS – Arthur H. Howland & Associates
 Mr. Scott Yates and Mr. Ray Walker - H&R Design, Inc.
 Kathleen Royle, Esq.

#### NOL 1002PG329

#### 34119

TO ALL PEOPLE TO WHOM THESE PRESENTS SHALL COME, GREETING:

Know Ye, That THE PERKIN-ELMER CORPORATION, a New York Corporation, with an office and place of business located at 761 Main Avenue in the City of Norwalk, County of Fairfield and State of Connecticut, acting herein by <u>STECHENL.RUDOF</u>, its. <u>ACENT</u>, duly authorized, for the consideration of Ten Dollars (\$10.00) and other valuable consideration, received to its full satisfaction of SVG LITHOGRAPHY SYSTEMS, INC., a Delaware Corporation, with an office and place of business located at 101 Metro Drive, Suite 400, San Jose, California 95110, does give, grant, bargain, sell and confirm unto the said SVG Lithography Systems, Inc. and unto its successors and assigns forever the following described three tracts or parcels of land, together with the buildings and improvements thereon located, situated in the Town of Wilton, County of Fairfield and State of Connecticut:

#### TRACT ONE

All that certain piece or parcel of land, with the buildings and improvements thereon, situated in the Town of Wilton, County of Fairfield and State of Connecticut, and bounded and described as follows, to wit: Northerly by land now or formerly of Elizabeth W. Rodger and by a stonewall; Easterly by the westerly bank of the Norwalk River, so-called, and being land now or formerly of Marguerite L. Arnold; thence northerly by land now or formerly of Marguerite L. Arnold; thence easterly by the Norwalk-Danbury Road; Southerly by land now or formerly of Charles and Florence Hoefle; and Westerly by land now or formerly of Charles and Florence Hoefle; containing 5.3 acres, more or less, and being more particularly shown on a certain map entitled "Map Showing Property Being Conveyed to Lillian Beilin, Wilton, Connecticut", Certified "Substantially Correct" by Walter K. Goodhue, Civil Engineer, New Canaan, Conn., dated Dec. 8, 1947, Scale 1" = 60'.

Being the same premises conveyed to The Perkin-Elmer Corporation by Thomas R. Lyons and John F. Lyons by Warranty Deed dated December 1, 1965 and recorded in Volume 116, page 469 of the Wilton Land Records.

#### TRACT TWO

All that certain piece or parcel of land, in quantity 16.806 acres, more or less, with the buildings and improvements thereon, situated in the Town of Wilton, County of Fairfield and State of Connecticut, and bounded and described as follows:

EASTERLY by the Norwalk-Danbury Road, U.S. Route #7:

SOUTHERLY

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by land now or formerly of Frantisca Vogel; S-\$175, 000.00

\$19, 250.00 Conveyance Tax Collected Town Clerk of Wilton:

### VOL 1002PG330

EASTERLY again,	by land now or formerly of Frantisca Vogel;
SOUTHERLY again,	by land now or formerly of Frantisca Vogel;
WESTERLY	by the Norwalk-Danbury Branch of the New York, New Haven and Hartford Railroad;
NORTHERLY	by land now or formerly of Harry Richmond;
NORTHEASTERLY	by land now or formerly of Robins P. Crowell;
NORTHERLY again,	by land now or formerly of Robins P. Crowell;
EASTERLY again,	by land now or formerly of said Robins P. Crowell along the center line of the Norwalk River;
NORTHERLY again,	by land now or formerly of said Robins P. Crowell.

Said property being the easterly parcel of the premises shown on a certain map entitled "Map of Property Belonging to Elizabeth and Lemuel Hurlburt and W.B. Hurlburt, Esq. situated at South Wilton, Conn.", on file in the Office of the Town Clerk of the Town of Wilton and numbered 68, reference thereto being had.

Being the same premises conveyed to The Perkin-Elmer Corporation by The Hallicrafters Co. by Warranty Deed dated April 1, 1966 and recorded in Volume 118, page 399 of the Wilton Land Records.

#### TRACT THREE

All that certain piece, parcel or tract of land together with the buildings and improvements thereon, and the heating, ventilating and air conditioning equipment attached thereto, situated in the Town of Wilton, designated as "Area = 6.62 Ac." as laid down and delineated on a certain map entitled "Map of Property Prepared For The Estate of Frantisca Vogel, Wilton, Conn.", which map is on file in the office of the Town Clerk of the said Town of Wilton as the map numbered 1869, reference thereto being had. Said premises are bounded and described as follows: Beginning at a point on the westerly line of Danbury Road marking the intersection therewith of the land herein described and land now or formerly of C.G.S. Laboratories, Inc., which point of intersection is marked by a Connecticut Highway Department monument, and running thence in a generally westerly direction along the northerly line of said land now or formerly of C.G.S. Laboratories, Inc., the following courses and distances: North  $61^{\circ}$  47' 20" West 380.00 feet, South 82' 41' 00" West 405.15 feet, South  $61^{\circ}$  03' 20" West 94.21 feet, and North 78' 34' West 210.13 feet to the easterly line of land of the Penn Central Transportation Company, Danbury Branch; running thence in a northerly direction along the easterly line of said land of the Penn

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Central Transportation Company, Danbury Branch, North 11° 26' East 420.67 feet to the southerly line of land now or formerly of Peter E. Olsen; running thence in a generally easterly direction along the southerly line of said land now or formerly of Peter E. Olsen, the following courses and distances: South 83° 24' 10" East 152.80 feet, South 74° 37' 10" East 74.50 feet, South 63° 01' 10" East 47.20 feet, South 48° 38' 10" East 76.60 feet, South 34° 13' 10" East 56.00 feet, South 75° 00' 50" East 30.10 feet, South 75° 23' 10" East 136.00 feet, and South 75° 14' 10" East 220.70 feet to a point; running thence in a northerly direction along the easterly line of said land now or formerly of Peter E. Olsen North 7° 42' 50" East 56.40 feet to a point; running thence in an easterly direction along the southerly line of said land now or formerly of Peter E. Olsen South 79° 36' 10" East 82.20 feet and South 76° 33' 10" East 172.77 feet to the westerly line of Danbury Road; running thence in a southerly direction along the westerly line of Danbury Road South 7° 34' West 199.16 feet and South 9° 43' West 102.90 feet to the northerly line of land now or formerly of C.G.S. Laboratories, Inc., being the point or place of beginning. Together with all rights appurtenant thereto including, without limitation, any right of Grantor in and to the Norwalk River and any other water courses flowing through the premises and the use of the bridges and spur railroad track hereinafter mentioned and rights of way.

Being the same premises conveyed to The Perkin-Elmer Corporation by Joan H. Faerman, formerly known as Joan H. Peltz, Executrix under the last will and testament of Harvey A. Peltz by an Executrix Deed dated January 6, 1981 and recorded in Volume 361, Page 268 of the Wilton Land Records.

#### SUBJECT TO:

- 1. Any and all provisions of any law, statute, ordinance, regulation, including zoning and planning, or public or private law of the Town of Wilton.
- 2. Taxes and Sewer Use charges to the Town of Wilton, hereinafter due and payable.
- Sewer Assessment Lien in the original amount of \$12,957.25 recorded in Volume 314, Page 116 of the Wilton Land Records.
- Sewer Assessment Lien in the original amount of \$96,317.75 recorded in Volume 314, Page 134 of the Wilton Land Records.
- Sewer Assessment Lien in the original amount of \$3,861.00 recorded in Volume 314, Page 135 of the Wilton Land Records.
- Sewer Assessment Lien in the original amount of \$3,208.00 recorded in Volume 360, Page 20 of the Wilton Land Records.
- Sewer Assessment Lien in the original amount of \$41,354.50 recorded in Volume 360, Page 30 of the Wilton Land Records.

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8.	Sewer Assessment Lien in the original amount of \$26,053.65 recorded in Volume 398, Page 218 of the Wilton Land Records.
9.	Common law and statutory rights of upper and lower riparian owners in and to the watercourses flowing through said premises.
10.	The effect, if any, of a grant of easement in favor of The Southern New England Telephone Company dated February 2, 1900 and recorded February 8, 1900 in Volume 23, page 389 of the Wilton Land Records.
11.	A Lease from James Adlard to the Southern New England Telephone Company recorded February 10, 1900 in Volume 23, Page 391 of the Wilton Land Records.
12.	A right of way from Sarah E. Smith to Samuel D. Folsom as set forth in a deed dated June 14, 1907, and recorded June 15, 1907 in Volume 25, Page 543 of the Wilton Land Records.
13.	A grant from Marshall P. Richards to The Connecticut Light & Power Company dated May 29, 1923, and recorded June 4, 1923 in Volume 35, Page 162 of the Wilton Land Records.
14.	A grant from William B. Hurlbutt to The Connecticut Light & Power Company dated May 31, 1923 and recorded June 8, 1923 in Volume 35, Page 164 of the Wilton Land Records.
15.	An easement in favor of The Connecticut Light & Power Company dated July 23, 1923 and recorded August 10, 1923 in Volume 35, Page 199 of the Wilton Land Records.
16.	An easement from Marshall P. Richards to The Connecticut Light & Power Company dated September 19, 1923 and recorded September 26, 1923 in Volume 35, Page 228 of the Wilton Land Records.
17.	Flood encroachment lines as set forth in a report from the State of Connecticut, Water Resources Commission dated October 18, 1965 and recorded October 28, 1965 in Volume 115, Page 634 of the Wilton Land Records, as shown on Map No. 2499 and Map No. 2500 both on file in the Wilton Town Clerk's Office and as may be of record in the Wilton Land Records as of the date of this deed.
18.	The effect, if any, of a right to connect with a spur track as set forth in a deed from Adolph Musil to C.G.S. Laboratories, Inc., dated December 31, 1958 and recorded January 2, 1959 in Volume 77, Page 453 of the Wilton Land Records.
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- 19. A grant in favor of the State of Connecticut from The Perkin-Elmer Corporation dated June 4, 1971 and recorded August 10, 1971 in Volume 158, Page 337 of the Wilton Land Records, as shown on Map No. 156, and Map No. 157 both on file in the Wilton Town Clerk's Office.
- 20. Zoning Board of Appeals Notice recorded May 9, 1978 in Volume 300, Page 177 of the Wilton Land Records.
- Planning and Zoning Special Permit recorded April 29, 1981 in Volume 366, Page 177 of the Wilton Land Records.
- 22. An easement in favor of the State of Connecticut dated January 6, 1986 and recorded October 15, 1986 in Volume 566, page 264 of the Wilton Land Records, as shown on Map No. 4373 on file in the Wilton Town Clerk's Office.
- 23. Planning & Zoning Special Permit recorded July 2, 1987 in Volume 609, page 26 of the Wilton Land Records.
- 24. Planning & Zoning Resolution dated June 6, 1988 and recorded June 9, 1988 in Volume 649, Page 267 of the Wilton Land Records.
- 25. Planning & Zoning Resolution dated July 25, 1988 and recorded July 28, 1988 in Volume 655, Page 295 of the Wilton Land Records.
- 26. An easement in favor of the State of Connecticut dated May 6, 1986 and recorded March 25, 1991 in Volume 740, page 344 of the Wilton Land Records, as shown on Map 4694 on file in the Wilton Town Clerk's Office.
- 27. Planning & Zoning Special Permit recorded July 30, 1991 in Volume 754, page 197 of the Wilton Land Records.
- 28. The effect, if any, of rights of others in and to the spur track as set forth in a deed to 59 Danbury Road Associates, Inc., dated and recorded June 10, 1992 in Volume 791, Page 158 of the Wilton Land Records.
- 29. An easement in favor of the State of Connecticut dated July 2, 1993 and recorded July 8, 1993 in Volume 852, Page 55 of the Wilton Land Records, as shown on Map No. 4830 on file in the Wilton Town Clerk's Office.

To Have and To Hold the above granted and bargained premises, with the appurtenances thereof, unto it, the said grantee and unto its successors and assigns forever, to it and their own proper use and behoof.

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<u> </u>		
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presents, it is has good right the same is	also, It, the said grantor, does for itself, its successors and assigns, covenant with ntee and with its successors and assigns, that at and until the ensealing of these s well seized of the premises, as a good indefeasible estate in FEE SIMPLE; and ht to bargain and sell the same in manner and form as is above written; and that free from all encumbrances whatsoever, except as hereinbefore mentioned.	
bargained pr	Furthermore, It, the said grantor, does by these presents bind itself and its and assigns forever to WARRANT AND DEFEND the above granted and remises to it, the said grantee and its successors and assigns, against all claims is whatsoever, except as hereinbefore mentioned.	
IN W August, 1996	TTNESS WHEREOF, It has hereunto caused its seal to be set this lst day of 6	
Signed, Seale in the Preser	ed and Delivered	
	10 Strong THE PERKIN-ELMER CORPORATION	
- Willing	am S. Strele In. By Atenhen & Under	
CATHERI	NE MIAGEUS Duly Authorized	
STATE OF (	CONNECTICUT :	
COUNTY O	: ss.: , August 1, 1996 F FAIRFIELD :	
Person সেও ডেও the foregoing free act and		
	Commissioner of the Superior Court Notary Public Williams S. STeeleth	
	ss of Grantee: Drive, Suite 400	
California 95	5110	
ceived for Record Aug	ust 02, 1996 at 12:12 P. M. Attest Manuel De De	
	Town Clerks	
-		

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000066885 Bk:01348 Pg:00202

Grantor: SVG Lithography Systems, Inc. Grantee: ASML US, Inc.

#### CERTIFICATE OF CHANGE OF NAME

SVG LITHOGRAPHY SYSTEMS, INC., a Delaware corporation ("SVG"), the owner of certain real property commonly known as 77 Danbury Road, Wilton, Connecticut, and more particularly bounded and described on Schedule A attached hereto and made a part hereof, has merged into its parent corporation, ASML US, INC., a Delaware corporation having its principal place of business at 8555 South River Parkway, Tempe, AZ 85284 (the "Company"), with the Company being the surviving entity. A copy of the Certificate of Merger filed with the office of the Secretary of State of Delaware is attached hereto as Schedule B.

This certificate is duly acknowledged and given for record in compliance with Connecticut General Statutes \$47-12.

Dated this \_3/ day of December, 2001.

Witnesses:

1.

WALLE GERMAN J DI STATE OF CALIFORNIA

COUNTY OF the

By: vp Finance AMLKI Its:

**Duly** Authorized

ASML US, INC.

SAN Jos SS.:

The foregoing instrument was acknowledged before me this <u>4</u> day of <del>December, 2001</del> by <u>500</u> of ASMI. US. Inc. a Delaware corporation, on behalf of the corporation.



Notary Public Commission Expires: 2005

OR

H:WOMEWRC/SVG/SVG LITHOGRAPHY/CERT.CHANGE.NAME.DOC

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(name of signer[s]),

On December, 2001,	before me,		 (name and title of officer),
COUNTY OF	ý		
STATE OF CALIFORNIA	)	ss.:	

personally appeared

Π personally known to me

proved to me on the basis of satisfactory evidence Π

to be the person (s) whose name(s) is/are subscribed to the within instrument and acknowledged to me that he/she/they executed the same in his/her/their authorized capacity(ies), and that by his/her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

WITNESS my hand and official seal.

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t

(Signature of Notary Public)

(Place Notary Seal Above)

#### **OPTIONAL**

Though the data below is not required by law, it may prove valuable to persons relying on the document and could prevent fraudulent reattachment of this form.

#### CAPACITY CLAIMED BY SIGNER

DESCRIPTION OF ATTACHED DOCUMENT

Number of Pages

Date of Document

Title or Type of Document

П Individual

Corporate Officer 

	Title(s)		
П	Partner(s)	B	Limited
	0.0		General
0	Attorney-in-Fact		
П	Trustee(s)		
П	Guardian/Conservator		
п	Other:		
			_

Signers(s) Other Than Named Above

SIGNER IS REPRESENTING: Name of Person(s) or Entity(ies)

H.VIOMENRC/SVG/SVG LITHOGRAPHY/CERT.CHANGE.NAME.DOC

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# SCHEDULE A

#### TRACT ONE

All that fritinia piece or parcel of land, with the buildings and improventents is there on, siunced in the Town of Wilton, Coharty of Fairfield and Sinte of Connerlicus, and bounded and described as follows, to with Northerity by land now or formerly of Bliazbeth W. Rodger and by a stonewall: Existivity by the wastery bank of the Norwalk River, se-called, and hering land now or formerly of Marguesite. LA prodit thence metharly by land of Marguerite L. Arnold; thence satisfy by the Norwalk-Danbury Rood, Southerly by land new or formerly of Charles and Florence Houfes; and Westerly by land now or formerly of Charles and Florence Houfe, being the craiter line of the Norwalk River, theore southering and westerly by land of Charles and Florence Houfe; could all and Showalk River; theore southering and westerly by land of Charles and Florence Houfe; could all and Showalk River; theore southering and westerly by land of Charles and Florence Houfe; could all and Showalk River; theore southering not westerly by land of Charles and Florence Houfe; could all and Showalk River; theore southering not westerly by land of Charles and Florence Houfe; could all all storence for the souther and westerly by land of Charles and Florence Houfe; could all all storence southers, and being nore partfularly above on a central map entitled "Must and Showals River; theore southers, conversed to Lillian Bellie, Wilton, Connectives", Centified "Substantinity Corteor" by Walter K. Goodake, Grid Engineer, New Chansan, Conn., datad Dec. 8, 1947, Soule 1" = 40".

Being the same premises conveyed to The Farkin-Elmer Corporation by Theorest R. Lycon and John F. Lycon by Warrany Dred dated Dependers 1, 1965 and recorded in Volume 116, page 469 of the Wilton Land Records.

#### TRACT TWO

All thes contain place or parcel of land. In quantity 16.806 series, store or loss, white the buildings and improvements thereon, situated in the Town of Wilton, County of Palefald and State of Contextuot, and bounded and described as follows:

by the Norwalk-Danbury Road, U.S. Route #7;
by laid now or formerly of Frantisea Vogel;
by had now or formerly of Frantisen Vogel;
by land now or formerty of Frantises Vogel;
by the Narwells-Danbury Branch of the New York, New Kaved and Hardord Railroad;
by land now or formerly of Harry Richmondy
by land now or farmarty of Robias P. Crowell;
by land now or formerly of Robins F. Crewell:
by land now or formerly of said Robins P. Crowell along the crater lise of the Norwalk River;
by land now or formerly of said Robins P. Crowell.

Said property being the ensuerly parcel of the premises shown on a certain map entitled "Map of Froperty Belonging to Elizabeth and Lemuel Hurburn and W.B. Hurburt, Esg. situated as South Wilton, Cond.", on Sie in the Office of the Town Clerk of the Town of Wilton and sumbared 68, reference therein being had.

Being the same premites conveyed to The Petkin-Elmar Corporation by The Hallicrafters Co. by Warranty Deed dated April 1, 1966 and recorded in Volume 113, page 399 of the Witton Land Records. . .----.... .

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# SCHEDULE A-1

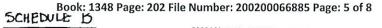
#### TRACT TURES

All that cortain piece, partel or tract of land rogether with the buildings and improvements thereton, and the brankag, vanilating and is conditioning approved that the labereto, tituated in the Town of Wilton, designated as "Ares - 642 A.T. and labereto delineated on a cortain map estilized "Map of Property Properts Town Cert to the said Town of Wilton as the map numbered 1460, reference thereto haling hand. Said premises are bounded and desertbed as follows: Beginning at a polot on the watery line of Danbury Road marking the intersection therwith of the land herein described and land gow or formerly of C.O.S. Laboratories, i.e., which polot of lournerston is marked by a Connectiont Highway Department measures, and runalag thereas in a generally resistry direction along the northerly line of said land new or formerly of C.O.S. Laboratories, j.e., has blood for the said distances. North 61' 47' 20' West 340.00 feet, South 32' 41' 00' West 405.15 fact, South 61' 03' 20' West 94:51 fact, and North 78' 34' Wat 310.35 fact to the easterly line of land of the Foun Cantral Transportation Company, Darbury Rest and otherly of contents of the Found and here and state of the said land of the assign is a northerly direction along the marked by a set of both sets of land of the Found Cantral Transportation Company, Darbury Rest.

Contral Transportations Company, Danbury Branch, North 11° 26' East 450.57 feet to the southerly line of land new or formerly of Peter E. Obset results there is a generally sharing directions along the southerly line of and land new or formisity of Peter E. Obset, the following courses and distances: South 35' 24' 10' East 132.40 feet. Bouh 74' 37' 10' East 74.50 feet. South 55' 01' 10' East 47.20 feet, Bouh 44' 38' 10' East 74.50 feet. South 34' 12' 10' East 36:00 feet, South 75' 00' 50' East 30.10 feet. South 75' 23' 10' East 136:00 feet, and South 75' 14' 10' East 230.70 feet to a polait running there is a wortherly distribution along the seaterly line of takid land new or formerly of Peter E. Obset North 74' 35' 30' East 36:40 feet to a polait running there is a south 75' 23' 10' East 31.20 feet. South 74' 31' 10' East 122.77 feet to the worterly file of Danbury Road South 73' Weet 199.16 feet and South 59' 31' 10' East 122.77 feet to the worterly line of Land new or formerly of C.O.3. Laboratorics. Inct, bring its south or place of beginning. Together with all rights appartenses therein brief lines of the to the southerly line of Land new or formerly of C.O.3. Laboratorics. Inct, bring its point or place of beginning. Together with all rights appartenses therein brief long the water courses flowing through the premises and to the Norwelk Rives and any other water courses flowing through the premises and the use of the prights and spur railroad track harding the mentioned and rights of Way.

Being the same premises conveyed to The Perkin-Einer Corporation by Joan H. Fastman, formerly known as Joan H. Peter, Executive under the last will and testament of Henvey A. Pete by an Executive Deed dated January 6, 1981 and recorded in Volume 361, Page 268 of the Wiljoin Land Records.

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The First State

I, HARRIET SMITH WINDSOR, SECRETARY OF STATE OF THE STATE OF DELAWARE, DO HEREBY CERTIFY THE ATTACHED IS A TRUE AND CORRECT COPY OF THE CERTIFICATE OF OWNERSHIP, WHICH MERGES:

"SVG LITHOGRAPHY SYSTEMS, INC.", A DELAWARE CORPORATION,

WITH AND INTO "ASML US, INC." UNDER THE NAME OF "ASML US, INC.", A CORPORATION ORGANIZED AND EXISTING UNDER THE LAWS OF THE STATE OF DELAWARE, AS RECEIVED AND FILED IN THIS OFFICE THE TWENTY-EIGHTH DAY OF DECEMBER, A.D. 2001, AT 2 O'CLOCK P.M.

AND I DO HEREBY FURTHER CERTIFY THAT THE EFFECTIVE DATE OF THE AFORESAID CERTIFICATE OF OWNERSHIP IS THE THIRTY-FIRST DAY OF DECEMBER, A.D. 2001.

A FILED COPY OF THIS CERTIFICATE HAS BEEN FORWARDED TO THE NEW CASTLE COUNTY RECORDER OF DEEDS.

2114543 B100M

Varriet Smith Windson

Harriet Smith Windsor, Secretary of State AUTHENTICATION: 1535710

DATE: 01-02-02

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: . .

STATE OF DELAMARE SECRETARY OF STATE DIVISION OF CORPORATIONS FILED 02:00 FM 12/28/2001 010674325 - 2114543

#### CERTIFICATE OF OWNERSHIP AND MERGER

#### MERGING

#### SVG LITHOGRAPHY SYSTEMS, INC. (A Delaware Corporation)

#### INTO

#### ASML US, INC. (A Delaware Corporation)

#### (Pursuant to Section 253 of the General Corporation Law of Delaware)

We, the undersigned Peter T.F.M. Wennink and Robert F. Roelofs, hereby certify as to the following facts relating to the merger of SVG Lithography Systems, Inc, and ASML US, Inc. (the "Merger"):

- 1. We are the President and Secretary, respectively, of ASML US, Inc., a corporation organized under the laws of the State of Delaware (the "Company"), the provisions of which permit the merger of a subsidiary corporation into a parent corporation.
- The Company owns at least 90% of the outstanding shares of SVG Lithography Systems, Inc., a Delaware corporation ("SVGL").
- The sole minority stockholder of SVGL owns less than 10% of the shares of Common Stock of SVGL.
- SVGL is hereby merged with and into ASML US, Inc., and the name of the surviving corporation shall be ASML US, Inc. (the "Surviving Corporation").
- The 5,000 shares of Common Stock of SVGL held by the sole minority stockholder is hereby converted into the right to receive an aggregate of \$37,000.00 upon the effectiveness of the Merger.
- 6. This Certificate of Merger shall be effective on December 31, 2001.
- The Board of Directors of the Company duly adopted the following resolutions on December 21, 2001 by unanimous written consent:

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# Merger of SVG Lithography Systems, Inc. with and into the Company

WHEREAS, the Company lawfully owns at least 90% of the capital stock of SVG Lithography Systems, Inc., a Delaware corporation ("SVGL"), and now desires to merge SVGL with and into the Company:

NOW, THEREFORE, BE IT RESOLVED: That the Board of Directors of the Company hereby determines that it is in the best interests of the Company and SVGL to merge SVGL with and into the Company, and for the Company to assume all of the liabilities and obligations of SVGL for all such actions to be carried out by the Company, as the majority stockholder of SVGL;

**RESOLVED FURTHER:** Upon completion of the merger, the five thousand (5,000) shares of SVGL Common Stock held by the sole minority stockholder will be automatically converted upon surrender of the certificate or certificates representing such shares of common stock into the right to receive \$37,000.00.

**RESOLVED FURTHER:** That the aggregate cash consideration of \$37,000.00 to be paid to the sole minority stockholder is fair, just and reasonable consideration for the five thousand (5,000) shares of SVGL common stock held by such stockholder.

**RESOLVED FURTHER:** That the Certificate of Ownership and Merger, substantially in the form attached hereto as  $\underline{\text{Exhibit } A}$ , is hereby approved and authorized in all respects, with such changes, additions, deletions, supplements and amendments thereto as the Chief Executive Officer, President or any Vice President of the Company may deem necessary or advisable, such determination to be conclusively evidenced by his or her execution thereof; and that each of the Chief Executive Officer, President of the Company is authorized and directed to execute and deliver the Certificate of Ownership and Merger on behalf of the Company, and to file the same in the office of the Secretary of State of the State of Delaware.

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Book: 1348 Page: 202 File Number: 200200066885 Page: 8 of 8

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IN WITNESS WHEREOF, the undersigned have executed this Certificate of Ownership and Merger this 21<sup>st</sup> day of December 2001.

1 1

/s/ Peter T, F. M. Wennink Peter T.F.M. Wennink President

/s/ Robert F. Roelofs Robert F. Roelofs Secretary

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RECEIVED FOR RECORD 01/17/2002 AT 03:17:15PM ATTEST: Bettye Joan Ragognetti TOWN CLERK



GREGORY AND ADAMS, P.C. 190 Old Ridgefield Road Wilton, Connecticut 06897

#### Certificate of Change of Name

#### TO WHOM IT MAY CONCERN:

Be it known that **ASML US, LLC**, a Delaware limited liability company, owning property by virtue of a deed recorded in the land records of the Town of Wilton, County of Fairfield and State of Connecticut, in Volume 1002 at Page 329 in the name of **SVG LITHOGRAPHY SYSTEMS, INC.**, which name was previously changed to **ASML US, INC.** by Certificate of Change of Name dated December 31, 2001 and recorded in Volume 1348 at Page 202 of the Wilton Land Records, and which name has now been changed to **ASML US, LLC** by virtue of Certificate of Conversion (a copy of which is attached hereto as Exhibit A), has duly acknowledged this certificate and given it for record in compliance the statutory requirements of the State of Connecticut. Premises commonly known as: **77 Danbury Road, Wilton, Connecticut** 

Dated this 30<sup>th</sup> day of January, 2019.

Witnesses:

for Fulling

SS:

State of Arizona County of Maricopa ASML US, LLC

By: Keith Maki Its: Treasurer Duly Authorized

Date: 30 Jan 2019

Personally appeared ASML US, LLC, acting herein by <u>Keith Maki</u>, its <u>Treasurer</u>, duly authorized, who subscribed and swore to the truth of the foregoing certificate, and who acknowledged that he executed the same before me, the undersigned officer.



NichelleKtholi

Notary Public My Commission Expires: 3/30/2019



Page 1

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I, JEFFREY W. BULLOCK, SECRETARY OF STATE OF THE STATE OF DELAWARE, DO HEREBY CERTIFY THAT THE ATTACHED IS A TRUE AND CORRECT COPY OF THE CERTIFICATE OF CONVERSION OF A DELAWARE CORPORATION UNDER THE NAME OF "ASML US, INC." TO A DELAWARE LIMITED LIABILITY COMPANY, CHANGING ITS NAME FROM "ASML US, INC." TO "ASML US, LLC", FILED IN THIS OFFICE ON THE NINETEENTH DAY OF DECEMBER, A.D. 2017, AT 5:53 O'CLOCK P.M.

AND I DO HEREBY FURTHER CERTIFY THAT THE EFFECTIVE DATE OF THE AFORESAID CERTIFICATE OF CONVERSION IS THE FIRST DAY OF JANUARY, A.D. 2018 AT 11 O'CLOCK A.M.



cretary of State

Authentication: 203809833 Date: 12-21-17

3294667 8100V SR# 20177671237

You may verify this certificate online at corp.delaware.gov/authver.shtml

State of Delaware Secretary of State Division of Corporations Delivered 05:53 PM 12/19/2017 FILED 05:53 PM 12/19/2017 SR 20177671237 - File Number 3294667

#### ASML US, INC.

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#### STATE OF DELAWARE CERTIFICATE OF CONVERSION FROM A CORPORATION TO A LIMITED LIABILITY COMPANY PURSUANT TO SECTION 18-214 OF THE LIMITED LIABILITY COMPANY ACT

1, The jurisdiction where the Corporation first formed is Delaware.

2. The jurisdiction immediately prior to filing this Certificate is Delaware.

3. The date the Corporation first formed is September 28, 2000.

4. The name of the Corporation immediately prior to filing this Certificate is "ASML US, Inc."

5. The name of the Limited Liability Company as set forth in the Certificate of Formation is "ASML US, LLC."

6. This Certificate of Conversion shall be effective at 11:00 a.m. Bastern Standard Time on January 1, 2018.

\* \* \*

QB\130429,00585\47522721.1

IN WITNESS WHEREOF, the undersigned has executed this Certificate as of the 19th day of December, 2017.

Name: Jorry Drube Title: Authorized Person

[Signature Page to Certificate of Conversion]

QB\130429.00585\47522721.1

-2-

Delaware

The First State

I, JEFFREY W. BULLOCK, SECRETARY OF STATE OF THE STATE OF DELAWARE DO HEREBY CERTIFY THAT THE ATTACHED IS A TRUE AND CORRECT COPY OF THE CERTIFICATE OF FORMATION OF "ASML US, LLC" FILED IN THIS OFFICE ON THE NINETEENTH DAY OF DECEMBER, A.D. 2017, AT 5:53 O`CLOCK P.M.

AND I DO HEREBY FURTHER CERTIFY THAT THE EFFECTIVE DATE OF THE AFORESAID CERTIFICATE OF FORMATION IS THE FIRST DAY OF JANUARY, A.D. 2018 AT 11 O'CLOCK A.M.



Julitay Wi Bulluck, Steeriary of State

Authentication: 203809833 Date: 12-21-17

Page 1

3294667 8100V SR# 20177671237

· · · ·

You may verify this certificate online at corp.delaware.gov/authver.shtml

State of Delaware Secretary of State Division of Corporations Delivered 05:53 PM 12/19/2017 FILED 05:53 PM 12/19/2017 SR 20177671237 - File Number 3294667

#### CERTIFICATE OF FORMATION

....

:

#### OF

#### ASML US, LLC

This Certificate of Formation is being executed as of this 19th day of December, 2017, for the purpose of forming a limited liability company pursuant to the Delaware Limited Liability Company Act, *Title 6 Del. Code* §§18-101, et seq.

The undersigned, being duly authorized to execute and file this Certificate of Formation, does hereby certify as follows:

1. Name. The name of the limited liability company is:

ASML US, LLC (the "Company"),

2. Registered Office and Registered Agent. The address of the Company's registered office in the State of Delaware is:

Corporation Trust Center 1209 Orange Street Wilmington, New Castle County, Delaware 19801

The name of the Company's registered agent at such address is:

The Corporation Trust Company

3. *Effective Time.* This Certificate of Formation shall be effective at 11:00 a.m. Eastern Standard Time on January 1, 2018.

\* \* \*

IN WITNESS WHEREOF, the undersigned has duly executed this Certificate of Formation as of the day and year first above written.

Name: erry Drube Title:\_ Authorized Person

[Signature Page to Certificate of Formation]

QB\130429.00585\47522490.1

-2-

Received for Record at Wilton, CT On 02/05/2019 At 10:49:00 am

Sani a. Holor to

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:

#### ASML USA, Inc. Application for Special Permit

### Premises: 77 Danbury Road, Wilton, Connecticut

#### Property Owners Within 500 Feet (Assessor's Map#69, Lot#18)

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)		
	Wilton Child Development Park, LLC			
68-21	11 Grumman Hill Road			
	Wilton, CT 06897			
	Holt McChord			
68-22	1 Grumman Hill Road			
	Wilton, CT 06897			
	Trofa Property Development LLC	236 Colonial Drive		
68-23	70 Danbury Road	Fairfield, CT 06824		
	Wilton, CT 06897			
	Trofa Property Development LLC	236 Colonial Drive		
68-24	3 Hollyhock Lane	Fairfield, CT 06824		
	Wilton, CT 06897			
	Vikram Mital			
68-25	5 Hollyhock Lane			
	Wilton, CT 06897			
(0.0)	7 R2 Properties LLC			
68-26	7 Hollyhock Lane			
	Wilton, CT 06897			
(0.07	Fujii Properties, LLC	9 Clubhouse Circle		
68-27	9 Hollyhock Lane	Darien, CT 06820		
	Wilton, CT 06897			
68-29	Hollyhock Associates LLC	10 Cliff Avenue		
08-29	6 Hollyhock Lane	Darien, CT 06820		
	Wilton, CT 06897 Clark Holdings LLC	245 Nourtourn Turneileo		
68-30	2 Hollyhock Lane	245 Newtown Turnpike		
08-30	Wilton, CT 06897	Weston, CT 06883		
	Wilton 40 LLC	Marcus Partners Acctg. Dept.		
68-33-1	40 Danbury Road	301 Merritt 7		
00 55 1	Wilton, CT 06897	Norwalk, CT 06851		
	Wilton 50 Danbury Road Owner LLC	280 Park Ave., 5 <sup>th</sup> Floor		
68-33-50	50 Danbury Road	New York, NY 10017		
	Wilton, CT 06897			
	Wilton Medical Realty, LLC	100 Avon Meadow Lane		
68-33-60	60 Danbury Road	Avon, CT 06001		
	Wilton, CT 06897			

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT) 280 Park Ave., 5 <sup>th</sup> Floor	
TICHIDIA	Wilton 64 Danbury Road Owner LLC		
68-33-64	64 Danbury Road	New York, NY 10017	
00 55 01	Wilton, CT 06897		
	Wilson Properties II, LLC	43 Danbury Road	
68-35	57 Danbury Road	Wilton, CT 06897	
	Wilton, CT 06897		
	Wilton Project LLC	Metro Center	
68-36-A	65 Danbury Road	One Station Place	
	Wilton, CT 06897	Stamford, CT 06902	
	Wilton Properties RSK LLC	470 West Ave., Ste. 2007	
68-36-В	59 Danbury Road	Stamford, CT 06902	
	Wilton, CT 06897		
	Wilton Project LLC	Metro Center	
68-36-C	Danbury Road	One Station Place	
	Wilton, CT 06897	Stamford, CT 06902	
	Louis Florio		
69-13	50 McFadden Drive		
	Wilton, CT 06897		
	State of Connecticut	2800 Berlin Turnpike	
69-14	McFadden Drive	Newington, CT 06131	
	Wilton, CT 06897		
	State of Connecticut	2800 Berlin Turnpike	
69-15	54 McFadden Drive	Newington, CT 06131	
	Wilton, CT 06897		
	Thomas F. Hickey		
69-20	Joseph C. Shafranek, Jr.		
	89 Danbury Road		
	Wilton, CT 06897		
	Thomas F. Hickey	89 Danbury Road	
69-21	Joseph C. Shafranek, Jr.	Wilton, CT 06897	
	Danbury Road		
	Wilton, CT 06897		
	Town of Wilton	238 Danbury Road	
69-22	91 Danbury Road	Wilton, CT 06897	
	Wilton, CT 06897		
	Ottaviano Veccia		
69-23	Giovanna Veccia		
	3 Arrowhead Road		
	Wilton, CT 06897		
	Paul T. Egan		
69-24	Sonia E. Egan		
	23 Arrowhead Road		
	Wilton, CT 06897		

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)		
	Sabrina Gibbs			
69-25	25 Arrowhead Road			
	Wilton, CT 06897			
	Zena Kim	23-88 31 <sup>st</sup> St., #5D		
69-26	27 Arrowhead Road	Astoria, NY 11105		
	Wilton, CT 06897			
	Laurence J. Arnold			
69-27	Sandra P. Arnold			
	Ericalynn Arnold			
	29 Arrowhead Road			
	Wilton, CT 06897			
	Wilson Contreras			
69-28	Jorge Bermeo			
	33 Arrowhead Road			
	Wilton, CT 06897			
	Nicholas J. Varrone			
69-29	Michelle L. Varrone			
	39 Arrowhead Road			
	Wilton, CT 06897			
	State of Connecticut	2800 Berlin Turnpike		
69-30	41 Arrowhead Road	Newington, CT 06131		
09 50	Wilton, CT 06897			
	State of Connecticut	2800 Berlin Turnpike		
69-31	42 Arrowhead Road	Newington, CT 06131		
07 51	Wilton, CT 06897			
	Pamela J. Musor			
69-32	40 Arrowhead Road			
07 52	Wilton, CT 06897			
	Michael W. Barnett			
69-33	Susan G. Barnett			
09-33	34 Arrowhead Road			
	Wilton, CT 06897			
	Arrowhead Community Association	Susan Barnett		
69-34				
	34 Arrowhead Road			
	Wilton, CT 06897	Wilton, CT 06897		
(0.5)	Brookdale Place of Wilton LLC	c/o Brookdale Senior Living – Acctg.		
69-56	96 Danbury Road	6737 W. Washington St., Ste. 2300		
(0.50	Wilton, CT 06897	Milwaukee, WI 53214		
	88 Danbury Road LLC	c/o Furst Properties		
69-58	88 Danbury Road	14648 N. Scotsdale Road, Ste. 140		
	Wilton, CT 06897	Scottsdale, AZ 85254		
	Danbury 84 LLC	2 Ruby Street		
69-59	84 Danbury Road	Norwalk, CT 06850		
	Wilton, CT 06897			

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)	
	Grumman Seven Associates, LLC	c/o Phillip Florio	
69-60	78 Danbury Road	82 Danbury Road	
	Wilton, CT 06897	Wilton, CT 06897	
	Piyush Pandey		
69-61-2	Anju Pandey		
	2 Village Court		
	Wilton, CT 06897		
	Robert P. Chiavon		
69-61-4	Peggy A. Chiavon, Trustees		
	4 Village Court		
	Wilton, CT 06897		
	Glenn A. Hutchinson		
69-61-6	6 Village Court		
	Wilton, CT 06897		
	Christopher V. Salvato		
69-61-8	Linda A. Salvato		
	8 Village Court		
	Wilton, CT 06897		
	Danjie Liu		
69-61-10	Yan Jiang		
	10 Village Court		
	Wilton, CT 06897		
	Raymond R. Koziak		
69-61-12	130 Lenox Ave., #9		
	Stamford, CT 06906		
	Joseph P. Careccia		
69-61-14	Olga Sidiropoulis		
	14 Village Court		
	Wilton, CT 06897		
	Kimberly Duffy		
69-61-16	16 Village Court		
	Wilton, CT 06897		
	Michael J. Gagliano		
69-61-18	Malgorzata Gagliano		
	18 Village Court		
	Wilton, CT 06897		
	Yubo Lu		
69-61-20	20 Village Court		
	Wilton, CT 06897		
	Anusha Thota		
69-61-22	Sandeep Malluri		
	22 Village Court		
	Wilton, CT 06897		

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)		
	Audrey Kurtz			
69-61-24	24 Village Court			
	Wilton, CT 06897			
	James E. Arenholz, Jr.			
69-61-26	26 Village Court			
	Wilton, CT 06897			
	Rosemary R. Vervoort			
69-61-28	Gary R. Vervoort			
	28 Village Court			
	Wilton, CT 06897			
	Assaf Eisdorfer			
69-61-30	Danit Eisdorfer			
	30 Village Court			
	Wilton, CT 06897			
	Elizabeth B. Callahan			
69-61-32	32 Village Court			
	Wilton, CT 06897			
	Ross S. Kazer			
69-61-34	Vicki W. Kazer			
	34 Village Court			
	Wilton, CT 06897			
	Paula D. Fleming			
69-61-36	36 Village Court			
	Wilton, CT 06897			
	Mark Emerick			
69-61-38	Jacquelyn Emerick			
	38 Village Court			
	Wilton, CT 06897			
	Kara Crowther			
69-61-40	40 Village Court			
	Wilton, CT 06897			
	Current Resident			
69-61-42	42 Village Court			
	Wilton, CT 06897			
	Yook Cheng Yen Ling			
69-61-44	44 Village Court			
	Wilton, CT 06897			
69-61-46	Bomi P. Dinshaw			
	Nina B. Dinshaw			
	46 Village Court			
	Wilton, CT 06897			
(0 (1 10	Marie Dunn			
69-61-48	48 Village Court			
	Wilton, CT 06897			

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)		
	Princelal Chiriyankandath			
69-61-50	Hency P. Chiriyankandath			
	50 Village Court			
	Wilton, CT 06897			
	Di Zhang			
69-61-52	Feng Zhang			
	52 Village Court			
	Wilton, CT 06897			
	Paul H. Luchansky			
69-61-54	Toni-Anne Luchansky			
	54 Village Court			
	Wilton, CT 06897			
	Monica R. Sprei			
69-61-56	56 Village Court			
	Wilton, CT 06897			
	Arun Swaminathan			
69-61-58	Sumithra Bakthavatchalam			
	58 Village Court			
	Wilton, CT 06897			
	Laura Cody			
69-61-60	60 Village Court			
	Wilton, CT 06897			
	Samira Vedantam			
69-61-62	Amith Mamidala			
	62 Village Court	5		
	Wilton, CT 06897			
	Kenneth Daniel Libby			
69-61-64	64 Village Court			
	Wilton, CT 06897			
	Ulysses Whitby			
69-61-66	Gussie Whitby			
	66 Village Court			
	Wilton, CT 06897			
	Serge A. Karpow			
69-61-68	68 Village Court			
	Wilton, CT 06897			
	Joann Logiurato			
69-61-70	70 Village Court			
	Wilton, CT 06897			
	Joseph Zarb			
69-61-72	Rose Zarb			
	72 Village Court			
	Wilton, CT 06897			

MAP/LOT NUMBER	OWNER'S NAME PROPERTY ADDRESS	MAILING ADDRESS (IF DIFFERENT)		
	John B. Canning			
69-61-74	Janet S. Canning			
	74 Village Court			
	Wilton, CT 06897			
	Gian Andreassi			
69-61-76	76 Village Court			
	Wilton, CT 06897			
	Arun Mahadevan Venkataman			
69-61-78	Radhika Nagaratnam			
	78 Village Court			
	Wilton, CT 06897			
	Tianshi Bu			
69-61-80	Kun Dong			
	80 Village Court			
	Wilton, CT 06897			
	Lee Armstrong	5		
69-61-82	82 Village Court			
	Wilton, CT 06897			
	Syma B. Gruss Revocable Trust			
69-61-84	84 Village Court			
	Wilton, CT 06897			
	Manuel T. Bastos			
69-61-86	Florinda F. Bastos			
	86 Village Court			
	Wilton, CT 06897			
	Stacey E. Reynolds			
69-61-88	88 Village Court			
	Wilton, CT 06897			
	Mark A. Messina			
69-61-90	Michele D. Messina			
	90 Village Court			
	Wilton, CT 06897			
	Kunwar Kalra			
69-61-92	Ruchika Khurana			
	92 Village Court			
	Wilton, CT 06897			
	Richard K. Dineen			
69-61-94	Claire Dineen			
	94 Village Court			
	Wilton, CT 06897			
(D) (A) D (	Lamba Tarun			
69-61-96	Talreja Jharna			
	96 Village Court			
	Wilton, CT 06897			

MAP/LOT	OWNER'S NAME	MAILING ADDRESS (IF		
NUMBER	PROPERTY ADDRESS	DIFFERENT)		
70-16-1	The Connecticut Light & Power Co.	P.O. Box 270		
	Danbury Road	Hartford, CT 06141		
	Wilton, CT 06897			
	Wilton Land Conservation Trust	P.O. Box 77		
84-15	Chessor Lane	Wilton, CT 06897		
	Wilton, CT 06897			
84-15-A	State of Connecticut	2800 Berlin Turnpike		
	Penn Central RR	Newington, CT 06131		
	Wilton, CT 06897	5		
84-15-9	Yang Zhang			
	Qiang Li			
	54 Chessor Lane			
	Wilton, CT 06897			
84-15-10	Dawn L. Padovan			
	50 Chessor Lane			
	Wilton, CT 06897			
	Troy A. Prario			
84-15-11	Lauren B. Prario			
	46 Chessor Lane			
	Wilton, CT 06897			
	J.A.&S.J. Burke Revocable Living Trust			
84-15-12	42 Chessor Lane			
	Wilton, CT 06897			
	State of Connecticut	2800 Berlin Turnpike		
84-16	Penn Central Railroad	Newington, CT 06131		
	Wilton, CT 06897			
84-17-A	State of Connecticut	2800 Berlin Turnpike		
	Kent Hills Lane	Newington, CT 06131		
	Wilton, CT 06897			
84-36	45 Danbury Rd. LLC	One Corporate Drive, Suite 100		
	45 Danbury Road	Shelton, CT 06484		
	Wilton, CT 06897			
84-39	Rings End Incorporated	181 West Avenue		
	53 Danbury Road	Darien, CT 06820		
	Wilton, CT 06897	Buildi, OT 00020		
84-40	Wilton Pediatrics Realty LLC			
	55 Danbury Road			
	Wilton, CT 06897			
	Lisa Ann Crosby			
85-7	60 McFadden Drive	5		
05-7	Wilton, CT 06897			
	witton, C1 00097			

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#### ASML US, LLC

#### Land Use Applications to Town of Wilton

#### Premises: 77 Danbury Road, Wilton, CT

#### List of Project Professionals

1. Owner and Applicant

ASML US, LLC c/o Gregory and Adams, P.C. 190 Old Ridgefield Road Wilton, CT 06897

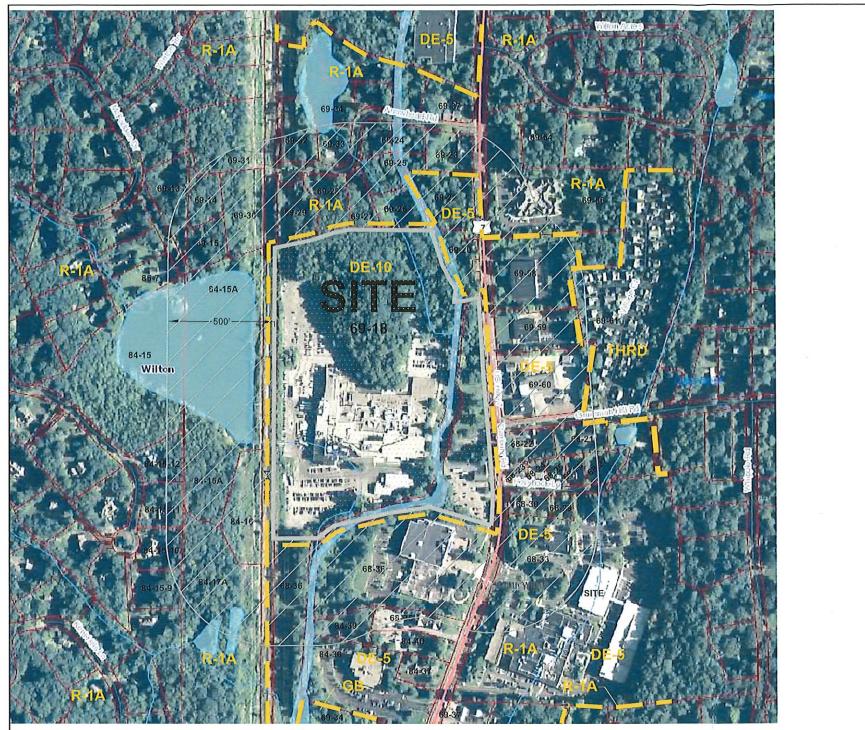
Mr. Jason Domena jason.domena@asml.com Mr. Patrick Van Den Bogaard patrick.van.den.bogaard@asml.com

2. Surveyor and Civil Engineer

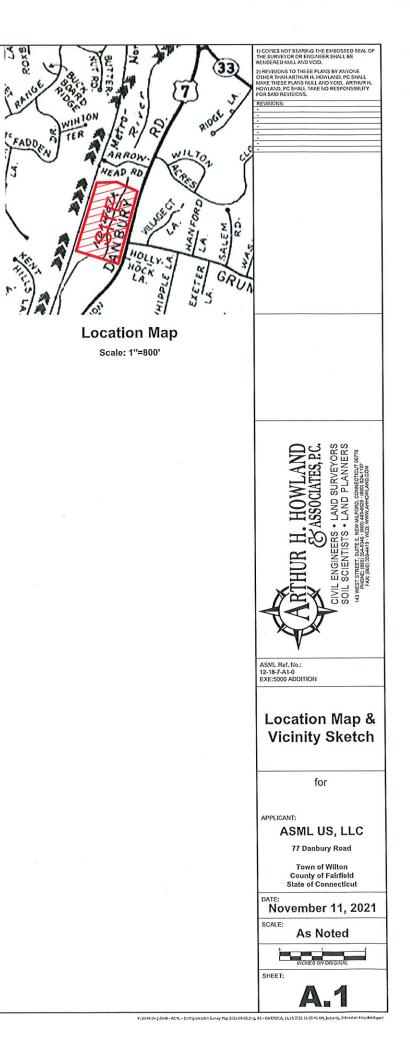
3. Attorney

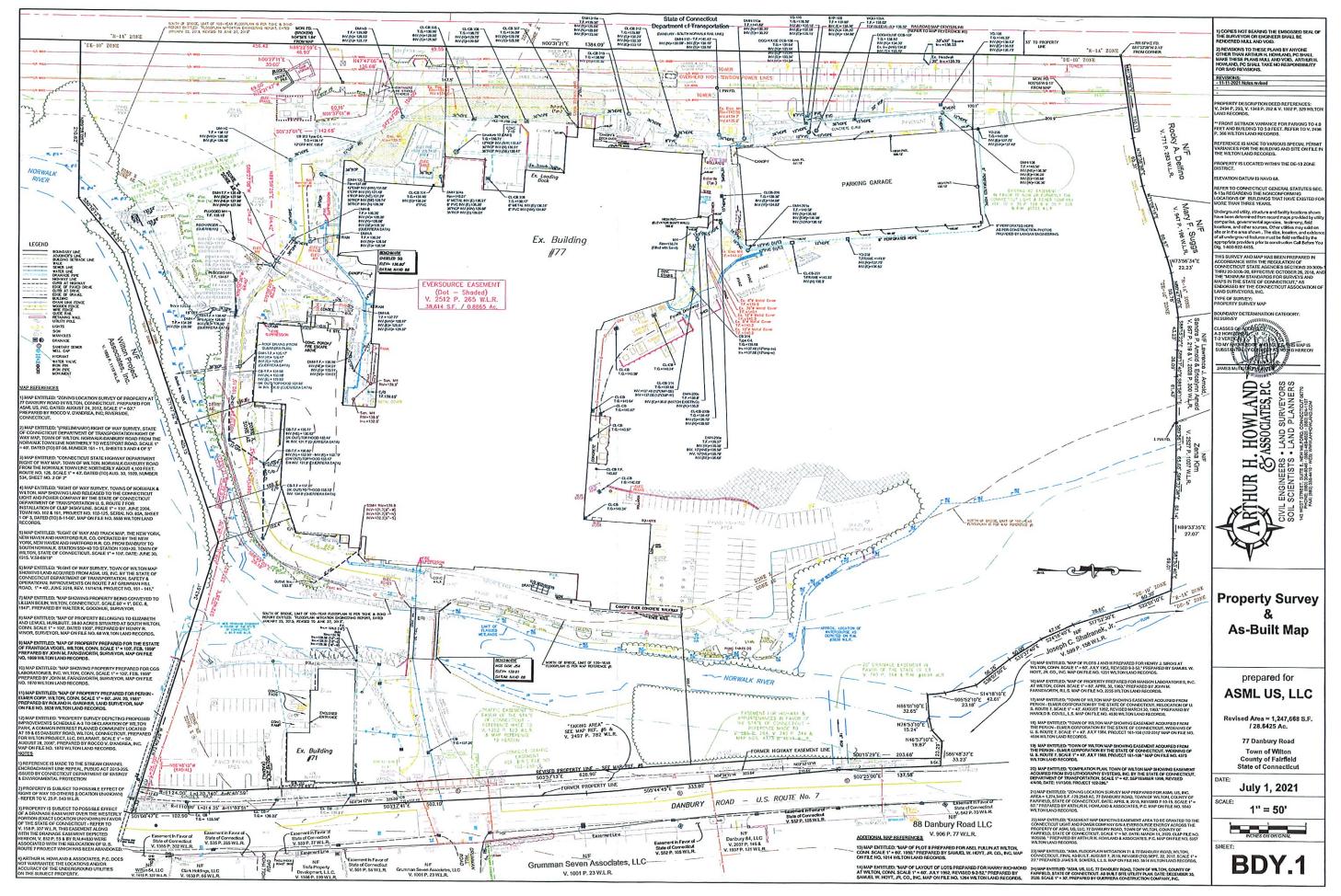
John W. Block, P.E. Mr. Joseph A. Canas Tighe & Bond, Inc. 1000 Bridgeport Avenue Shelton, CT 06484 jwblock@tighebond.com jacanas@tighebond.com (203) 712-1100

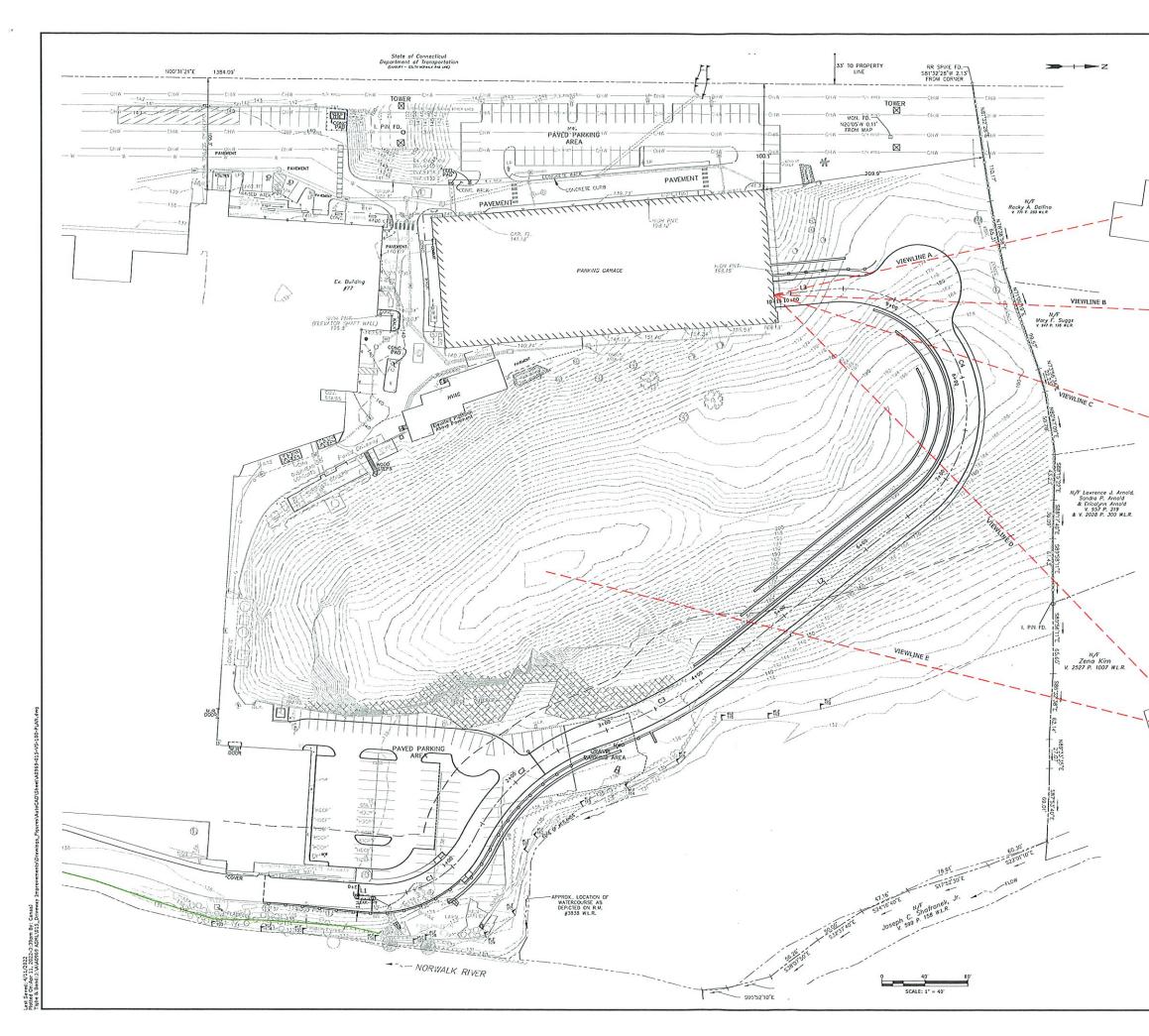
James D'Alton Murphy, Esq. Kathleen L. Royle, Esq. Gregory and Adams, P.C. 190 Old Ridgefield Road Wilton, CT 06897 jmurphy@gregoryandadams.com kroyle@gregoryandadams.com (203) 762-9000

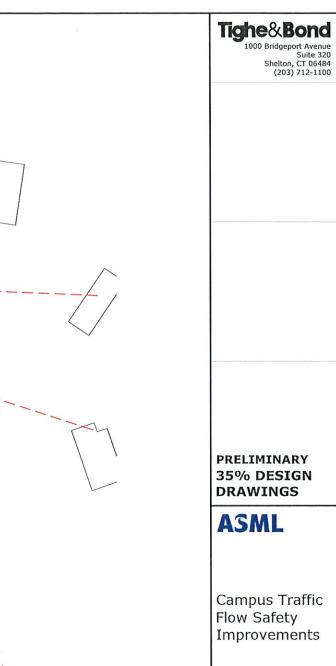


Vicinity Sketch Scale: 1"=200'









77 Danbury Road Wilton, Connecticut

MARK	DATE	DESCRIPTION
PROJECT	T NO:	A0969-015
DATE:		04/12/2022
FILE:		959-015-VS-100-PLAN.dng
DRAWN	BY:	MDS
DESIGN	ED/CHECK	ED BY: JAC
APPROV	ED BY:	JWB
		LINE STUDY CATIONS
SCALE	:	1" = 40
	١	/-100





DATE FCT NO:

VED BY:

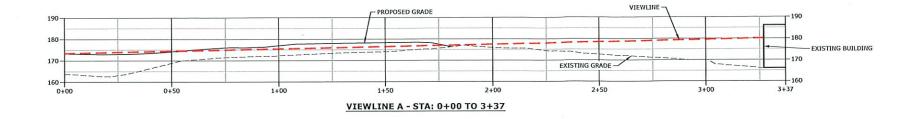
CALE:

04/12 A0969-015-VS-101-PLAN-AE MDS

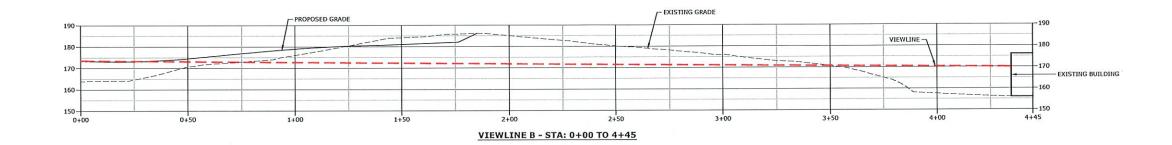
JWB VIEW LINE STUDY LOCATIONS (AERIAL IMAGERY)

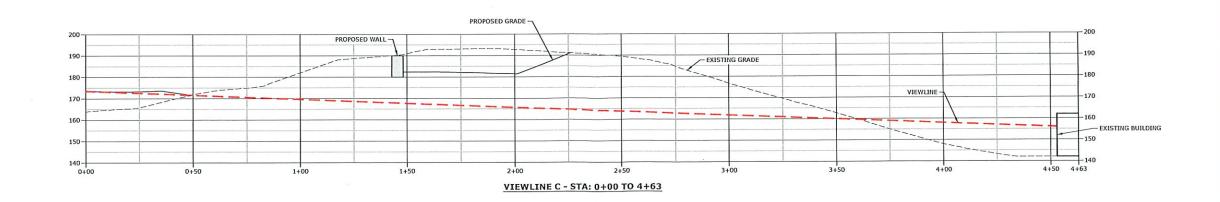
V-101

1" = 40

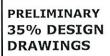


Last Saved: 4/11/2022 Plotted On:Apr 11, 2022-3:39pm By: Canas) Tinhe & Bond:3: (A)40969 ASML/015\_Drivews











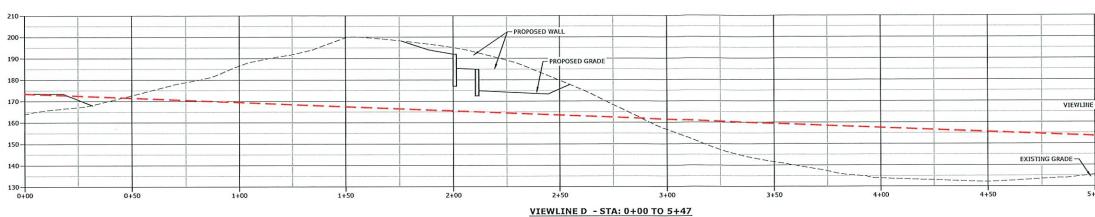
Campus Traffic Flow Safety Improvements

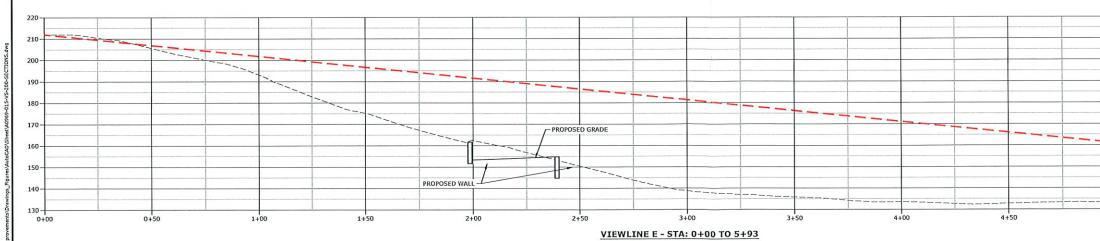
77 Danbury Road Wilton, Connecticut



V-200

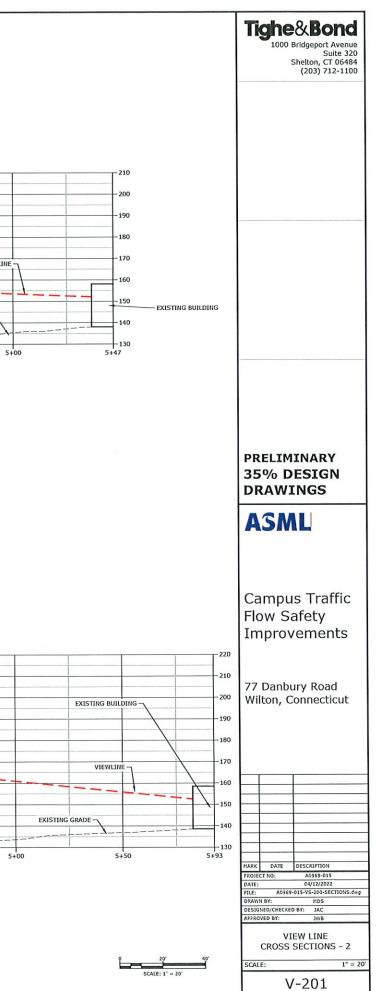
SCALE: 1" = 20'





Last Saved: 4/11/2022 Plotted On:Apr 11, 2022-3:39pm By: CunasJ Tighe & Bond:3:XA/A0969 ASML/015\_Drivew:

4





VIEWLINE B NOTE: VIEWS ARE DEPICTED WITHOUT PROPOSED SCREENING



VIEWLINE E NOTE: VIEWS ARE DEPICTED WITHOUT PROPOSED SCREENING



**VIEWLINE A** NOTE: VIEWS ARE DEPICTED WITHOUT PROPOSED SCREENING



VIEWLINE C NOTE: VIEWS ARE DEPICTED WITHOUT PROPOSED SCREENING

Tighe& Bond 1000 Bridgeport Avenue Suite 320 Shelton, CT 05484 (203) 712-1100

# PRELIMINARY 35% DESIGN DRAWINGS



Campus Traffic Flow Safety Improvements

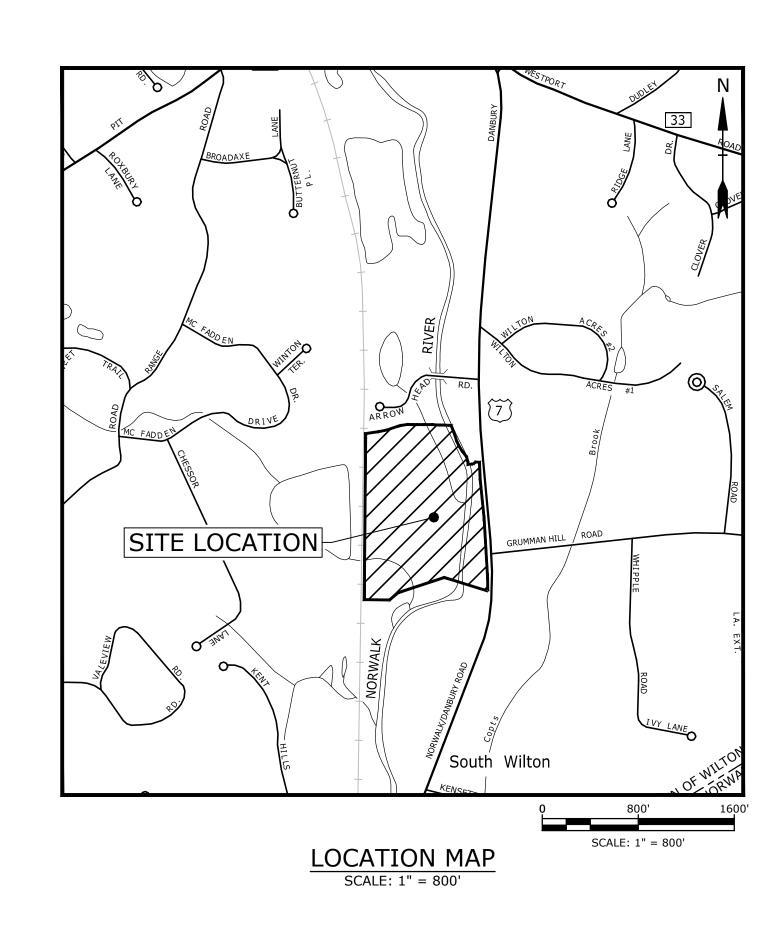
77 Danbury Road Wilton, Connecticut

		1
MARK	DATE	DESCRIPTION
FROJEC	T NO:	A0969-015
DATE:		04/12/2022
FILE:	ROA	59-015-VS-300-PHOTOS.drig
DRAWN	BY:	MDS
DESIGN	ED/CHECK	D BY: JAC
APPRON	ED BY:	JWB
		IEW LINE PHOTOS
SCALE	:	1" = 20'
	١	/-300

# ASML CAMPUS TRAFFIC FLOW SAFETY IMPROVEMENTS DANBURY ROAD WILTON, CONNECTICUT

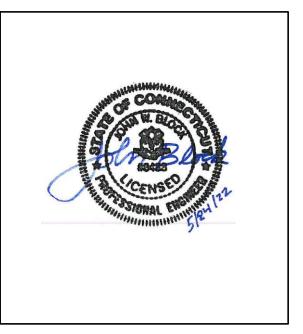
# TOWN SUBMISSION DRAWINGS MAY 24, 2022

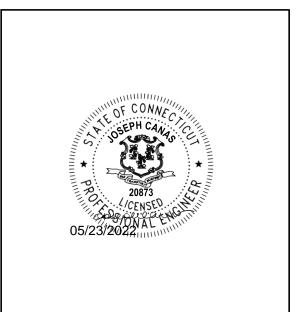
r				
	LIST OF DRAWINGS			
SHEET NO.	DRAWING NO.	DRAWING TITLE		
	•	GENERAL		
1	G-001	COVER SHEET		
		CIVIL		
2	C-000	GENERAL NOTES, ABBREVIATIONS AND LEGEND		
3	C-100	EXISTING CONDITIONS PLAN		
4	C-200	ROADWAY TYPICAL SECTIONS		
5	C-210	ALIGNMENT PLAN		
6	C-220	DRIVEWAY PROFILE		
7	C-300	SITE PLAN		
8	C-310	SITE PLAN ENLARGEMENT		
9	C-400	GRADING PLAN		
10	C-410	GRADING PLAN ENLARGEMENT		
11	C-500	DRAINAGE AND UTILITY PLAN		
12	C-510	DRAINAGE AND UTILITY PLAN EMLARGEMENT		
13	C-601	SEDIMENT AND EROSION CONTROL PLAN PHASE - 1		
14	C-602	SEDIMENT AND EROSION CONTROL PLAN PHASE - 2		
15	C-603	SEDIMENT AND EROSION CONTROL PLAN PHASE - 3		
16	C-604	SEDIMENT AND EROSION CONTROL PLAN PHASE - 4		
17	C-605	SEDIMENT AND EROSION CONTROL PLAN PHASE - 5		
18	C-611	SEDIMENT AND EROSION CONTROL NOTES, NARRATIVE AND DETAILS		
19	C-612	SEDIMENT AND EROSION CONTROL DETAILS		
20 - 28	C-700-C-708	CROSS-SECTIONS		
29	C-800	TRAFFIC OPERATIONS PLAN		
30 - 36	C-900 - C-906	SITE DETAILS		
37 - 43	C-910 - C-916	DRAINAGE DETAILS		
44	L-100	PLANTING PLAN - 1		
45	L-101	PLANTING PLAN - 2		
46	L-102	PLANTING DETAILS		











PREPARED FOR:



77 DANBURY ROAD WILTON, CT 06897

**COMPLETE SET 46 SHEETS** 

### **GENERAL NOTES**

- 1. THE ACCURACY AND COMPLETENESS OF SUBSURFACE INFORMATION SHOWN ON THESE DRAWINGS IS NOT GUARANTEED. THE CONTRACTOR LOCATIONS AND ELEVATIONS OF ALL UTILITIES WHICH MAY AFFECT CONSTRUCTION OPERATIONS. THE CONTRACTOR MUST ADEQUATELY PRO UTILITIES AND SHALL BE RESPONSIBLE FOR ALL DAMAGE INCURRED AT NO EXPENSE TO THE OWNER. ANYONE USING UTILITY INFORMATION HEREIN SHALL CONTACT "CALL BEFORE YOU DIG", 1-800-922-4455 OR WWW.CBYD.COM, 72 HOURS IN ADVANCE TO VERIFY THE LOCATION OF STARTING CONSTRUCTION.
- 2. REFERENCE IS MADE TO PLAN TITLED "PROPOSED DRIVEWAY, EXISTING CONDITIONS, PREPARED FOR ASML US, INC..." PREPARED BY ARTHUR ASSOCIATES, PC, DATED APRIL 20, 2022.
- 3. IT IS THE RESPONSIBILITY OF THE CONTRACTOR IN EVALUATING THESE PLANS TO MAKE EXAMINATIONS IN THE FIELD BY VARIOUS METHODS INFORMATION FROM AVAILABLE RECORDS, UTILITY COMPANIES, AND INDIVIDUALS AS TO THE LOCATION OF SUBSURFACE STRUCTURES.
- 4. THE WETLANDS DEPICTED ON THE PLANS HAVE BEEN FLAGGED BY RAINA VOLOVSKI, PROFESSIONAL SOIL SCIENTIST OF TIGHE & BOND.
- 5. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO REVIEW ALL OF THE DRAWINGS AND SPECIFICATIONS ASSOCIATED WITH THIS PROJECT THE INITIATION OF CONSTRUCTION, SHOULD THE CONTRACTOR FIND A CONFLICT WITH THE DOCUMENTS RELATIVE TO THE DRAWINGS, SPE APPLICABLE CODES, IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE OWNER'S REPRESENTATIVE IN WRITING PRIOR TO THE START FAILURE BY THE CONTRACTOR TO NOTIFY THE OWNER'S REPRESENTATIVE SHALL CONSTITUTE ACCEPTANCE OF FULL RESPONSIBILITY BY THE COMPLETE THE SCOPE OF WORK AS DEFINED BY THE DRAWINGS AND IN FULL CONFORMANCE WITH REGULATIONS AND CODES.
- 6. AS CONSTRUCTION IS COMPLETED, THE CONTRACTOR SHALL REMOVE ALL EXCESS MATERIAL, DEBRIS, ETC. AND RESTORE OR REPLACE ANY D AND SITE FEATURES.
- 7. AREAS OUTSIDE THE PROJECT LIMIT LINE DISTURBED BY CONSTRUCTION SHALL BE RETURNED TO THEIR ORIGINAL CONDITION OR BETTER AN MEET PROPOSED CONSTRUCTION AS DIRECTED BY THE OWNER'S REPRESENTATIVE. COST FOR THIS WORK SHALL BE BORNE BY THE CONTRAC COST TO THE OWNER.
- 8. THE CONTRACTOR SHALL PROCURE ALL THE NECESSARY PERMITS AND LICENSES, AT THE TIME REQUIRED, PAY ALL THE CHARGES AND FEES, NECESSARY AND DUE IN CONNECTION WITH THE LAWFUL EXECUTION OF THE WORK AT NO ADDITIONAL COST TO THE OWNER.
- 9. ALL UTILITY BOXES, FRAMES, AND GRATES, ETC. AFFECTED BY THE CONSTRUCTION ACTIVITIES SHALL BE RESET/RECONSTRUCTED TO THE PR RELATED TO SUCH WORK SHALL BE INCLUDED IN THE BID PRICE.
- 10. EXCAVATION OF ANY TYPE SHALL BE ACCOMPLISHED IN SUCH A MANNER THAT UNDERGROUND UTILITIES OR STRUCTURES ARE NOT DAMAGE CONTRACTOR'S SOLE RESPONSIBILITY FOR ANY DAMAGED INCURRED DURING CONSTRUCTION OPERATIONS. ALL EXCAVATION SHALL BE IN C LATEST OSHA REQUIREMENTS.
- 11. ALL DRIVEWAYS, ROADS, STAIRS, AND SIDEWALKS DISTURBED BY THE CONSTRUCTION IN OR OUTSIDE THE PROJECT LIMIT LINE SHALL BE R ORIGINAL CONDITION OR BETTER AND SHALL BE GRADED TO MEET THE PROPOSED CONSTRUCTION AS DIRECTED BY THE OWNER'S REPRESENT ADDITIONAL COST TO THE OWNER.
- 12. THE CONTRACTOR SHALL SUFFICIENTLY COVER ALL DISTURBED AREAS AT THE END OF EACH WORK DAY TO AVOID ANY RISK OF INJURY TO P VEHICULAR TRAFFIC. THE CONTRACTOR SHALL INSTALL TEMPORARY SUPPORT SYSTEMS OVER TRENCH EXCAVATIONS THAT ARE TAMPER RESIST VEHICULAR AND PEDESTRIAN TRAFFIC. THE CONTRACTOR SHALL INSTALL BARRICADES TO PROTECT AGAINST PEDESTRIAN ACCESS. THE CON APPROVAL OF THE TEMPORARY SAFETY MEASURES BY THE OWNER'S REPRESENTATIVE. ALL MAINTENANCE AND PROTECTION OF BOTH PEDEST TRAFFIC ARE INCLUDED IN THE BID PRICE FOR THIS PROJECT.
- 13. THE STANDARD SPECIFICATIONS (FOR SITE /CIVIL WORK) SHALL BE THE STATE OF CONNECTICUT, DEPARTMENT OF TRANSPORTATION, STAND FOR ROADS, BRIDGES, AND INCIDENTAL CONSTRUCTION, FORM 818, 2020, INCLUDING ALL SUPPLEMENTS THERETO. FORM 818 IS AVAILABLE CTDOT WEBSITE WWW.CT.GOV/DOT.
- 14. ALL DISTURBED AREAS NOT PROVIDED WITH SPECIFIC SITE IMPROVEMENTS (PAVING, CONCRETE SIDEWALK, LANDSCAPING, ETC.) SHALL HAV INSTALLED, SEED AND ESTABLISH GRASS
- 15. THE CONTRACTOR SHALL RECORD THE LOCATIONS OF ALL UNDERGROUND UTILITIES INSTALLED OR FOUND WITHIN THE PROJECT AREA DURI UTILITIES SHALL BE MEASURED FROM PERMANENT SURFACE FEATURES AND COMPILED BY THE CONTRACTOR ON RECORD DRAWINGS. AN AS BE PREPARED BY A SURVEYOR LICENSED IN THE STATE OF CONNECTICUT AND IN ACCORDANCE THE TOWN OF WILTON, AND SUBMITTED TO THE AND ENGINEER FOR REVIEW AND APPROVAL.
- 16. THE CONTRACTOR SHALL COMPLETE ALL WORK SO THAT ANY MATERIALS WHICH ARE TO REMAIN IN PLACE OR WHICH ARE TO REMAIN THE PR WILL NOT BE DAMAGED. IF THE CONTRACTOR DAMAGES ANY MATERIALS WHICH ARE TO REMAIN, OR WHICH ARE TO REMAIN THE PROPERTY C DAMAGED MATERIALS SHALL BE REPLACED TO THE SATISFACTION OF THE OWNER'S REPRESENTATIVE AT THE EXPENSE OF THE CONTRACTOR.
- 17. EROSION CONTROL PLANS SHALL BE STRICTLY ENFORCED. PUBLIC ROADS SHALL BE SWEPT CLEAN OF ALL DIRT AND DEBRIS AT THE END OF
- 18. THERE SHALL BE NO CONSTRUCTION ACTIVITIES ON THE SITE ON SUNDAYS OR FEDERAL HOLIDAYS. ALL CONSTRUCTION RELATED ACTIVITIE BETWEEN THE HOURS OF 7:00 A.M. AND 6:00 P.M. MONDAY THROUGH FRIDAY AND BETWEEN THE HOURS OF 8:00 A.M. AND 6 P.M. ON SATURI DOES NOT APPLY TO INTERIOR FINISH WORK PERFORMED WITHIN A FULLY-ENCLOSED BUILDING.
- 19. VERTICAL DATUM IS NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).

## **ZONING TABLE**

Lot Dimensions and Covera	ge			Building Coverage Summary	
Item	Required	Existing	Proposed	Item	Exis
Min. Lot Area (ac)	10	28.64	28.64	77 Danbury Road (sf)	230
Min. Frontage (feet)	150	1,065.12	1,065.12	71 Danbury Road (sf)	11,4
Max. Building Coverage	25%	24.0%	24.0%	Parking Garage (sf)	38,7
Max Site Coverage	50%	42.2%	43.3%	Total (sf)	292,
Building Setbacks		,		Site Cover	age Sum
Min. Front Yard Overall (ft)	100	5	5	Building Coverage (sf)	292,
Min. Side Yard Overall (ft)	100	101.3	101.3	Other Impervious Areas (sf)	233,
Min. Side Yard Abutting Residential (feet)	150 / 50	209.9	209.9	Total (sf)	526,
Min. Rear Yard (feet)	100 / 150	N/A	N/A	Parking Summary	
Min. Rear Yard Abutting Residential District (feet)	150 / 10	100.1	100.1	Industrial Use (1 per 400 sf + 1 per 1000sf outdoor storage) Buildings = 940 spaces Outdoor storage = 4 spaces Total required = 944 spaces	1,1

Notes:

- A four story and or 55 foot high building may be located on lots that are in conformance with minimum area requirements of the DE-10 or DE-5 district. They shall not be permitted by action of the Zoning Board of Appeals.
- Where adjoining property in a residence district to the side or rear lies within the right of way of a railroad, the side or rear yard setbacks may be reduced to 50 feet. Where adjoining property In a residence district to the side and rear lies within the right-of-way of a railroad, and where the railroad property adjoins a public utility right of way and or a publicly owned right of way with a total width of not less than 200 feet, the side and rear yard building setbacks and the parking setbacks maybe reduced to 10 feet.
- Where property adjoining in a residence district to the side or rear lies within the right-of-way of a railroad, the side or rear yard parking and loading setbacks may be 3. reduced to ten feet.

# **STANDARD ABBREVIATIONS**

BW

BIT

BC

BS

BOT

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CB

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CLF

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END

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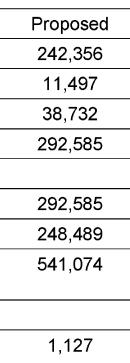
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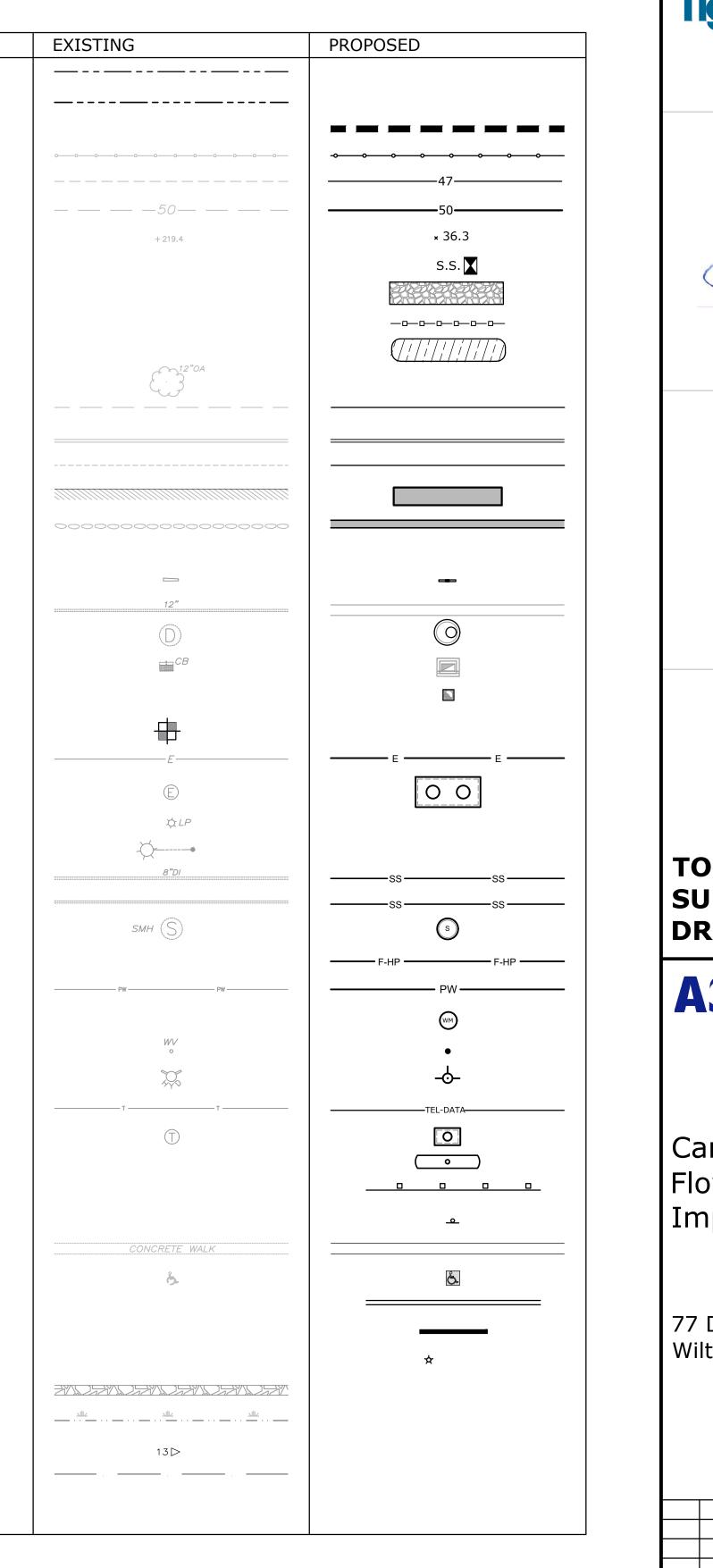


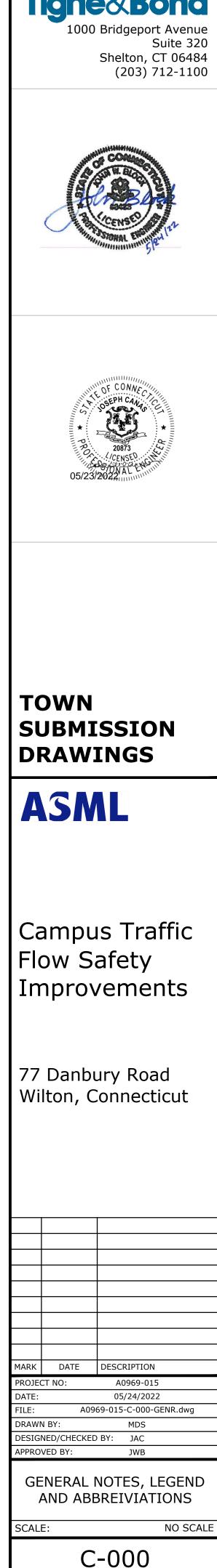
AT ACRE/AIR CONDITIONING BASELINE BOTTOM OF WALL BITUMINOUS BOTTOM OF CURB BOTTOM OF STAIRS BLDG BUILDING BOTTOM CATV CABLE TELEVISION CAST IRON PIPE CATCH BASIN CENTERLINE CHAIN LINK FENCE CL&P CONNECTICUT LIGHT & POWER CTDEEP CONNECTICUT DEPT. OF ENERGY & ENV. PROTECTION CTDOT CONNECTICUT DEPT. OF TRANSPORTATION CONC CONCRETE CLEAN-OUT CORRUGATED POLYETHYLENE PIPE CUBIC YARDS DUCTILE IRON PIPE DOWN DWG DRAWING EAST/ELECTRIC EXISTING GRADE ELECTRIC ELEC ELEVATION EL/ELEV ELECTRIC MANHOLE EMH ENDWALL EX/EXIST EXISTING EXPANSION JOINT EXP. JT. FIRST FLOOR GAS GAS GATE HDPE HIGH DENSITY POLYETHYLENE PIPE HYDRANT INCHES INCORPORATED INVERT LENGTH OF CURVE LEFT LIGHT POLE MAXIMUM MINIMUM MANHOLE MISC MISCELLANEOUS MON MONUMENT NAVD88 NORTH AMERICAN VERTICAL DATUM OF 1988 NOT IN CONTRACT NORTH NOT TO SCALE NOT APPLICABLE NOW OR FORMERLY OVERHEAD POINT OF CURVATURE POINT OF COMPOUND CURVATURE PEDESTRIAN POINT OF INTERSECTION POINT OF TANGENCY POINT OF REVERSE CURVATURE POLYVINYL CHLORIDE RADIUS REVISION RIGHT OF WAY RIGHT SANITARY SCHEDULE SQUARE FEET SOUTH STATION STANDARD STRM STORM TANGENT LENGTH/TEL-DATA TEL-DATA TOP OF FRAME TYPICAL TOP OF CURB TOP OF STAIRS TOP OF WALL WATER WETLAND BOUNDARY WATER GATE/VALVE WG/WV AND

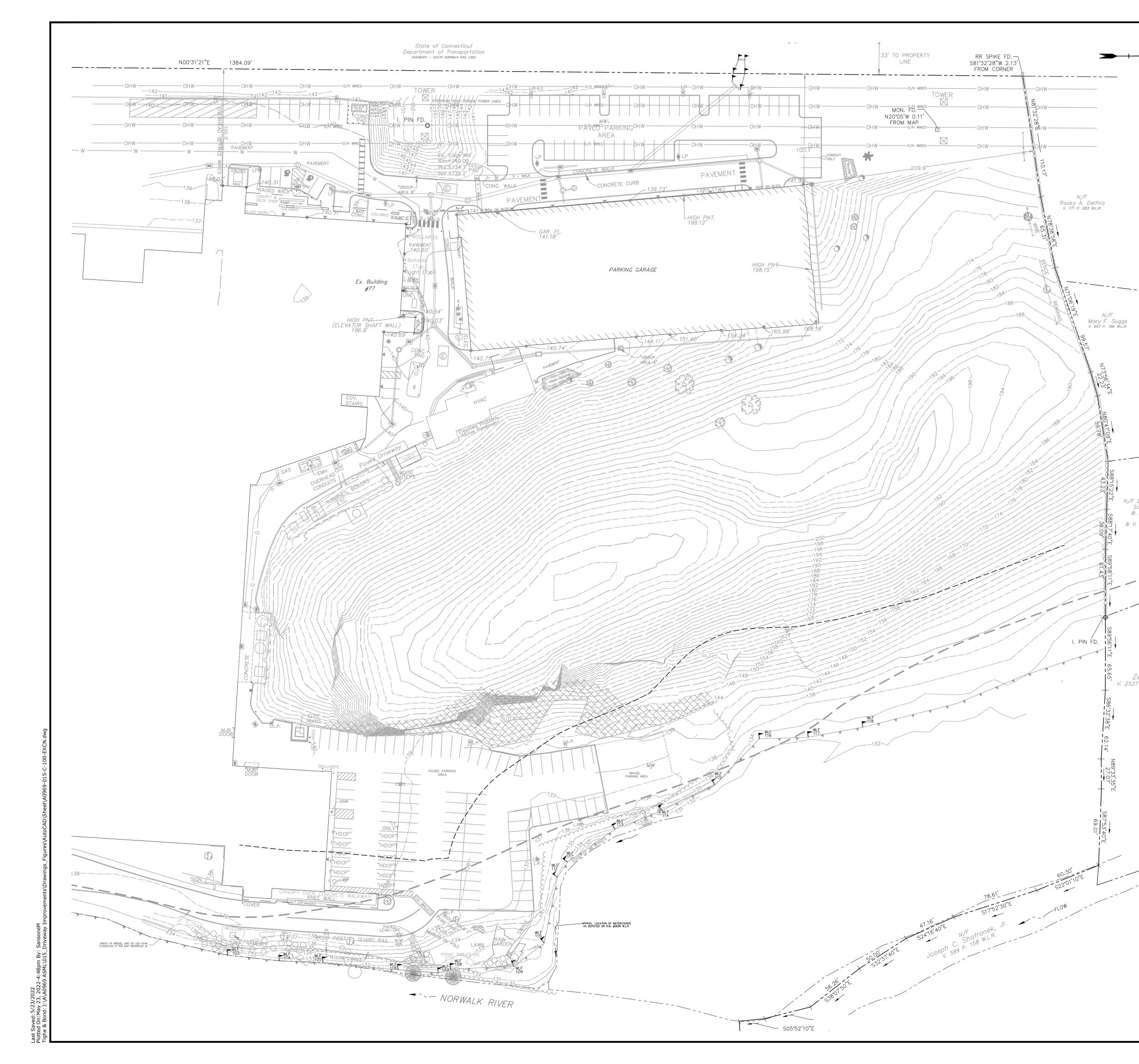
## LEGEND

DESCRIPTION PROPERTY LINE EASEMENT LINE PROJECT LIMIT LINE FENCE MINOR CONTOUR MAJOR CONTOUR SPOT ELEVATION SILT SACK CONSTRUCTION ENTRANCE SILT FENCE TEMPORARY SOIL STOCKPILE AREA TREES EDGE OF PAVEMENT CONCRETE CURB LINE WHITE PAINTED LINES BUILDING WALL WOOD POST ENDWALL STORM SEWER STORM MANHOLE CATCH BASIN YARD DRAIN DEEP TEST HOLE UNDERGROUND ELECTRIC ELECTRIC MANHOLE LIGHT POLE UTILITY POLE SANITARY SEWER SANITARY LATERAL SANITARY MANHOLE FIRE SERVICE WATER MAIN WATER METER WATER VALVE HYDRANT TEL-DATA - BURIED TEL-DATA MANHOLE FUEL TANK GUIDERAIL SIGN & SIGN POST SIDEWALK HANDICAP PARKING YELLOW PAINT LINE STOP BAR LIGHT INFILTRATION SWALE WETLAND LIMIT WETLAND FLAG

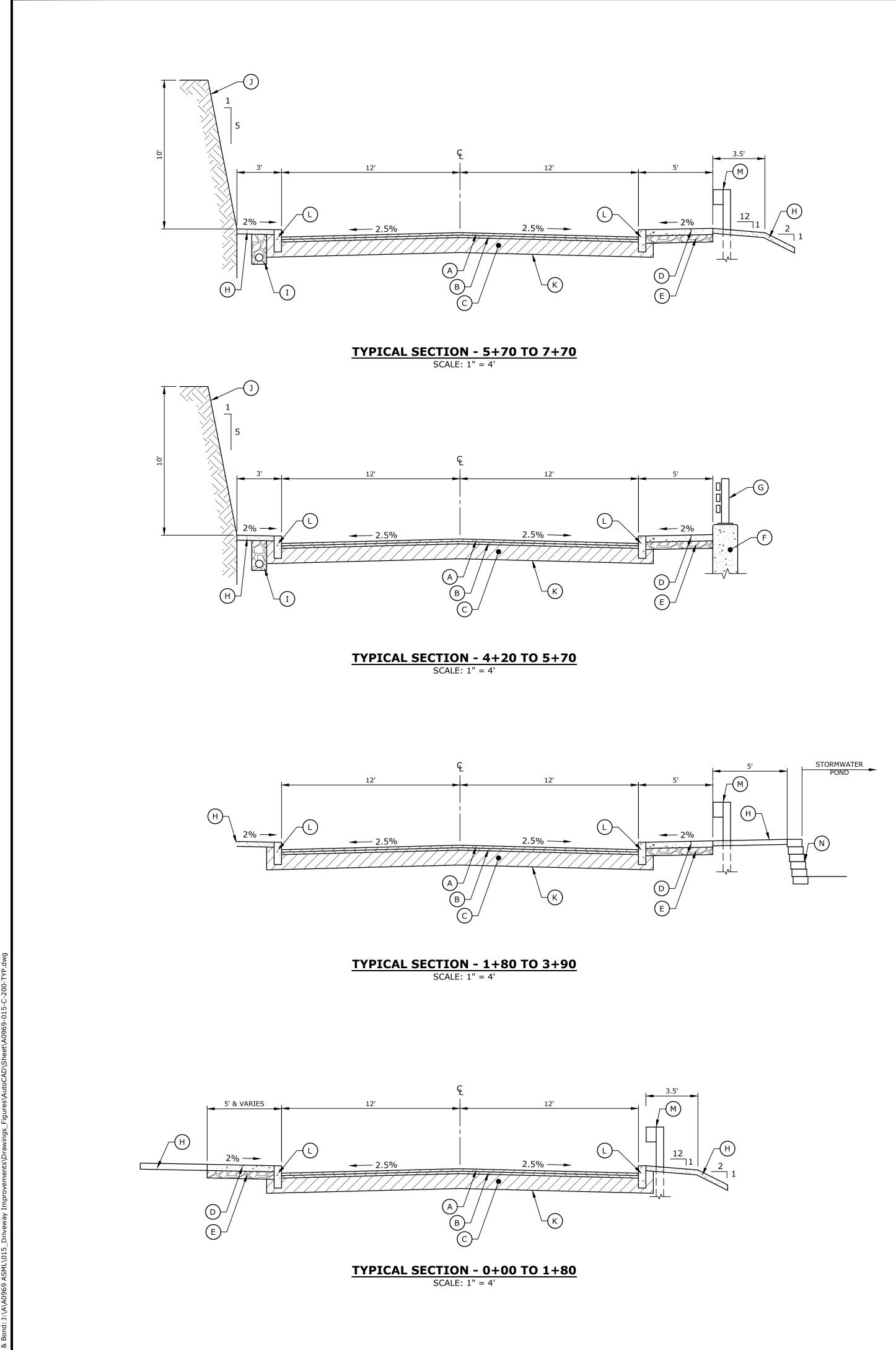
WETLAND BUFFER



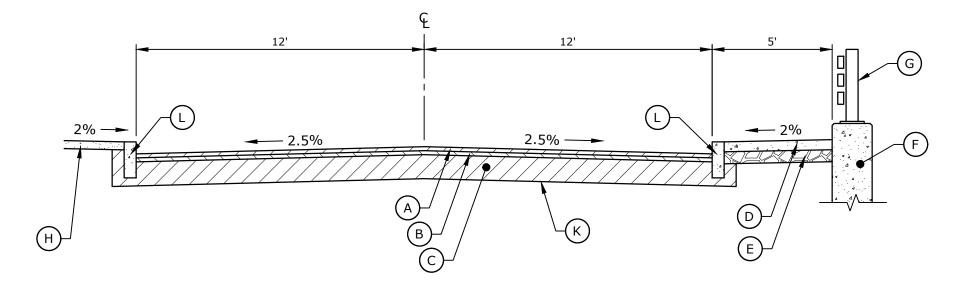




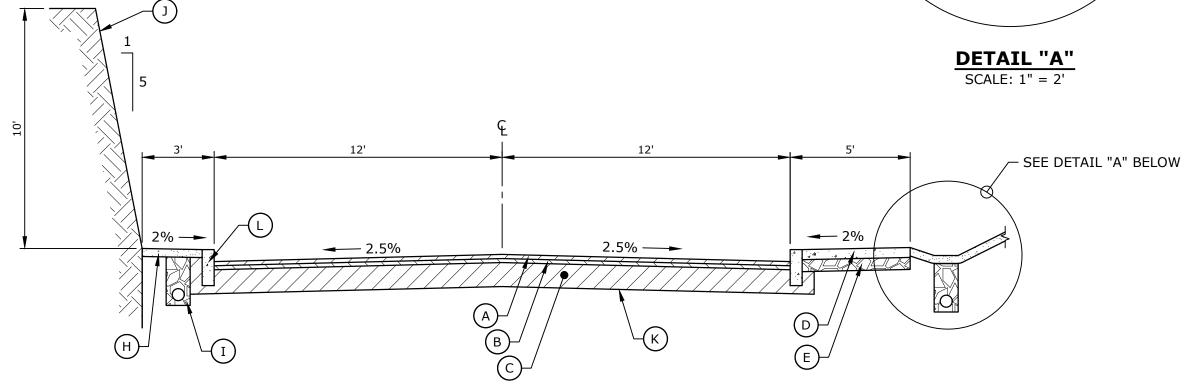
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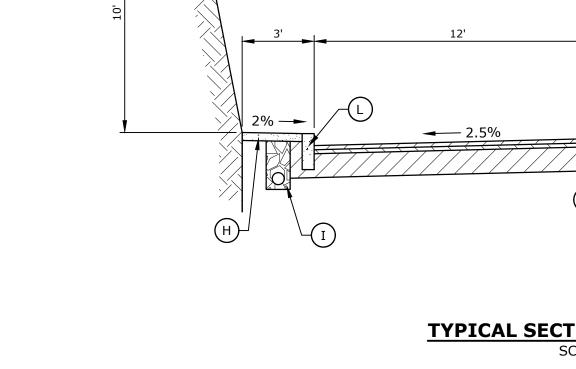
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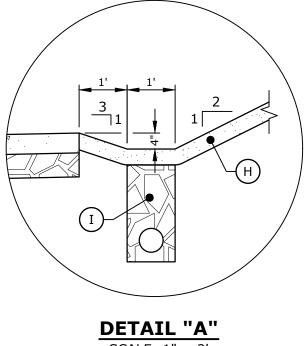
**TYPICAL SECTION - 10+50 TO 11+00** SCALE: 1" = 4'

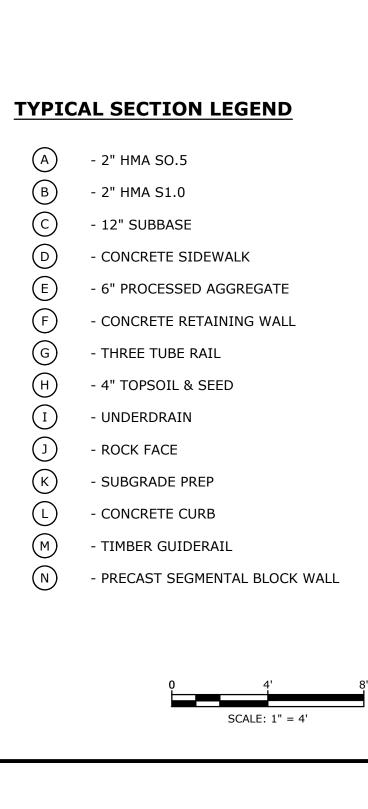


**TYPICAL SECTION - 7+70 TO 9+60** SCALE: 1" = 4'



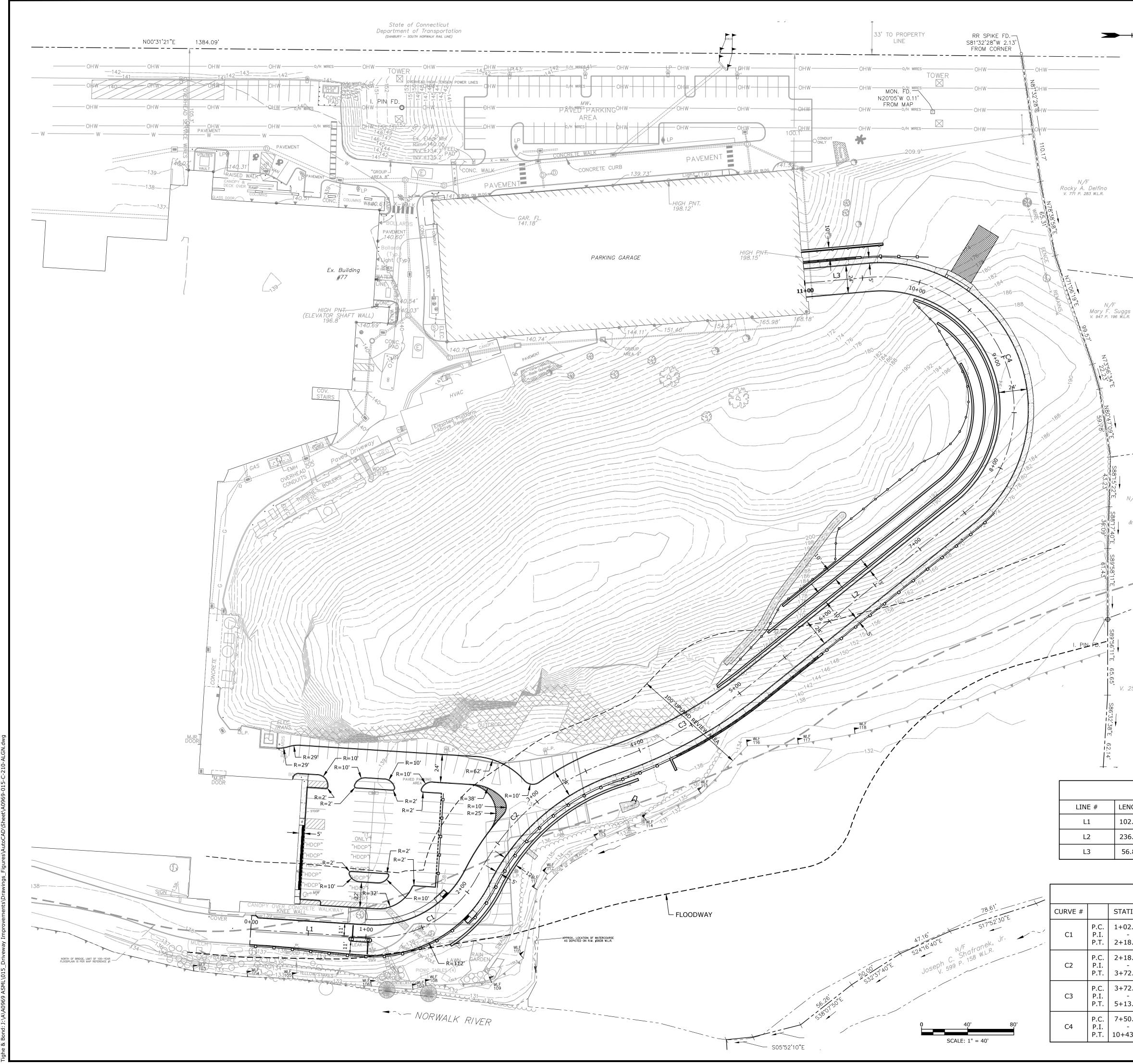






**Tighe&Bond** 1000 Bridgeport Avenue Suite 320 Shelton, CT 06484 (203) 712-1100 TOWN SUBMISSION DRAWINGS ASML Campus Traffic Flow Safety Improvements 77 Danbury Road Wilton, Connecticut MARK DATE DESCRIPTION PROJECT NO: A0969-015 05/24/2022 DATE: A0969-015-C-200-TYP.dwg FTI F DRAWN BY: MDS DESIGNED/CHECKED BY: JAC APPROVED BY: JWB ROADWAY TYPICAL SECTIONS SCALE: 1" = 4

C-200



# ALIGNMENT PLAN NOTES

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N/F

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N/F Lawrence J. Arnold, Sandra P. Arnold

& Ericalynn Arnold V. 957 P. 219 & V. 2028 P. 300 W.L.R.

N/F Zena Kim V. 2527 P. 1007 W.L.R.

# **ALIGNMENT PLAN LEGEND**

- 100 FT UPLAND REVIEW AREA

- – – – – – EASEMENT LINE
  - PROPOSED CURB
    - PROPOSED RETAINING WALL
    - PROPOSED BUILDING

  - - PROPOSED GUIDE RAIL
- × × × × × PROPOSED FENCE

LINE TABLE				
#	LENGTH	DIRECTION	START POINT	END POINT
	102.14'	N3° 40' 22.46"E	N: 623649.47, E: 816289.34	N: 623751.40, E: 816295.88
	236.24'	N38° 48' 12.84"W	N: 624084.11, E: 816076.04	N: 624268.20, E: 815928.00
	56.87'	S5° 00' 58.10"E	N: 624186.08, E: 815723.82	N: 624129.43, E: 815728.79

	CURVE TABLE						
	STATION	NORTHING	EASTING	DELTA (Δ)	TANGENT	LENGTH	RADIUS
P.C. P.I. P.T.	1+02.14 - 2+18.24	N: 623,751.40 N: 623,816.85 N: 623,846.78	E: 816,295.88 E: 816,300.08 E: 816,241.72	66° 31' 02.9"	65.58'	116.09'	100.00'
P.C. P.I. P.T.	2+18.24 - 3+72.71	N: 623,846.78 N: 623,883.90 N: 623,960.97	E: 816,241.72 E: 816,169.37 E: 816,143.44	44° 15' 10.3"	81.32'	154.47'	200.00'
P.C. P.I. P.T.	3+72.71 - 5+13.82	N: 623,960.97 N: 624,028.55 N: 624,084.11	E: 816,143.44 E: 816,120.71 E: 816,076.04	20° 12' 42.7"	71.29'	141.11'	400.00'
P.C. P.I. P.T.	7+50.05 - 10+43.52	N: 624,268.20 N: 624,563.29 N: 624,186.08	E: 815,928.00 E: 815,690.71 E: 815,723.82	146° 12' 45.3"	378.66'	293.47'	115.00'

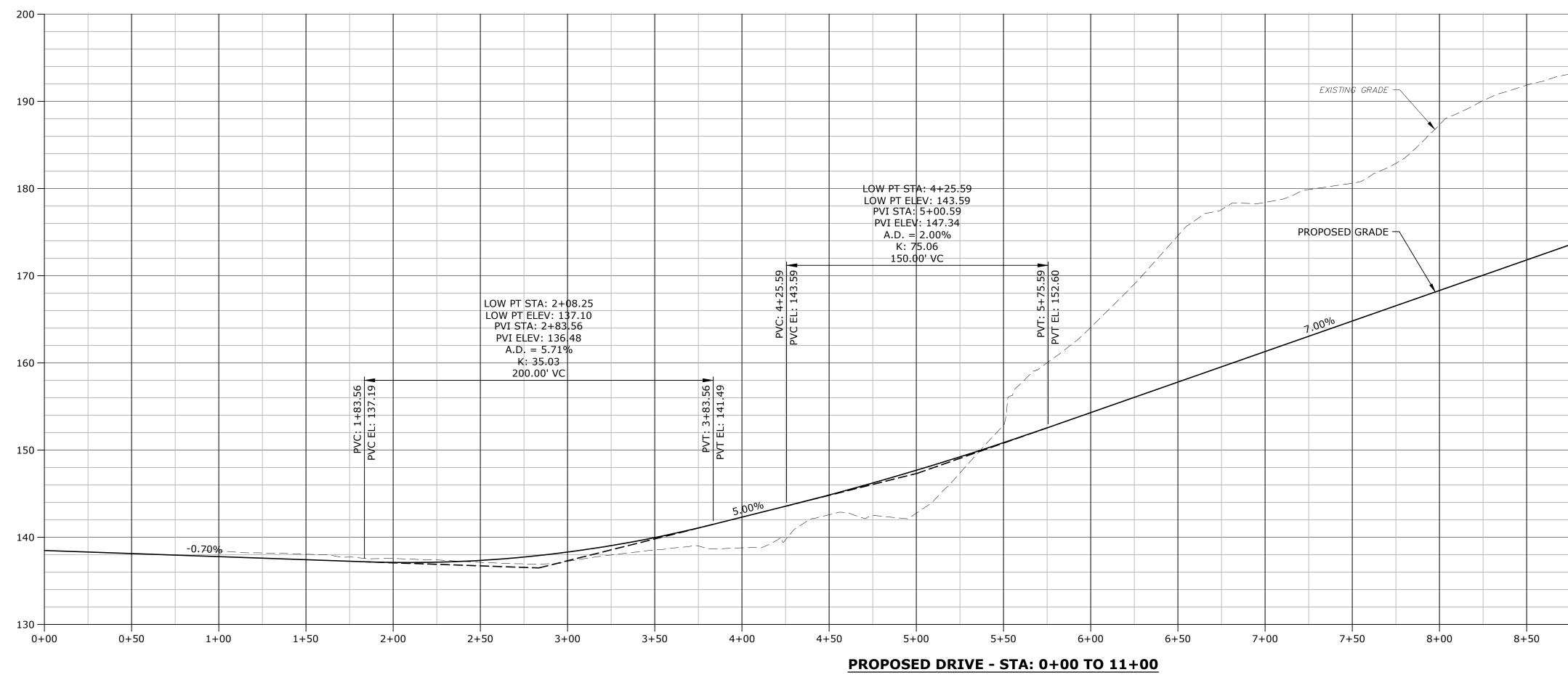
# Tighe&L 1000 Bridgeport Avenue Suite 320 Shelton, CT 06484 (203) 712-1100 05/23/2022 TOWN SUBMISSION DRAWINGS ASML Campus Traffic Flow Safety Improvements 77 Danbury Road Wilton, Connecticut 1ARK DATE DESCRIPTION A0969-015 ROJECT NO: ATE: 05/24/2022 A0969-015-C-210-ALGN.dwg DRAWN BY: MDS ESIGNED/CHECKED BY: JAC PPROVED BY: JWB ALIGNMENT PLAN

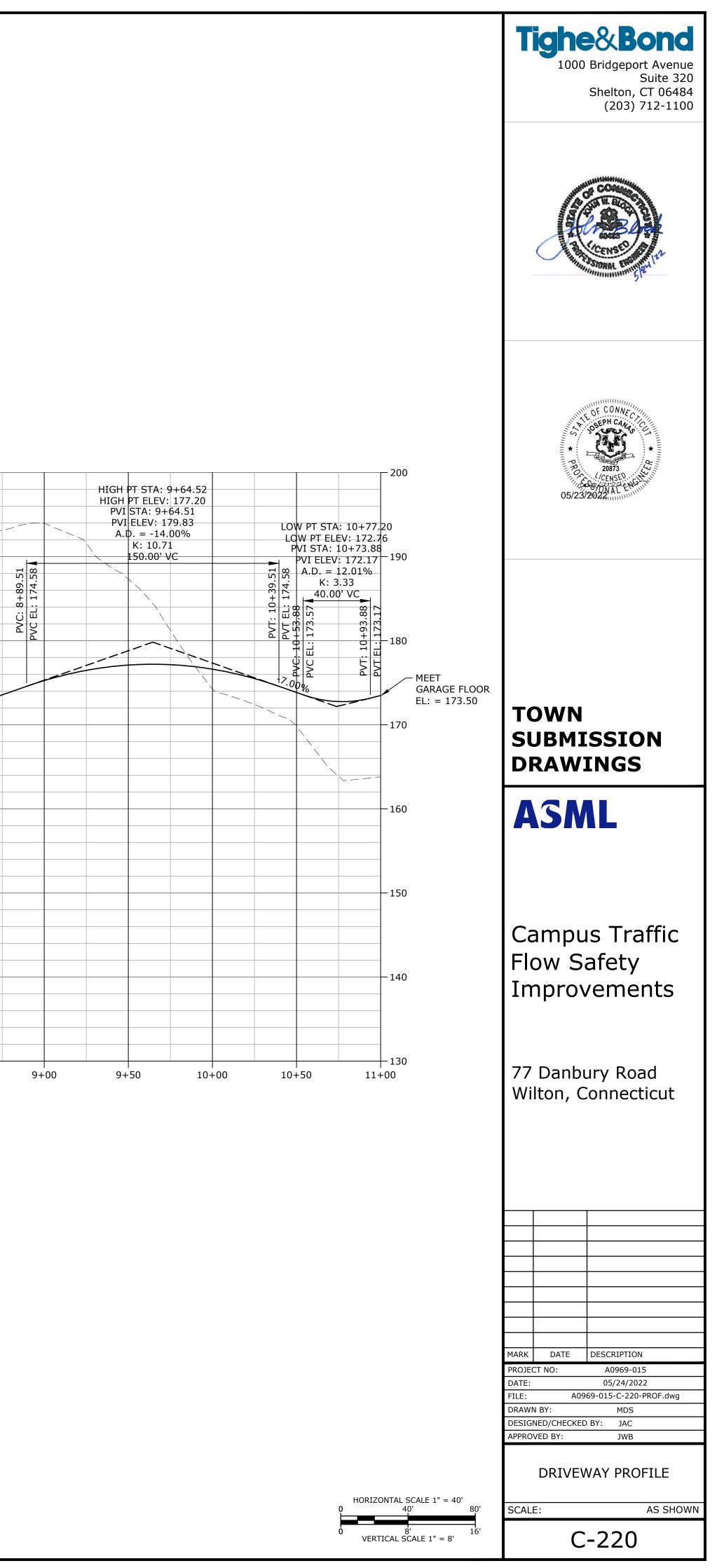
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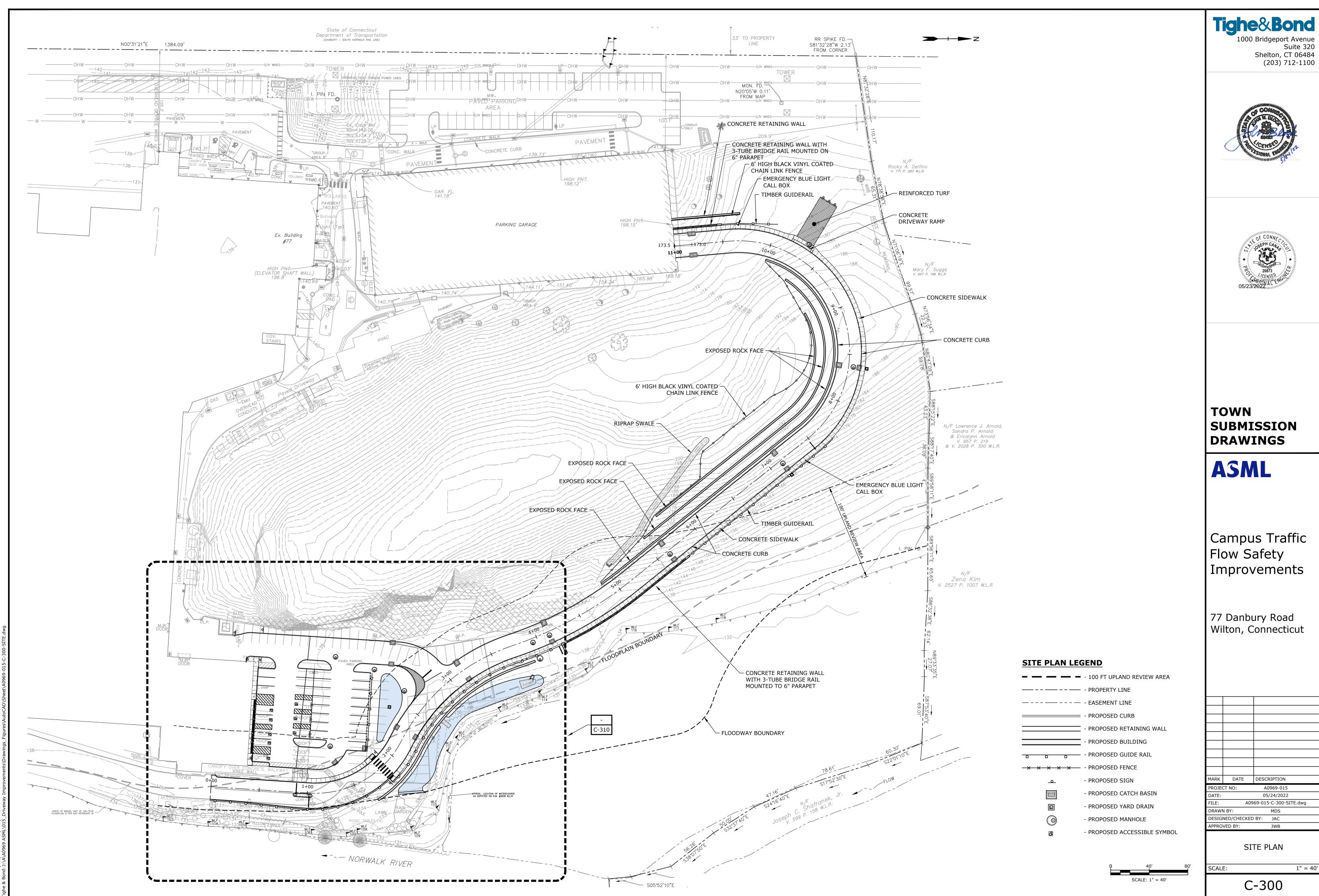
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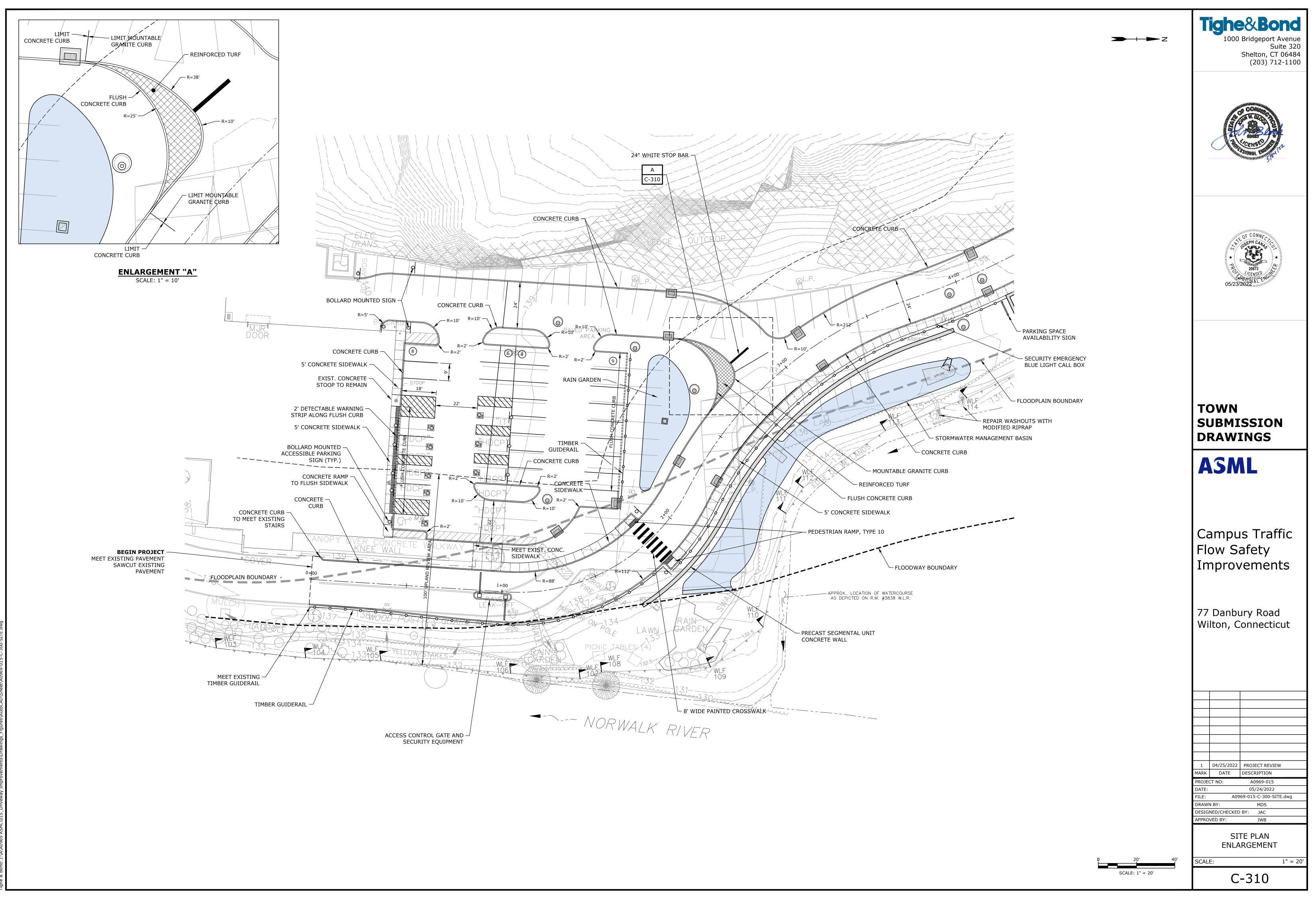
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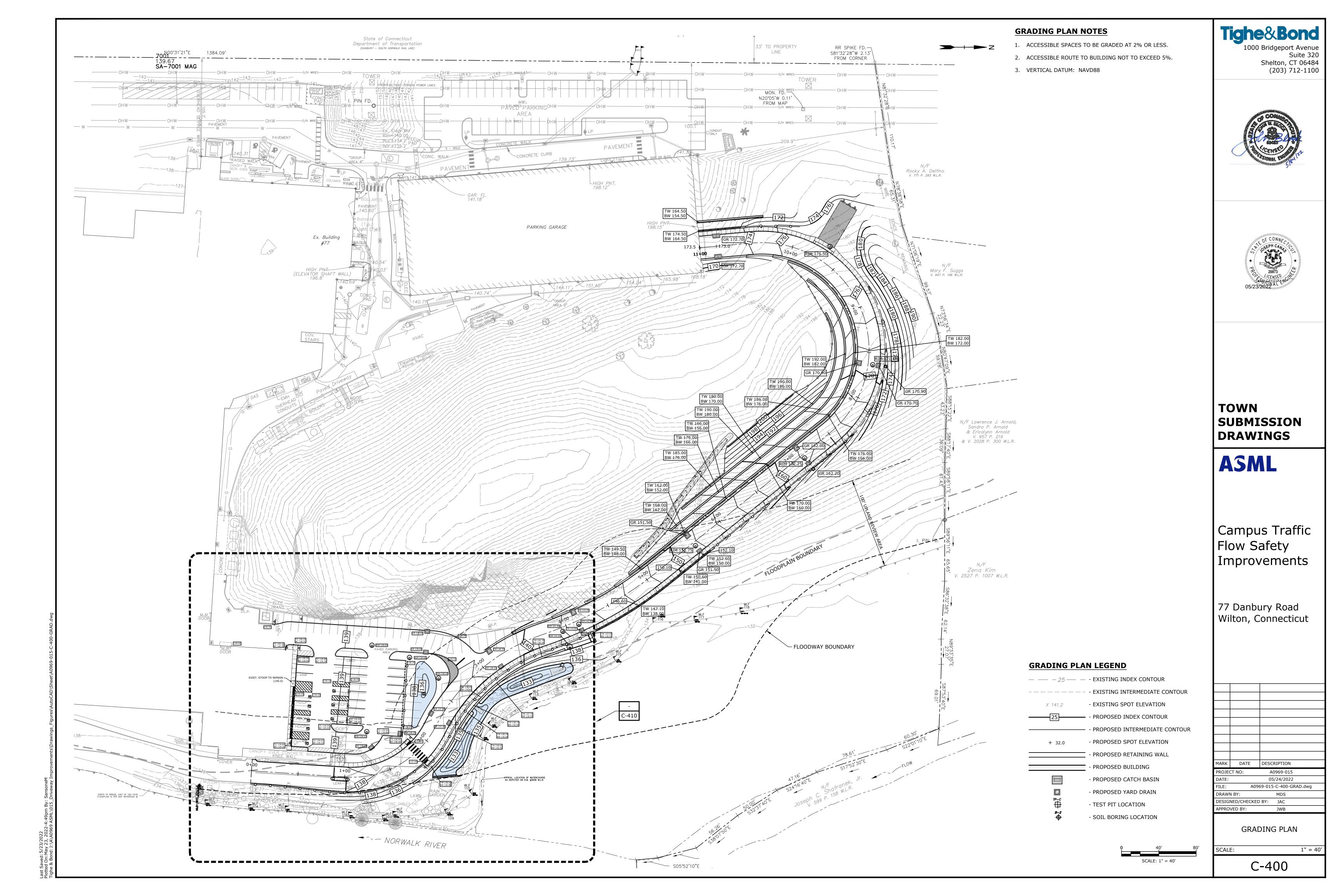




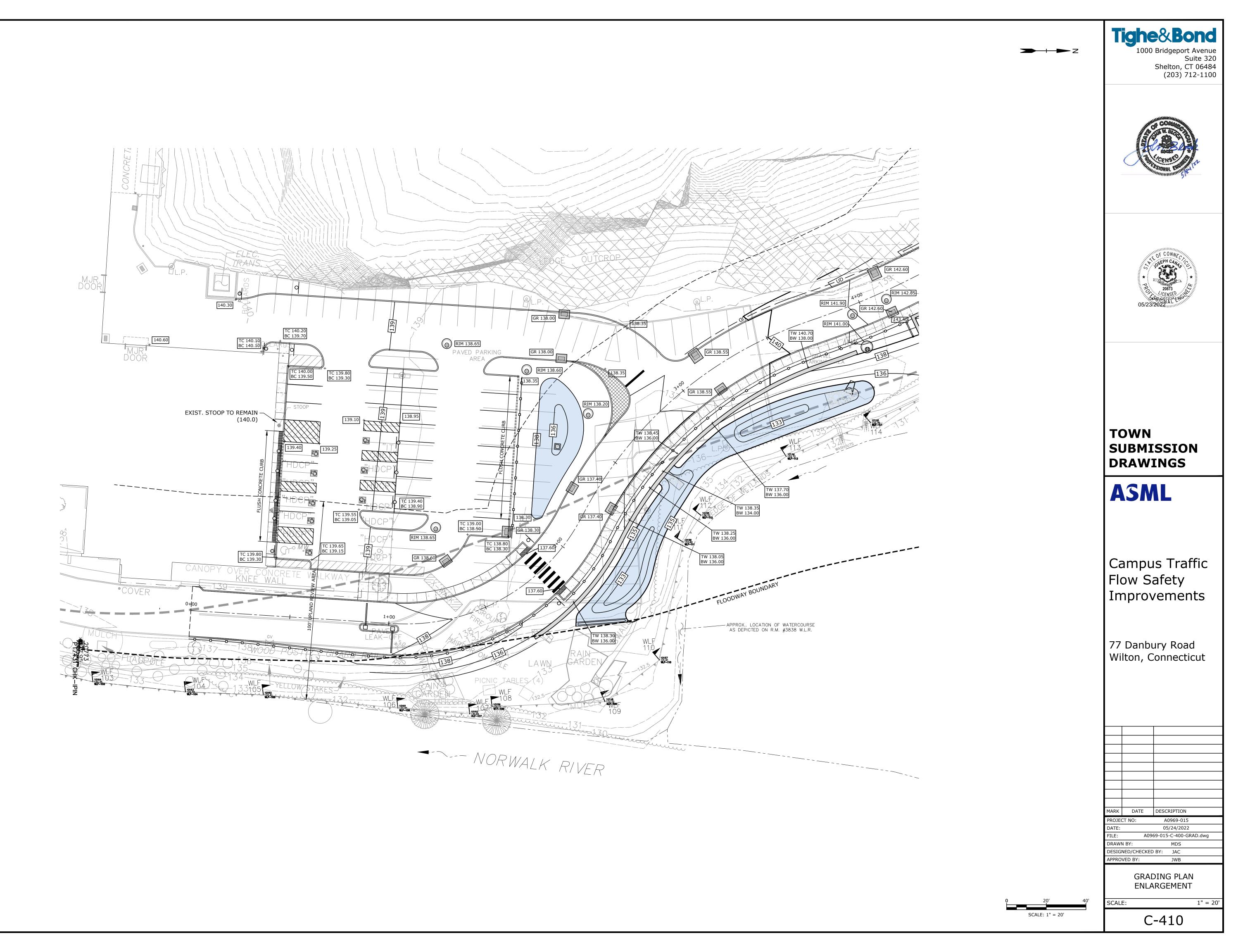
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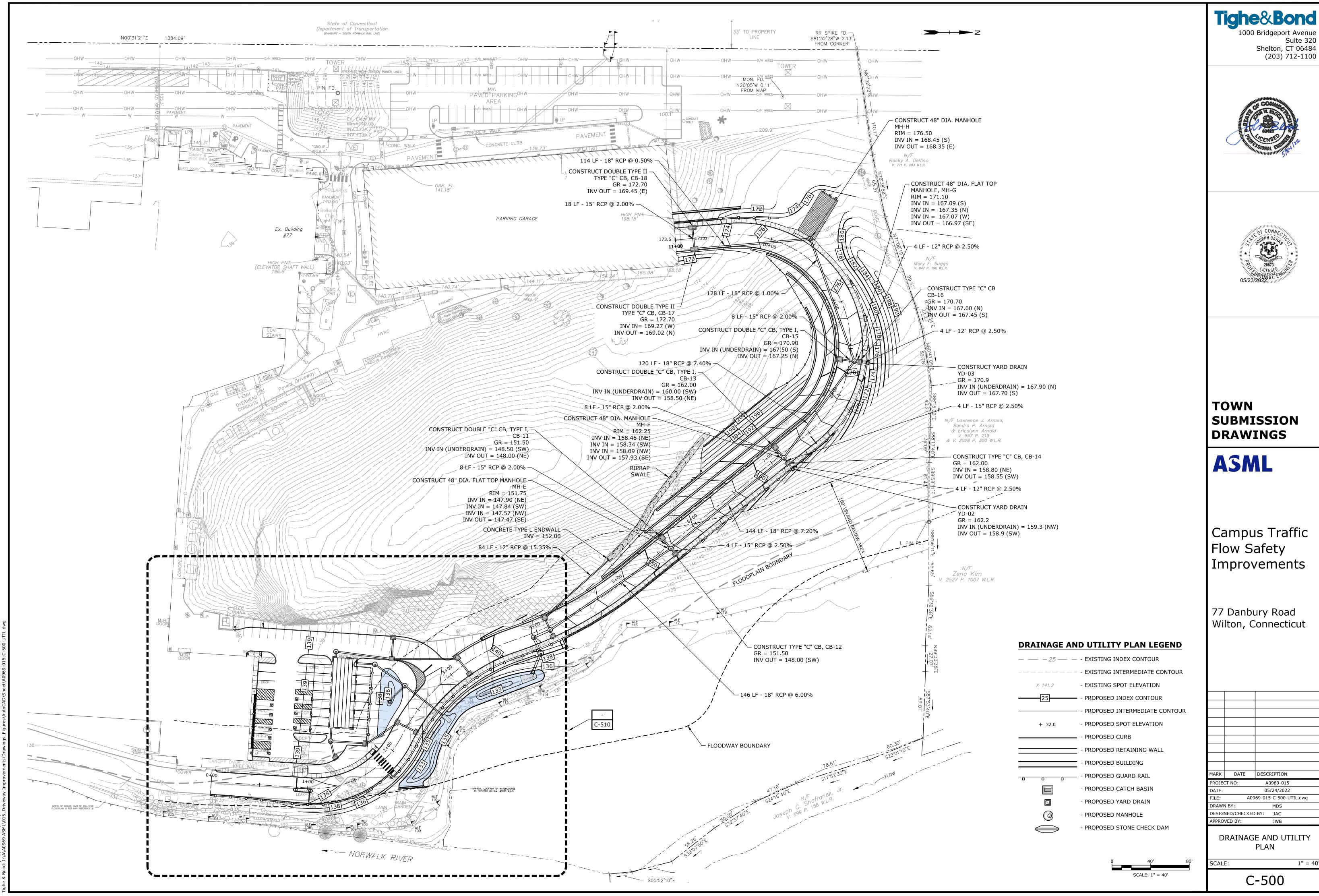


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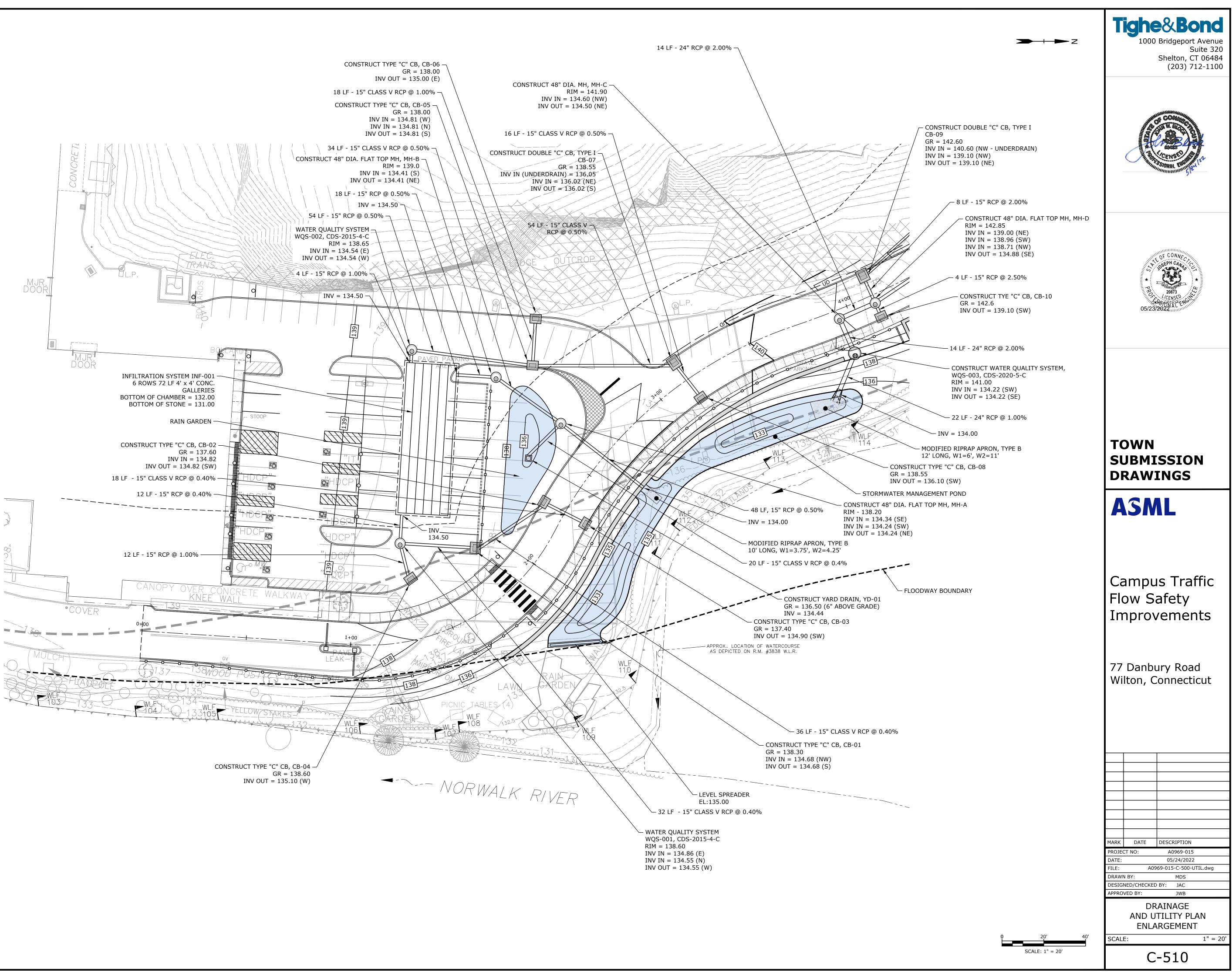
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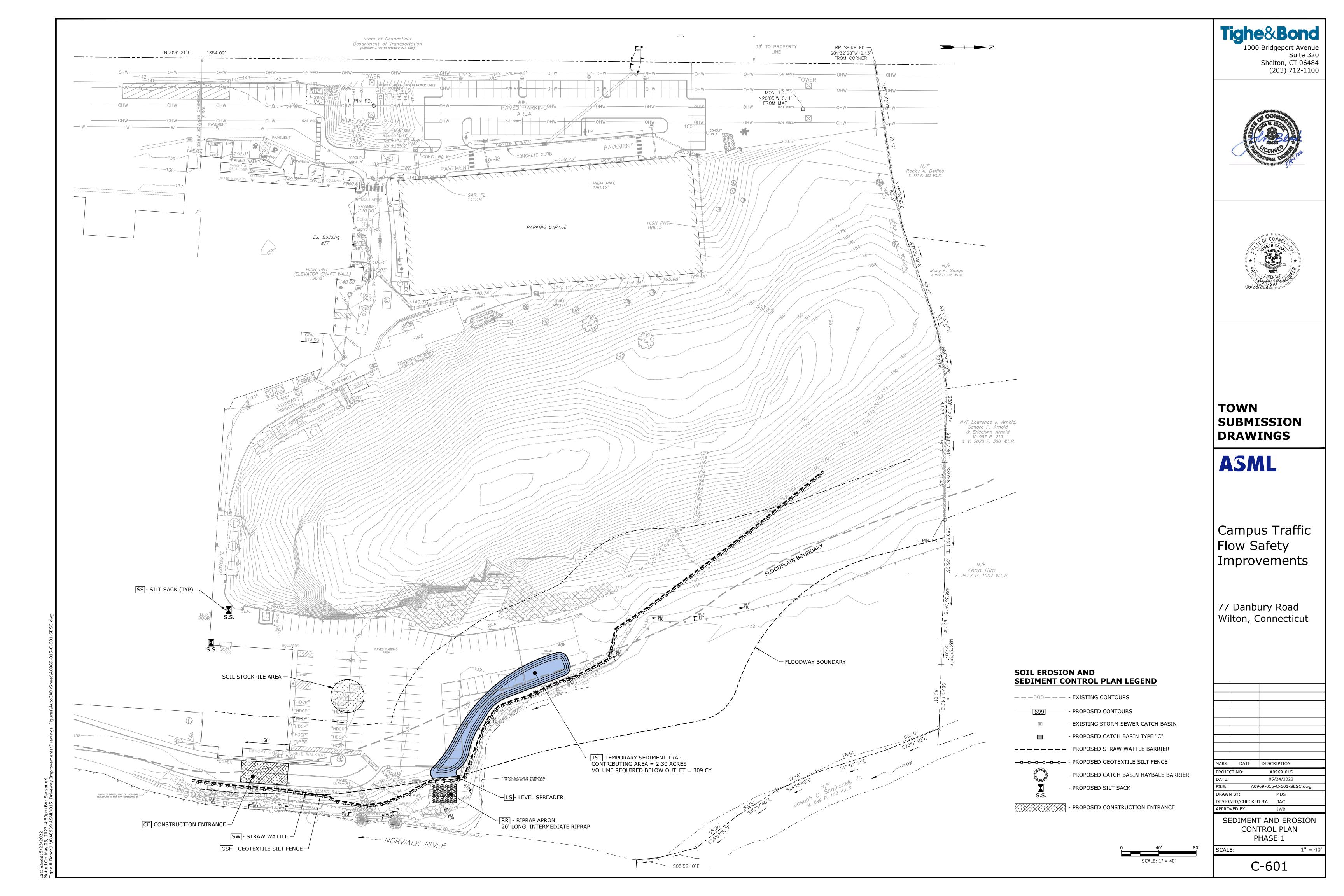


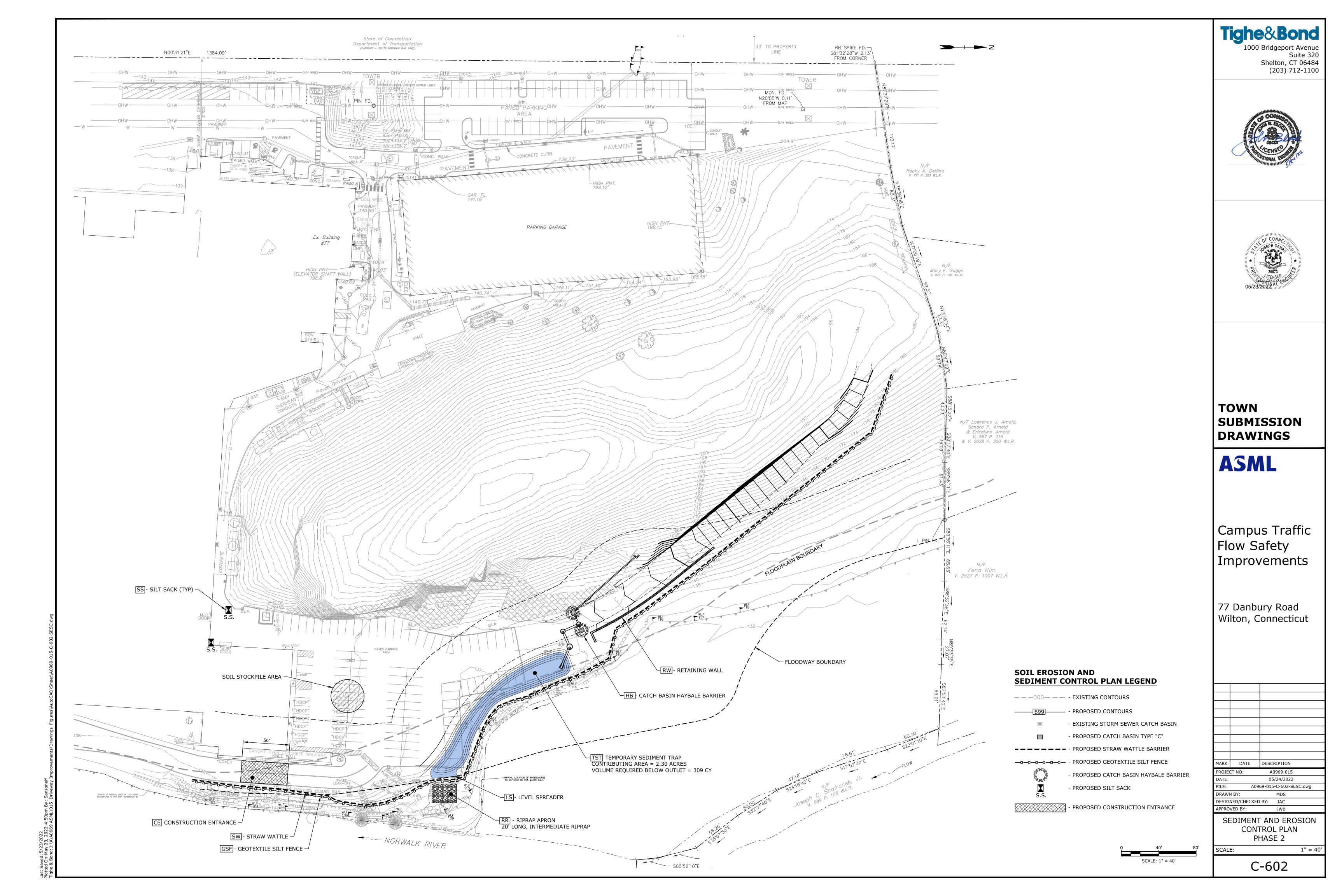


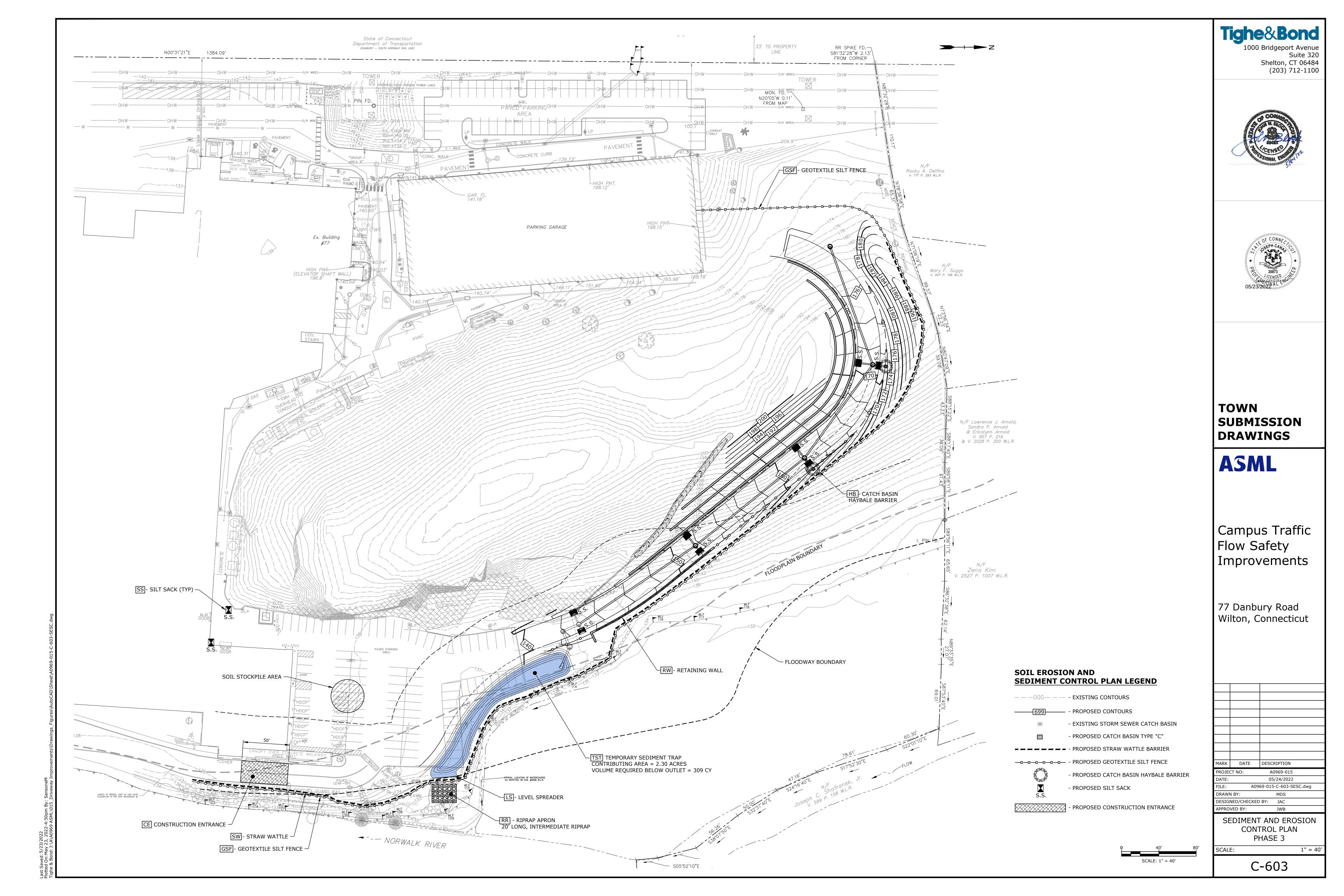
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25	- PROPOSED INDEX CONTOUR
	- PROPOSED INTERMEDIATE CONTOUR
+ 32.0	- PROPOSED SPOT ELEVATION
	- PROPOSED CURB
	- PROPOSED RETAINING WALL
	- PROPOSED BUILDING
	— - PROPOSED GUARD RAIL
	- PROPOSED CATCH BASIN
	- PROPOSED YARD DRAIN
0	- PROPOSED MANHOLE
	- PROPOSED STONE CHECK DAM

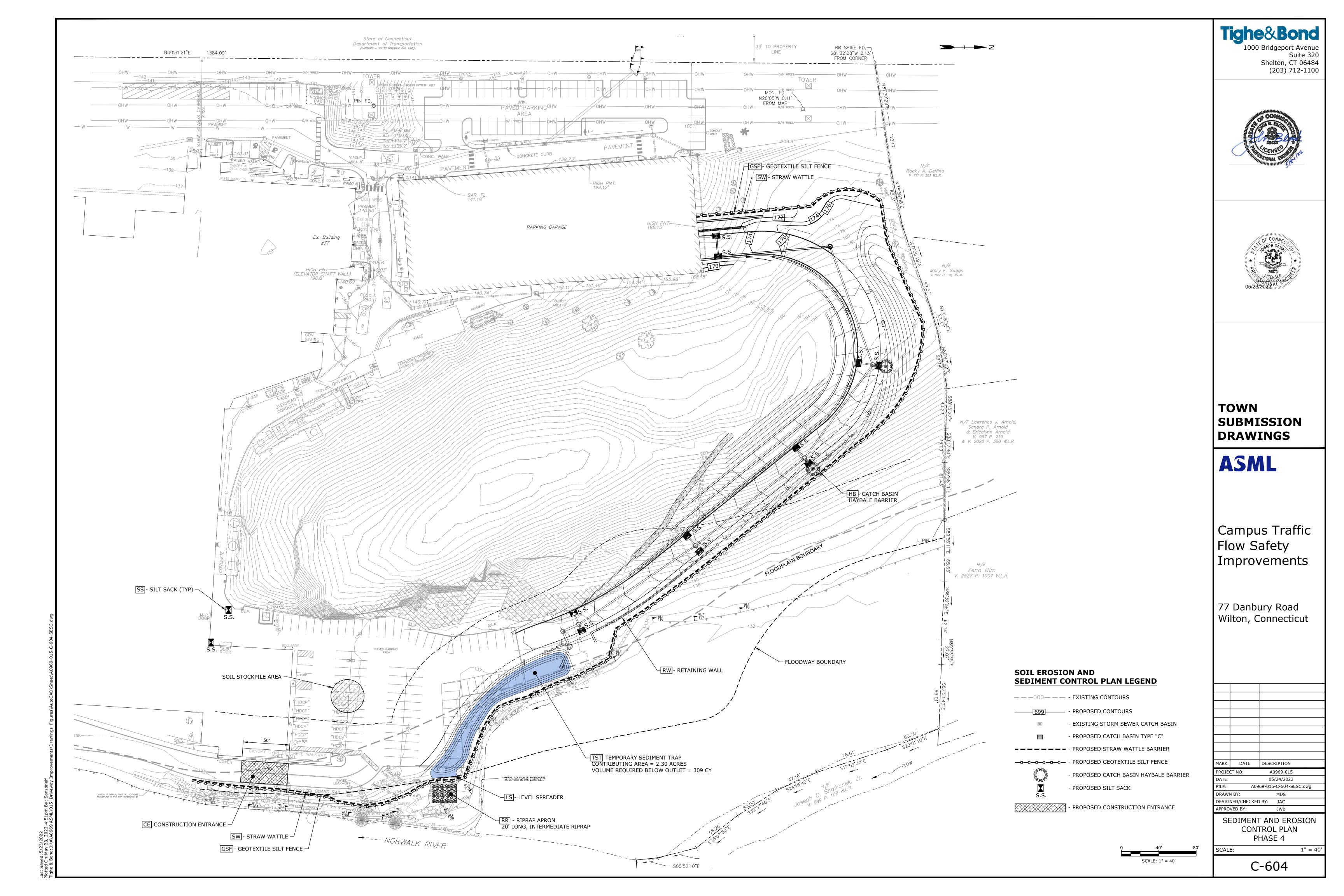
DRAINAGE AND UTIL PLAN
SCALE:

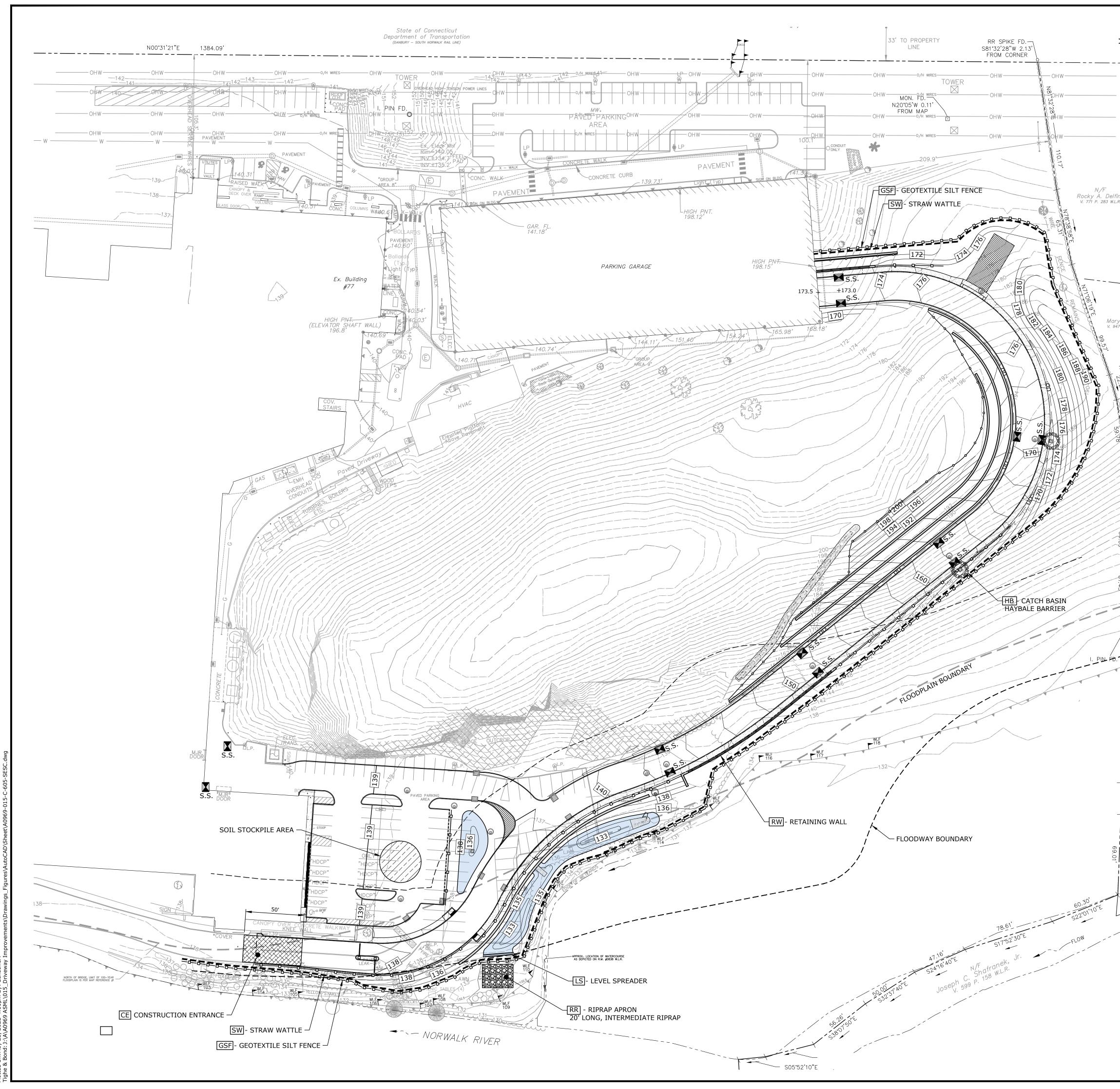












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Delfino W.L.R.			CONSESSIONAL ENSUINE
N/F Mary F. Suggs A 947 P. 196 W.L.R.			SEPH CANSO 20873 20873
N73"56'34"E N80'47'09"E			05/23/2022
S88815 S88815 S22 F N/F Lawrence J. Arnol Sandra P. Arnold & Ericalynn Arnold S88177 & V. 2028 P. 300 W.L. S609			TOWN SUBMISSION DRAWINGS
0"E \$89.58'11"E			ASML
FD. 55, N/F 55, Zena Kim V. 2527 P. 1007 W.L.R.			Campus Traffic Flow Safety Improvements
S86"32'38"E 62.14' N89"33'		NTROL PLAN LEGEND	77 Danbury Road Wilton, Connecticut
5,35"E 57 97 88753'40"E 69.01'	- <u>699</u> - 	• EXISTING CONTOURS • PROPOSED CONTOURS • EXISTING STORM SEWER CATCH BASIN • PROPOSED CATCH BASIN TYPE "C" • PROPOSED HAYBALE BARRIER • PROPOSED GEOTEXTILE SILT FENCE	
		PROPOSED CONSTRUCTION FENCE PROPOSED CATCH BASIN HAYBALE BARRIER PROPOSED SILT SACK PROPOSED CONSTRUCTION ENTRANCE	MARK     DATE     DESCRIPTION       PROJECT NO:     A0969-015       DATE:     05/24/2022       FILE:     A0969-015-C-605-SESC.dwg
		PROPOSED EROSION CONTROL BLANKET	DRAWN BY: MDS DESIGNED/CHECKED BY: JAC APPROVED BY: JWB SEDIMENT AND EROSION CONTROL PLAN PHASE 5 SCALE: 1" = 40'
		SCALE: 1" = 40'	C-605

### SEDIMENT AND EROSION CONTROL NOTES

- ALL SEDIMENTATION AND EROSION CONTROL MEASURES SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARDS AND SPECIFICATIONS OF THE "2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL", CTDEEP BULLETIN NO. 34, AND ALL AMENDMENTS AND ADDENDA THERETO AS PUBLISHED BY THE CONNECTICUT DEPARTMENT OF ENERGY AND ENVIRONMENTAL PROTECTION.
- 2. LAND DISTURBANCE SHALL BE KEPT TO THE MINIMUM NECESSARY FOR CONSTRUCTION OPERATIONS.
- 3. INSTALL ALL EROSION CONTROL MEASURES AS SHOWN ON THE PLAN AND ELSEWHERE AS ORDERED BY THE ENGINEER OR THE TOWN.
- 4. PROTECT ALL CATCH BASINS WITH A SILT SACKS, HAYBALE RING, SILT FENCE OR BLOCK AND STONE INLET PROTECTION THROUGHOUT THE CONSTRUCTION PERIOD AND UNTIL ALL DISTURBED AREAS ARE THOROUGHLY STABILIZED.
- 5. WHENEVER POSSIBLE, INSTALL EROSION AND SEDIMENT CONTROL MEASURES PRIOR TO CONSTRUCTION. SEE "EROSION CONTROL NARRATIVE".
- 6. INSTALL ADDITIONAL CONTROL MEASURES DURING THE CONSTRUCTION PERIOD AS ORDERED BY THE ENGINEER.
- 7. MAINTAIN ALL SEDIMENTATION AND EROSION CONTROL MEASURES IN EFFECTIVE CONDITION THROUGHOUT THE CONSTRUCTION PERIOD.
- 8. SEDIMENT REMOVED SHALL BE DISPOSED OF OFF SITE OR IN A MANNER AS REQUIRED BY THE ENGINEER.
- 9. THE CONSTRUCTION CONTRACTOR SHALL BE RESPONSIBLE FOR CONSTRUCTION AND MAINTENANCE OF ALL CONTROL MEASURES THROUGHOUT THE CONSTRUCTION PERIOD.
- 10. PROTECT ALL DISTURBED AREAS EXPOSED FOR MORE THAN 30 DAYS WITH A TEMPORARY VEGETATIVE COVER. SEED THESE AREAS WITH PERENNIAL RYEGRASS AT THE RATE OF 40 LBS. PER ACRE (1 LB. PER 1,000 SO. FT). APPLY SOIL AMENDMENTS AND MULCH AS REQUIRED TO ESTABLISH A UNIFORM STAND OF VEGETATION OVER ALL DISTURBED AREAS.
- 11. THE CONSTRUCTION CONTRACTOR SHALL UTILIZE APPROVED METHODS/MATERIALS FOR PREVENTING THE BLOWING AND MOVEMENT OF DUST FROM EXPOSED SOIL SURFACES ONTO ADJACENT PROPERTIES AND SITE AREAS.
- 12. THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A SUPPLY OF SILT FENCE/HAYBALES AND ANTI-TRACKING CRUSHED STONE ON SITE FOR EMERGENCY REPAIRS. 13. THE CONTRACTOR SHALL INSPECT WEEKLY AT A MINIMUM, ALL DRAINAGE STRUCTURES AND CLEAN THEM AS NEEDED TO PREVENT THE BUILD-UP OF SILT.
- 14. THE CONSTRUCTION CONTRACTOR SHALL CAREFULLY COORDINATE THE PLACEMENT OF EROSION CONTROL MEASURES WITH THE PHASING OF CONSTRUCTION.
- 15. KEEP ALL PAVED ROADWAYS CLEAN. SWEEP BEFORE FORECASTED STORMS.
- 16. TREAT ALL UNPAVED SURFACE WITH 4" MINIMUM OF TOPSOIL PRIOR TO FINAL STABILIZATION.
- 17. INSTALL HAYBALE BARRIERS AND SILT FENCING ALONG THE TOE OF CRITICAL CUT AND FILL SLOPES.
- 18. THE CONTRACTOR SHALL NOTIFY THE TOWN OF WILTON'S ENVIRONMENTAL OFFICIAL PRIOR TO THE INSTALLATION OF EROSION CONTROLS, CUTTING OF TREES, OR ANY EXCAVATION.
- 19. COVER ALL TRUCKS LEAVING THE SITE.
- 20. SOIL TYPE BOUNDARIES SHOWN ON THESE MAPS WERE OBTAINED FROM DIGITAL FILES FROM THE UNIVERSITY OF CONNECTICUT'S MAP AND GEOGRAPHIC INFORMATION CENTER. SOIL TYPE DESIGNATIONS WERE TAKEN FROM THE UNITED STATES DEPARTMENT OF AGRICULTURE, SOIL CONSERVATION SERVICE "SOIL SURVEY OF FAIRFIELD COUNTY."
- 21. CHECK ALL SEDIMENTATION AND EROSION CONTROLS WEEKLY AND/OR AFTER EACH RAINFALL EVENT. MAKE NECESSARY REPAIRS IMMEDIATELY.
- 22. INSPECT AND REPAIR EROSION AND SEDIMENT CONTROLS PRIOR TO FORECASTED RAIN EVENTS.
- 23. REMOVE EROSION CONTROLS WHEN ALL DISTURBED AREAS HAVE BEEN STABILIZED AND THE TOWN HAS PROVIDED AUTHORIZATION. DISTURBED AREAS SHALL BE SEEDED AND MULCHED.

### **CONSTRUCTION SEQUENCE**

### PHASE 1

- 1. HOLD PRE-CONSTRUCTION MEETING WITH DESIGN TEAM AND THE TOWN'S ENVIRONMENTAL AFFAIRS DIRECTOR TO DISCUSS THE SEQUENCE OF OPERATIONS AND THE SEDIMENT AND EROSION CONTROLS.
- 2. INSTALL SILT FENCE AND STRAW WATTLES ALONG RIPARIAN CORRIDOR.
- **3. INSTALL SILT SACKS AT CATCH BASINS**
- 4.POST SIGNAGE AT DRIVEWAY BRIDGE DIRECTING ALL TRAFFIC TO TURN LEFT, EXCEPT CONSTRUCTION VEHICLES. **5. INSTALL CONSTRUCTION ENTRANCE**
- 6. EXCAVATE TEMPORARY SEDIMENT TRAP

### PHASE 2

- 1. MAINTAIN AND REPLENISH/REPLACE CONTROLS FROM PHASE 1.
- 2. CONSTRUCT LOWER RETAINING WALL
- 3. ROUGH GRADE LOWER SECTION OF ROADWAY
- 4. EXCAVATE UP THE HILLSIDE TO CREATE HAUL ROAD ACCESS TO THE TOP OF THE RIDGE.
- 5. PLACE SOME OF THE ROCK REMOVED ON THE DOWN SLOPE SIDE OF THE HAUL ROAD FILL TO ARMOR THE SLOPE, 6. INSTALL LOWEST PORTION OF DRAINAGE SYSTEM.
- 7. PROTECT BASIN INLETS WITH SILT SACKS.
- 8. PROTECT HEADWALL INLET WITH STONE CHECK DAM.

### PHASE 3

- 1. MAINTAIN AND REPLENISH/REPLACE CONTROLS FROM PHASE 2.
- 2. INSTALL SEDIMENT AND EROSION CONTROLS NEAR PARKING GARAGE.
- 3. EXCAVATE EASTERN PORTION OF DRIVEWAY AND ROUGH GRADE, CONSTRUCTING ROCK CUTS AND WALLS.
- 4. CONSTRUCT RIPRAP SWALE ABOVE WALLS.
- 5. INSTALL DRAINAGE SYSTEM.
- 6.PROTECT NEW CATCH BASINS WITH SILT SACKS.

### <u>PHASE 4</u>

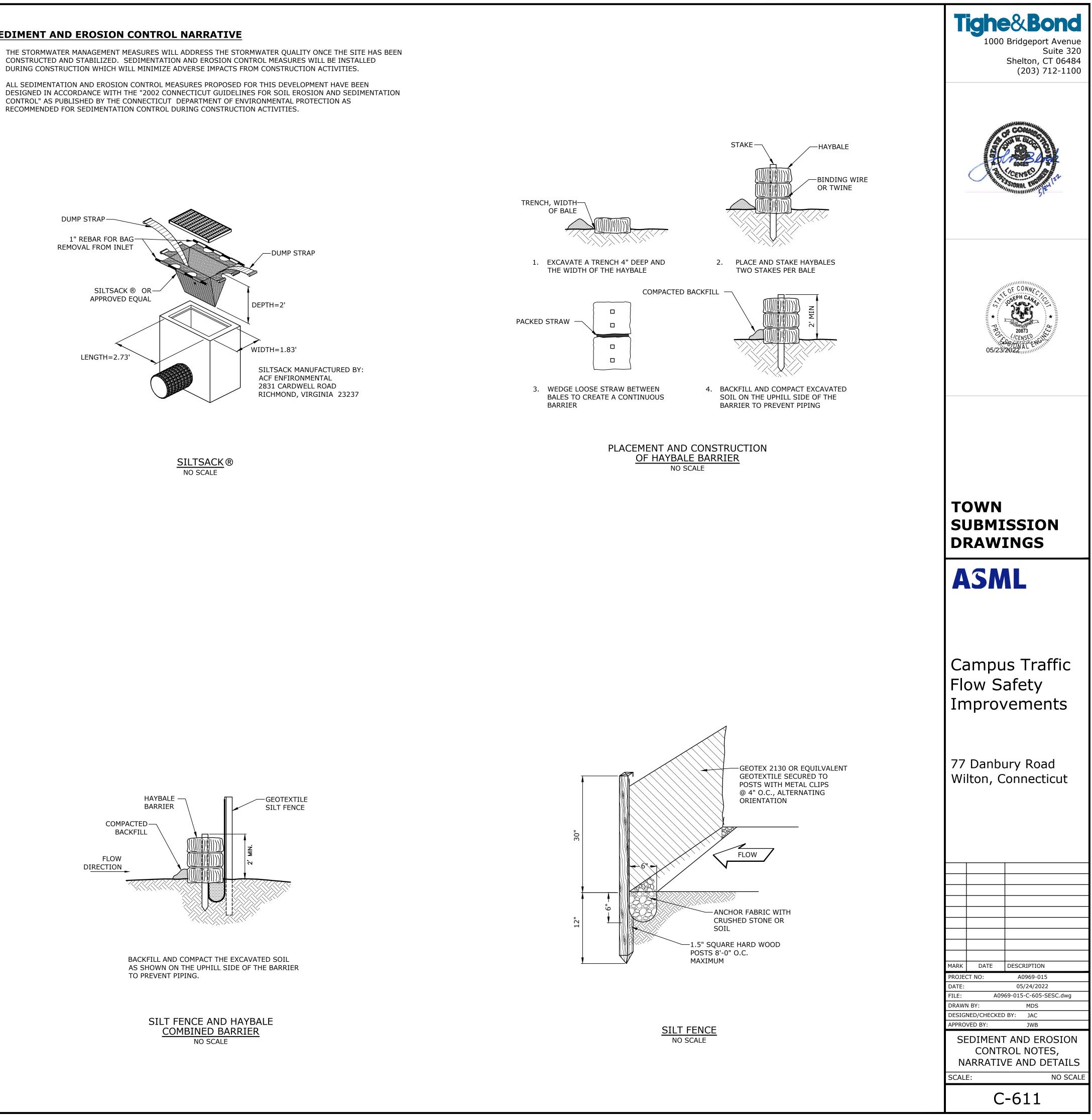
- 1. MAINTAIN AND REPLENISH/REPLACE CONTROLS FROM PHASE 3.
- 2. CONSTRUCT RETAINING WALLS NEAR PARKING GARAGE.
- 3. MAKE STRUCTURAL MODIFICATIONS TO PARKING GARAGE FOR NEW ENTRANCE.
- 4. INSTALL UPPERMOST CATCH BASINS OF DRIVEWAY DRAINAGE SYSTEM
- 5. PROTECT NEW CATCH BASINS WITH SILT SACKS.

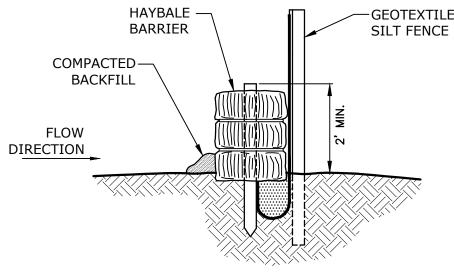
### PHASE 5

- 1. ROUGH GRADE PARKING LOT.
- 2. INSTALL PARKING LOT DRAINAGE, RAIN GARDEN AND INFILTRATION SYSTEM.
- 3. CONSTRUCT SIDEWALKS, REINFORCED TURF AREAS, AND OTHER APPURTENANCES.
- 4.CONSTRUCT STORMWATER MANAGEMENT BASIN AND RETAINING WALL.
- 5. PAVE PARKING AREA AND DRIVEWAY.
- 6.ESTABLISH TURF AND STABILIZE
- 7. REMOVE EROSION CONTROLS.

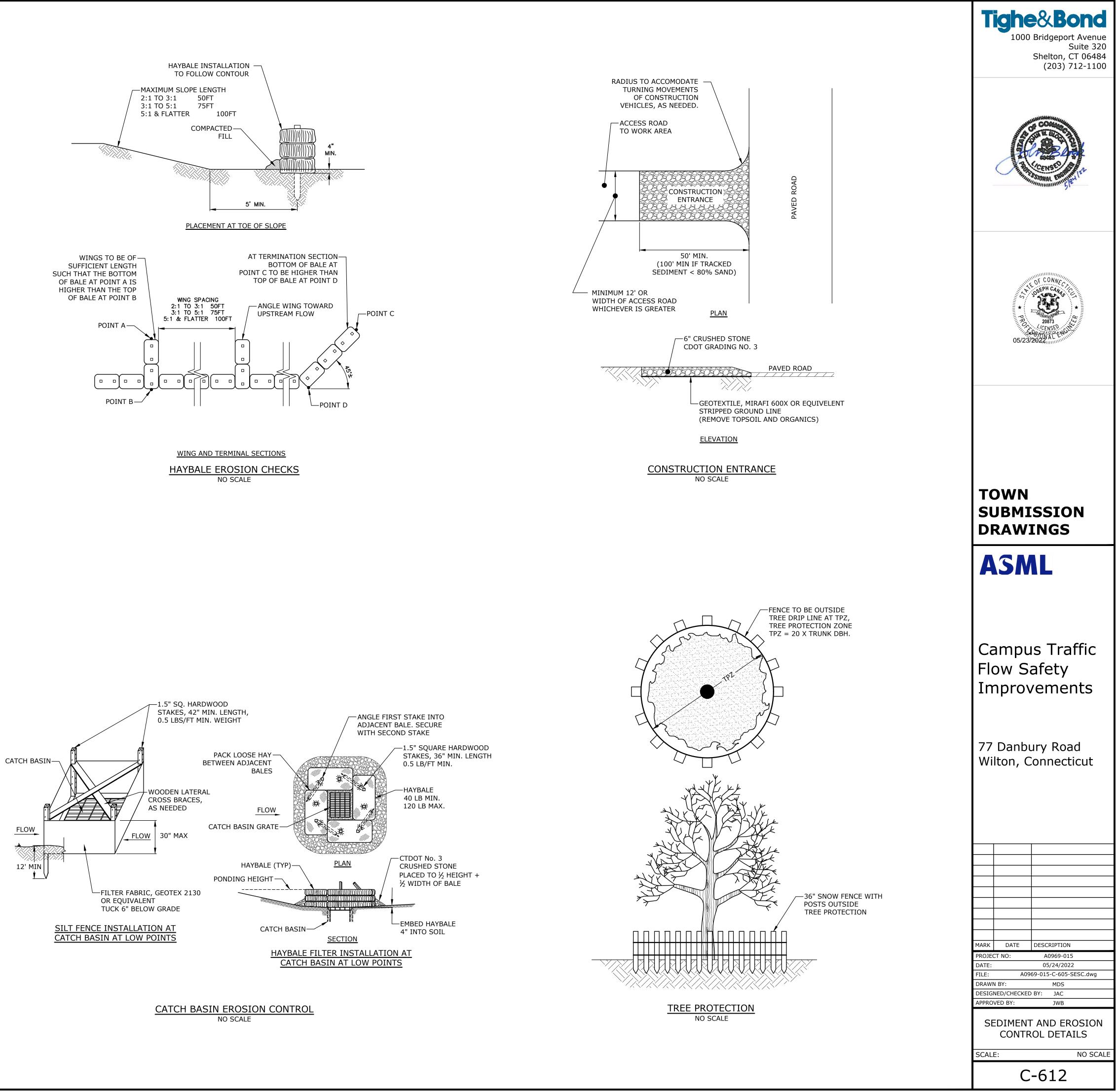
### SEDIMENT AND EROSION CONTROL NARRATIVE

- THE STORMWATER MANAGEMENT MEASURES WILL ADDRESS THE STORMWATER QUALITY ONCE THE SITE HAS BEEN CONSTRUCTED AND STABILIZED. SEDIMENTATION AND EROSION CONTROL MEASURES WILL BE INSTALLED DURING CONSTRUCTION WHICH WILL MINIMIZE ADVERSE IMPACTS FROM CONSTRUCTION ACTIVITIES.
- DESIGNED IN ACCORDANCE WITH THE "2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENTATION CONTROL" AS PUBLISHED BY THE CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION AS RECOMMENDED FOR SEDIMENTATION CONTROL DURING CONSTRUCTION ACTIVITIES.

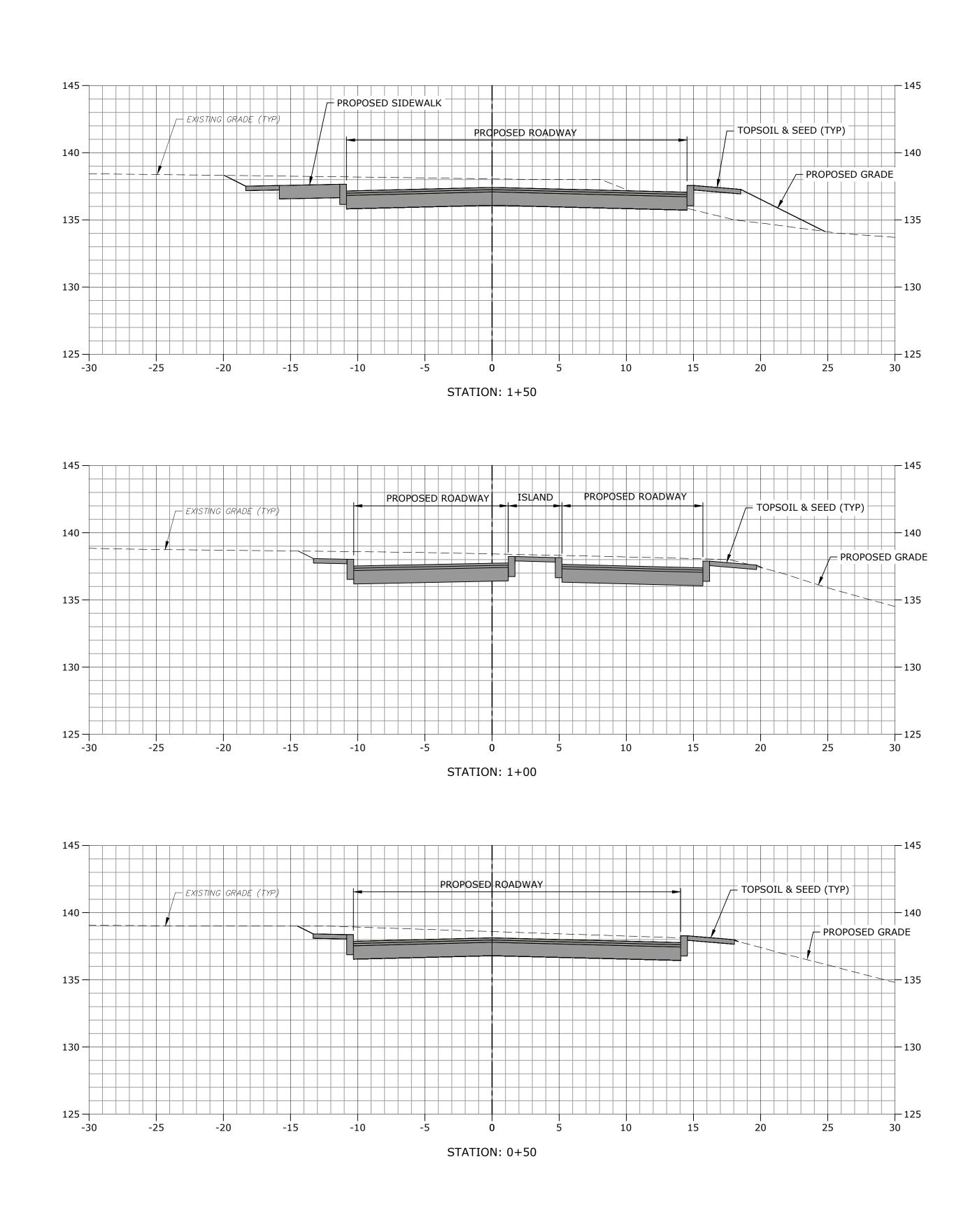


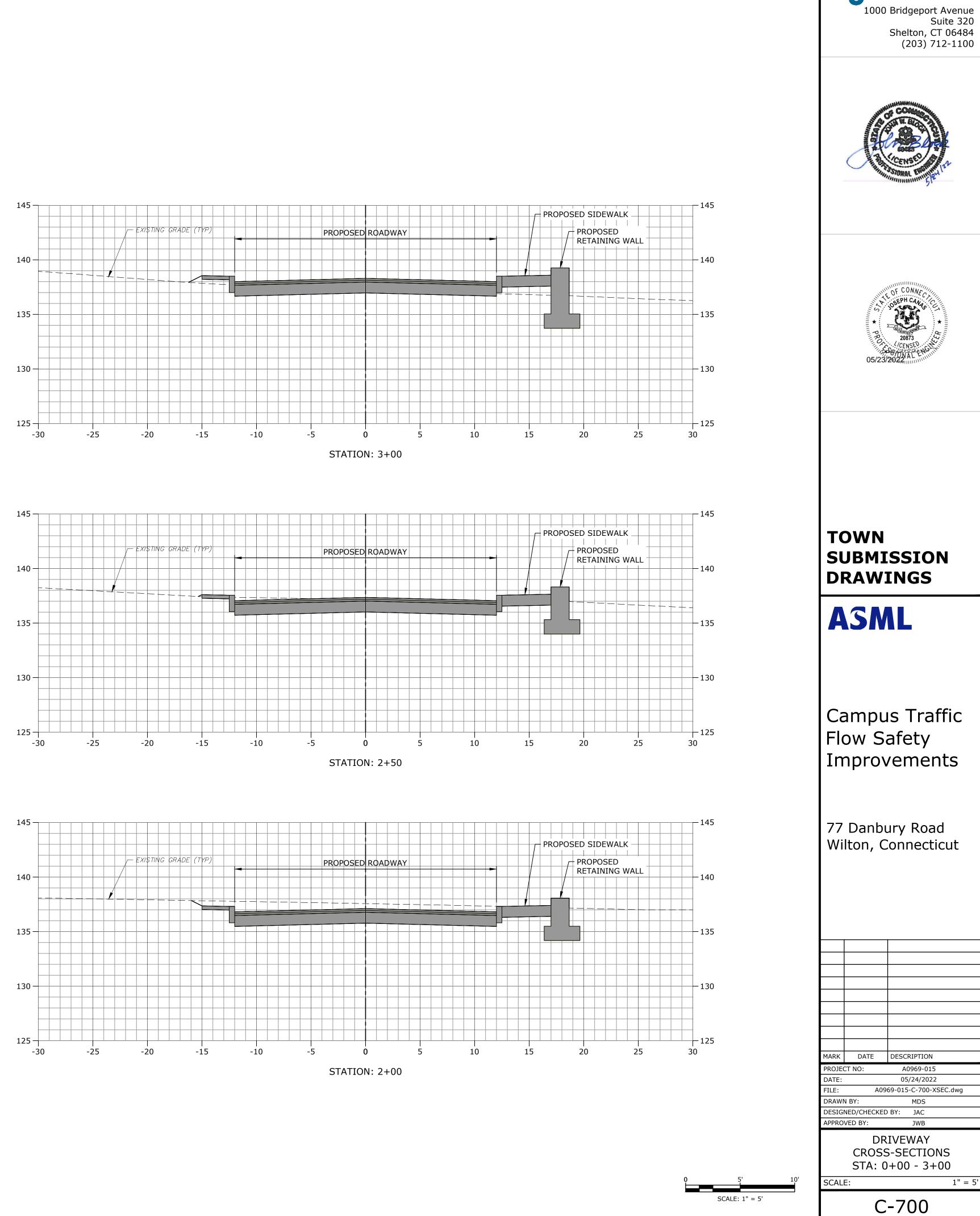


FLOW









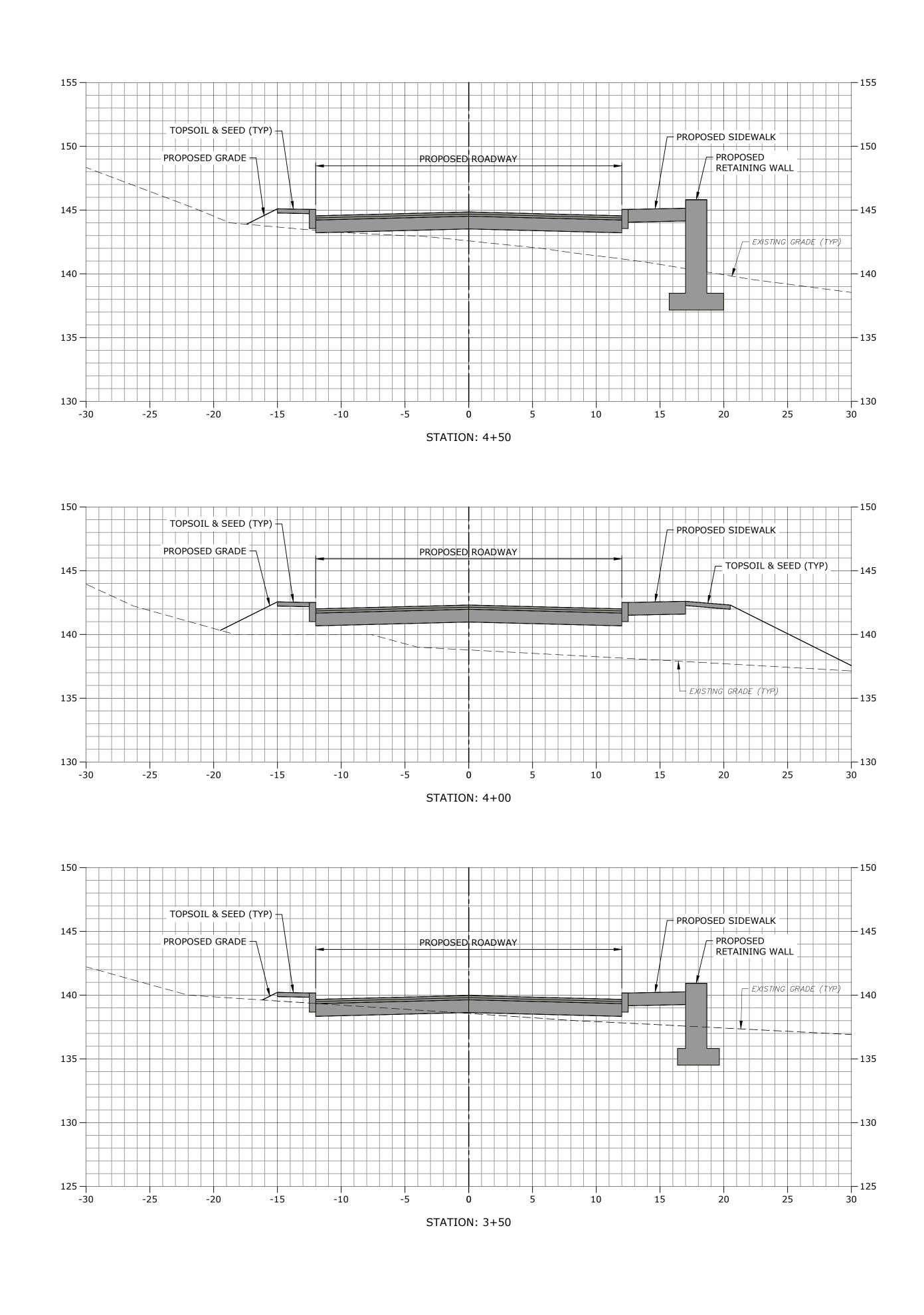
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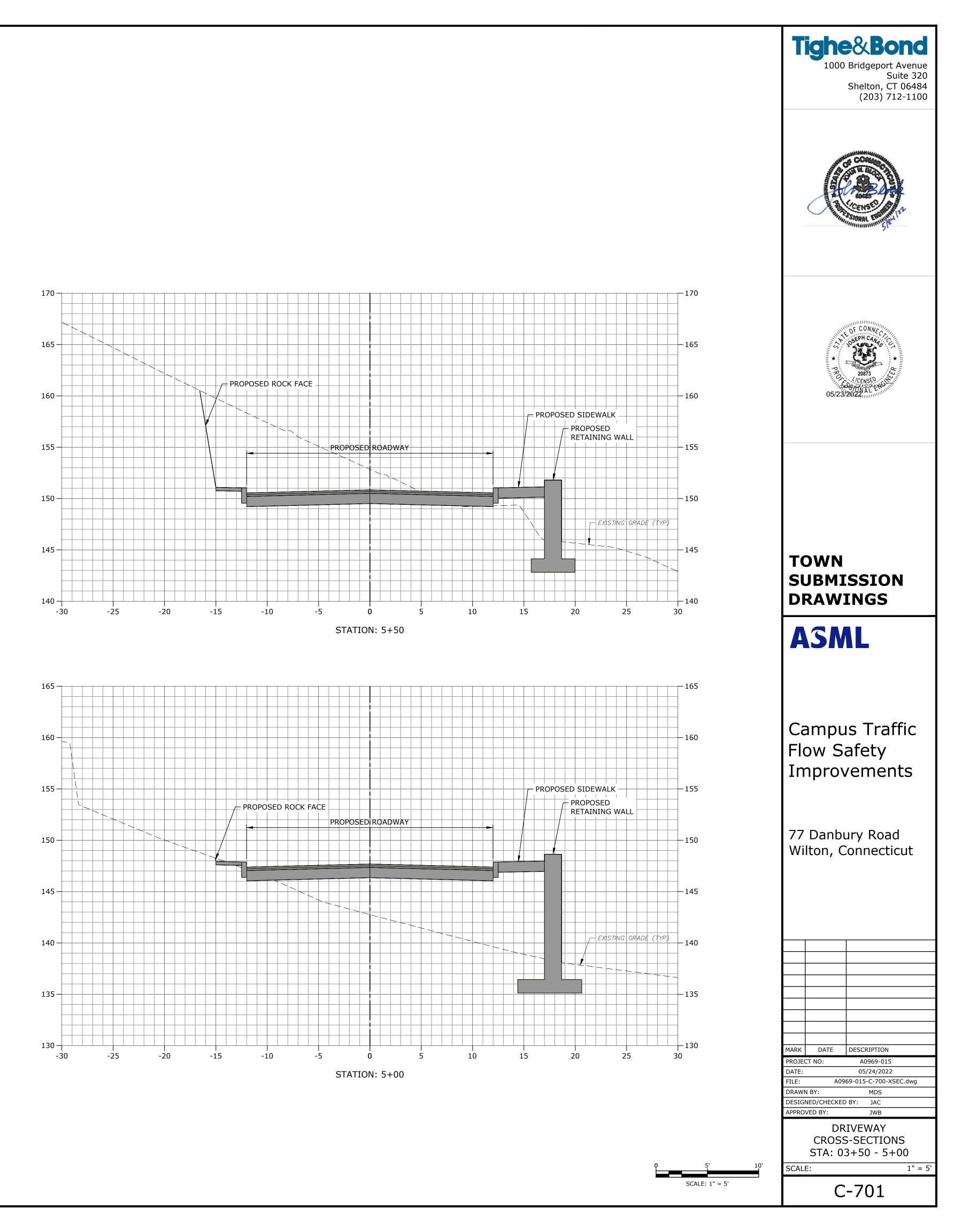
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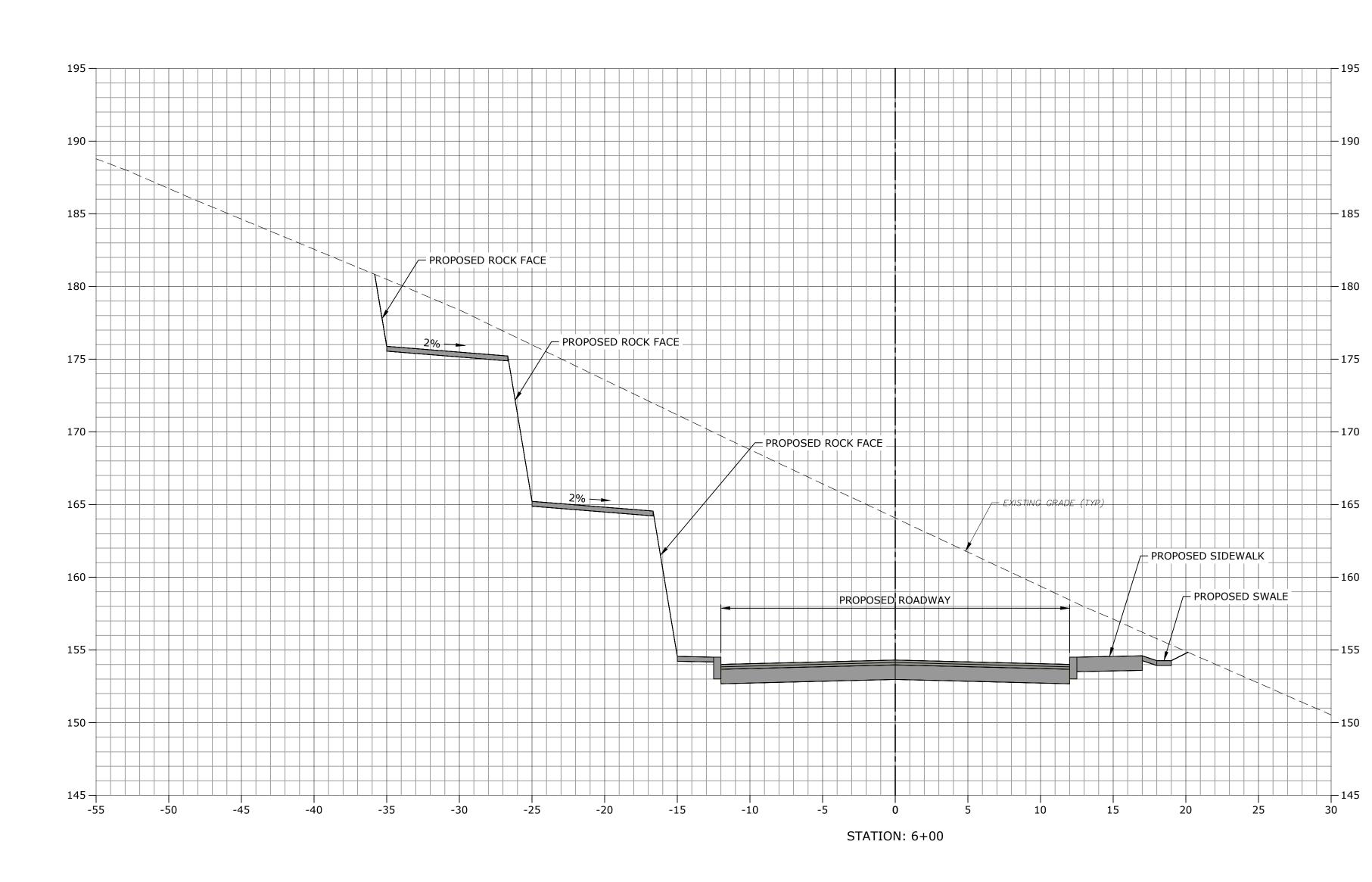
JWB

1" = 5'

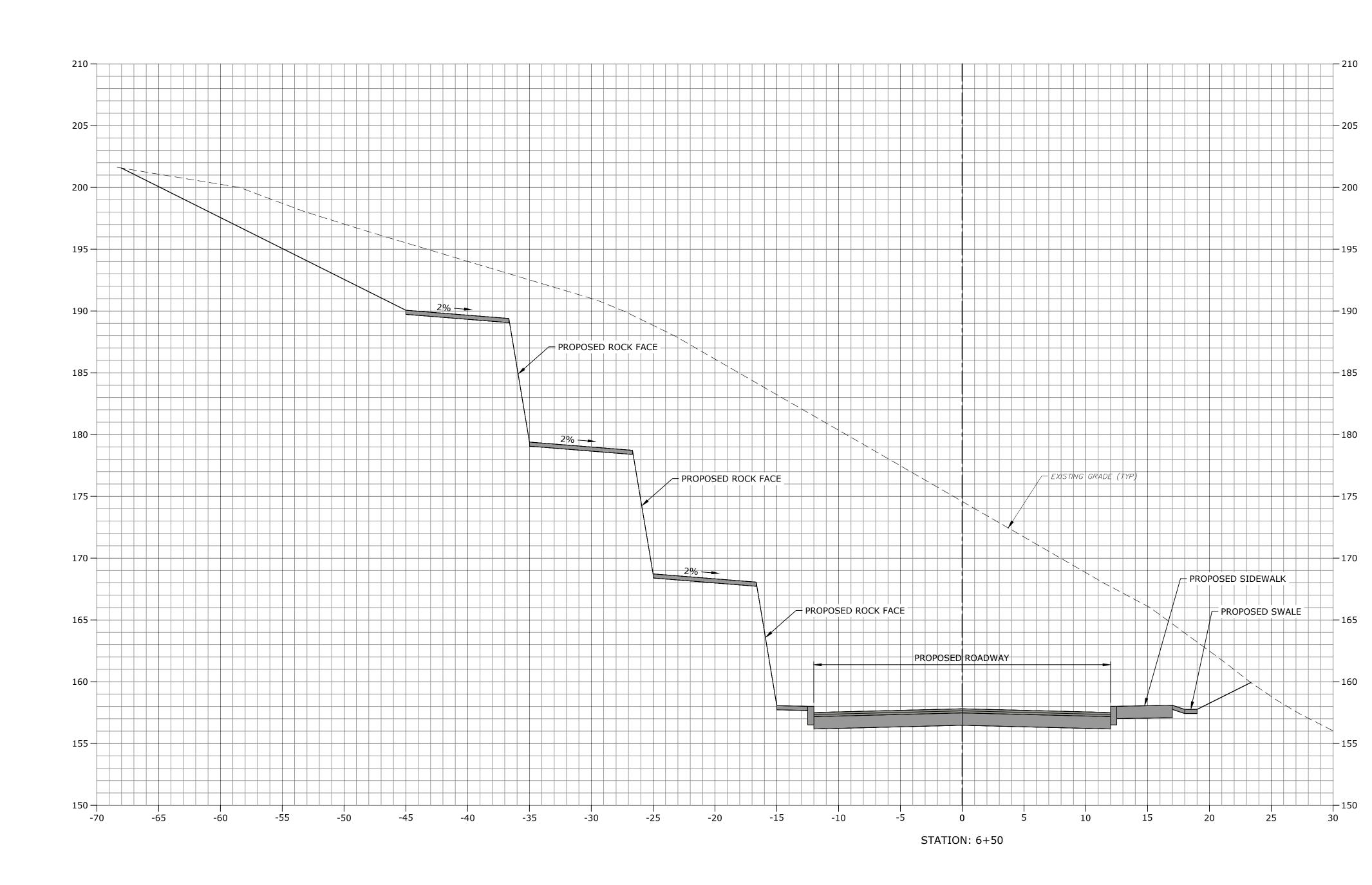


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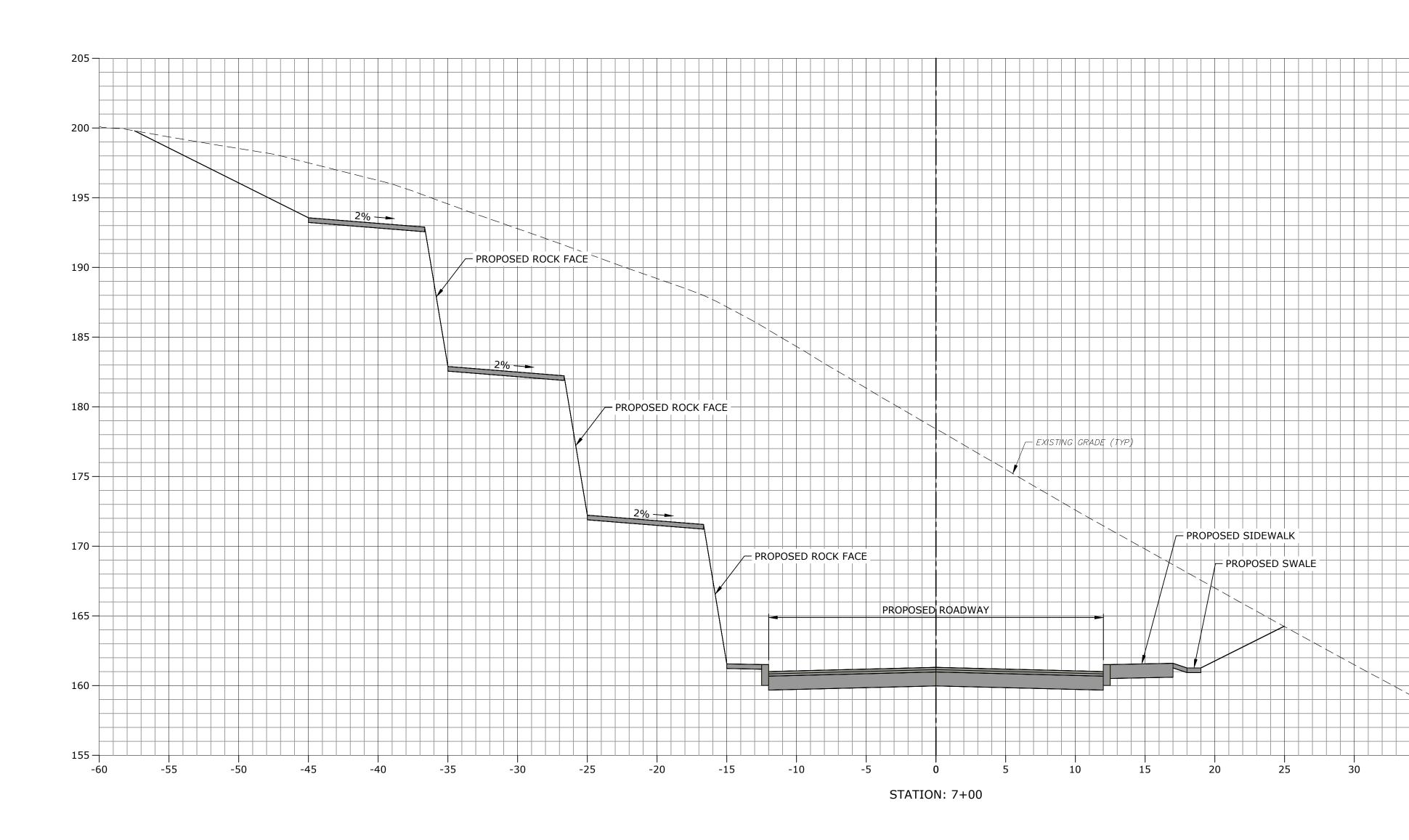
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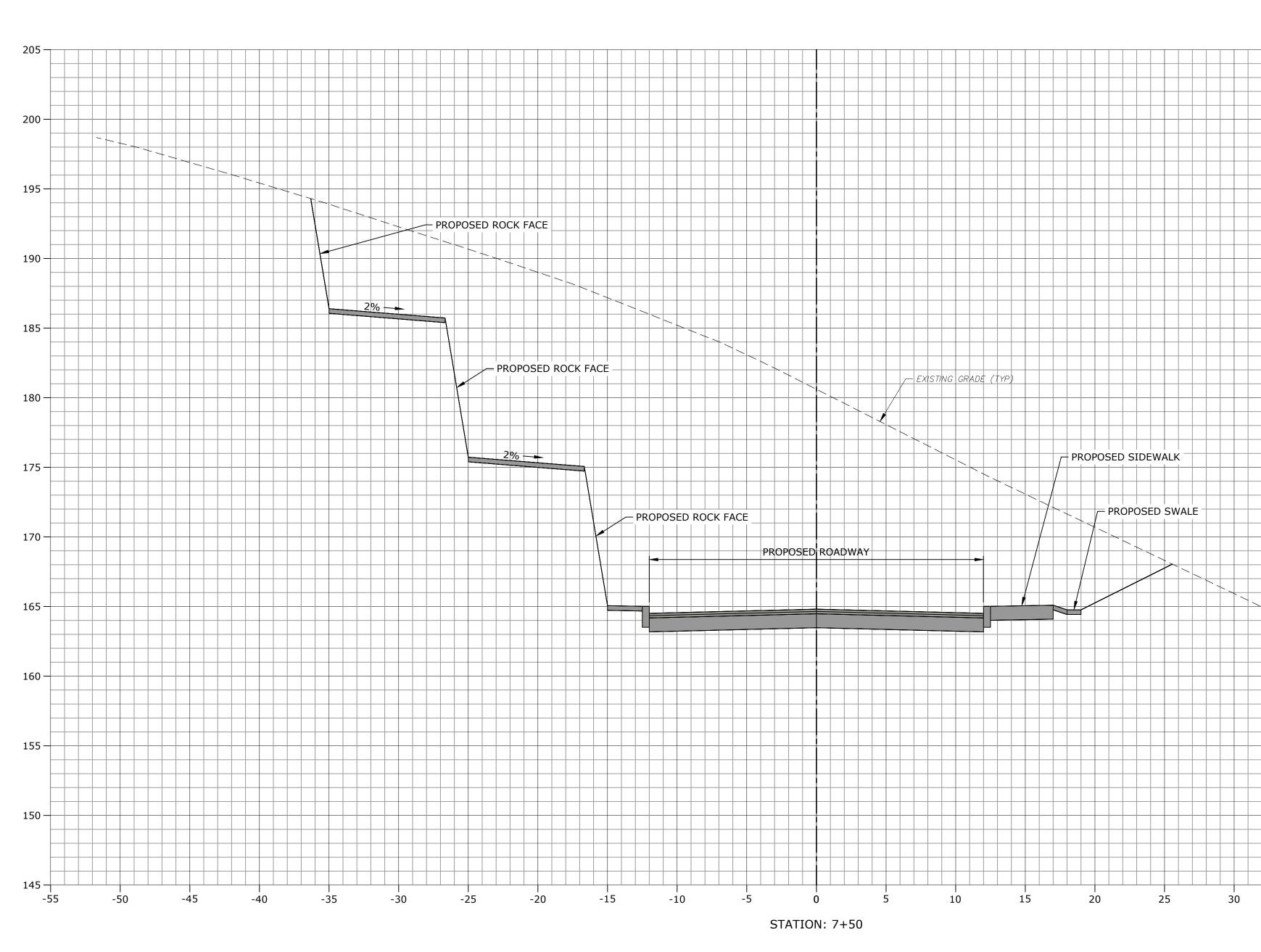
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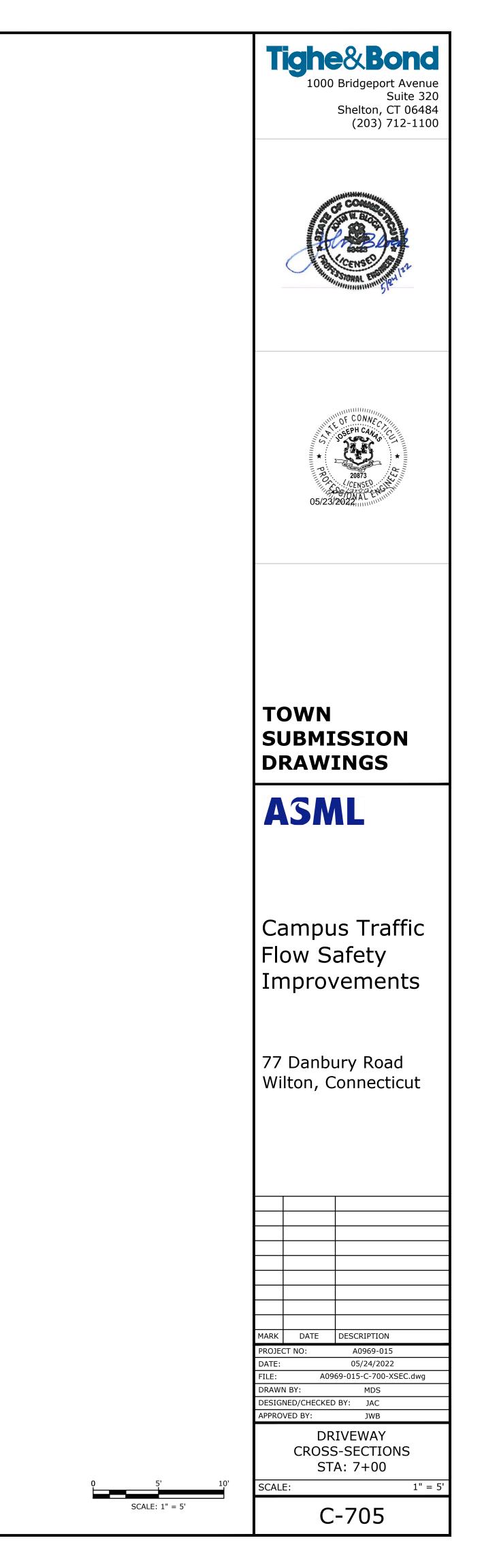
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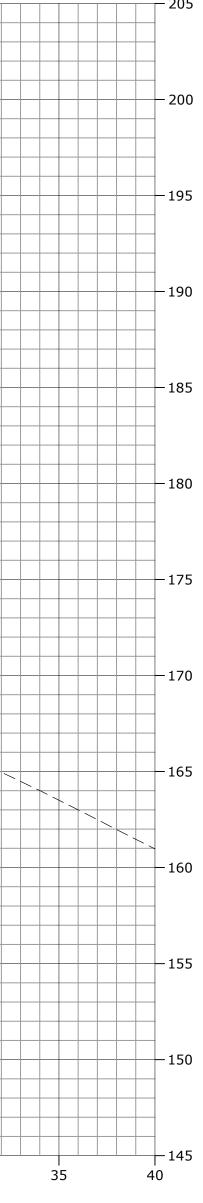


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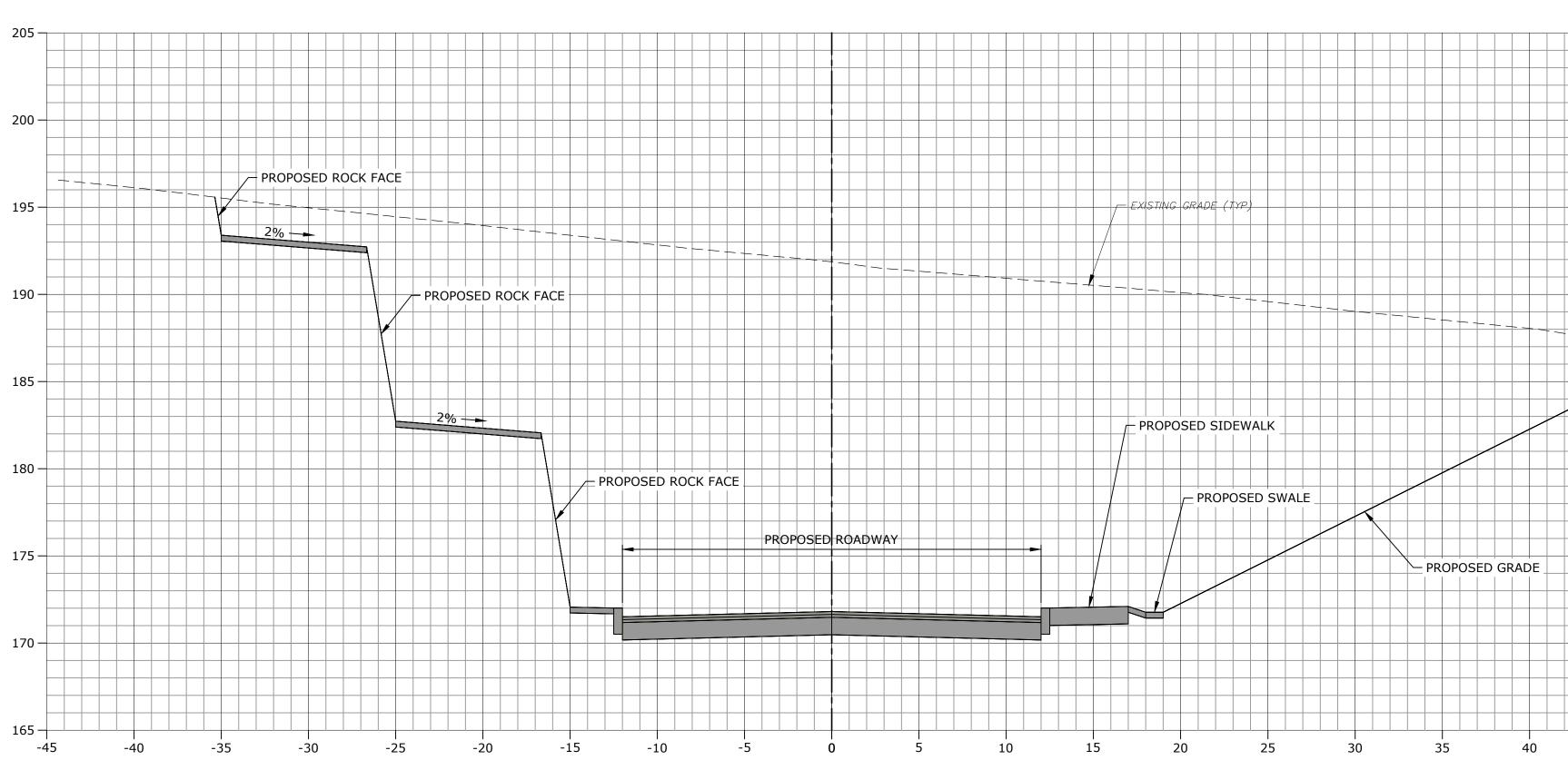
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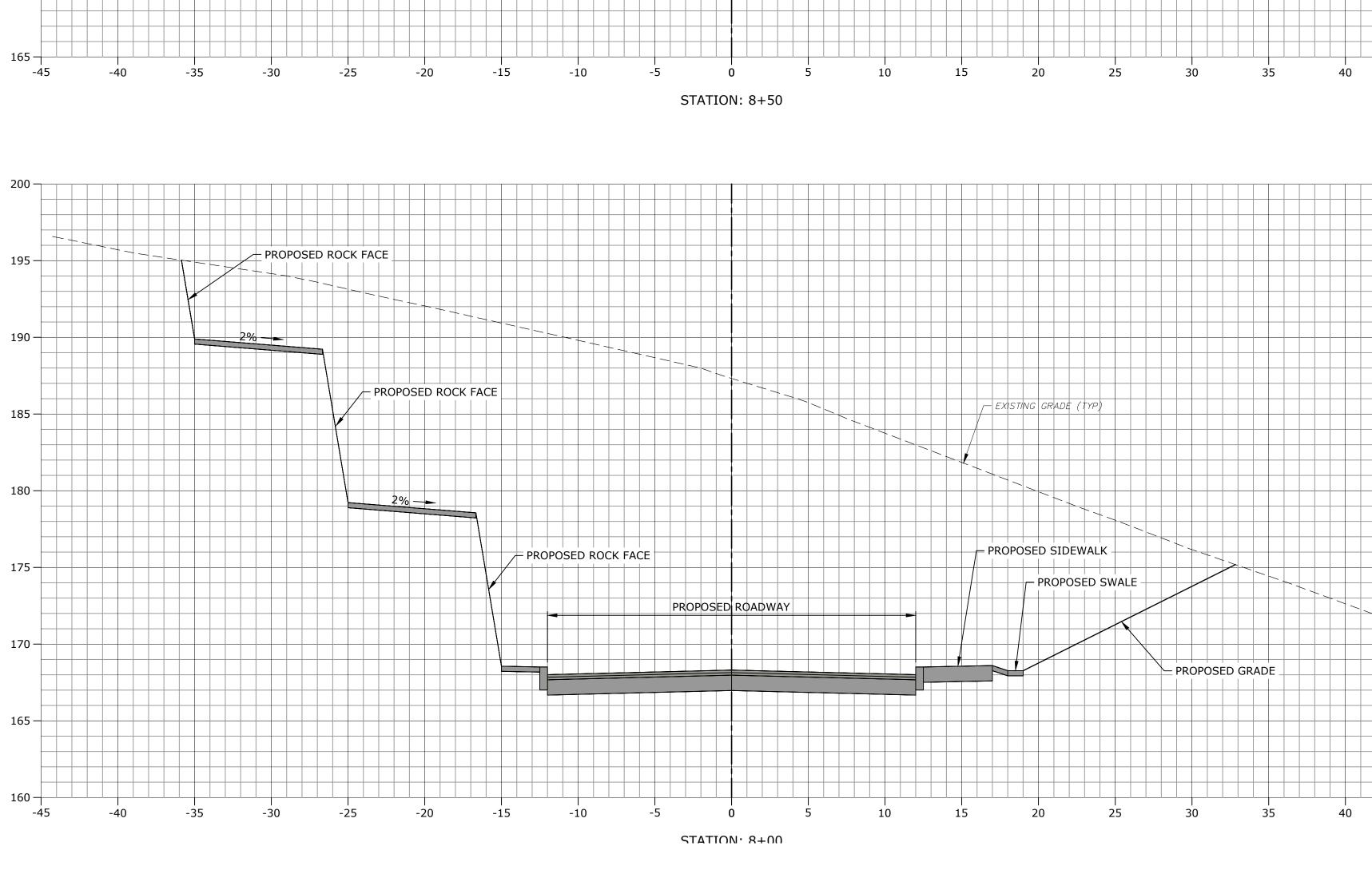


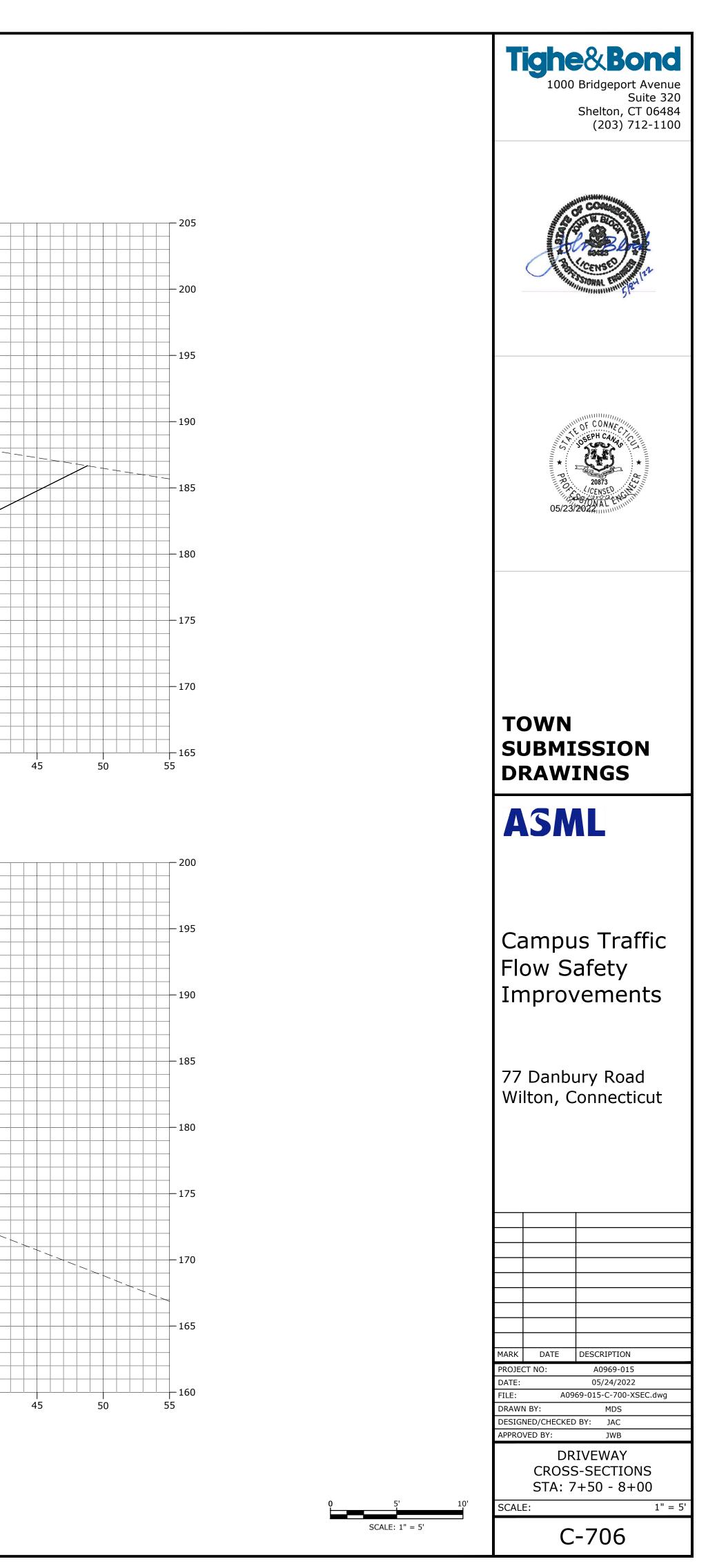


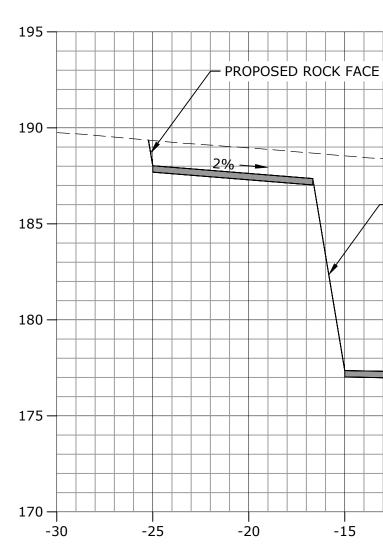


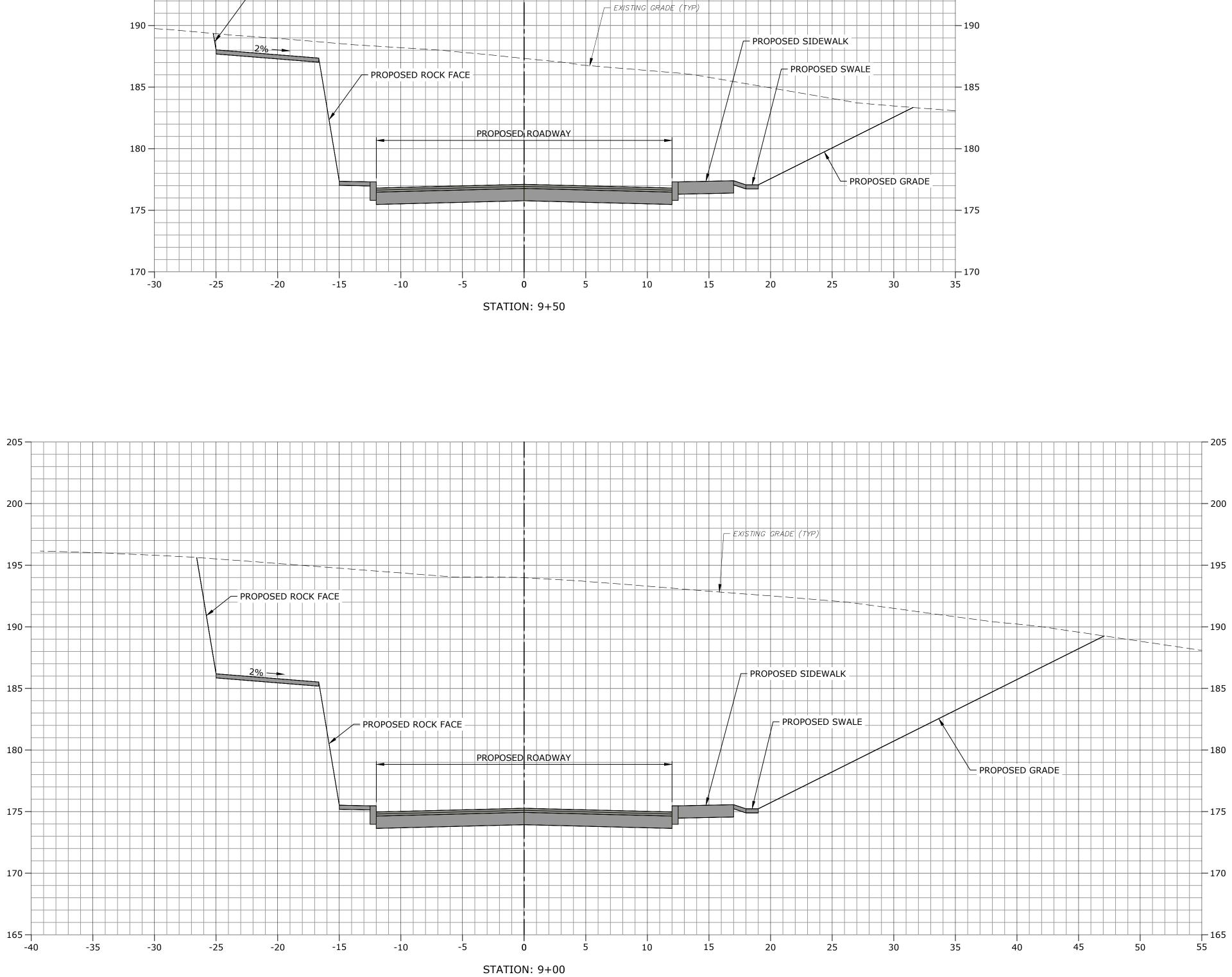


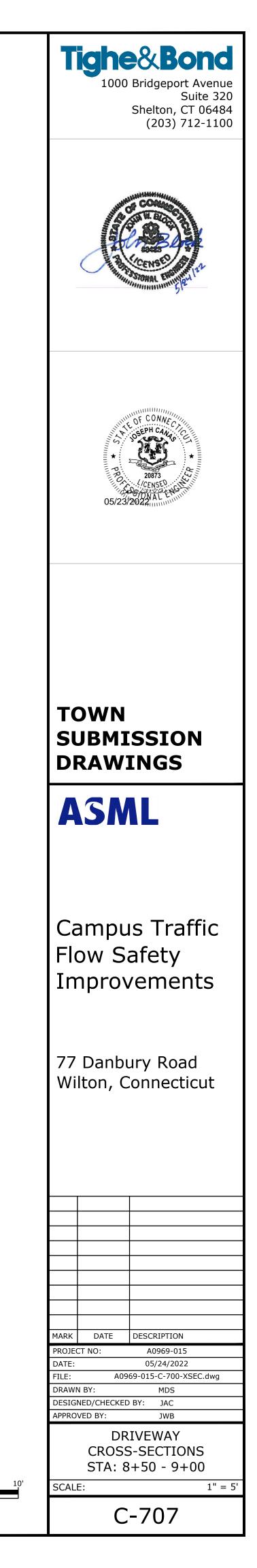




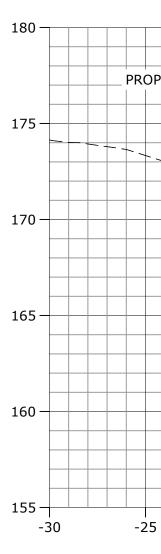


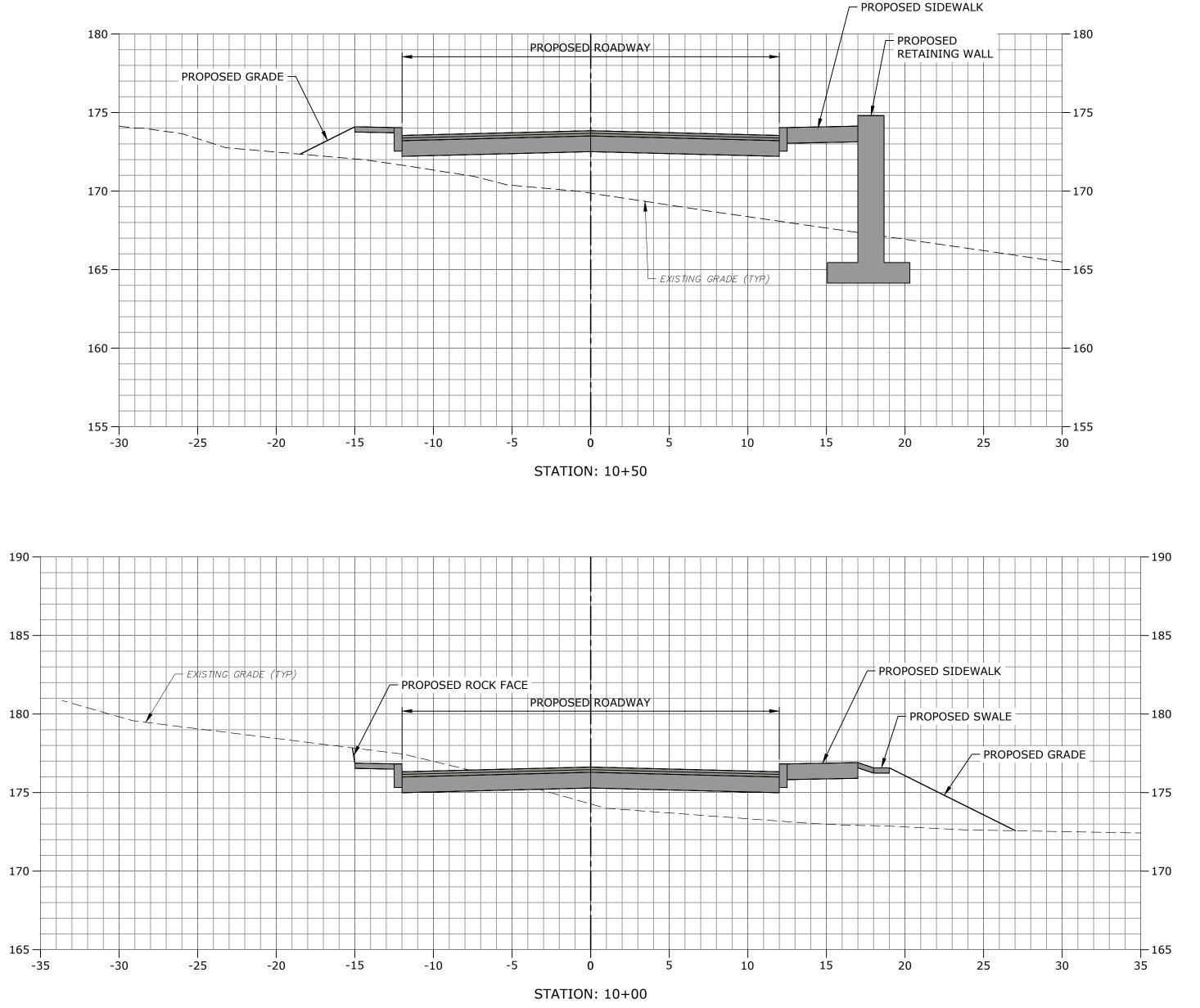




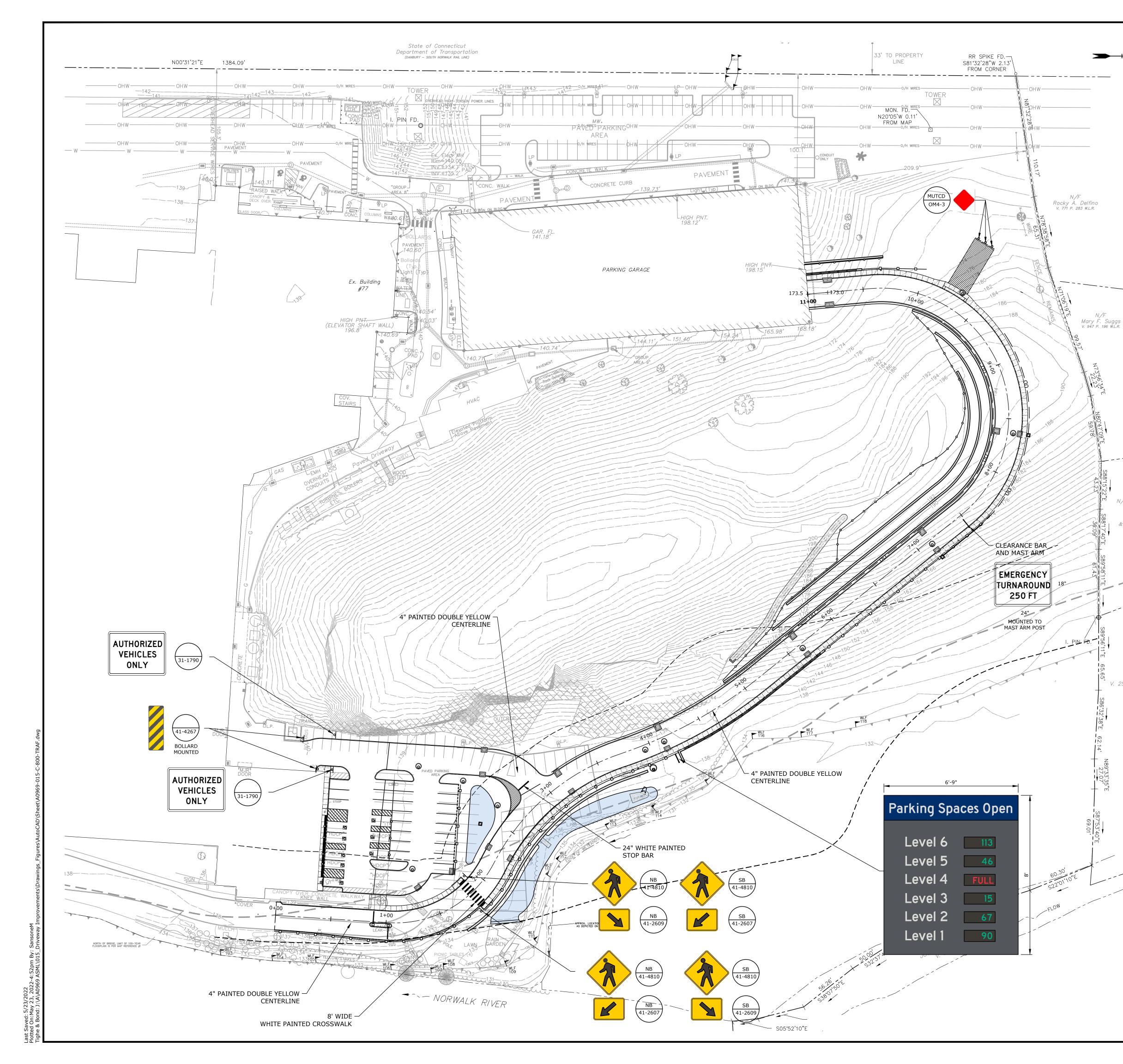


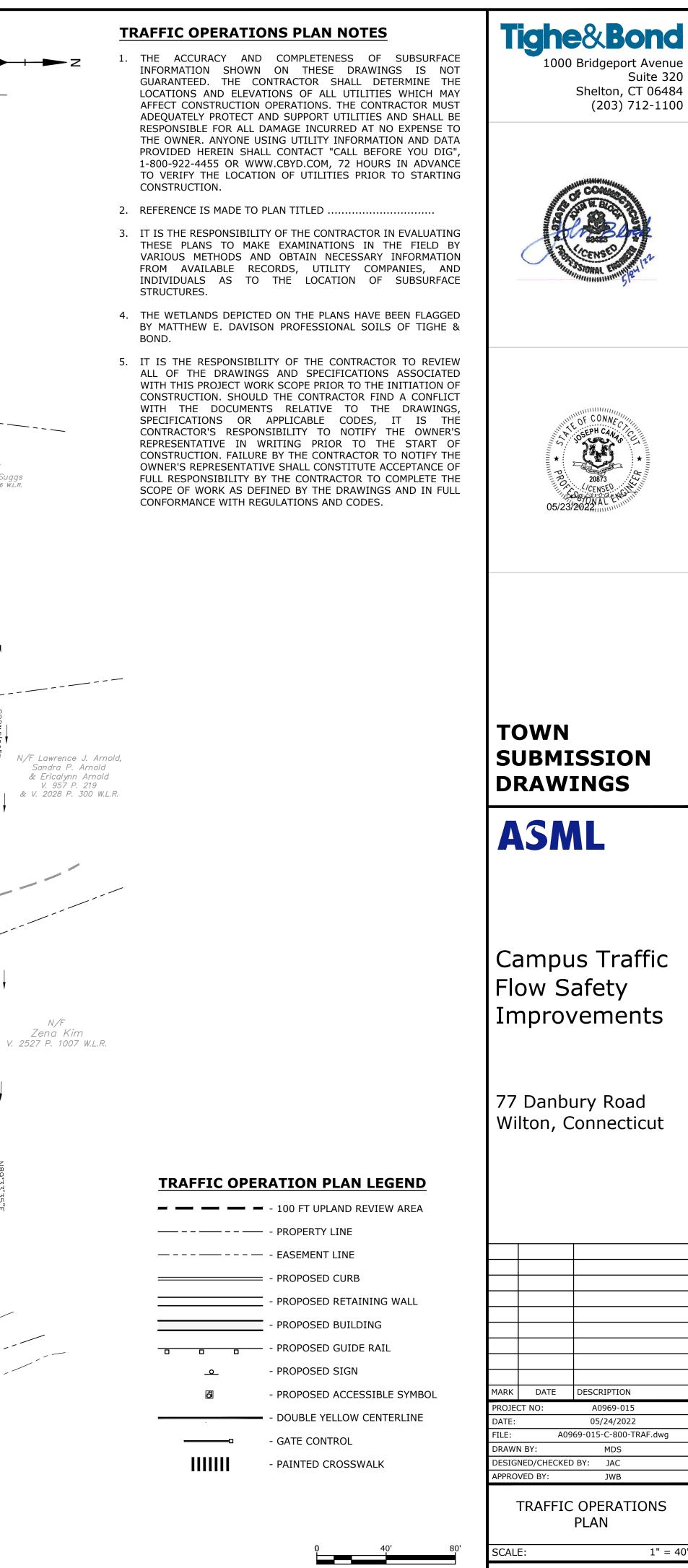
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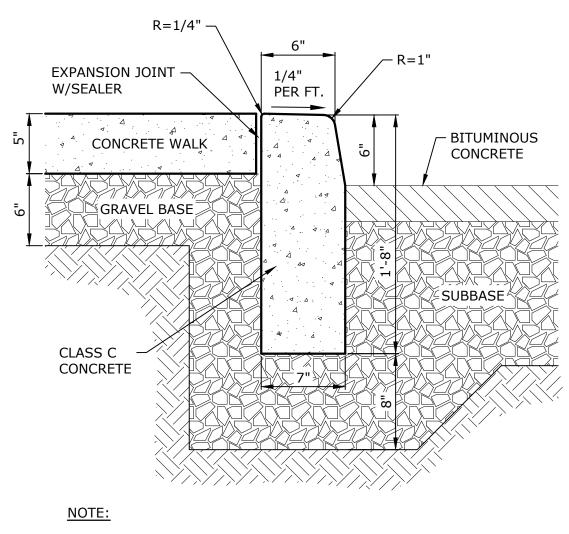
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10'	DRIVEWAY CROSS-SECTIONS STA: $9+50 - 10+00$ SCALE: $1'' = 5'$ C-708





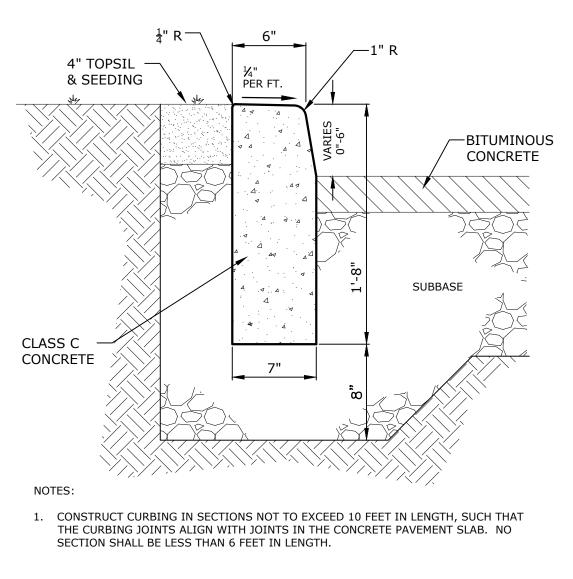
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C-800

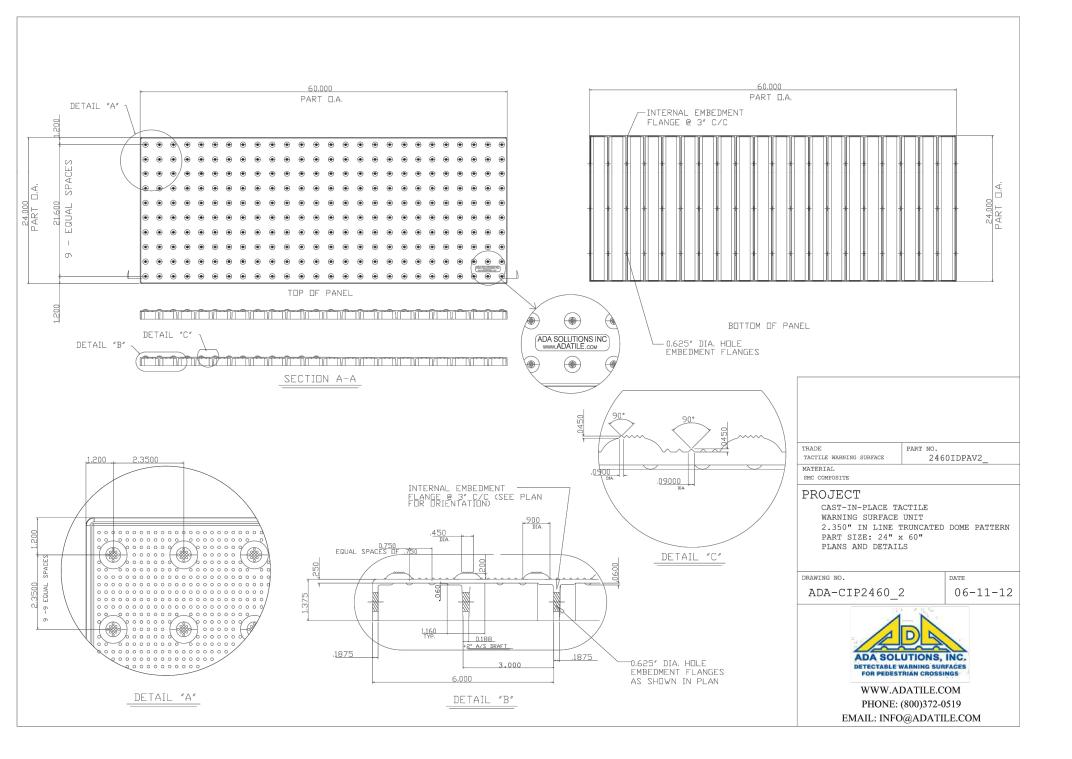


1. CONSTRUCT CURBING IN SECTIONS NOT TO EXCEED 10 FEET IN LENGTH, SUCH THAT THE CURBING JOINTS ALIGN WITH JOINTS IN THE CONCRETE PAVEMENT SLAB. NO SECTION SHALL BE LESS THAN 6 FEET IN LENGTH.

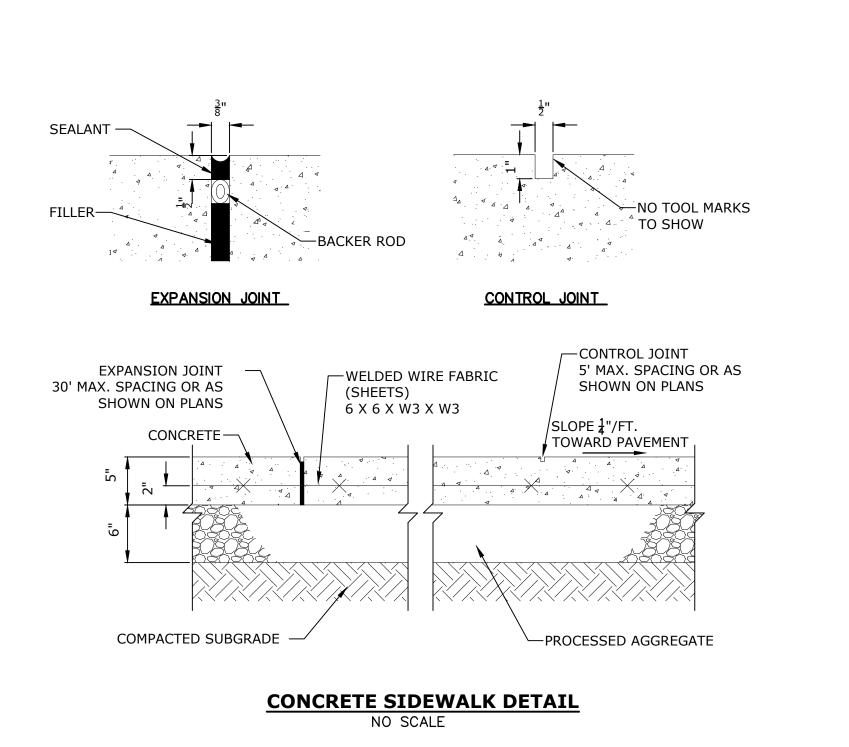


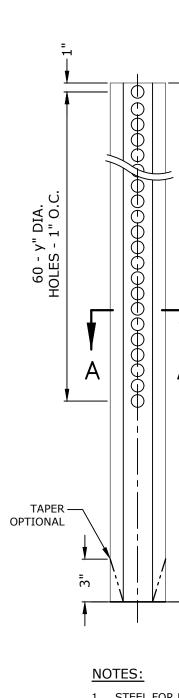


**CONCRETE CURB ADJACENT TO GRASS** NO SCALE

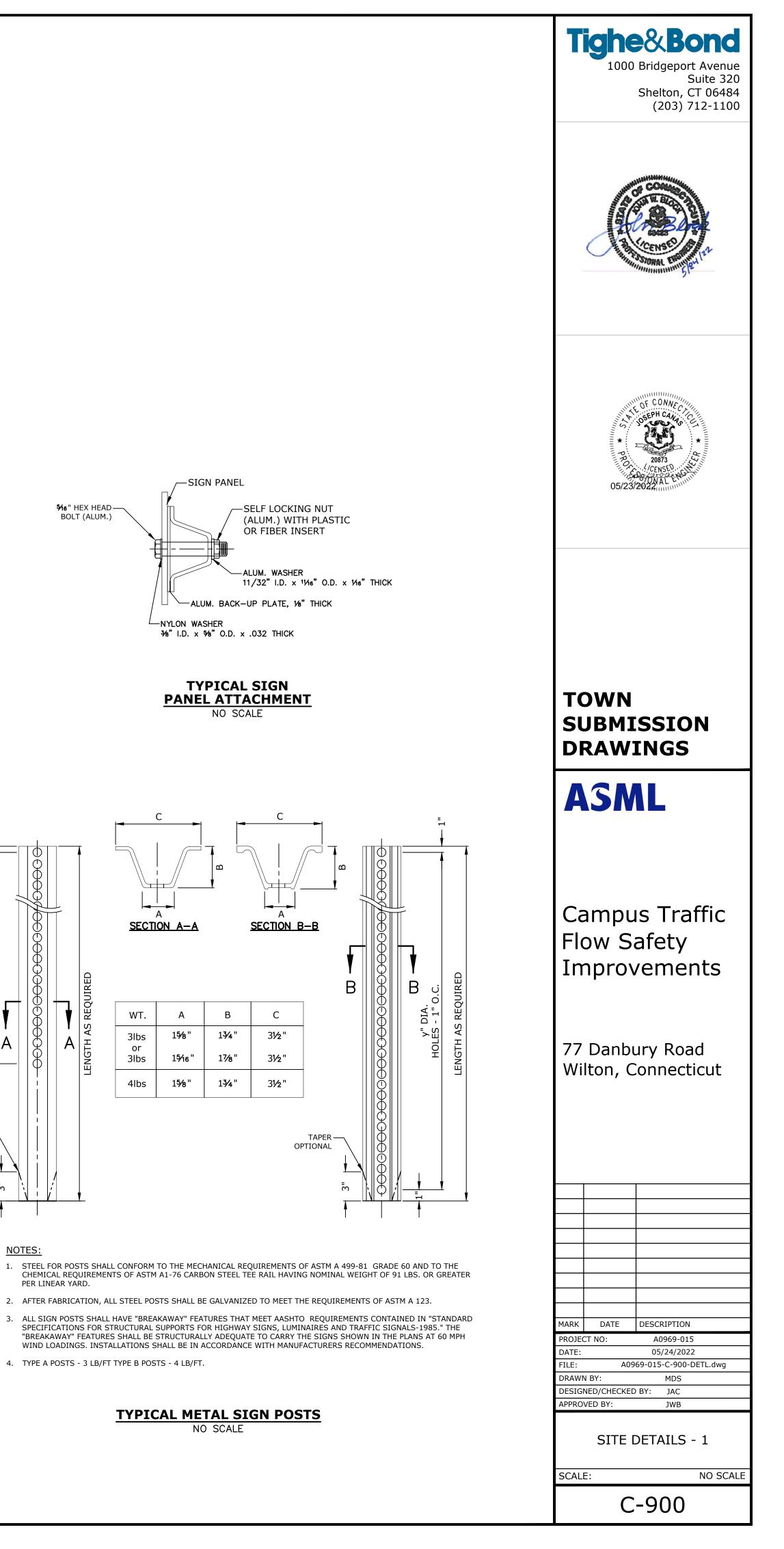


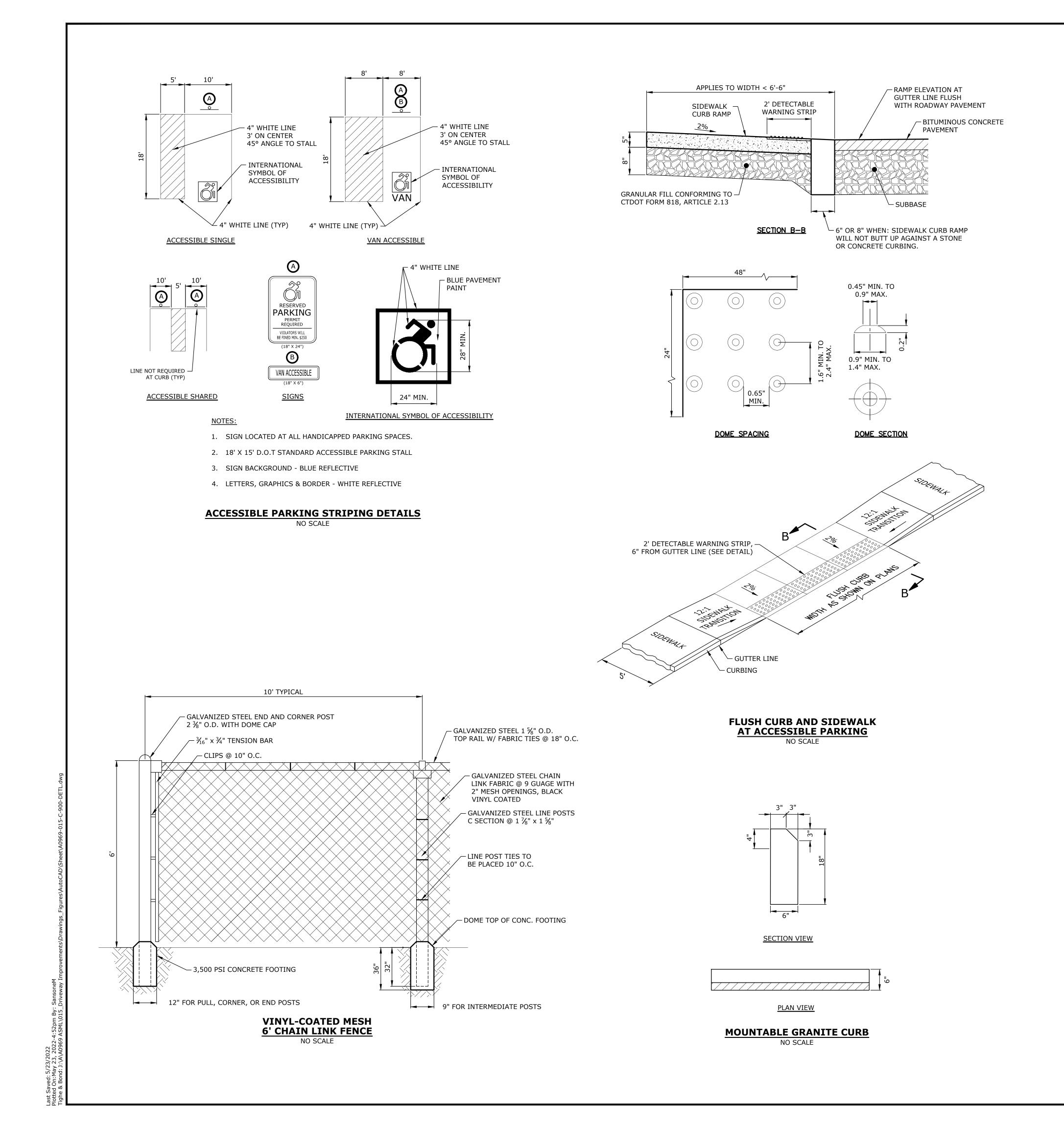
DETECTABLE WARNING TILE NO SCALE

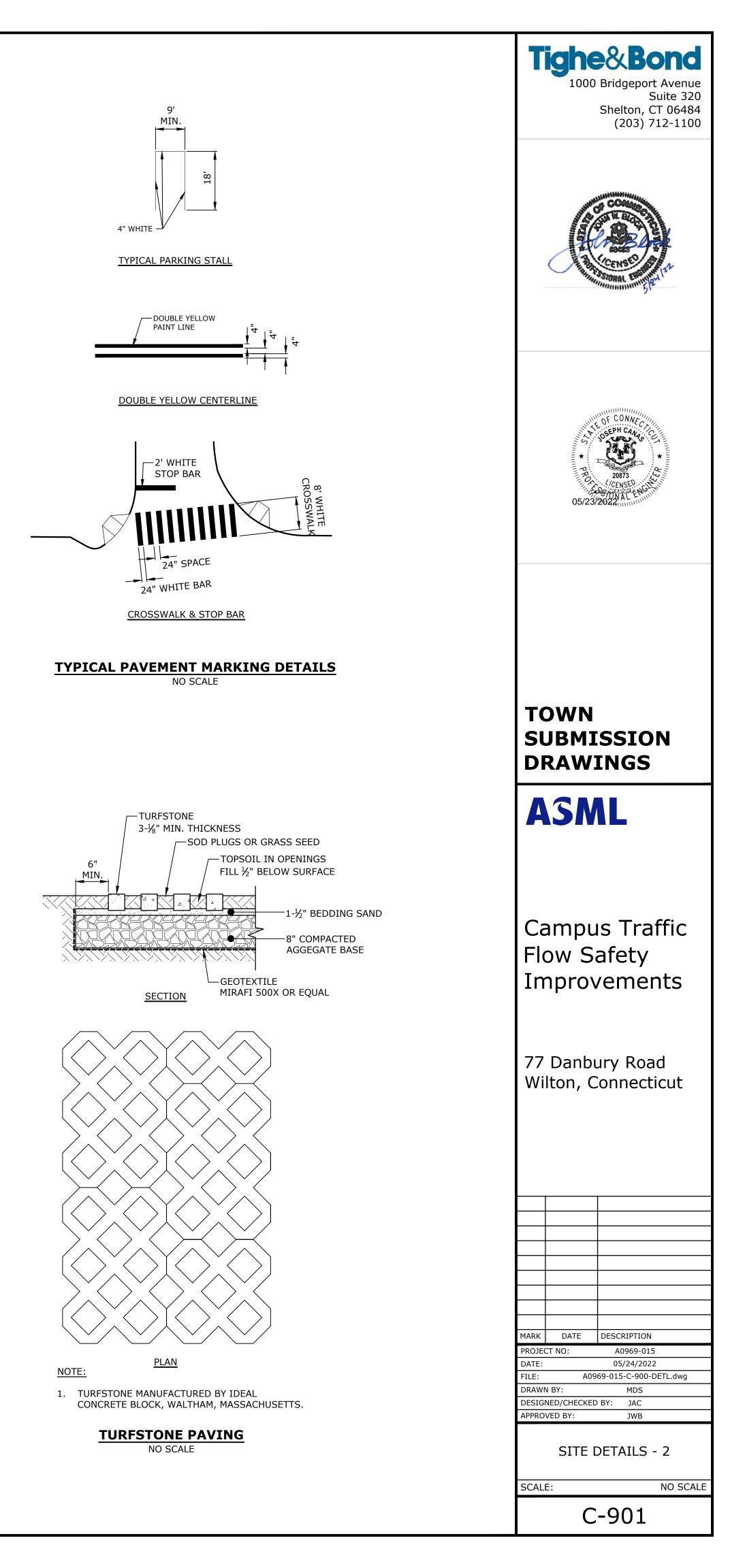


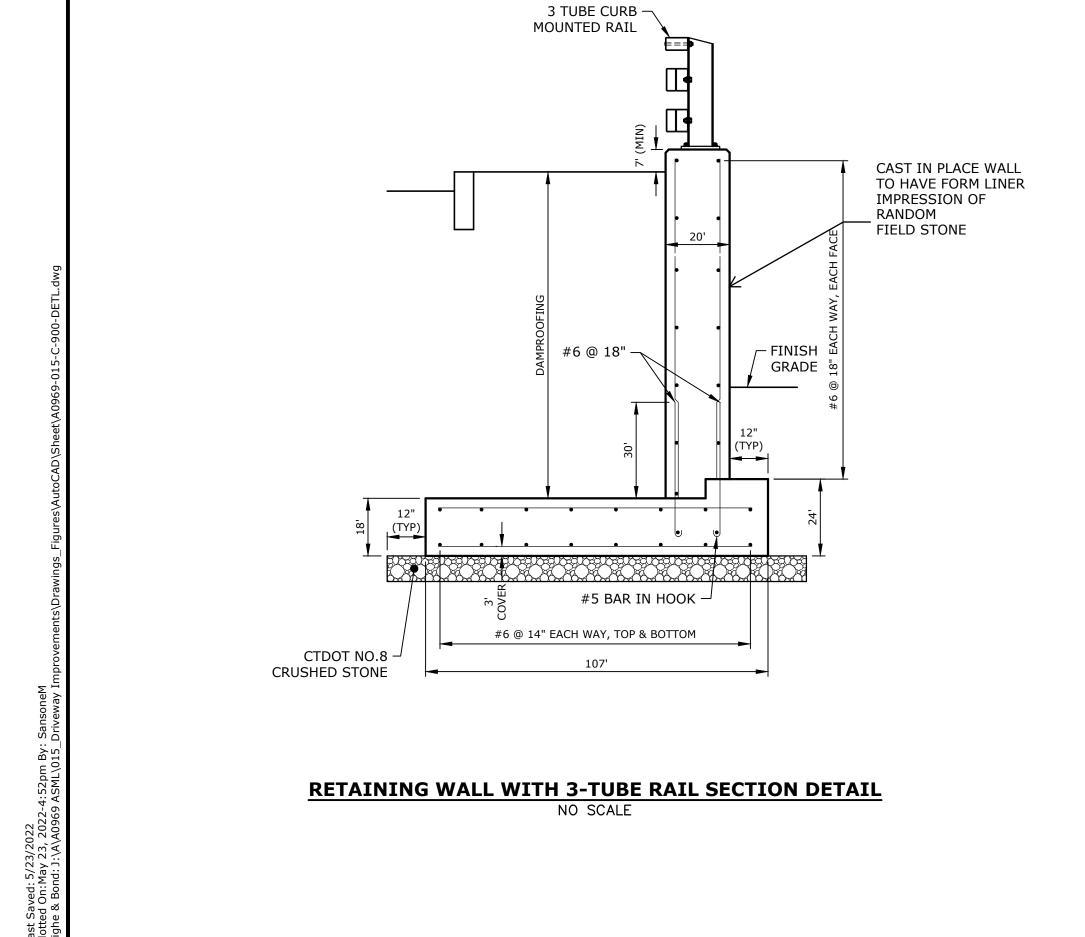


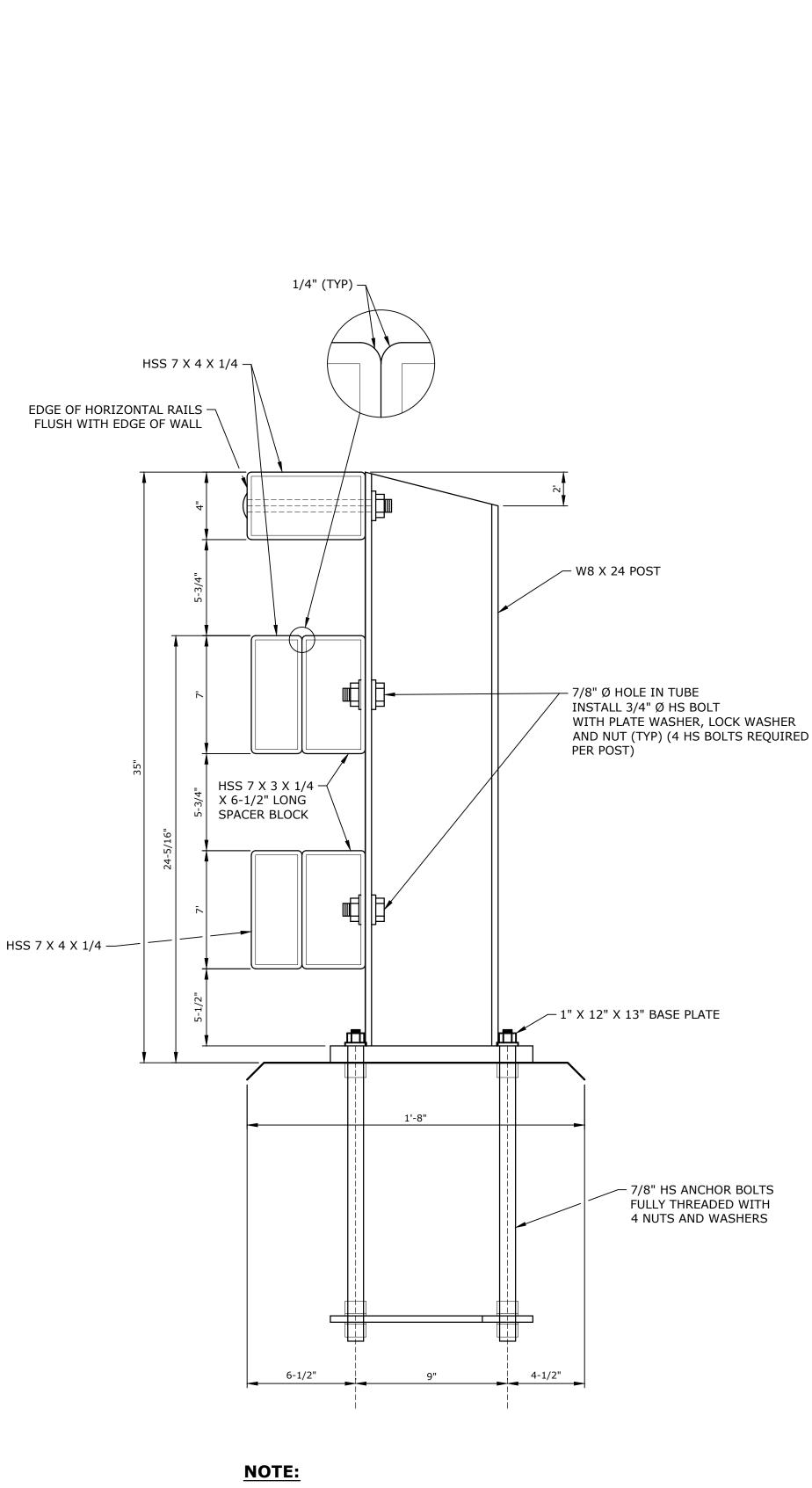
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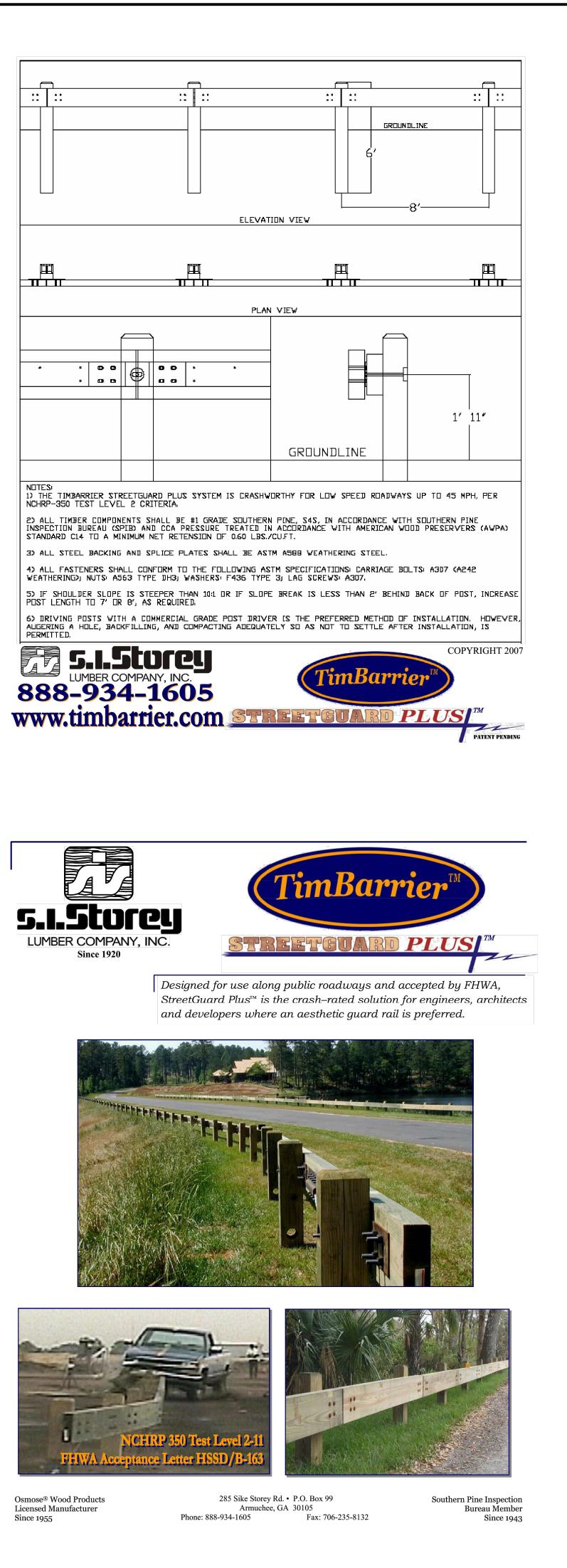






ALL EXPOSED GUIDERAIL ELEMENTS TO BE POWDER COATED, FEDERAL STANDARD 17038, MATTE BLACK.

**3-TUBE - CURB MOUNTED RAIL SECTION** NO SCALE

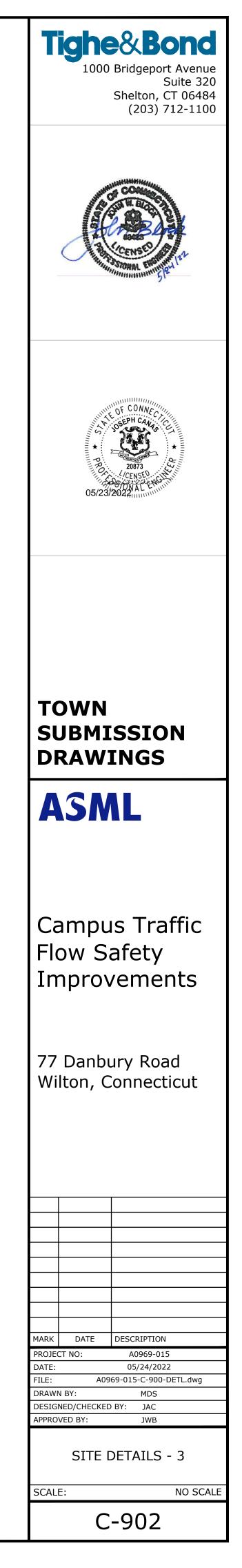




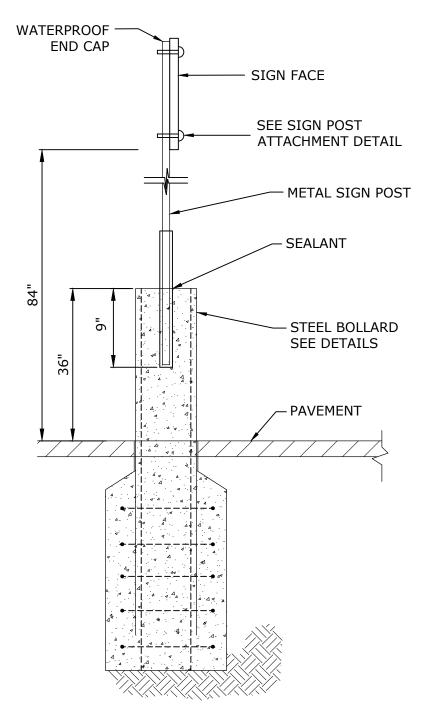




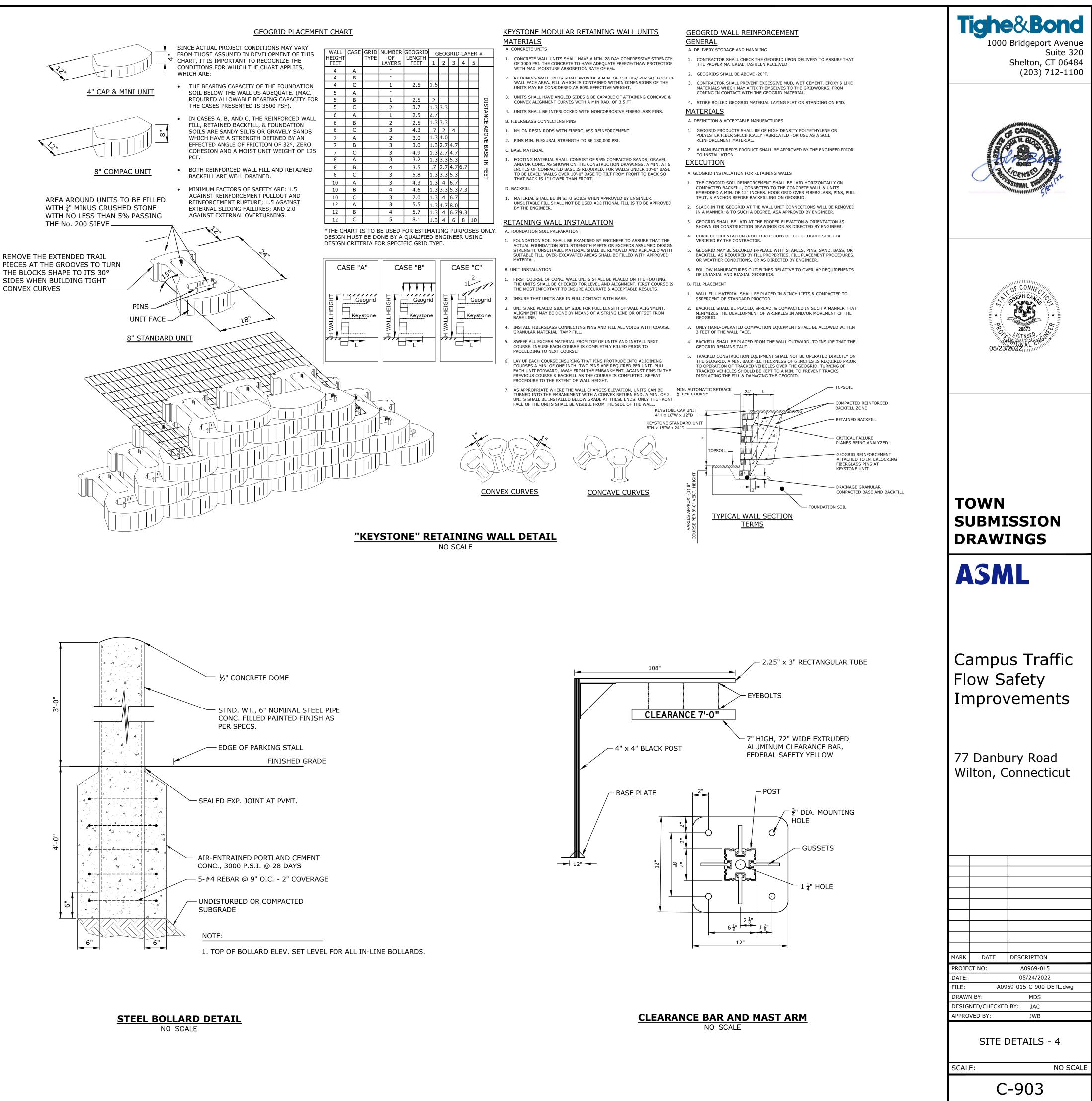
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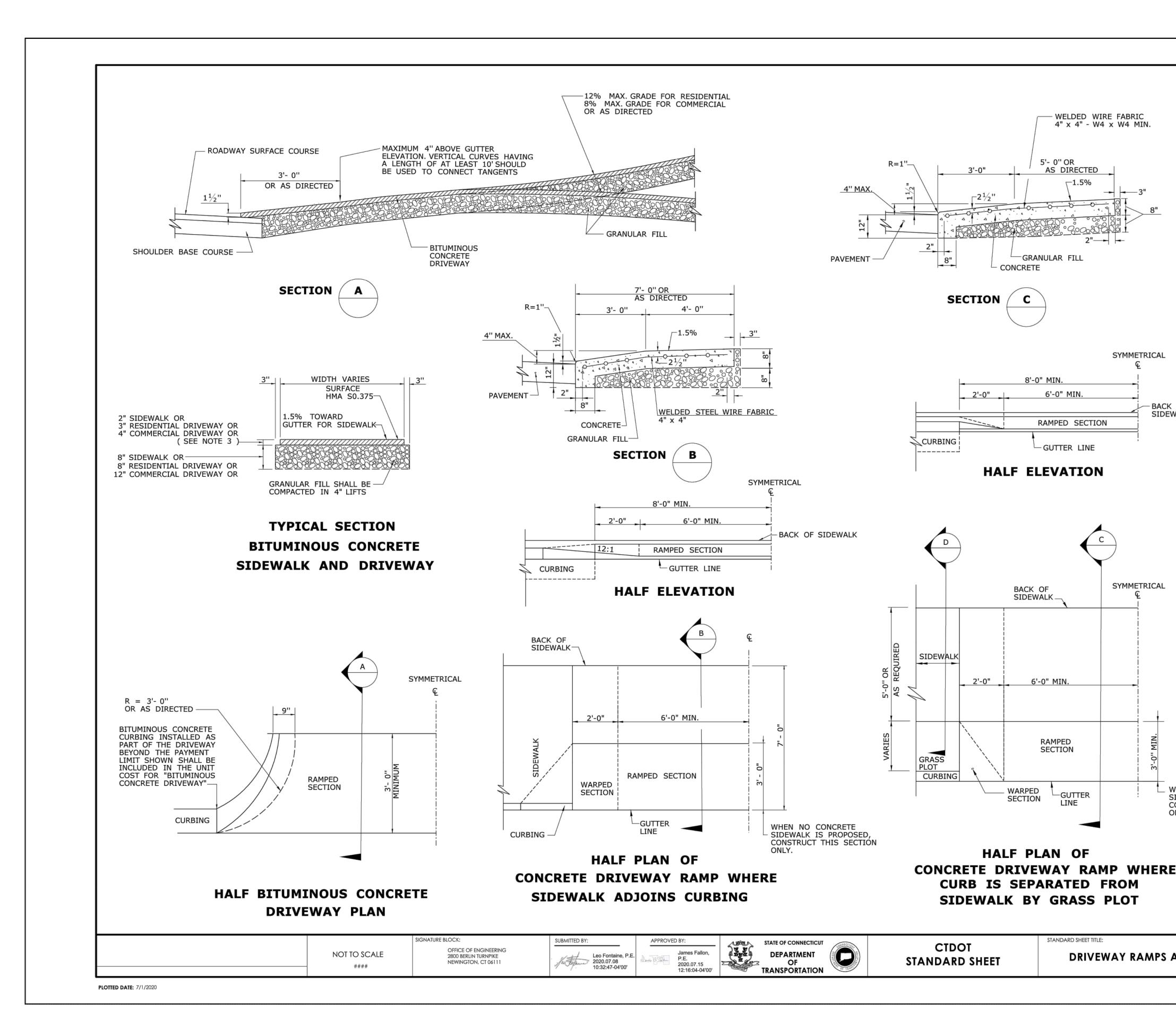


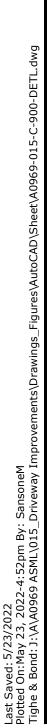




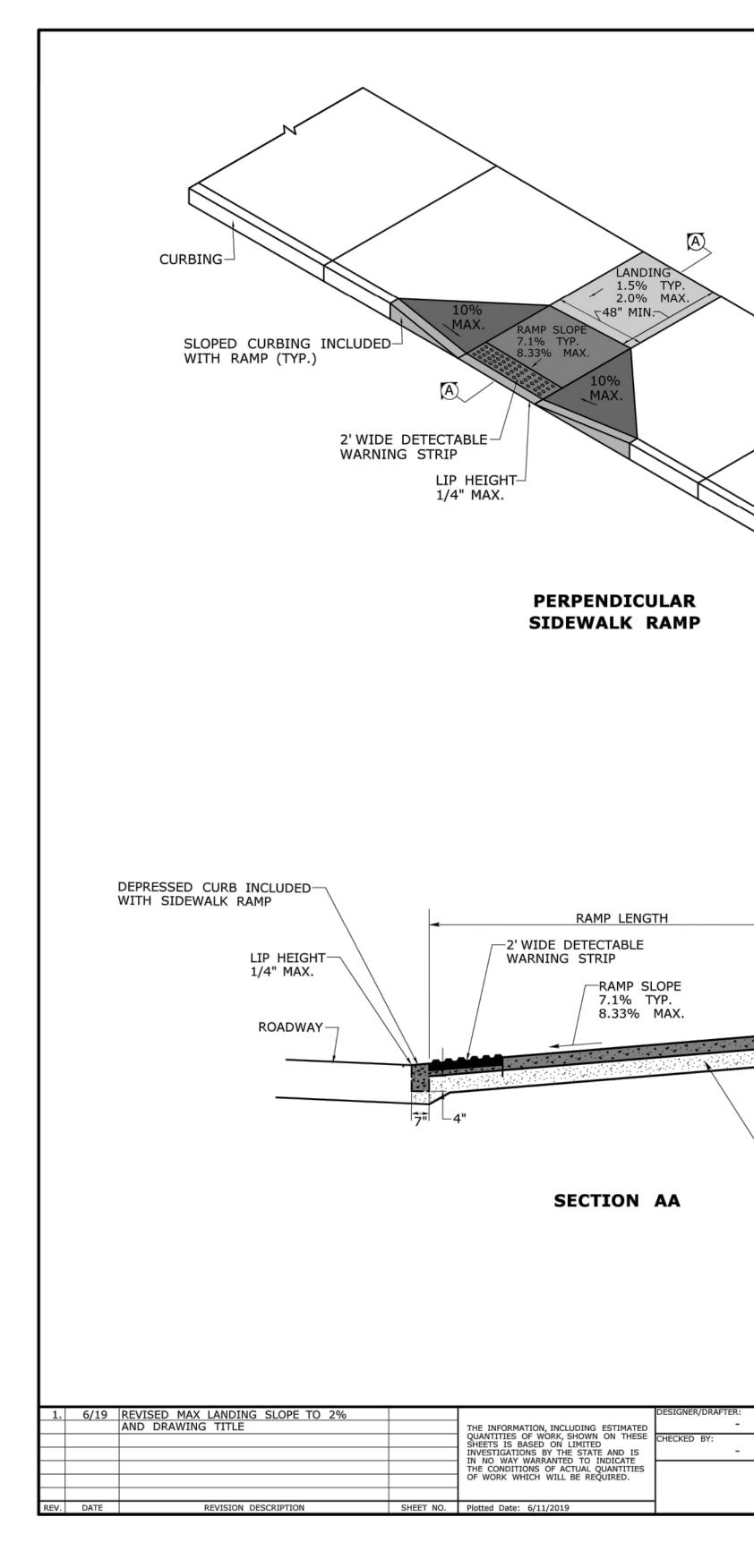
### **BOLLARD SIGN MOUNTING DETAIL** NO SCALE



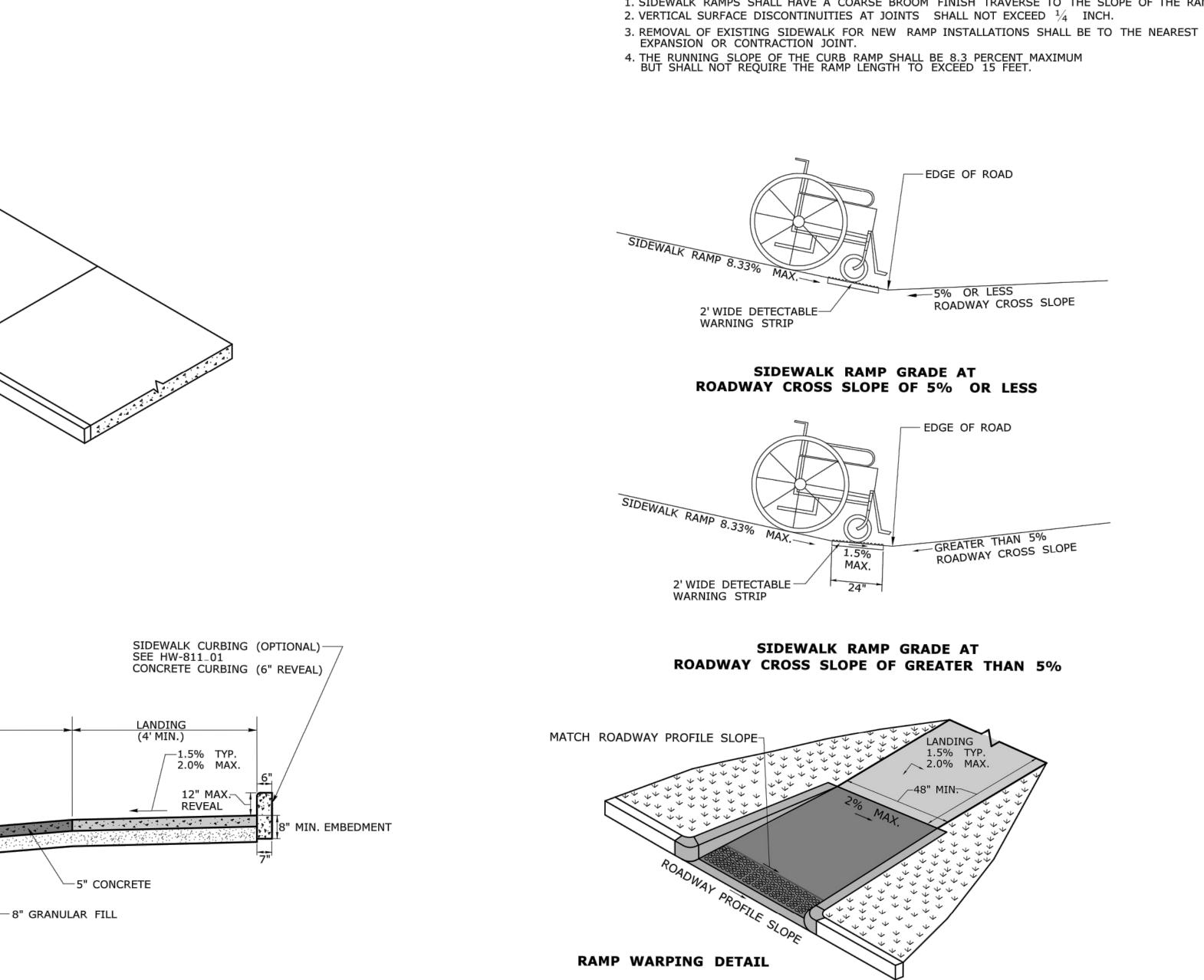




		Tighe&Bond 1000 Bridgeport Avenue Suite 320 Shelton, CT 06484 (203) 712-1100
<ul> <li><b>GENERAL NOTES:</b></li> <li>1. DRIVEWAY ENTRANCE SHALL BE A MINIMUM OF 1: WIDE, EXCLUDING CURBING WHEN PRESENT.</li> <li>2. WELDED WIRE FABRIC MATS WITH REINFORCING SPACING MAY BE USED.</li> <li>3. SURFACE HMA \$0.375 TO BE PLACED IN TWO EQ FOR BOTH RESIDENTIAL AND COMMERCIAL DRIVEN</li> </ul>	AT CLOSER	R COMPANY COMPANY R COMPANY R DOG R COMPANY R
CONCRETE SURFACE SHALL BE FINISHED WITH WOOD FLOAT OR BY OTH APPROVED MEANS 5'-0" OR AS REQUIRED	H A IER	visiting of CONNECCION seph can be connected at the conne
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5' WIDE CONCRET SIDEWALK WITH GRAS		ASML
		Campus Traffic Flow Safety Improvements 77 Danbury Road Wilton, Connecticut
VHEN NO CONCRETE SIDEWALK IS PROPOSED, CONSTRUCT THIS SECTION DNLY.		
Ξ		
AND SIDEWALKS	STANDARD SHEET NO.: HW-921_01	MARK DATE DESCRIPTION PROJECT NO: A0969-015 DATE
		DATE:05/24/2022FILE:A0969-015-C-900-DETL.dwgDRAWN BY:MDSDESIGNED/CHECKED BY:JACADDROV/CD_DY:JWD
		APPROVED BY: JWB SITE DETAILS - 5
		SCALE: NO SCALE



3/25 23, ·\A\, : 5/23 May 2



1. TRANSITION SIDEWALK RAMP TO MATCH ROADWAY PROFILE AS GRADUALLY AS POSSIBLE. DO NOT EXCEED 3 % PER FOOT CROSS SLOPE RATE OF CHANGE WHEN TRANSITIONING TO ROADWAY PROFILE.

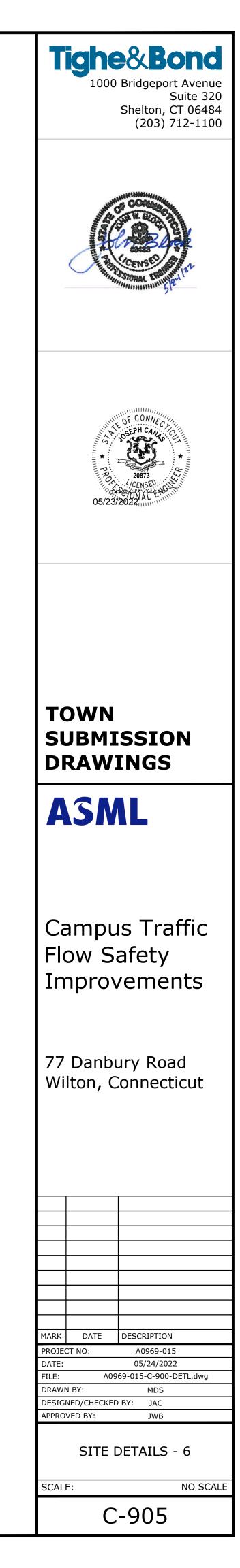
**GENERAL NOTES:** 

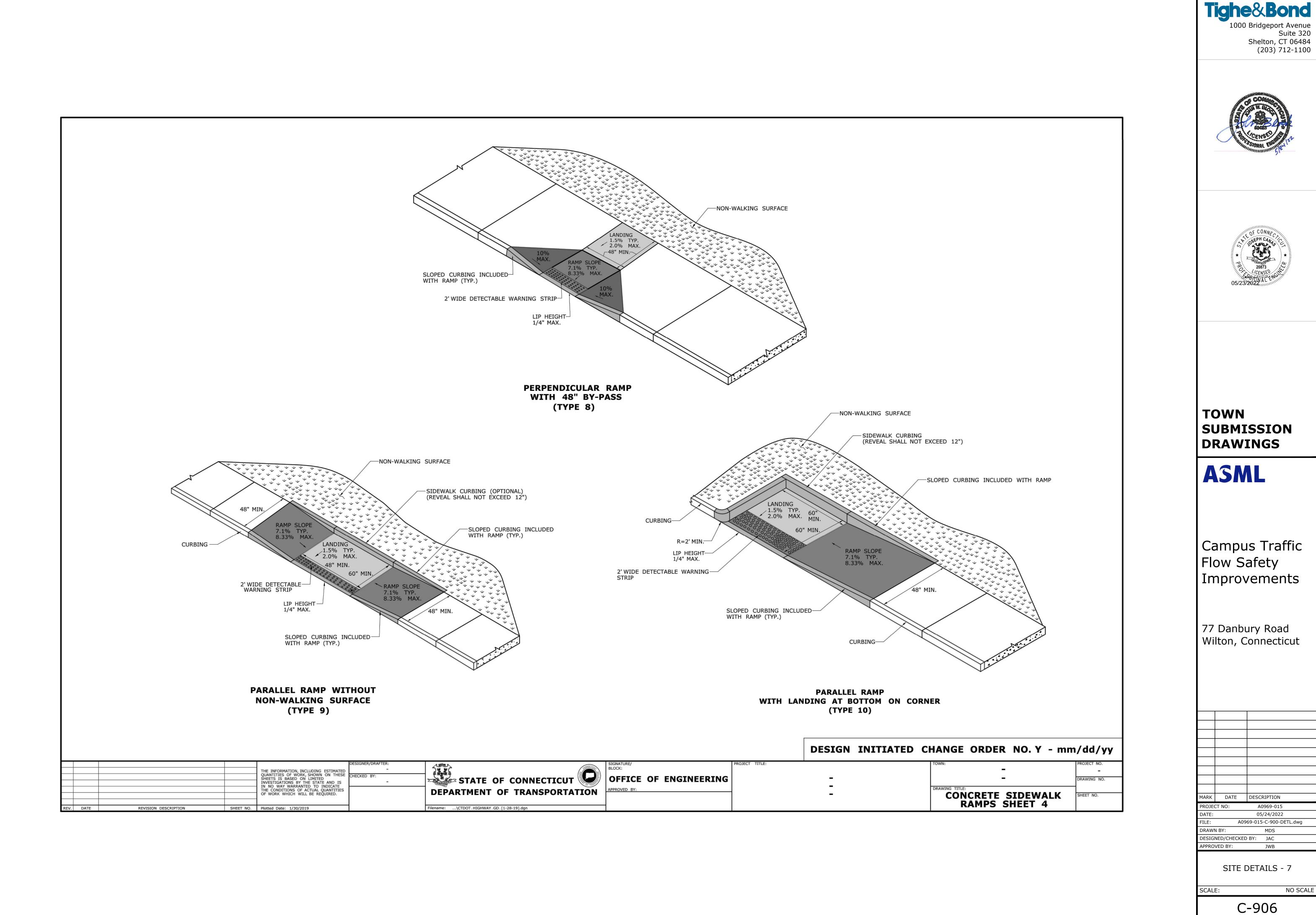
COMPLETE TRANSITION TO ROADWAY PROFILE BEHIND DETECTABLE WARNING SURFACE.

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	Filename:\CTDOT_HIGHWAY_GD [5-30-19].dgn			RAMPS SHEET 1	

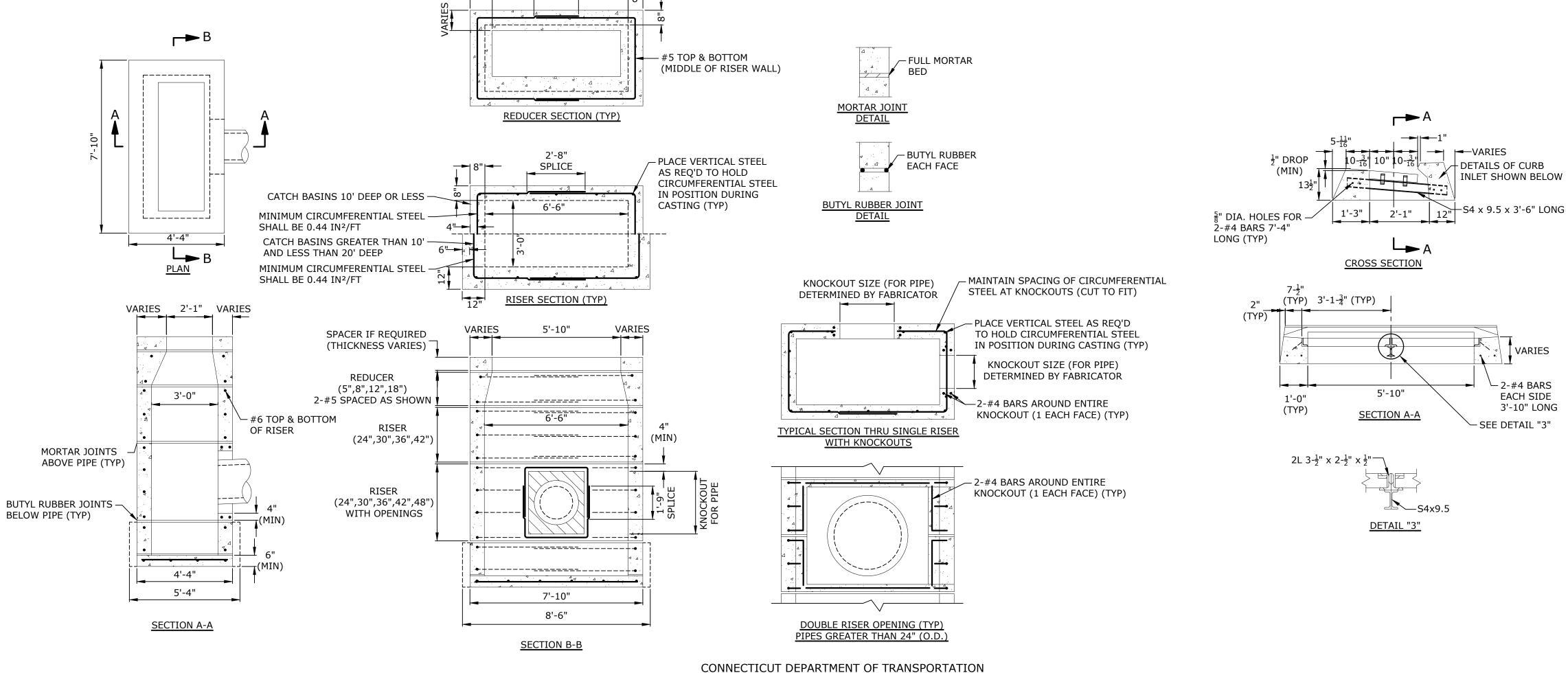
1. SIDEWALK RAMPS SHALL HAVE A COARSE BROOM FINISH TRAVERSE TO THE SLOPE OF THE RAMP.

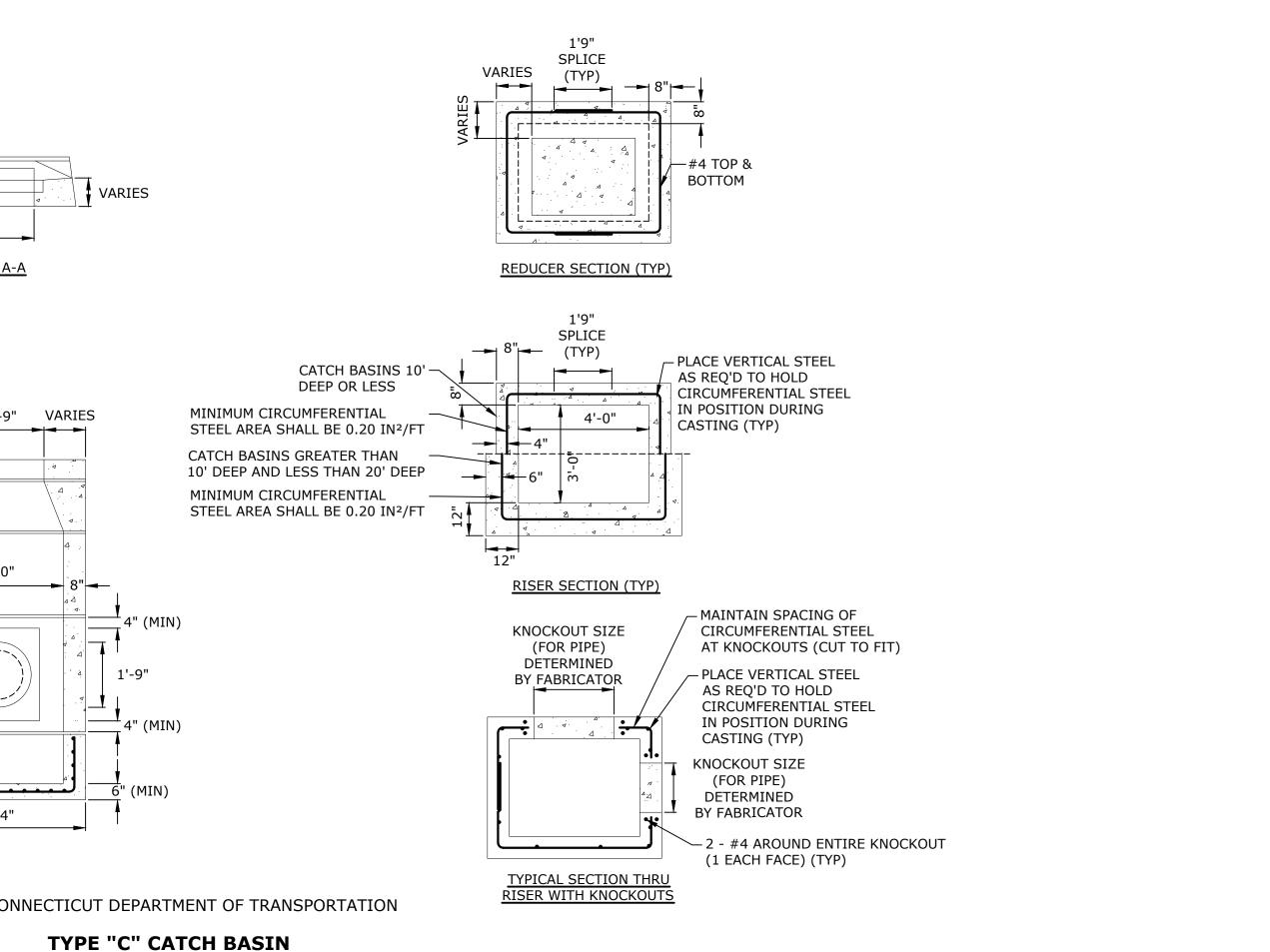




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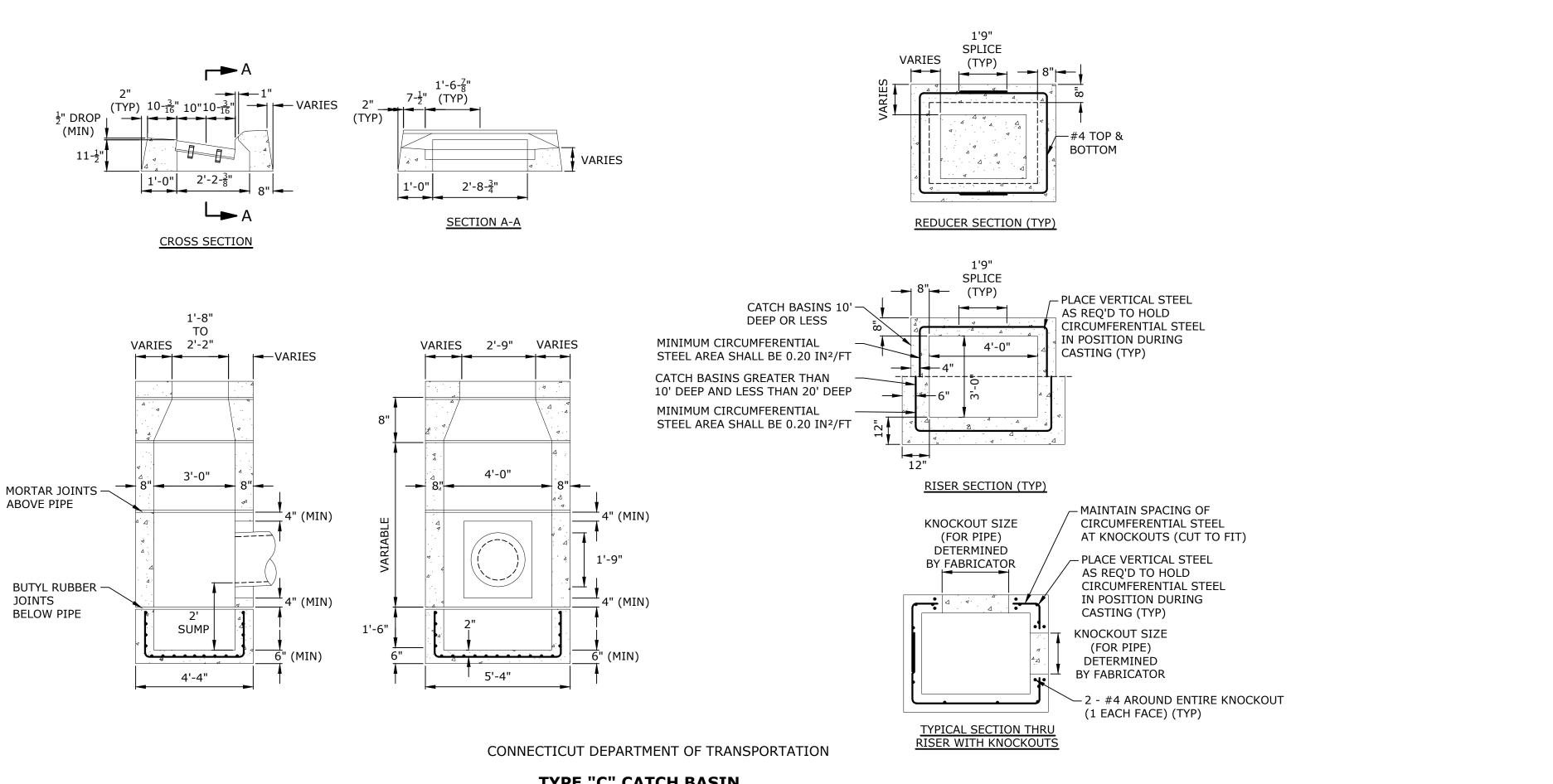






NO SCALE

VARIES





2'-0"

SPLICE

\_\_\_\_0"\_\_\_

1. REINFORCEMENT SHALL CONFORM TO ASTM A615, GRADE 60.

NOTES:

SUBSTITUTED.

BRIDGES.

REVIEW.

HERE.

2. DETAILS ON THIS SHEET SHOW STANDARD REINFORCEMENT. WELDED WIRE FABRIC WITH AN AREA EQUAL TO OR GREATER THAN THE REINFORCING SHOWN MAY BE

3. ALL LAP SPLICES, DEVELOPMENT LENGTHS, BENDS FOR REINFORCEMENT, AND WELDED WIRE FABRIC SHALL CONFORM TO AASHTO STANDARD SPECIFICATIONS FOR HIGHWAY

4. ALL REINFORCEMENT SHALL HAVE A MINIMUM CLEAR COVER OF 2", EXCEPT FOR BENEATH BOTTOM REINFORCEMENT IN TOP SLABS, WHERE THE MINIMUM MAY BE  $1\frac{1}{2}$ " 5. MINIMUM CONCRETE COMPRESSIVE STRENGTH FC'=4,000PSI SHALL BE OBTAINED BEFORE SHIPPING.

6. BASES AND RISERS AT A DEPTH OF 20' AND GREATER SHALL BE DESIGNED BY THE CONTRACTOR AND WORKING DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER FOR

7. SEE STANDARD DRAWING 507-K FOR CATCH BASIN FRAMES AND GRATES.

8. FOR DOT MAINTENANCE PERSONNEL, RISERS MAY BE PREFABRICATED WITH PIPE OPENINGS IN ALL FOUR WALLS. ADEQUATE REINFORCING AROUND PIPE OPENINGS TO CONFORMING TO THESE PLANS SHALL BE PROVIDED. ANY RISERS USED WHERE A PIPE OPENING IS TO REMAIN IN PLACE MUST BE FORMED UP WITH BRICK AS DIRECTED BY THE ENGINEER.

9. RISERS SHALL NEVER HAVE CORNER PIPE ENTRIES. WHERE THE ALIGNMENT OF THE PIPE WITH RESPECT TO THE CORNER OF THE CATCH BASIN CANNOT BE CHANGED, A ROUND STRUCTURE CONFORMING TO ASTM C478 SHALL BE USED. REINFORCING FOR THE ROUND TOP SLAB WITH A RECTANGULAR OPENING SHALL CONFORM TO DETAILS SHOWN

10. ALL PIPE OPENINGS SHALL BE CLOSED USING MATERIALS WHICH CONFORM TO STATE OF CONNECTICUT STANDARD SPECIFICATIONS SECTION M.08.02. IF THE ENGINEER DETERMINES THAT THE CLOSURE OF ANY PIPE OPENING IS UNSATISFACTORY, THE CONTRACTOR SHALL RECLOSE SAID OPENING AT NO ADDITIONAL COST TO THE STATE. KNOCKOUTS FOR PIPE OPENINGS SHALL NOT RESULT IN A REDUCED WALL THICKNESS.

11. THE LATEST STATE OF CONNECTICUT STANDARD SPECIFICATIONS AND SUPPLEMENTALS SHALL GOVERN.

12. FOR ADDITIONAL DETAILS, SEE OTHER CATCH BASIN SHEETS.

13. WALL THICKNESS OF ALL CB'S OVER 10' DEEP SHALL BE INCREASED TO 12" THICK. INSIDE DIMENSION SHALL REMAIN THE SAME. (THE 12" THICKNESS SHALL START AFTER THE FIRST 10")

14. BUTYL RUBBER JOINT SEAL SHALL CONFORM TO AASHTO M-198 AND MORTAR SHALL CONFORM TO THE LATEST STATE OF CONNECTICUT STANDARD SPECIFICATIONS MATERIAL SECTION M11.04.

15. SHRINKAGE AND TEMPERATURE REINFORCEMENT SHALL BE PROVIDED IN THE TOPS OF SLABS. THE TOTAL AREA OF REINFORCEMENT PROVIDED SHALL BE AT LEAST 0.125 IN<sup>2</sup>/FT IN EACH DIRECTION. THE MAXIMUM SPACING OF THIS REINFORCEMENT SHALL NOT EXCEED 18 INCHES.

16. THE DETAILS SHOWN IN THE PLAN VIEW FOR THE PRECAST CONCRETE ROUND STRUCTURES SHALL ALSO BE USED FOR CONVERTING MANHOLES TO CATCH BASINS.

	Q			VARIES
		\		#4 BARS
5'-	10"		EA	ACH SIDE
ECTIC	DN A-A		_	-10" LONG
			– SEE DI	ETAIL "3"







# TOWN **SUBMISSION** DRAWINGS

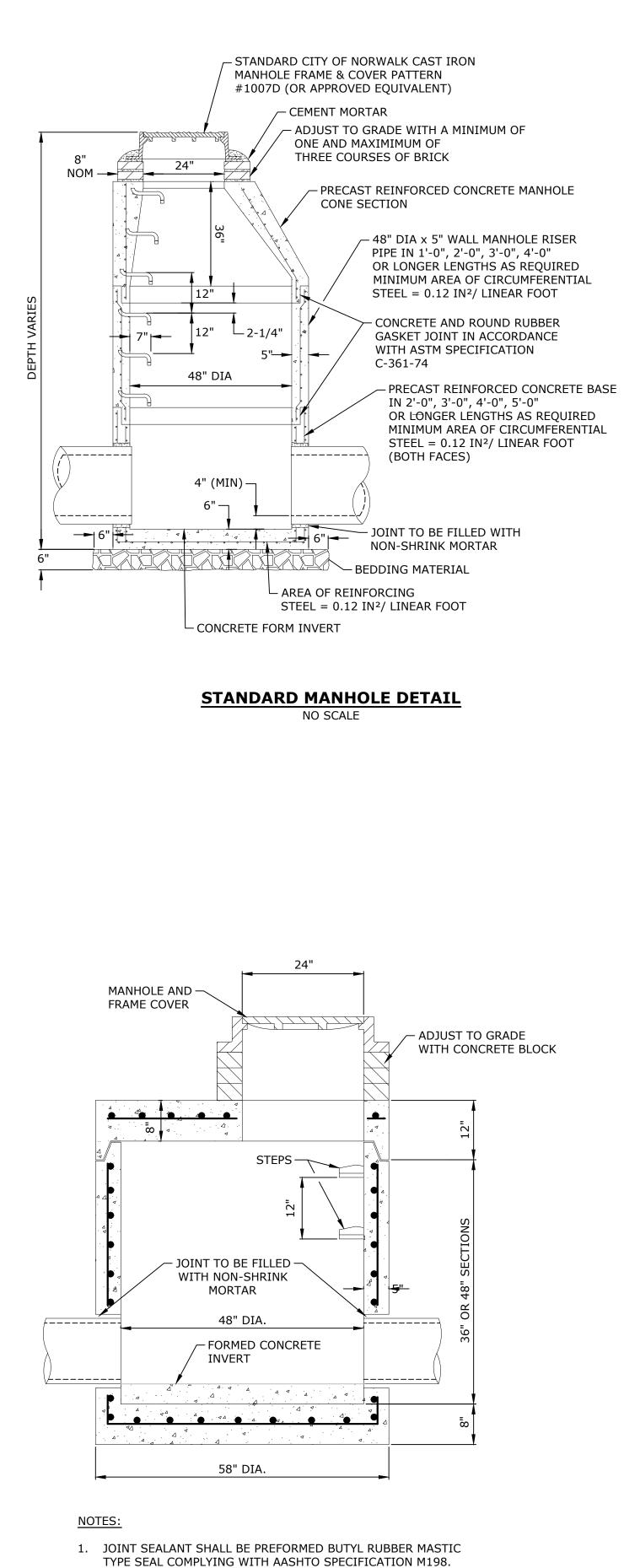


# Campus Traffic Flow Safety Improvements

77 Danbury Road Wilton, Connecticut

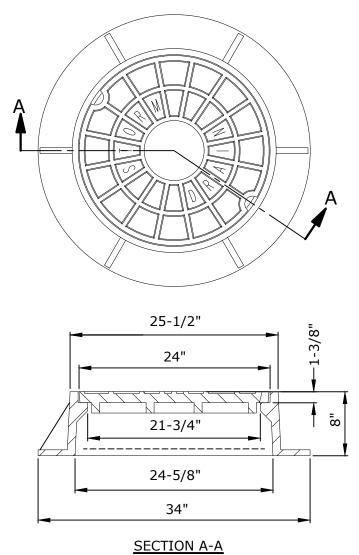
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- 2. REINFORCING 0.12 IN<sup>2</sup>/VERTICAL FOOT PER ASTM A185.
- 3. CONCRETE COMPRESSIVE STRENGTH: 5,000 PSI, 28 DAYS
- 4. BASE SECTION IS MONOLITHIC.

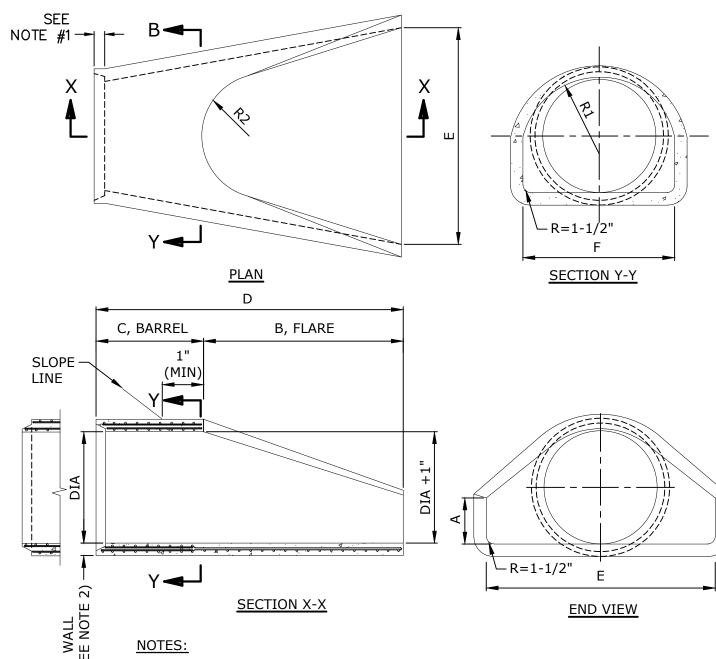
SHALLOW MANHOLE NO SCALE



NOTE:

MANHOLE FRAMES & COVERS SHALL BE PATTERN #1007D AS MANUFACTURED BY THE CAMPBELL FOUNDRY COMPANY OF NORTH HAVEN, CONNECTICUT, OR APPROVED EQUAL.

### MANHOLE FRAME AND COVER NO SCALE

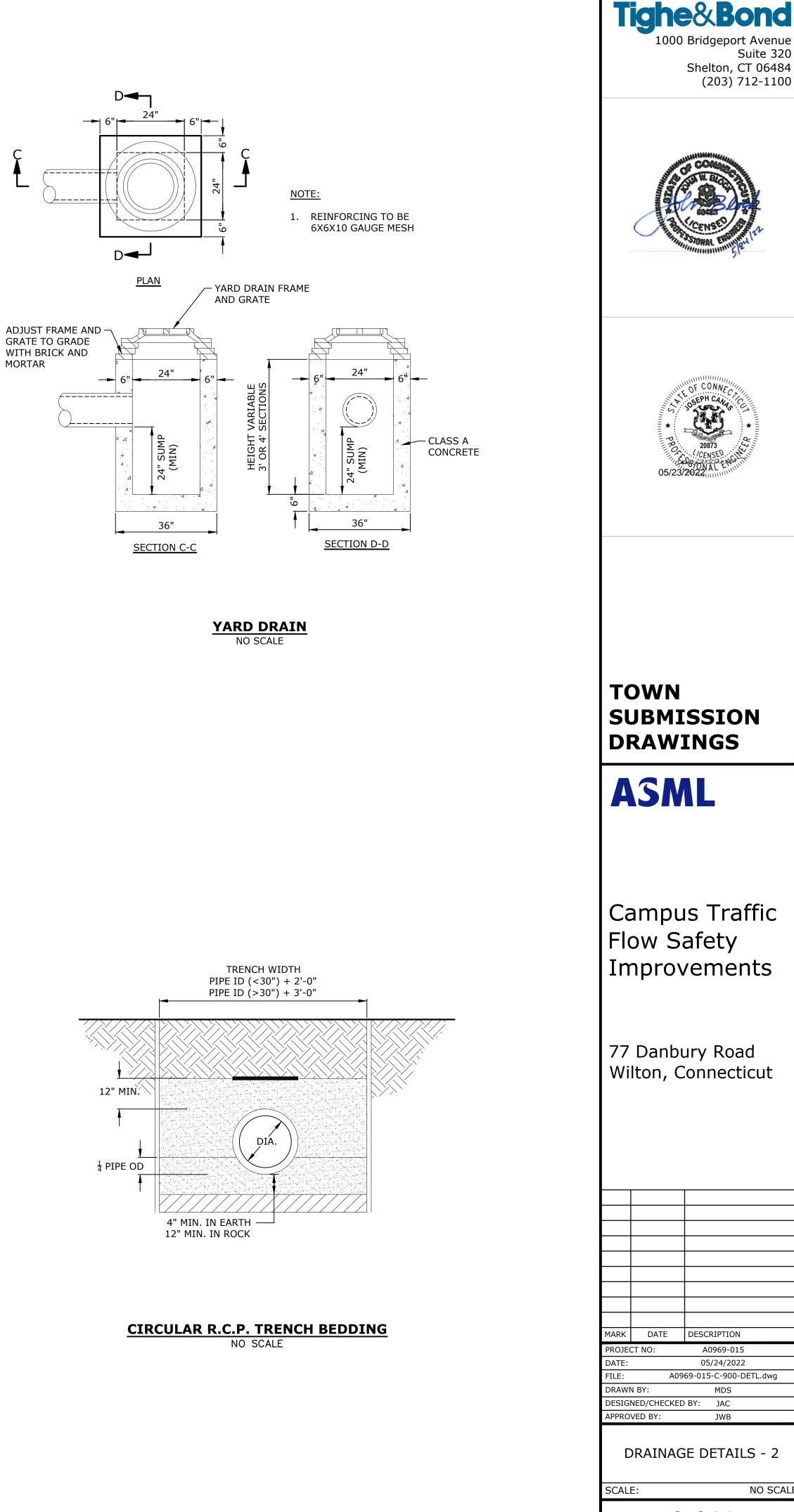


JOINTS SHALL BE TONGUE AND GROOVE OR BELL AND SPIGOT AS REQUIRED TO CONFORM TO PIPE INSTALLED.

2. WALL THICKNESS SHALL CONFORM TO PIPE THICKNESS.

DIMENSIONS FOR REINFORCED CONCRETE CULVERT END							REINFO	LARE DRCEMENT IN CENTER OF WALL		
DIA.	А	В	С	D	Е	F	$R_1$	R <sub>2</sub>	MIN. AREA OF LONGITUDINALS SQ. IN PER FT.	MIN. AREA OF TRANSVERSE STEEL SQ. IN PER FT.
12"	4"	2'-0"	4'-0 <sup>3</sup> "	6'-0 <sup>3</sup> "	2'-0"	1'-7 <sup>15</sup> "	10 <del>1</del> "	9"	0.048	0.048
15"	6"	2'-3"	3'-10"	6'-1"	2'-6"	2'-0 <sup>5</sup>	$1' - 0\frac{1}{2}''$	11"	0.054	0.054
18"	9"	2'-3"	3'-10"	6'-1"	3'-0"	2'-5"	$1' - 3\frac{1}{2}''$	1'-0"	0.060	0.060
21"	9"	2'-11"	3'-2"	6'-1"	3'-6"	2'-7 <sup>1</sup> / <sub>2</sub> "	1'-4"	1'-1"	0.066	0.066
24"	9 <del>1</del> "	3'-7 <sup>1</sup> /2"	2'-6"	$6' - 1\frac{1}{2}''$	4'-0"	2'-9 <sup>3</sup>	$1' - 4\frac{3}{16}''$	1'-2"	0.072	0.072
30"	1'-0"	4'-6"	$1' - 7\frac{3}{4}"$	6'-1 <u>3</u> "	5'-0"	3'-1"	$1'-6\frac{1}{2}"$	1'-3"	0.084	0.084
36"	1'-3"	5'-3"	$2' - 10\frac{3}{4}''$	8'-1 <sup>3</sup>	6'-0"	3'-11 <sup>13</sup> "	2'-0 <sup>5</sup> 16"	1'-8"	0.096	0.096
42"	1'-9"	5'-3"	2'-11"	8'-2"	6'-6"	4'-5 <sup>z</sup> "	2'-3 <sup>1</sup> / <sub>2</sub> "	1'-10"	0.108	0.108
48"	2'-0"	6'-0"	2'-2"	8'-2"	7'-0"	4'-8 <sup>1</sup> / <sub>2</sub> "	2'-4 <sup>1</sup> / <sub>2</sub> "	1'-10"	0.120	0.120
54"	2'-3"	5'-5"	2'-11"	8'-4"	7'-6"	5'-5 <sup>1</sup> / <sub>2</sub> "	2-9 <u>1</u> "	2'-0"	0.132	0.132
60"	2'-9"	5'-0"	3'-3"	8'-3"	8'-0"	6'-0 <sup>1</sup> / <sub>2</sub> "	3'-0 <sup>11</sup> "	2'-0"	0.144	0.144

**REINFORCED CONCRETE CULVERT END** NO SCALE



MORTAR

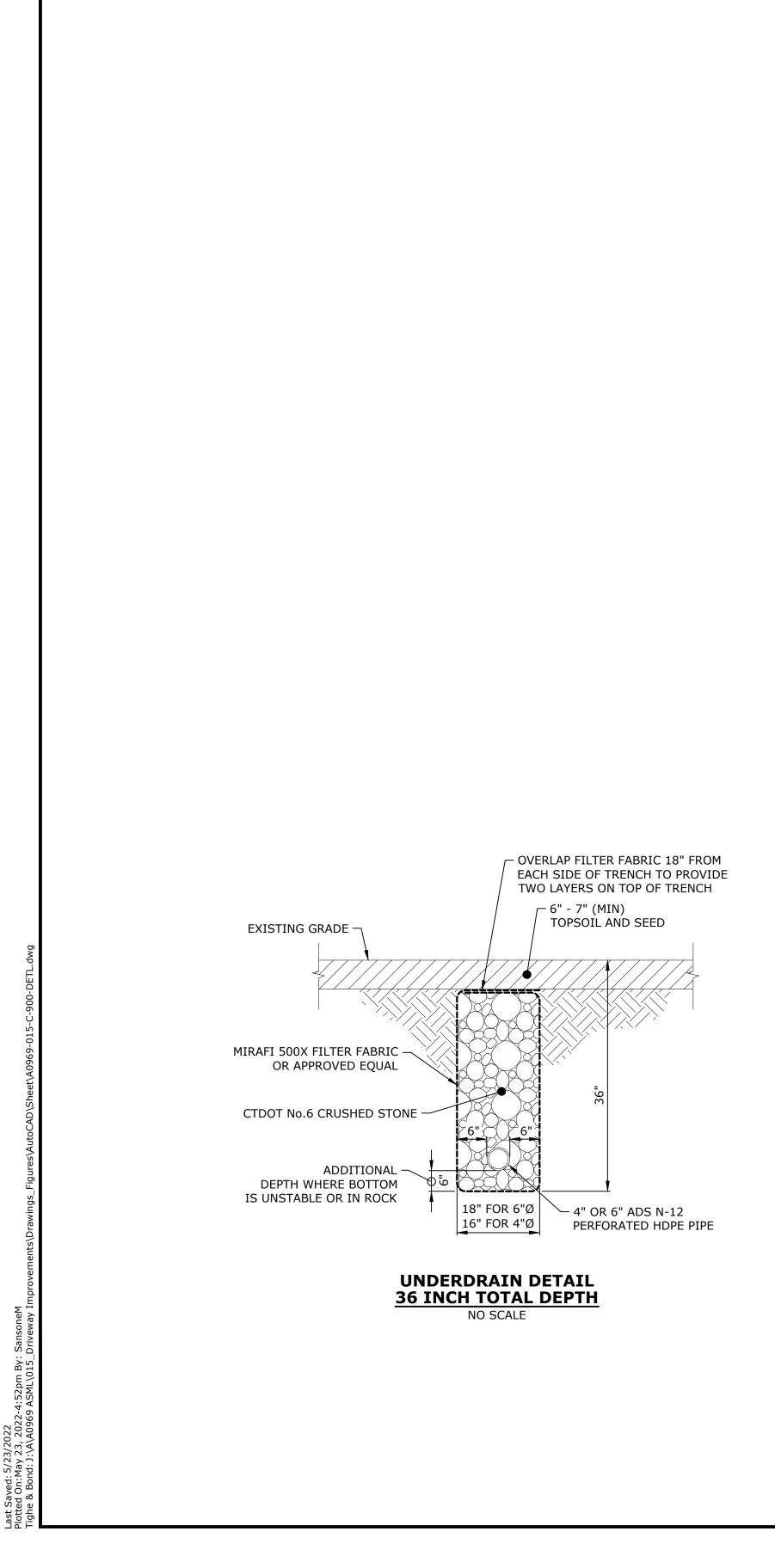
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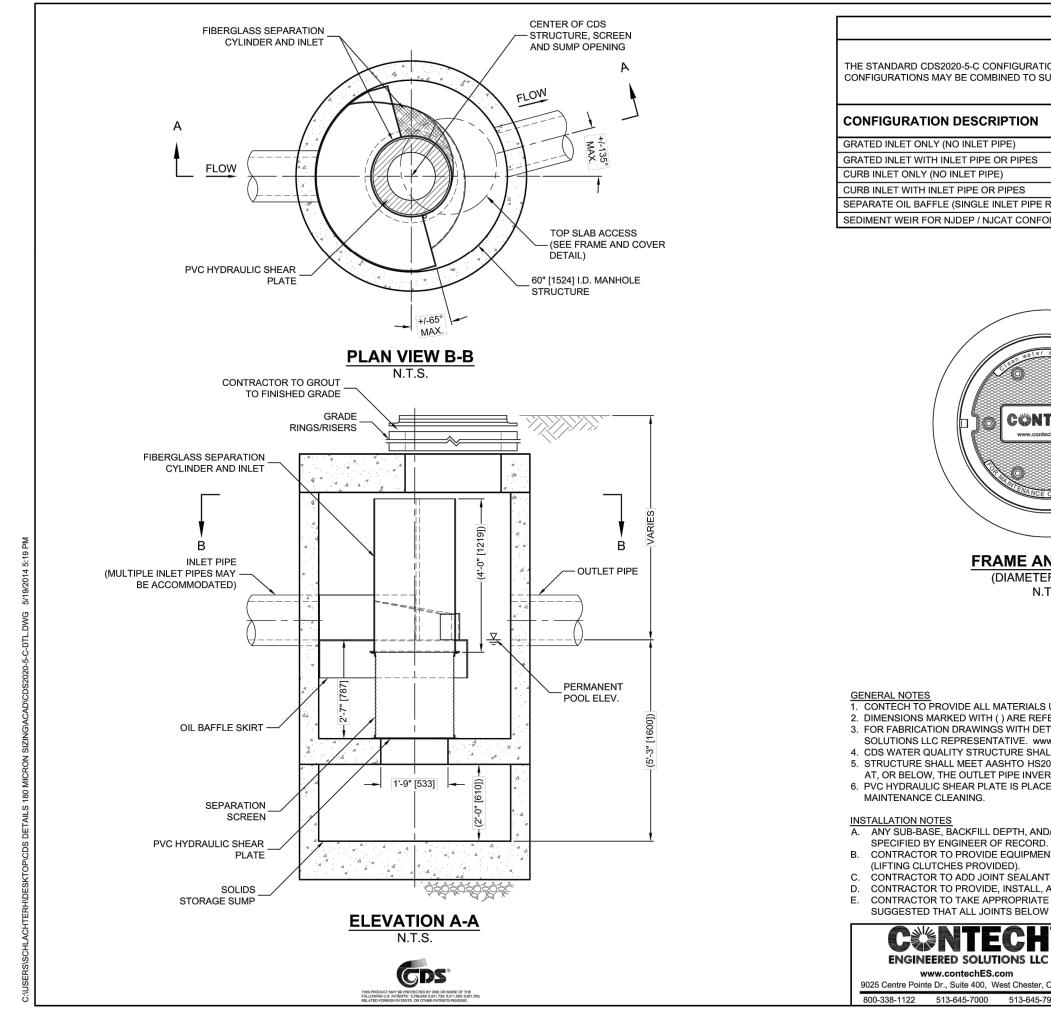
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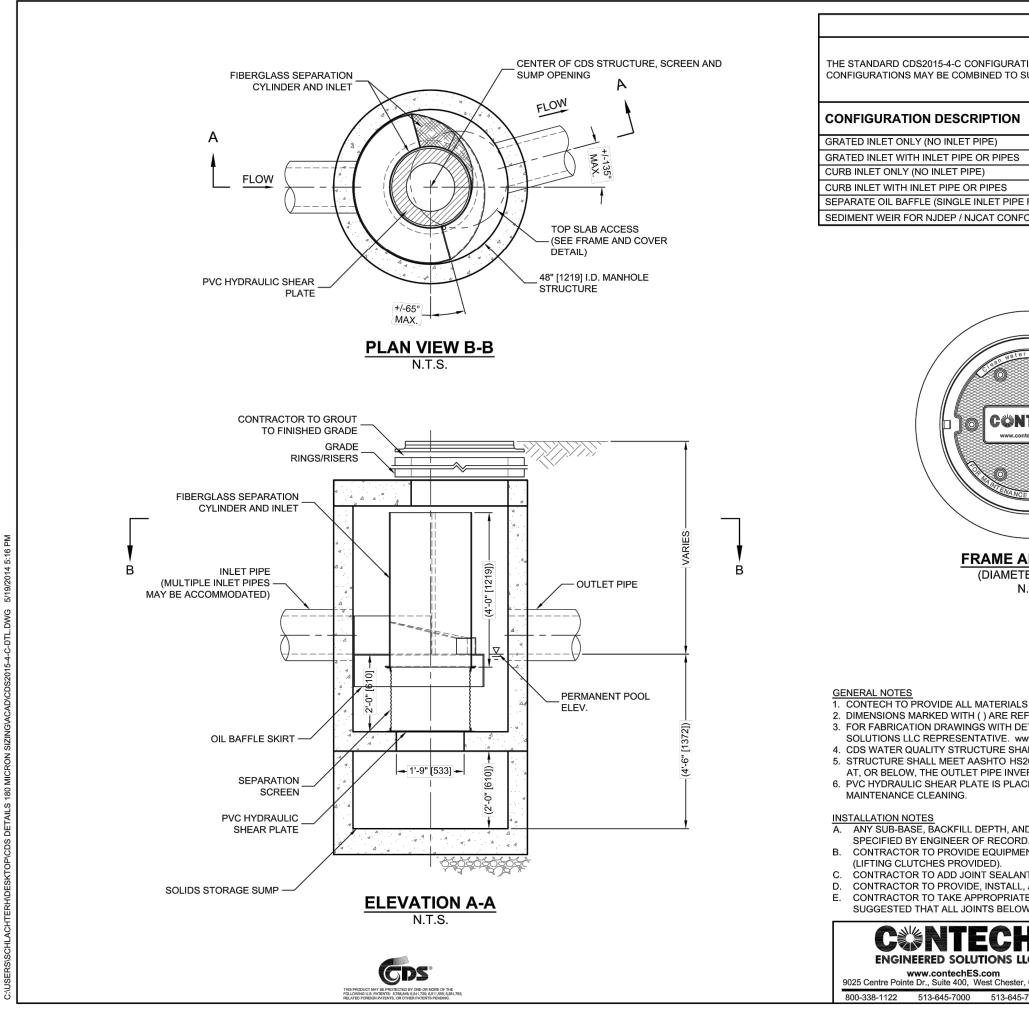
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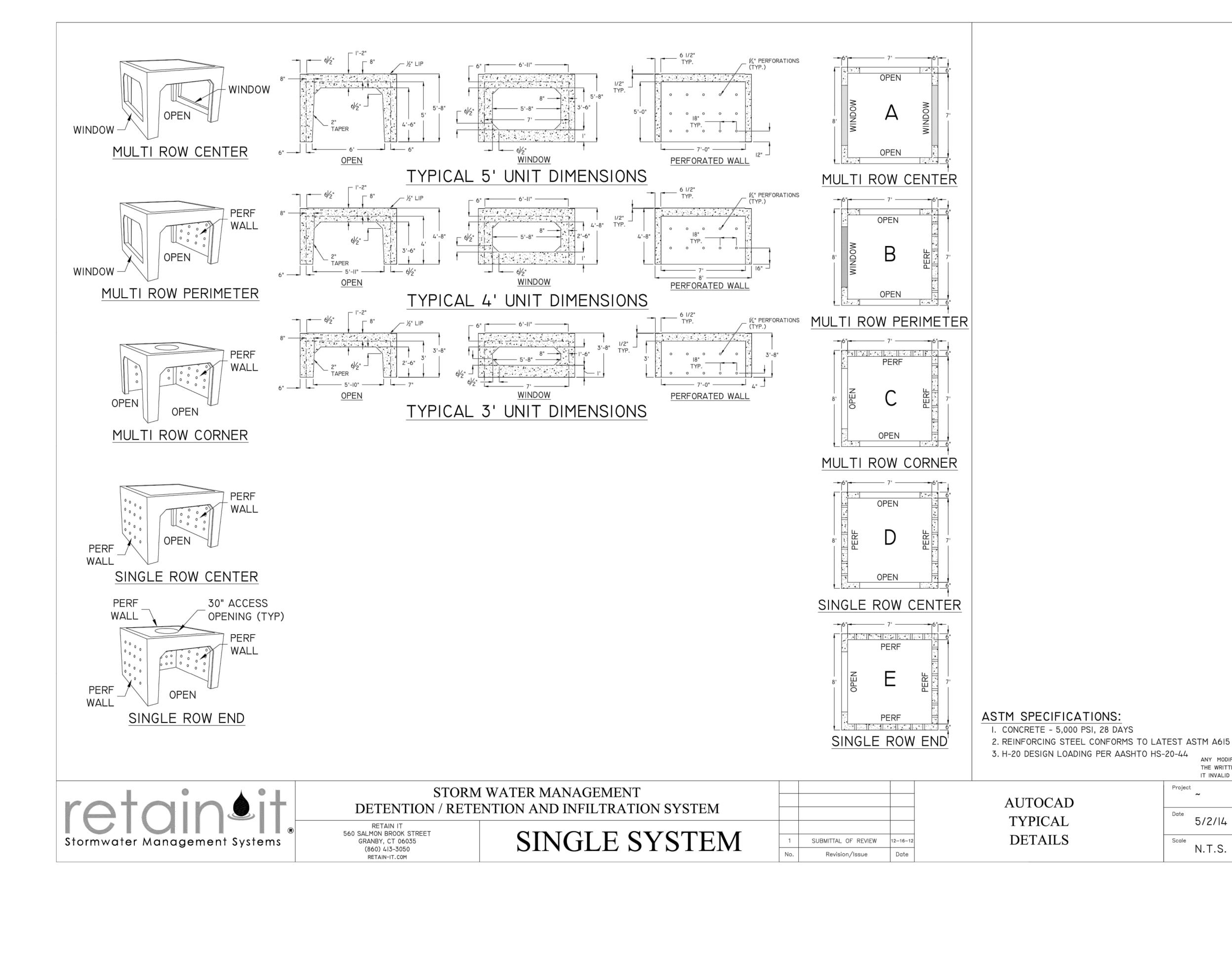
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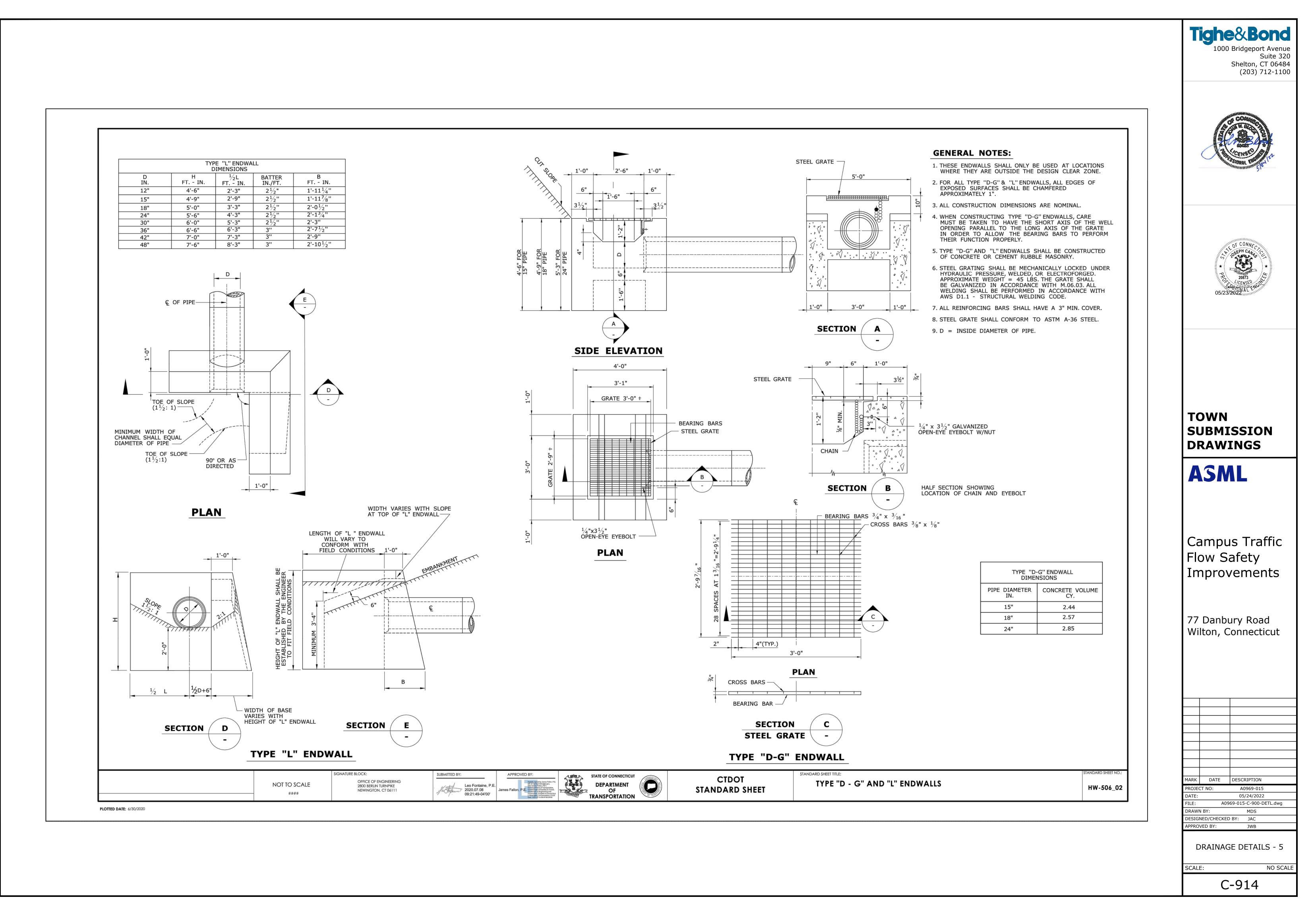
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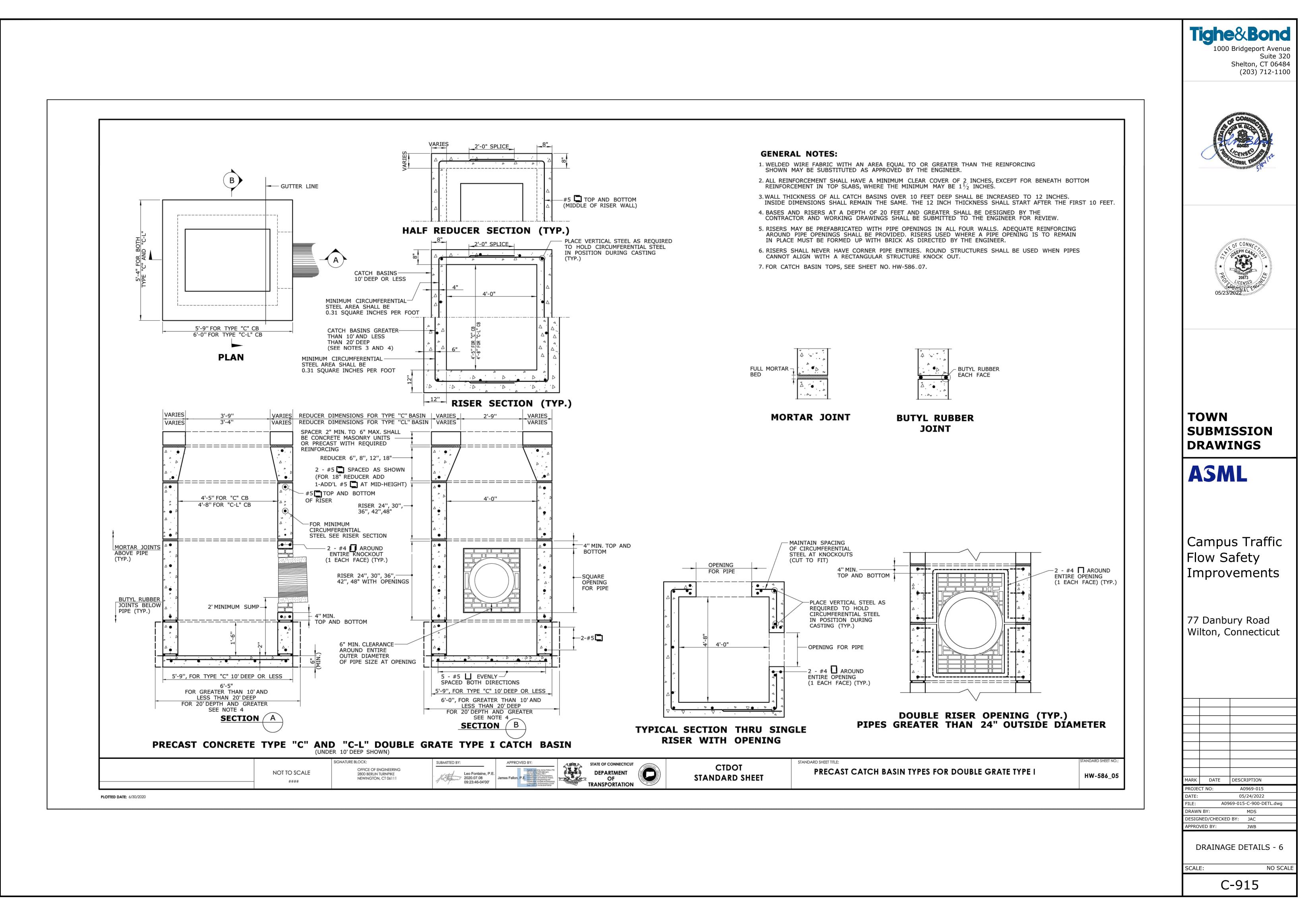
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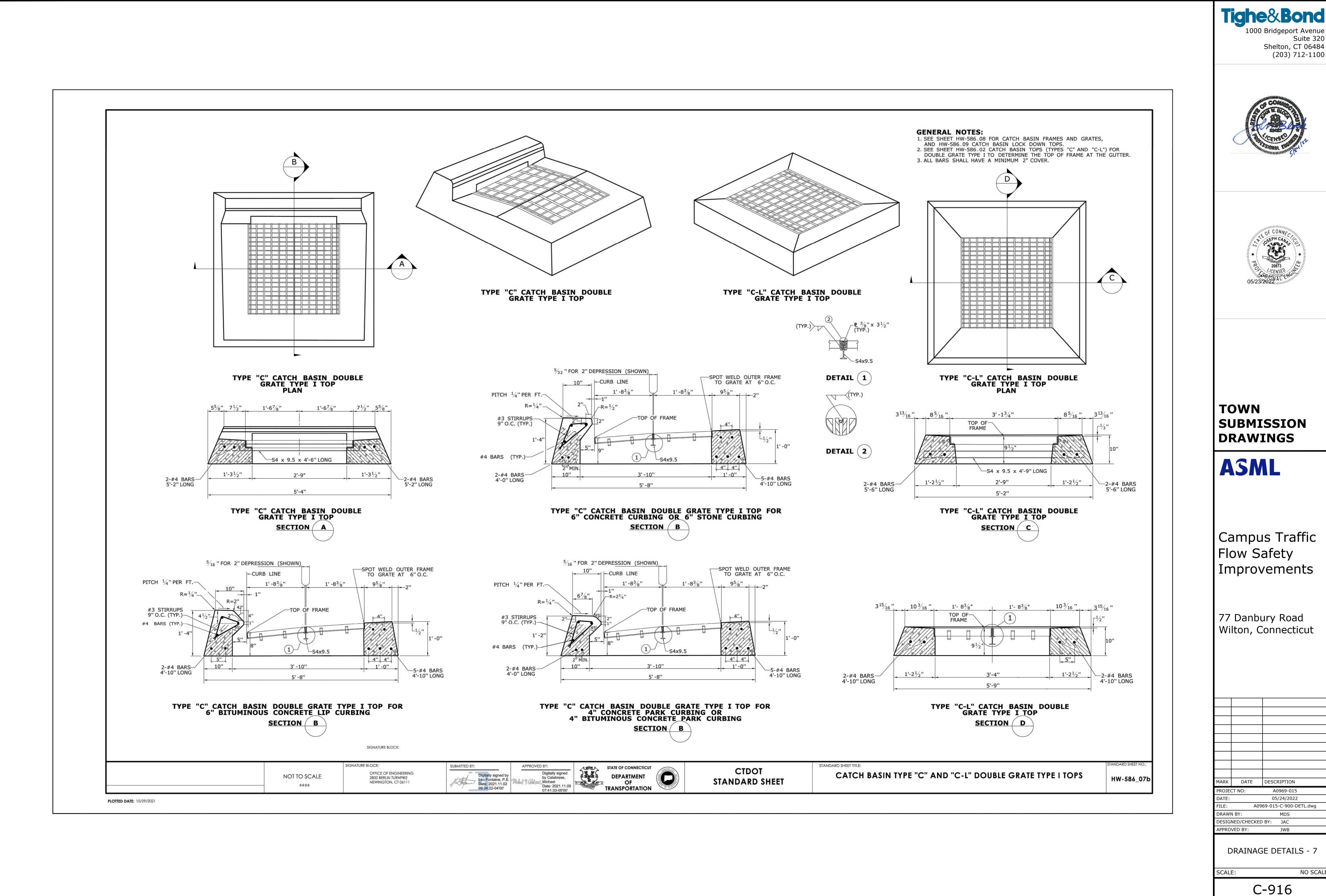
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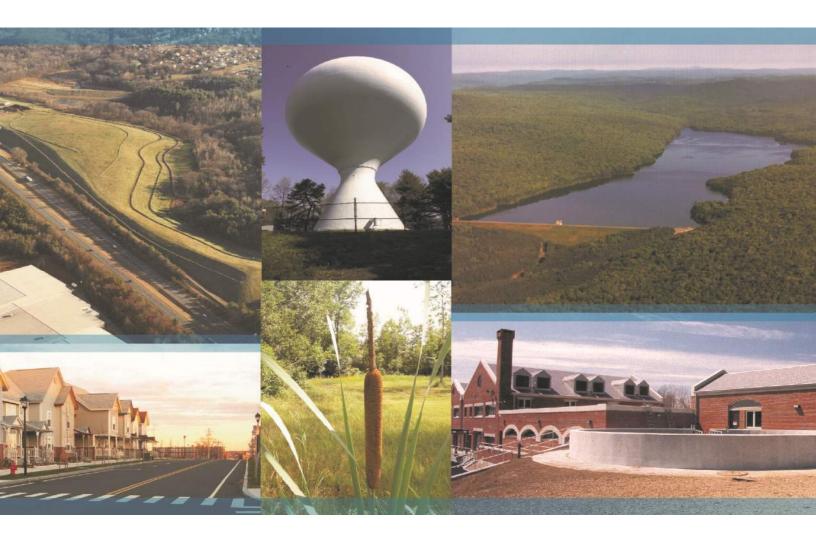
Campus Traffic Safety Flow Improvements

## INLAND WETLANDS AND WATERCOURSES SIGNIFICANT ACTIVITY PERMIT APPLICATION

ASML US, Inc. 77 Danbury Road Wilton, Connecticut

May 24, 2022





ASML 77 Danbury Road, Wilton, Connecticut

### INLAND WETLANDS AND WATERCOURSES SIGNIFICANT ACTIVITY PERMIT APPLICATION

ASML

May 2022

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Figure 2 – Orthophotograph

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   Web Soil Survey
   Natural Diversity Database Map
   FEMA Firmette
- 4 Abutter List
- 5 Self-Verification Notification Form

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### Section 1 Introduction

Tighe & Bond is submitting this Inland Wetlands and Watercourse Permit Application on behalf of ASML for Significant Regulated Activity within the 100-Foot Town regulated review area and within the boundary of regulated wetlands. This report details existing wetland and environmental conditions and regulatory compliance for a proposed driveway at 77 Danbury Road in Wilton. The proposed traffic flow safety improvements will alleviate concerns and hazards with the current driveway conditions, allowing employees to safely access the existing parking garage.

# Section 2 Existing Conditions

This section provides a description of the project site and wetland resource areas.

# 2.1 Site Description

The existing 28.88-acre site is bounded by Danbury Road (U.S. Route 7) to the east, the Metro North Commuter Railroad to the west, residential properties along Arrowhead Road to the north, and commercial property to the south. The Norwalk River flows through the eastern portion of the site, and forms part of the boundary along the southern portion of the site, and along the extreme northeast corner of the site. The project property is within a commercial and residentially developed area with interspersed open space and mature forest.

The proposed project area within the northern portion of the property. The project area consists of ledge with an existing cover of mature deciduous forest mixed with sparse evergreen trees. A forested wetland and perennial watercourses are located east of the proposed project area, within the town's 100-Foot Review Area.

The project locations are shown on the USGS Site Location Map (Figure 1) provided in Appendix A. The site and surrounding area are also shown on the Orthophotograph (Figure 2). Photographs of the resource areas are provided in Appendix B.

# 2.2 Mapped Soil Types

Digitally available soil survey information was obtained from the Natural Resources Conservation Service (NRCS) and generally confirmed during a wetland investigation and delineation conducted by a Tighe & Bond qualified Professional Soil Scientist. The Soil Scientist Report and Soil Survey Map are provided in Appendix C.

# 2.3 Resource Area Investigation

On April 1, 2022, a Tighe & Bond Certified Professional Soil Scientist and Professional Wetland Scientist conducted wetland resource area delineations within the limits of the project area. Tighe & Bond's wetland delineation was conducted in accordance with local, state, and federal guidelines, the Connecticut Inland Wetlands and Watercourses Act (§ 22a-36 to 22a-45), and Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Northcentral and Northeast Region (Version 2.0, U.S. Army Corps of Engineers, January 2012).

# 2.4 Description of Resource Areas

This section describes wetland and watercourses delineated during the April 1, 2022, field investigation.

#### 2.4.1 Watercourse 1

Watercourse 1 (flag series WC1 100 $\rightarrow$ 113; 200 $\rightarrow$ 217) consists of an unnamed perennial tributary to the Norwalk River and the Norwalk River. The western bank of the

watercourses was demarcated during the field investigation. Both watercourses are classified by the National Wetland Inventory (NWI) as riverine unknown perennial with an unconsolidated bottom and permanently flooded water regime (R5UBH). The northern tributary channel is approximately 20-feet wide with banks at gradient with the wetland boundary. The channel narrows to approximately 10-feet wide, becoming more defined as the watercourse flows south and the west bank increases in height. The bank height increase is due to fill material from previous construction of the adjacent parking lot. The watercourse substrate consists of sand and muck with approximately six to eight-inchdeep flowing water at the time of the delineation.

The confluence of the tributary and Norwalk River is west of the northeastern parking lot. The Norwalk River is approximately 40-feet wide and several feet deep with high velocity flow at the time of the delineation. The west bank has been reinforced with boulders and cut stone, and the vegetation maintained at approximately four feet in height. Besides the reinforced banks, the river has been channelized, redirected, and historically disturbed due to development.

#### 2.4.2 Wetland 1

Wetland 1(flag series 100  $\rightarrow$ 115) is located along the west banks of the Norwalk River and an unnamed tributary, where the watercourses form the eastern wetland boundary. The wetland was not identified by the NWI, however, can be classified as palustrine forested broad-leaved deciduous with a seasonally saturated water regime (PFO1E). The wetland is historically disturbed due to the channelization of the watercourse and development of adjacent properties.

Dominant vegetation observed includes red maple (*Acer rubrum*; FAC), American hornbeam (*Carpinus caroliniana*; FAC); spicebush (*Lindera benzoin*; FACW), speckled alder (*Alnus incana*; FACW), silky dogwood (*Cornus amomum*; FACW), skunk cabbage (*Symplocarpus foetidus*; OBL), and sensitive fern (*Onoclea sensibilis*; FACW).

Hydrologic indicators include surface water (8 inches), saturation to the soil surface, inundation and saturation visible on aerial imagery, water-stained leaves, drainage patterns, and microtopographic relief.

Soil observed was 24 inches of dark gray (10YR 4/1) mucky sand with brown (7.5YR 4/4) redoximorphic concentrations within the matrix. The soil meets the Sandy Mucky Mineral (S1) and Sandy Redox (S5) hydric soil indicators and meets hydric soil criteria.

# **2.5 Wetland Functions and Values**

The functions and values evaluation had been conducted generally in accordance with *The Highway Methodology Workbook Supplement, Wetland Functions and Values: A descriptive Approach* issued by the U.S. Army Corps of Engineers New England District (ACOE NED), September 1999. The *Highway Methodology* recognizes 13 separate wetland functions and values.

Functions are those properties inherent to a given wetland system that exist in the absence of society. Values are the benefits derived from functions and physical characteristics associated with a wetland. Functions and values can be principal if they are an important physical component of a wetland ecosystem (function only), and/or are considered of special value to society, from a local, regional, and/or national perspective.

The degree to which a wetland provides each of these functions and values is determined by one or more of the following factors: landscape position, substrate, hydrology, vegetation, history of disturbance, and size. The delineated wetland area may provide one or more of the listed functions and values at a principal level.

The ACOE NED workbook includes thirteen (13) functions and values that have been recognized as functions wetlands can provide: groundwater recharge/discharge, floodflow alteration, fish and shellfish habitat, sediment/toxicant retention, nutrient removal/retention/ transformation, production export, sediment/shoreline stabilization, wildlife habitat, recreation, education/scientific value, uniqueness/heritage, visual quality/aesthetics, and habitat for threatened or endangered species.

The principal functions and values of the wetland system in the project area include groundwater recharge and discharge, floodflow alteration, and wildlife habitat. The reasoning for the principal functions and values include:

#### Groundwater recharge and discharge

The wetland system allows water to move between the soil surface and subsurface.

#### Floodflow Alteration

The wetland is broad, concave, and relatively flat allowing flood storage of bank overflow from the two associated perennial watercourses. The wetland system is effective for reducing peak flow and water volume to buffer downstream properties from flooding.

#### Wildlife Habitat

Signs of wildlife, including deer, racoons, birds, chipmunks, and squirrels were observed during the investigation. The wetland is part of a wildlife corridor and is effective habitat for disturbance tolerant species.

#### 2.6 Floodplain

Based on the Federal Emergency Management Agency's (FEMA) Panel Number 09001C0391F (effective 6/18/2010), the eastern portion of the project site is located within Special Flood Hazard Area Floodway and Zone AE – area with a 1% annual chance of flooding. The FEMA Firmette is provided in Appendix C.

#### **2.7 Natural Diversity Database**

The Connecticut Department of Energy and Environmental Protection's Natural Diversity Database (NDDB) map dated December 2021 indicates that there are no areas of concern for endangered and threatened species. The NDDB Map is provided in Appendix C.

# Section 3 Project Description

This section provides a description of the proposed driveway, storm water management, proposed site stabilization measures along the project boundaries, Best Management Practices (BMPs), and post-construction measures.

# **3.1 Proposed Activities**

The proposed project will construct a new driveway from the parking lot northeast of the building, proceeding up the hillside, curving northwest, and connecting to the northeast corner of the existing parking garage between the third and fourth floors. The project will address erosion and stormwater runoff from the existing northeastern parking lot. Additional project details are provided in the Engineering Report and Project Plans submitted under separate cover and concurrently with this application.

Construction of the driveway will result in 37,185 sf of disturbance within the 100-Foot Upland Review Area for driveway improvements and 20 sf within wetland boundaries to address washout areas. Total excavation within regulated areas is 940 cy of cut and 1,072 cy of fill for a net fill of 132 cy with an increase of 2,628 sf of impervious surface.

# **3.2 Driveway Improvements**

Driveway Improvements include a full depth reconstruction, milling, regrading, curbing, 12-foot-wide travel lanes with 5-foot-wide sidewalk, and 3-foot-wide shelf for underdrainage. Timber guard rails and lighting will be upgraded along with storm water catch and management basins. Details of improvements are provided in the Engineering Report Project Plans submitted concurrently with this application.

# **3.3 Protective Measures**

Wetland resource areas at the site will be protected by an erosion control barrier consisting of straw bales and/or silt fence. The control measures are to be installed along the edge of the work areas. These protective measures will be placed in a fashion that restricts access to the wetland resource areas while allowing the contractor to conduct work within the limit of the Project. Existing catch basins will be protected with silt sacks prior to the start of construction. The locations of the protective measures are shown on the Project Drawings provided with this application. The Project Drawings also includes Erosion Control Notes on Sheets C-600 and 610 and details on Sheets C-611 and 612.

- The contractor will be required to maintain a reserve supply of straw bales and silt fence on-site to make repairs as necessary
- Protective measures will be inspected after significant precipitation events and repaired as necessary

### **3.4 Constructive Sequencing**

Proposed construction sequencing includes:

- Install sediment and erosion controls
- Grade driveway alignment
- Install underdrains
- Construct stormwater management systems
- Pave and mark driveway and parking lot
- Restore disturbed areas, plant rain garden and bioswale
- Remove sediment and erosion controls after stabilization

### **3.5 Post Construction Restoration**

The restoration measures within the Site will consist of stabilizing all disturbed areas by loaming and seeding. Erosion controls will not be removed from the site until revegetation has occurred. The driveway will be resurfaced once all installation work is completed and backfilled.

# 3.6 Mitigation

Disturbances within wetland boundaries and the 100-Foot Upland Review Area will be mitigated by improved stormwater management, plantings, and rain gardens. The list of proposed planting species is provided in Table 3-1.

#### 3.6.1 Improved Stormwater Management

The existing parking lot within the project area has limited storm water management by way of surface runoff over maintained grass to the adjacent wetland or Norwalk River, causing erosion along the eastern slope of the parking lot.

Proposed improvements include a network of catch basins and storm drains, increase of the average distance of impervious cover to wetlands, and improved water quality discharged to the river. Infiltration chambers beneath the parking area will recharge ground water and decrease peak volume and flow discharge to the river. Additionally, one 1,158 sf raingarden and a 2,978 sf biofiltration swale will improve stormwater quality discharged from the area.

#### 3.6.2 Planting Plan

Vegetation will be planted within the riparian buffer west of the Norwalk River and east of the driveway to provide plant and habitat diversity, additional nutrient uptake, and reduce overland runoff velocity. In addition, water and drought tolerant vegetation will be added to the two rain gardens and one bioswale for stormwater management and biodiversity. Table 3-1

Planting Plan Species		Wetland
Scientific Name	Common Name	Indicator Status
Raingarden Plantings		
Chasmanthium latifolium (Cl)	Indian Wood-Oats	FACW
Eutrochium purpureum (EP)	Sweet-Scented Joe-Pye-Weed	FAC
Schizachyrium scoparium (Ss)	Little false bluestem	FACU
Asclepias tuberosa (At)	Butterfly milkweed	NI
Panicum virgatum (Pv)	Want panic grass	FAC
Bioswale Plantings		
Carex stricta (Cs)	Uptight Sedge	OBL
Heuchera americana (Ha)	American alumroot	FACU
Morella pensylvanica (Mp)	Northern bayberry	FACU
Viburnum dentatum (Vd)	Arrowwood Viburnum	FAC
Ilex verticillata (Iv)	Winterberry	FACW
Monarda didyma (Md)	Scarlet beebalm	FACU
Symphyotrichum novae-angliae (Sna)	New England American-Aster	FACW
Osmundastrum cinnamomeum (Oc)	Cinnamon Fern	FACW
Riparian Plantings		
Leucothoe fontanesiana (Lf)	Highland Doghobble	FACW
Amelanchier arborea (Aa)	Downy Service-Berry	FACU
Ilex verticillata (Iv)	Winterberry	FACW
Viburnum dentatum (Vd)	Arrowwood Viburnum	FAC
Morella pensylvanica (Mp)	Northern bayberry	FACU

# 3.7 Alternatives

Four alternatives, No Build, Conducting Activity in a Different Location, Conducting an Activity of a Different Nature, and Alternate Grades, were considered for the design of the new driveway. The project and current proposal evolved through several iterations and was selected by ASML. Alternative assessment details are provided in Section 4.7 of the Engineering Report.

# Section 4 Regulatory Information

Wetlands and watercourses are regulated by municipal, state, and federal laws and regulations, each with different definitions and regulatory requirements. Accordingly, the state and municipalities may regulate wetlands and waters that fall outside of federal jurisdiction; however, where federal jurisdiction exists, concurrent state and municipal jurisdiction is almost always present.

Connecticut wetland determinations and municipal regulations are prepared and adopted in accordance with the Connecticut Inland Wetlands and Watercourse Act,  $\S$  22a-36 to 22a-45.

# 4.1 Federal Regulations

Jurisdictional wetlands at the Federal level consist of "Waters of the United States", which includes lakes, rivers and streams, as well as vegetated wetlands (See 33 CFR 328.8). The onsite waters and wetlands, regulated by the U.S. Army Corps of Engineers (ACOE), were delineated in accordance with the Regional Supplement to the Corps of Engineers Wetland Delineation Manual Northcentral and Northeast Region (Version 2.0) (January 2012). This Manual requires there to be dominant hydrophytic vegetation, hydric soils, and hydrological conditions present in determining wetland areas.

Direct impacts to Waters of the United States regulated by the U.S. Army Corps of Engineers requires authorization under the Regional General Permits for the State of Connecticut in accordance with 33 CFR 320-332. A Self-Verification Notification Form (SV) under General Permit 17- New and Expansion of Recreational, Residential, Institutional, and Commercial Developments was submitted to the ACOE concurrently with this permit. The SV is provided in Appendix E.

# 4.2 State Regulations

State wetland boundaries are based on the presence of poorly drained, very poorly drained, alluvial, or floodplain soils and submerged land. Watercourses are defined as "rivers, streams, brooks, waterways, lakes, ponds, marshes, swamps, bogs and all other bodies of water, natural or artificial, vernal or intermittent, public or private, which are contained within, flow through or border upon the state or any portion thereof." Intermittent watercourse determinations are made based on the presence of a defined permanent channel and bank, and two of the following characteristics: (1) evidence of scour or deposits of recent alluvium or detritus, (2) the presence of standing or flowing water for a duration longer than a particular storm incident, and (3) the presence of hydrophytic vegetation.

# 4.3 Municipal Regulations

The Town of Wilton Inland Wetlands and Watercourse Regulations (revised June 1, 2007), use the state definitions of wetlands and watercourses and apply to activities within the boundaries of wetlands and watercourses, and within 100-feet of wetlands and watercourses (Upland Review Area).

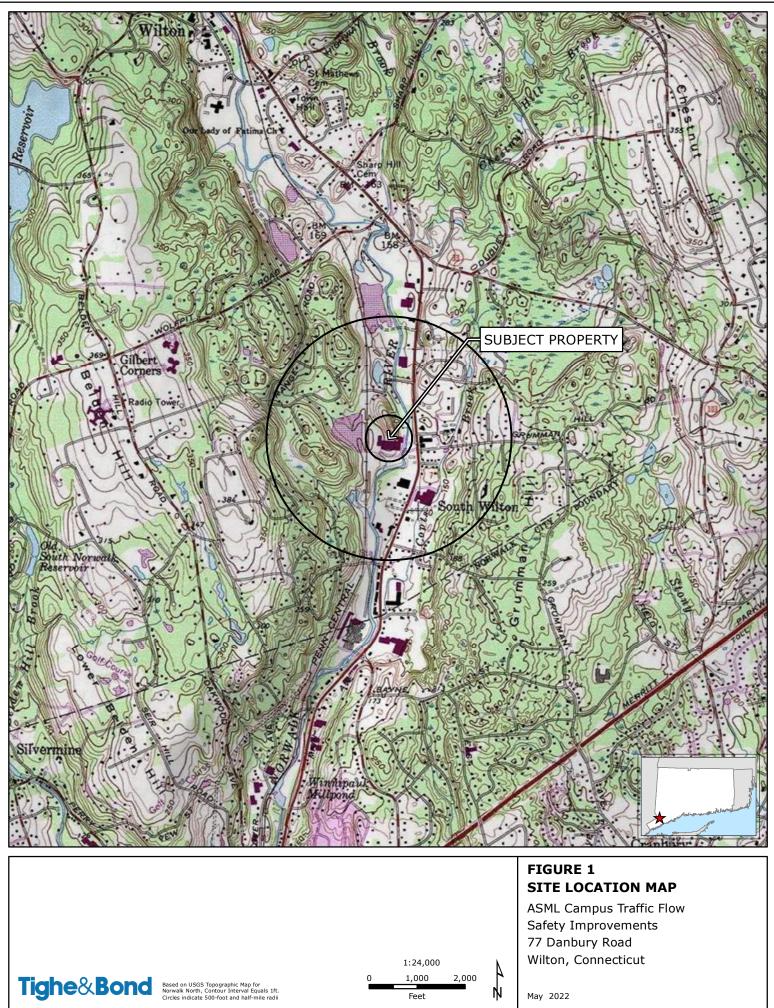
A Wilton Inland Wetlands and Watercourses Permit application is required for the proposed disturbance of 37,185 sf (0.85 acres) within the 100-foot Upland Review Area and 20 sf of wetland.

The proposed project will not substantially change on-site wetland or watercourses, has been designed to minimize disturbance within the Upland Review Area, reduce siltation and sedimentation within natural resources, and enhance pollutant management through stormwater controls.

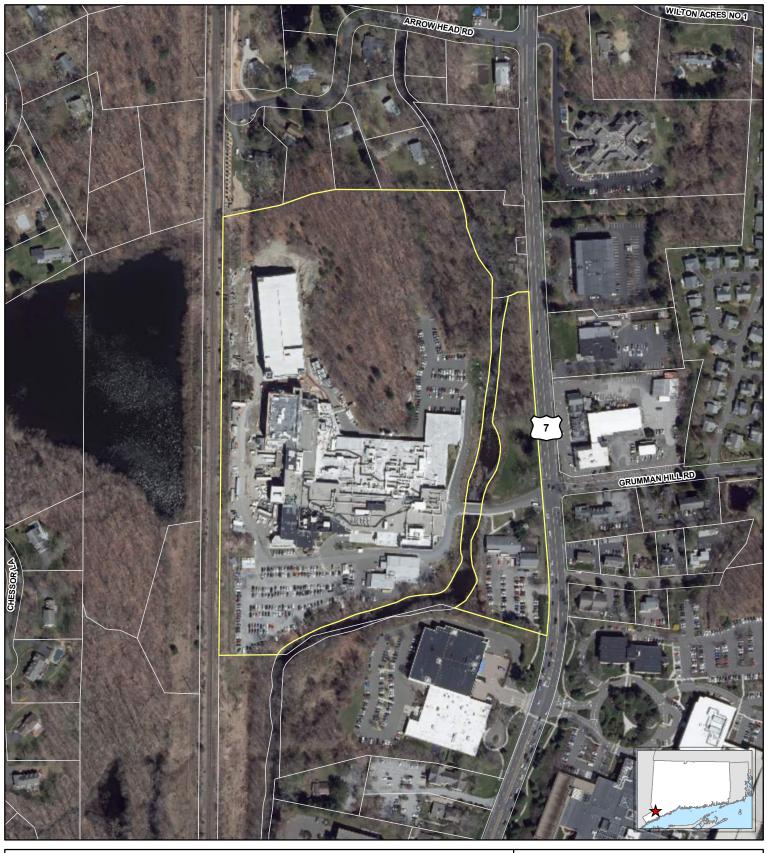
# Section 5 Summary

Two perennial watercourses and one forested wetland were identified during the April 1, 2022, site investigation. Proposed activities are in compliance with the Town of Wilton Significant Regulated Activity for 20 sf of work proposed within wetland boundaries and 37,185 sf of work within the 100-Foot Review Area. The activities directly impacting wetlands require the submittal of a Self-Verification regulated by the U.S. Army Corps of Engineers, submitted concurrently with this application.

**APPENDIX A** 



:\Projects\A\A0969\ASMLDrivewayImprovement\_topo.mxd [Exported By: SMMorse, 5/6/2022, 2:20:10 PM]



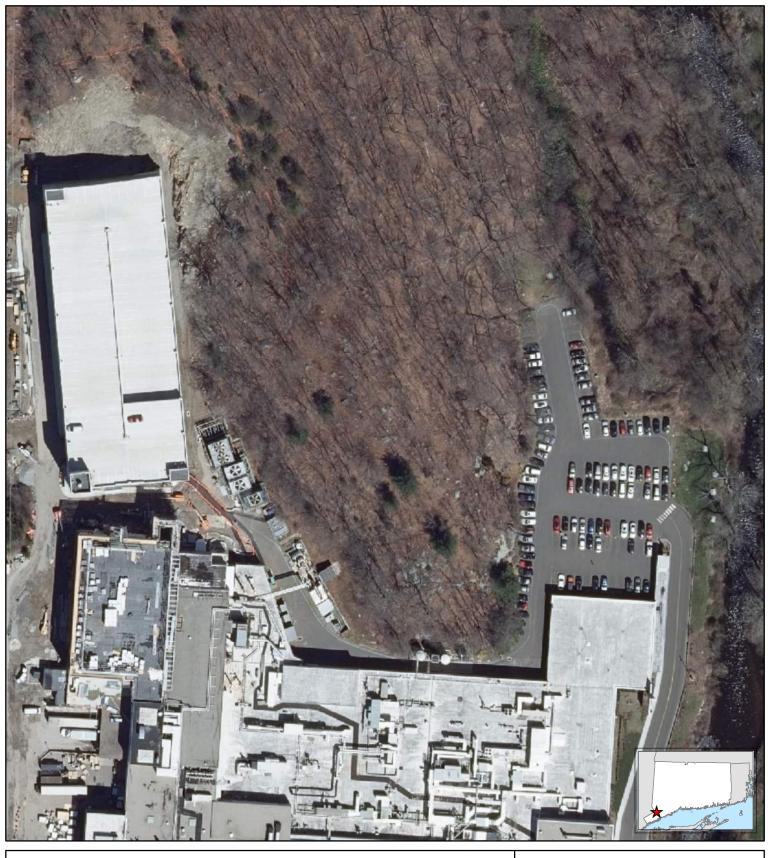
# LEGEND Approximate Subject Property Approximate Parcel Boundary Image: Statewide Leaf-Off Orthophotography, Courtesty of CTECO. Withon Parcels (Pr20) provided by WestCOG and are approximate.

#### FIGURE 2 ORTHOPHOTOGRAPH

ASML Campus Traffic Flow Safety Improvements 77 Danbury Road Wilton, Connecticut

May 2022

:\Projects\A\A0969\ASMLDrivewayImprovement\_aerial.mxd [Exported By: SMMorse, 5/6/2022, 2:19:59 PM]



#### FIGURE 3 SITE LOCATION

May 2022

ASML Campus Traffic Flow Safety Improvements 77 Danbury Road Wilton, Connecticut

Tighe&Bond Based on 2019 Statewide Leef-Off Orthophotography, Courtesty of CTECO.

LEGEND

1:1,200 50 100 Feet

**APPENDIX B** 

# **Photographic Log**

# Tighe&Bond

#### Client: ASML

#### Job Number: <u>A0969-0</u>15

Site: 77 Danbury Road, Wilton, Connecticut



Photograph No.: 2	Date: 4/1/2022	Direction Taken: East

**Description:** The proposed drainage improvements will address the current stormwater runoff conditions.



# **Photographic Log**

# Tighe&Bond

#### Client: ASML

#### Job Number: <u>A0969-0</u>15

Site: 77 Danbury Road, Wilton, Connecticut

Photograph No.: 3	Date: 4/1/2022	Direction Taken: North
<b>Description:</b> Norwalk Ri lot.	ver bounds the site to	the east with an upland riparian buffer to the parking
	AND REAL PROPERTY.	
		Notes The second



### **Photographic Log**

#### Client: ASML

#### **Job Number:** A0969-015

Tighe&Bond

Site: 77 Danbury Road, Wilton, Connecticut

Photograph No.: 5 Date: 4/1/2022	Direction Taken: North
----------------------------------	------------------------

**Description:** Stormwater collected along the eastern boundary of the parking lot observed flowing into the adjacent wetland.



Photograph No.: 6	Date: 4/1/2022	Direction Taken: South

**Description:** The forested wetland and perennial tributary to the Norwalk River are north of the building and parking lot.



**APPENDIX C** 

### SOIL REPORT

Project: ASML- Driveway Improvement Wilton, CT Project No. A-0969-015 Site Inspection Date 4/1/2022

**PROJECT DESCRIPTION:** Inland wetland identification and delineation.

#### METHOD FOR IDENTIFICATION OF MAP UNITS

Wetlands

<u>X</u> Field marking (flagging) for survey

\_\_\_\_Field plotting on \_\_\_\_\_

\_\_\_\_\_Field plotting on aerial photography

#### **Non Wetland Soils**

\_\_\_\_\_High intensity field identification by Soil Scientist

X\_Medium intensity identification from USDA, Natural Resources Conservation Service

#### METHOD OF SOIL IDENTIFICATION

<u>X</u>Spade and Auger Deep test pits (backhoe) Other\_\_

#### SOIL MOISTURE CONDITION

Dry\_\_\_\_ Moist <u>X</u> Wet\_\_\_\_ Frost Depth \_\_\_\_\_in. Snow Depth \_\_\_\_\_in.

The classification system of the National Cooperative Soil Survey, USDA, Soil Conservation Service and the County Identification Legend were used in this investigation. The investigation was conducted by the undersigned Certified Soil Scientist.

All wetland boundary lines established by the undersigned Soil Scientist are subject to change until officially adopted by local, state, or federal regulatory agencies.

Respectively submitted by,

#### TIGHE & BOND, INC.

Raina Volovski

Raina Volovski Certified Professional Soil Scientist Professional Wetland Scientist

#### **SOIL REPORT** continued

#### **PROJECT:** Nystrom Pond Dam

#### **MAPS/PLANS GENERATED**

\_\_\_\_Site plan with soil types and wetland flags located by survey

\_\_\_\_Sketch location of wetlands and other soil types

\_X\_\_Site Plan with wetland flags, USDA-NRCS Web soil survey

\_\_\_\_None

#### NUMBERING SEQUENCE OF WETLAND BOUNDARY LINE MARKERS

W1 100-115 WC1 100-113, 200-217

#### SUMMARY SOIL DESCRIPTIONS

Digitally available updated soil survey information was obtained from the Natural Resources Conservation Service (NRCS) as depicted on the attached soil map. The following soil types were identified during the delineation:

#### Hydric Soils

#### Pootatuck fine sandy loam (Map Unit 102)

The Pootatuck component is on flood plains with parent material consisting of course-loamy alluvium. The natural drainage class is moderately well drained; however, this soil is frequently flooded. This component is in the F144AY012CT Sandy Low Floodplain ecological site. The ecological site is typically comprised of a floodplain forest found in early to mid-successional staged due to the dynamic nature of floodplains. The frequency, duration, and timing of floods is the primary natural disturbance affecting species composition. River types vary in gradient, hydrologic regime, and fluvial geomorphology resulting in different community composition. This soil meets the Connecticut Inland Wetland hydric criteria and concurrent with the field delineated wetland.

#### Non-hydric Soils

#### Hollis-Chatfield- Rock outcrop complex (75E)

The Hollis and Chatfield soils have slopes from 3 to 15 percent. Both of these components are on uplands, bedrock controlled hills and bedrock controlled ridges. The parent material of Hollis soils consists of loamy melt-out till derived from granite and/or schist and/or gneiss, with Chatfield parent material consisting of course-loamy melt-out till derived from granite and/or schist and/or schist and/or gneiss. The natural drainage class for Hollis soil is somewhat excessively drained, and well drained for Chatfield soil. This component is in the F144AY033MA Shallow Dry Till Uplands ecological site with plant communities dominated by oak forests. Trees are generally lower is stature and productivity relative to forests in deeper soils. This soil complex does not meet hydric criteria.

#### Charlton-Urban land complex (Map Unit 260C)

The Charlton component is on hills on glaciated uplands with slopes between 8 and 15 percent. The parent material consists of coarse-loamy melt-out till derived from gneiss, granite, and/or schist. The natural drainage class is well drained. This component is in the F144AY034CT Well Drained Till Uplands ecological site. The ecology of the site is dominated by oak species and the unique red soil minerology

213 Court Street, Suite 1100 • Middletown, CT 06457 • Tel 860.704.4760 • Fax 860.704.4775



of the Connecticut River Valley provides a relatively rich substrate for vegetation growth. This soil does not meet hydric criteria.

Urban land is land mostly covered by streets, parking lots, buildings, and other structures of urban areas. Slopes range from 0 to 45 percent. No drainage class is assigned and does not meet hydric criteria.

#### Haven silt loam (Map Unit 703B)

The Haven soil is typically found on outwash terraces on valleys with a 3 to 8 percent slope. The parent material consists of course-loamy eolian deposits over sandy and gravelly glaciofluvial deposits derived from granite and/or schist and/or gneiss. This component is in the F144AY023CT Well Drained Outwash ecological site. Representative plant communities are varied but consist largely of pines and oaks. The natural drainage class is well drained and does not meet hydric criteria.



**Conservation Service** 

Web Soil Survey National Cooperative Soil Survey

	MAP L	EGEND		MAP INFORMATION	
Area of Interest (AOI)		33	Spoil Area	The soil surveys that comprise your AOI were mapped at	
Are	Area of Interest (AOI)	۵	Stony Spot	1:12,000.	
Soils		â	Very Stony Spot	Warning: Soil Map may not be valid at this scale.	
	l Map Unit Polygons	Ŷ	Wet Spot	Enlargement of maps beyond the scale of mapping can cause	
	l Map Unit Lines		Other	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of	
Soi	Map Unit Points		Special Line Features	contrasting soils that could have been shown at a more detailed	
Special Point		Water Fea	•	scale.	
•	wout row Pit	~	Streams and Canals	Please rely on the bar scale on each map sheet for map measurements.	
💥 Cla	y Spot	Transport	Rails	Source of Map: Natural Resources Conservation Service	
🚫 Clo	sed Depression	~	Interstate Highways	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)	
💥 Gra	vel Pit	~	US Routes	Maps from the Web Soil Survey are based on the Web Mercate	
👬 Gra	velly Spot	~	Major Roads	projection, which preserves direction and shape but distorts	
🙆 Lan	dfill	~	Local Roads	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more	
A Lav	a Flow	Backgrou	nd	accurate calculations of distance or area are required.	
	rsh or swamp	Buokgrou	Aerial Photography	This product is generated from the USDA-NRCS certified data of the version date(s) listed below.	
🙊 Min	e or Quarry			Soil Survey Area: State of Connecticut	
Mis	cellaneous Water			Survey Area Data: Version 21, Sep 7, 2021	
O Per	ennial Water			Soil map units are labeled (as space allows) for map scales	
👽 Roo	ck Outcrop			1:50,000 or larger.	
🕂 Sali	ine Spot			Date(s) aerial images were photographed: Oct 8, 2020—Oct 2020	
👬 Sar	ndy Spot			The orthophoto or other base map on which the soil lines were	
🕳 Sev	verely Eroded Spot			compiled and digitized probably differs from the background	
👌 Sin	khole			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.	
Slid	le or Slip				
👩 Soc	lic Spot				



# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
75E	Hollis-Chatfield-Rock outcrop complex, 15 to 45 percent slopes	3.8	14.0%
102	Pootatuck fine sandy loam	3.5	12.8%
103	Rippowam fine sandy loam	0.1	0.5%
260C	Charlton-Urban land complex, 8 to 15 percent slopes	4.9	17.8%
306	Udorthents-Urban land complex	0.8	2.8%
307	Urban land	8.6	31.3%
703B	Haven silt loam, 3 to 8 percent slopes	4.8	17.6%
W	Water	0.8	3.1%
Totals for Area of Interest	· ·	27.3	100.0%



# Natural Diversity Data Base

#### Areas

WILTON, CT

December 2021



Critical Habitat

State and Federal Listed Species

#### . . .

Town Boundary

NOTE: This map shows general locations of State and Federal Listed Species and Critical Habitats. Information on listed species is collected and compiled by the Natural Diversity Data Base (NDDB) from a variety of data sources. Exact locations of species have been buffered to produce the generalized locations.

This map is intended for use as a preliminary screening tool for conducting a Natural Diversity Data Base Review Request. To use the map, locate the project boundaries and any additional affected areas. If the project is within a hatched area there may be a potential conflict with a listed species. For more information, complete a Request for Natural Diversity Data Base State Listed Species Review form (DEP-APP-007), and submit it to the NDDB along with the required maps and information. More detailed instructions are provided with the request form on our website.

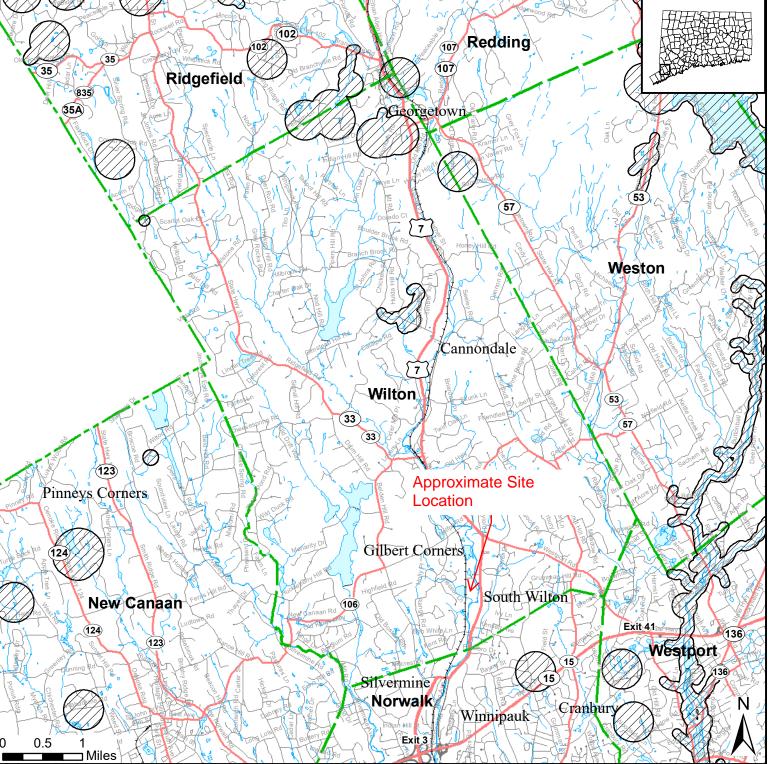
#### www.ct.gov/deep/nddbrequest

Use the CTECO Interactive Map Viewers at http://cteco.uconn.edu to more precisely search for and locate a site and to view aerial imagery with NDDB Areas.

QUESTIONS: Department of Energy and Environmental Protection (DEEP) 79 Elm St, Hartford, CT 06106 email: deep.nddbrequest@ct.gov Phone: (860) 424-3011



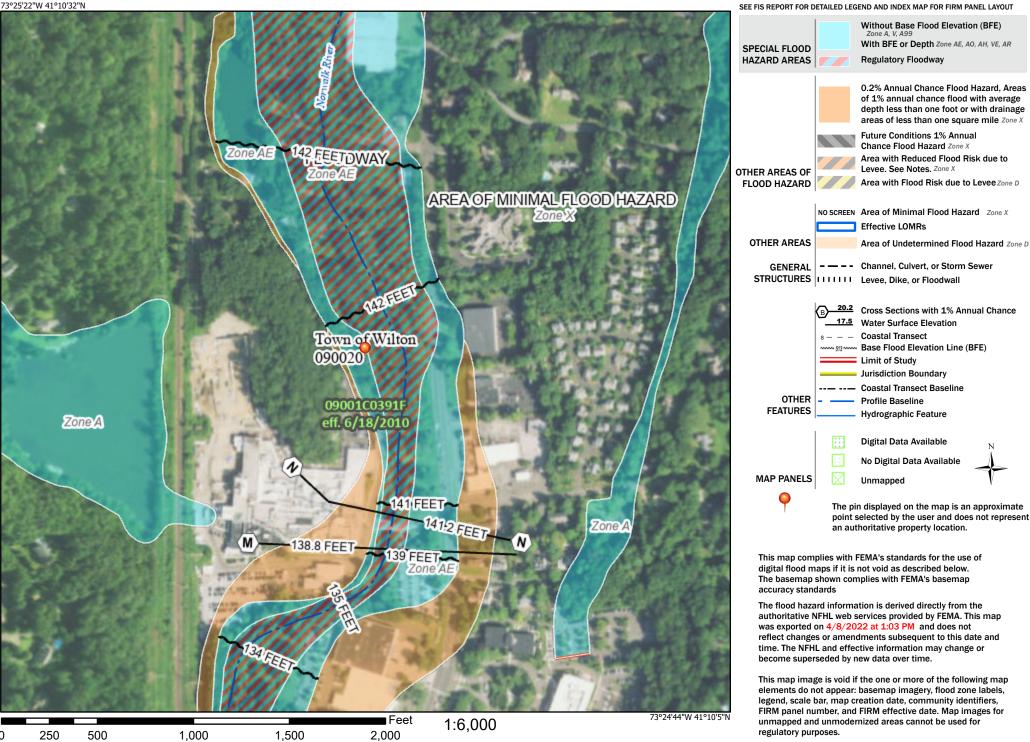
Connecticut Department of Energy & Environmental Protection Bureau of Natural Resources Wildlife Division



# National Flood Hazard Layer FIRMette



#### Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

**APPENDIX D** 

#### TOWN OF WILTON, CONNECTICUT

			-			
Parcel ID	Site Address	Owner Name	Mailing Address	Mailing City	Mailing State	Mailing Zip
68-36-B	59 DANBURY RD	WILTON PROPERTIES RSK LLC	470 WEST AVE STE 2007	STAMFORD	СТ	06902-0000
69-18	77 DANBURY RD	ASML US LLC	6115 CAMP BOWIE #152	FORT WORTH	тх	76116-0000
69-18	77 DANBURY RD	ASML US LLC	6115 CAMP BOWIE #152	FORT WORTH	тх	76116-0000
69-20	89 DANBURY RD	HICKEY THOMAS F	89 DANBURY RD	WILTON	СТ	06897-0000
69-22	91 DANBURY RD	WILTON TOWN OF	238 DANBURY RD	WILTON	СТ	06897-0000
69-26	27 ARROWHEAD RD	KIM ZENA	23-88 31ST ST #5D	ASTORIA	NY	11105-0000
69-27	29 ARROWHEAD RD	ARNOLD LAURENCE J & SANDRA P	29 ARROWHEAD RD	WILTON	СТ	06897-0000
69-28	33 ARROWHEAD RD	CONTRERAS WILSON &	33 ARROWHEAD RD	WILTON	СТ	06897-0000
69-29	39 ARROWHEAD RD	VARRONE NICHOLAS J & MICHELLE L	39 ARROWHEAD RD	WILTON	СТ	06897-0000
70-16-1	DANBURY RD	CONN LIGHT & POWER CO THE	PO BOX 270	HARTFORD	СТ	06141-0000
68-36-A	65 DANBURY RD	WILTON PROJECT LLC	METRO CENTER ONE STATION PL	STAMFORD	СТ	06902- 0000
68-36	59-65 DANBURY RD		59-65 DANBURY RD	WILTON	СТ	06897-0000
68-36-C	DANBURY RD	WILTON PROJECT LLC	METRO CENTER ONE STATION PL	STAMFORD	СТ	06902- 0000

**APPENDIX E** 



#### US Army Corps of Engineers ® New England District

#### **Appendix E: Self-Verification Notification Form**

This form is required for all inland projects in Connecticut, but it is not required if work is done within boundaries of Mashantucket Pequot or Mohegan Tribal Lands. At least two weeks before work commences, complete all fields (write "none" if applicable) below, send this form, Official Species List (see GC 12), documentation of THPO and SHPO notifications if applicable, site location map, project plans (not required for projects involving the installation of construction mats only) and any State or local approval(s) to:

Regulatory Division, Branch B U.S. Army Corps of Engineers 696 Virginia Road and Concord, MA 01742-2751 or cenae-r-ct@usace.army.mil	CT DEEP 79 Elm Street Hartford, CT 06106-5127 or DEEP.LWRDRegulatorySubmittals@ct.gov
State Permit Number:	Date of State Permit:
Permittee:	
Address, City, State & Zip:	
Phone(s) and Email:	
Address City State & Zin:	
Phone(s) and Email:	
Contractor:	
Address, City, State & Zip:	
Phone(s) and Email:	
Project Name: CAMPUS TRAFFIC FLOW SAFETY	IMPROVEMENTS
Project Location (provide detailed description	
Lat. ° N, Long ° (Decimal Degrees):	
Waterway Name:	
Proposed Work Dates: Start:	Finish:
Work will be done under the following GPs (	circle all that apply):
2 5 6 9 10 11 12 13 14 15 1	7 18 19 21
Area of Wetland Impacts (SF): Permanent:	Temporary:
Area of Waterway Impacts (SF): Permanent:	Temporary:
TOTAL Project Impact (SF): Permanent:	Temporary:

Describe the specific work that will be undertaken in waters and wetlands:
Storm water runoff from an existing parking lot created washout within the wetland. The proposed work includes the restoration of 20 square feet of previously disturbed wetland along the toe slope of fill. Restoration includes removal of non-native material, loaming and seeding as the wetland and adjacent area is maintained as grass. Wetland soils will not be disturbed due to work activities. No work is proposed within watercourses.
-
Have the THPOs and the CT SHPO been notified of the proposed work per the procedures in GC 11? If so, attach any responses received to this form. Yes date contactedNo
Are there Federally listed endangered/threatened species, other than the northern long-eared bat, present? (see GC 12) Yes No
Confirm no SAVs are present or will be impacted: Yes No         Applicable to GPs:         2       5       6       9       10       11       12       13       14       15       17       18       19       21
Confirm no unconfined work with impact to diadromous fish (see App. H): Yes No Applicable to GPs: 2 5 6 9 10 19
Confirm work complies with Stream Crossing BMPs (see App. G): YesNo
Applicable to GPs:261719
If GP 19 and work does not comply with Appendix G, identify date of Interagency Meeting where waiver was granted: Date of Meeting:
waiver was granted: Date of Meeting: Identify interagency participants: CT DEEP: USACE:
Will your project include any secondary effects? (Secondary effects include, but are not limited to, non-tidal waters or wetlands drained, flooded, fragmented, or mechanically cleared resulting from a

single and complete project. See Appendix F - Definitions.) If YES, describe here: <u>The project will not include secondary effects.</u>

Your signature below, as permittee, indicates that you accept and agree to comply with the terms, eligibility criteria, and general conditions for Self-Verification under the Connecticut GPs.

Permittee Signature: Raina Volovski \_\_\_\_ Date: \_\_\_\_\_



Campus Traffic Safety Flow Improvements

# **ENGINEERING REPORT**

ASML US, Inc. 77 Danbury Road Wilton, Connecticut

May 24, 2022









Campus Traffic Safety Flow Improvements

# **ENGINEERING REPORT**

ASML US, Inc. 77 Danbury Road Wilton, Connecticut

May 24, 2022

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### **Abbreviations**

ac	acres
BFE	Base Flood Elevation
BMP	Best Management Practice
CAM	Coastal Area Management
CB	catch basin
CCMA	Connecticut Coastal Management Act
cf	cubic feet
cfs	cubic feet per second
CGS	Connecticut General Statutes
CIRCA	Connecticut Institute for Resilience and Climate Adaptation
CN	Curve Number
CT	Connecticut
CTDEEP	Connecticut Department of Energy and Environmental Protection
CTSWQM	Connecticut Stormwater Quality Manual
DCIA	Directly Connected Impervious Area
FEMA	Federal Emergency Management Agency
FIS	Flood Insurance Study
ft	feet
ft/s	feet per second
GNHWPCA	Greater New Haven Water Pollution Control Authority
gpd	gallons per day
GRV	Groundwater Recharge Volume
HSG	Hydrologic Soil Group
LEP	Licensed Environmental Professional
LiDAR	Light Imaging and Detection and Rnaging
LLC	Limited Liability Corporation
МН	Manhole
NAVD88	North American vertical Datum of 1988
NDDB	Natural Diversity Database
NFIP	National Flood Insurance Program
NGVD29	National Geodetic Vertical Datum of 1929
NOAA	National Oceanic and Atmospheric Administration
NRCS	Natural Resources Conservation Service
RCP	Reinforced Concrete Pipe
RCV	Runoff Capture Volume
RWA	Regional Water Authority

- s second
- TDTrench DrainTSSTotal Suspended Solids
- UI United Illuminating USACE United States Army Corps of Engineers
- WQFWater Quality FlowWQSWater Quality SystemWQVWater Quality Volume
- YD Yard Drain

## Section 1 Introduction and Site Conditions

Tighe & Bond has prepared this engineering report in connection with the ASML Traffic Flow Safety Improvements at ASML's campus located at 77 Danbury Road in Wilton, Connecticut. ASML proposes the construction of a new driveway from the north parking lot, climbing the existing topography to reach the landing between the third and fourth floor of the existing parking garage. The proposed driveway will include the construction of new stormwater management systems, and landscaping.

Refer to **Figure 1** for the Site Location Map.

## **1.1 Site Description**

The existing 28.64 acre site is bounded by Danbury Road (U.S. Route 7) to the east, the Metro North Commuter Railroad to the west, residential properties along Arrowhead Drive to the north, and commercial property to the south. The Norwalk River flows through the eastern portion of the site, and forms part of the boundary along the southern portion of the site, and along the extreme northeast corner of the site. The property is located in Zoning District DE-10.

The main facility building and the parking garage are located on the portion of the site west of the Norwalk River. Most of the on-site parking is located in the parking garage, although there are surface lots located immediately west of the parking garage, southwest of the building, and northeast of the building along the Norwalk River. Another building on the subject parcel, is located east of the Norwalk River at the southeastern corner of the site, with an address of 71 Danbury Road.

Loading docks are located along the west facing side of the main facility building. All existing traffic accessing the parking garage must turn left after the Norwalk River bridge and proceed around the south side of the building, and pass through the loading dock area.

Please refer to Aerial Map in Figure 2.

The southern portion of the property is generally flat, draining toward the Norwalk River. The north central portion of the site is dominated by up to an 80 foot rise in the topography that acts as a ridge separating the parking garage from the northeast parking lot.

There are wetlands associated with the Norwalk River corridor, as well as a regulatory floodway and floodplain.

## **1.2 Project Proposal**

The proposed project will construct a new driveway from the parking lot northeast of the building that would proceed up the hillside, curving approximately 150 degrees, and connecting to the northeast corner of the parking garage between the third and fourth floors. Associated lighting, landscaping, security and stormwater management

improvements are also proposed to accommodate the new driveway. The driveway will be constructed at a grade of 7%, which will require rock cuts and retaining walls along the alignment. A sidewalk is also proposed along the driveway, as well as an emergency vehicle turnaround near the entrance to the parking garage.

The northeastern parking area will be reconfigured to accommodate the alignment of the proposed driveway, resulting in the loss of 66 spaces. The loss of the 66 spaces would bring the total number of parking spaces on the site down to 1,127, which is more than the 944 parking spaces that are required.

### **1.2.1 Project Purpose**

Under existing conditions, in order to access the parking garage, all traffic entering the site must turn left at the driveway bridge after entering the site from Route 7, and proceed in a clockwise path around the building to access the parking garage at the northwest corner of the site. As a result passenger cars and truck traffic is comingled, and must pass through the active loading areas on the south and west sides of the building. In order to improve the safety of the campus traffic flow, ASML proposes the new driveway so that employees can turn right after the driveway bridge and continue along the driveway to access the parking garage. The new driveway would allow for separation of vehicular and truck traffic, and reduce the amount of traffic proceeding through the active loading areas, which would improve overall campus traffic flow safety.

Refer to **Figures 3 and 4** for current and proposed traffic flow.

### 1.2.2 Proposed Lighting

The proposed site lighting fixtures are full cutoff and have been selected to avoid light trespass onto adjacent properties.

### 1.2.5 Stormwater Management

The proposed driveway will have a network of catch basins and storm drains. The proposed improvements will increase the average distance of impervious coverage from the wetlands associated with the Norwalk River. New stormwater treatment practices are proposed that will improve the quality of stormwater that is discharged into the river, as none exist under existing conditions. Proposed infiltration chambers beneath the proposed parking area will recharge groundwater and decrease peak volume and flow discharged into the river, and proposed rain gardens and a biofiltration swale will also improve stormwater quality discharged from the project area. Please refer to Section 2 for more detail.

## 1.3 Floodplain Management

The Flood Insurance Study for Fairfield County, dated June 18, 2010 shows that there is a Special Flood Hazard Area, Zone AE and floodway associated with the Norwalk River.

The proposed driveway is located outside of the regulatory floodway, though a portion of the embankment near the first curve to the northwest are within the floodway. Portions of the driveway are within the regulatory floodplain, extending from the existing driveway bridge north to just east of the proposed northeast parking lot entrance. Base flood (1% annual chance) elevations near the northeastern parking lot are approximately elevation 140 NAVD88. We prepared a hydraulic model to demonstrate compliance with the Town's floodplain management regulations, and to demonstrate compliance with the no-rise standard for encroachments into the regulatory floodway.

Please refer to **Figure 5** for the flood zone in the area.

## 1.4 Soils & Geology

The NRCS Web Soil Survey indicates that the underlying soils for the project area includes Pootatuck Fine Sandy Loam (102) for the northeastern part of the site, Hollis-Chatfield-Rock outcrop complex, 15 to 45 percent slopes (75E) for the east slope of the hillside, and Charlton-Urban land complex, 8 to 15 percent slopes (260C) for the west slope of the hillside. The balance of the work area around the building is Urban Land (307).

The Hydrologic Soil Group for each of the soil types is described in Table 1-1 below.

### Table 1-1 Hydrologic Soils Group

Description	HSG
Charlton-Urban land complex, 8 to 15 percent slopes (260C)	В
Hollis-Chatfield-Rock outcrop complex, 15 to 45 percent slopes (75E)	D
Pootatuck Fine Sandy Loam (102)	В
Urban Land (307)	D

The NRCS Web Soil Survey Report is located in **Appendix A**.

Please refer to **Figure 6** for the soil type boundaries.

### **1.4.1 Hydrologic Soil Groups**

Soils are classified by the Natural Resource Conservation Service into four Hydrologic Soil Groups (HSG) based on the soil's runoff potential. The four Hydrologic Soils Groups are A, B, C and D. Group A soils generally have the smallest runoff potential, while Group D soils have the greatest runoff potential. All on-site soils are HSG B.

**Group A.** Soils in this group have low runoff potential when thoroughly wet. Water is transmitted freely through the soil. Group A soils typically have less than 10 percent clay and more than 90 percent sand or gravel and have gravel or sand textures. Some soils having loamy sand, sandy loam, loam or silt loam textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments.

**Group B.** Soils in this group have moderately low runoff potential when thoroughly wet. Water transmission through the soil is unimpeded. Group B soils typically have between 10 percent and 20 percent clay and 50 percent to 90 percent sand and have loamy sand or sandy loam textures. Some soils having loam, silt loam, silt, or sandy clay loam textures

may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments.

**Group C.** Soils in this group have moderately high runoff potential when thoroughly wet. Water transmission through the soil is somewhat restricted. Group C soils typically have between 20 percent and 40 percent clay and less than 50 percent sand and have loam, silt loam, sandy clay loam, clay loam, and silty clay loam textures. Some soils having clay, silty clay, or sandy clay textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments.

**Group D**. Soils in this group have high runoff potential when thoroughly wet. Water movement through the soil is restricted or very restricted. Group D soils typically have greater than 40 percent clay, less than 50 percent sand, and have clayey textures. In some areas, they also have high shrink-swell potential.

**Dual Group Soils.** Certain wet soils are placed in group D based solely on the presence of a water table within 24 inches of the surface even though the saturated hydraulic conductivity may be favorable for water transmission. If these soils can be adequately drained, then they are assigned to dual hydrologic soil groups (A/D, B/D, and C/D) based on their saturated hydraulic conductivity and the water table depth when drained.

Based on the Surficial Map of Connecticut (1993) and Bedrock Geological Mpa of Connecticut (1985), the site subsurface conditions are anticipated to consist of naturally deposited sands and gravel over bedrock. The bedrock is anticipated to consist of the Harrison Gneiss formation.

### **1.5 Natural Diversity Communities**

The Connecticut Department of Energy and Environmental Protection's Natural Diversity Database (NDDB) map dated December 2021 indicates that there are no areas of concern for endangered and threatened species, as shown in **Figure 7**.

## **1.6 Earthwork Activities**

The proposed driveway will require cut into the existing hillside, as well as some limited areas of fill. The filling will occur on the downslope side of the driveway. In some instances, the extent of fill will be restrained by a proposed retaining wall to minimize encroachment into the floodway and the wetlands along the east side of the site. Additionally, a retaining wall is proposed on the north side of the proposed driveway, where it connects to the existing parking garage. The proposed driveway will be on the high side of the wall. The wall is proposed in this location to minimize the extent to fill encroachment so that it does not project into the exterior openings of the existing garage.

We anticipate that due to the depth of cut, portions of the excavation will be in rock.

The maximum depth of cut will be approximately 27 feet, as shown in Figure 8.

Blasting is not expected for rock removal, since the rock was able to be hammered for the parking garage, and blasting could disrupt the sensitive operations within the building.

We have scheduled borings to better determine the characteristics of the underlying rock, and its depth.

The Town of Wilton has a limitation on the contiguous area allowed to be disturbed on slopes of 15% and 35% and greater. The proposed project will disturb 17,541 square feet of land steeper than 35%, with a maximum contiguous area steeper than 15% disturbed of 24,026 square feet. There is currently a proposed text amendment to the zoning regulations that would increase the 15,000 square foot limit on such disturbances in the Zoning Regulations. Please refer to **Figure 9**.

Earthwork is summarized in Table 1-2.

#### Table 1-2 Earthwork Summary

Cut	Fill	Net
12,657 cy	2,245 cy	10,412 cy

Please refer to Section 5 for a detailed description of the Construction Sequence and proposed erosion controls.

### **1.6.1** Chemical and Physical Description of Fill Materials

The proposed project will require limited fill within the upland review area to support the construction of the driveway. The fill material to be deposited will be clean soil, free of large stone, organic material and woody debris. The fill material shall be moderately to well drained.

Other material to be deposited within the upland review area includes crushed stone for to support the foundation of the proposed retaining wall.

## Section 2 Stormwater Management

## 2.1 Design Criteria

The following storm drainage design criteria were used in our hydrologic and hydraulic analyses:

- 1. Design storm rainfall data was based on NOAA Precipitation Atlas 14.
- 2. Comparative hydrology assessed the 2, 10, 25, 50 and 100-year storm events.
- 3. Piped storm drainage system and the outlets are designed for a 25-year storm event.
- 4. Minimum time of concentration = 5 minutes.
- 5. For Rational Method peak flow calculations, runoff coefficients were as follows:
  - a. Impervious (Pavement/Roof) areas = 0.90
  - b. Wooded areas = 0.50
  - c. Landscaped areas = 0.30
- 6. Minimum diameter pipes, excluding roof leaders, underdrains, outlet control and foundation drains = 12 inches
- 7. Minimum pipe slope = 0.35 percent
- 8. The storm water management plan for the site is designed to treat the Water Quality Volume, remove Total Suspended Solids and promote groundwater recharge while reducing peak flow.
- 9. Watershed areas delineated using polylines in AutoCAD Civil 3D 2018.
- 10. Comparative hydrology analyzed using AutoCAD Civil 3D 2018 Hydraflow Hydrographs Extension Version 10.40 by Autodesk software.
- 11. Storm sewer capacities analyzed using AutoCAD Civil 3D 2018 Hydraflow Storm Sewers by Autodesk.

### 2.1.1 Site Soil Characteristics

The underlying site soil characteristics are described in Section 1.4 Soils & Geology.

### 2.1.2 Location of Surface Waterbodies

The Norwalk River runs through the eastern portion of the site. There is a small tributary that drains a pond north of Arrowhead Drive that drains through the site, and discharges to the Norwalk River approximately 480 feet north of the ASML driveway bridge over the Norwalk River. The proposed project begins approximately 290 feet north of the driveway bridge, and therefore the proposed improvements run parallel to the Norwalk River from the project beginning north to the confluence of the tributary, and then parallel to the tributary for approximately 300 feet, before entering a 150 curve toward the parking garage.

Immediately west of the site, there is a pond located west of the Metro North Railroad that discharges into a short channel beneath the railroad, and into the on-site drainage system. The proposed improvements are located outside the watershed of the pond and watercourse and will not have any adverse impact to that system.

### 2.1.3 Surface and Groundwater Quality Classifications

### 2.1.3.1 Surface Waters

CTDEEP classifies the unnamed tributary as Class A. Class A water designated uses are potential drinking water supply, fish and wildlife habitat, recreation use, agricultural and industrial supply and other legitimate uses including navigation. CTDEEP classifies the Norwalk River as Class B. Class B designated uses are habitat for fish and aquatic life and wildlife recreation navigation and industrial and agricultural water supply. The project's stormwater management measures have been designed in accordance with the 2004 Connecticut Stormwater Management Manual to improve the quality of stormwater discharge and to preserve the designated uses.

### 2.1.3.2 Groundwater

CTDEEP classifies the groundwater quality on the site. Class GA water designated uses include existing private supplies of water suitable for drinking without treatment, baseflow for hydraulically connected surface waterbodies. The project's stormwater management measures have been designed in accordance with the 2004 Connecticut Stormwater Management Manual to improve the quality of stormwater discharge and to preserve the designated uses.

### 2.1.4 Impaired Waterbodies

CTDEEP's 2020 Integrated Water Quality Report lists the Norwalk River as impaired. The impairments identified for the segment of the Norwalk River along the frontage of the site are bacteria and "other pollutant of concern". The cause of the impairment is listed as Escherichia coli, cause unknown. The impaired designated use is recreation, habitat for fish, other aquatic life and wildlife. The project proposed stormwater best management practices will improve the quality of the stormwater discharged from the site by encouraging infiltration and biological uptake through purposefully selected native plantings.

## **2.2 Precipitation Depths**

Precipitation depths for both existing and proposed conditions were computed from NOAA's Atlas 14 Point Precipitation Frequency Estimates online utility. The precipitation depths for a 24-hour duration storm at the project site are shown in **Table 2-1**.

# Table 2-124-Hour Duration Precipitation Depth (inches)

2-year	5-year	10-year	25-year	50-year	100-year
3.52	4.54	5.38	6.55	7.41	8.34

The precipitation output from the NOAA website is in **Appendix B**.

## 2.3 Existing Site Hydrologic Analysis

The project is located in the Norwalk River Mainstem Regional Drainage Subbasin.

The project location discharges into three directions, northwest from the garage, southwest toward the drainage system between the building and the parking garage, and east toward the Norwalk River corridor and the unnamed tributary, as shown in **Figure 10**.

Impervious and pervious areas, weighted curve numbers, and times of concentration were calculated for each watershed and entered into a hydraulic model to determine the project's peak flow as part of the comparative hydrology analysis. The hydrologic analysis was conducted using the Hydraflow Hydrographs modeling software, utilizing the Natural Resources Conservation Service (NRCS) Curve Number (CN) method.

A breakdown of watershed composite curve numbers, concentration times, and existing conditions volumetric hydrographs, are included in **Appendix C** of this report, respectively.

We selected the most downstream discharge point of the proposed improvements for peak flow comparison, which is located approximately 350 feet north of the ASML driveway bridge. Using the Hydraflow Hydrographs extension for Autodesk Civil 3D 2018, the peak flows of the site under existing and proposed conditions were calculated for both design points.

The results of the existing conditions are summarized in **Table 2-2**.

	Frequency (Years)						
Design Point	2	5	10	25	50	100	
EX-WS-01 Northwest	0.50	0.99	1.44	2.14	2.68	3.28	
EX-WS-02 Southwest	2.08	3.64	5.05	7.12	8.71	10.48	
EX-WS-03 Norwalk River	7.47	11.45	14.84	19.66	23.23	27.10	

# Table 2-2Existing Conditions Peak Flow Summary (cfs)

### 2.3.1 Existing Impervious Cover

The parking area north of the building is impervious cover that discharges untreated impervious cover to the river and tributary. Total impervious coverage on the site is 526,285 square feet.

## 2.4 Proposed Site Hydrologic Analysis

Stormwater runoff will generally follow the same drainage patterns, though the runoff from the portion of the driveway near the garage entrance will be directed to the east under proposed conditions. Runoff from the proposed improvements will be collected by a series of inlets and conveyed by storm drains.

Runoff from the portion of the driveway above the entrance to the north parking lot will be collected and sent to a two-cell stormwater pond. The upper cell of the pond overflows to a lower cell, which will discharge over a level spreader to the Norwalk River. The purpose of the two-cell system is to provide extended detention and stormwater treatment. Stormwater will be pretreated by a gross particle separator prior to discharge into the stormwater treatment pond.

Runoff from the lower driveway and the north parking lot will discharge into an underground stormwater infiltration chamber located under the north parking lot. Under existing conditions, the north parking lot discharges untreated to the Norwalk River via sheet flow, which has caused bank erosion. The project will repair some washouts. Stormwater will be pretreated by a gross particle separator prior to discharge into the stormwater treatment pond. Additionally, a portion of the runoff will discharge for treatment in a rain garden located between the driveway and the reconfigured parking lot.

The proposed treatment measures have been sized to meet the Water Quality Volume, and the gross particle separators have been sized for the Water Quality Flow volume. The proposed watershed map is shown in **Figure 11**.

The results of the proposed conditions peak flows are summarized in **Table 2-3**.

	Frequency (Years)							
Design Point	2	5	10	25	50	100		
EX-WS-01 Northwest	0.18	0.41	0.64	0.99	1.27	1.59		
EX-WS-02 Southwest	2.08	3.64	5.03	7.10	8.69	10.46		
EX-WS-03 Norwalk River	6.04	9.17	11.83	15.66	18.55	21.68		

# Table 2-3Proposed Conditions Peak Flow Summary (cfs)

A breakdown of watershed composite curve numbers, concentration times, and proposed conditions volumetric hydrographs, are included in **Appendix C** of this report, respectively.

### 2.4.1 Proposed Impervious Cover

The proposed improvements will add 14,788 square feet of impervious cover to the site as a result of the proposed driveway, of which 2,628 square feet within the regulated area.

Although impervious cover is increasing, the amount of Directly Connected Impervious Area will be reduced from existing conditions because of the new stormwater treatment measures. The decrease in directly connected impervious area is 36,319 square feet.

## 2.5 Comparative Hydrology

A summary of the existing and proposed peak runoff from the project area, is shown in **Table 2-4**.

#### Table 2-4

Comparison of Existing and Proposed Conditions Peak Flow, (cfs)

		Frequency (Years)						
Design Point	Condition	2	5	10	25	50	100	
	Existing	0.50	0.99	1.44	2.14	2.68	3.28	
<b>EX-WS-01</b> Northwest	Proposed	0.18	0.41	0.64	0.99	1.27	1.59	
	Change	♦ 64%	<b>↓</b> 58%	<b>↓</b> 55%	<b>↓</b> 53%	<b>↓</b> 52%	<b>↓</b> 51%	
	Existing	2.08	3.64	5.05	7.12	8.71	10.48	
EX-WS-02 Southwest	Proposed	2.08	3.64	5.03	7.10	8.69	10.46	
	Change	-	-	♦ 0.3%	♦ 0.2%	♦ 0.2%	♦ 0.1%	

Design Point	Condition	2	5	10	25	50	100
<b>EX-WS-03</b> Norwalk River	Existing	7.47	11.45	14.84	19.66	23.23	27.10
	Proposed	6.04	9.17	11.83	15.66	18.55	21.68
	Change	<b>↓</b> 19%	<b>↓</b> 19%	<b>↓</b> 20%	<b>↓</b> 20%	<b>↓</b> 20%	<b>↓</b> 20%

As shown in the Table above, the resulting total peak flows under proposed conditions are lower than the existing conditions in all three directions. Due to the proposed infiltration chambers, rain garden and stormwater management pond, there is an overall decrease in stormwater runoff to the Norwalk River. Runoff to the northwest is decreased because the total drainage area in that direction has been reduced. Runoff to the southwest is decreased due to a slight decrease in drainage area.

**Table 2-5** below compares the volume of discharge between existing and proposed conditions for all three directions, and shows a decrease in runoff volume in all three directions.

# Table 2-5Comparison of Existing and Proposed Conditions Volume, (cf)

Design Point	Condition	2	5	10	25	50	100
EX-WS-01 Northwest	Existing	2,842	5,059	7,138	10,310	12,797	15,598
	Proposed	947	1,816	2,659	3,973	5,021	6,215
	Change	<b>↓</b> 66%	<b>↓</b> 64%	<b>↓</b> 62%	<b>↓</b> 61%	♦ 60%	<b>↓</b> 60%
EX-WS-02 Southwest	Existing	9,176	15,288	20,846	29,137	35,530	42,658
	Proposed	9,127	15,223	20,770	29,047	35,433	42,553
	Change	♦ 0.5%	<b>↓</b> 0.4%	♦ 0.3%	♦ 0.3%	♦ 0.2%	♦ 0.2%
<b>EX-WS-03</b> Norwalk River	Existing	25,749	39,100	50,704	67,462	80,087	93,951
	Proposed	21,408	32,590	42,360	56,533	67,249	79,046
	Change	<b>↓</b> 16%	<b>↓</b> 16%	<b>↓</b> 16%	<b>↓</b> 16%	<b>↓</b> 16%	♦ 15%

## 2.6 Hydraulic Design

We analyzed the proposed storm drainage system to convey a 25-year storm without ponding, using the AutoCAD Civil 3D Hydraflow Storm Sewers Extension for the analysis. The first step in the analysis is to delineate the area contributing to each inlet of the system and then develop a runoff coefficient and time of concentration for each area. The inlet watershed computation worksheets appear in **Appendix D**. The contributing area to each inlet of the system is shown in **Figure 12**.

The results of the Storm Sewers Analysis also appear in **Appendix D**. The results show that the proposed storm sewer system is capable of conveying the 25-year storm event.

### 2.6.1 Starting Water Surface Elevation

The Norwalk River will exert a tailwater influence on any storm drainage system. In order to determine the appropriate tailwater for design, we utilized the Joint Probability Analysis Table in Chapter 8 of the CTDOT Drainage Manual. The procedure compares the watershed size of the site to the watercourse, and assigns a storm frequency for the watercourse tailwater based on the ratio. The storm system drainage area is 3.6 acres, while the watershed above is 18,624 acres, an area ratio greater than 1,000:1, therefore for a 25-year design on the stormwater conveyance system, a 2-year water surface elevation was used on the Norwalk River as the tailwater condition for the storm sewers analysis.

Since flow rates for the 2-year frequency are not published in the FIS, we estimated the 2-year discharge on the Norwalk River by plotting the discharge probability against the discharge and fitting a logarithmic best fit curve to the data to interpolate the discharge. We estimated 344 cfs using this method. As a check, we applied a Log-Pearson Distribution analysis for the USGS Stream Gauge downstream of the site at Kent Road, and then applied the USGS Transposition Equation to the results to obtain the flow rate at the site. Using this method, we obtained a 2-year discharge of 347 cfs, which is what we used in the existing condition HEC-RAS hydraulic model of the river to determine the corresponding water surface elevation for a 2-year event. The model computed a water surface elevation of 132.91 NGVD29, or approximately 131.91 NAVD88.

### 2.6.2 Outfall Energy Dissipation

The proposed outfalls will have a riprap energy dissipator. The dissipators have been designed in accordance with the CTDOT Drainage Manual, Chapter 11. The velocities under full at both outfalls are both less than 14 ft/s, and the discharges are both less than the maximum for a standard riprap apron. Please refer to the riprap sizing computations in **Appendix D**.

## 2.7 Stormwater Quality

### 2.7.1 Water Quality Volume and Water Quality Flow

The Water Quality Volume (WQV) for the area of the proposed improvements was calculated to be 6,711 cubic feet, based on the equation in Chapter 7 of the Connecticut Stormwater Quality Manual. The WQV will be provided by the proposed infiltration system.

Since we are proposing the use of a proprietary stormwater gross particle separator, the Water Quality Flow (WQF) is the appropriate measure to size the pretreatment practice. We are proposing three gross particle separators, with water quality flow requirements highlighted in **Table 2-6**.

System	WQF (cfs)	Unit Model
WQS-001, south inlet to infiltration system	0.336	CDS-2015-4-C
WQS-002, north inlet to infiltration system	0.355	CDS-2015-4-C
WQS-003, near outlet of main driveway drainage	0.401	CDS-2020-5-C

### Table 2-6 Water Quality Flow Summary

Please refer to the Water Quality Volume and Water Quality Flow computations in **Appendix E**.

### 2.7.2 Groundwater Recharge Volume

We computed a groundwater recharge volume of 1,662 cubic feet based upon the impervious area and the underlying soils, using the appropriate equation in the 2004 Connecticut Stormwater Quality Manual. The computed water quality volume is 6,711 cubic feet, which will be captured by the on-site retention system.

The development proposes an underground chamber system that will provide 15,555 cubic feet of storage, meeting the Groundwater Recharge Volume requirement and the requirement to retain the full water quality volume on the site.

### 2.7.3 Runoff Capture Volume

The Runoff Capture Volume only applies to new stormwater discharges within 500 feet of tidal wetlands which are not fresh-tidal wetlands. Since tidal wetlands do not exist on the site, the RCV is not required.

### 2.7.4 Stream Channel Protection

The Stream Channel Protection criterion in Section 7.6.1 of the CTSWQM does not apply to the project, as it meets one of the three exceptions, specifically, that the site discharges to a large river, fourth order or greater, where the development area is less than 5% of the watershed above. The project site is 0.02 percent of the watershed of the Norwalk River above the site, and the Norwalk River is a fifth order stream as it passes the site. Please refer to **Figure 13** for an analysis of the stream order.

### 2.7.5 Conveyance Protection

The project exceeds the Conveyance Protection criterion in Section 7.6.2 of the CTSWQM, which requires a 10-year conveyance design. The project proposes a 25-year design.

### 2.7.6 Peak Runoff Attenuation

The project meets the Peak Runoff Attenuation criterion in Section 7.6.3 of the CTSQWM, since peak runoff is reduced for all storms analyzed, principally through reduction of directly connected impervious coverage.

### 2.7.7 Emergency Outlet Sizing

The project has a stormwater pond and rain garden. Both features can pass the 100-year storm safely. The rain garden has an overflow grate set 6 inches above the bottom of the treatment measure, and the stormwater pond has a level spreader at its downstream end to allow runoff to discharge without overtopping.

### 2.7.8 Downstream Analysis

Section 7.6.5 of the CTSWQM requires routing computations downstream to a confluence point where the site drainage area represents 10 percent of the total drainage area. The site is only 0.02 percent of the watershed area of the Norwalk River, therefore, this criteria does not apply.

## 2.8 Stormwater Best Management Practices

The proposed Stormwater Management Plan is designed to meet Connecticut Department of Energy and Environmental Protection's (CTDEEP) goal of 80% removal of suspended solids from site stormwater discharge. Runoff from the proposed building roofs, driveways, sidewalks, and landscaped areas will be collected by a system of catch basins, drains, and pipes and will be routed through stormwater treatment practices before discharging from the site. Structures such as gross particle separators, infiltration systems, and storm drainage inlets will function to remove suspended solids and pollutants from stormwater runoff.

The on-site BMPs include:

### 2.8.1 Catch Basins with Sumps:

Catch basins are installed to have a two foot sump below the outlet pipe to collect sediment and debris. The installation of traps on the upstream-most structure on-site prevents the discharge of oil, floatable debris, and other pollutants into the Town storm drainage system.

### **2.8.2 Gross Particle Separators**

Gross particle separators are installed to remove grit, contaminated sediment, metals, hydrocarbons, and other floating fluids from surface runoff. Suspended sands, grit, and sediment in the stormwater runoff will be allowed to settle with the separator. Any suspended oils will rise to the surface within the separator, where they will be trapped.

This systems are designed for 80% removal of suspended solids. Under pre-existing conditions, no water quality systems were present, and runoff discharged untreated into the West River. In the proposed condition, runoff from the building and driveway will be treated by gross particle separators prior to discharge off-site. The gross particle separator has been located beneath the building but in an area with more vertical clearance to allow for maintenance.

### 2.8.3 Underground Infiltration Chambers

The underground infiltration chambers are intended to retain the water quality volume to meet the MS4 Permit requirements, and the groundwater recharge volume requirement. Stormwater entering the chambers will be pretreated by the gross particle separator to maximize the performance of the system.

We used default infiltration rates (Rawls, Brakensiek and Saxton, 1982) to compute the drawdown time for the proposed chambers, and estimated that they will drawdown within 48 hours.

### 2.8.4 Rain Gardens

A rain garden is proposed to treat the runoff from the north parking area. The plantings were selected by the project wetland scientist to promote biological uptake and pollutant renovation.

## 2.9 Pollutant Removal

Pollutant loadings for the existing and proposed conditions were calculated using the method prescribed by Debo and Reese in "Municipal Stormwater Management", 1995. This method determines the mass of pollutant loading by inputting the fraction of impervious area, the contributing area, the mean annual rainfall, and the event mean concentration of pollutant (EMC). The EMC is based upon the pollutant analyzed and the general characteristic of the contributing area – residential, commercial, or open space.

The area of proposed disturbance was chosen for the comparison of existing and proposed conditions. The pollutant loadings were calculated for existing and proposed conditions.

For the proposed conditions, the contributing area was further broken down into contributing areas to certain best management practices (BMPs). Pollutant loading reductions were taken at certain BMPs, depending upon the removal efficiency of the BMP as stated in the 2003 edition of Debo and Reese. Pollutant removal efficiencies for proprietary products were taken from data provided by the New Jersey Corporation for Advanced Technology. Based upon these pollutant reductions, we have determined that pollutant loadings will be less for the proposed conditions, as shown in **Table 2-7** below.

			Pollutant					
Item	Units	TKN	Р	TSS	Pb	Cu	Zn	
Infiltration System to EW-01								
Proposed, Pre Treatment	lb/yr	5.61	0.96	328.11	0.49	0.14	1.07	
Proposed, Post Treatment	lb/yr	0.00	0.00	0.00	0.00	0.00	0.00	
Reduction, Pre to Post Treat		100%	100%	100%	100%	100%	100%	
Upper Driveway to FE-01								
Proposed, Pre Treatment	lb/yr	12.72	2.17	743.51	1.12	0.31	2.44	
Proposed, Post Treatment	lb/yr	7.79	0.51	63.20	0.20	0.07	0.13	
Reduction, Pre to Post Treat		38.7%	76.5%	91.5%	82.3%	76.3%	94.6%	

#### Table 2-7 Pollutant Loading Summary

The pollutant loading calculations are presented in **Appendix E**.

The project will also reduce the salinity of water discharged under existing conditions, since the first flush from the parking lot will be treated by infiltration, and the runoff from the driveway will be treated in the proposed stormwater management pond. Currently, there is no treatment of the runoff from the parking lot.

## Section 3 Floodplain Management

## 3.1 Floodplain Management Overview

The Flood Insurance Study for Fairfield County, Connecticut, dated June 18, 2010, Panel No. 09001C0391F shows that there is a Special Flood Hazard Area, Zone AE and floodway associated with the Norwalk River.

The proposed driveway is located outside of the regulatory floodway, though a portion of the embankment near the first curve to the northwest are within the floodway. Portions of the driveway are within the regulatory floodplain, extending from the existing driveway bridge north to just east of the proposed northeast parking lot entrance.

Base flood (1% annual chance) elevations near the northeastern parking lot are approximately between elevations 140 and 141 NAVD88.

There are several requirements that the project will need to meet, the most significant of which are highlighted below:

### 3.1.1 No-Rise for Work within the Floodway

The Town of Wilton's floodplain management regulations, specified in Section 29-9.F.7.j requires that no encroachments, including fill, new construction, substantial improvements, and other developments shall be permitted unless certification (with supporting technical data) by a registered professional engineer is provided demonstrating through hydrologic and hydraulic analysis performed in accordance with standard engineering practices that the proposed encroachments shall not result in any (0.00 feet) increase in flood levels during occurrence of the base flood discharge. Our analysis indicates that there will no increase in the base flood elevation as a result of the proposed project.

### 3.1.2 Equal Conveyance

Section 29-9.F.7.k of the Town's floodplain management regulations requires that within the floodplain, except those areas which are tidally influenced, as designated on the flood insurance rate map (FIRM) for the community, encroachments resulting from filling, new construction or substantial improvements involving an increase in footprint of the structure, are prohibited unless the applicant provides certification by a registered professional engineer demonstrating, with supporting hydrologic and hydraulic analyses performed in accordance with standard engineering practices, that such encroachments shall not result in any (0.00 feet) increase in flood levels (base flood elevation). Work within the floodplain and the land adjacent to the floodplain, including work to provide compensatory storage shall not be constructed in such a way so as to cause an increase in flood stage or flood velocity. The project will not reduce conveyance based upon our computations and analysis.

### **3.1.3 Compensatory Storage**

Section 29.9-F.7.I of the Town's floodplain management regulations states that the water holding capacity of the floodplain, except those areas which are tidally influenced, shall not be reduced. Any reduction caused by filling, new construction or substantial improvements involving an increase in footprint to the structure, shall be compensated for by deepening and/or widening of the floodplain. Storage shall be provided on-site, unless easements have been gained from adjacent property owners; it shall be provided within the same hydraulic reach and a volume not previously used for flood storage; it shall be hydraulically comparable and incrementally equal to the theoretical volume of flood water at each elevation, up to and including the 100-year flood elevation, which would be displaced by the proposed project. Such compensatory volume shall have an unrestricted hydraulic connection to the same waterway or water body.

Within the floodplain, the proposed embankment adds 18 cubic yards of fill material within the floodplain, but the excavation for the proposed stormwater management basin above the elevation of the basin outlet's level spreader will result in 55 cubic yards of cut that are hydraulically connected to the floodplain. Therefore, the proposed project results in a net cut of material in the floodplain, increasing storage.

## 3.2 Comparison of Existing and Proposed Conditions

In order to determine the impact of the proposed project, and document compliance with the Town floodplain management regulations requiring that there will be no increase in the base flood elevation for the 100-year storm event, and no loss of storage or conveyance, we used the HEC-RAS model that was used for the river improvement project that was approved by the Town in 2013. Since the improvements have been completed, we used the as-built conditions HEC-RAS model from that project as the

HEC-RAS is a hydraulic modeling software developed by the U.S. Army Corps of Engineers, and is the primary modeling software used in FEMA's Flood Insurance Studies. HEC-RAS is the successor modeling system to USACE's HEC-2, which was used for older flood insurance studies.

### 3.2.1 Water Surface Elevations

We ran the model for existing conditions, and then modified the cross section impacted by the proposed improvements to reflect grading changes and changes in surface roughness. Under both models, we used a 100-year discharge of 7,455 cfs, which is the same discharge used in the Flood Insurance Study.

The model cross section locations are shown in Figure 14.

We compiled the results for the water surface elevations, and compared them in **Table 3-1**.

River Station	Existing WSEL (NGVD29)	Proposed WSEL (NGVD29)	Difference (ft)	Notes
29920	153.96	153.96	0.00	
29760	152.19	152.19	0.00	
28240	147.71	147.71	0.00	
27468	147.53	147.53	0.00	
27110	147.46	147.46	0.00	
27025	146.24	146.24	0.00	
27020				Substation Bridge
27015	146.08	146.08	0.00	
26680	142.89	142.89	0.00	
26209	143.04	143.04	0.00	
26136	142.10	142.10	0.00	
26127.5				Arrowhead Drive
26119	142.25	142.25	0.00	
26058	142.21	142.21	0.00	
25358	141.83	141.83	0.00	ASML Site, North End
25340	141.64	141.64	0.00	
25334	141.74	141.74	0.00	
24975	140.90	140.90	0.00	Project Area
24922	140.97	140.96	-0.01	Project Area
24677	140.94	140.94	0.00	
24620	140.48	140.48	0.00	
24597	140.63	140.63	0.00	
24570	139.43	139.43	0.00	
24542.5				ASML Driveway Bridge
24540	138.19	138.19	0.00	
24485	136.91	136.91	0.00	
24430	137.85	137.85	0.00	
24401	137.67	137.67	0.00	
24381	136.85	136.85	0.00	
24180	136.78	136.78	0.00	
24105	135.32	135.32	0.00	
23805	135.70	135.70	0.00	ASML Site, South End
23415	133.11	133.11	0.00	
23171	131.12	131.12	0.00	

# Table 3-1100-year Water Surface Elevation, Existing Model vs. Proposed

River Station	Existing WSEL (NGVD29)	Proposed WSEL (NGVD29)	Difference (ft)	Notes
23036	131.62	131.62	0.00	
22916	131.63	131.63	0.00	
22765	131.64	131.64	0.00	
22450	131.48	131.48	0.00	
22140	127.84	127.84	0.00	
21825	125.26	125.26	0.00	
21770	125.08	125.08	0.00	
21757.5				Kent Road
21745	124.39	124.39	0.00	
21695	124.15	124.15	0.00	
21285	124.30	124.30	0.00	Norwalk Town Line

# Table 3-1100-year Water Surface Elevation, Existing Model vs. Proposed

### 3.2.2 Velocities

We also ran the HEC-RAS model to compare the resultant velocities. There will be a very slight increase in velocity as a result of the project near the beginning of the project. However, the velocity increase is less than 1% and is therefore not expected to have an adverse impact on the stability of the river embankment.

# Table 3-2100-year Base Flood Velocities, Existing Model vs. Proposed

River Station	Existing Velocity (ft/s)	Proposed Velocity (ft/s)	Difference (ft/s)	Notes
29920	11.86	11.86	0.00	
29760	7.45	7.45	0.00	
28240	12.69	12.69	0.00	
27468	1.37	1.37	0.00	
27110	3.29	3.29	0.00	
27025	10.68	10.68	0.00	
27020				Substation Bridge
27015	11.26	11.26	0.00	
26680	10.6	10.59	0.00	
26209	2.70	2.70	0.00	
26136	9.59	9.59	0.00	
26127.5				Arrowhead Drive

River Station	Existing Velocity (ft/s)	Proposed Velocity (ft/s)	Difference (ft/s)	Notes
26119	5.04	5.04	0.00	
26058	5.08	5.07	-0.01	
25358	5.61	5.61	0.00	ASML Site, North End
25340	6.55	6.55	0.00	
25334	4.96	4.96	0.00	
24975	8.49	8.49	0.00	Project Area
24922	7.23	7.30	+ 0.07	Project Area
24677	5.44	5.44	0.00	
24620	7.78	7.78	0.00	
24597	6.38	6.38	0.00	
24570	10.31	10.31	0.00	
4542.5				ASML Driveway Bridge
24540	11.88	11.88	0.00	
24485	14.75	14.75	0.00	
24430	6.88	6.88	0.00	
24401	6.86	6.86	0.00	
24381	10.71	10.71	0.00	
24180	8.02	8.02	0.00	
24105	11.57	11.57	0.00	
23805	7.99	7.99	0.00	ASML Site, South End
23415	14.27	14.27	0.00	
23171	9.91	9.91	0.00	
3036	3.98	3.98	0.00	
22916	5.38	5.38	0.00	
22765	4.19	4.19	0.00	
2450	4.04	4.04	0.00	
22140	16.12	16.12	0.00	
21825	14.07	14.07	0.00	
21770	12.71	12.71	0.00	
1757.5				Kent Road
21745	13.75	13.75	0.00	
21695	13.66	13.66	0.00	
1285	8.42	8.42	0.00	Norwalk Town Line

# Table 3-2100-year Base Flood Velocities, Existing Model vs. Proposed

## **3.3 Floodplain Impacts**

Table 3-1 shows that the proposed improvements will not increase base flood elevations while Table 3-2 shows that the increase in velocity will be of no significant impact, since it is less than 1%. Therefore, the proposed project is complaint with the NFIP requirements as well as the requirements of the Town of Wilton.

Please refer to **Appendix G** for the HEC-RAS modeling results.

## Section 4 Wetlands and Watercourses

## 4.1 Overview

The Project design has been made to avoid impact when possible and to minimize and mitigate the impacts which are unavoidable to accomplish the Project.

Due to the nature of the project, complete avoidance of the Site's wetland and upland review areas is not possible. The Applicant proposes to minimize impacts to the greatest extent practicable. Impacts will be minimized through implementation of best management practices, including construction phasing.

Wetlands impacts are limited to 20 square feet, and involve the repair of existing eroded areas along the bank.

An analysis of the possible effects of unavoidable impacts is provided below.

## 4.2 Natural Diversity Communities

The Connecticut Department of Energy and Environmental Protection's Natural Diversity Database (NDDB) Map for the Town of Wilton, dated June 2021, shows no state endangered or threatened species on the site.

## 4.3 Aquifer Protection Areas

The proposed crossing is not located within any Aquifer Protection Area as identified by CTDEEP.

## 4.4 Floodplain Management

The Flood Insurance Study for Fairfield County, dated June 18, 2010 shows that there is a Special Flood Hazard Area, Zone AE and floodway associated with the Norwalk River. Refer to Section 3 of this report.

## 4.5 Wetland Identification

Raina Volovski, Professional Soils Scientist, of Tighe & Bond identified wetland soils and their boundaries, which were located by Arthur H. Howland & Associates, Inc.

## 4.6 Wetland Impacts

The project proposes a direct impact of 20 square feet to the wetlands to repair areas of erosion along the riverbank.

Upland review area impacts construction of the proposed driveway, walkway and associated grading, retaining walls, and stormwater infrastructure.

The project impacts are summarized in **Table 4-1**.

# Table 4-1Impact Summary within Project Limits

Disturbance sf	Disturbance ac
20	< 0.001
26,113	0.599
22,080	0.506
4,033	0.092
	<b>sf</b> 20 26,113 22,080

## 4.7 Alternatives Assessment

The proposed activity within the riparian corridor represents the most feasible and prudent alternative considered with the least amount of environmental impact.

### 4.7.1 No-Build

The no-build alternative would not address the safety challenges the current site experiences with traffic flow, and is therefore neither prudent or feasible.

### 4.7.2 Conducting the Activity in a Different Location

The proposed activity requires separation of truck and delivery traffic from employee traffic. The route left from the driveway bridge is constrained, having choke points at the southeast corner of the building due to the proximity of the river, and along the west side of the building due to the railroad.

Routing traffic along the north side of the building would be challenging because of all the support equipment such as power equipment and storage tanks that are located in the narrow corridor between the north face of the building and the hillside. Therefore, the driveway alignment over the hillside is the only location where the driveway can be constructed and meet the project traffic safety objectives.

### 4.7.3 Alternatives Considered

The project evolved through several alternatives before the current proposal was selected by ASML. Please refer to the supporting figures in **Appendix H**.

### 4.7.3.1 Alternative 1: 9% Grade, Alignment A

The Town of Wilton allows driveway grades of up to 10%. Alternative 1 was the initial layout based upon concept drawings provided by ASML. Alternative 1 explores a driveway at a 9% grade, and preservation of as many parking spaces north of the building as possible. The alignment brought the edge of the driveway 5 feet from the adjacent wetlands, and left little room for stormwater management facilities. The alignment also featured a series of "broken back" curves, which are also undesirable.

A large paved turnaround for emergency vehicles in front of the garage is also provided.

### 4.7.3.2 Alternative 2: 9% Grade, Alignment B

Alternative 1 brough the roadway too close to the wetlands and didn't provide enough room for stormwater management. Alternative 2 kept the driveway grade at 9%, but adjusted the alignment to increase the separation distance from the wetlands, and to better align the curves and the approach to the parking garage. Minimum separation distance to the wetlands increased to 21 feet.

The improved alignment allows more room for stormwater management features, though it removes more parking spaces from the north lot. Additionally, the areas of existing parking closest to the wetlands will be removed, including the gravel parking area that is only 4 feet from the wetlands. At that point, the proposed sidewalk along the east side of the new driveway will be 41 feet from the wetland boundary.

Alternative 2 also reconfigures the parking lot, providing a turnaround area for vehicles that are denied entry. Alternative 2 also retains the paved turnaround for emergency vehicles in front of the garage.

### 4.7.3.3 Alternative 3: 10% Grade, Alignment B

Alternative 3 is a permutation of Alternative 2, using the steeper alignment, but increasing the grade to 10 percent. The intent was to explore the grading impacts of using a steeper grade, which would reduce earthwork, but our analysis showed that the increase was not significant to warrant a steeper driveway, as tiered rock slopes / retaining walls would still be required, as would the retaining wall near the beginning of the site driveway.

#### 4.7.3.4 Alternative 4: 6% Grade, Alignment C

Alternative 4 uses a slightly different alignment than Alternative 3, taking a more direct route up the hillside than Alternative 3. The alignment is similar to the south end of the alignment used in Alternative 4, but diverges from Alignment B as it climbs the slope. The minimum separation to the wetlands is the same as Alignment B. Alternative 4 is at a 6% grade, and results in additional retaining walls on the east side as it approaches the garage.

#### 4.7.3.5 Alternative 5 – 8% Grade, Alignment B

Alternative 5 follows Alignment B, which was used in Alternatives 2 and 3, and is on an 8% grade. Although there is more earthwork, the retaining wall configuration remains the same as Alternatives 2 and 3, the earthwork isn't substantially different, and provides a less steep driveway.

### 4.7.3.6 Alternative 6 – 7% Grade, Alignment B

Alternative 6 also follows Alignment B, but at a 7% grade. There is additional cut, but the configuration of walls is similar to Alternatives 2, 3, and 6. 7% is the maximum grade the Town allows without additional special consideration under its Zoning Regulations.

### 4.7.3.7 Alternative 7 – 10% Grade, Alignment D

Alternative 7 is on a new alignment that would connect to the parking area at grade level near the garage as opposed to between the third and fourth levels. Although this would

provide a minimum 35 foot separation from the wetlands, it would also require up to a 60 foot cut into the hillside, essentially creating a trench through the hillside, which would generate an enormous amount of earthwork, therefore, this alternative was not considered feasible or prudent.

### 4.7.3.8 Alternative 8, 7% Grade, Alignment E

Alternative 8 is the project proposal. It is a further refinement of Alternates 1 through 6. The alignment was adjusted to increase the minimum separation distance from the wetlands to 23 feet. It also eliminates the two turnarounds, and instead relies upon reinforced turf for vehicle turning movements.

## Section 5 Sedimentation & Erosion Control

## **5.1 Erosion Control Narrative**

The stormwater management measures will address the stormwater quality once the site has been constructed and stabilized. Sedimentation and erosion control measures will be installed during construction which will minimize adverse impacts from construction activities.

All sedimentation and erosion control measures proposed for this development have been designed in accordance with the "2002 Connecticut Guidelines for Soil Erosion and Sedimentation Control" as published by the Connecticut Council on Soil Erosion and Water Conservation. Additional guidelines have also been followed that are available from the Connecticut Department of Energy and Environmental Protection as recommended for sedimentation control during construction activities.

### 5.1.1. General

- 1. The proposed development is entitled "ASML Campus Traffic Safety Improvements" in Wilton, Connecticut.
- Estimated
   Project Start: Fall 2022
   Project Completion: Spring 2023
- 3. Erosion Control Narrative refers to Drawings C600 to C610
- 4. The Site is located at 77 Danbury Road, Wilton, Connecticut.

### 5.1.2 Construction Sequence

### 5.1.2.1 Phase 1

- 1. Hold pre-construction meeting with design team and the Town's Environmental Affairs Director to discuss the sequence of operations and the sediment and erosion controls.
- 2. Install silt fence and straw wattles along riparian corridor.
- 3. Install silt sacks at catch basins
- 4. Post signage at driveway bridge directing all traffic to turn left, except construction vehicles.
- 5. Install construction entrance
- 6. Excavate Temporary Sediment Trap

### 5.1.2.2 Phase 2

- 1. Maintain and replenish/replace controls from Phase 1.
- 2. Construct lower retaining wall
- 3. Rough grade lower section of roadway
- 4. Excavate up the hillside to create haul road access to the top of the ridge.
- 5. Place some of the rock removed on the down slope side of the haul road fill to armor the slope,
- 6. Install lowest portion of drainage system.
- 7. Protect basin inlets with silt sacks.
- 8. Protect headwall inlet with stone check dam.

### 5.1.2.3 Phase 3

- 1. Maintain and replenish/replace controls from Phase 2.
- 2. Install sediment and erosion controls near parking garage.
- 3. Excavate eastern portion of driveway and rough grade, constructing rock cuts and walls.
- 4. Construct riprap swale above walls.
- 5. Install drainage system.
- 6. Protect new catch basins with silt sacks.

### 5.1.2.4 Phase 4

- 1. Maintain and replenish/replace controls from Phase 3.
- 2. Construct retaining walls near parking garage.
- 3. Make structural modifications to parking garage for new entrance.
- 4. Install uppermost catch basins of driveway drainage system.
- 5. Protect new catch basins with silt sacks.

### 5.1.2.5 Phase 5

- 1. Rough grade parking lot.
- 2. Install parking lot drainage, rain garden and infiltration system.
- 3. Construct sidewalks, reinforced turf areas, and other appurtenances.

- 4. Construct stormwater management basin and retaining wall.
- 5. Pave parking area and driveway.
- 6. Establish turf and stabilize.
- 7. Remove erosion controls.

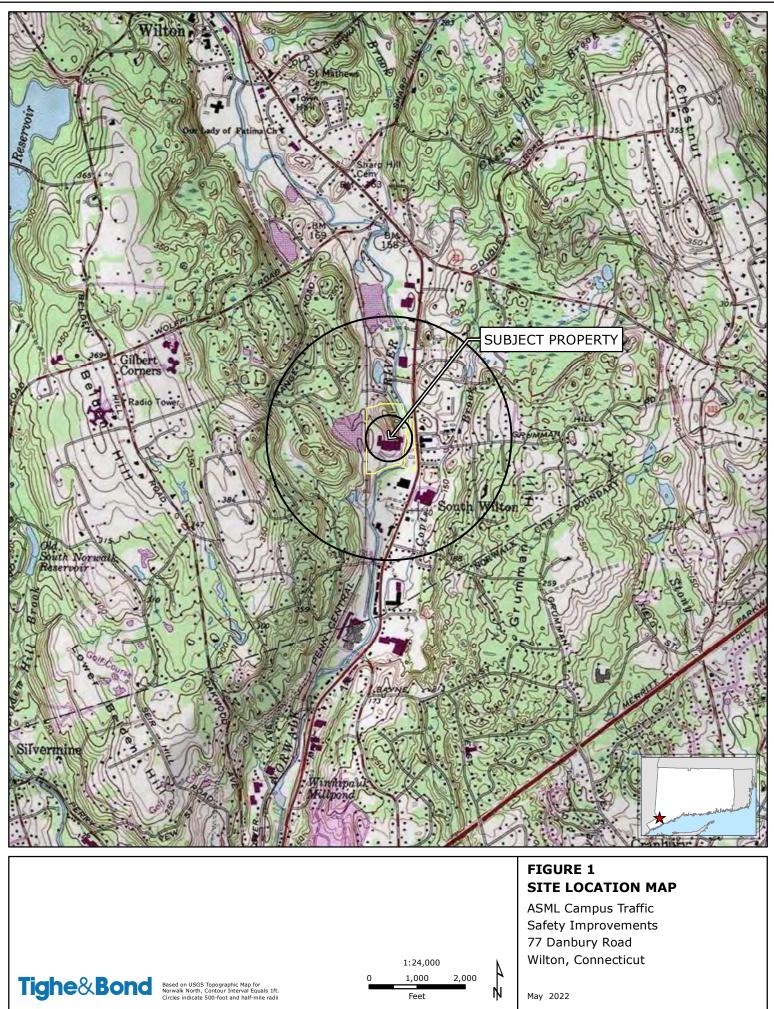
### **5.2 Erosion Control Notes**

- 1. All sedimentation and erosion control measures shall be constructed in accordance with the standards and specifications of the "2002 Connecticut Guidelines for Soil Erosion and Sediment Control", DEP Bulletin No. 34, and all amendments and addenda thereto as published by the Connecticut Department of Environmental Protection.
- 2. Land disturbance shall be kept to the minimum necessary for construction operations.
- 3. Install all erosion control measures as shown on the plan and elsewhere as ordered by the Engineer or the City.
- 4. Protect all catch basins with a silt sacks, haybale ring, silt fence or block and stone inlet protection throughout the construction period and until all disturbed areas are thoroughly stabilized.
- 5. Whenever possible, install erosion and sediment control measures prior to construction. See "Erosion Control Narrative".
- 6. Install additional control measures during the construction period as ordered by the Engineer.
- 7. Maintain all sedimentation and erosion control measures in effective condition throughout the construction period.
- 8. Sediment removed shall be disposed of off-site or in a manner as required by the Engineer
- 9. The construction contractor shall be responsible for construction and maintenance of all control measures throughout the construction period.
- 10. Protect all disturbed areas exposed for more than 30 days with a temporary vegetative cover. Seed these areas with perennial ryegrass at the rate of 40 lbs. per acre (1 lb. per 1,000 sq. ft). Apply soil amendments and mulch as required to establish a uniform stand of vegetation over all disturbed areas.
- 11. The construction contractor shall utilize approved methods/materials for preventing the blowing and movement of dust from exposed soil surfaces onto adjacent properties and site areas.

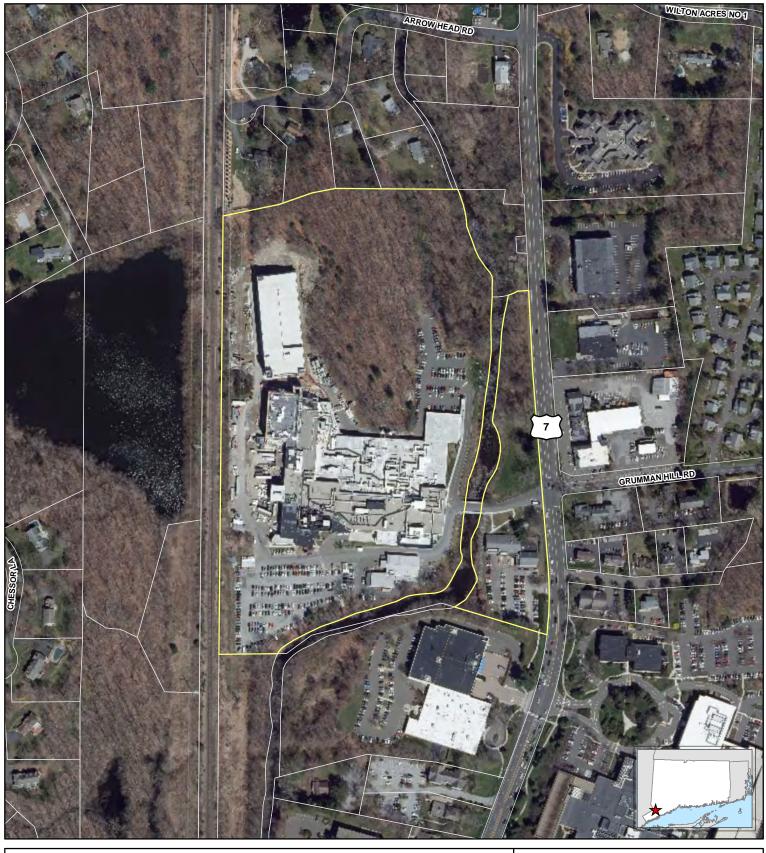
- 12. The construction contractor shall maintain a supply of silt fence/haybales and antitracking crushed stone on site for emergency repairs.
- 13. The contractor shall inspect weekly at a minimum, and before all forecasted storms all drainage structures and clean them as needed to prevent the build-up of silt.
- 14. The construction contractor shall carefully coordinate the placement of erosion control measures with the phasing of construction.
- 15. Keep all paved roadways clean. Sweep the driveways used for construction access before forecasted storms. Sweep adjacent roadways as warranted.
- 16. Treat all unpaved surfaces with 4" minimum of topsoil prior to final stabilization.
- 17. Install haybale barriers and silt fencing along the toe of critical cut and fill slopes.
- 18. The contractor shall notify the Town of Wilton Environmental Official prior to the installation of erosion controls, cutting of trees, or any excavation.
- 19. Cover all trucks leaving the site.
- 20. Check all sedimentation and erosion controls weekly and/or after each rainfall event. Make necessary repairs immediately.
- 21. Inspect and repair erosion and sediment controls prior to forecasted rain events.
- 22. Remove erosion controls when all disturbed areas have been stabilized and the city has provided authorization. Disturbed areas shall be seeded and mulched.

## **5.3 Engineered Controls**

The proposed stormwater basin will function as a temporary sediment trap during construction. The trap was sized in accordance with the criteria in the 2002 Connecticut Erosion and Sediment Control Guidelines. The trap will be reshaped, cleaned, restored and planted prior to project completion. Please refer to computations in **Appendix I**.



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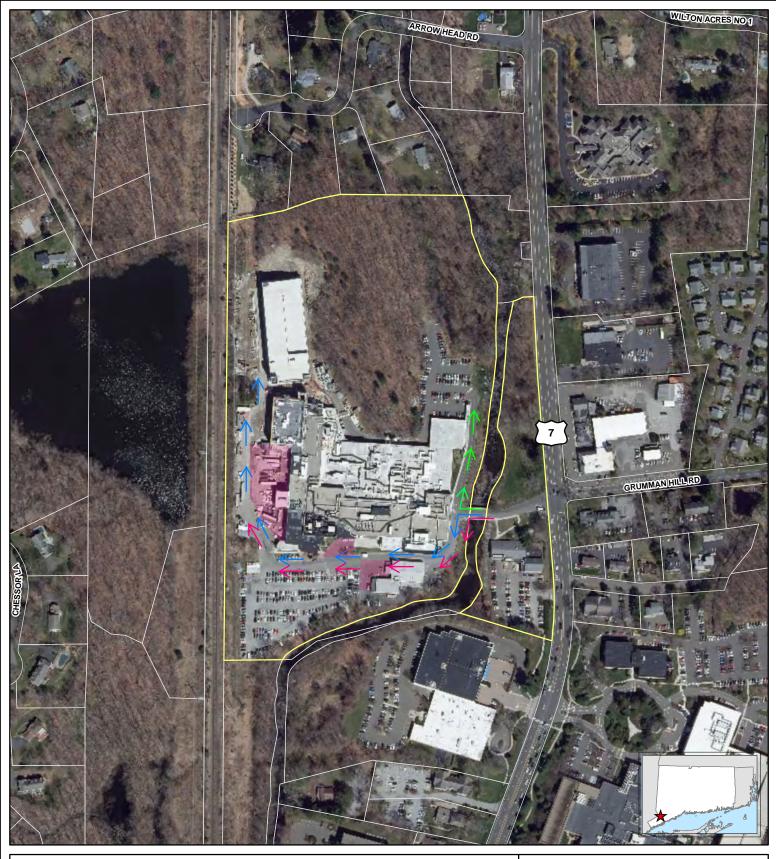




### FIGURE 2 ORTHOPHOTOGRAPH

ASML Campus Traffic Safety Improvements 77 Danbury Road Wilton, Connecticut

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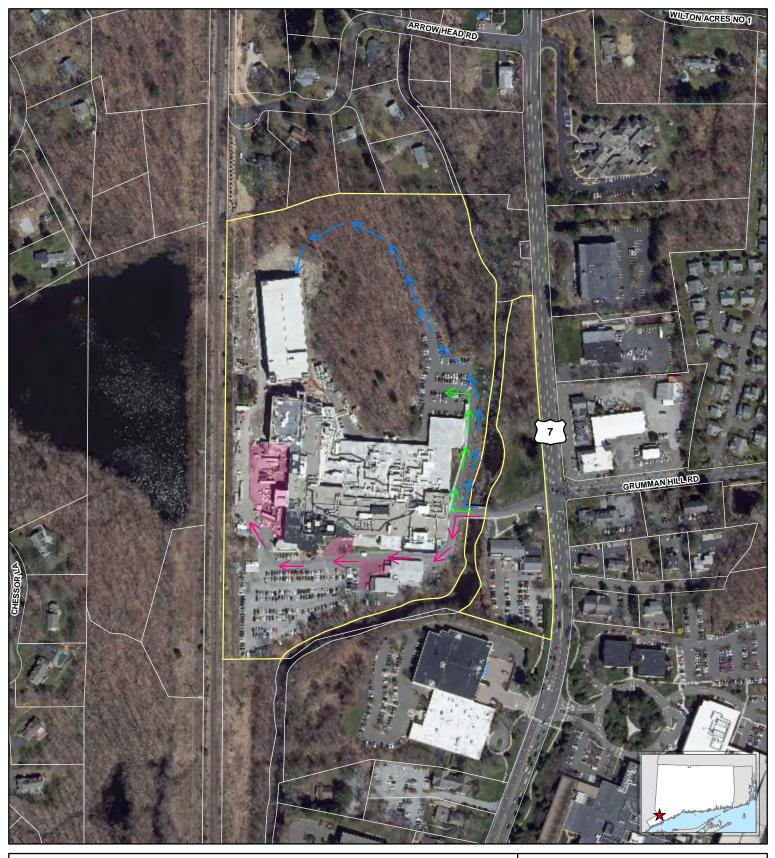




### FIGURE 3 EXISTING TRAFFIC FLOW

ASML Campus Traffic Safety Improvements 77 Danbury Road Wilton, Connecticut

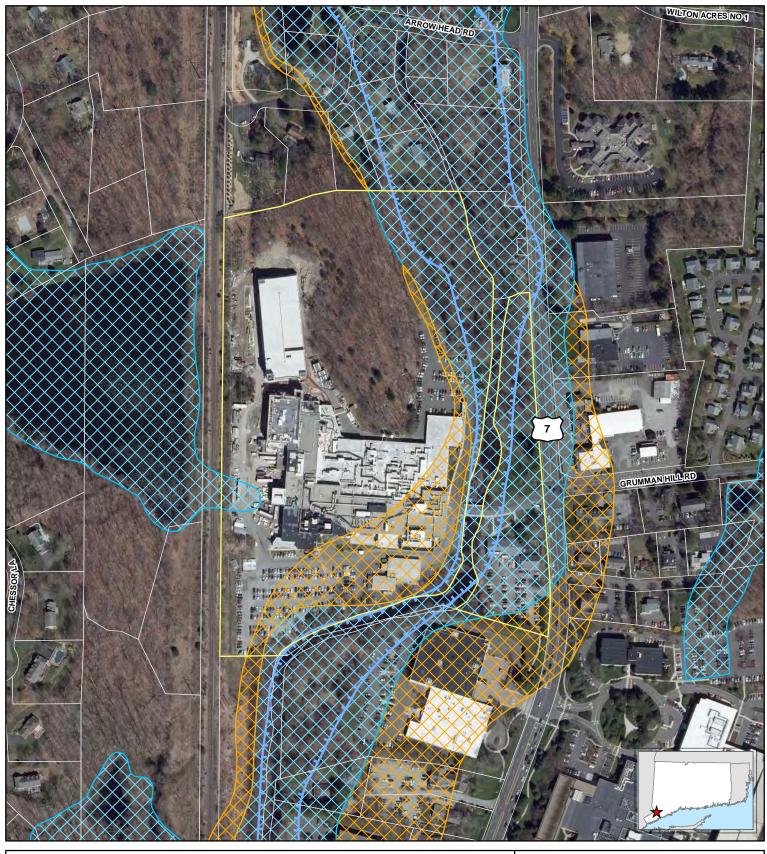
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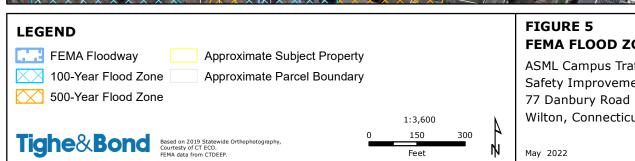




#### FIGURE 4 PROPOSED TRAFFIC FLOW

ASML Campus Traffic Safety Improvements 77 Danbury Road Wilton, Connecticut

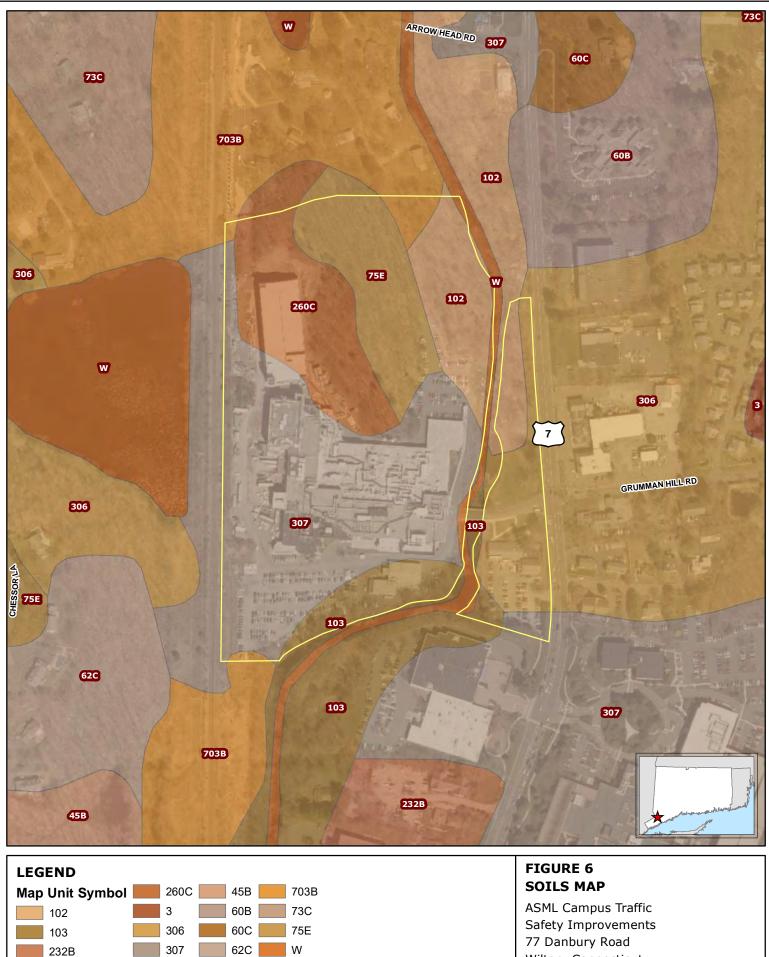




## **FEMA FLOOD ZONES**

ASML Campus Traffic Safety Improvements Wilton, Connecticut

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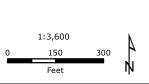
 Source:

 Based on 2019 Statewide Leaf-Off Orthophotography,

 Courtesty of CTECO.

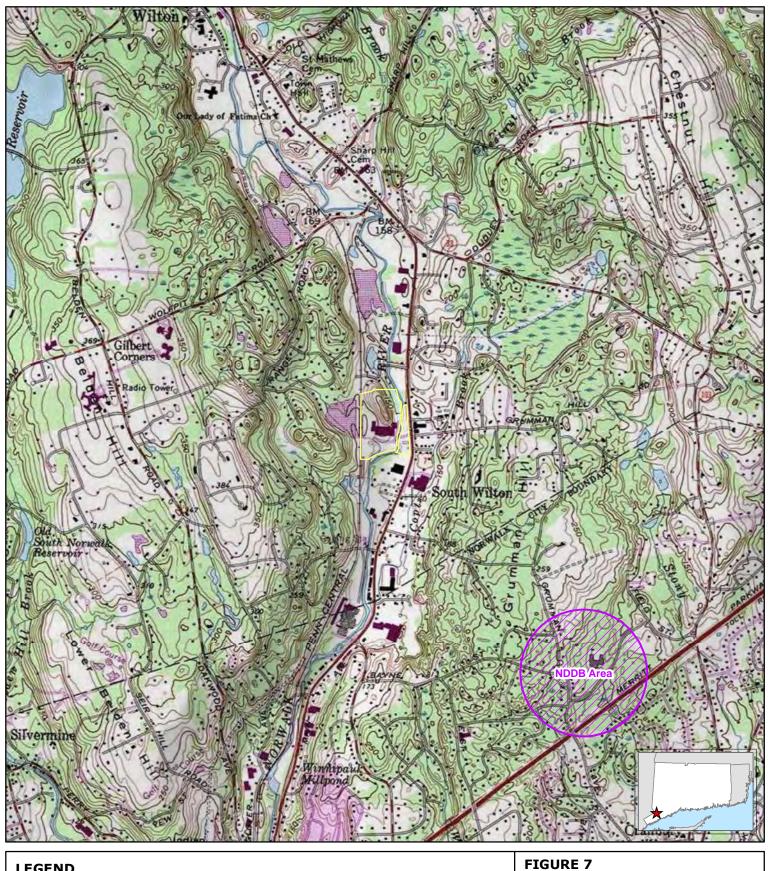
 Soil Boundary data obtained from the United States Department of Apriculture Natural Resources Conservation Service (NRCS; http://soildatamart.nrs.usda.gov/).

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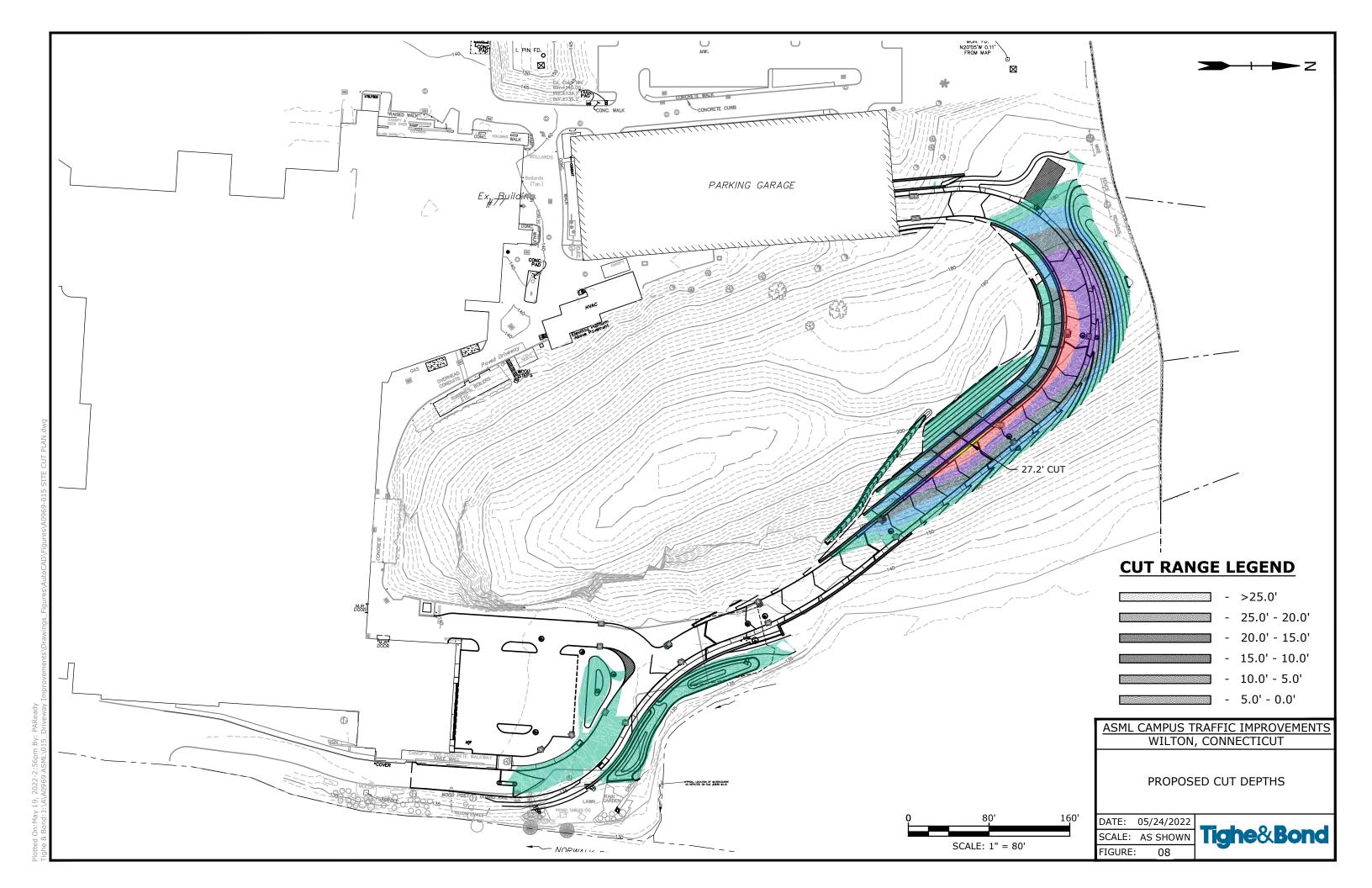
Wilton, Connecticut

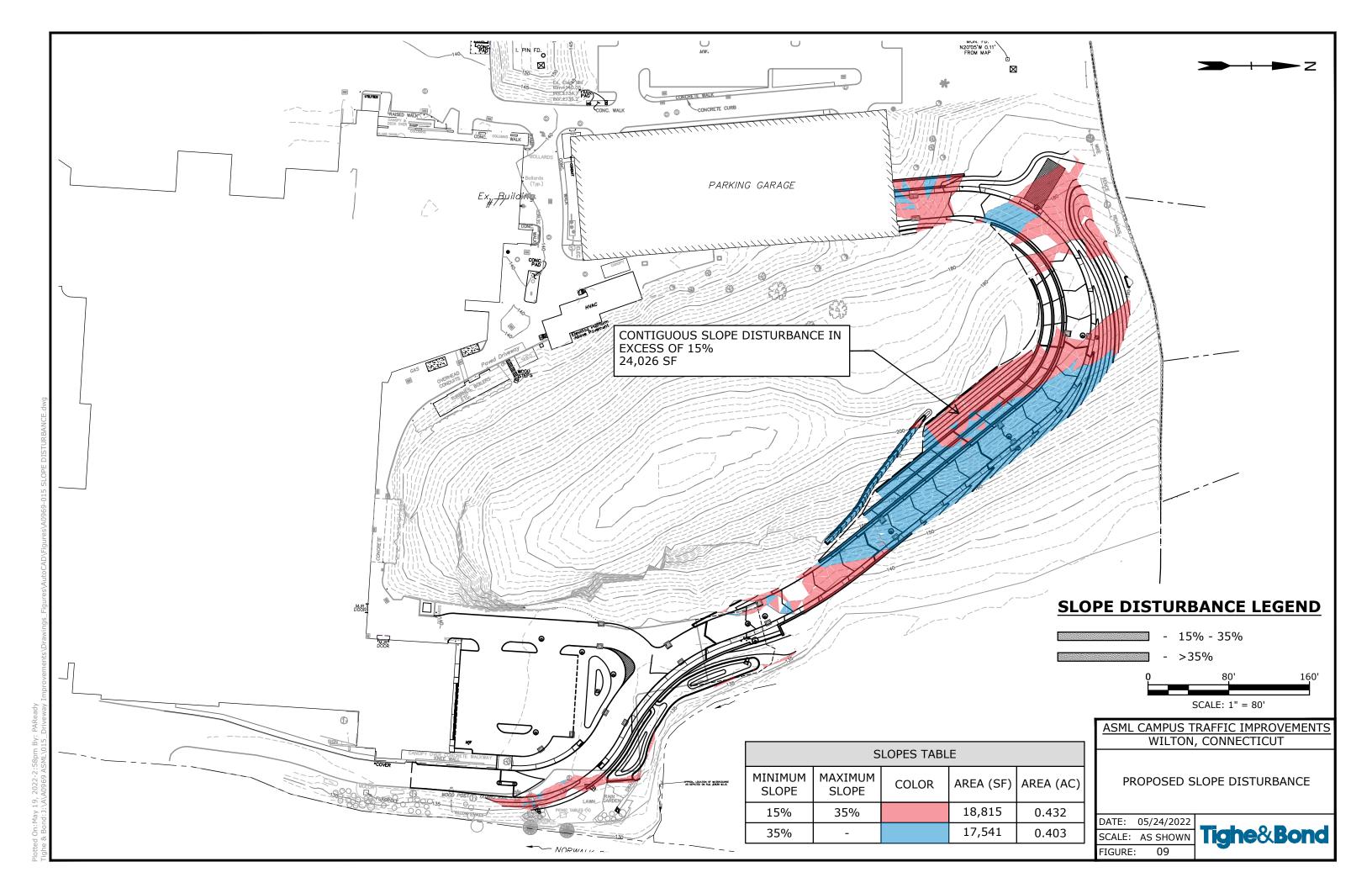
May 2022



#### LEGEND **NDDB AREA** Natural Diversity Database Area (Dec 2021) ASML Campus Traffic Approximate Subject Property Safety Improvements 77 Danbury Road Wilton, Connecticut 1:24,000 Δ 1,000 2,000 Tighe&Bond Based on 2019 Statewide Orthophotography, Courtesty of CT ECO. NDDB data from CTDEEP. Ŵ May 2022 Feet

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## LEGEND

WATERSHED BOUNDARY Tc PATH IMPERVIOUS, BLDG IMPERVIOUS, CONC IMPERVIOUS, PAVEMENT IMPERVIOUS, ROCK GRAVEL WOODS, HSG B WOODS, HSG D LANDSCAPE, HSG B

CAMPUS TRAFFIC FLOW SAFETY IMPROVEMENTS WILTON, CT

## EXISTING CONDITIONS WATERSHED MAP

DATE: 05/20/2022 FIGURE: 10

SCALE: AS SHOWN Tighe&Bond

► Z

160'



PR-WS-01

## LEGEND

WATERSHED BOUNDARY Tc PATH IMPERVIOUS, BLDG IMPERVIOUS, CONC IMPERVIOUS, PAVEMENT IMPERVIOUS, ROCK GRAVEL WOODS, HSG B WOODS, HSG D LANDSCAPE, HSG B

CAMPUS TRAFFIC FLOW SAFETY IMPROVEMENTS WILTON, CT

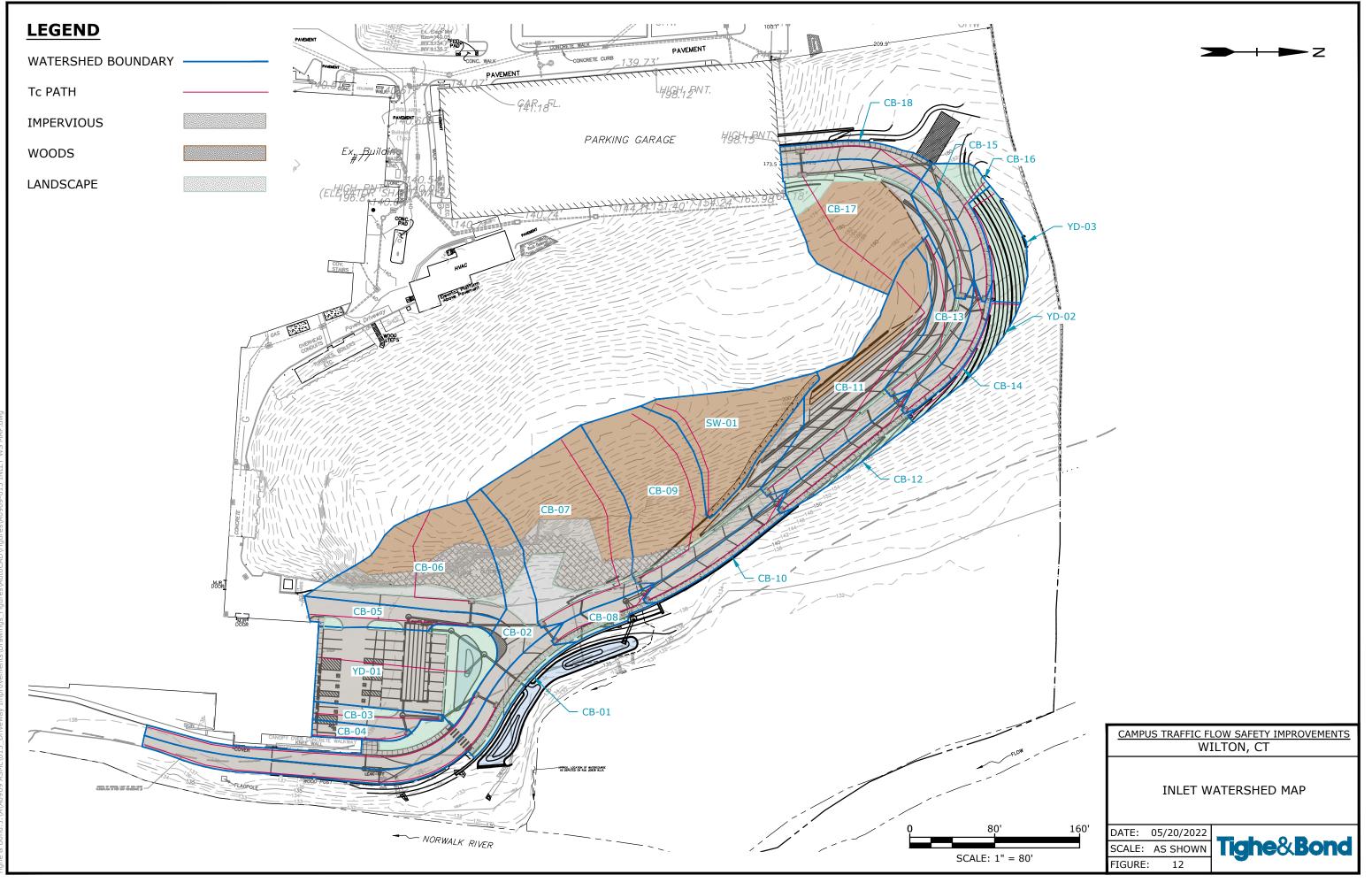
#### PROPOSED CONDITIONS WATERSHED MAP

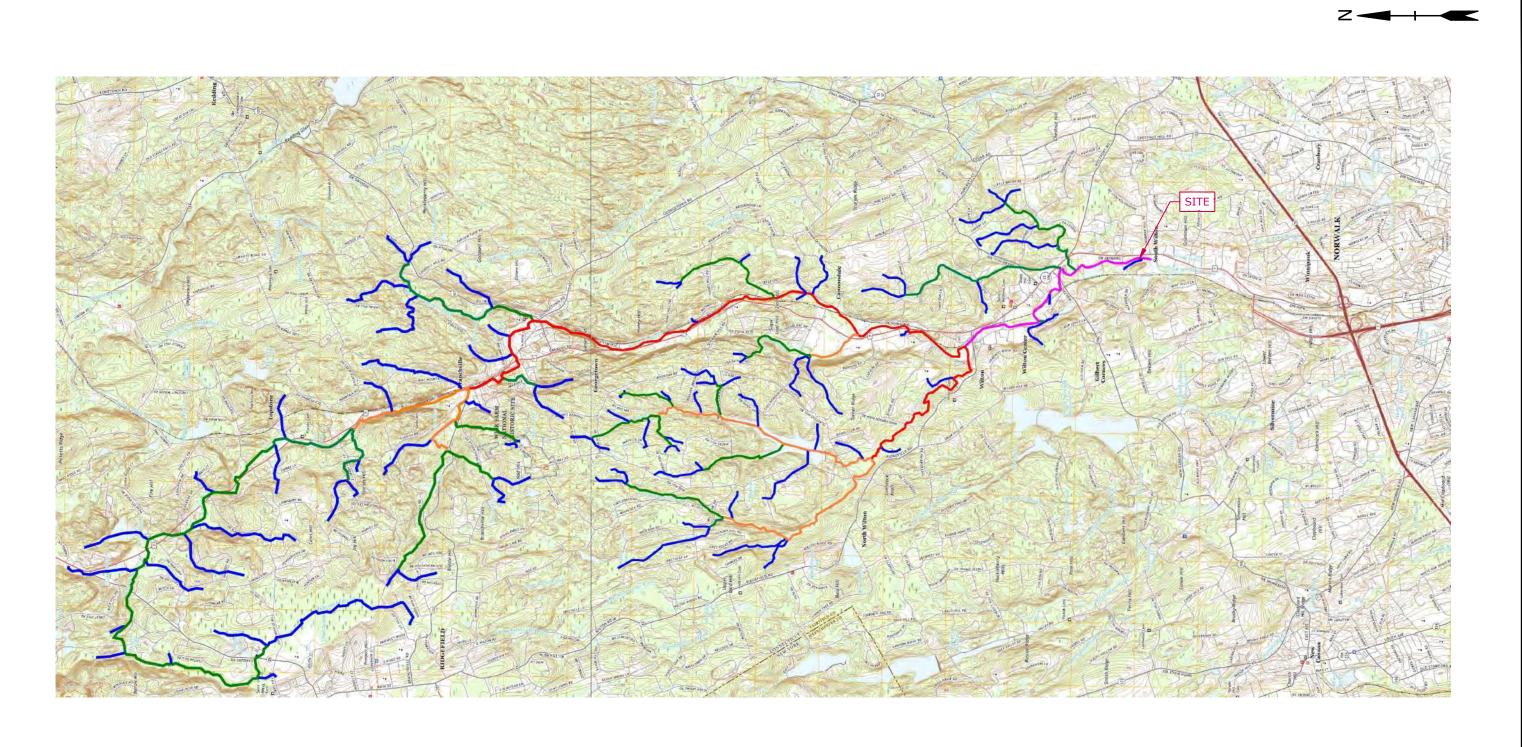
DATE: 05/20/2022 FIGURE: 11

SCALE: AS SHOWN Tighe&Bond

► Z

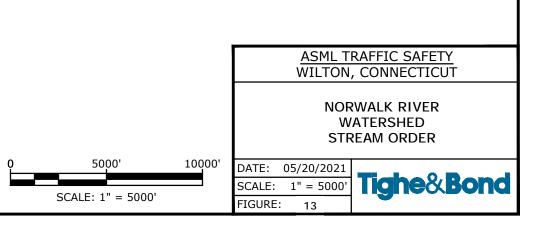
160'

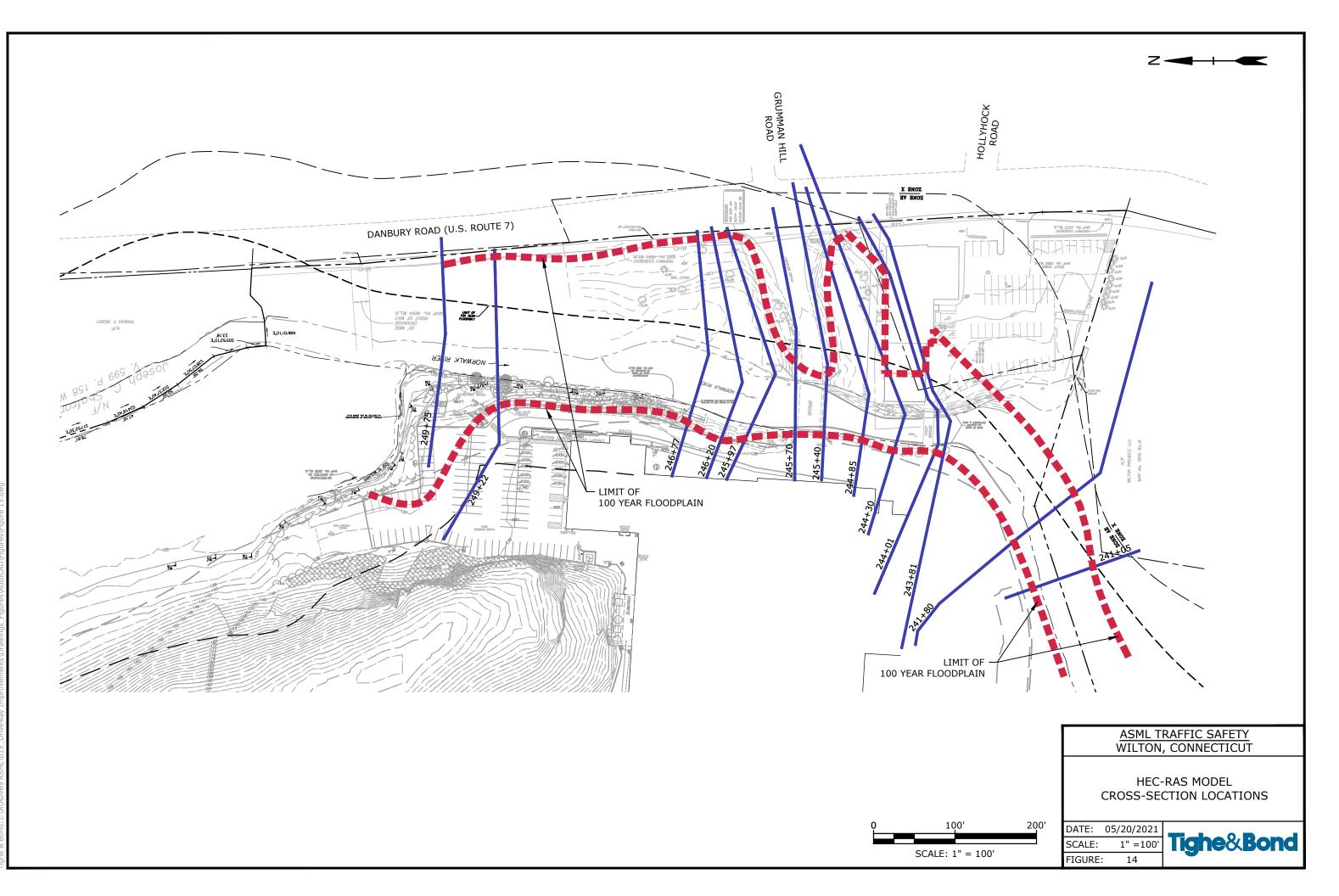




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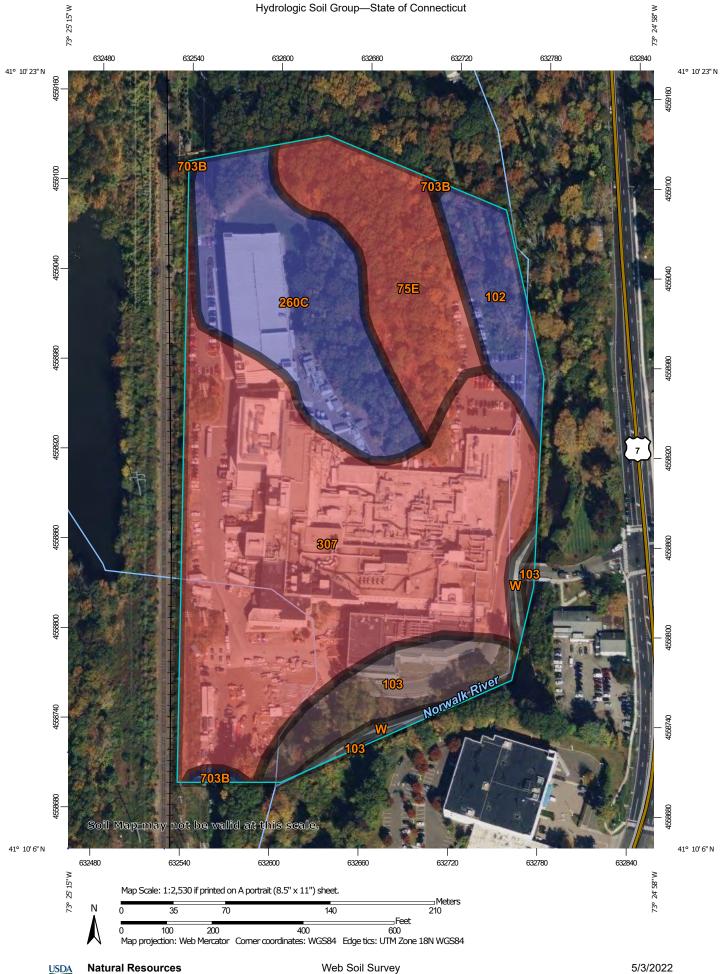
- FIRST ORDER STREAM
- SECOND ORDER STREAM
- THIRD ORDER STREAM
- FOURTH ORDER STREAM
- FIFTH ORDER STREAM





# **Tighe&Bond**

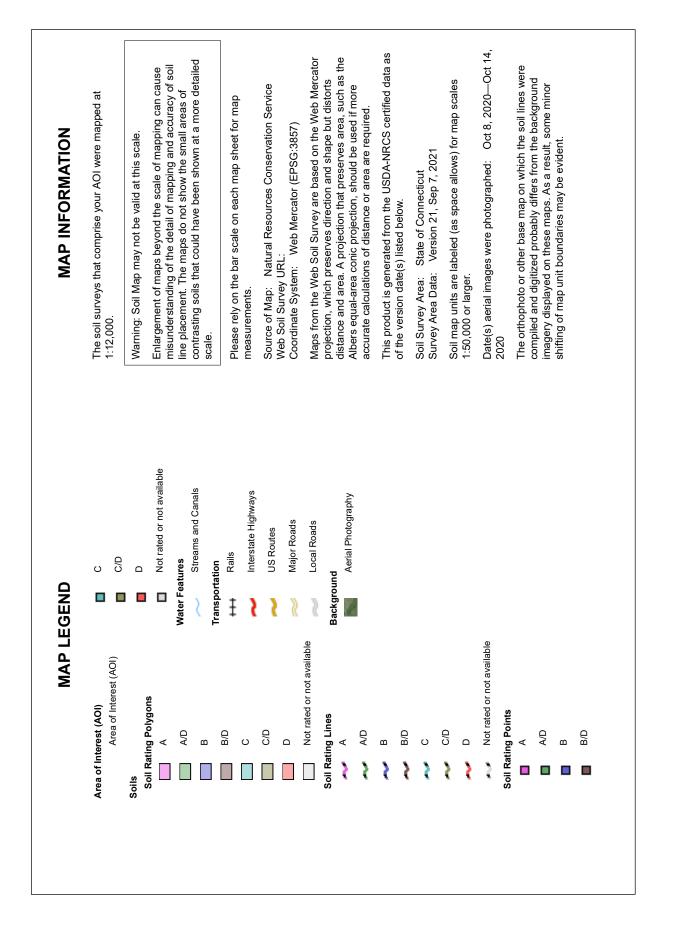
**APPENDIX A** 



Page 1 of 4

Conservation Service

Web Soil Survey National Cooperative Soil Survey Hydrologic Soil Group—State of Connecticut



Web Soil Survey National Cooperative Soil Survey

Natural Resources Conservation Service

NSDA

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
75E	Hollis-Chatfield-Rock outcrop complex, 15 to 45 percent slopes	D	3.1	14.0%
102	Pootatuck fine sandy loam	В	1.4	6.3%
103	Rippowam fine sandy loam	B/D	1.8	8.0%
260C	Charlton-Urban land complex, 8 to 15 percent slopes	В	4.2	19.0%
307	Urban land	D	11.4	50.8%
703B	Haven silt loam, 3 to 8 percent slopes	В	0.1	0.4%
W	Water		0.3	1.4%
Totals for Area of Inter	rest	22.4	100.0%	

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

# **Tighe&Bond**

**APPENDIX B** 

Precipitation Frequency Data Server



NOAA Atlas 14, Volume 10, Version 3 Location name: Wilton, Connecticut, USA\* Latitude: 41.1708°, Longitude: -73.4183° Elevation: 164 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

#### **PF** tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>									
Duration				Average	recurrence	interval (ye	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.365</b> (0.286-0.461)	<b>0.425</b> (0.333-0.537)	<b>0.523</b> (0.408-0.663)	<b>0.604</b> (0.468-0.770)	<b>0.716</b> (0.536-0.946)	<b>0.801</b> (0.586-1.08)	<b>0.888</b> (0.629-1.23)	<b>0.981</b> (0.662-1.40)	<b>1.11</b> (0.719-1.63)	<b>1.21</b> (0.766-1.82)
10-min	<b>0.518</b> (0.405-0.654)	<b>0.602</b> (0.471-0.761)	<b>0.740</b> (0.577-0.938)	<b>0.855</b> (0.664-1.09)	<b>1.01</b> (0.759-1.34)	<b>1.14</b> (0.831-1.53)	<b>1.26</b> (0.892-1.75)	<b>1.39</b> (0.938-1.98)	<b>1.57</b> (1.02-2.31)	<b>1.71</b> (1.09-2.57)
15-min	<b>0.609</b> (0.477-0.769)	<b>0.709</b> (0.555-0.896)	<b>0.872</b> (0.680-1.11)	<b>1.01</b> (0.781-1.28)	<b>1.19</b> (0.894-1.58)	<b>1.34</b> (0.977-1.80)	<b>1.48</b> (1.05-2.06)	<b>1.64</b> (1.10-2.33)	<b>1.85</b> (1.20-2.72)	<b>2.02</b> (1.28-3.03)
30-min	<b>0.849</b> (0.665-1.07)	<b>0.987</b> (0.772-1.25)	<b>1.21</b> (0.946-1.54)	<b>1.40</b> (1.09-1.78)	<b>1.66</b> (1.24-2.19)	<b>1.86</b> (1.36-2.49)	<b>2.06</b> (1.45-2.84)	<b>2.26</b> (1.53-3.22)	<b>2.53</b> (1.65-3.73)	<b>2.74</b> (1.74-4.12)
60-min	<b>1.09</b> (0.853-1.38)	<b>1.26</b> (0.990-1.60)	<b>1.55</b> (1.21-1.97)	<b>1.79</b> (1.39-2.29)	<b>2.12</b> (1.59-2.80)	<b>2.38</b> (1.74-3.19)	<b>2.63</b> (1.85-3.63)	<b>2.88</b> (1.95-4.11)	<b>3.22</b> (2.09-4.73)	<b>3.47</b> (2.19-5.21)
2-hr	<b>1.39</b> (1.10-1.75)	<b>1.64</b> (1.29-2.06)	<b>2.05</b> (1.61-2.59)	<b>2.39</b> (1.87-3.03)	<b>2.86</b> (2.16-3.76)	<b>3.22</b> (2.37-4.31)	<b>3.58</b> (2.56-4.96)	<b>3.98</b> (2.70-5.64)	<b>4.54</b> (2.96-6.64)	<b>4.99</b> (3.17-7.44)
3-hr	<b>1.60</b> (1.26-2.00)	<b>1.90</b> (1.50-2.38)	<b>2.39</b> (1.89-3.00)	<b>2.80</b> (2.19-3.54)	<b>3.37</b> (2.55-4.42)	<b>3.79</b> (2.81-5.08)	<b>4.24</b> (3.04-5.87)	<b>4.74</b> (3.21-6.69)	<b>5.45</b> (3.55-7.95)	<b>6.03</b> (3.84-8.96)
6-hr	<b>2.01</b> (1.60-2.50)	<b>2.41</b> (1.92-2.99)	<b>3.06</b> (2.42-3.81)	<b>3.60</b> (2.83-4.51)	<b>4.34</b> (3.31-5.67)	<b>4.90</b> (3.65-6.52)	<b>5.49</b> (3.97-7.57)	<b>6.16</b> (4.20-8.65)	<b>7.15</b> (4.68-10.4)	<b>7.98</b> (5.09-11.8)
12-hr	<b>2.49</b> (1.99-3.07)	<b>2.99</b> (2.39-3.69)	<b>3.81</b> (3.03-4.71)	<b>4.49</b> (3.55-5.58)	<b>5.42</b> (4.15-7.04)	<b>6.12</b> (4.59-8.11)	<b>6.86</b> (4.99-9.42)	<b>7.73</b> (5.28-10.8)	<b>8.99</b> (5.90-12.9)	<b>10.1</b> (6.43-14.7)
24-hr	<b>2.90</b> (2.34-3.55)	<b>3.52</b> (2.84-4.32)	<b>4.54</b> (3.64-5.58)	<b>5.38</b> (4.29-6.66)	<b>6.55</b> (5.05-8.45)	<b>7.41</b> (5.59-9.77)	<b>8.34</b> (6.11-11.4)	<b>9.43</b> (6.47-13.1)	<b>11.1</b> (7.28-15.8)	<b>12.4</b> (7.99-18.1)
2-day	<b>3.21</b> (2.60-3.90)	<b>3.97</b> (3.22-4.83)	<b>5.21</b> (4.21-6.37)	<b>6.24</b> (5.01-7.67)	<b>7.67</b> (5.95-9.86)	<b>8.72</b> (6.63-11.5)	<b>9.86</b> (7.29-13.5)	<b>11.2</b> (7.74-15.5)	<b>13.4</b> (8.83-19.0)	<b>15.2</b> (9.79-22.0)
3-day	<b>3.44</b> (2.80-4.17)	<b>4.28</b> (3.48-5.19)	<b>5.65</b> (4.58-6.87)	<b>6.78</b> (5.46-8.29)	<b>8.34</b> (6.50-10.7)	<b>9.50</b> (7.25-12.4)	<b>10.8</b> (7.98-14.7)	<b>12.3</b> (8.47-16.8)	<b>14.6</b> (9.68-20.7)	<b>16.7</b> (10.7-24.0)
4-day	<b>3.67</b> (3.00-4.44)	<b>4.56</b> (3.72-5.51)	<b>6.00</b> (4.88-7.28)	<b>7.20</b> (5.81-8.78)	<b>8.85</b> (6.91-11.3)	<b>10.1</b> (7.70-13.1)	<b>11.4</b> (8.46-15.5)	<b>13.0</b> (8.99-17.8)	<b>15.5</b> (10.2-21.8)	<b>17.6</b> (11.3-25.2)
7-day	<b>4.37</b> (3.58-5.25)	<b>5.33</b> (4.37-6.41)	<b>6.90</b> (5.64-8.32)	<b>8.20</b> (6.66-9.95)	<b>10.00</b> (7.83-12.7)	<b>11.3</b> (8.68-14.7)	<b>12.8</b> (9.48-17.1)	<b>14.5</b> (10.0-19.6)	<b>17.0</b> (11.3-23.8)	<b>19.1</b> (12.4-27.3)
10-day	<b>5.05</b> (4.16-6.04)	<b>6.06</b> (4.99-7.26)	<b>7.71</b> (6.32-9.27)	<b>9.09</b> (7.40-11.0)	<b>11.0</b> (8.61-13.8)	<b>12.4</b> (9.50-15.9)	<b>13.9</b> (10.3-18.5)	<b>15.6</b> (10.9-21.1)	<b>18.1</b> (12.1-25.3)	<b>20.2</b> (13.1-28.8)
20-day	<b>7.12</b> (5.91-8.47)	<b>8.26</b> (6.84-9.82)	<b>10.1</b> (8.34-12.1)	<b>11.6</b> (9.54-14.0)	<b>13.8</b> (10.8-17.1)	<b>15.4</b> (11.8-19.5)	<b>17.0</b> (12.6-22.3)	<b>18.8</b> (13.2-25.2)	<b>21.2</b> (14.2-29.4)	<b>23.2</b> (15.1-32.7)
30-day	<b>8.85</b> (7.37-10.5)	<b>10.1</b> (8.37-11.9)	<b>12.1</b> (9.99-14.3)	<b>13.7</b> (11.3-16.4)	<b>16.0</b> (12.6-19.8)	<b>17.8</b> (13.7-22.3)	<b>19.5</b> (14.4-25.3)	<b>21.3</b> (15.0-28.5)	<b>23.7</b> (15.9-32.7)	<b>25.5</b> (16.6-36.0)
45-day	<b>11.0</b> (9.18-13.0)	<b>12.3</b> (10.3-14.5)	<b>14.5</b> (12.0-17.1)	<b>16.3</b> (13.4-19.4)	<b>18.7</b> (14.8-23.0)	<b>20.7</b> (15.9-25.8)	<b>22.6</b> (16.7-29.0)	<b>24.4</b> (17.2-32.4)	<b>26.8</b> (18.0-36.8)	<b>28.5</b> (18.6-39.9)
60-day	<b>12.8</b> (10.7-15.0)	<b>14.2</b> (11.9-16.7)	<b>16.5</b> (13.7-19.5)	<b>18.4</b> (15.2-21.8)	<b>21.0</b> (16.7-25.7)	<b>23.1</b> (17.8-28.7)	<b>25.0</b> (18.5-32.0)	<b>26.9</b> (19.0-35.7)	<b>29.3</b> (19.8-40.1)	<b>31.0</b> (20.3-43.3)

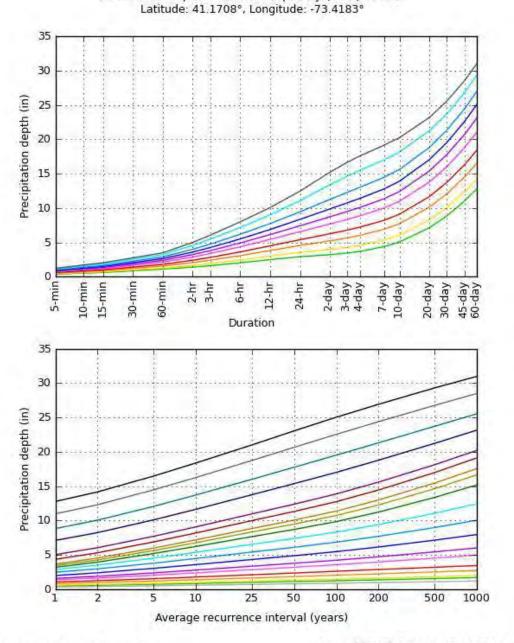
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

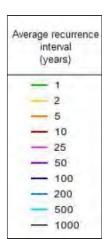
Please refer to NOAA Atlas 14 document for more information.

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#### **PF** graphical



PDS-based depth-duration-frequency (DDF) curves



Duration 5-min 2-day 10-min 3-day 4-day 15-min 30-min 7-day 60-min 10-day 2-hr 20-day 30-day 3-hr 6-hr 45-day 12-hr 60-day 24-hr

NOAA Atlas 14, Volume 10, Version 3

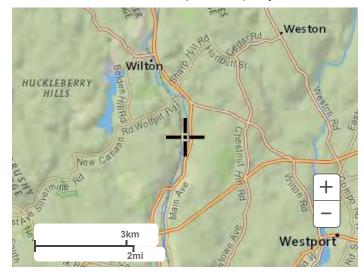
Created (GMT): Sun May 15 14:50:13 2022

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Maps & aerials

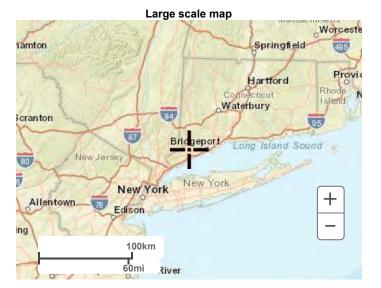
Small scale terrain

Precipitation Frequency Data Server



Large scale terrain





Large scale aerial

Precipitation Frequency Data Server



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

**Disclaimer** 

# **Tighe&Bond**

**APPENDIX C** 



Name: EX-WS-01

Location: North of parking garage

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.000	98.00	0.000
Gravel	0.000	85.00	0.000
Pervious HSG B, Good Condition	0.148	61.00	9.010
Pavement	0.000	98.00	0.000
Rock	0.000	98.00	0.000
Sidewalk	0.000	98.00	0.000
Woods, HSG B, Good Condition	0.451	55.00	24.822
Woods, HSG D, Good Condition	0.415	77.00	31.993
			65.825

#### Total Area: 1.015 CN: 64.88

#### Time of Concentration:

Sheet-Flow Travel Time							
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)		
A - B	0.4	3.4	77	0.286	5.8		
B - C	0.4	3.4	90	0.067	11.8		
C - D	0.4	3.4	53	0.415	3.7		

Shallow Concentrated Flow Travel Time								
Segment ID	D Cover Flow Length (ft) Slope (ft/ft) V (ft/s) Time (min)							
	Paved	0	0.010	2.03	0.0			

Total Tc = 21.4



#### Name: EX-WS-02

Location: West facing slope located east of parking garage

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.085	98.00	8.340
Gravel	0.000	85.00	0.000
Pervious HSG B, Good Condition	0.119	61.00	7.272
Pavement	0.277	98.00	27.159
Rock	0.000	98.00	0.000
Sidewalk	0.000	98.00	0.000
Woods, HSG B, Good Condition	1.055	55.00	58.047
Woods, HSG D, Good Condition	0.991	77.00	76.277
			177.095

#### Total Area: 2.527 CN: 70.07

#### Time of Concentration:

Sheet-Flow Travel Time							
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)		
A - B	0.4	3.4	94	0.085	11.1		
B - C	0.4	3.4	41	0.341	3.3		

Shallow Concentrated Flow Travel Time								
Segment ID	ent ID Cover Flow Length (ft) Slope (ft/ft) V (ft/s) Time (min)							
C - D	Unpaved	138	0.152	6.29	0.4			

Total Tc = 14.8



Name: EX-WS-03

Location: East facing slope

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.002	98.00	0.157
Gravel	0.147	85.00	12.465
Pervious HSG B, Good Condition	0.318	61.00	19.399
Pavement	0.908	98.00	89.010
Rock	0.238	98.00	23.371
Sidewalk	0.022	98.00	2.167
Woods, HSG B, Good Condition	0.452	55.00	24.851
Woods, HSG D, Good Condition	2.320	77.00	178.624
	·		350.044

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#### Time of Concentration:

Sheet-Flow Travel Time							
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)		
A - B	0.4	3.4	25	0.240	2.5		
B - C	0.4	3.4	34	0.471	2.5		

Shallow Concentrated Flow Travel Time								
Segment ID	Cover         Flow Length (ft)         Slope (ft/ft)         V (ft/s)         Time (min)							
C - D	Paved	50	0.400	12.86	0.1			
D - E	Paved	142	0.007	1.71	1.4			
E - F	Unpaved	64	0.063	4.03	0.3			

Total Tc = 6.7



Name:PR-WS-01Location:North of parking garage

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.000	98.00	0.000
Gravel	0.000	85.00	0.000
Pervious HSG B, Good Condition	0.122	61.00	7.451
Pavement	0.000	98.00	0.000
Rock	0.000	98.00	0.000
Sidewalk	0.000	98.00	0.000
Woods, HSG B, Good Condition	0.259	55.00	14.254
Woods, HSG D, Good Condition	0.077	77.00	5.897
	•		27.602

	Total Area:	0.458	CN:	60.28	
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#### Time of Concentration:

		Shee	et-Flow Travel Time		
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A - B	0.4	3.4	8	0.500	0.8
B - C	0.4	3.4	51	0.118	6.0
C - D	0.4	3.4	53	0.415	3.7

		Shallow Concentrat	ed Flow Travel Tir	ne	
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)
	Paved	0	0.010	2.03	0.0

Total Tc = 10.5



#### Name: PR-WS-02

Location: West facing slope located east of parking garage

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.085	98.00	8.340
Gravel	0.000	85.00	0.000
Pervious HSG B, Good Condition	0.119	61.00	7.272
Pavement	0.277	98.00	27.159
Rock	0.000	98.00	0.000
Sidewalk	0.000	98.00	0.000
Woods, HSG B, Good Condition	1.055	55.00	58.047
Woods, HSG D, Good Condition	0.991	77.00	76.277
	-		177.095

#### Total Area: 2.527 CN: 70.07

#### Time of Concentration:

		Shee	et-Flow Travel Time		
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A - B	0.4	3.4	94	0.085	11.1
B - C	0.4	3.4	41	0.341	3.3

		Shallow Concentrat	ed Flow Travel Tir	ne	
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)
C - D	Unpaved	138	0.152	6.29	0.4

Total Tc = 14.8



Name:PR-WS-03ALocation:Parking area

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.002	98.00	0.157
Gravel	0.002	85.00	0.191
Pervious HSG B, Good Condition	0.142	61.00	8.661
Pavement	0.498	98.00	48.757
Rock	0.119	98.00	11.694
Sidewalk	0.020	98.00	1.989
Woods, HSG B, Good Condition	0.000	55.00	0.000
Woods, HSG D, Good Condition	0.364	77.00	28.048
	·		99.498

Total Area: 1.147 CN: 86.73

Time of Concentration:

		Shee	et-Flow Travel Time		
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)
A - B	0.4	3.4	36	0.278	3.2
B - C	0.015	3.4	39	1.462	0.1

		Shallow Concentrat	ed Flow Travel Tir	ne	
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)
C - D	Paved	55	0.009	1.94	0.5

Total Tc = 5.0 Minimum



Name: PR-WS-03B

Location: Roadway

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.000	98.00	0.000
Gravel	0.067	85.00	5.708
Pervious HSG B, Good Condition	0.637	61.00	38.860
Pavement	0.694	98.00	68.024
Rock	0.356	98.00	34.867
Sidewalk	0.142	98.00	13.879
Woods, HSG B, Good Condition	0.081	55.00	4.432
Woods, HSG D, Good Condition	0.891	77.00	68.582
		•	234.352

|--|

#### Time of Concentration:

Sheet-Flow Travel Time									
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)				
A - B	0.4	3.4	59	0.305	4.6				
B - C	0.4	3.4	38	0.158	4.2				

Shallow Concentrated Flow Travel Time									
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)				
	Paved 0 0.009 1.94 0.0								

Total Tc = 8.8



Name:PR-WS-03CLocation:Below Roadway

#### **Runoff Coefficient:**

Cover Type	Area (ac)	CN	A x CN
Building	0.000	98.00	0.000
Gravel	0.000	85.00	0.000
Pervious HSG B, Good Condition	0.000	61.00	0.000
Pavement	0.000	98.00	0.000
Rock	0.000	98.00	0.000
Sidewalk	0.000	98.00	0.000
Woods, HSG B, Good Condition	0.444	55.00	24.395
Woods, HSG D, Good Condition	0.506	77.00	38.986
			63.381

Total Area:	0.950	CN:	66.73	

Time of Concentration:

Sheet-Flow Travel Time										
Segment ID	"n"	P <sub>2</sub> (in)	Flow Length (ft)	Slope (ft/ft)	Time (min)					
A - B	0.4	3.4	41	0.439	3.0					
B - C	0.4	3.4	72	0.181	6.6					

Shallow Concentrated Flow Travel Time									
Segment ID	Cover	Flow Length (ft)	Slope (ft/ft)	V (ft/s)	Time (min)				
	Paved	0	0.009	1.94	0.0				

Total Tc = 9.6

## Watershed Model Schematic







## Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

	Hydrograph	Inflow				Peak Ou	tflow (cfs)	)			Hydrograph
о.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			0.506		0.991	1.445	2.142	2.683	3.288	EX-WS-01
2	SCS Runoff			2.088		3.649	5.050	7.123	8.719	10.48	EX-WS-02
3	SCS Runoff			7.474		11.45	14.84	19.66	23.23	27.10	EX-WS-03
Pro	j. file: A0969	9-015 202	2 04-04	Existing	Conditio	ns.apw			Sa	turdav. 0	05 / 21 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.506	2	740	2,842				EX-WS-01
2	SCS Runoff	2.088	2	732	9,176				EX-WS-02
3	SCS Runoff	7.474	2	726	25,749				EX-WS-03
	969-015 2022								05 / 21 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.991	2	738	5,059				EX-WS-01
2	SCS Runoff	3.649	2	732	15,288				EX-WS-02
3	SCS Runoff	11.45	2	726	39,100				EX-WS-03
	969-015 2022			onditions		Doried: 5 V		Saturday	05 / 21 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.445	2	738	7,138				EX-WS-01
2	SCS Runoff	5.050	2	732	20,846				EX-WS-02
3	SCS Runoff	14.84	2	726	50,704				EX-WS-03
AUd	969-015 2022	2 04-04 F	xisting C	onditions		Period: 10 \	/ear	Saturday	05 / 21 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.142	2	736	10,310				EX-WS-01
2	SCS Runoff	7.123	2	730	29,137				EX-WS-02
2 3	SCS Runoff	7.123	2	730	29,137 67,462				EX-WS-02 EX-WS-03
A09	969-015 2022	04-04 E	xisting C	onditions	.gpRveturn F	Period: 25 \	/ear	Saturday, (	05 / 21 / 2022

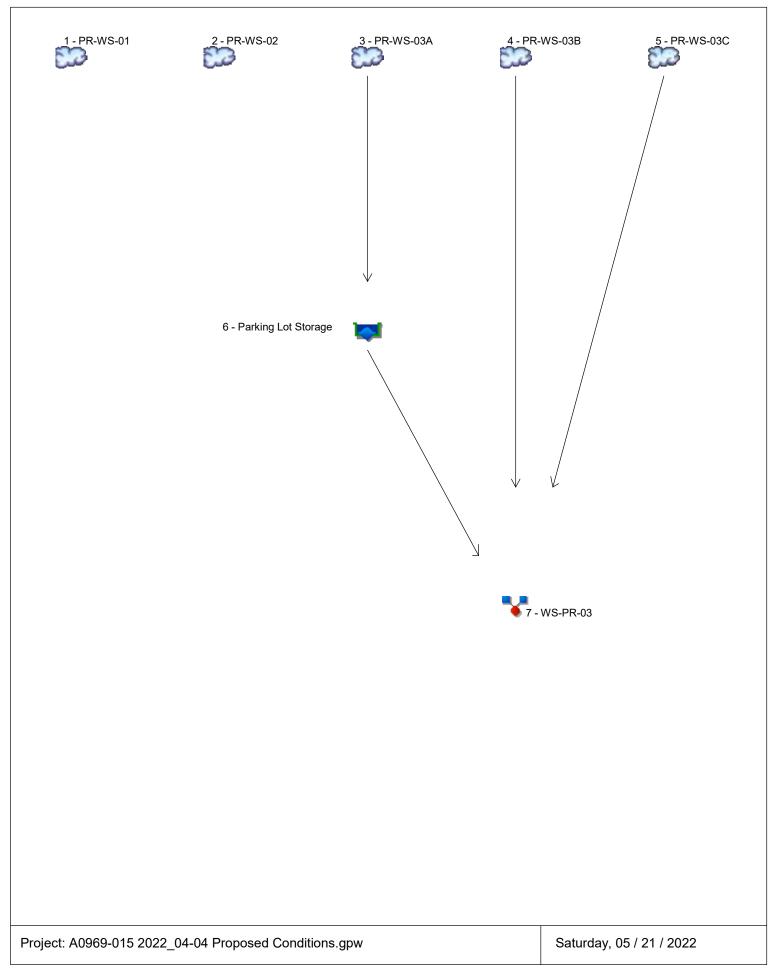
## Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.683	2	736	12,797				EX-WS-01
2	SCS Runoff	8.719	2	730	35,530				EX-WS-02
3	SCS Runoff	23.23	2	726	80,087				EX-WS-03
A09	969-015 2022	 2_04-04 E	 xistina C	onditions	.gpRveturn F	ן Period: 50 ץ	/ear	Saturdav. (	) )5 / 21 / 2022

## Hydrograph Summary Report

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	3.288	2	736	15,598				EX-WS-01
2	SCS Runoff	10.48	2	730	42,658				EX-WS-02
3	SCS Runoff	27.10	2	726	93,951				EX-WS-03
A09	969-015 2022	2_04-04 E	Existing C	onditions	.gpRveturn	Period: 100	Year	Saturday,	05 / 21 / 2022

### Watershed Model Schematic



# Hydrograph Return Period Recap Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

	Hydrograph	Inflow	Peak Outflow (cfs)							Hydrograph	
lo.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			0.175		0.410	0.640	0.997	1.278	1.596	PR-WS-01
2	SCS Runoff			2.074		3.631	5.030	7.100	8.695	10.46	PR-WS-02
3	SCS Runoff			2.828		3.997	4.963	6.306	7.288	8.346	PR-WS-03A
4	SCS Runoff			5.402		8.058	10.30	13.46	15.79	18.31	PR-WS-03B
5	SCS Runoff			1.208		2.190	3.080	4.402	5.432	6.586	PR-WS-03C
6	Reservoir	3		0.000		0.000	0.000	0.000	0.000	0.000	Parking Lot Storage
7	Combine	4, 5, 6		6.046		9.167	11.83	15.66	18.55	21.68	WS-PR-03
										h	 \
ro	j. file: A0969	9-015 2022	∠_04-04	Propose	a Condit	ions.gpv	/		Sa	turday, 0	5 / 21 / 2022

## Hydrograph Summary Report

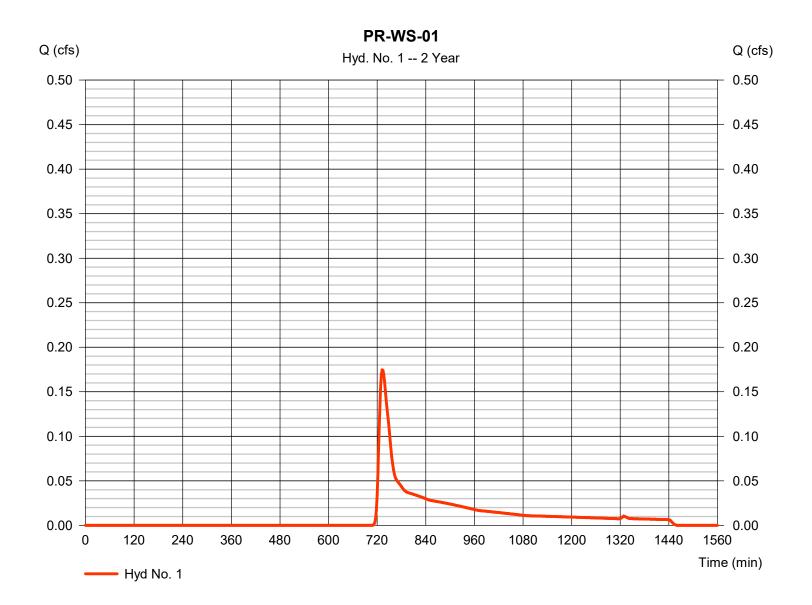
lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.175	2	732	947				PR-WS-01
2	SCS Runoff	2.074	2	732	9,127				PR-WS-02
3	SCS Runoff	2.828	2	724	8,489				PR-WS-03A
4	SCS Runoff	5.402	2	726	18,490				PR-WS-03B
5	SCS Runoff	1.208	2	720	2,918				PR-WS-03C
6	Reservoir	0.000	2	660	0	3	131.89	2,772	Parking Lot Storage
7	Combine	6.046	2	726	21,408	4, 5, 6			WS-PR-03
A09	969-015 2022	2_04-04 P	roposed	Conditio	ns. <b>Græv</b> turn	Period: 2 Y	ear	Saturday,	05 / 21 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.175 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 947 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 3.52 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	

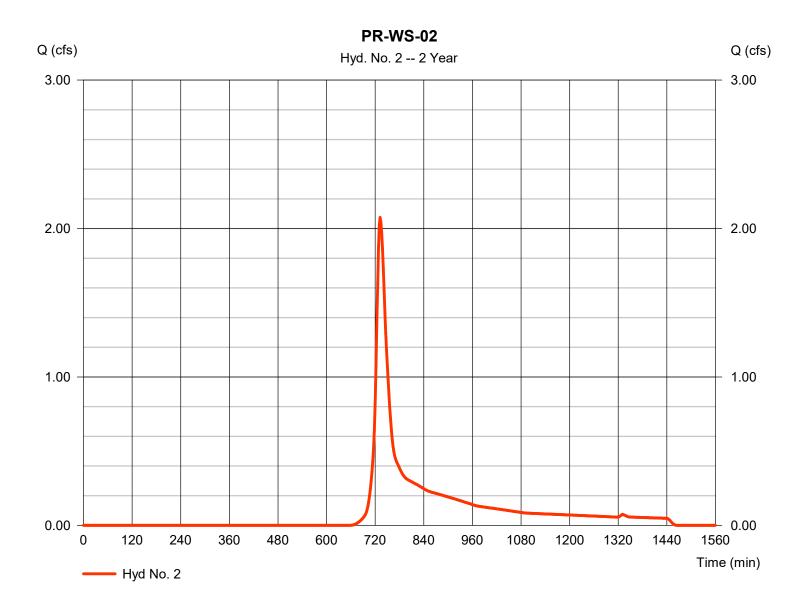


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 2

Hydrograph type	= SCS Runoff	Peak discharge	= 2.074 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 9,127 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 3.52 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



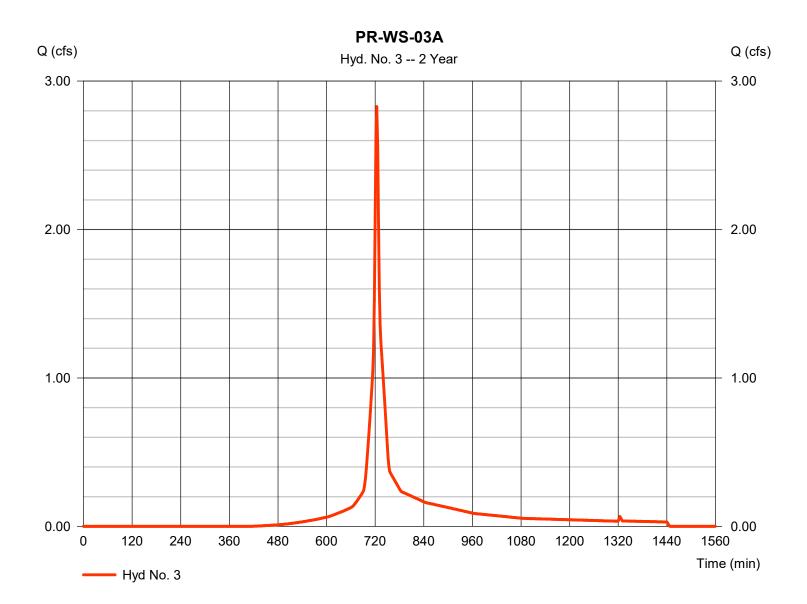
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 3

PR-WS-03A

Hydrograph type	= SCS Runoff	Peak discharge	= 2.828 cfs
Storm frequency	= 2 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 8,489 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 3.52 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



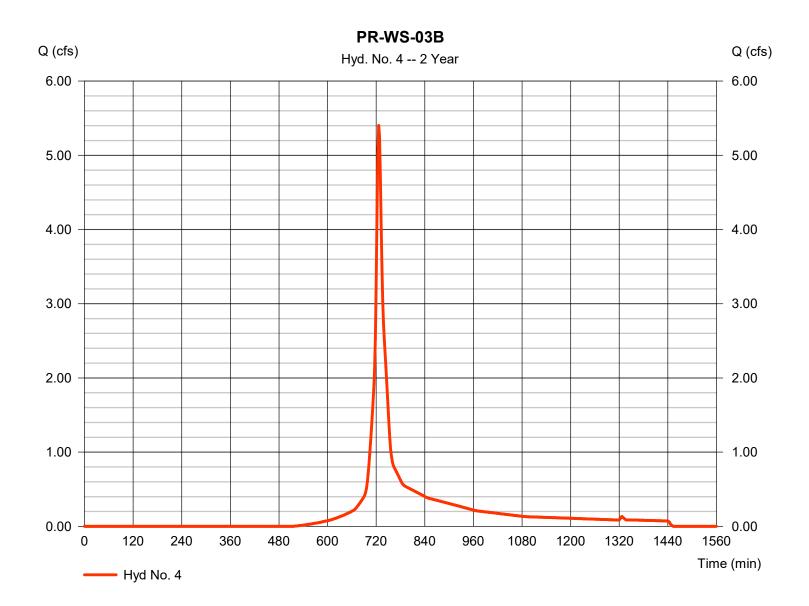
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 5.402 cfs
Storm frequency	= 2 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 18,490 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 3.52 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



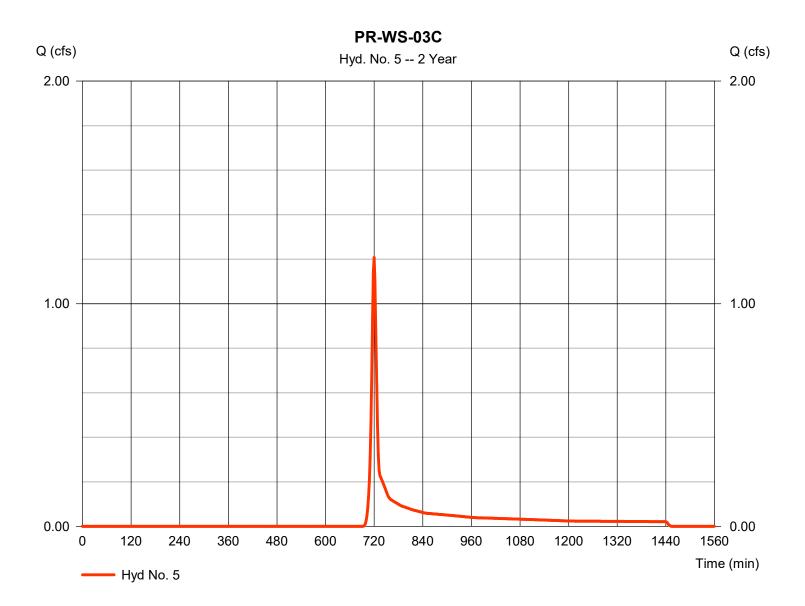
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 1.208 cfs
Storm frequency	= 2 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 2,918 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 3.52 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484
		·	



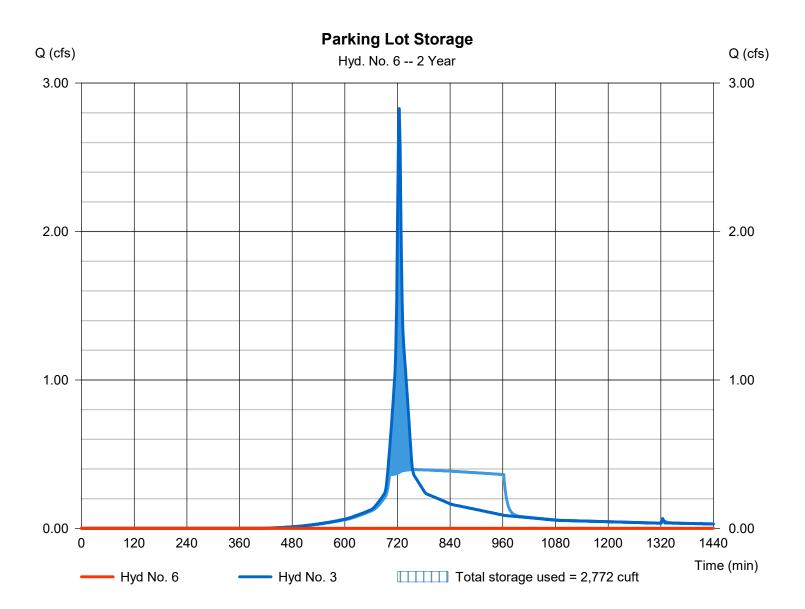
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 2 yrs	Time to peak	= 660 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 131.89 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 2,772 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Saturday, 05 / 21 / 2022

### **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Pond No. 1 - Parking Lot Detention

#### Pond Data

**UG Chambers -**Invert elev. = 132.00 ft, Rise x Span =  $4.00 \times 4.00$  ft, Barrel Len = 72.00 ft, No. Barrels = 6, Slope = 0.00%, Headers = No **Encasement -**Invert elev. = 131.00 ft, Width = 18.00 ft, Height = 5.00 ft, Voids = 40.00%

#### Stage / Storage Table

Stage (ft) Elevation (ft)		Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	131.00	n/a	0	0
0.50	131.50	n/a	1,556	1,556
1.00	132.00	n/a	1,556	3,111
1.50	132.50	n/a	2,074	5,185
2.00	133.00	n/a	2,074	7,259
2.50	133.50	n/a	2,074	9,333
3.00	134.00	n/a	2,074	11,407
3.50	134.50	n/a	2,074	13,481
4.00	135.00	n/a	2,074	15,555
4.50	135.50	n/a	2,074	17,629
5.00	136.00	n/a	2,074	19,703

#### **Culvert / Orifice Structures**

### Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 135.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 100.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.000 (by Wet area)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

Olugo /	otorago / i	sioonargo i	abio										
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	131.00	0.00								0.000		0.000
0.05	156	131.05	0.00								0.362		0.362
0.10	311	131.10	0.00								0.364		0.364
0.15	467	131.15	0.00								0.366		0.366
0.20	622	131.20	0.00								0.368		0.368
0.25	778	131.25	0.00								0.370		0.370
0.30	933	131.30	0.00								0.372		0.372
0.35	1,089	131.35	0.00								0.374		0.374
0.40	1,244	131.40	0.00								0.376		0.376
0.45	1,400	131.45	0.00								0.378		0.378
0.50	1,556	131.50	0.00								0.380		0.380
0.55	1,711	131.55	0.00								0.382		0.382
0.60	1,867	131.60	0.00								0.384		0.384
0.65	2,022	131.65	0.00								0.386		0.386
0.70	2,178	131.70	0.00								0.388		0.388
0.75	2,333	131.75	0.00								0.390		0.390
0.80	2,489	131.80	0.00								0.392		0.392
0.85	2,644	131.85	0.00								0.394		0.394
0.90	2,800	131.90	0.00								0.396		0.396
0.95	2,955	131.95	0.00								0.398		0.398
1.00	3,111	132.00	0.00								0.400		0.400
1.05	3,318	132.05	0.00								0.402		0.402
1.10	3,526	132.10	0.00								0.404		0.404
1.15	3,733	132.15	0.00								0.406		0.406
1.20	3,941	132.20	0.00								0.408		0.408
1.25	4,148	132.25	0.00								0.410		0.410
1.30	4,355	132.30	0.00								0.412		0.412
1.35	4,563	132.35	0.00								0.414		0.414
1.40	4,770	132.40	0.00								0.416		0.416
1.45	4,978	132.45	0.00								0.418		0.418
1.50	5,185	132.50	0.00								0.420		0.420
1.55	5,392	132.55	0.00								0.422		0.422
	•										Continuo		+ 2000

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## Parking Lot Detention Stage / Storage / Discharge Table

Stage /	Storage / I	Jischarge i	able										
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
1.60	5,600	132.60	0.00								0.424		0.424
1.65	5,807	132.65	0.00								0.426		0.426
1.70	6,015	132.70	0.00								0.428		0.428
1.75	6,222	132.75	0.00								0.430		0.430
1.80	6,429	132.80	0.00								0.432		0.432
1.85	6,637	132.85	0.00								0.434		0.434
1.90	6,844	132.90	0.00								0.436		0.436
1.95	7,052	132.95	0.00								0.438		0.438
2.00 2.05	7,259	133.00 133.05	0.00 0.00								0.440 0.442		0.440 0.442
2.05	7,466 7,674	133.05	0.00								0.442		0.442
2.10	7,881	133.15	0.00								0.446		0.446
2.20	8,089	133.20	0.00								0.448		0.448
2.25	8,296	133.25	0.00								0.450		0.450
2.30	8,503	133.30	0.00								0.452		0.452
2.35	8,711	133.35	0.00								0.454		0.454
2.40	8,918	133.40	0.00								0.456		0.456
2.45	9,126	133.45	0.00								0.458		0.458
2.50	9,333	133.50	0.00								0.460		0.460
2.55	9,540	133.55	0.00								0.462		0.462
2.60	9,748	133.60	0.00								0.464		0.464
2.65	9,955	133.65	0.00								0.466		0.466
2.70 2.75	10,163 10,370	133.70 133.75	0.00 0.00								0.468 0.470		0.468 0.470
2.75	10,370	133.80	0.00								0.470		0.470
2.85	10,785	133.85	0.00								0.472		0.472
2.90	10,992	133.90	0.00								0.476		0.476
2.95	11,200	133.95	0.00								0.478		0.478
3.00	11,407	134.00	0.00								0.480		0.480
3.05	11,614	134.05	0.00								0.482		0.482
3.10	11,822	134.10	0.00								0.484		0.484
3.15	12,029	134.15	0.00								0.486		0.486
3.20	12,237	134.20	0.00								0.488		0.488
3.25	12,444	134.25	0.00								0.490		0.490
3.30	12,651	134.30	0.00								0.492		0.492
3.35 3.40	12,859 13,066	134.35 134.40	0.00 0.00								0.494 0.496		0.494 0.496
3.40	13,000	134.40	0.00								0.490		0.490
3.50	13,481	134.50	0.00								0.500		0.500
3.55	13,688	134.55	0.00								0.502		0.502
3.60	13,896	134.60	0.00								0.504		0.504
3.65	14,103	134.65	0.00								0.506		0.506
3.70	14,311	134.70	0.00								0.508		0.508
3.75	14,518	134.75	0.00								0.510		0.510
3.80	14,726	134.80	0.00								0.512		0.512
3.85	14,933	134.85	0.00								0.514		0.514
3.90	15,140	134.90	0.00								0.516		0.516
3.95	15,348	134.95	0.00								0.518		0.518
4.00	15,555	135.00	0.00 0.01 ic								0.520		0.520
4.05 4.10	15,763 15,970	135.05 135.10	0.01 ic 0.04 ic								0.522 0.524		0.533 0.568
4.10	16,177	135.15	0.04 ic 0.10 ic								0.524		0.624
4.20	16,385	135.20	0.10 ic 0.17 ic								0.528		0.699
4.25	16,592	135.25	0.26 ic								0.530		0.792
4.30	16,800	135.30	0.37 ic								0.532		0.903
4.35	17,007	135.35	0.49 ic								0.534		1.029
4.40	17,214	135.40	0.63 ic								0.536		1.168
4.45	17,422	135.45	0.78 ic								0.538		1.322
4.50	17,629	135.50	0.95 ic								0.540		1.487
4.55	17,837	135.55	1.12 ic								0.542		1.660
4.60	18,044	135.60	1.30 ic								0.544		1.843
4.65	18,251	135.65	1.48 ic								0.546		2.029
4.70	18,459	135.70	1.67 oc								0.548		2.220
4.75	18,666	135.75	1.81 oc								0.550		2.364
4.80	18,874	135.80	1.94 oc								0.552		2.491
4.85 4.90	19,081 19,288	135.85 135.90	2.05 oc 2.13 oc								0.554 0.556		2.600 2.682
4.90 4.95	19,288	135.90	2.13 oc 2.16 oc								0.556		2.682
5.00	19,490	136.00	2.10 oc 2.08 oc								0.560		2.638
0.00	10,700	100.00	2.00 00								0.000		2.000

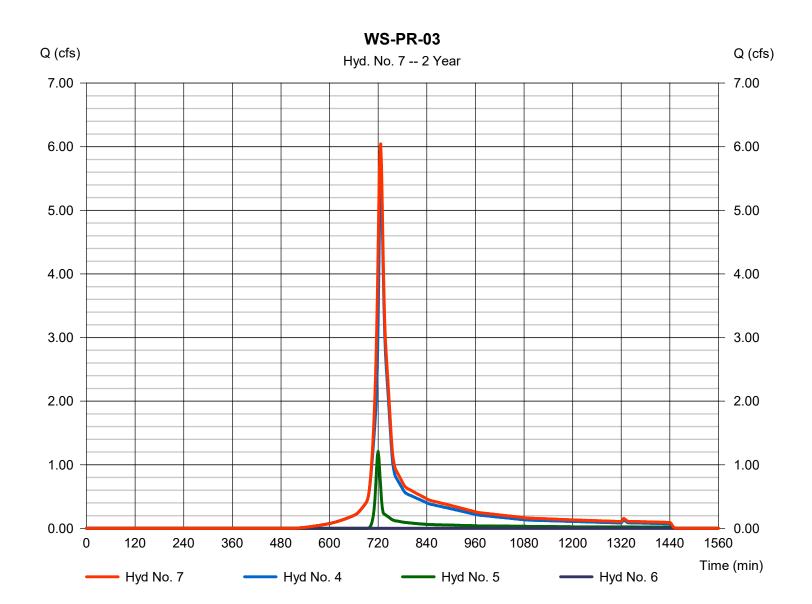
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Saturday, 05 / 21 / 2022

### Hyd. No. 7

### WS-PR-03

Hydrograph type	= Combine	Peak discharge	= 6.046 cfs
Storm frequency	= 2 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 21,408 cuft
Inflow hyds.	= 4, 5, 6	Contrib. drain. area	= 3.817 ac



## Hydrograph Summary Report

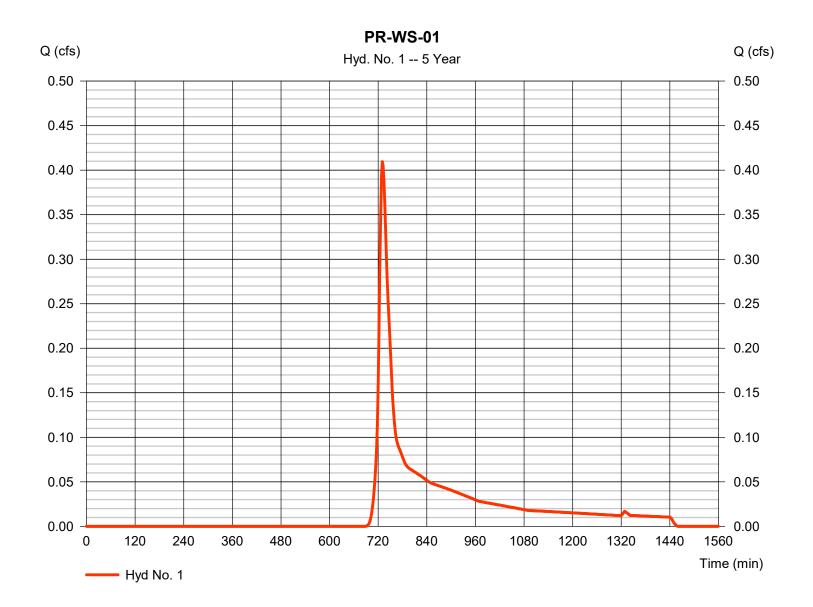
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.410	2	730	1,816				PR-WS-01
2	SCS Runoff	3.631	2	732	15,223				PR-WS-02
3	SCS Runoff	3.997	2	724	12,129				PR-WS-03A
4	SCS Runoff	8.058	2	726	27,522				PR-WS-03B
5	SCS Runoff	2.190	2	720	5,068				PR-WS-03C
6	Reservoir	0.000	2	674	0	3	132.33	4,478	Parking Lot Storage
7	Combine	9.167	2	726	32,590	4, 5, 6			WS-PR-03
A09	969-015 2022	2 04-04 F	Proposed	Conditio	ns.@Reaturn	Period: 5 Y	ear	Saturdav	05 / 21 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.410 cfs
Storm frequency	= 5 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 1,816 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 4.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

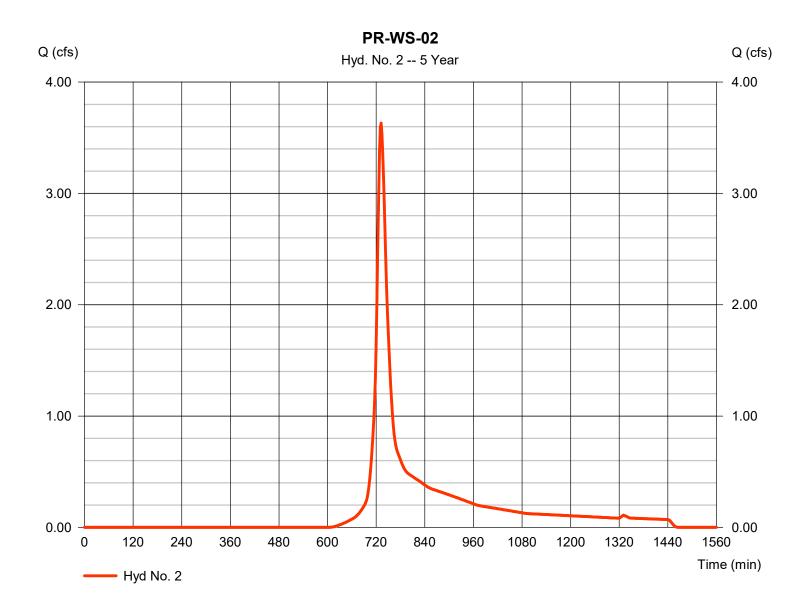


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 2

Hydrograph type	= SCS Runoff	Peak discharge	= 3.631 cfs
Storm frequency	= 5 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 15,223 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 4.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
Tc method Total precip.	= User = 4.54 in	Time of conc. (Tc) Distribution	= 14.80 min = Type III



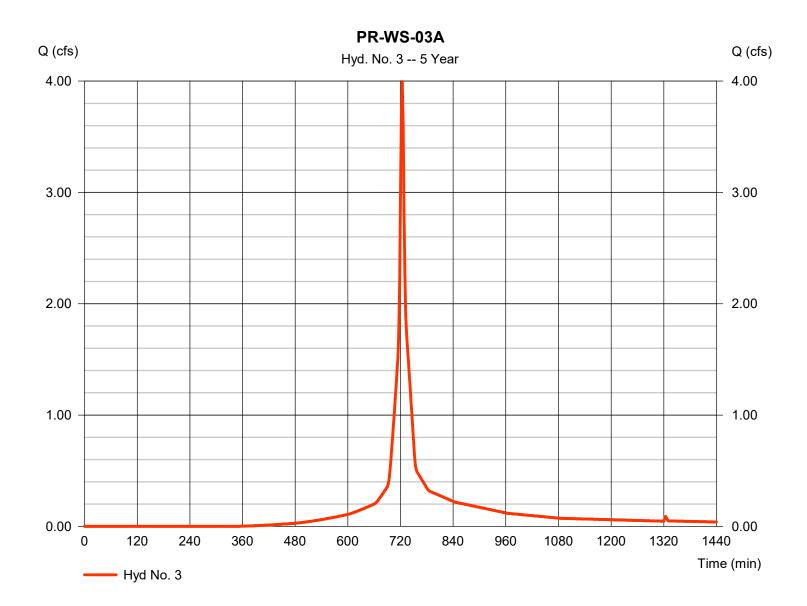
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 3

PR-WS-03A

Hydrograph type	= SCS Runoff	Peak discharge	= 3.997 cfs
Storm frequency	= 5 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 12,129 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 4.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



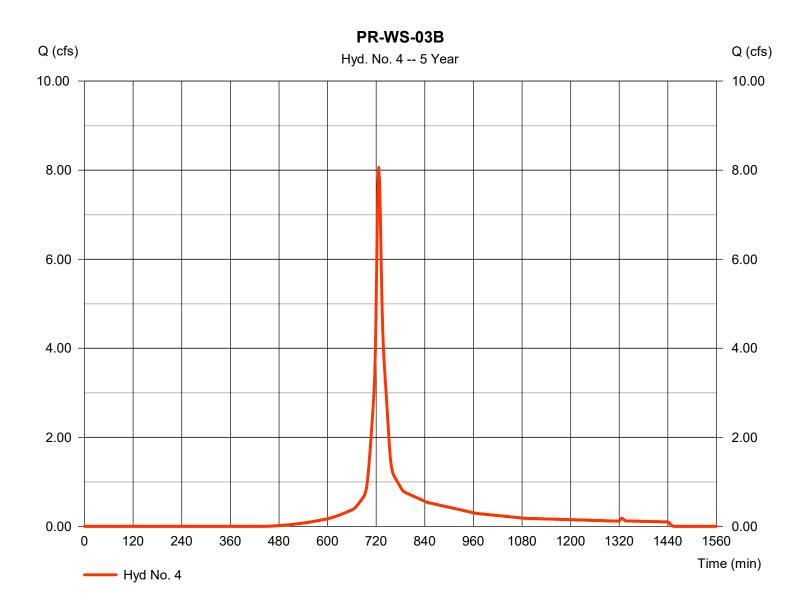
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 8.058 cfs
Storm frequency	= 5 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 27,522 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 4.54 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



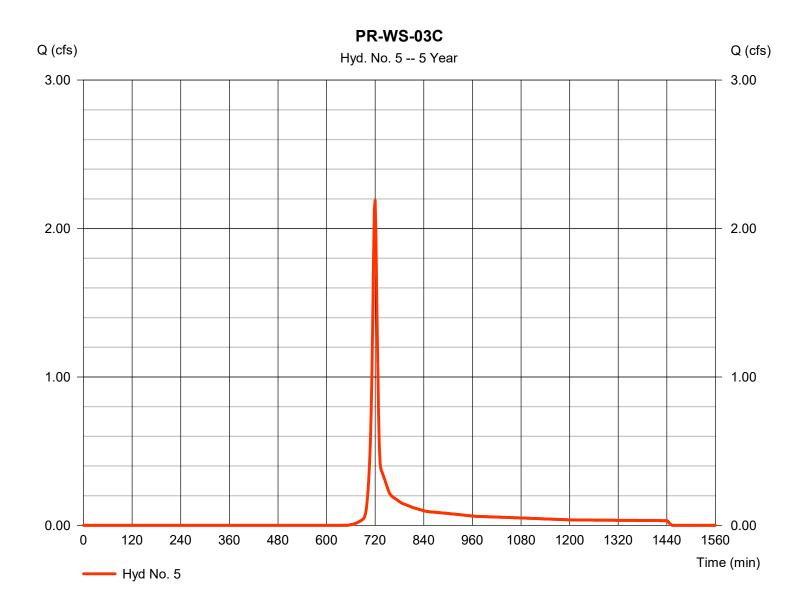
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 2.190 cfs
Storm frequency	= 5 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 5,068 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 4.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484
		-	



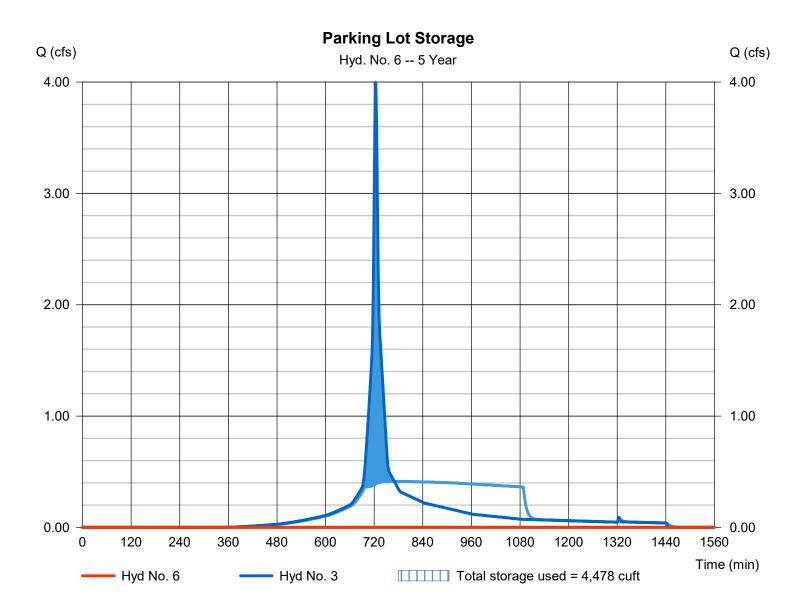
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 5 yrs	Time to peak	= 674 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 132.33 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 4,478 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Saturday, 05 / 21 / 2022

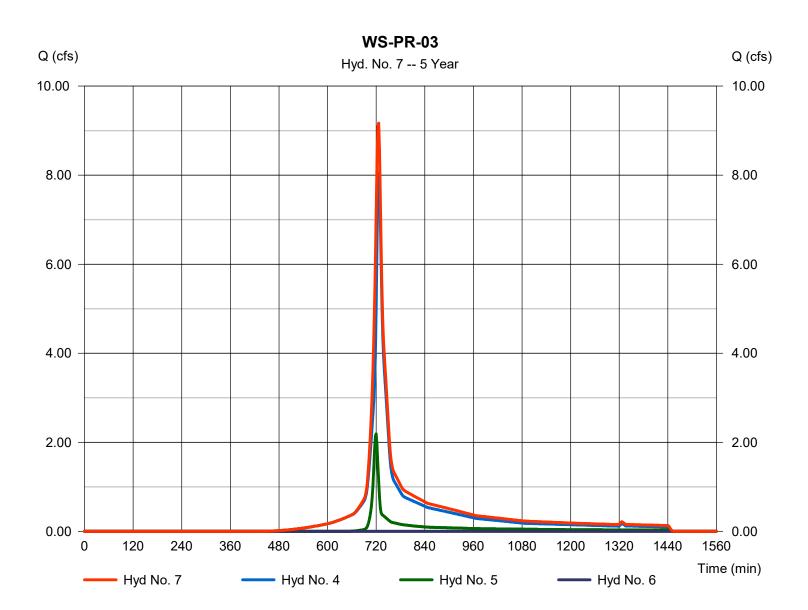
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Saturday, 05 / 21 / 2022

### Hyd. No. 7

WS-PR-03

Hydrograph type	= Combine	Peak discharge	= 9.167 cfs
Storm frequency	= 5 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 32,590 cuft
Inflow hyds.	= 4, 5, 6	Contrib. drain. area	= 3.817 ac
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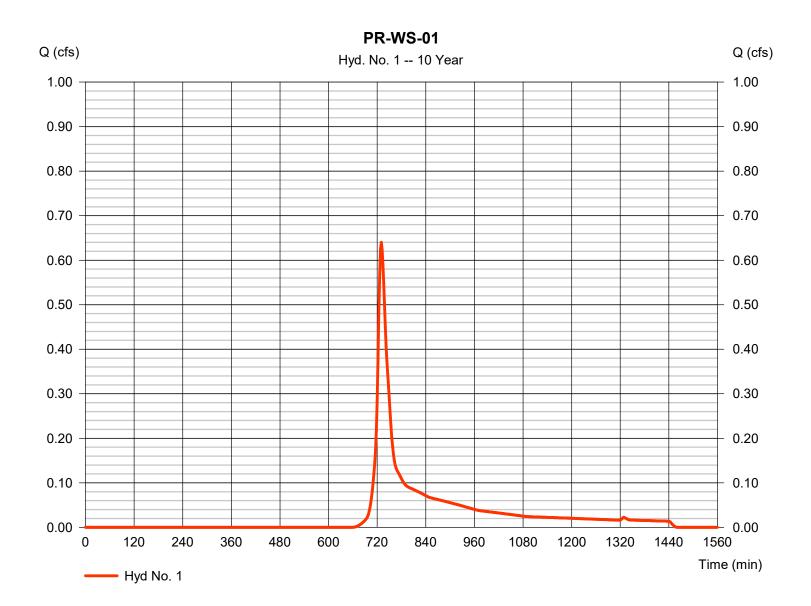
## Hydrograph Summary Report

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.640	2	730	2,659				PR-WS-01
2	SCS Runoff	5.030	2	732	20,770				PR-WS-02
3	SCS Runoff	4.963	2	724	15,205				PR-WS-03A
4	SCS Runoff	10.30	2	726	35,298				PR-WS-03B
5	SCS Runoff	3.080	2	720	7,062				PR-WS-03C
6	Reservoir	0.000	2	580	0	3	132.70	6,014	Parking Lot Storage
7	Combine	11.83	2	726	42,360	4, 5, 6			WS-PR-03
A09	969-015 2022	2 04-04 F	roposed	Conditio	ns.@Roevtrurn	Period: 10 `	Year	Saturday.	05 / 21 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.640 cfs
Storm frequency	= 10 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 2,659 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 5.38 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

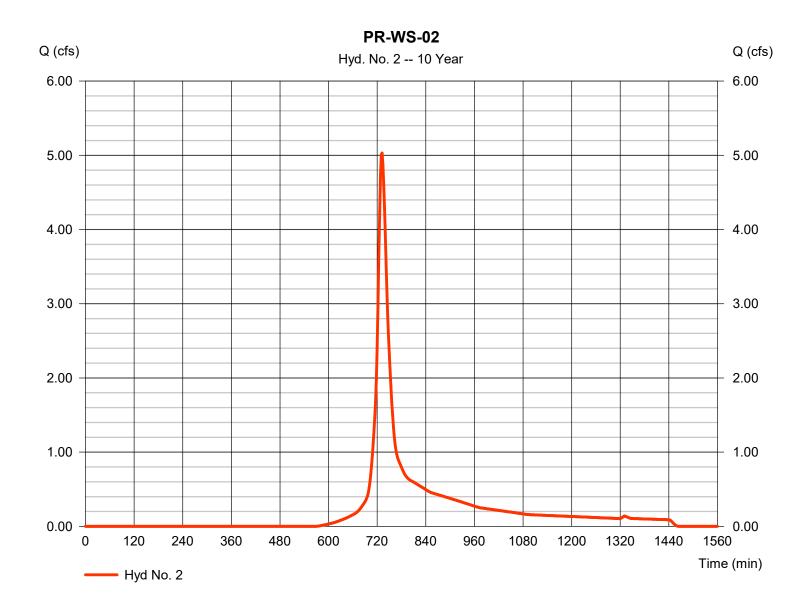


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 2

Hydrograph type	= SCS Runoff	Peak discharge	= 5.030 cfs
Storm frequency	= 10 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 20,770 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 5.38 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



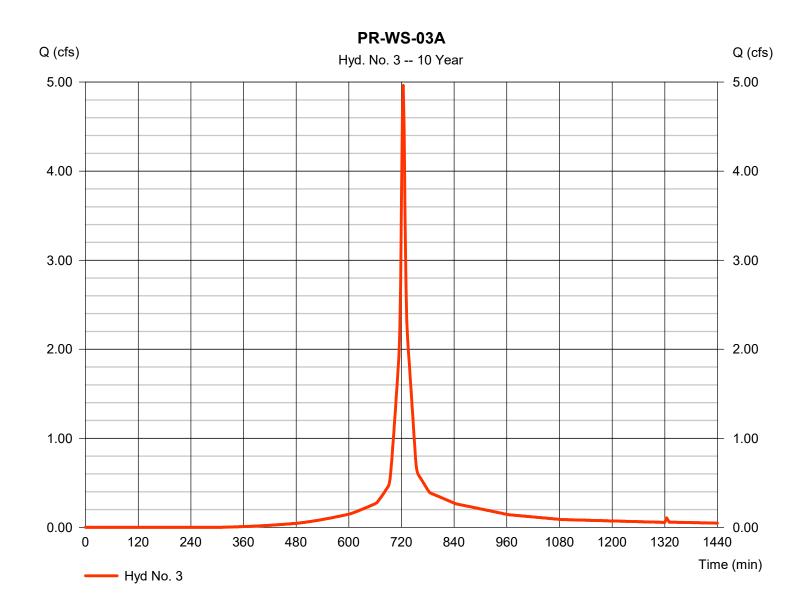
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 3

PR-WS-03A

Hydrograph type	= SCS Runoff	Peak discharge	= 4.963 cfs
Storm frequency	= 10 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 15,205 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.38 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



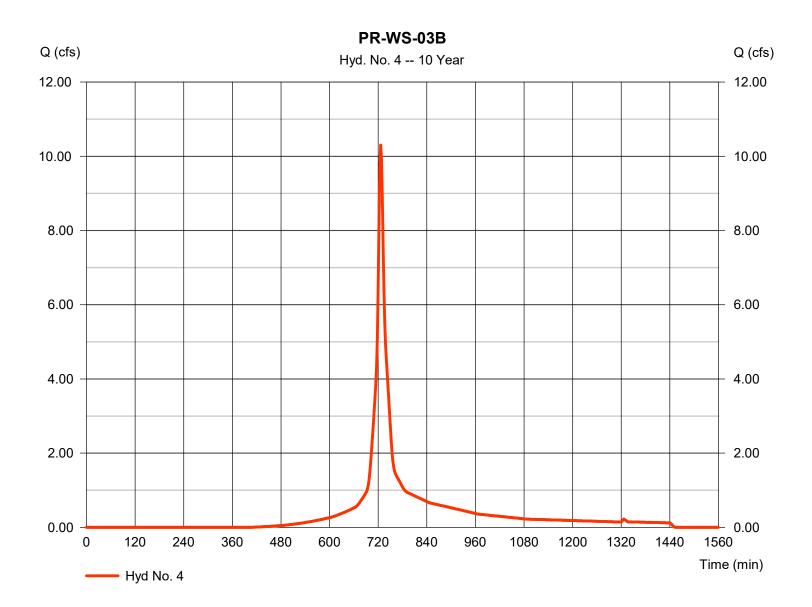
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 10.30 cfs
Storm frequency	= 10 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 35,298 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 5.38 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



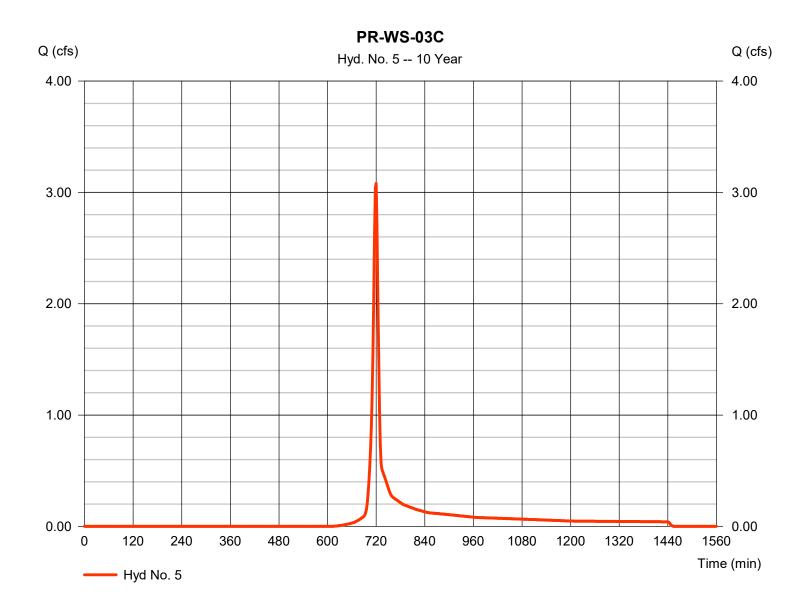
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 3.080 cfs
Storm frequency	= 10 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 7,062 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 5.38 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484
		-	



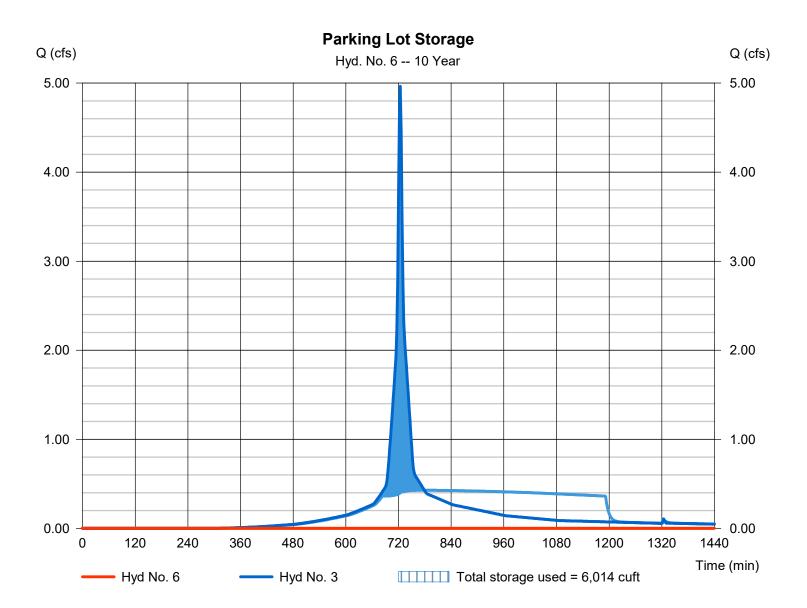
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 10 yrs	Time to peak	= 580 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 132.70 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 6,014 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



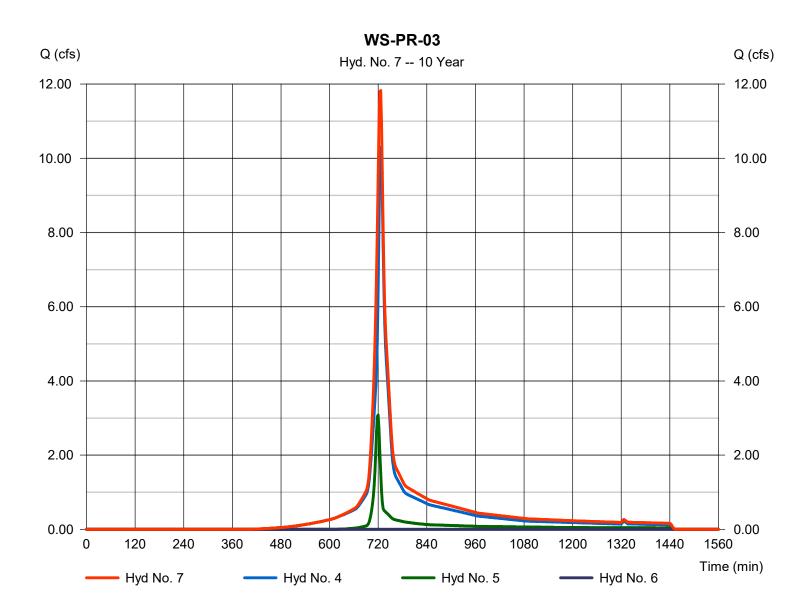
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Saturday, 05 / 21 / 2022

### Hyd. No. 7

WS-PR-03

Hydrograph type	= Combine	Peak discharge	= 11.83 cfs
Storm frequency	= 10 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 42,360 cuft
Inflow hyds.	= 4, 5, 6	Contrib. drain. area	= 3.817 ac



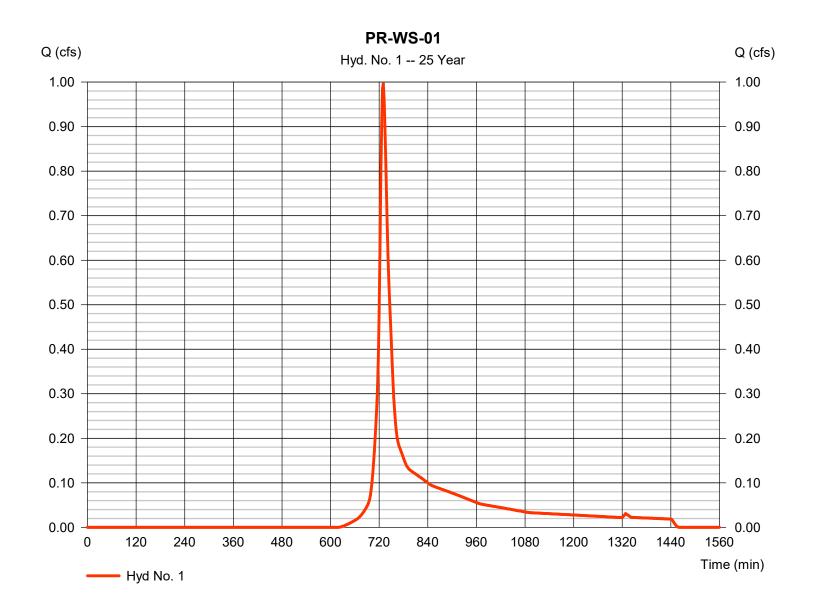
## Hydrograph Summary Report

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.997	2	730	3,973				PR-WS-01
2	SCS Runoff	7.100	2	730	29,047				PR-WS-02
3	SCS Runoff	6.306	2	724	19,563				PR-WS-03A
4	SCS Runoff	13.46	2	726	46,453				PR-WS-03B
5	SCS Runoff	4.402	2	720	10,080				PR-WS-03C
6	Reservoir	0.000	2	618	0	3	133.25	8,312	Parking Lot Storage
7	Combine	15.66	2	724	56,533	4, 5, 6			WS-PR-03
	1		1		+				1

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 0.997 cfs
Storm frequency	= 25 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 3,973 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 6.55 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

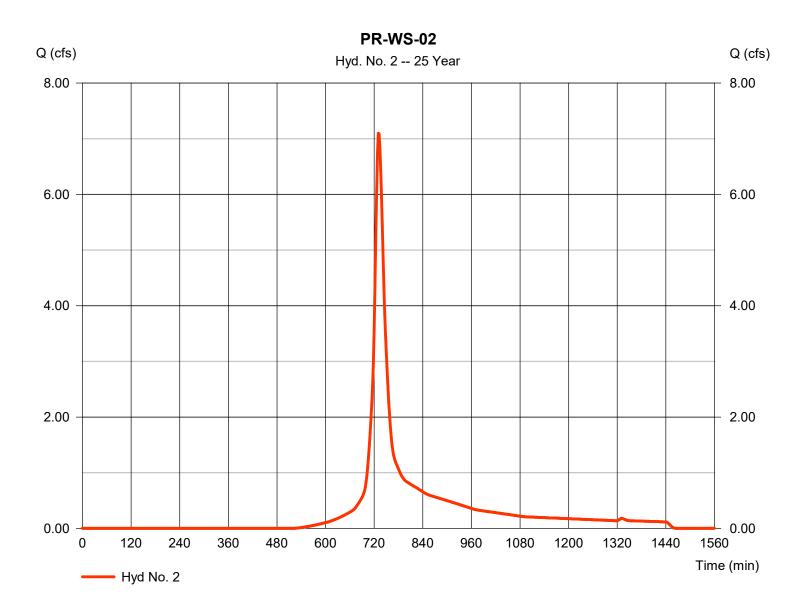


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 2

Hydrograph type	= SCS Runoff	Peak discharge	= 7.100 cfs
Storm frequency	= 25 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 29,047 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 6.55 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



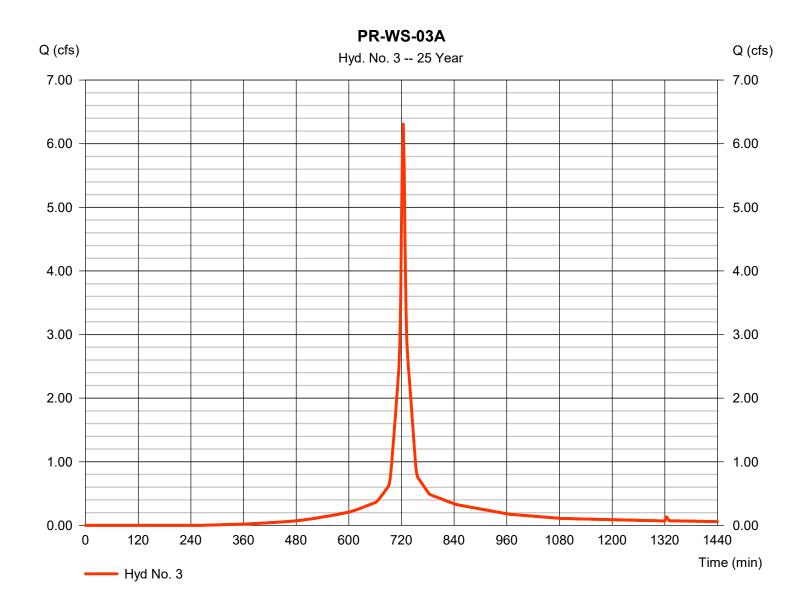
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 3

PR-WS-03A

Hydrograph type	= SCS Runoff	Peak discharge	= 6.306 cfs
Storm frequency	= 25 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 19,563 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 6.55 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



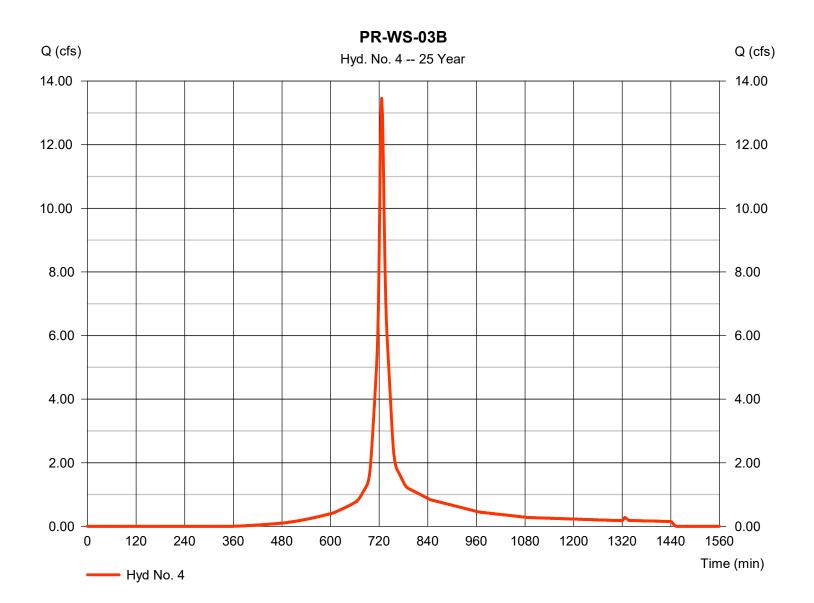
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

### Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 13.46 cfs
Storm frequency	= 25 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 46,453 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 6.55 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484

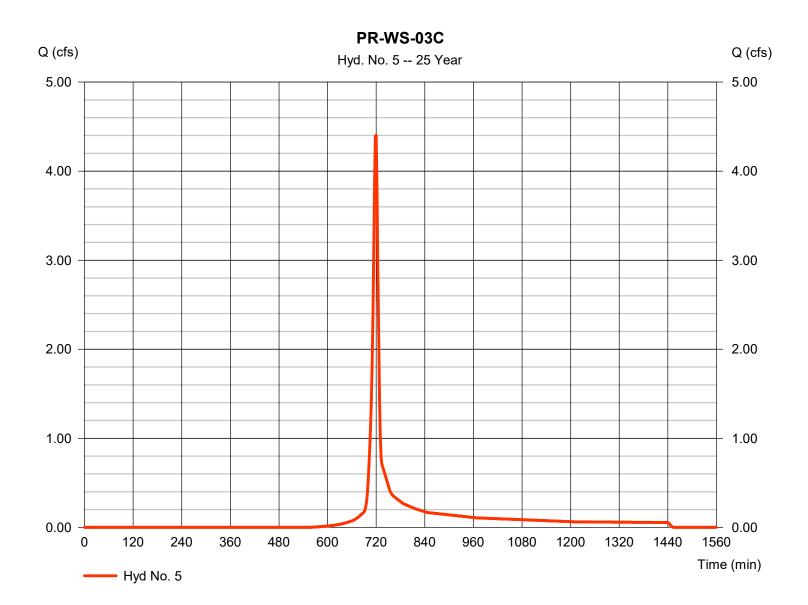


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

### Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 4.402 cfs
Storm frequency	= 25 yrs	Time to peak	= 720 min
Time interval	= 2 min	Hyd. volume	= 10,080 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 6.55 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Saturday, 05 / 21 / 2022

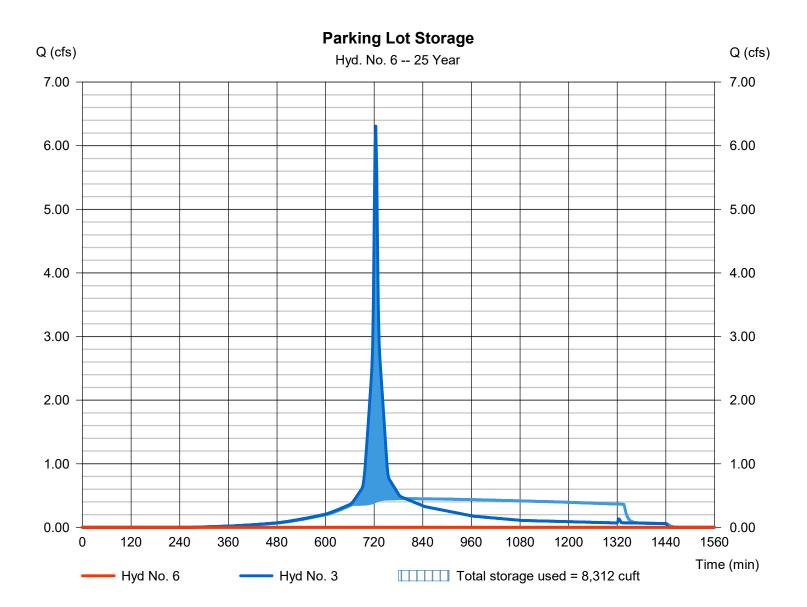
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

# Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 25 yrs	Time to peak	= 618 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 133.25 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 8,312 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Saturday, 05 / 21 / 2022

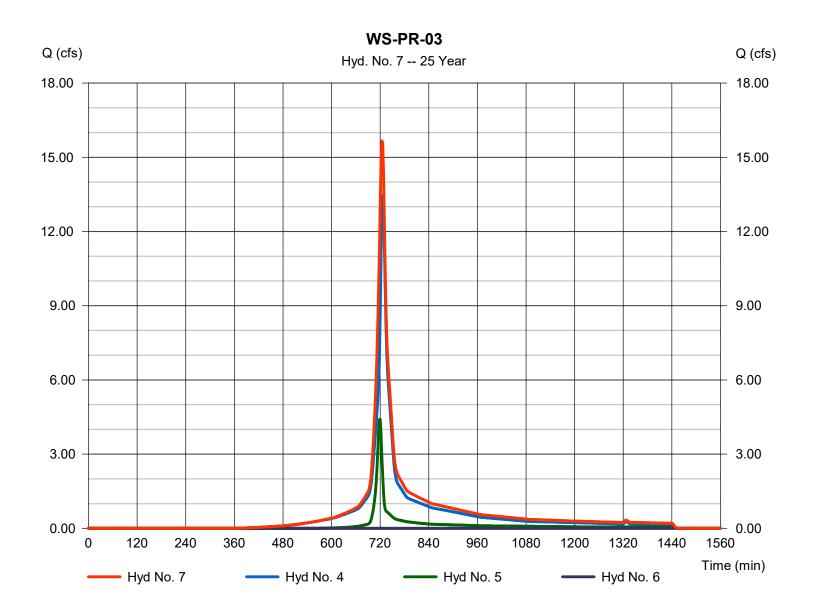
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Saturday, 05 / 21 / 2022

# Hyd. No. 7

## WS-PR-03

Hydrograph type	= Combine	Peak discharge	= 15.66 cfs
Storm frequency	= 25 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 56,533 cuft
Inflow hyds.	= 4, 5, 6	Contrib. drain. area	= 3.817 ac
5	, , , -		



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.278	2	730	5,021				PR-WS-01
2	SCS Runoff	8.695	2	730	35,433				PR-WS-02
3	SCS Runoff	7.288	2	724	22,802				PR-WS-03A
4	SCS Runoff	15.79	2	726	54,818				PR-WS-03B
5	SCS Runoff	5.432	2	718	12,431				PR-WS-03C
6	Reservoir	0.000	2	598	0	3	133.69	10,128	Parking Lot Storage
7	Combine	18.55	2	724	67,249	4, 5, 6			WS-PR-03
	- 969-015 2022		Proposed	Conditio	ne Andrew teurn	Period: 50	Voor	Saturday	05 / 21 / 2022

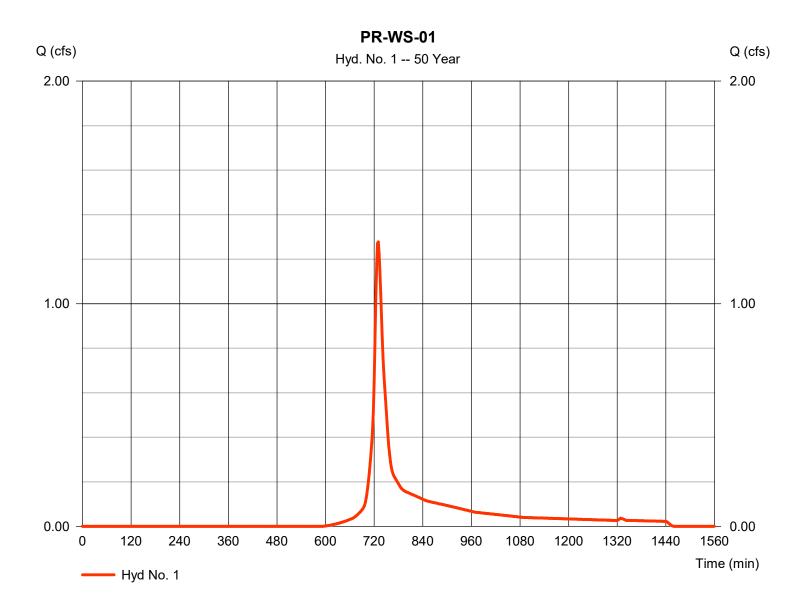
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 1

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.278 cfs
Storm frequency	= 50 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 5,021 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 7.41 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



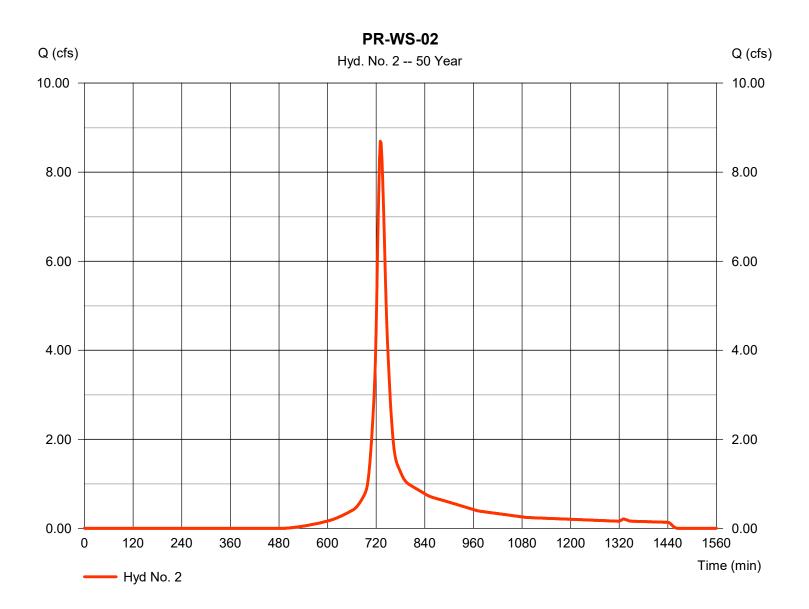
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 2

**PR-WS-02** 

Hydrograph type	= SCS Runoff	Peak discharge	= 8.695 cfs
Storm frequency	= 50 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 35,433 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 7.41 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



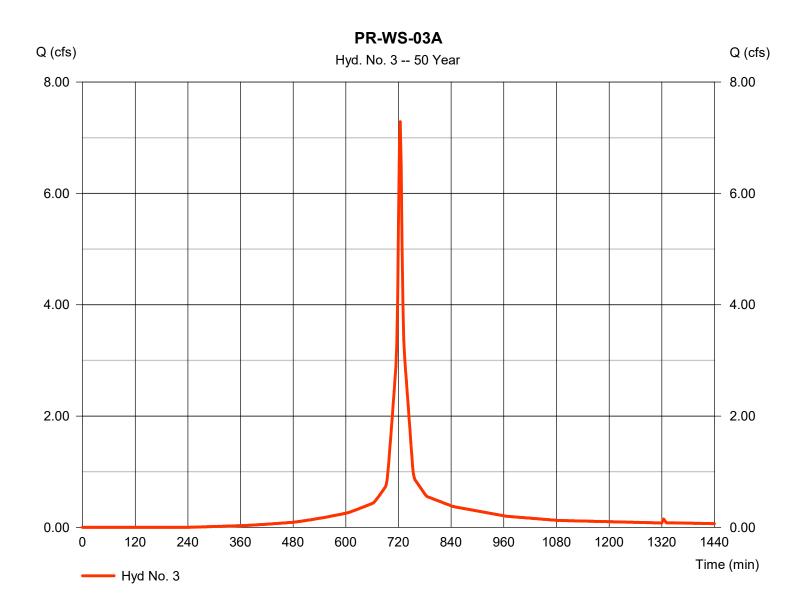
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

Saturday, 05 / 21 / 2022

# Hyd. No. 3

PR-WS-03A

Hydrograph type	= SCS Runoff	Peak discharge	= 7.288 cfs
Storm frequency	= 50 yrs	Time to peak	= 724 min
Time interval	= 2 min	Hyd. volume	= 22,802 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 7.41 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



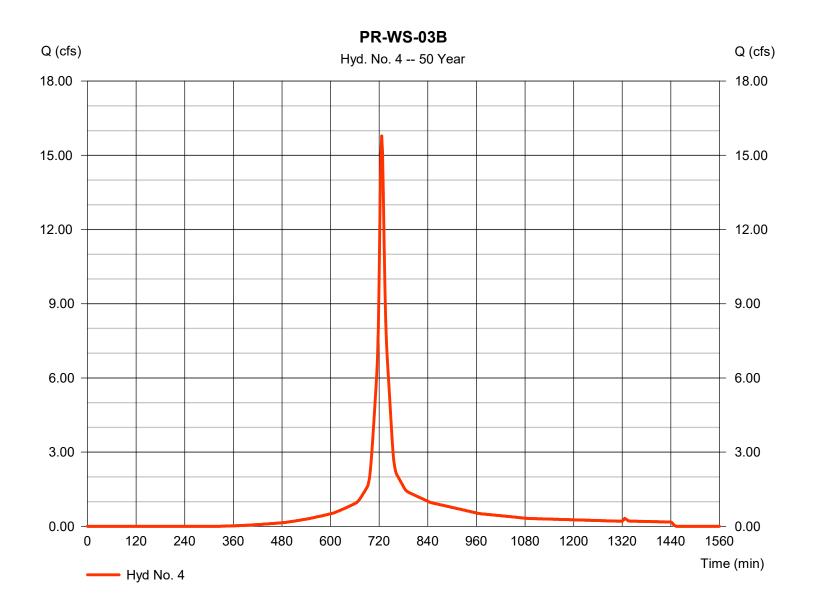
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 15.79 cfs
Storm frequency	= 50 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 54,818 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 7.41 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



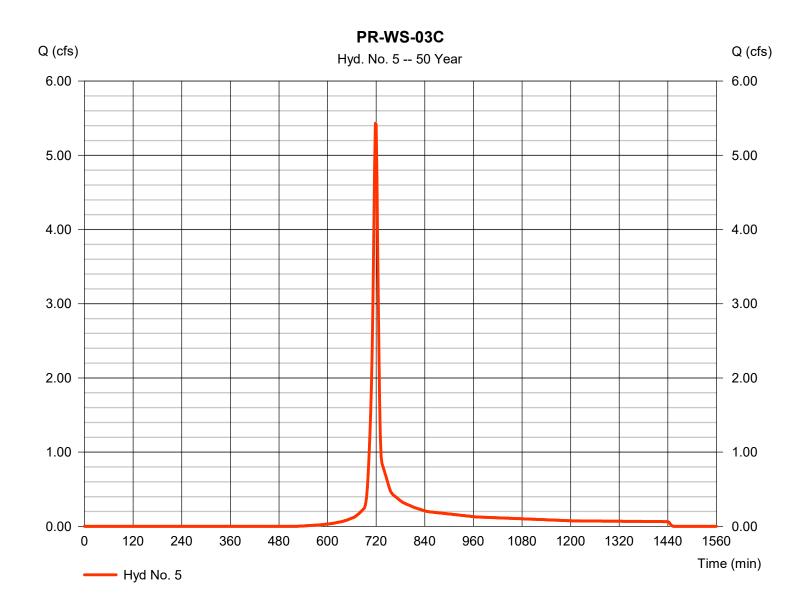
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 5.432 cfs
Storm frequency	= 50 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 12,431 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 7.41 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484
		-	



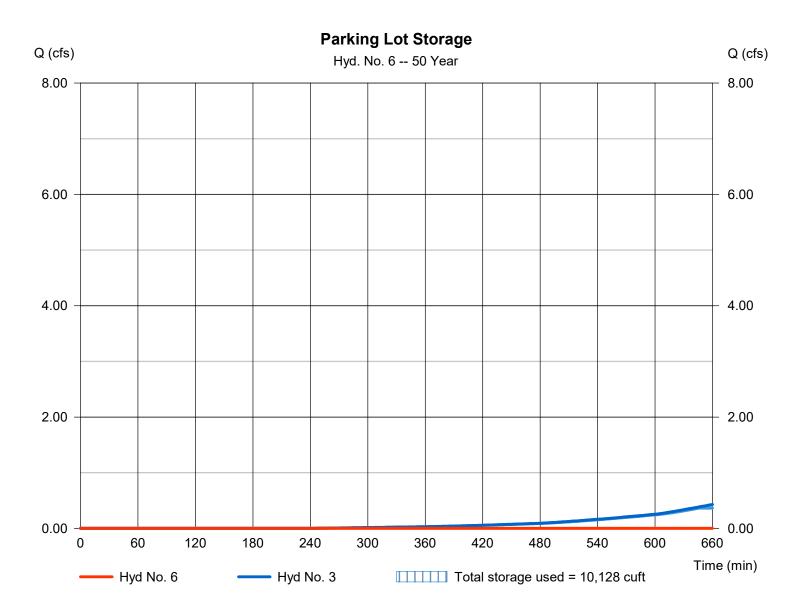
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

# Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 50 yrs	Time to peak	= 598 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 133.69 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 10,128 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Saturday, 05 / 21 / 2022

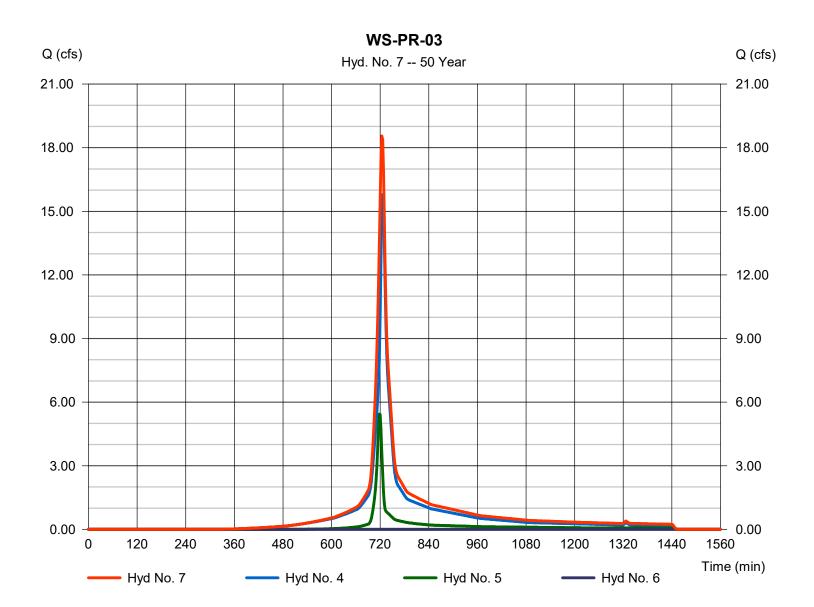
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#### Saturday, 05 / 21 / 2022

# Hyd. No. 7

## WS-PR-03

Hydrograph type	<ul> <li>Combine</li> <li>50 yrs</li> <li>2 min</li> <li>4, 5, 6</li> </ul>	Peak discharge	= 18.55 cfs
Storm frequency		Time to peak	= 724 min
Time interval		Hyd. volume	= 67,249 cuft
Inflow hyds.		Contrib. drain. area	= 3.817 ac
innew nyae.	1, 0, 0		0.017 40



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.596	2	730	6,215				PR-WS-01
2	SCS Runoff	10.46	2	730	42,553				PR-WS-02
3	SCS Runoff	8.346	2	724	26,329				PR-WS-03A
4	SCS Runoff	18.31	2	726	63,976				PR-WS-03B
5	SCS Runoff	6.586	2	718	15,069				PR-WS-03C
6	Reservoir	0.000	2	572	0	3	134.19	12,198	Parking Lot Storage
7	Combine	21.68	2	724	79,046	4, 5, 6			WS-PR-03
	1			1	ns.offcentrurn l			Saturday,	

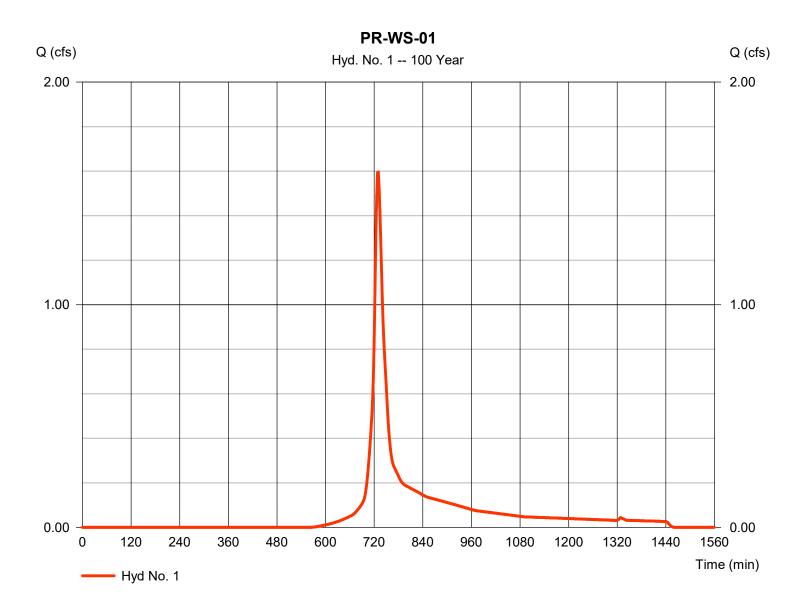
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 1

PR-WS-01

Hydrograph type	= SCS Runoff	Peak discharge	= 1.596 cfs
Storm frequency	= 100 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 6,215 cuft
Drainage area	= 0.458 ac	Curve number	= 60.3
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.40 min
Total precip.	= 8.34 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



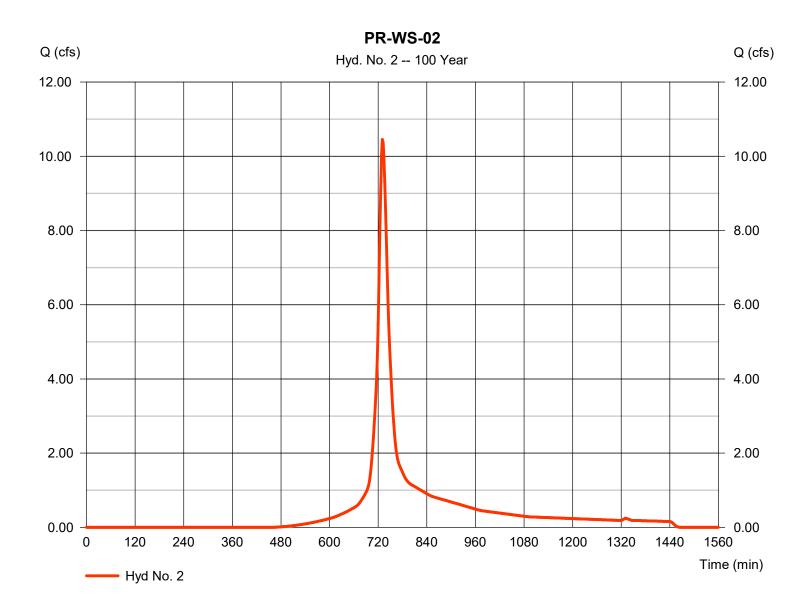
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#### Saturday, 05 / 21 / 2022

# Hyd. No. 2

**PR-WS-02** 

Hydrograph type	= SCS Runoff	Peak discharge	= 10.46 cfs
Storm frequency	= 100 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 42,553 cuft
Drainage area	= 2.527 ac	Curve number	= 70
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 14.80 min
Total precip.	= 8.34 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	



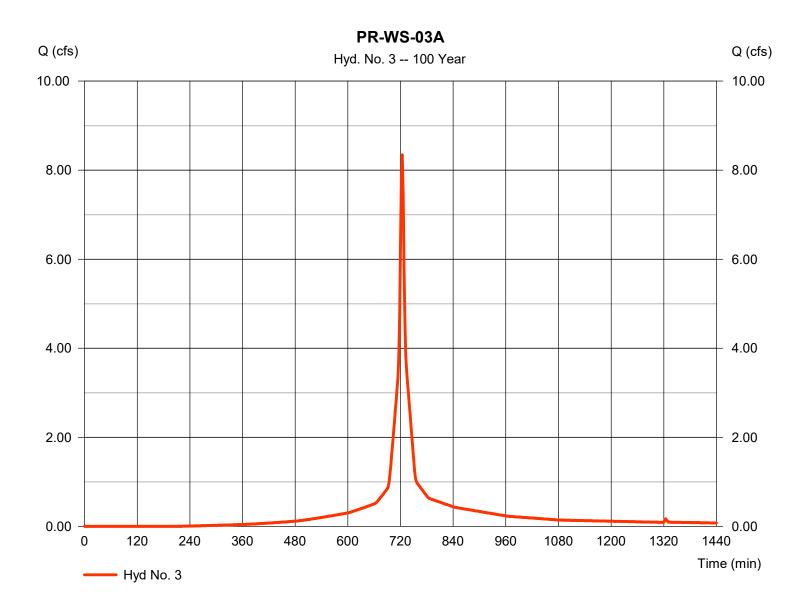
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#### Saturday, 05 / 21 / 2022

# Hyd. No. 3

PR-WS-03A

Hydrograph type Storm frequency	= SCS Runoff = 100 yrs	Peak discharge Time to peak	= 8.346 cfs = 724 min
Time interval	= 2 min	Hyd. volume	= 26,329 cuft
Drainage area	= 1.147 ac	Curve number	= 86.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 8.34 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



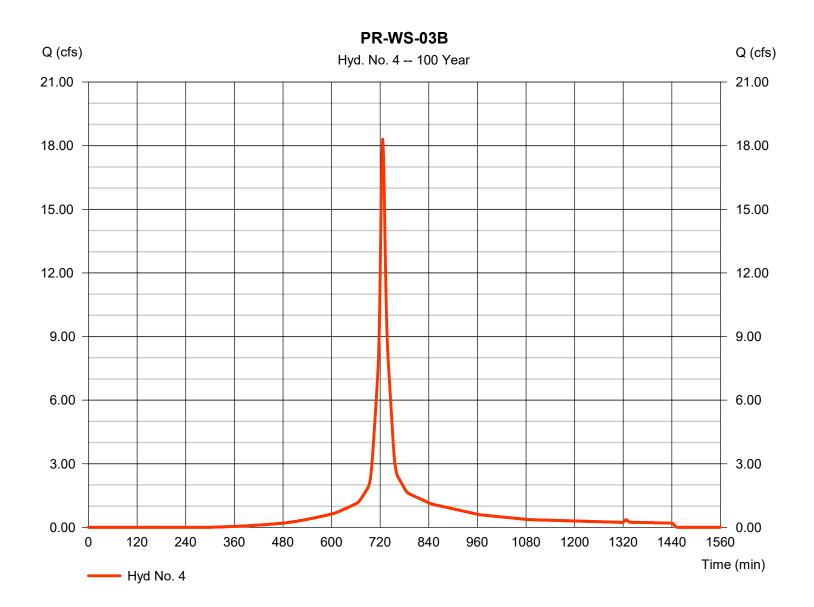
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#### Saturday, 05 / 21 / 2022

# Hyd. No. 4

PR-WS-03B

Hydrograph type	= SCS Runoff	Peak discharge	= 18.31 cfs
Storm frequency	= 100 yrs	Time to peak	= 726 min
Time interval	= 2 min	Hyd. volume	= 63,976 cuft
Drainage area	= 2.867 ac	Curve number	= 81.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 8.80 min
Total precip.	= 8.34 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484
		-	

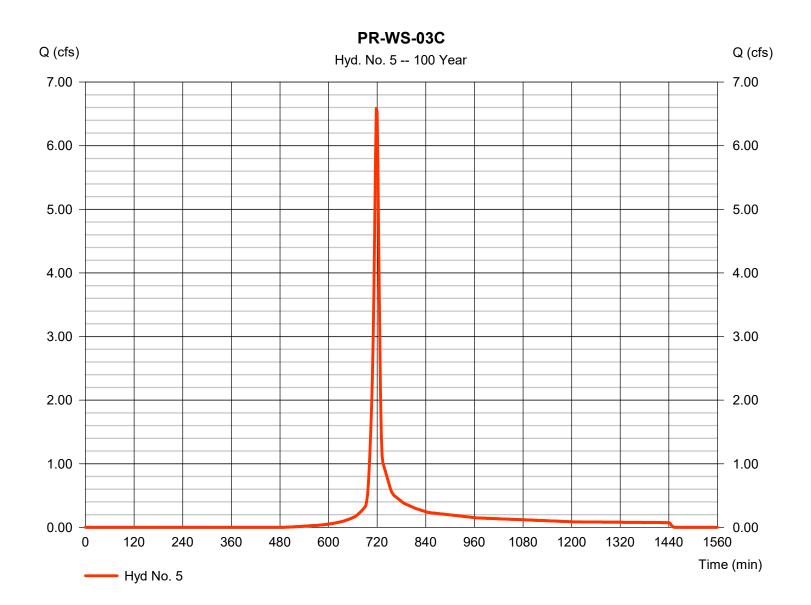


Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

# Hyd. No. 5

PR-WS-03C

Hydrograph type	= SCS Runoff	Peak discharge	= 6.586 cfs
Storm frequency	= 100 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 15,069 cuft
Drainage area	= 0.950 ac	Curve number	= 66.7
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 9.60 min
Total precip.	= 8.34 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484
		-	



Saturday, 05 / 21 / 2022

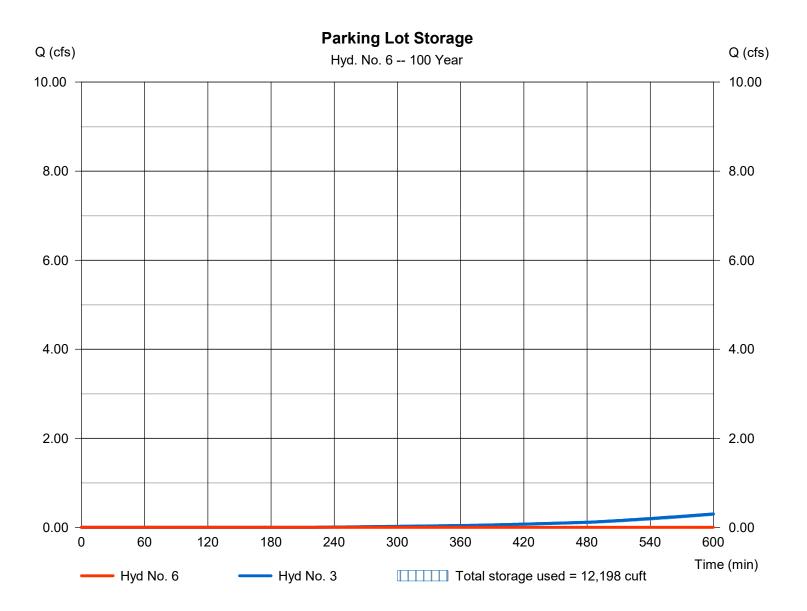
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

# Hyd. No. 6

Parking Lot Storage

Hydrograph type	= Reservoir	Peak discharge	= 0.000 cfs
Storm frequency	= 100 yrs	Time to peak	= 572 min
Time interval	= 2 min	Hyd. volume	= 0 cuft
Inflow hyd. No.	= 3 - PR-WS-03A	Max. Elevation	= 134.19 ft
Reservoir name	= Parking Lot Detention	Max. Storage	= 12,198 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



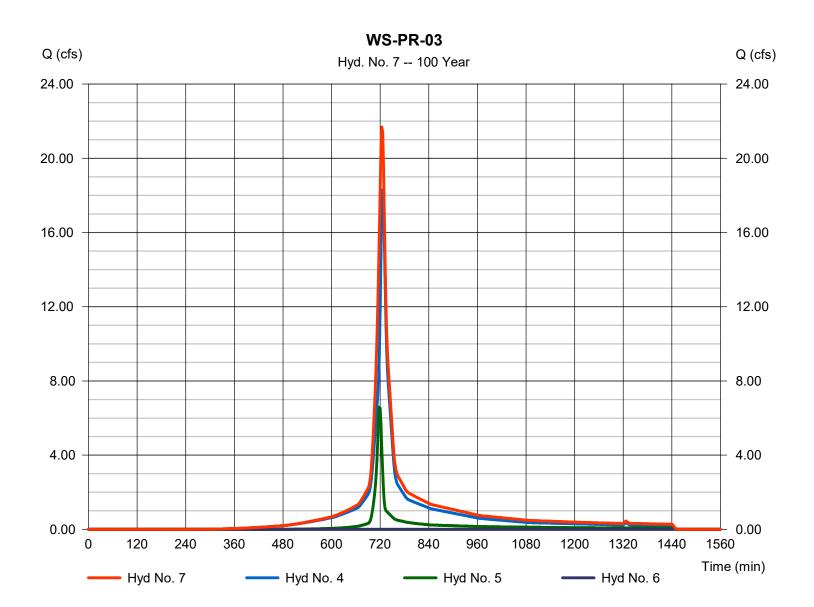
Saturday, 05 / 21 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2021

#### Saturday, 05 / 21 / 2022

# Hyd. No. 7

# WS-PR-03



# **Tighe&Bond**

**APPENDIX D** 



## Designation: CB-01

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.151	0.90	0.136
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.016	0.30	0.005
	0.167		0.140

#### Weighted C: 0.84

#### (computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	300	0.006	6.0

#### Total Tc: 6.0

## Designation: CB-02

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.172	0.90	0.155
Gravel	0.024	0.70	0.017
Wooded	0.029	0.45	0.013
Landscaped and Lawns	0.007	0.30	0.002
	0.232		0.187

#### Weighted C: 0.81

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

	Ov	erland		
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	300	0.006	6.0

## Total Tc: 6.0



## Designation: CB-03

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.037	0.90	0.033
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.005	0.30	0.002
	0.042		0.035

#### Weighted C: 0.82

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Segment Surface "n" Flow Length (ft.) Slope (ft/ft)	
	Time (min.)
Segment A - B 0.015 118 0.005	3.0

Total Tc: 3.0

Minimum Tc: 5.0

## Designation: CB-04

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.026	0.90	0.023
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.000	0.30	0.000
	0.026		0.023

#### Weighted C: 0.90

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.015	89	0.005	2.4	

Total Tc: 2.4

Minimum Tc: 5.0



## Designation: CB-05

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.072	0.90	0.065
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.008	0.30	0.002
	0.080		0.067

#### Weighted C: 0.84

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time	
	(min.)
Segment A - B 0.015 149 0.015 2	2.4

Total Tc: 2.4

Minimum Tc: 5.0

## Designation: CB-06

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.138	0.90	0.124
Gravel	0.027	0.70	0.019
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.000	0.30	0.000
	0.165		0.143

## Weighted C: 0.87

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.4	69	0.261	5.6		
Segment B - C	0.015	21	0.381	0.1		
Segment C - D	0.015	81	0.015	1.4		

#### Total Tc: 7.2

Note:



## Designation: CB-07

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.122	0.90	0.110
Gravel	0.045	0.70	0.032
Wooded	0.209	0.45	0.094
Landscaped and Lawns	0.000	0.30	0.000
	0.376		0.236

#### Weighted C: 0.63

## Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)		
Segment A - B	0.4	127	0.472	7.2		
Segment B - C	0.015	25	0.400	0.2		
Segment C - D	0.015	81	0.037	1.0		

Total Tc: 8.4

## Designation: CB-08

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.037	0.90	0.033
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.007	0.30	0.002
	0.044		0.035

Weighted C: 0.81

## **Time of Concentration**

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	105	0.029	1.4

Total Tc: 1.4

Minimum Tc: 5.0



## Designation: CB-09

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.088	0.90	0.079
Gravel	0.000	0.70	0.000
Wooded	0.252	0.45	0.113
Landscaped and Lawns	0.010	0.30	0.003
	0.350		0.196

#### Weighted C: 0.56

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.4	151	0.46	8.4	
Segment B - C	0.015	40	0.05	0.5	

Total Tc: 8.9

## Designation: CB-10

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.060	0.90	0.054
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.000	0.30	0.000
	0.060		0.054

#### Weighted C: 0.90

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment		Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment	: A - B	0.015	163	0.047	1.6	

Total Tc: 1.6

Minimum Tc: 5.0



## Designation: CB-11

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.158	0.90	0.142
Gravel	0.000	0.70	0.000
Wooded	0.091	0.45	0.041
Landscaped and Lawns	0.010	0.30	0.003
	0.259		0.186

#### Weighted C: 0.72

#### **Time of Concentration** (computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.4	39	0.103	5.2	
Segment B - C	0.015	226	0.071	1.8	

Total Tc: 6.9

## Designation: CB-12

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.059	0.90	0.053
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.017	0.30	0.005
	0.076		0.058

#### Weighted C: 0.76

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.015	161	1	0.5	
	01010	101		0.0	

Total Tc: 0.5

Minimum Tc: 5.0



## Designation: CB-13

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.087	0.90	0.079
Gravel	0.000	0.70	0.000
Wooded	0.002	0.45	0.001
Landscaped and Lawns	0.008	0.30	0.002
	0.097		0.082

#### Weighted C: 0.84

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	168	0.071	1.4

## Designation: CB-14

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.051	0.90	0.046
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.000	0.30	0.000
	0.051		0.046

#### Weighted C: 0.90

## Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.015	142	1	0.4	

Total Tc: 0.4

#### Minimum Tc: 5.0



## Designation: CB-15

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.058	0.90	0.053
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.008	0.30	0.002
	0.066		0.055

#### Weighted C: 0.83

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.015	114	0.061	1.1	

Total Tc: 1.1

Minimum Tc: 5.0

## Designation: CB-16

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.052	0.90	0.047
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.023	0.30	0.007
	0.075		0.053

#### Weighted C: 0.71

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.24	25	0.400	1.4	
Segment B - C	0.015	96	0.052	1.0	

Total Tc: 2.4

Minimum Tc: 5.0

Note:



## Designation: CB-17

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.049	0.90	0.044
Gravel	0.000	0.70	0.000
Wooded	0.191	0.45	0.086
Landscaped and Lawns	0.038	0.30	0.011
	0.277		0.141

#### Weighted C: 0.51

## **Time of Concentration**

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.015	118	0.034	1.4

Total Tc: 1.4

Minimum Tc: 5.0

## Designation: CB-18

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.056	0.90	0.051
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.000	0.30	0.000
	0.056		0.051

#### Weighted C: 0.90

## Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.4	132	0.106	13.6	

#### Total Tc: 13.6



#### Designation: SW-01

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.000	0.90	0.000
Gravel	0.000	0.70	0.000
Wooded	0.200	0.45	0.090
Landscaped and Lawns	0.000	0.30	0.000
	0.200		0.090

#### Weighted C: 0.45

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland				
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.4	127	0.409	7.7

#### Total Tc: 7.7

## Designation: **YD-01**

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.205	0.90	0.184
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.081	0.30	0.024
	0.285		0.208

#### Weighted C: 0.73

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland						
Segment Surface "n" Flow Length (ft.) Slope (ft/ft) Time (min						
Segment A - B	0.015	121	0.005	3.1		
Segment B - C	0.24	20	0.050	2.7		

#### Total Tc: 5.8



## Designation: **YD-02**

**Time of Concentration** 

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.000	0.90	0.000
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.046	0.30	0.014
	0.046		0.014

#### Weighted C: 0.30

#### (computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

Overland					
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)	
Segment A - B	0.24	25	0.500	1.3	
Segment B - C	0.24	90	0.067	8.0	

#### Total Tc: 9.2

## Designation: YD-03

Cover Type	Area, ac	Coef.	A x C
Hardscape/Rock	0.000	0.90	0.000
Gravel	0.000	0.70	0.000
Wooded	0.000	0.45	0.000
Landscaped and Lawns	0.078	0.30	0.023
	0.078		0.023

#### Weighted C: 0.30

# Time of Concentration

(computed in accordance with ConnDOT Drainage Manual, Sec. 6C)

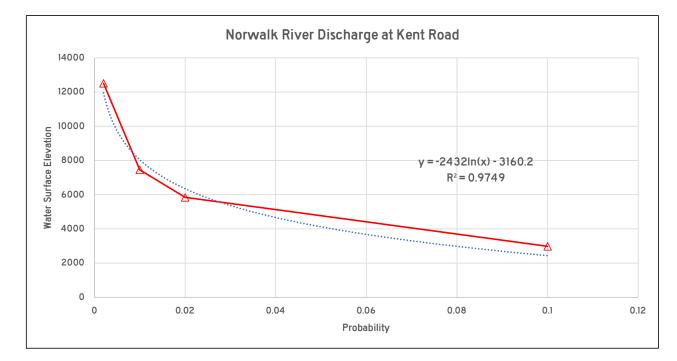
	Ov	erland		
Segment	Surface "n"	Flow Length (ft.)	Slope (ft/ft)	Time (min.)
Segment A - B	0.24	24	0.500	1.2
Segment B - C	0.24	90	0.056	8.6

#### Total Tc: 9.8

#### 2-YEAR DISCHARGE COMPUTATION ASML CAMPUS TRAFFIC SAFETY IMRPOVEMENTS 22-May-22



By; J. Canas

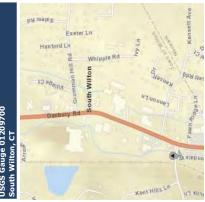


Frequency	Probability	FIS	Computed
10	0.1	2980	2440
50	0.02	5840	6354
100	0.01	7455	8040
500	0.002	12505	11954
2	0.5		344.10



				Ranking of	Kanking of Gauging Data		Exceedence
Jued	TEAN	Peak Flow	0.00	(log Q - avg(log0))^2	(log Q - avo(log())^3	Return Period	Probability
1	1956	12,000	4.0792	1.0887	1.1359	47.0000	0.0213
2	2007	3,490	3.5428	0.2571	0.1304	23.5000	0.0426
e	2011	2,440	3.3874	0.1236	0.0435	15.6667	0.0638
4	2006	2,340	3.3692	0.1112	0.0371	11.7500	0.0851
5	1980	2,300	3.3617	0.1062	0.0346	9.4000	0.1064
9	1979	1,940	3.2878	0.0635	0.0160	7.8333	0.1277
~	2021	1,870	3.2718	0.0557	0.0132	6.7143	0.1489
8	2010	1,830	3.2625	0.0514	0.0116	5.8750	0.1702
6	1989	1,800	3.2553	0.0482	0.0106	5.2222	0.1915
10	1999	1,720	3.2355	0.0399	0.0080	4.7000	0.2128
;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	1987	1,710	3.2330	0.0389	0.0077	4.2727	0.2340
12	1972	1,690	3.2279	0.0369	0.00/1	3.9167	0.2553
13	1984	1,690	3.2279	0.0369	0.0071	3.6154	0.2766
14	1970	1,660	3.2201	0.0340	0.0063	3.3571	0.2979
15	1973	1,610	3.2068	0.0293	0.0050	3.1333	0.3191
16	1974	1,540	3.1875	0.0230	0.0035	2.9375	0.3404
17	1996	1,510	3.1790	0.0205	0.0029	2.7647	0.3617
18	1978	1,480	3.1703	0.0181	0.0024	2.6111	0.3830
19	1983	1,480	3.1703	0.0181	0.0024	2.4737	0.4043
20	1977	1,440	3.1584	0.0150	0.0018	2.3500	0.4255
21	1982	1,400	3.1461	0.0122	0.0013	2.2381	0.4468
22	1997	1,400	3.1461	0.0122	0.0013	2.1364	0.4681
23	1971	1,360	3.1335	0.0096	0.0009	2.0435	0.4894
24	1991	1,360	3.1335	0.0096	0.0009	1.9583	0.5106
52 96	2004	1,340	3.1206	0.0083	0.000	1.88UU 1.8077	0.5537
27	1976	1.290	3.1106	0.0056	0.0004	1.7407	0.5745
28	2014	1,280	3.1072	0.0051	0.0004	1.6786	0.5957
29	2019	1,270	3.1038	0.0046	0.0003	1.6207	0.6170
30	2009	1,230	3.0899	0.0029	0.0002	1.5667	0.6383
31	1975	1,220	3.0864	0.0026	0.0001	1.5161	0.6596
32	2020	1,200	3.0792	0.0019	0.0001	1.4688	0.6809
55	2018	1,190	3.0/2	0.0016	0,000	1.4242	0./021
04 25	1007	1 000 T	3.0374	0.000		1 3429	0.7234 07447
36	1968	1,020	3.0086	0.0007	0.0000	1.3056	0.7660
37	1990	1,010	3.0043	0.0010	0.0000	1.2703	0.7872
38	1985	696	2.9863	0.0024	-0.0001	1.2368	0.8085
39	1986	962	2.9832	0.0028	-0.0001	1.2051	0.8298
40	2005	892	2.9504	0.0073	-0.0006	1.1750	0.8511
41	2015	831	2.9196	0.0135	-0.0016	1.1463	0.8723
42	1963	715	2.8543	0.0329	-0.0060	1.1190	0.8936
43	1964	CT/	2,8243	0.0329	-0.0065	1.0597	0.9149
41	2001	672	2.0494	0.0347	10000-	1 0444	0.9502
46	2001	655	2.8162	0.0482	-0.0106	1.0217	0.9787
47	2013	618	2.7910	0.0599	-0.0147	1.0000	1.0000
48	1992	612	2.7868	0.0620	-0.0154	0.9792	1.0213
49	2003	586	2.7679	0.0718	-0.0192	0.9592	1.0426
20	1981	560	2.7482	0.0827	-0.0238	0.9400	1.0638
21	2007	950	2./451	0.0845	-0.0246	0126.0	1.0801
22	1998 2017	517	2./165	0.1007	-0.0335	0.9050	1 1 2 7 7
54	2000	495	2.6946	0.1164	-0.0397	0.8704	1.1489
55	2016	477	2.6785	0.1276	-0.0456	0.8545	1.1702

				Ignexbond	
Log-Pearson Distribution Analysis, Flows at South Wilton, CT Gauging Sta.	alysis, Flov	vs at Soutl	h Wilton, CT Ga	uging Sta.	
No. of Years in Record	60 60				
Avg. Q Peak	13/b.33				
Avg. log Q Sum //hog O - avo/hog O1)^2\	0CU.C				
Sum {(loa O - ava(loa O))^3}	0.693				
	0.0747				
Std. Dev. log Q	0.2733				
Skewness (C <sub>s</sub> )	0.5953				
Skew coefficient (C <sub>m</sub> )	0.70		- from USGS Publication 17B	8	
Variance of Regional Skewness V(C <sub>m</sub> )	0.302	- 0.302 for U.S.	- U.S.		
A = - 0.52 + 0.3(C.)	-0.34141				
$B = 0.94 - 0.26(C_s)$	0.78523				
Variance of Station Skewness V(C <sub>s</sub> )	0.111574	$V(C_s) = 10$	$V(C_s) = 10^{[A-B^*(log(n/10))]}$		
Weighting Factor (W)	0.73022	$W = V(C_m)$	$W = V(C_m)/[V(C_s)+V(C_m)]$		
Weighted Skewness (C <sub>w</sub> )	0.62354	C <sub>w</sub> = [W*C	$C_{w} = [W^{*}C_{s}] + [(1-W)^{*}C_{m}]$		
Table Upper C <sub>w</sub> Value	0.7	- from Table 7.7	le 7.7		
Table Lower C <sub>w</sub> Value	0.6	- from Table 7.7	le 7.7		
Calculated C <sub>w</sub> Value	0.62354				
Return Period, T, K lower	K lower	K upper	Slope K c	K calculated	Q (cfs)
2	-1.880	-1.506	3.74	-1.792	352
S		0.790	-0.1	0.798	1794
10		1.333	0.05	1.329	2506
25		1.967	0.28	1.946	3694
50		2.407	0.48	2.370	4826
100		2.824	0.69	2.771	6211
200	3.132	3.223	16.0	٤٢١.٤	006/
USGS Gauge 01209700			Transposition of Flow to Site	of Flow to	Site
South Wilton, CT					



Cfs

Using Transposition Eqn

 $Q_1 = Q_2 \sqrt{\frac{A_1}{A_2}}$ 

6.

100-Year Event Q<sub>2</sub>, Flow at Gauged Site A<sub>1</sub>, Watershed at Site A<sub>2</sub>, Watershed at Gauge

		_	_	_
1.1915	1.2128	1.2340	1.2553	1.2766
0.8393	0.8246	0.8103	0.7966	0.7833
-0.0481	-0.0816	-0.1062	-0.1189	-0.1577
0.1323	0.1881	0.2242	0.2418	0.2919
2.6721	2.6021	2.5623	2.5441	2.4955
470	400	365	350	313
1965	1988	1967	1966	1995
56	57	58	59	60

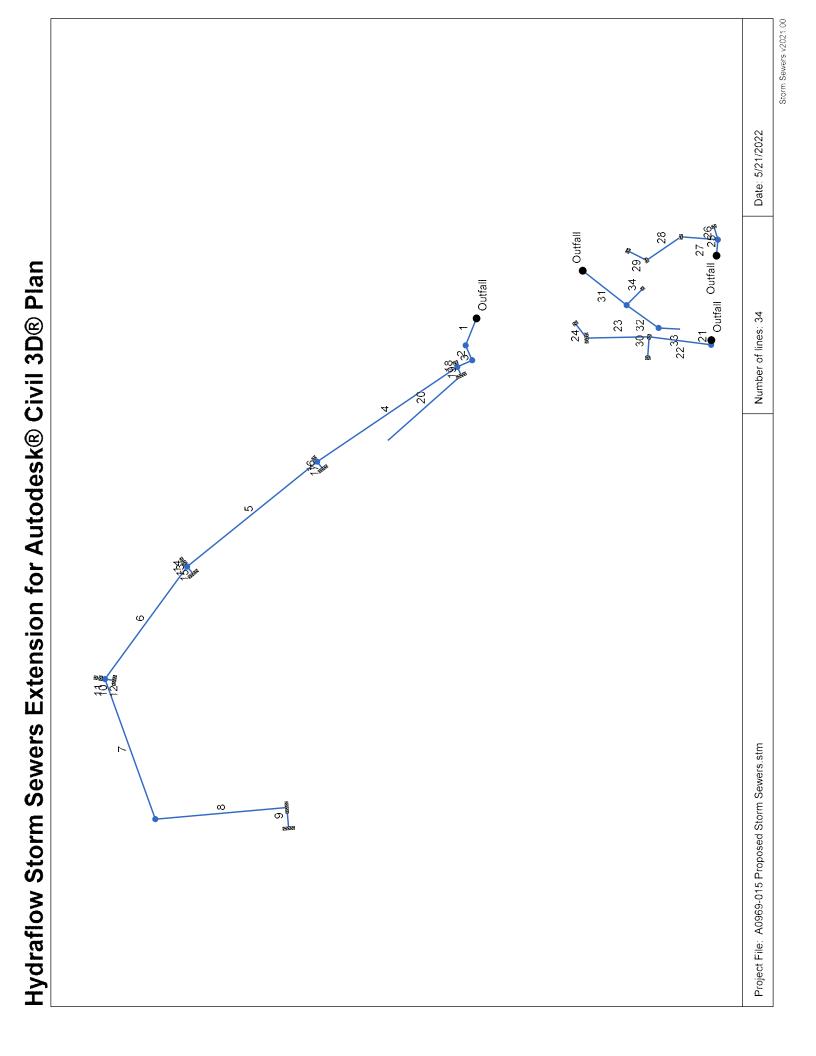
6								
/EIGHTED	I	2	5	Recurren 10	Recurrence Interval In Years 10 25	fears 50	100	200
SKEW COEFI	66	G.	02	Percent	Percent Chance (>=) =	= 1-F 2	-	0.5
	-0.667	-0.396	0.42	1.18	2.278	3.152	4.051	4.97
2.9	-0.69	-0.39	0.44	1.195	2.277	3.134	4.013	4.904
2.8	-0.714	-0.384	0.46	1.21	2.275	3.114	3.973	4.847
2.7	-0.74	-0.376	0.479	1.224	2.272	3.093	3.932	4.783
2.5	-0.799	-0.36	0.518	1.25	2.262	3.048	3.845	4.652
2.4	-0.832	-0.351	0.537	1.262	2.256	3.023	3.8	4.584
2.3	-0.867	-0.341	0.555	1.274	2.248	2.997	3.753	4.515
2.2	-0.905	-0.33	0.574	1.284	2.24	2.97	3.705	4.444
2.1	-0.946	-0.319	0.592	1.294	2.23	2.942	3.656	4.372
7 7	-0.99	-0.307	0.609	1.302	2.219	2.912	3.605	4.298
1.4 1.4	-1.03/	-0.294	0.643	1 218 1 218	2.207	188.2	566.5 001 5	4.223
1.7	-1.14	-0.268	0.66	1.324	2.179	2.815	3.444	4.069
1.6	-1.197	-0.254	0.675	1.329	2.163	2.78	3.388	3.99
1.5	-1.256	-0.24	0.69	1.333	2.146	2.743	3.33	3.91
1.4	-1.318	-0.225	0.705	1.337	2.128	2.706	3.271	3.828
	-1.383	-0.21	0./19	1.339	2.108	2.666	3.211	3./45
7.7	-1.518	-0.18	0.745	1.341	2.066	2.585	3.149 3.087	3.575
	-1.588	-0.164	0.758	1.34	2.043	2.542	3.022	3.489
0.9	-1.66	-0.148	0.769	1.339	2.018	2.498	2.957	3.401
0.8	-1.733	-0.132 -0.116	0.78	1.336	1.993	2.453	2.891	3.312
0.6	-1.88	-0.099	0.8	1.328	1.939	2.359	2.755	3.132
0.5	-1.955	-0.083	0.808	1.323	1.91	2.311	2.686	3.041
0.3	-2.104	-0.05	0.824	1.309	1.849	2.211	2.013	2.949
0.2	-2.178	-0.033	0.83	1.301	1.818	2.159	2.472	2.763
0.1	-2.252	-0.017	0.836	1.292	1.785	2.107	2.4	2.67
0.1	-2.4	0.017	0.846	1.27	1.716	2	2.252	2.482
-0.2	-2.472	0.033	0.85	1.258	1.68	1.945	2.178	2.388
0.0 0	-2.544	0.05	0.853	1.245	1.643	1 024	2.104	2.294
-0.5	-2.686	0.083	0.856	1.216	1.567	1.777	2.029 1.955	2.108
-0.6	-2.755	0.099	0.857	1.2	1.528	1.72	1.88	2.016
0.7	-2.824	0.116	0.857	1.183	1.488	1.663	1.806	1.926
0.9 -0.9	-2.957	0.148	0.854	1.147	1.407	1.549	1.66	1.749
÷	-3.022	0.164	0.852	1.128	1.366	1.492	1.588	1.664
1.1	-3.087	0.18	0.848	1.107	1.324	1.435	1.518	1.581
7.7	-3.149 -3.211	C6T.0	0.844	1 064	1 24	1 374	1.449 1.383	1 424
-1.4	-3.271	0.225	0.832	1.041	1.198	1.27	1.318	1.351
-1.5	-3.33	0.24	0.825	1.018	1.157	1.217	1.256	1.282
-1.6	-3.88	0.254	0.817	0.994	1.116	1.166	1.197	1.216
-1.8	-3.499	0.282	0.799	0.945	1.035	1.069	1.087	1.097
-1.9	-3.553	0.294	0.788	0.92	0.996	1.023	1.037	1.044
- 1-	-3.656	0.307	0.765	0.869	0.933	0.30	0 946	0490
-2.2	-3.705	0.33	0.752	0.844	0.888	0.9	0.905	0.907
-2.3	-3.753	0.341	0.739	0.819	0.855	0.864	0.867	0.869
-2.5	-3.0	0.36	0.711	0.711	0.793	0.798	269:0	0.8
-2.6	-3.899	0.368	0.696	0.747	0.764	0.768	0.769	0.769
-2.7	-3.932	0.376	0.681	0.724	0.738	0.74	0.74	0.741
-2.9	-4.013	0.39	0.651	0.681	0.683	0.689	0.69	0.69
ę	-4.051	0.396	0.636	0.66	0.666	0.666	0.667	0.667

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Reach-1 Reach-1 Reach-1 Reach-1 Reach-1			U IOTAI	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
Reach-1 Reach-1 Reach-1 Reach-1			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1 Reach-1 Reach-1 Reach-1	29920	50% Chance	347.00	147.00	148.79	148.79	149.36	0.012637	6.07	57.54	51.97	1.00
Reach-1 Reach-1 Reach-1	29760	50% Chance	347.00	142.20	144.79		144.88	0.001279	2.43	142.56	87.81	0.34
Reach-1 Reach-1	28240	50% Chance	347.00	138.00	139.78	139.78	140.33	0.012939	5.93	58.63	54.94	1.01
Reach-1	27468	50% Chance	347.00	132.10	138.74		138.74	0.000001	0.10	4715.82	499.27	0.01
	27110	50% Chance	347.00	136.60	138.64		138.72	0.001351	2.79	231.26	179.61	0.36
Reach-1	27025	50% Chance	347.00	135.50	138.16	137.47	138.47	0.003089	4.51	81.60	43.66	0.55
Reach-1	27020		Bridge									
Reach-1	27015	50% Chance	347.00	135.50	138.07	137.48	138.41	0.003540	4.70	78.00	43.22	0.58
Reach-1	26680	50% Chance	347.00	134.00	137.02	136.34	137.33	0.002861	4.63	100.21	80.84	0.54
Reach-1	26209	50% Chance	347.00	133.40	134.83		135.24	0.007705	5.15	67.38	50.53	0.79
Reach-1	26136	50% Chance	347.00	130.20	134.92	132.33	135.01	0.000375	2.41	144.06	56.00	0.21
Reach-1	26127.5		Bridge									
Reach-1	26119	50% Chance	347.00	131.30	134.69	133.14	134.80	0.000838	2.65	130.95	49.09	0.29
Reach-1	26058	50% Chance	347.00	131.30	134.63	133.13	134.74	0.000900	2.71	128.03	49.03	0.30
Reach-1	25358	50% Chance	347.00	131.00	132.57	132.56	133.12	0.012416	6.66	77.85	80.61	1.02
Reach-1	25340	50% Chance	347.00	128.10	132.91		132.96	0.000197	1.81	370.12	299.31	0.15
Reach-1	25334	50% Chance	347.00	130.31	132.86		132.95	0.001293	2.74	198.44	154.16	0.35
Reach-1	24975	50% Chance	347.00	129.20	131.12	131.12	131.83	0.012066	6.76	51.33	36.52	1.01
Reach-1	24922	50% Chance	347.00	127.89	131.26		131.40	0.001135	3.04	114.26	45.49	0.34
Reach-1	24677	50% Chance	347.00	127.87	131.20		131.24	0.000316	1.64	211.54	81.18	0.18
Reach-1	24620	50% Chance	347.00	128.90	130.62	130.62	131.14	0.013758	5.76	60.25	60.21	1.01
Reach-1	24597	50% Chance	347.00	127.30	129.76		129.90	0.001952	3.07	112.94	66.00	0.41
Reach-1	24570	50% Chance	347.00	127.60	129.61	129.09	129.83	0.003297	3.78	91.86	66.39	0.54
Reach-1	24542.5		Bridge									
Reach-1	24540	50% Chance	347.00	127.60	129.09	129.09	129.59	0.013128	5.72	60.69	64.37	1.00
Reach-1	24485	50% Chance	347.00	126.30	128.59		128.92	0.003896	4.64	83.39	49.80	0.60
Reach-1	24430	50% Chance	347.00	126.60	128.37		128.60	0.007804	3.87	89.65	69.12	0.60
Reach-1	24401	50% Chance	347.00	124.66	128.33		128.44	0.002561	2.60	133.48	76.83	0.35
Reach-1	24381	50% Chance	347.00	124.66	128.22		128.39	0.001523	3.47	116.23	69.19	0.39
Reach-1	24180	50% Chance	347.00	124.70	127.92		128.07	0.001616	3.14	110.60	54.80	0.39
Reach-1	24105	50% Chance	347.00	124.80	127.66		127.90	0.002882	3.94	88.15	46.92	0.51
Reach-1	23805	50% Chance	347.00	124.00	127.15		127.30	0.001373	3.12	111.32	49.16	0.37
Reach-1	23415	50% Chance	347.00	123.00	125.31	125.31	126.04	0.012066	6.85	50.63	35.13	1.01
Reach-1	23171	50% Chance	347.00	120.30	124.40		124.54	0.001195	3.02	115.02	47.99	0.34
Reach-1	23036	50% Chance	347.00	121.70	123.84	123.44	124.22	0.005348	4.91	70.69	43.93	0.68
Reach-1	22916	50% Chance	347.00	121.00	122.62	122.62	123.25	0.012502	6.38	54.41	43.39	1.00
Reach-1	22765	50% Chance	347.00	114.20	121.53		121.54	0.000024	0.71	492.28	88.75	0.05
Reach-1	22450	50% Chance	347.00	116.90	121.30		121.49	0.001549	3.51	98.76	31.38	0.35
Reach-1	22140	50% Chance	347.00	117.00	120.52		120.83	0.002978	4.50	84.83	77.39	0.54
Reach-1	21825	50% Chance	347.00	115.90	120.52		120.57	0.000249	1.82	217.68	69.79	0.17

HEC-RAS PI	an: EXIST Rive	HEC-RAS Plan: EXIST River: RIVER-1 Reach: Reach-1 Profile: 50% Chance (Continued)	h: Reach-1 Pr	ofile: 50% Cha	ince (Continued	(						
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	21770	50% Chance	347.00	115.40	120.52	116.98	120.55	0.000079	1.19	290.68	91.28	0.10
Reach-1	21757.5		Bridge									
Reach-1	21745	50% Chance	347.00	115.40	120.52	116.98	120.54	0.000079	1.19	290.53	91.26	0.10
Reach-1	21695	50% Chance	347.00	114.20	120.52		120.54	0.000090	1.20	288.09	67.17	0.10
Reach-1	21285	50% Chance	347.00	114.30	120.50	115.93	120.51	0.000042	0.87	406.46	101.77	0.07

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(Continued	
% Chance	
Profile: 50	
Reach: Reach-1	
River: RIVER-1	
Plan: EXIST	
EC-RAS	



Stc	Storm		ver	Tal	Sewer Tabulation	Itiol	~															Page 1
Station		Len	Drng Area		Rnoff	Area x C	U	Чc	v	Rain T	Total C	Cap V	Vel	Pipe	<u> </u>	Invert Elev	>	HGL Elev	>	Grnd / Rim Elev	m Elev	Line ID
Line	To I ine		Incr	Total		Incr	Total	Inlet	Syst			5	رن <sub>ا</sub>	Size S	Slope D	Du	цр	Dn	٩Ŋ	Dn	цр	
		(11)	(ac)	(ac)	(C)			(min)	(min) (	(in/hr)	(cfs)	(cfs)	(ft/s) (i	(in) ('	(%)	(ft)	(#)	(ft)	(ft)	(tt)	(ft)	
<del>.</del>	End	25.034	0.00	1.72	00.0	0.00	1.07	0.0	16.7	4.7	5.04	22.97	4.66	24	0.88	134.00	134.22	134.72	135.01	134.00	141.00	Pipe - (12)
0				1.72	0.00	0.00	1.07	0.0	16.7	2		34.65	4.37			134.22	134.50	135.01	135.29	141.00	141.90	Pipe - (11)
ო	2	14.000	0.00	1.72	0.00	0.00	1.07	0.0	16.6	4.7	5.06	34.65	4.81	24	2.00	134.60	134.88	135.29	135.67	141.90	142.85	Pipe - (10)
4	ო	146.000	0.00	1.11	0.00	0.00	0.73	0.0	16.3	4 8.8	3.49	27.87	7.49	6	6.00	138.71	147.47	139.07	148.18	142.85	151.75	Pipe - (09)
ъ	4	144.000	0.00	0.77	0.00	0.00	0.48	0.0	15.6	4.9	2.36	30.51	3.60	18	7.19	147.57	157.93	148.18	158.51	151.75	162.25	Pipe - (08)
9	ц,	120.000	0.00	0.57	0.00	0.00	0.34	0.0	15.1	5.0	1.68	30.95	3.76	6	7.40	158.09	166.97	158.51	167.46	162.25	171.10	Pipe - (07)
7	Q	128.000	0.00	0.34	0.00	0.00	0.20	0.0	14.3	5.2	1.01	11.38	2.87	6	1.00	167.07	168.35	167.46	168.73	171.10	176.50	Pipe - (06)
ø	~	114.000	0.28	0.34	0.51	0.14	0.20	5.0	13.7	5.3	1.04	8.04	3.04	18	0.50	168.45	169.02	168.81	169.40	176.50	172.70	CB-02
6	ω	18.000	0.06	0.06	06.0	0.05	0.05	13.6	13.6	5.3	0.29	3.86	2.56	12	1.00	169.27	169.45	169.45	169.67	172.70	172.70	Pipe - (04)
10	9	4.000	0.08	0.16	0.71	0.06	0.08	5.0	9.8	6.3	0.51	11.06	3.54	15	2.50	167.35	167.45	167.53	167.73	171.10	170.70	Pipe - (14)
<u>+</u> 4	10 6	4.000 8.000	0.08 0.07	0.08 0.07	0.30 0.83	0.02 0.06	0.02 0.06	9.8 5.0	9.8 5.0	8.6.3 8.6	0.15 0.50	11.06 9.89	2.06 2.08	15	2.50	167.60 167.09	167.70 167.25	167.73 167.46	167.85 167.52	170.70 171.10	170.90 170.90	Pipe - (15)
13	ъ	4.000	0.05	0.10	06.0	0.05	0.06	5.0	9.2	6.5	0.39	11.06	3.28	15	2.50	158.45	158.55	158.61	158.79	162.25	162.00	Pipe - (18)
14	13	4.000	0.05	0.05	0.30	0.02	0.02	9.2	9.2	6.5	0.10	11.06	2.20	15	2.50	158.80	158.90	158.88	159.02	162.00	162.20	Pipe - (17)
15	ъ	8.000	0.10	0.10	0.84	0.08	0.08	5.0	5.0	8.6	0.72	9.89	3.73	15	2.00	158.34	158.50	158.57	158.83	162.25	162.00	Pipe - (16)
16	4	4.000	0.08	0.08	0.76	0.06	0.06	5.0	5.0	8.6	0.52	11.06	2.52	15	2.50	147.90	148.00	148.18	148.28	151.75	151.50	Pipe - (19)
17	4	8.000	0.26	0.26	0.72	0.19	0.19	6.9	6.9	7.5	1.40	9.89	4.24	15	2.00	147.84	148.00	148.18	148.47	151.75	151.50	Pipe - (20)
18	ო	4.000	0.06	0.06	06.0	0.05	0.05	5.0	5.0	8.6 0.5	0.46	11.06	3.45	15	2.50	139.00	139.10	139.17	139.36	142.85	142.60	Pipe - (19) (1)
19	ო	8.000	0.35	0.55	0.56	0.20	0.29	6.8	6.9	6.6	1.90	5.10	4.99	4	1.75	138.96	139.10	139.38	139.69	142.85	142.60	Pipe - (22)
20	19	84.000	0.20	0.20	0.45	0.09	0.09	7.7	7.7	7.1	0.64	15.12	2.07	4	15.36	139.10	152.00	139.69	152.33	142.60	152.00	Pipe - (21)
21	End	4.000	0.00	0.67	0.00	0.00	0.49	0.0	9.0	6.6	3.22	6.99	4.64	15	1.00	134.50	134.54	135.16	135.26	138.65	138.65	Pipe - (26)
22	21	54.000	0.08	0.67	0.84	0.07	0.49	5.0	8.7	6.7	3.25	4.95	4.31	15	0.50	134.54	134.81	135.28	135.55	138.65	138.00	Pipe - (25)
23	22	54.000	0.38	0.42	0.63	0.24	0.27	8.4	8.4	8.9	1.85	10.47	2.60	15	2.24	134.81	136.02	135.98	136.56	138.00	138.55	Pipe - (24)
Proje	Project File:		)15 Pro	bosed St	A0969-015 Proposed Storm Sewers.stm	/ers.stm										Number of lines:	of lines: 34			Run Date:	te: 5/21/2022	22

Storm Sewers v2021.00

NOTES:Intensity = 39.87 / (Inlet time + 3.80) ^ 0.71; Return period = Yrs. 25 ; c = cir e = ellip b = box

Page 2

				5																			
Station	uc	Len	Drng Area		Rnoff	Area x C	U	Tc		Rain	Total Flow	Cap	Vel	Pipe	_	Invert Elev	>	HGL Elev	>	Grnd / Rim Elev	m Elev	Line ID	
Line	To Line		Incr	Total		Incr	Total	Inlet	Syst			5		Size	Slope I	Dn	цр	Dn	dŊ	Dn	цр		
	ב	(tt)	(ac)	(ac)	(c)			(min)	(min) (	(in/hr)	(cfs)	(cfs) (	(ft/s) (i	(in) (	(%)	(tt)	(tt)	(tt)	(tt)	(tt)	(ft)		
24	23	16.000	0.04	0.04	0.81	0.03	0.03	5.0	5.0	8.6	0.28	4.95	1.34	15	0.50	136.02	136.10	136.56	136.30	138.55	138.55	Pipe - (23)	
25	End	13.712	0.00	0.47	0.00	0.00	0.39	0.0	6.7	7.6	2.92	4.22	3.99	15	0.36	134.50	134.55	135.19	135.30	138.60	138.60	Pipe - (35)	
26	25	12.000	0.03	0.03	0.90	0.02	0.02	5.0	5.0	8.6	0.20	9.89	1.13	15	2.00	134.86	135.10	135.53	135.27	138.60	0.00	Pipe - (36)	
27	25	32.000	0.04	0.44	0.82	0.03	0.36	5.0	6.5	7.7	2.78	4.46	2.85	15	0.41	134.55	134.68	135.53	135.56	138.60	138.30	Pipe - (34)	
28	27	36.000	0.23	0.40	0.81	0.19	0.33	6.0	6.3	7.8	2.57	4.36	2.52	15	0.39	134.68	134.82	135.70	135.74	138.30	137.60	Pipe - (33)	
29	28	18.000	0.17	0.17	0.84	0.14	0.14	6.0	6.0	8.0	1.14	4.66	1.06	15	0.44	134.82	134.90	135.89	135.89	137.60	137.40	Pipe - (32)	
30	22	18.000	0.17	0.17	0.87	0.15	0.15	7.2	7.2	7.3	1.08	7.19	2.00	15	1.06	134.81	135.00	135.98	135.41	138.00	138.00	CB-15	
31	End	48.000	0.00	0.29	0.00	0.00	0.21	0.0	6.0	7.9	4.87	4.95	4.01	15	0.50	134.00	134.24	135.23	135.43	134.00	138.20	Pipe - (30)	
32	31	34.000	0.00	0.00	0.00	0.00	0.00	0.0	0.1	0.0	3.22	4.95	2.62	15	0.50	134.24	134.41	135.68	135.75	138.20	139.00	Pipe - (29)	
33	32	18.000	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	3.22	4.95	2.62	15	0.50	134.41	134.50	135.82	135.85	139.00	138.65	Pipe - (28)	
34		20.000	0.29	0.29	0.73	0.21	0.21	5.8	5.8	6.1	1.68	7.00	1.37	15	1.00	134.24	134.44	135.68	135.69	138.20	0.00	Pipe - (31)	
Proj	ect File:	Project File: A0969-015 Proposed Storm Sewers.stm	015 Pro	posed St	torm Sew	vers.stm			]			1	1	1		Number of lines:		34		Run Date:	te: 5/21/2022	022	
NO.	TES:Inte	NOTES: Intensity = $39.87$ / (Inlet time + $3.80$ ) ^ 0.71; Return period = Yrs. 25 ; c =	9.87 / (1	nlet time	+ 3.80)	^ 0.71;	Return p	∋riod =Υr	s. 25 ;	c = cir e	= ellip	= ellip b = box											

Storm Sewers v2021.00

FE-01, 24"
$Q_{25} = 5.04$ cfs,
$V_{25} = 4.66$ ft/s

#### **OUTLET PROTECTION - OUTLET VELOCITY** $\leq$ 14 feet/sec

			OUT	LET PI	PE DIA	METE	ER OR SP	AN (in)		
DISCHARGE	12	15	18	24	30	36	42	48	54	60
(cfs)		•	•	*		•			-	-
0-5	10	10		USE						
5.5	12	11								
6		12	12			MIN	TMUM			
7		14	13	12						
8			15	13						
8.5			16	14			l í	LEN	GTH	1
9				14						
10				15	14					
11				16	15					
12				17	15	14			OUTI	INED
13				18	16	15	-			
14					17	15	14			
16		USE			18	16	15	14		
18						18	16	15		
20						19	17	16		
22						20	18	16		
24							19	17	16	
26							20	18	17	16
28			PR	EFORM	<b>IED</b>		21	19	17	16
30							21	19	18	17
32							22	20	18	17
35								21	19	18
40								23	21	19
45								25	23	21
48					SCO	OUR		26	24	22
50									24	22
55									26	23
60									27	25
63									28	26
65										26
75							HOLE			29
80										30

#### Table 11-13.1 - Length - L<sub>a</sub> (feet) Type B or C Riprap Apron

Notes: 1. Bold face outlined boxes indicate minimum L<sub>a</sub> to be used for a given pipe diameter or span. 2. Rounding and interpolating are acceptable.

	Х	W1	W2	W1 = 6'
Type A Riprap Apron	3	3Sp	3Sp+0.7 La	
Type B Riprap Apron	5	3Sp	3Sp+0.4 La	W2 = 10.8'

EW-01, 15"
$Q_{25} = 4.87$ cfs
$V_{or} = 4.01  \text{ft/s}$

#### **OUTLET PROTECTION - OUTLET VELOCITY** $\leq$ 14 feet/sec

			OUT	LET PI	PE DIA	METE	R OR SP	AN (in)		
DISCHARGE	12	15	18	24	30	36	42	48	54	60
(cfs)		•					•		•	•
0-5	10	10		USE						
5.5	12	11								
6		12	12			MIN	TMUM			
7		14	13	12						
8			15	13						
8.5			16	14				LEN	GTH	
9				14						
10				15	14					
11				16	15					
12				17	15	14	<b>1</b>		OUTL	INED
13				18	16	15				
14					17	15	14			
16		USE			18	16	15	14		
18						18	16	15		
20						19	17	16	-	
22						20	18	16		
24							19	17	16	
26							20	18	17	16
28			PR	EFORM	IED		21	19	17	16
30							21	19	18	17
32							22	20	18	17
35								21	19	18
40								23	21	19
45								25	23	21
48					SCO	OUR		26	24	22
50									24	22
55									26	23
60									27	25
63									28	26
65										26
75							HOLE			29
80										30

#### Table 11-13.1 - Length - L<sub>a</sub> (feet) Type B or C Riprap Apron

Notes: 1. Bold face outlined boxes indicate minimum L<sub>a</sub> to be used for a given pipe diameter or span. 2. Rounding and interpolating are acceptable.

]	Х	W1	W2	W1 = 3.75'
Type A Riprap Apron	3	3Sp	3Sp+0.7 La	
Type B Riprap Apron	5	3Sp	3Sp+0.4 La	W2 = 4.15'

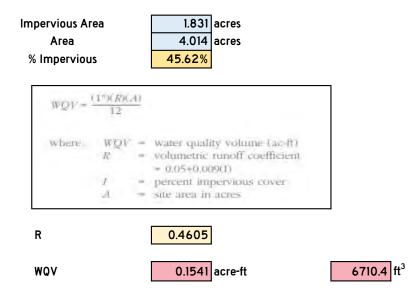
# **Tighe&Bond**

**APPENDIX E** 

# Tighe&Bond

Water Quality Volume Computation: WS-PR-03A + 03B ASML Campus Traffic Safety Improvements Date: May 22, 2022

Prepared by: J. Canas



#### Groundwater Recharge Volume Computation

NRCS Hydrologic Soil Group	Average Annual Recharge	Groundwater Recharge Depth (D)	
A	18 Inches/year	0.4 inches	
В	12 inches/year	0.25 inches	
C	6 inches/year	0.10 inches	
D	3 inchiei/year	G inches (waived)	)
here GRU D	<ul> <li>depth of r</li> <li>site area 0</li> </ul>	icres)	ime (ac-ft) arged (inches), see <b>Table 7-4</b> erviousness (decimal, not percent) for new development
1			e in site imperviousness for re-development projects

▶ 15,555 cubic feet provided below chamber system outlet, so WQV and GRV met

#### Chamber System Design - Drawdown

Drawdown time, use default Rawls infiltration rates (Rawls, Brakenseik and Saxton, 1982):

Sandy Loam, HSG B = 1.02 inches/hour

48 in / 1.02 in/hr = 47.059 hours

# Tighe&Bond

#### Water Quality Flow Computation ASML Campus Traffic Safety Improvements, WQS-001 Date: May 22, 2022 Prepared by: J. Canas

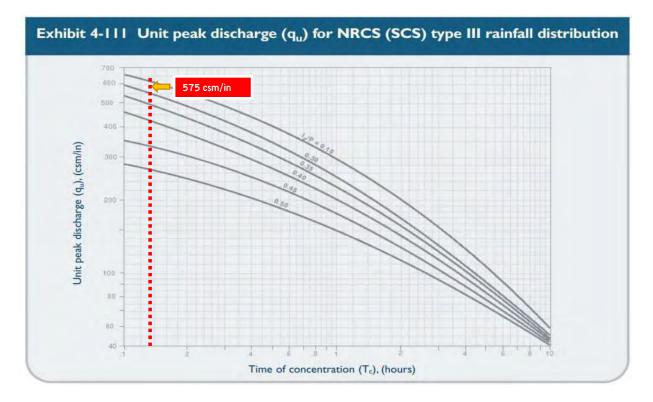
Proposed Conditions CN	89.5			
Area	0.47	acres	0.0007	mi2
Time of Concentration	6.7	minutes	0.1117	hours

Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)	Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)
40		55		70	0.857	85	
4.1	2.878	56		71	0.817	86	0.326
42	2.762	57	1.509	72	0.778	87	0.29
43		58		73	0.740	88	
44		59		74	0.703	89	
45		60		75	0.667	90	
46		61		76		91	
47		62		77		92	
48		63		78		93	
49		64		79		94	
50		65		80		95	
51		66		81	0.469	96	
52		67		82		97	
53		68		83		98	
54		69		84			

	Upper	Lower	Diff	Interpolated
CN	90	89	1	89.5
l <sub>a</sub>	0.222	0.247	-0.025	0.2345
			_	
1	inches		la/P	0.2345

P, water quality storm

From Exhibit 4-111, q<sub>u</sub>, csm/in



 $WQF = q_u \times A \times Q$ 

$\mathbf{q}_{u}$	575	cfs/mi <sup>2</sup> /inch
Α	0.0007	mi <sup>2</sup>

 $Q = WQV(ac-ft) \times 12 (in/ft) / A (acres)$ 

	WQV A	0.0312 0.47	ac-ft acres
	Q	0.797	cfs
WQF	0.3365 cfs		

# Tighe&Bond

#### Water Quality Flow Computation ASML Campus Traffic Safety Improvements, WQS-002 Date: May 22, 2022 Prepared by: J. Canas

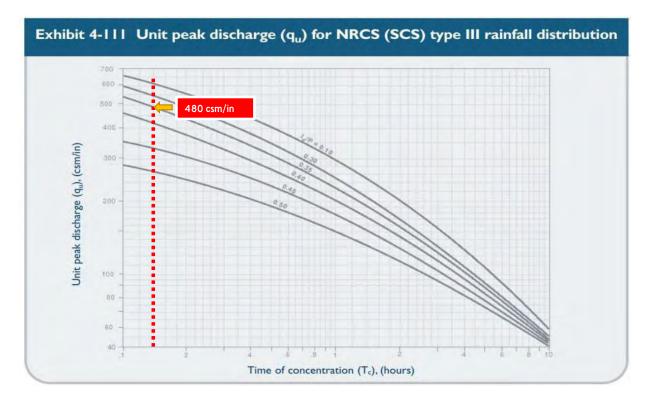
Proposed Conditions CN	84.5			
Area	0.67	acres	0.001	mi2
Time of Concentration	9	minutes	0.15	hours

Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)	Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)
40		55	1.636	70	0.857	85	
4.1	2.878	56		71	0.817	86	0.326
42		57		72	0.778	87	0.29
43		58		73	0.740	88	
44		59		74	0.703	89	
45		60		75	0.667	90	
46		61		76		91	
47	2.255	62		77	0.597	92	
48	2.167	63		78	0.564	93	
49		64		79	0.532	94	
50	2.000	65		80	0.500	95	0.10
51		66	1.030	81	0.469	96	
52		67		82		97	
53	1.774	68		83		98	
54	1.704	69	0.899	84			

	Upper	Lower	Diff	Interpolated			
CN	85	84	1	84.5			
l <sub>a</sub>	0.353	0.381	-0.028	0.367			
1	inches		la/P	0.367			

P, water quality storm

From Exhibit 4-111, q<sub>u</sub>, csm/in



 $WQF = q_u \times A \times Q$ 

qu	480 cfs/mi <sup>2</sup> /inch
Α	0.001 mi <sup>2</sup>

 $Q = WQV(ac-ft) \times 12 (in/ft) / A (acres)$ 

	WQV A	0.0395 0.67	ac-ft acres
	Q	0.7079	cfs
WQF	0.3557 cfs	5	

# Tighe&Bond

#### Water Quality Flow Computation ASML Campus Traffic Safety Improvements, WQS-003 Date: May 22, 2022 Prepared by: J. Canas

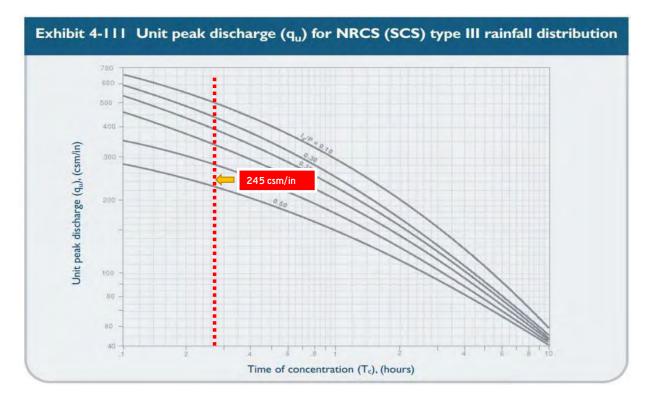
Proposed Conditions CN	80.5		
Area	1.72	acres	0.0027 mi2
Time of Concentration	16.7	minutes	0.2783 hours

Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)	Curve number	l <sub>a</sub> (in)	Curve	l <sub>a</sub> (in)
40	3.000	55	1.636	70		85	
4.1	2.878	56		71	0.817	86	
42	2.762	57	1.509	72	0.778	87	0.29
43		58	1.448	73	0.740	88	
44	2.545	59		74	0.703	89	
45		60		75	0.667	90	
46		61		76		91	
47	2.255	62		77	0.597	92	
48	2.167	63		78	0.564	93	
49		64		79		94	
50	2.000	65		80	0.500	95	
51		66		81		96	
52		67		82		97	
53		68		83		98	
54		69	0.899	84	0.381		

	Upper	Lower	Diff	Interpolated	
CN	81	80	1	80.5	
l <sub>a</sub>	0.469	0.5	-0.031	0.4845	
1	inches		la/P	0.4845	

P, water quality storm

From Exhibit 4-111, q<sub>u</sub>, csm/in



 $WQF = q_u \times A \times Q$ 

$\mathbf{q}_{u}$	245 cfs/mi <sup>2</sup> /inch
Α	0.0027 mi <sup>2</sup>

 $Q = WQV(ac-ft) \times 12 (in/ft) / A (acres)$ 

	WQV A	0.0874 1.72	ac-ft acres
	Q	0.6098	cfs
WQF	0.4015 cfs	5	



# Hydrodynamic Separation Product Calculator

#### ASML Campus Traffic Safety Improvements

WQS-001

CDS CDS2015-4-C

Project Information					
Project Name	ASML Campus Traffic Safety Improvements			Option #	A
Country	UNITED_STATES	State	City	Wilton	

Contact Information					
First Name         Joseph         Last Name         Canas					
Company	Tighe & Bond	Phone #	203-712-1109		
Email jacanas@tighebond.com					

Design Criteria							
Site Designation	WQS-001			Sizing Method	Treatment Flow Rate		
Screening Required?	No	Treatment Flow Rate	0.34	Peak Flow (cfs)	2.92		
Groundwater Depth (ft)	5 - 10	Pipe Invert Depth (ft)	0 - 5	Bedrock Depth (ft)	5 - 10		
Multiple Inlets?	Yes	Grate Inlet Required?	No	Pipe Size (in)	15.00		
Required Particle Size Distribution?		90° between two inlets?	Yes				

Treatment Selection						
Treatment Unit CDS System Model CDS2015-4-C						
Target Removal	80%	Particle Size Distribution (PSD)	50			



# Hydrodynamic Separation Product Calculator

ASML Campus Traffic Safety Improvements

WQS-001

CDS CDS2015-4-C

CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD								
Rainfall Intensity <sup>1</sup> (in/hr)	hr) % Rainfall Volume <sup>1</sup> Cumulative Rainfall Volume Treated Created Flowrate Created Flowra							
						Removal Efficier	ncy Adjustment <sup>2</sup> =	
	Predicted % Annual Rainfall Treated =							
					Predicted Net	t Annual Load Rer	moval Efficiency =	
1 -								
2 - Reduction due t	o use of 60-min	ute data for a site th	hat has a time of	concentration less	than 30-minutes.			

#### SECTION (\_\_\_\_\_) STORM WATER TREATMENT DEVICE

#### 1.0 GENERAL

- 1.1 This item shall govern the furnishing and installation of the CDS<sup>®</sup> by Contech Engineered Solutions LLC, complete and operable as shown and as specified herein, in accordance with the requirements of the plans and contract documents.
- 1.2 The Contractor shall furnish all labor, equipment and materials necessary to install the storm water treatment device(s) (SWTD) and appurtenances specified in the Drawings and these specifications.
- 1.3 The manufacturer of the SWTD shall be one that is regularly engaged in the engineering design and production of systems deployed for the treatment of storm water runoff for at least five (5) years and which have a history of successful production, acceptable to the Engineer. In accordance with the Drawings, the SWTD(s) shall be a CDS<sup>®</sup> device manufactured by:

Contech Engineered Solutions LLC 9025 Centre Pointe Drive West Chester, OH, 45069 Tel: 1 800 338 1122

- 1.4 Related Sections
  - 1.4.1 Section 02240: Dewatering
  - 1.4.2 Section 02260: Excavation Support and Protection
  - 1.4.3 Section 02315: Excavation and Fill
  - 1.4.4 Section 02340: Soil Stabilization
- 1.5 All components shall be subject to inspection by the engineer at the place of manufacture and/or installation. All components are subject to being rejected or identified for repair if the quality of materials and manufacturing do not comply with the requirements of this specification. Components which have been identified as defective may be subject for repair where final acceptance of the component is contingent on the discretion of the Engineer.
- 1.6 The manufacturer shall guarantee the SWTD components against all manufacturer originated defects in materials or workmanship for a period of twelve (12) months from the date the components are delivered to the owner for installation. The manufacturer shall upon its determination repair, correct or replace any manufacturer originated defects advised in writing to the manufacturer within the referenced warranty period. The use of SWTD components shall be limited to the application for which it was specifically designed.
- 1.7 The SWTD manufacturer shall submit to the Engineer of Record a "Manufacturer's Performance Certification" certifying that each SWTD is capable of achieving the specified removal efficiencies listed in these specifications. The certification shall be supported by independent third-party research

1.8 No product substitutions shall be accepted unless submitted 10 days prior to project bid date, or as directed by the Engineer of Record. Submissions for substitutions require review and approval by the Engineer of Record, for hydraulic performance, impact to project designs, equivalent treatment performance, and any required project plan and report (hydrology/hydraulic, water quality, stormwater pollution) modifications that would be required by the approving jurisdictions/agencies. Contractor to coordinate with the Engineer of Record any applicable modifications to the project estimates of cost, bonding amount determinations, plan check fees for changes to approved documents, and/or any other regulatory requirements resulting from the product substitution.

#### 2.0 MATERIALS

- 2.1 Housing unit of stormwater treatment device shall be constructed of pre-cast or cast-in-place concrete, no exceptions. Precast concrete components shall conform to applicable sections of ASTM C 478, ASTM C 857 and ASTM C 858 and the following:
  - 2.1.1 Concrete shall achieve a minimum 28-day compressive strength of 4,000 pounds per square-inch (psi);
  - 2.1.2 Unless otherwise noted, the precast concrete sections shall be designed to withstand lateral earth and AASHTO H-20 traffic loads;
  - 2.1.3 Cement shall be Type III Portland Cement conforming to ASTM C 150;
  - 2.1.4 Aggregates shall conform to ASTM C 33;
  - 2.1.5 Reinforcing steel shall be deformed billet-steel bars, welded steel wire or deformed welded steel wire conforming to ASTM A 615, A 185, or A 497.
  - 2.1.6 Joints shall be sealed with preformed joint sealing compound conforming to ASTM C 990.
  - 2.1.7 Shipping of components shall not be initiated until a minimum compressive strength of 4,000 psi is attained or five (5) calendar days after fabrication has expired, whichever occurs first.
- 2.2 Internal Components and appurtenances shall conform to the following:
  - 2.2.1 Screen and support structure shall be manufactured of Type 316 and 316L stainless steel conforming to ASTM F 1267-01;
  - 2.2.2 Hardware shall be manufactured of Type 316 stainless steel conforming to ASTM A 320;
  - 2.2.3 Fiberglass components shall conform to applicable sections of ASTM D-4097
  - 2.2.4 Access system(s) conform to the following:
  - 2.2.5 Manhole castings shall be designed to withstand AASHTO H-20 loadings and manufactured of cast-iron conforming to ASTM A 48 Class 30.

#### 3.0 PERFORMANCE

- 3.1 The SWTD shall be sized to either achieve an 80 percent average annual reduction in the total suspended solid load with a particle size distribution having a mean particle size (d<sub>50</sub>) of 125 microns unless otherwise stated.
- 3.2 The SWTD shall be capable of capturing and retaining 100 percent of pollutants greater than or equal to 2.4 millimeters (mm) regardless of the pollutant's specific gravity (i.e.: floatable and neutrally buoyant materials) for flows up to the device's rated-treatment capacity. The SWTD shall be designed to retain all previously captured pollutants addressed by this

subsection under all flow conditions. The SWTD shall be capable of capturing and retaining total petroleum hydrocarbons. The SWTD shall be capable of achieving a removal efficiency of 92 and 78 percent when the device is operating at 25 and 50 percent of its rated-treatment capacity. These removal efficiencies shall be based on independent third-party research for influent oil concentrations representative of storm water runoff ( $20 \pm 5 \text{ mg/L}$ ). The SWTD shall be greater than 99 percent effective in controlling dry-weather accidental oil spills.

- 3.3 The SWTD shall be designed with a sump chamber for the storage of captured sediments and other negatively buoyant pollutants in between maintenance cycles. The minimum storage capacity provided by the sump chamber shall be in accordance with the volume listed in Table 1. The boundaries of the sump chamber shall be limited to that which do not degrade the SWTD's treatment efficiency as captured pollutants accumulate. The sump chamber shall be separate from the treatment processing portion(s) of the SWTD to minimize the probability of fine particle re-suspension. In order to not restrict the Owner's ability to maintain the SWTD, the minimum dimension providing access from the ground surface to the sump chamber shall be 16 inches in diameter.
- 3.4 The SWTD shall be designed to capture and retain Total Petroleum Hydrocarbons generated by wet-weather flow and dry-weather gross spills and have a capacity listed in Table 1 of the required unit.
- 3.5 The SWTD shall convey the flow from the peak storm event of the drainage network, in accordance with required hydraulic upstream conditions as defined by the Engineer. If a substitute SWTD is proposed, supporting documentation shall be submitted that demonstrates equal or better upstream hydraulic conditions compared to that specified herein. This documentation shall be signed and sealed by a Professional Engineer registered in the State of the work. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.
- 3.6 The SWTD shall have completed field tested following TARP Tier II protocol requirements

#### 4.0 EXECUTION

- 4.1 The contractor shall exercise care in the storage and handling of the SWTD components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted and unloading has commenced shall be borne by the contractor.
- 4.2 The SWTD shall be installed in accordance with the manufacturer's recommendations and related sections of the contract documents. The manufacturer shall provide the contractor installation instructions and offer on-site guidance during the important stages of the installation as identified by the manufacturer at no additional expense. A minimum of 72 hours notice shall be provided to the manufacturer prior to their performance of the services included under this subsection.
- 4.3 The contractor shall fill all voids associated with lifting provisions provided by the manufacturer. These voids shall be filled with non-shrinking grout providing a finished surface consistent with adjacent surfaces. The contractor shall trim all protruding lifting provisions flush with the adjacent concrete surface in a manner, which leaves no sharp points or edges.

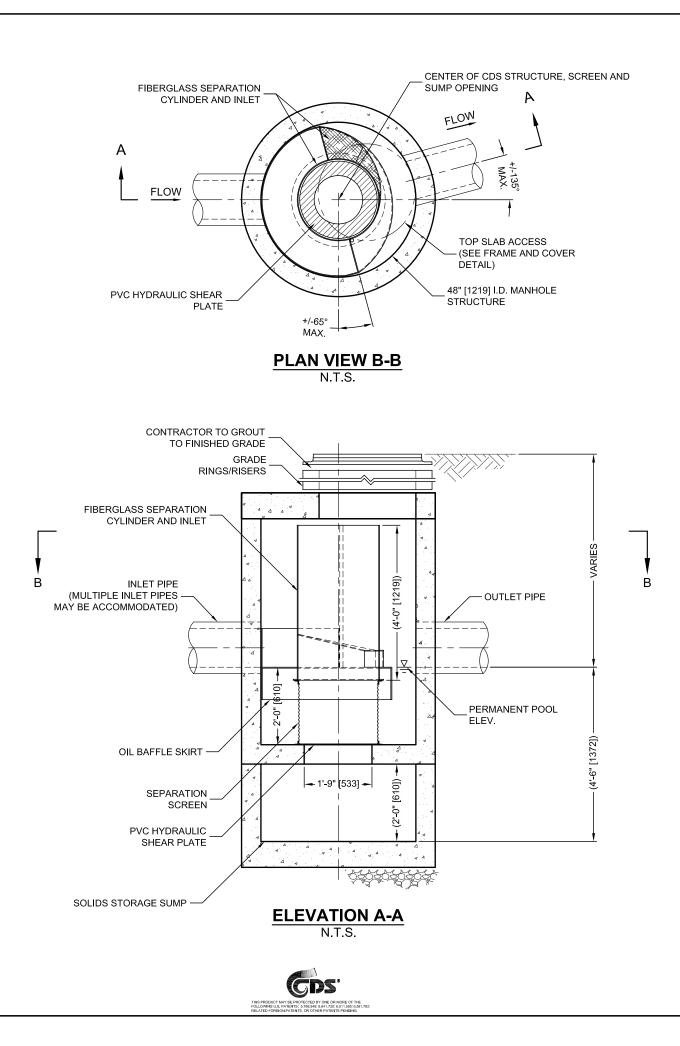
4.4 The contractor shall removal all loose material and pooling water from the SWTD prior to the transfer of operational responsibility to the Owner.

Storage capacities							
CDS Model	Minimum Sump Storage Capacity	Minimum Oil Storage					
	(yd <sup>3</sup> )/(m <sup>3</sup> )	Capacity (gal)/(L)					
CDS2015-4	0.9(0.7)	61(232)					
CDS2015-5	1.5(1.1)	83(313)					
CDS2020-5	1.5(1.1)	99(376)					
CDS2025-5	1.5(1.1)	116(439)					
CDS3020-6	2.1 (1.6)	184(696)					
CDS3025-6	2.1(1.6)	210(795)					
CDS3030-6	2.1 (1.6)	236(895)					
CDS3035-6	2.1 (1.6)	263(994)					
CDS3535-7	2.9(2.2)	377(1426)					
CDS4030-8	5.6(4.3)	426(1612)					
CDS4040-8	5.6 (4.3)	520(1970)					
CDS4045-8	5.6 (4.3)	568(2149)					
CDS5640-10	8.7(6.7)	758(2869)					
CDS5653-10	8.7(6.7)	965(3652)					
CDS5668-10	8.7(6.7)	1172(4435)					
CDS5678-10	8.7(6.7)	1309(4956)					
CDS7070-DV	3.6(2.8)	914 (3459)					
CDS10060-DV	5.0 (3.8)	792 (2997)					
CDS10080-DV	5.0 (3.8)	1057 (4000)					
CDS100100-DV	5.0 (3.8)	1320 (4996)					

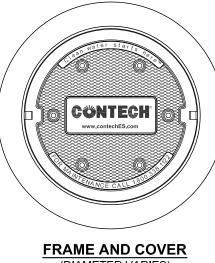
TABLE 1 Storm Water Treatment Device Storage Capacities

**END OF SECTION** 

#### CDS2015-4-C DESIGN NOTES



THE STANDARD CDS2015-4-C CONFIGURATION IS SHOWN. ALTERNAT CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS.
CONFIGURATION DESCRIPTION
GRATED INLET ONLY (NO INLET PIPE)
GRATED INLET WITH INLET PIPE OR PIPES
CURB INLET ONLY (NO INLET PIPE)
CURB INLET WITH INLET PIPE OR PIPES
SEPARATE OIL BAFFLE (SINGLE INLET PIPE REQUIRED FOR THIS CON
SEDIMENT WEIR FOR NJDEP / NJCAT CONFORMING UNITS



(DIAMETER VARIES) N.T.S.

**GENERAL NOTES** 

- 1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERW
- 2. DIMENSIONS MARKED WITH ( ) ARE REFERENCE DIMENSIONS. AC 3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIME SOLUTIONS LLC REPRESENTATIVE. www.contechES.com
- 4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND 5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET HS20 (AASHTO M 306) LOAD RATING, ASSUMING GROUNDWATER ELEVATION
- AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. 6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

#### INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE В. (LIFTING CLUTCHES PROVIDED).
- CONTRACTOR TO ADD JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS, AND ASSEMBLE STRUCTURE. C.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.



NATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME

ONFIGURATION)

SITE SPECIFIC DATA REQUIREMENTS							
STRUCTURE ID							
WATER QUALITY	FLOW RAT	E (0	CFS OR L/s)		*		
PEAK FLOW RAT	E (CFS OR I	_/s)			*		
RETURN PERIOD	OF PEAK F	LO	W (YRS)		*		
SCREEN APERTURE (2400 OR 4700) *							
		_			1		
PIPE DATA:	I.E.	1	MATERIAL	D	IAMETER		
INLET PIPE 1	*		*		*		
INLET PIPE 2	*		*		*		
OUTLET PIPE	*		*		*		
					1		
RIM ELEVATION					*		
ANTI-FLOTATION	BALLAST		WIDTH	Т	HEIGHT		
	* *						
NOTES/SPECIAL REQUIREMENTS:							
* PER ENGINEER OF RECORD							

STRUCTURE ID							
WATER QUALITY		*					
PEAK FLOW RAT	E (CFS OR I	_/s)			*		
RETURN PERIOD	OF PEAK F	LO	W (YRS)		*		
SCREEN APERTL	JRE (2400 C	R 4	700)		*		
PIPE DATA:	IAMETER						
INLET PIPE 1	* * *						
INLET PIPE 2	*	* * *					
OUTLET PIPE	*		*		*		
RIM ELEVATION					*		
ANTI-FLOTATION	HEIGHT						
* *							
NOTES/SPECIAL REQUIREMENTS:							

CDS2015-4-C

**INLINE CDS** 

STANDARD DETAIL

ISE.	
CTUAL DIMENSIONS MAY VARY.	
NSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED	
TH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING	



# Hydrodynamic Separation Product Calculator

#### ASML Campus Traffic Safety Improvements

WQS-002

CDS CDS2015-4-C

Project Information						
Project Name	ASML Campus Traffic Safety Improvements				A	
Country	UNITED_STATES	State	City	Wilton		

Contact Information						
First Name	Joseph	Last Name	Canas			
Company	Tighe & Bond	Phone #	203-712-1109			
Email jacanas@tighebond.com						

Design Criteria								
Site Designation	WQS-002			Sizing Method	Treatment Flow Rate			
Screening Required?	No	Treatment Flow Rate	0.35	Peak Flow (cfs)	3.22			
Groundwater Depth (ft)	0 - 5	Pipe Invert Depth (ft)	0 - 5	Bedrock Depth (ft)	0 - 5			
Multiple Inlets?	No	Grate Inlet Required?	No	Pipe Size (in)	15.00			
Required Particle Size Distribution?		90° between two inlets?	N/A					

Treatment Selection							
Treatment Unit	CDS	System Model	CDS2015-4-C				
Target Removal	80%	Particle Size Distribution (PSD)	50				



# Hydrodynamic Separation Product Calculator

ASML Campus Traffic Safety Improvements

WQS-002

CDS CDS2015-4-C

CDS	CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD									
Rainfall Intensity <sup>1</sup> (in/hr)	% Rainfall Volume <sup>1</sup>	Cumulative Rainfall Volume	Rainfall Volume Treated	Total Flowrate (cfs)	Treated Flowrate (cfs)	Operating Rate (%)	Removal Efficiency (%)	Incremental Removal (%)		
Removal Efficiency Adjustment <sup>2</sup> =										
Predicted % Annual Rainfall Treated =										
Predicted Net Annual Load Removal Efficiency =										
1 -										
2 - Reduction due t	- Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.									

#### SECTION (\_\_\_\_\_) STORM WATER TREATMENT DEVICE

#### 1.0 GENERAL

- 1.1 This item shall govern the furnishing and installation of the CDS<sup>®</sup> by Contech Engineered Solutions LLC, complete and operable as shown and as specified herein, in accordance with the requirements of the plans and contract documents.
- 1.2 The Contractor shall furnish all labor, equipment and materials necessary to install the storm water treatment device(s) (SWTD) and appurtenances specified in the Drawings and these specifications.
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Contech Engineered Solutions LLC 9025 Centre Pointe Drive West Chester, OH, 45069 Tel: 1 800 338 1122

- 1.4 Related Sections
  - 1.4.1 Section 02240: Dewatering
  - 1.4.2 Section 02260: Excavation Support and Protection
  - 1.4.3 Section 02315: Excavation and Fill
  - 1.4.4 Section 02340: Soil Stabilization
- 1.5 All components shall be subject to inspection by the engineer at the place of manufacture and/or installation. All components are subject to being rejected or identified for repair if the quality of materials and manufacturing do not comply with the requirements of this specification. Components which have been identified as defective may be subject for repair where final acceptance of the component is contingent on the discretion of the Engineer.
- 1.6 The manufacturer shall guarantee the SWTD components against all manufacturer originated defects in materials or workmanship for a period of twelve (12) months from the date the components are delivered to the owner for installation. The manufacturer shall upon its determination repair, correct or replace any manufacturer originated defects advised in writing to the manufacturer within the referenced warranty period. The use of SWTD components shall be limited to the application for which it was specifically designed.
- 1.7 The SWTD manufacturer shall submit to the Engineer of Record a "Manufacturer's Performance Certification" certifying that each SWTD is capable of achieving the specified removal efficiencies listed in these specifications. The certification shall be supported by independent third-party research

1.8 No product substitutions shall be accepted unless submitted 10 days prior to project bid date, or as directed by the Engineer of Record. Submissions for substitutions require review and approval by the Engineer of Record, for hydraulic performance, impact to project designs, equivalent treatment performance, and any required project plan and report (hydrology/hydraulic, water quality, stormwater pollution) modifications that would be required by the approving jurisdictions/agencies. Contractor to coordinate with the Engineer of Record any applicable modifications to the project estimates of cost, bonding amount determinations, plan check fees for changes to approved documents, and/or any other regulatory requirements resulting from the product substitution.

#### 2.0 MATERIALS

- 2.1 Housing unit of stormwater treatment device shall be constructed of pre-cast or cast-in-place concrete, no exceptions. Precast concrete components shall conform to applicable sections of ASTM C 478, ASTM C 857 and ASTM C 858 and the following:
  - 2.1.1 Concrete shall achieve a minimum 28-day compressive strength of 4,000 pounds per square-inch (psi);
  - 2.1.2 Unless otherwise noted, the precast concrete sections shall be designed to withstand lateral earth and AASHTO H-20 traffic loads;
  - 2.1.3 Cement shall be Type III Portland Cement conforming to ASTM C 150;
  - 2.1.4 Aggregates shall conform to ASTM C 33;
  - 2.1.5 Reinforcing steel shall be deformed billet-steel bars, welded steel wire or deformed welded steel wire conforming to ASTM A 615, A 185, or A 497.
  - 2.1.6 Joints shall be sealed with preformed joint sealing compound conforming to ASTM C 990.
  - 2.1.7 Shipping of components shall not be initiated until a minimum compressive strength of 4,000 psi is attained or five (5) calendar days after fabrication has expired, whichever occurs first.
- 2.2 Internal Components and appurtenances shall conform to the following:
  - 2.2.1 Screen and support structure shall be manufactured of Type 316 and 316L stainless steel conforming to ASTM F 1267-01;
  - 2.2.2 Hardware shall be manufactured of Type 316 stainless steel conforming to ASTM A 320;
  - 2.2.3 Fiberglass components shall conform to applicable sections of ASTM D-4097
  - 2.2.4 Access system(s) conform to the following:
  - 2.2.5 Manhole castings shall be designed to withstand AASHTO H-20 loadings and manufactured of cast-iron conforming to ASTM A 48 Class 30.

#### 3.0 PERFORMANCE

- 3.1 The SWTD shall be sized to either achieve an 80 percent average annual reduction in the total suspended solid load with a particle size distribution having a mean particle size (d<sub>50</sub>) of 125 microns unless otherwise stated.
- 3.2 The SWTD shall be capable of capturing and retaining 100 percent of pollutants greater than or equal to 2.4 millimeters (mm) regardless of the pollutant's specific gravity (i.e.: floatable and neutrally buoyant materials) for flows up to the device's rated-treatment capacity. The SWTD shall be designed to retain all previously captured pollutants addressed by this

subsection under all flow conditions. The SWTD shall be capable of capturing and retaining total petroleum hydrocarbons. The SWTD shall be capable of achieving a removal efficiency of 92 and 78 percent when the device is operating at 25 and 50 percent of its rated-treatment capacity. These removal efficiencies shall be based on independent third-party research for influent oil concentrations representative of storm water runoff ( $20 \pm 5 \text{ mg/L}$ ). The SWTD shall be greater than 99 percent effective in controlling dry-weather accidental oil spills.

- 3.3 The SWTD shall be designed with a sump chamber for the storage of captured sediments and other negatively buoyant pollutants in between maintenance cycles. The minimum storage capacity provided by the sump chamber shall be in accordance with the volume listed in Table 1. The boundaries of the sump chamber shall be limited to that which do not degrade the SWTD's treatment efficiency as captured pollutants accumulate. The sump chamber shall be separate from the treatment processing portion(s) of the SWTD to minimize the probability of fine particle re-suspension. In order to not restrict the Owner's ability to maintain the SWTD, the minimum dimension providing access from the ground surface to the sump chamber shall be 16 inches in diameter.
- 3.4 The SWTD shall be designed to capture and retain Total Petroleum Hydrocarbons generated by wet-weather flow and dry-weather gross spills and have a capacity listed in Table 1 of the required unit.
- 3.5 The SWTD shall convey the flow from the peak storm event of the drainage network, in accordance with required hydraulic upstream conditions as defined by the Engineer. If a substitute SWTD is proposed, supporting documentation shall be submitted that demonstrates equal or better upstream hydraulic conditions compared to that specified herein. This documentation shall be signed and sealed by a Professional Engineer registered in the State of the work. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.
- 3.6 The SWTD shall have completed field tested following TARP Tier II protocol requirements

#### 4.0 EXECUTION

- 4.1 The contractor shall exercise care in the storage and handling of the SWTD components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted and unloading has commenced shall be borne by the contractor.
- 4.2 The SWTD shall be installed in accordance with the manufacturer's recommendations and related sections of the contract documents. The manufacturer shall provide the contractor installation instructions and offer on-site guidance during the important stages of the installation as identified by the manufacturer at no additional expense. A minimum of 72 hours notice shall be provided to the manufacturer prior to their performance of the services included under this subsection.
- 4.3 The contractor shall fill all voids associated with lifting provisions provided by the manufacturer. These voids shall be filled with non-shrinking grout providing a finished surface consistent with adjacent surfaces. The contractor shall trim all protruding lifting provisions flush with the adjacent concrete surface in a manner, which leaves no sharp points or edges.

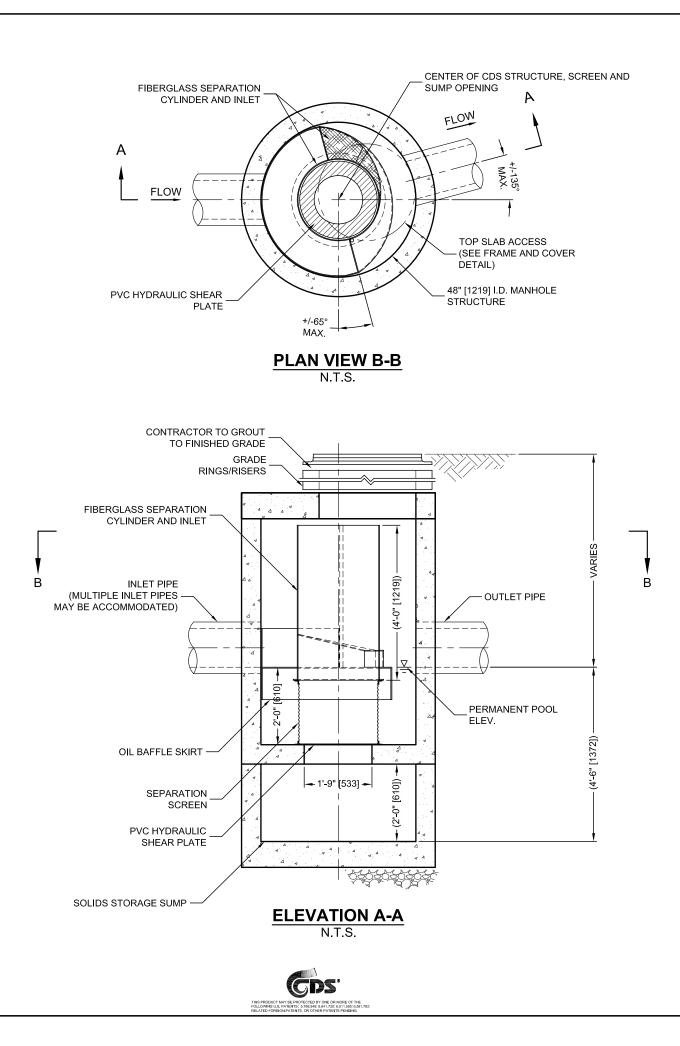
4.4 The contractor shall removal all loose material and pooling water from the SWTD prior to the transfer of operational responsibility to the Owner.

Storage capacities								
CDS Model	Minimum Sump Storage Capacity	Minimum Oil Storage						
	(yd <sup>3</sup> )/(m <sup>3</sup> )	Capacity (gal)/(L)						
CDS2015-4	0.9(0.7)	61(232)						
CDS2015-5	1.5(1.1)	83(313)						
CDS2020-5	1.5(1.1)	99(376)						
CDS2025-5	1.5(1.1)	116(439)						
CDS3020-6	2.1 (1.6)	184(696)						
CDS3025-6	2.1(1.6)	210(795)						
CDS3030-6	2.1 (1.6)	236(895)						
CDS3035-6	2.1 (1.6)	263(994)						
CDS3535-7	2.9(2.2)	377(1426)						
CDS4030-8	5.6(4.3)	426(1612)						
CDS4040-8	5.6 (4.3)	520(1970)						
CDS4045-8	5.6 (4.3)	568(2149)						
CDS5640-10	8.7(6.7)	758(2869)						
CDS5653-10	8.7(6.7)	965(3652)						
CDS5668-10	8.7(6.7)	1172(4435)						
CDS5678-10	8.7(6.7)	1309(4956)						
CDS7070-DV	3.6(2.8)	914 (3459)						
CDS10060-DV	5.0 (3.8)	792 (2997)						
CDS10080-DV	5.0 (3.8)	1057 (4000)						
CDS100100-DV	5.0 (3.8)	1320 (4996)						

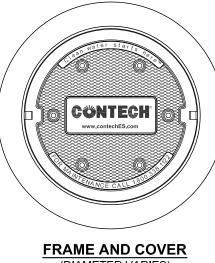
TABLE 1 Storm Water Treatment Device Storage Capacities

**END OF SECTION** 

#### CDS2015-4-C DESIGN NOTES



THE STANDARD CDS2015-4-C CONFIGURATION IS SHOWN. ALTERNAT CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS.
CONFIGURATION DESCRIPTION
GRATED INLET ONLY (NO INLET PIPE)
GRATED INLET WITH INLET PIPE OR PIPES
CURB INLET ONLY (NO INLET PIPE)
CURB INLET WITH INLET PIPE OR PIPES
SEPARATE OIL BAFFLE (SINGLE INLET PIPE REQUIRED FOR THIS CON
SEDIMENT WEIR FOR NJDEP / NJCAT CONFORMING UNITS



(DIAMETER VARIES) N.T.S.

**GENERAL NOTES** 

- 1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERW
- 2. DIMENSIONS MARKED WITH ( ) ARE REFERENCE DIMENSIONS. AC 3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIME SOLUTIONS LLC REPRESENTATIVE. www.contechES.com
- 4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND 5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET HS20 (AASHTO M 306) LOAD RATING, ASSUMING GROUNDWATER ELEVATION
- AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. 6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

#### INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE В. (LIFTING CLUTCHES PROVIDED).
- CONTRACTOR TO ADD JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS, AND ASSEMBLE STRUCTURE. C.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.



NATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME

ONFIGURATION)

SITE SPECIFIC DATA REQUIREMENTS							
STRUCTURE ID							
WATER QUALITY	FLOW RAT	E (0	CFS OR L/s)		*		
PEAK FLOW RAT	E (CFS OR I	_/s)			*		
RETURN PERIOD	OF PEAK F	LO	W (YRS)		*		
SCREEN APERTURE (2400 OR 4700) *							
		_			1		
PIPE DATA:	I.E.	1	MATERIAL	D	IAMETER		
INLET PIPE 1	*		*		*		
INLET PIPE 2	*		*		*		
OUTLET PIPE	*		*		*		
					1		
RIM ELEVATION					*		
ANTI-FLOTATION	BALLAST		WIDTH	Т	HEIGHT		
	* *						
NOTES/SPECIAL REQUIREMENTS:							
* PER ENGINEER OF RECORD							

STRUCTURE ID							
WATER QUALITY		*					
PEAK FLOW RAT		*					
RETURN PERIOD		*					
SCREEN APERTL		*					
PIPE DATA:	I.E. MATERIAL DI						
INLET PIPE 1	*	*					
INLET PIPE 2	*	*					
OUTLET PIPE	*		*		*		
RIM ELEVATION					*		
ANTI-FLOTATION	HEIGHT						
	*						
NOTES/SPECIAL REQUIREMENTS:							

CDS2015-4-C

**INLINE CDS** 

STANDARD DETAIL

ISE.	
CTUAL DIMENSIONS MAY VARY.	
NSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED	
TH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING	



# Hydrodynamic Separation Product Calculator

#### ASML Campus Traffic Safety Improvements

WQS-003

CDS CDS2020-5-C

Project Information						
Project Name	ASML Campus Traffic Safety Improvements				A	
Country	UNITED_STATES	State	City	Wilton		

Contact Information					
First Name	Joseph	Last Name	Canas		
Company	Tighe & Bond	Phone #	203-712-1109		
Email	jacanas@tighebond.com				

Design Criteria						
Site Designation	WQS-003			Sizing Method	Treatment Flow Rate	
Screening Required?	No	Treatment Flow Rate	0.41	Peak Flow (cfs)	5.04	
Groundwater Depth (ft)	5 - 10	Pipe Invert Depth (ft)	5 - 10	Bedrock Depth (ft)	5 - 10	
Multiple Inlets?	No	Grate Inlet Required?	No	Pipe Size (in)	24.00	
Required Particle Size Distribution?		90° between two inlets?	N/A			

Treatment Selection					
Treatment Unit	CDS	System Model	CDS2020-5-C		
Target Removal	80%	Particle Size Distribution (PSD)	50		



# Hydrodynamic Separation Product Calculator

ASML Campus Traffic Safety Improvements

WQS-003

CDS CDS2020-5-C

CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD								
Rainfall Intensity <sup>1</sup> (in/hr)	% Rainfall Volume <sup>1</sup>	Cumulative Rainfall Volume	Rainfall Volume Treated	Total Flowrate (cfs)	Treated Flowrate (cfs)	Operating Rate (%)	Removal Efficiency (%)	Incremental Removal (%)
Removal Efficiency Adjustment <sup>2</sup> =								
Predicted % Annual Rainfall Treated =								
Predicted Net Annual Load Removal Efficiency =								
1 -								
2 - Reduction due t	2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.							

#### SECTION (\_\_\_\_\_) STORM WATER TREATMENT DEVICE

#### 1.0 GENERAL

- 1.1 This item shall govern the furnishing and installation of the CDS<sup>®</sup> by Contech Engineered Solutions LLC, complete and operable as shown and as specified herein, in accordance with the requirements of the plans and contract documents.
- 1.2 The Contractor shall furnish all labor, equipment and materials necessary to install the storm water treatment device(s) (SWTD) and appurtenances specified in the Drawings and these specifications.
- 1.3 The manufacturer of the SWTD shall be one that is regularly engaged in the engineering design and production of systems deployed for the treatment of storm water runoff for at least five (5) years and which have a history of successful production, acceptable to the Engineer. In accordance with the Drawings, the SWTD(s) shall be a CDS<sup>®</sup> device manufactured by:

Contech Engineered Solutions LLC 9025 Centre Pointe Drive West Chester, OH, 45069 Tel: 1 800 338 1122

- 1.4 Related Sections
  - 1.4.1 Section 02240: Dewatering
  - 1.4.2 Section 02260: Excavation Support and Protection
  - 1.4.3 Section 02315: Excavation and Fill
  - 1.4.4 Section 02340: Soil Stabilization
- 1.5 All components shall be subject to inspection by the engineer at the place of manufacture and/or installation. All components are subject to being rejected or identified for repair if the quality of materials and manufacturing do not comply with the requirements of this specification. Components which have been identified as defective may be subject for repair where final acceptance of the component is contingent on the discretion of the Engineer.
- 1.6 The manufacturer shall guarantee the SWTD components against all manufacturer originated defects in materials or workmanship for a period of twelve (12) months from the date the components are delivered to the owner for installation. The manufacturer shall upon its determination repair, correct or replace any manufacturer originated defects advised in writing to the manufacturer within the referenced warranty period. The use of SWTD components shall be limited to the application for which it was specifically designed.
- 1.7 The SWTD manufacturer shall submit to the Engineer of Record a "Manufacturer's Performance Certification" certifying that each SWTD is capable of achieving the specified removal efficiencies listed in these specifications. The certification shall be supported by independent third-party research

1.8 No product substitutions shall be accepted unless submitted 10 days prior to project bid date, or as directed by the Engineer of Record. Submissions for substitutions require review and approval by the Engineer of Record, for hydraulic performance, impact to project designs, equivalent treatment performance, and any required project plan and report (hydrology/hydraulic, water quality, stormwater pollution) modifications that would be required by the approving jurisdictions/agencies. Contractor to coordinate with the Engineer of Record any applicable modifications to the project estimates of cost, bonding amount determinations, plan check fees for changes to approved documents, and/or any other regulatory requirements resulting from the product substitution.

#### 2.0 MATERIALS

- 2.1 Housing unit of stormwater treatment device shall be constructed of pre-cast or cast-in-place concrete, no exceptions. Precast concrete components shall conform to applicable sections of ASTM C 478, ASTM C 857 and ASTM C 858 and the following:
  - 2.1.1 Concrete shall achieve a minimum 28-day compressive strength of 4,000 pounds per square-inch (psi);
  - 2.1.2 Unless otherwise noted, the precast concrete sections shall be designed to withstand lateral earth and AASHTO H-20 traffic loads;
  - 2.1.3 Cement shall be Type III Portland Cement conforming to ASTM C 150;
  - 2.1.4 Aggregates shall conform to ASTM C 33;
  - 2.1.5 Reinforcing steel shall be deformed billet-steel bars, welded steel wire or deformed welded steel wire conforming to ASTM A 615, A 185, or A 497.
  - 2.1.6 Joints shall be sealed with preformed joint sealing compound conforming to ASTM C 990.
  - 2.1.7 Shipping of components shall not be initiated until a minimum compressive strength of 4,000 psi is attained or five (5) calendar days after fabrication has expired, whichever occurs first.
- 2.2 Internal Components and appurtenances shall conform to the following:
  - 2.2.1 Screen and support structure shall be manufactured of Type 316 and 316L stainless steel conforming to ASTM F 1267-01;
  - 2.2.2 Hardware shall be manufactured of Type 316 stainless steel conforming to ASTM A 320;
  - 2.2.3 Fiberglass components shall conform to applicable sections of ASTM D-4097
  - 2.2.4 Access system(s) conform to the following:
  - 2.2.5 Manhole castings shall be designed to withstand AASHTO H-20 loadings and manufactured of cast-iron conforming to ASTM A 48 Class 30.

#### 3.0 PERFORMANCE

- 3.1 The SWTD shall be sized to either achieve an 80 percent average annual reduction in the total suspended solid load with a particle size distribution having a mean particle size (d<sub>50</sub>) of 125 microns unless otherwise stated.
- 3.2 The SWTD shall be capable of capturing and retaining 100 percent of pollutants greater than or equal to 2.4 millimeters (mm) regardless of the pollutant's specific gravity (i.e.: floatable and neutrally buoyant materials) for flows up to the device's rated-treatment capacity. The SWTD shall be designed to retain all previously captured pollutants addressed by this

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- 3.3 The SWTD shall be designed with a sump chamber for the storage of captured sediments and other negatively buoyant pollutants in between maintenance cycles. The minimum storage capacity provided by the sump chamber shall be in accordance with the volume listed in Table 1. The boundaries of the sump chamber shall be limited to that which do not degrade the SWTD's treatment efficiency as captured pollutants accumulate. The sump chamber shall be separate from the treatment processing portion(s) of the SWTD to minimize the probability of fine particle re-suspension. In order to not restrict the Owner's ability to maintain the SWTD, the minimum dimension providing access from the ground surface to the sump chamber shall be 16 inches in diameter.
- 3.4 The SWTD shall be designed to capture and retain Total Petroleum Hydrocarbons generated by wet-weather flow and dry-weather gross spills and have a capacity listed in Table 1 of the required unit.
- 3.5 The SWTD shall convey the flow from the peak storm event of the drainage network, in accordance with required hydraulic upstream conditions as defined by the Engineer. If a substitute SWTD is proposed, supporting documentation shall be submitted that demonstrates equal or better upstream hydraulic conditions compared to that specified herein. This documentation shall be signed and sealed by a Professional Engineer registered in the State of the work. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.
- 3.6 The SWTD shall have completed field tested following TARP Tier II protocol requirements

#### 4.0 EXECUTION

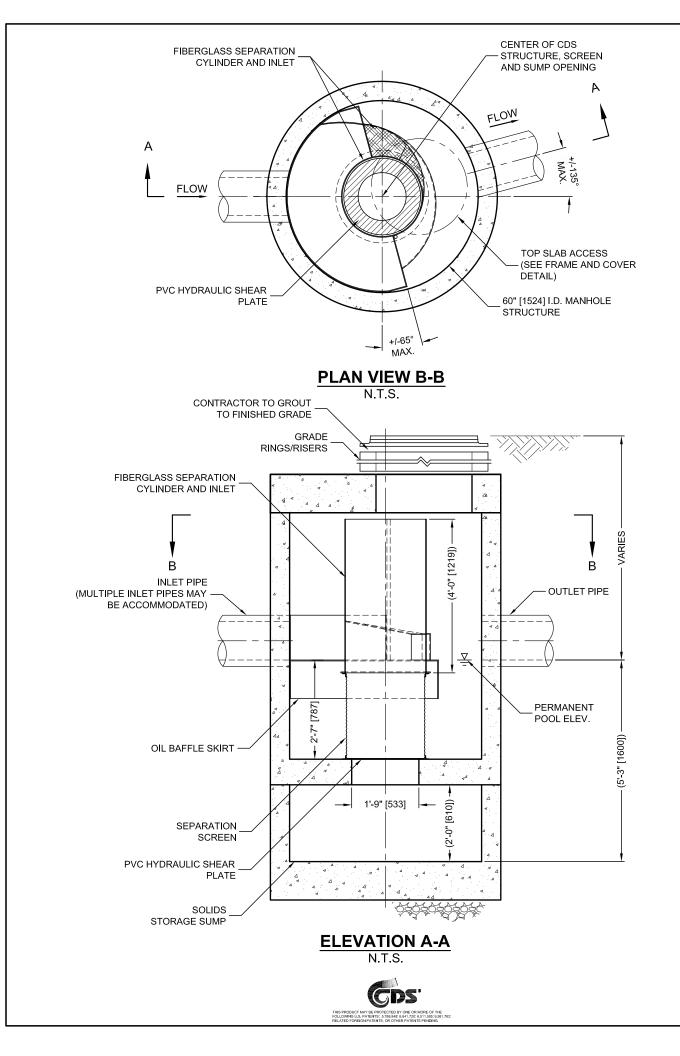
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- 4.2 The SWTD shall be installed in accordance with the manufacturer's recommendations and related sections of the contract documents. The manufacturer shall provide the contractor installation instructions and offer on-site guidance during the important stages of the installation as identified by the manufacturer at no additional expense. A minimum of 72 hours notice shall be provided to the manufacturer prior to their performance of the services included under this subsection.
- 4.3 The contractor shall fill all voids associated with lifting provisions provided by the manufacturer. These voids shall be filled with non-shrinking grout providing a finished surface consistent with adjacent surfaces. The contractor shall trim all protruding lifting provisions flush with the adjacent concrete surface in a manner, which leaves no sharp points or edges.

4.4 The contractor shall removal all loose material and pooling water from the SWTD prior to the transfer of operational responsibility to the Owner.

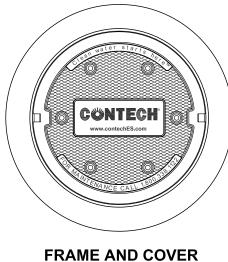
Storage capacities					
CDS Model	Minimum Sump Storage Capacity	Minimum Oil Storage			
	(yd <sup>3</sup> )/(m <sup>3</sup> )	Capacity (gal)/(L)			
CDS2015-4	0.9(0.7)	61(232)			
CDS2015-5	1.5(1.1)	83(313)			
CDS2020-5	1.5(1.1)	99(376)			
CDS2025-5	1.5(1.1)	116(439)			
CDS3020-6	2.1 (1.6)	184(696)			
CDS3025-6	2.1(1.6)	210(795)			
CDS3030-6	2.1 (1.6)	236(895)			
CDS3035-6	2.1 (1.6)	263(994)			
CDS3535-7	2.9(2.2)	377(1426)			
CDS4030-8	5.6(4.3)	426(1612)			
CDS4040-8	5.6 (4.3)	520(1970)			
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CDS5668-10	8.7(6.7)	1172(4435)			
CDS5678-10	8.7(6.7)	1309(4956)			
CDS7070-DV	3.6(2.8)	914 (3459)			
CDS10060-DV	5.0 (3.8)	792 (2997)			
CDS10080-DV	5.0 (3.8)	1057 (4000)			
CDS100100-DV	5.0 (3.8)	1320 (4996)			

TABLE 1 Storm Water Treatment Device Storage Capacities

**END OF SECTION** 



#### THE STANDARD CDS2020-5-C CONFIGURATION IS SHOWN. ALTERNATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS. **CONFIGURATION DESCRIPTION** GRATED INLET ONLY (NO INLET PIPE) GRATED INLET WITH INLET PIPE OR PIPES CURB INLET ONLY (NO INLET PIPE) CURB INLET WITH INLET PIPE OR PIPES SEPARATE OIL BAFFLE (SINGLE INLET PIPE REQUIRED FOR THIS CONFIGURATION) SEDIMENT WEIR FOR NJDEP / NJCAT CONFORMING UNITS



(DIAMETER VARIES) N.T.S.

**GENERAL NOTES** 

- 1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
- 2. DIMENSIONS MARKED WITH ( ) ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
- SOLUTIONS LLC REPRESENTATIVE. www.contechES.com
- 6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

#### INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE В. (LIFTING CLUTCHES PROVIDED).
- CONTRACTOR TO ADD JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS, AND ASSEMBLE STRUCTURE. C.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN
- CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS E. SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.

ENGINEERED SOLUTIONS LLC www.contechES.com 9025 Centre Pointe Dr., Suite 400, West Chester, OH 45069 800-338-1122 513-645-7000 513-645-7993 FAX

#### CDS2020-5-C DESIGN NOTES

SITE SPECIFIC DATA REQUIREMENTS					
STRUCTURE ID					
WATER QUALITY	FLOW RAT	E (CFS OR L/s)		*	
PEAK FLOW RAT		, ,		*	
RETURN PERIOD	OF PEAK F	LOW (YRS)		*	
SCREEN APERTU	*				
	•	,	-		
PIPE DATA:	I.E.	MATERIAL	DIAMETER		
INLET PIPE 1	*	*	*		
INLET PIPE 2	*	*		*	
OUTLET PIPE	*	*	*		
RIM ELEVATION				*	
ANTI-FLOTATION BALLAST WIDTH			HEIGHT		
* *				*	
NOTES/SPECIAL REQUIREMENTS:					

RIM ELEVATION					
ANTI-FLOTATION BALLAST	WIDTH	HEIG			
	*	*			
NOTES/SPECIAL REQUIREMENTS:					
* PER ENGINEER OF RECORD					

3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED

4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING. 5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET HS20 (AASHTO M 306) LOAD RATING, ASSUMING GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION.

CDS2020-5-C

**INLINE CDS** 

STANDARD DETAIL





# Hydrodynamic Separation



## The experts you need to solve your stormwater challenges

Contech is the leader in stormwater solutions, helping engineers, contractors and owners with infrastructure and land development projects throughout North America.

With our responsive team of stormwater experts, local regulatory expertise and flexible solutions, Contech is the trusted partner you can count on for stormwater management solutions.

## Your Contech Team









#### STORMWATER CONSULTANT

It's my job to recommend the best solution to meet permitting requirements.

#### STORMWATER DESIGN ENGINEER

I work with consultants to design the best approved solution to meet your project's needs.

#### **REGULATORY MANAGER**

I understand the local stormwater regulations and what solutions will be approved.

SALES ENGINEER

I make sure our solutions meet the needs of the contractor during construction.

#### Contech is your partner in stormwater management solutions



### Removing Pollutants using Hydrodynamic Separation

HDS systems play a vital role in protecting our waterways by removing high levels of sediment, trash, debris, and hydrocarbons from stormwater runoff.

Frequently used as end-of-pipe solutions, they are also used to provide stormwater quality treatment in places where space is limited.

HDS systems capture and retain a variety of stormwater pollutants and are very easy to maintain. These two key benefits have resulted in new uses for HDS technologies, such as pretreating detention, Low Impact Development, and green infrastructure practices, as well as other land-based stormwater treatment systems. Utilize high-performance hydrodynamic separation to effectively remove finer sediment, oil and grease, and floating and sinking debris.





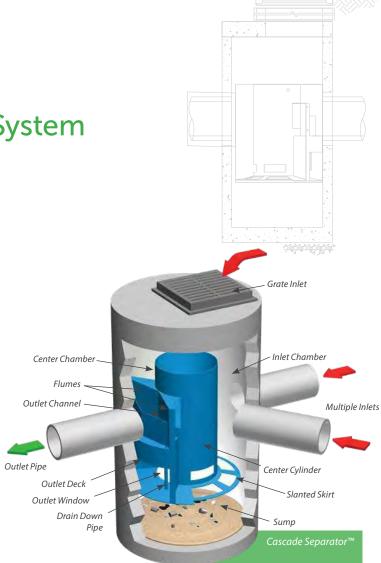


## The Cascade Separator<sup>™</sup> System

#### Advanced Sediment Capture Technology ...

The Cascade Separator<sup>™</sup> is the newest innovation in stormwater treatment from Contech. The Cascade Separator was developed by Contech's stormwater experts using advanced modeling tools and Contech's industry leading stormwater laboratory.

This innovative hydrodynamic separator excels at sediment capture and retention while also removing hydrocarbons, trash, and debris from stormwater runoff. What makes the Cascade Separator unique is the use of opposing vortices that enhance particle settling and a unique skirt design that allows for sediment transport into the sump while reducing turbulence and resuspension of previously captured material. These two factors allow the Cascade Separator to treat high flow rates in a small footprint, resulting in an efficient and economical solution for any site.



FEATURE	BENEFIT
Unique skirt design & opposing vortices	Superior TSS removal; reduced system size and costs
Inlet area accepts wide range of inlet pipe angles	Design and installation flexibility
Accepts multiple inlet pipes	Eliminates the need for separate junction structure
Grate inlet option	Eliminates the need for a separate grate inlet structure
Internal bypass	Eliminates the need for a separate bypass structure
Clear access to sump and stored pollutants	Fast, easy maintenance

Learn More: www.ContechES.com/cascade

#### SELECT CASCADE APPROVALS

 New Jersey Department of Environmental Protection Certification (NJDEP)

#### CASCADE MAINTENANCE

Cascade provides unobstructed access to stored pollutants, making it easy to maintain using a vacuum truck, with no requirement to enter the unit.

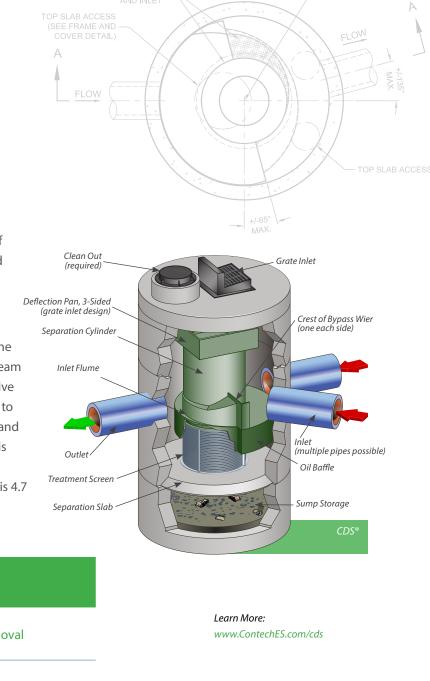
#### Setting new standards in Stormwater Treatment

## The CDS® System

#### Superior Trash Removal ...

The CDS is a hybrid technology that uses a combination of swirl concentration and indirect screening to separate and trap trash, debris, sediment, and hydrocarbons from stormwater runoff.

At the heart of the CDS system is a unique screening technology used to capture and retain trash and debris. The screen face is louvered so that it is smooth in the downstream direction. The effect created is called "Continuous Deflective Separation." The power of the incoming flow is harnessed to continually shear debris off the screen and to direct trash and sediment toward the center of the separation cylinder. This results in a screen that is self-cleaning and provides 100% removal of floatables and neutrally buoyant material debris 4.7 mm or larger, without blinding.



FEATURE	BENEFIT
Captures and retains 100% of floatables and neutrally buoyant debris 4.7 mm or larger	Superior trash removal
Self-cleaning screen	Ease of maintenance
Isolated storage sump eliminates scour potential	Excellent pollutant retention
Internal bypass	Eliminates the need for additional structures
Multiple pipe inlets and 90-180° angles	Design flexibility
Clear access to sump and stored pollutants	Fast, easy maintenance

#### SELECT CDS APPROVALS

- Washington Department of Ecology (GULD)
   Pretreatment
- New Jersey Department of Environmental Protection Certification (NJDEP)
- Canadian Environmental Technology Verification (ETV)
- California Statewide Trash Amendments
   Full Capture System Certified\*

\* The CDS System has been certified by the California State Water Resources Control Board as a Full Capture System provided that it is sized to treat the peak flow rate from the region specific 1-year, 1-hour design storm, or the peak flow capacity of the corresponding storm drain, whichever is less.



## The Vortechs® System

## Stormwater Treatment in a Shallow Footprint ....

Vortechs combines swirl concentration and flow controls into a single treatment unit that captures and retains trash, debris, sediment, and hydrocarbons from stormwater runoff.

The Vortechs system's large swirl chamber and flow controls work together to create a low energy environment, ideal for capturing and retaining particles down to 50 microns.

Vortechs is the ideal solution for sites with high groundwater, bedrock, utility conflicts, or sites with a large volume runoff.

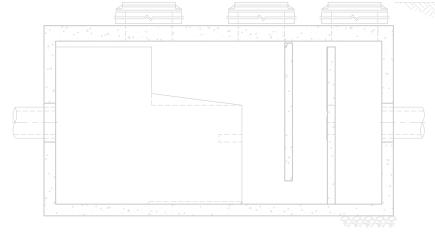
The Vortechs System is approved by the Washington Department of Ecology (GULD) - Pretreatment.

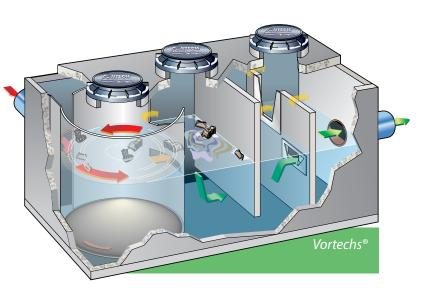
#### SELECT VORTECHS APPROVALS

Washington Department of Ecology (GULD)
 Pretreatment

Learn More: www.ContechES.com/vortechs

FEATURE	BENEFIT
Large swirl chamber	Fine particle removal down to 50 microns
Shallow profile – Typical depth below pipe invert is only 3 feet.	Can be used on sites with high groundwater, bedrock, or utility conflicts
Unobstructed access to stored pollutants	Fast, easy maintenance





### Design Your Own Hydrodynamic Separator (DYOHDS<sup>™</sup>)

÷	Hydrodynamic Separation	n Product Calculator	Jane Smith (external) එ
Project Name : Birmingham Gas Station			Site Designation : WQ
1 Project	2 Design	3 Treatment	Performance
System Sizing			
CDS or Cascade Separator		c	ascade Separator Features
User Selected Treatment System * Cascade Separator Learn More About Cascade Separator Particle Size Distribution or DS0 * 110 System Model CS-4 CS-4 Prediment free Languit Learner of Predimery (Col 80.85 The peaks flow rate exceeds the maximum capacity Contact Us			Grate Inler Inler Chamber Unleiple Inlets Genter Cylinder Stanted Skirt Sump

Learn More: www.ContechES.com/dyohds

#### Quickly prepare designs for estimates and project meetings ...

Engineers are always looking for new ways to quickly prepare designs for estimates and project meetings. Contech has developed an online tool to help with the hydrodynamic separation product selection process... the Design Your Own Hydrodynamic Separator (DYOHDS<sup>™</sup>) tool.

This free, online tool fully automates the layout process for identifying the proper hydrodynamic separator for your site. You can create multiple systems for each project while saving all project information for future use.

- Multiple sizing methods available.
- Site-specific questions ensure the selected unit will comply with site constraints.
- Multiple treatment options may be available based on regulations and site parameters.
- Follow up reports contain a site-specific design, sizing summary, standard detail, and specification.

## A free, online tool to aid in the selection of a hydrodynamic separation solution.



## A partner





STORMWATER SOLUTIONS



Few companies offer the wide range of highquality stormwater resources you can find with us — state-of-the-art products, decades of expertise, and all the maintenance support you need to operate your system cost-effectively.



#### THE CONTECH WAY

Contech® Engineered Solutions provides innovative, cost-effective site solutions to engineers, contractors, and developers on projects across North America. Our portfolio includes bridges, drainage, erosion control, retaining wall, sanitary sewer and stormwater management products.

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**STRUCTURES** 

**SOLUTIONS** 



IF

Project Name:ASML Campus Traffic Flow Safety ImprovementProject Number:A0969-015Project Location:Wilton, CTDescription:Stormwater BMP Pollutant Removal EstimatePrepared By:JACDate:May 22, 2022

				Pollu	utant		
Item	Units	TKN	P	TSS	Pb	Cu	Zn
Proposed, Pre Treatment	lb/yr	5.61	0.96	328.11	0.49	0.14	1.07
Proposed, Post Treatment	lb/yr	0.00	0.00	0.00	0.00	0.00	0.00
Reduction, Pre to Post Treat		100.0%	100.0%	100.0%	100.0%	100.0%	100.0%



Project Name:ASML Campus Traffic Flow Safety ImprovementProject Number:A0969-015Project Location:Wilton, CTDescription:Stormwater BMP Pollutant Removal EstimatePrepared By: JACDate: May 22, 2022

Location: Annual Rainfall:	Infiltrat 44.84	ion Syste	em (PR-V	/S-03B)		Со	ndition: <b>P</b>	roposed
Impervious Fraction:	0.73	inches			Tota	al Area =	0.67	acres
Pollutant	<u>Resid</u>	ential	<u>Comr</u>	<u>nercial</u>	<u>Op</u>	<u>en</u>	Weighted	
	A (acres)	EMC (mg/L)	A (acres)	EMC (mg/l)	A (acres)	EMC (mg/L)	EMC (mg/L)	L (lbs/yr)
Total Nitrogen (N)	0.000	1.900	0.670	1.180	0.000	0.965	1.180	5.611
Total Phosphorus (P)	0.000	0.383	0.670	0.201	0.000	0.121	0.201	0.956
Total Suspended Solids	0.000	101.0	0.670	69.0	0.000	70.0	69.0	328.1
Lead	0.000	0.144	0.670	0.104	0.000	0.030	0.104	0.495
Copper	0.000	0.033	0.670	0.029	0.000	0.000	0.029	0.138
Zinc	0.000 0.135 0.670 0.226 0.000 0.195 0.226						1.075	
L EMC I P A	Pollution Mean Eve Fraction of Annual R	Loading ( ent Mean	Concentra ious Acres )	tion (mg/				

Notes:

1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.



Project Name:ASML Campus Traffic Flow Safety ImprovementProject Number:A0969-015Project Location:Wilton, CTDescription:Stormwater BMP Pollutant Removal EstimatePrepared By:JACDate:May 22, 2022

Location:	North Park	ing Lot				Co	ndition: Proposed
Annual Rainfall:	44.84	inches					
Impervious Fraction:	0.73				Total	Area =	0.67 acres
BMP:	<b>Gross Parti</b>	cle Sepai	rators W	QS-001	+ WQS-00	)2	
		-		-	-		
Pollutant	Lin 1	Lin 2	Sum L	RR	Lremoved	Lout	
	(lbs)	(lbs)	(lbs)	(-)	(lbs)	(lbs)	
Total Nitrogen (N)	5.611	0.000	5.611	18.3	1.03	4.584	
Total Phosphorus (P)	0.956	0.000	0.956	66.9	0.64	0.316	
Total Suspended Calida	328.111	0.0	328.1	FO	164.06	164.1	
Total Suspended Solids	520.111	0.0	520.1	50	104.00	104.1	
Lead	0.495	0.000	0.495	46.5	0.23	0.265	
Leud	0.155	0.000	0.155	10.5	0.25	0.205	
Copper	0.138	0.000	0.138	56.2	0.08	0.060	
Zinc	1.075	0.000	1.075	85.3	0.92	0.158	
Lin 1	Pollutant Loa	ad Area 1					
Sum L	Sum of Pollu	tant Load	to this Bl	ЧP			
RR	Removal rate	e in perce	ntage				
Lout	Pollutant Loa	ad out of E	3MP				

Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D.,Millsaps College December 9th, 2009.



Project Name:ASML Campus Traffic Flow Safety ImprovementProject Number:A0969-015Project Location:Wilton, CTDescription:Stormwater BMP Pollutant Removal EstimatePrepared By:JACDate:May 22, 2022

Location: Annual Rainfall:	North Parking Lot 44.84 inches	;			Со	ndition: <b>Proposed</b>
Impervious Fraction: BMP:	0.73 Infiltration System	m		Tota	Area =	0.67 acres
Pollutant	Lin 1 (Ibs)	Sum L (lbs)	RR (%)	Lremoved (Ibs)	Lout (Ibs)	
Total Nitrogen (N)	4.584	4.584	100	4.58	0.000	
Total Phosphorus (P)	0.316	0.316	100	0.32	0.000	
Total Suspended Solids	164.055	164.1	100	164.06	0.0	
Lead	0.265	0.265	100	0.26	0.000	
Copper	0.060	0.060	100	0.06	0.000	
Zinc	0.158	0.158	100	0.16	0.000	
Lin 1 Sum L RR Lout	Pollutant Load Out of Sum of Pollutant Lo Removal rate in per Pollutant Load out of	ad to this centage	•	ch Basins B	MP	

Notes:

- 1. Pollution loading calculated using *Municipal Stormwater Management, Second Edition*, by Debo & Reese, pgs. 193-195.
- 2. Pollutant removal rates for Rain Garden/Infiltration Trench and Wet Pond taken from *Municipal Stormwater Management, Second Edition*, by Debo & Reese, Tbl. 13-13, p. 748.
- 3. Pollutant removal rates for Vortechnics Stormwater Quality Unit and Deep Sump Catch Basins taken from *Final Report, Stormwater Treatment Devices Section 319 Project, Project* #99-07, Submitted to CT DEP April 15, 2002.
- 4. Pollutant removal rates for Ultra Urban Filter Catch Basin inserts taken from *Final Report: Sediment Removal from Simulated Stormwater Runoff by Abtech Industries, Inc. UltraUrban Filter-CO in Laboratory Flume Tests*, Submitted by Stan Galicki, Ph.D.,Millsaps College December 9th, 2009.

## **Tighe&Bond**

**APPENDIX F** 



### ASML Campus Traffic Safety Improvements Stormwater Maintenance Plan

May 24, 2022

#### F.1 Storm Drainage Maintenance and Inspection Schedule

The maintenance of stormwater treatment systems is critical to their performance because without proper maintenance, these structures are likely to fail. Proper operation and maintenance ensure that the structures remain effective at removing pollutants as originally designed. It will:

- Reduce failure, therefore improve water quality;
- Maintain the volume of stormwater treated in the long term; and
- Increase pollutant removal efficiency

The storm drainage system as a whole will be inspected semi-annually to ensure that the system is functioning properly. The inspections will occur in early fall and late spring initially. If these inspections show that debris and sediment accumulate, more frequent inspections will be scheduled according to the rate of debris generation. Additional inspections and cleanup work will be conducted following major runoff events.

The initial inspection will be made during an intense rainfall to check the adequacy of the catch basins, piping, oil separators, gross particle separators and outlets.

The following is a generalized checklist of items that will be checked and maintained during scheduled maintenance operations.

- 1. Catch basin grates will be cleaned of all debris. Catch basins and sumps will be cleaned of all silt, debris, and sediment, and the outlets from the catch basins will be inspected and cleaned to make sure nothing is clogging the discharge pipe.
- 2. The gross particle separators will be skimmed, and oil and scum removed. In a separate operation, silt sand and sediment will be removed. Once the structures are cleaned of debris, the chamber will be refilled with clean water to prevent wash through of debris and oil during next storm event.
- 3. All pipe outlets will be inspected, and any debris removed.
- 4. Remove accumulated trash and debris around the site on a weekly basis to prevent debris from washing into inlets.
- 5. Inspect the underground chamber system for signs of clogging.
- 6. Inspect the rain garden and stormwater management pond for signs of erosion, and confirm plantings are in good condition.

#### F1.1 Catch Basins

#### F1.1.1 Design Purpose

A catch basin is an inlet with a grate designed to intercept the flow of stormwater from the surface and to convey it into the storm sewer system.

#### F1.1.2 Design Features

Catch basins have sumps, a space below the lowest outlet pipe. The purpose of the sump is to catch and collect debris before it enters the outlet pipe, potentially clogging the pipe, or resulting in the downstream accumulation of the debris.

#### **F1.1.3 Inspection Requirements**

Each catch basin shall be inspected quarterly, with one inspection occurring during the month of April. Note depth of debris accumulation, and overall condition of the catch basin structure itself. Note any floating oils or sheens. Maintain a log of inspections.

#### **F1.1.4 Maintenance Requirements**

Any debris occurring within one foot from the bottom of each sump shall be removed by Vacuum "Vactor" type of maintenance equipment by a Connecticut licensed hauler who shall legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed. Maintain a log of maintenance activity.

Floating oils shall be removed using oil absorptive pads and disposed in a legal manner off site.

#### F1.2 Manholes

#### F1.2.1 Design Purpose

A manhole is used as a structure to join two or more segments of storm sewer piping as a junction, or to allow deflections along a pipe alignment. Manholes do not allow for capture of surface stormwater runoff.

#### F1.2.2 Design Features

Manholes have formed inverts which allow for less abrupt flow transitions around alignment deflections.

#### **F1.2.3 Inspection Requirements**

Each manhole shall be opened once a year in April. Note any accumulation of debris and sediment, as well as the structural integrity of the manhole itself. Maintain a log of inspections.

#### **F1.2.4** Maintenance Requirements

Any debris occurring within the manhole shall be removed by Vacuum "Vactor" type of maintenance equipment by a Connecticut licensed hauler who shall legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed. Maintain a log of maintenance activity.



#### F1.3 Yard Drains

#### F1.3.1 Design Purpose

Yard drains are inlets with a grate designed to intercept the flow of stormwater from the surface and to convey it into the storm sewer system. Yard drains are similar to catch basins, except that they are smaller in cross section because they drain smaller areas. Trench drains are inlets with a with long and narrow grates, typically positioned around buildings and parking garages to prevent stormwater from entering.

#### F1.3.2 Design Features

Yard drains have sumps, a space below the lowest outlet pipe. The purpose of the sump is to catch and collect debris before it enters the outlet pipe, potentially clogging the pipe, or resulting in the downstream deposition of the debris. Trench drains contain a channel below the grate where stormwater runoff flows to the outlet pipe. Smaller debris is collected within this channel prior to discharging.

#### **F1.3.3 Inspection Requirements**

Each yard drain and trench drain shall be inspected quarterly, with one inspection occurring during the month of April. Note depth of debris accumulation, any visible oil sheens, and overall condition of the yard drain and trench drain structure itself. Maintain a log of inspections.

#### F1.3.4 Maintenance Requirements

Any debris occurring within one foot from the bottom of each sump or significant debris accumulation within the trench drain channel shall be removed by Vacuum "Vactor" type of maintenance equipment or by hand using hand tools by a Connecticut licensed hauler who shall legally dispose of removed sand at an off-site location. The road sand may not be reused or stored on-site. As part of the hauling contract, the hauler shall notify the Owner in writing where the material is being disposed. Maintain a log of maintenance activity.

Floating oils shall be removed using oil absorptive pads and disposed in a legal manner off site.

#### F1.4 Gross Particle Separators

#### F1.4.1 Design Purpose

Gross particle separators promote the interception of oils and suspended solids by forcing low flows into a swirl chamber, utilizing hydrodynamic separation to achieve pollutant removal.

#### F1.4.2 Design Features

Gross particle separators include internal bypasses to allow heavier storm events to bypass the swirl chamber, avoiding resuspension of sediments.

#### **F1.4.3 Inspection Requirements**

Inspection is the key to effective maintenance. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. Installations should also be inspected more frequently where excessive amounts of trash are expected.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument. If absorbent material is used for enhanced removal of hydrocarbons, the level of discoloration of the sorbent material should also be identified during inspection. Keep inspection records.

Access to the gross particle separators are typically achieved through the manhole access covers. One opening allows for inspection and cleanout of the separation chamber (cylinder and screen) and isolated sump. The other allows for inspection and cleanout of sediment captured and retained outside the screen. For deep units, a single manhole access point would allow both sump cleanout and access outside the screen.

#### **F1.4.4 Maintenance Requirements**

The gross particle separators should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated. If absorbent material is used, it should be replaced when significant discoloration has occurred. Performance will not be impacted until 100% of the sump capacity is exceeded however it is recommended that the system be cleaned prior to that for easier removal of sediment. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Once this measurement is recorded, it should be compared to the as-built drawing for the unit to determine whether the height of the sediment pile off the bottom of the sump floor exceeds 75% of the total height of isolated sump.

Cleaning should be done during dry weather conditions when no flow is entering the system. The use of a vacuum truck is generally the most effective and convenient method of removing pollutants from the system. Simply remove the manhole covers and insert the vacuum hose into the sump. The system should be completely drained down and the sump fully evacuated of sediment. The area outside the screen should also be cleaned out if pollutant build-up exists in this area.

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, the system should be cleaned out immediately in the event of an oil or gasoline spill. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use absorbent pads since they are usually less expensive to dispose than the oil/water emulsion that may be created by vacuuming the oily layer. Trash and debris can be netted out to separate it from the other pollutants. The screen should be power washed to ensure it is free of trash and debris.

Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure that proper safety precautions have been followed. Confined space entry procedures need to be followed if physical access is required. Disposal of all material removed should be done in accordance with local regulations. In many jurisdictions, disposal of the sediments may be handled in the same manner as the disposal of sediments removed from catch basins or deep sump manholes.

#### F1.5 Underground Infiltration Chambers

#### F1.5.1 Design Purpose

The underground infiltration chambers are intended to retain the water quality volume to meet the MS4 Permit requirements, and the groundwater recharge volume requirement. Stormwater entering the chambers will be pretreated by the gross particle separator to maximize the performance of the system.

#### F1.5.2 Design Features

The infiltration chambers are concrete, which are more durable than plastic systems. They are surrounded by stone on the sides and bottom which provides additional stormwater storage in the voids.

#### F1.5.3 Inspection Requirements

Inspection is the key to effective maintenance. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations.

Inspections shall note if there is evidence of an unusual amount of silt build-up, the presence of water, and other structural defects.

The underground chamber systems have inspection manholes to facilitate access to observe underlying conditions, such as sediment build-up and failure to drain.

#### **F1.5.4 Maintenance Requirements**

The underground chamber systems should be vacuumed out when sediment begins to accumulate to the extent that the system does not drain within 48 hours. Large accumulations of debris that reduce the storage capacity shall be removed. Cleanout should be scheduled during dry weather.

#### F1.6 Rain Garden

#### F1.6.1 Design Purpose

The rain garden is proposed to promote biological uptake of stormwater pollutants and to recharge groundwater. The rain garden is designed to allow up to 6 inches of ponding, at which point, the ponded runoff would overflow into a grate set 6 inches above the bottom of the rain garden.

#### F1.6.2 Design Features

The rain garden is designed with specifically selected plantings that can tolerate periodic inundation and dryness.

#### **F1.6.3 Inspection Requirements**

Inspection is the key to effective maintenance. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per



year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations.

Inspections shall note if there is evidence of an unusual amount of silt build-up, the persistent presence of water, and other structural defects.

#### **F1.6.4** Maintenance Requirements

The large accumulations of debris that reduce the storage capacity shall be removed. Cleanout should be scheduled during dry weather.

#### **F1.7 Other Site Areas**

#### F1.7.1 Vegetated Areas

Inspect annually in April, and after heavy rains, observe all slopes and embankments for signs of erosion, and replant areas of bare soil or with sparse growth. Armor rill erosion areas with riprap or divert the runoff to a stable area.

Throughout the year, mow vegetated areas as needed.

#### F1.7.2 Driveways and Parking Areas

The Owner shall sweep paved areas on the property in the spring to remove winter accumulations of road sand. Perform a visual inspection of paved areas four times per year with one inspection after the last snowfall, but no later than April 1. Clean paved areas as necessary during the remainder of the year

#### F1.7.3 Preventative Maintenance Overview

The following preventative maintenance schedule and activities are recommended for the site.

#### Table F-1

#### **Stormwater Preventative Maintenance Schedule**

Frequency	Preventative Maintenance Actions	Stormwater Measures/ No.
Monthly	Vegetation mowing and removal in growing season	Throughout site
Quarterly	Inspect catch basins and yard drains for accumulation of sediment and debris, note structural integrity of catch basin or yard drain. Remove if debris is within one foot of the sump.	CB, TD & YD
Semiannual	Inspect gross particle separators.	WQS
Annual	Inspect manholes for accumulation of sediment and debris, note structural integrity of manhole. Remove debris.	МН
	Sweep parking lots and driveways of accumulated sand	Parking lots and driveways
Unscheduled	Quick inspection after every 1" rain	CB, TD, YD, WQS Vegetated areas
	Mow vegetated areas as needed	Vegetated areas



#### F.2 Tools and Supplies Required

The following lists tools that may be necessary to carry out a maintenance program. Additional tools and supplies may be needed depending on the task:

Tool	Purpose
Clipboard and pen	Filling out maintenance logs
Manhole hook	For lifting grates
Safety goggles	Eye protection
Work gloves	Performing manual activities
Tape measure	Measurement of depth
Flashlight	Make observations in dark spaces
Shovel	Sediment removal from rain gardens
Vactor truck	Removal of sediments from sumps and gross particle separators
Lawn mower	Maintaining vegetation height in lawn and rain garden areas
Debris containers	Collection of debris
Hard hat	Safety
First Aid kit	Safety

### Table F-2Preventative Maintenance Equipment List

#### Some of the items in the list may need to be subcontracted out, such as the Vactor Truck.

J:\A\A0969 ASML\015\_Driveway Improvements\Report\Appendix F - Stormwater Maintenance Plan.docx

## **Tighe&Bond**

**APPENDIX G** 

Reach River Sta Profile	River Sta	Profile Q Total	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(tt)	(ff)	(ff)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(fft)	
Reach-1	29920	1% Chance	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86	1676.50	693.44	0.83
Reach-1	29760	1% Chance	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	28240	1% Chance	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	27468	1% Chance	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	27110	1% Chance	7455.00	136.60	147.46		147.51	0.000187	3.29	6234.70	1005.58	0.18
Reach-1	27025	1% Chance	7455.00	135.50	146.24	146.03	147.20	0.002112	10.68	2304.78	899.67	0.59
Reach-1	27020		Bridge									
Reach-1	27015	1% Chance	7455.00	135.50	146.08	146.08	147.18	0.002399	11.26	2163.67	894.64	0.63
Reach-1	26680	1% Chance	7455.00	134.00	142.89		143.57	0.002787	10.60	2063.23	590.00	0.65
Reach-1	26209	1% Chance	7455.00	133.40	143.04		143.12	0.000252	2.70	4826.43	949.44	0.19
Reach-1	26136	1% Chance	7455.00	130.20	142.10	141.28	142.87	0.001511	9.59	2344.50	703.85	0.51
Reach-1	26127.5		Bridge									
Reach-1	26119	1% Chance	7455.00	131.30	142.25	138.86	142.41	0.000532	5.04	3781.94	742.73	0.28
Reach-1	26058	1% Chance	7455.00	131.30	142.21		142.37	0.000543	5.08	3755.15	742.11	0.28
Reach-1	25358	1% Chance	7455.00	131.00	141.83		141.99	0.000552	5.61	3360.84	499.89	0.30
Reach-1	25340	1% Chance	7455.00	128.10	141.64		141.96	0.000587	6.55	3740.65	512.66	0.32
Reach-1	25334	1% Chance	7455.00	130.31	141.74		141.92	0.000444	4.96	3149.10	457.22	0.27
Reach-1	24975	1% Chance	7455.00	129.20	140.90		141.61	0.001359	8.49	1683.39	414.42	0.46
Reach-1	24922	1% Chance	7455.00	127.89	140.97		141.50	0.000829	7.23	1850.23	441.04	0.37
Reach-1	24677	1% Chance	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24620	1% Chance	7455.00	128.90	140.48		141.22		7.78	1737.87	369.05	0.42
Reach-1	24597	1% Chance	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-1	24570	1% Chance	7455.00	127.60	139.43	135.90	140.99	0.001698	10.31	1145.22	348.43	0.54
Reach-1	24542.5		Bridge									
Reach-1	24540	1% Chance	7455.00	127.60	138.19	135.88	140.32	0.002630	11.88	844.91	232.45	0.66
Reach-1	24485	1% Chance	7455.00	126.30	136.91	136.91	139.86	0.005771	14.75	837.67	207.98	0.90
Reach-1	24430	1% Chance	7455.00	126.60	137.85		138.46	0.002969	6.88	1464.10	254.64	0.39
Reach-1	24401	1% Chance	7455.00	124.66	137.67		138.37	0.003234	6.86	1278.84	257.49	0.39
Reach-1	24381	1% Chance	7455.00	124.66	136.85		138.24	0.002563	10.71	931.57	185.57	0.62
Reach-1	24180	1% Chance	7455.00	124.70	136.78	133.49	137.70	0.001560	8.02	1209.32	290.98	0.48
Reach-1	24105	1% Chance	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reach-1	23805	1% Chance	7455.00	124.00	135.70		136.34	0.001191	7.99	2548.56	544.98	0.44
Reach-1	23415	1% Chance	7455.00	123.00	133.11	133.11	135.33	0.004719	14.27	1451.84	358.59	0.84
Reach-1	23171	1% Chance	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23036	1% Chance	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	22916	1% Chance	7455.00	121.00	131.63		131.97	0.000628	5.38	2037.14	480.80	0.31
Reach-1	22765	1% Chance	7455.00	114.20	131.64		131.87	0.000301	4.19	2548.37	511.91	0.19
Reach-1	22450	1% Chance	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	22140	1% Chance	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	21825	1% Chance	7455.00	115.90	125.26	125.26	128.03	0.005781	14.07	847.23	239.90	0.91
Reach-1	21770	1% Chance	7455.00	115.40	125.08	123.47	127.59	0.003512	12.71	586.71	127.05	0.75
Reach-1	21757.5		Bridge									
Reach-1	21745	1% Chance	7455.00	115.40	124.39	123.47	127.33	0.004565	13.75	542.30	121.68	0.84
Reach-1	21695	1% Chance	7455.00	114.20	124.15	123.52	127.06	0.005894	13.66	548.04	85.02	0.89
Reach-1	21285	1% Chance	7455.00	114.30	124.30	122.75	125.23	0.001823	8.42	1577.95	503.26	0.52

Reach River Sta	River Sta	Profile	Q Total Min C	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(tt)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	29920	1% Chance	7455.00	147.00	153.96	153.96	155.12	0.004919	11.86		693.44	0.83
Reach-1	29760	1% Chance	7455.00	142.20	152.19		152.97	0.001276	7.45	1317.25	222.00	0.44
Reach-1	28240	1% Chance	7455.00	138.00	147.71	147.71	149.80	0.003506	12.69	1059.97	366.77	0.75
Reach-1	27468	1% Chance	7455.00	132.10	147.53		147.54	0.000024	1.37	10389.13	832.33	0.06
Reach-1	27110	1% Chance	7455.00	136.60	147.46		147.51	0.000187	3.29	6234.70	1005.58	0.18
Reach-1	27025	1% Chance	7455.00	135.50	146.24	146.03	147.20	0.002112	10.68	2304.78	899.67	0.59
Reach-1	27020		Bridge									
Reach-1	27015	1% Chance	7455.00	135.50	146.08	146.08	147.18	0.002399	11.26	2163.67	894.64	0.63
Reach-1	26680	1% Chance	7455.00	134.00	142.89		143.57	0.002786	10.59	2063.45	590.02	0.65
Reach-1	26209	1% Chance	7455.00	133.40	143.04		143.12	0.000252	2.70	4826.73	949.44	0.19
Reach-1	26136	1% Chance	7455.00	130.20	142.10	141.28	142.87	0.001510	9.59	2345.18	703.90	0.51
Reach-1	26127.5		Bridge									
Reach-1	26119	1% Chance	7455.00	131.30	142.25	138.86	142.41	0.000532	5.04	3782.66	742.75	0.28
Reach-1	26058	1% Chance	7455.00	131.30	142.21		142.37	0.000542	5.07	3755.88	742.13	0.28
Reach-1	25358	1% Chance	7455.00	131.00	141.83		141.99	0.000552	5.61	3361.43	500.04	0.30
Reach-1	25340	1% Chance	7455.00	128.10	141.64		141.97	0.000586	6.55	3741.29	512.66	0.32
Reach-1	25334	1% Chance	7455.00	130.31	141.74		141.92	0.000444	4.96	3149.66	457.23	0.27
Reach-1	24975	1% Chance	7455.00	129.20	140.90		141.61	0.001358	8.49	1684.37	414.69	0.46
Reach-1	24922	1% Chance	7455.00	127.89	140.96		141.50	0.000844	7.30	1830.66	440.06	0.38
Reach-1	24677	1% Chance	7455.00	127.87	140.94		141.30	0.000460	5.44	2180.83	396.78	0.28
Reach-1	24620	1% Chance	7455.00	128.90	140.48		141.22	0.001143	7.78	1737.87	369.05	0.42
Reach-1	24597	1% Chance	7455.00	127.30	140.63		141.12	0.000653	6.38	2207.50	395.10	0.32
Reach-1	24570	1% Chance	7455.00	127.60	139.43	135.90	140.99	0.001698	10.31	1145.22	348.43	0.54
Reach-1	24542.5		Bridge									
Reach-1	24540	1% Chance	7455.00	127.60	138.19	135.88	140.32	0.002630	11.88	844.91	232.45	0.66
Reach-1	24485	1% Chance	7455.00	126.30	136.91	136.91	139.86	0.005771	14.75	837.67	207.98	0.90
Reach-1	24430	1% Chance	7455.00	126.60	137.85		138.46	0.002969	6.88	1464.10	254.64	0.39
Reach-1	24401	1% Chance	7455.00	124.66	137.67		138.37	0.003234	6.86	1278.84	257.49	0.39
Reach-1	24381	1% Chance	7455.00	124.66	136.85		138.24	0.002563	10.71		185.57	0.62
Reach-1	24180	1% Chance	7455.00	124.70	136.78	133.49	137.70	0.001560	8.02	1209.32	290.98	0.48
Reach-1	24105	1% Chance	7455.00	124.80	135.32	134.24	137.40	0.004605	11.57	660.02	164.97	0.79
Reach-1	23805	1% Chance	7455.00	124.00	135.70		136.34	0.001191	7.99	2548.56	544.98	0.44
Reach-1	23415	1% Chance	7455.00	123.00	133.11	133.11	135.33	0.004719	14.27	1451.84	358.59	0.84
Reach-1	23171	1% Chance	7455.00	120.30	131.12	130.85	132.49	0.003967	9.91	913.48	264.15	0.67
Reach-1	23036	1% Chance	7455.00	121.70	131.62		132.07	0.000479	3.98	1491.73	341.41	0.25
Reach-1	22916	1% Chance	7455.00	121.00	131.63		131.97	0.000628	5.38		480.80	0.31
Reach-1	22765	1% Chance	7455.00	114.20	131.64		131.87	0.000301	4.19	2548.37	511.91	0.19
Reach-1	22450	1% Chance	7455.00	116.90	131.48		131.70	0.001059	4.04	2388.82	500.92	0.21

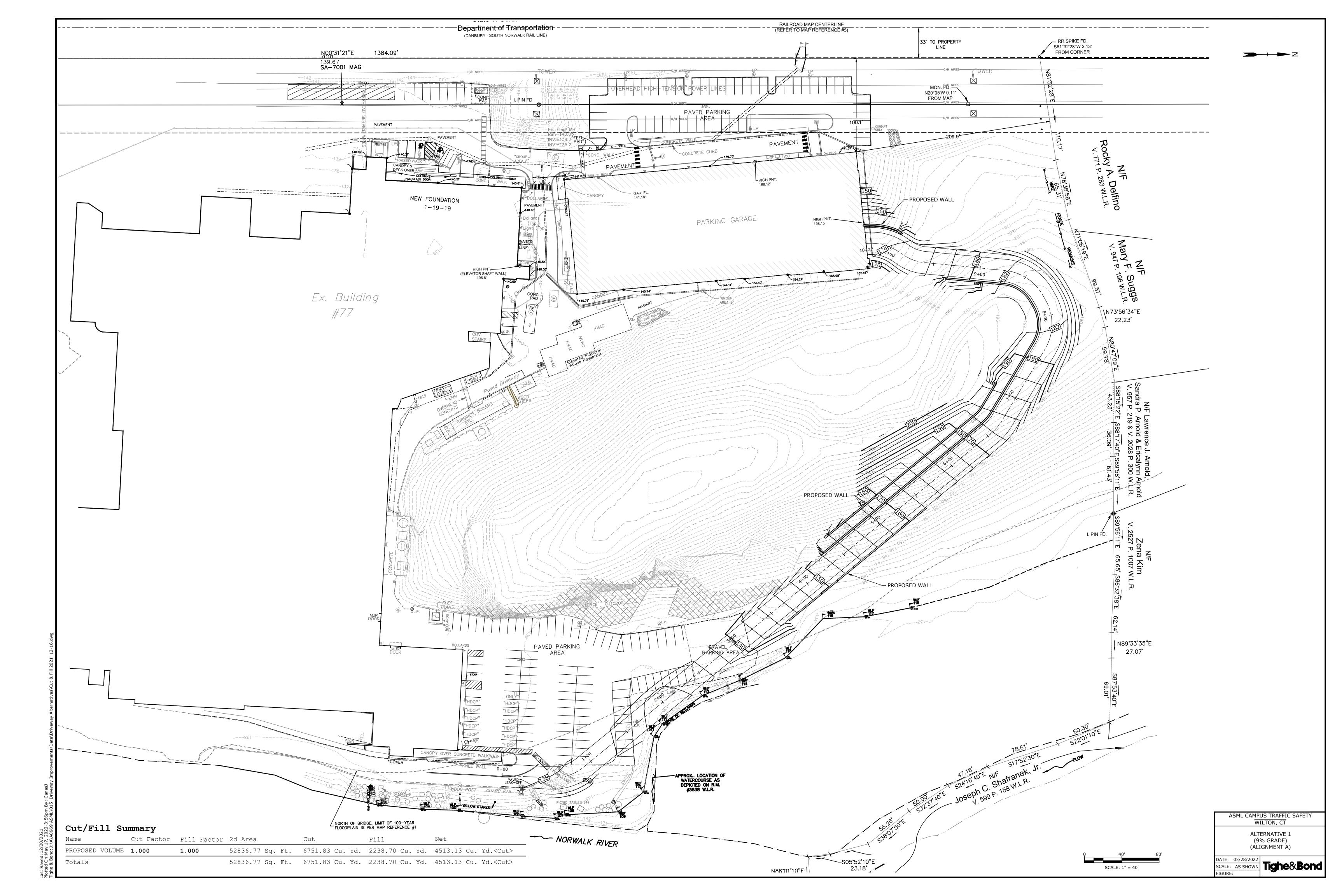
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Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	22140	1% Chance	7455.00	117.00	127.84	127.84	130.78	0.005382	16.12	1119.61	224.02	0.92
Reach-1	21825	1% Chance	7455.00	115.90	125.26	125.26	128.03		14.07	847.23	239.90	0.91
Reach-1	21770	1% Chance	7455.00	115.40	125.08	123.47	127.59	-	12.71	586.71	127.05	0.75
Reach-1	21757.5		Bridge									
Reach-1	21745	1% Chance	7455.00	115.40	124.39	123.47	127.33	0.004565	13.75	542.30	121.68	0.84
Reach-1	21695	1% Chance	7455.00	114.20	124.15	123.52	127.06	0.005894	13.66	548.04	85.02	0.89
Reach-1	21285	1% Chance	7455.00	114.30	124.30	122.75	125.23	0.001823	8.42	1577.95	503.26	0.52

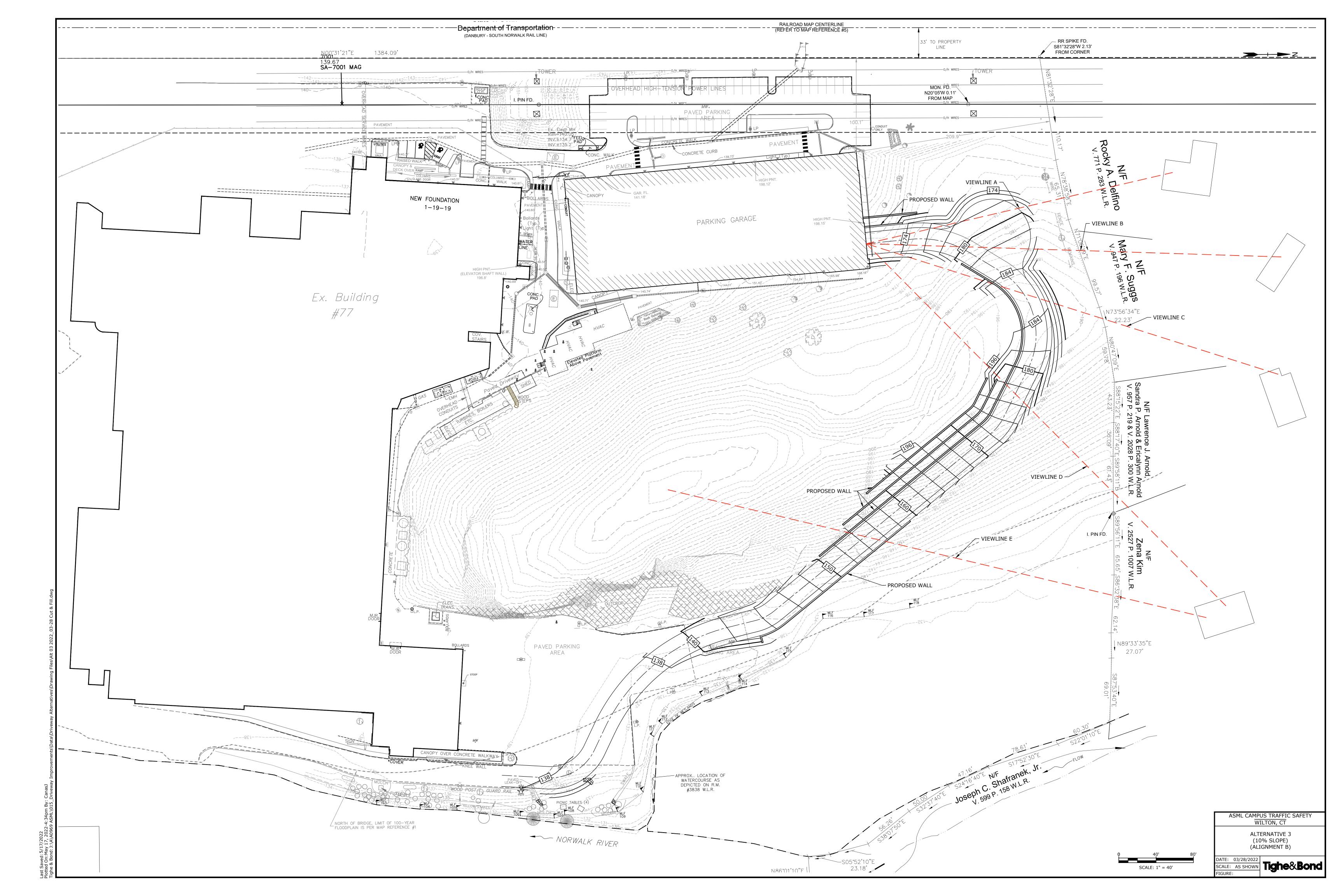
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le: 1% Chance	
1 Profile	
Reach: Reach-	
River: RIVER-1	
Plan: PROPOSED	
HEC-RAS	

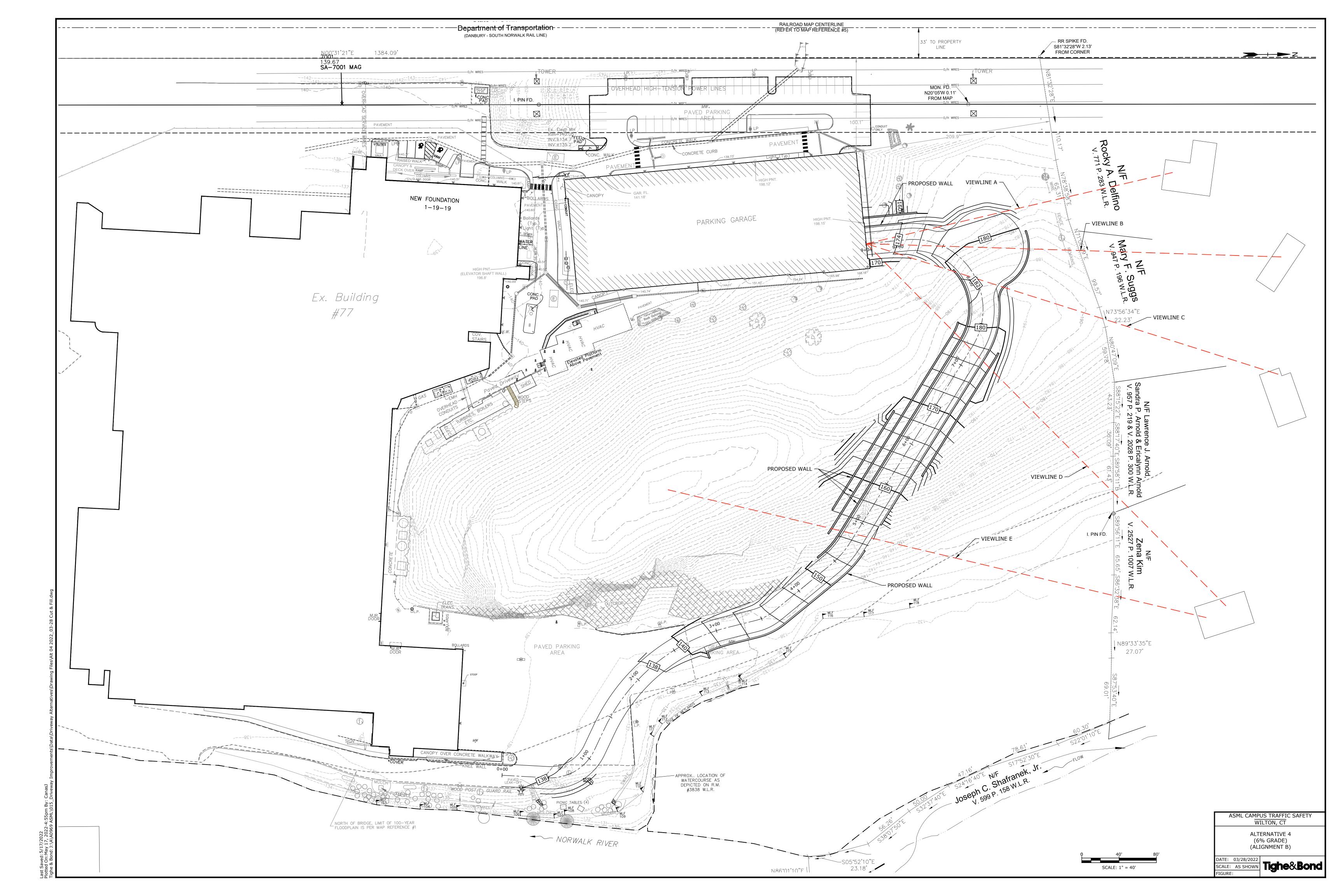
# **Tighe&Bond**

**APPENDIX H** 

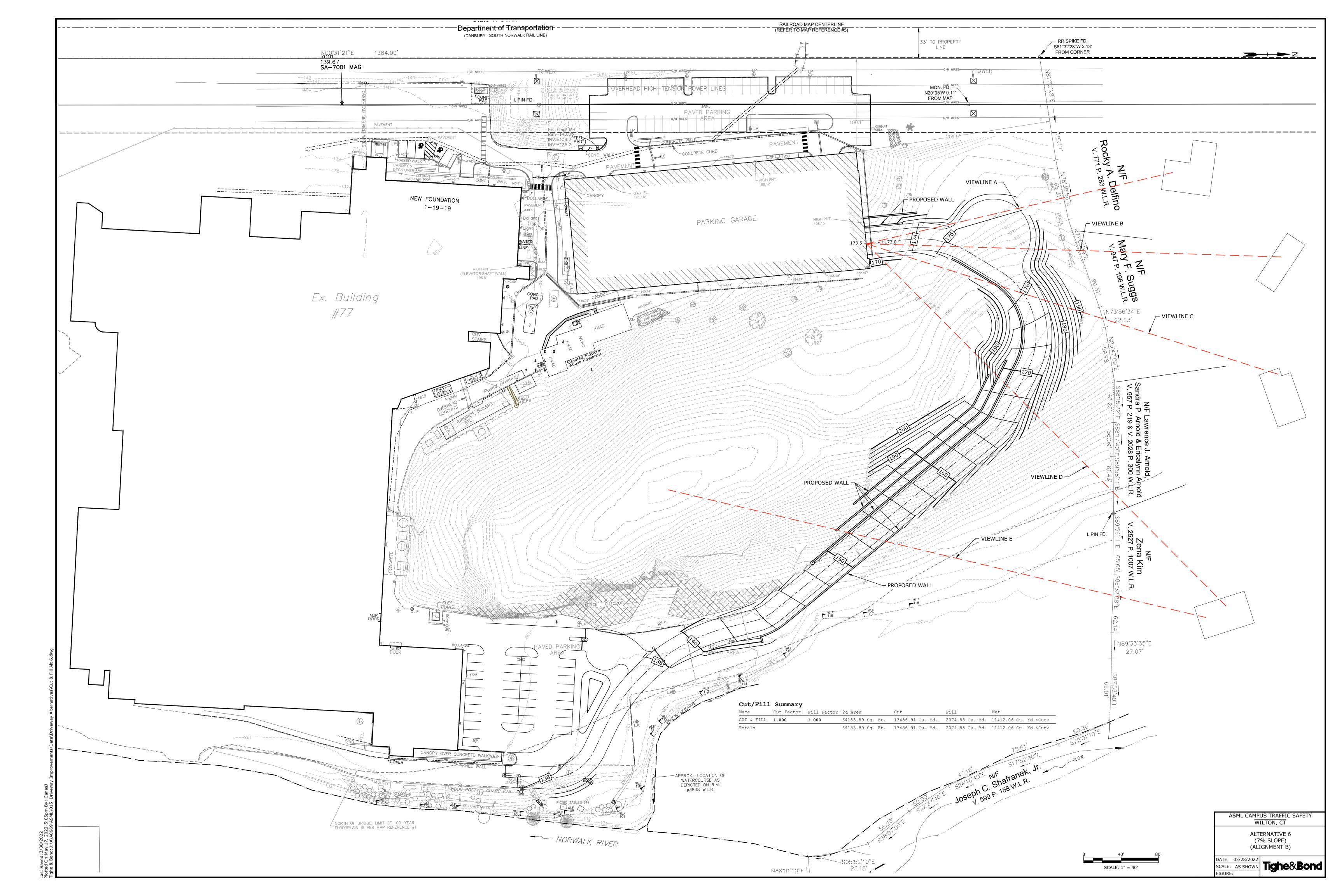


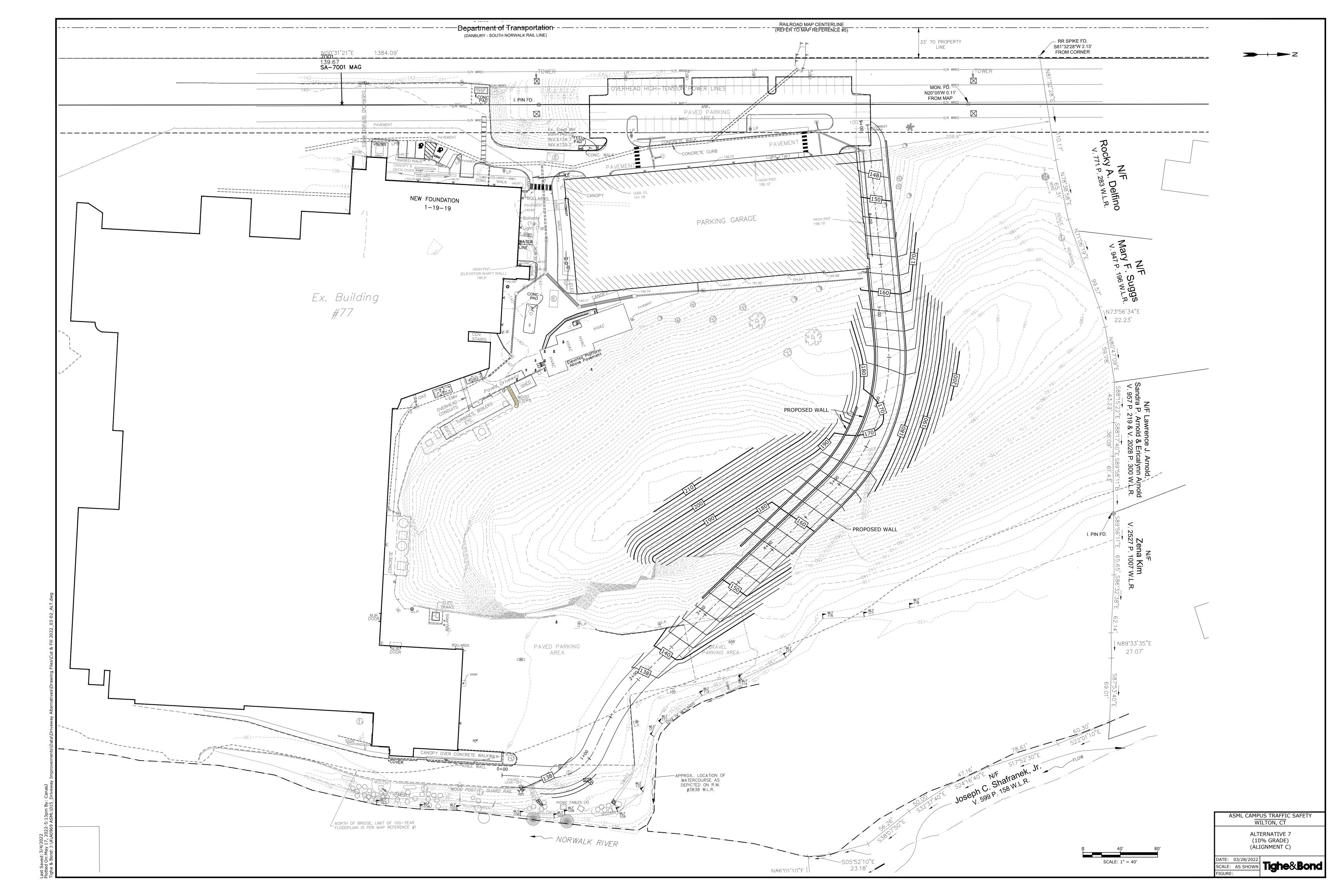












# **Tighe&Bond**

**APPENDIX I** 

#### SEDIMENT TRAP COMPUTATIONS ASML CAMPUS TRAFFIC SAFETY IMPROVEMENTS



Date: May 22, 2022

Prepared by J. Canas

Distu	rbance Summary
Area Disturbed	2.3 acres
Trap Required	308.2 cubic yards
nap keyuneu	8321.4 cubic feet

#### Proposed Stormwater Management Pond

	Cell	Area	Area	Area	Depth	Vol	Cum Vol
Elev	South	North	Total, sf	Avg, ft2	ft	ft3	ft3
133	221	147	368				0
				879	1	879	
134	797	593	1390				879
				2184	1	2184	
135			2978				3063

\* Too small, need to enlarge during construction

#### Proposed Sediment Trap

	Cell	Area	Area	Area	Depth	Vol	Cum Vol
Elev	South	North	Total, sf	Avg, ft2	ft	ft3	ft3
132			1774				0
				2046.5	1	2046.5	
133			2319				2046.5
				2721	1	2721	
134			3123				4767.5
				3576	1	3576	
135			4029				8343.5