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DRA	AWING INDEX	lssued For:	Planning & Zoning		
	Ι	<u>ш</u>	. 30, 2022		
<u>Dwg No.</u>	Title	DA	Sept. 30,		
T100	Title Sheet		Х		
Civil Engin Redniss & Mea	eer Drawings ad				
PSTS	Property & Topographic Survey		Х		
SE-1	Site Development Plan		Х		
SE-2	Sedimentation & Erosion Control Plan		Х		
SE-3	Details & Soil Data		Х		1
SE-4	Details		Х		
Landscape Granoff Archit	-				
L100	Landscape Plan		Х	<u> </u>	+
	ral Drawings				
AS100	Architectural Site Plan & Zoning Information		Х	 	+
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A300	Building Elevations (West & East)		X	 	+
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A302A	Exterior Renderings		X	 	+
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A304	Signage		X	 	+
A304 A400	Building Sections		X	 	+
L-1	Ground Floor Photometric Calculation		X	 	+
L-1 L-2	First & Second Floor Photometric Calculation		X	 	+
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DRA



GRANOFF ARCHITECTS

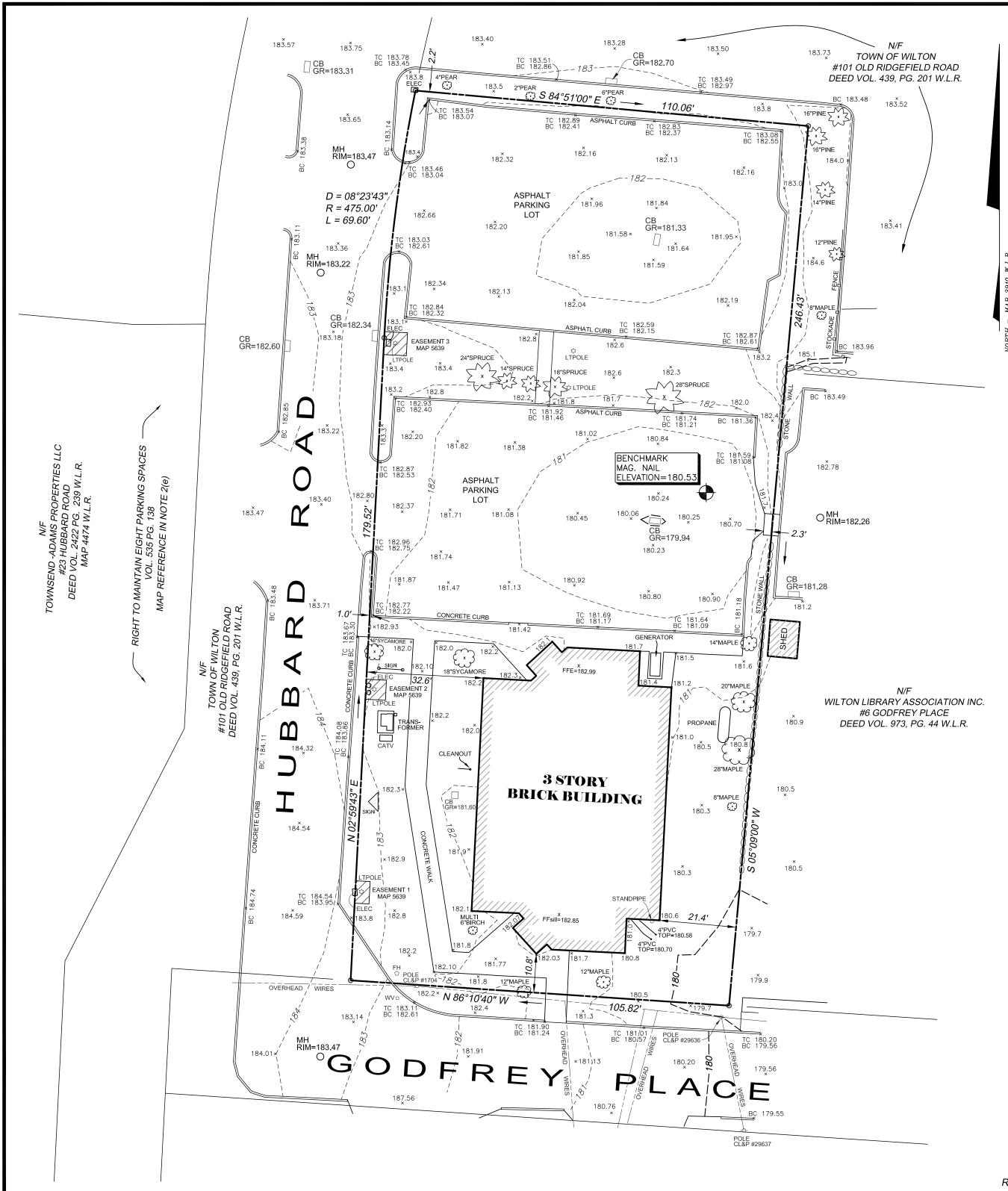
330 RAILROAD AVENUE GREENWICH, CT 06830 203.625.9460 WWW.GRANOFFARCHITECTS.COM

CONSULTANTS

CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: GRANOFF ARCHITECTS 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

REVI	SIONS			
#	DATE	REVISION	N DESCRIPTION	BY
1	09.30.2022	P&Z SUBM	IISSION	СС
	ZSUB		<u>ION</u> NSTRUCTI	ON
		STATICE PRACTICE	TA RECEIVE	
	JECT NAME: ILTON	CEN	TER LOFT	S
12 G	JECT ADDRE ODFREY PLA TON, CT 0689	CE		
JOB	NO.: 220	13		
DRA	WN BY: CC/	GC	PROJ. MANAGER:	RG
DAT	E: 09/	30/2022	SCALE: AS NOTE	D
DRA	WING TITLE			
CO	VER SH	EET		
DRA	WING NO.			
			00	



ZONING TABLE WC DISTRICT ____ (WILTON CENTER DISTRICT)

STANDARD	MIN.REQ./MAX.ALL.	EXISTING
BUILDING REQUIREMENTS		
MINIMUM LOT AREA	NONE	27,246 Sq. Ft.
MINIMUM LOT FRONTAGE	NONE	354.94'
FRONT YARD - MINIMUM	10'	
FRONT YARD - MAXIMUM	20'	10.8'
SIDE YARD - MINIMUM	0'	21.4'
SIDE YARD (abutting res. dist.)	75'	N/A
REAR YARD - MINIMUM	20'	150.2'
REAR YARD (abutting res. dist.)	75'	N/A
BUILDING COVERAGE - MAXIMUM	30% / 8,173 SF	3,990 SF / 14.6%
SITE COVERAGE - MAXIMUM	80% / 21,796 SF	17,405 SF / 63.9%
PARKING REQUIREMENTS		
FRONT YARD - MINIMUM	10'	1.0'
SIDE YARD - MINIMUM	0'	2.3'
SIDE YARD (abutting res. dist.)	60'	N/A
REAR YARD - MINIMUM	0'	2.2'
REAR YARD (abutting res. dist.)	60'	N/A
TOTAL SPACES		NON STRIPED

NOTES:

- 1. This survey has been prepared in accordance with Sections 20-300bthru 20-300b-20 of the Regulations of Connecticut State Agencies and the Standards for Surveys and Maps in the State of Connecticut as adopted by the Connecticut Association of Land Surveyors, Inc. as a Property and Topographic Survey the Boundary Determination Category of which is a Resurvey conforming to Horizontal Accuracy Class A-2 and the locations and elevations of which conform to Topographic Accuracy Class T-2. It is intended to depict property boundaries, locations and elevations of improvements and topographic features.
- 2. Reference is hereby made to the following on file with Wilton Land Records (W.L.R.):
 - a) Vol. 522, Pg. 98 Declaration of 12 Godfrey Place
 - b) Vol. 380, Pg. 52+54 ingress / egress, installation of utilities (Parcel A, Map 3910, Hubbard Rd.)
 - c) Vol. 2025, Pg. 142 Map 5639 Utility Easement
 - d) Map 3910
 - e) 'Map of Property prepared for D.A.W.N., Wilton, Connecticut ', dated Sept. 25, 1985, prepared by Ryan and Faulds. (depicted in deed of record Vol. 522, Pg. 143)
- 3. Elevations depicted hereon are based on North American Vertical Datum of 1988 (NAVD88).
- 4. Reference is hereby made instruments of record as labeled hereon.
- 5. Reference is made to Tax Map 73, Parcel 33.
- 6. Lot Area = 27,246 S.F. / 0.625 Acres
- 7. Reference is made to FEMA Flood Insurance Rate Map No. 09001C0383F, Effective Date 6/18/2010. Subject Parcel does not lie within a Special Flood Hazard Area.

PROPERTY & TOPOGRAPHIC SURVEY DEPICTING **#12 GODFREY PLACE**

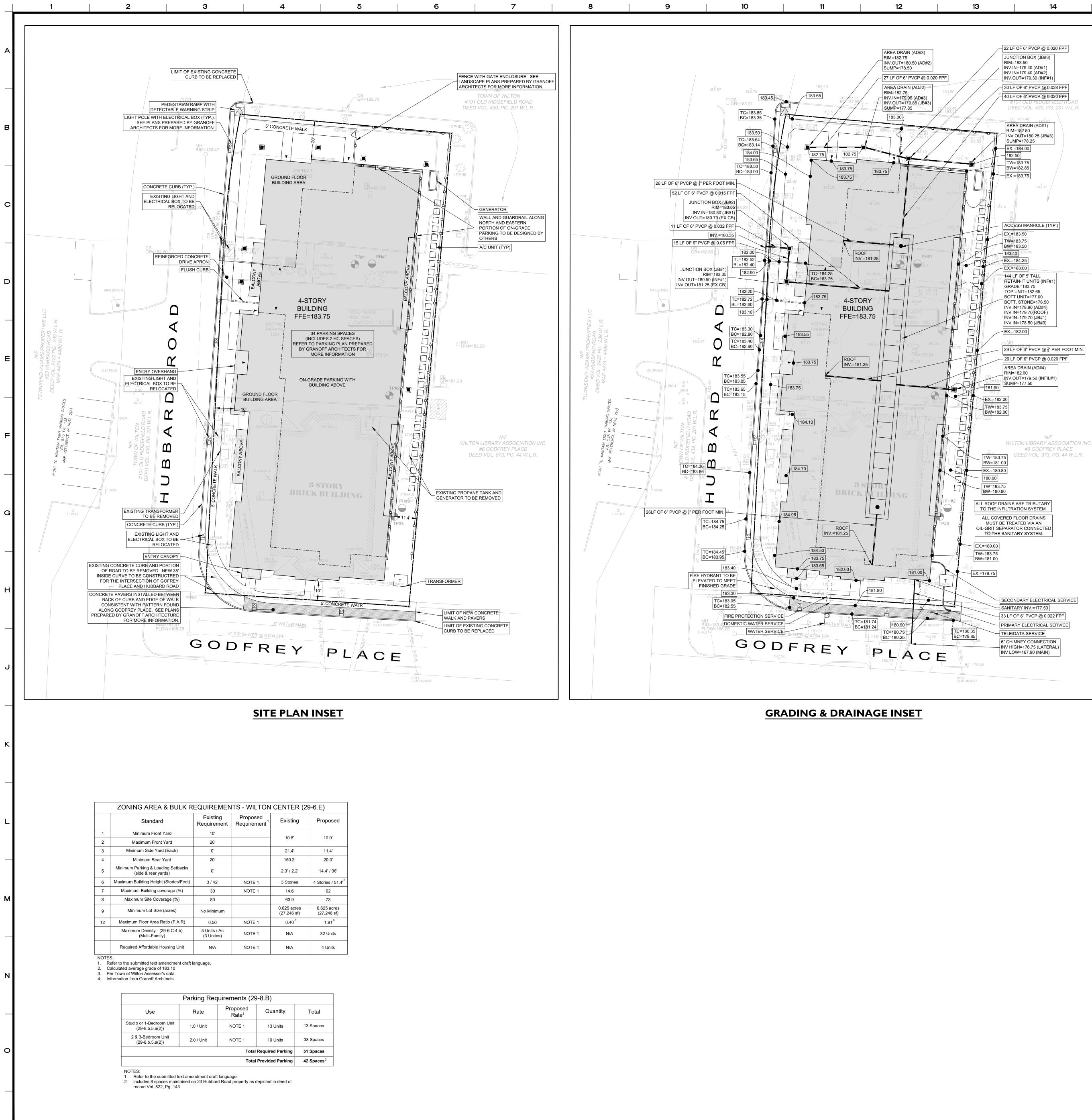
WILTON, CONNECTICUT

PREPARED FOR



	Scale: (1"=20')	40
	Drawn By: CJV	Checked By: LWP	Date: 04/2	2/2022
	To my knowle correct as note	dge and belief this map d here	o is substantially	
REDNISS		mmg 1	Josson	2
& MEAD	LAWRE	NCE W. POSSON, JR 6/9/20)
\sim		DATE		
LAND SURVEYING		ppies thereof are valid or designated licensed prof nereon null & void.		
Civil Engineering Planning & Zoning Consulting Permitting	ASSOCIATION AND AND AND AND AND AND AND AND AND AN	Sheet N		-0
22 First Street Stamford, CT 06905 Tel: 203.327.0500 Fax: 203.357.1118	E CAL		PST	3
www.rednissmead.com	WO SURY	Comm.	No.: 10556-1	1

Rev. 6/9/2022 - add utility easement



15 17 16 58. Existing fire valves shall be **GENERAL NOTES:** 59. The electric transformer These drawings are intended only to depict the design of site grading, drainage, sanitary, utilities and sediment & erosion controls. These drawings are for approval purposes only. No construction may begin 60. Detectable Tape shall be u prior to obtaining all necessary permits and approvals. 6-inches to 10-inches belo All survey data, boundary lines, topography, building locations and area calculations are from a survey prepared by Redniss & Mead, Inc. entitled Property & Topographic Survey dated April 22, 2022 and revised Telephone & Control lune 9, 2022. Elevations depicted or labeled are based on NAVD-88. Natural Gas Water Systems Refer to plans prepared by Granoff Architects for information and design of the proposed buildings. These Fire Protection Systems drawings depict site plans corresponding to the latest architectural plans received from Granoff Architects Mains received on August 30, 2022. IS & S Communication C Property lies in the Wilton Center District Zone. 61. Underground-Type Plastic All construction shall comply with the Town of Wilton requirements, the State of Connecticut Basic tape, continuous-printed Building Code Americans with Disabilities Act (ADA), the Connecticut Guidelines for Soil and Erosion and thick. Sediment Control, OSHA, and CT DOT Form 818 (latest edition). PAVEMENT AND PAVEMI All development activities to be undertaken within the street right-of-way and other public lands shall comply fully with Town standards unless approved deviation is specifically set forth as part of this 62. Areas of asphalt pavemen application. All work within the State right-of-way will comply with the CT DOT Form 818 with the latest accordance with the aspha special Provisions and Typical State Standard Details. existing grade and the edge Contractor shall supply complete shop drawings including manufacturer's product data sheets to the Site Engineer, for all construction material used in conjunction with these drawings. Contractor shall allow a 5 Existing features such as b day review period, prior to fabrication and installation. shall be repaired at no add Information on existing utilities has been compiled from various sources including utility company records, 64. Saw cut perimeter of area municipal record maps and field survey and is not guaranteed to be correct or complete. The contractor is solely responsible for determining actual locations and elevations of all utilities including underground 65. Contractor shall engage a services. and perform compaction the contractor the require P. The property is served by public water and sewer system. course prior to placement 10. Prior to any excavation the Contractor and/or Applicant, in accordance with Public Act 77-350, shall be required to contact "Call Before You Dig" at 1-800-922-4455 for mark-out of underground utilities. Dig The Contractor shall engag test pit(s) at utility crossing(s) to check actual clearances with new utilities prior to construction. If and to prepare test repor conflicts are found the contractor shall notify the engineer, at which time the sewer in question shall be whether tested work con redesigned. If such redesign is not possible, the existing pipes or utilities shall be relocated to avoid the conflict. Such relocation shall be done with knowledge of and in accordance with the owner of the utility. Additional testing, at Cont with specified requirement It shall be the responsibility of the contractor to provide any excavation safeguards, necessary barricades, measurements indicate th flagmen, etc., for traffic control and site safety. All work shall be done in accordance with OSHA Engineer. requirements. The contractor shall be responsible for compliance with OSHA requirements. 68. Contractor is responsible 12. When preparing the existing site for the proposed development, all materials removed shall be disposed of applicable Section of the O in conformance with all governing agencies. 69. Compaction shall be const 13. Remove stumps and brush from site, or chip and use during landscaping. Do not bury stumps on site. specification, the drawing as directed by the Site Er 14. Building elevations are subject to change and shall be finalized prior to building permit. 5. Special attention of the contractor is called to the required type and compaction of pipe bedding and After the asphalt pavemer backfill specified on these drawings. These requirements will be strictly enforced. the newly installed paven water truck shall spray a s 16. Prior to issuance of a Certificate of Occupancy, the Engineering Bureau may require a certification letter water. There shall be pos stating that the development was constructed in accordance to the approved plans, and an "as-built" significant water (greater drawing shall be submitted Contractor to repair prio base course prior to repla 17. The Contractor is responsible for coordinating with a licensed surveyor to prepare an "as-built" plan. The course and edges of sawc Contractor is responsible to coordinate with a site engineer 48 hours prior to any inspections. installed. The Owner's Re test so that he may be pre 8. The Engineering Department and the inspecting engineer shall be notified by the contractor three (3) days prior to the commencement of each phase of construction. The inspecting engineer a meeting. At this meeting, 19. The work shall be done in conformance with the contract documents/plans unless changes have been and approval of the subgra approved in writing by the design engineer prior to the work being done. determine if the work cor base course, contractor s 20. A preconstruction meeting shall be held with the Owner, Architect and Engineer to review the scope of material, base course and a construction. The Contractor shall be responsible to coordinate the preconstruction meeting. 72. Finished paving shall be fre **EARTHWORK & GRADING** 21. Grade away from building walls at 2% minimum (typical). 73. Finished grade shall be with 22. Earth slopes shall be no steeper than 2:1 (horz.:vert.) 74. The pavement shall be pro minimum period of 24 hou 23. General fill beyond paved areas shall be free of brush rubbish, stumps and stones larger than 8". Fill shall spills, hydraulic leaks, and be placed in compacted layers not to exceed 8" in thickness. The dry density after compaction shall not be Representative acceptance less than 95% of the Standard Proctor Test and done in accordance with the requirements of ASTM D698. re-striping as necessary to After compacting, the fill shall be 4" below the required grade as shown on the plan. Thicknesses of all layers shown are after compaction. Compact all layers to 95% per ASTM D 1557 24. General fill may be till, loam, sand or gravel mixture classified as SP, SW, SM, GP, GM, ML per the United (Modified Proctor Method). Soil Classification System. It shall have not more than 40% fines passing the #100 sieve, not more than 8% passing the #200 sieve, and no stones larger than 8". Subgrade and fill shall be uniformly compacted by the use of equipment manufactured for that purpose. edition of AASHTO Highway Design Manual. Rollers shall deliver a ground pressure of not less than 300 pounds per linear inch of contact width and weigh not less than 10 tons. Vibratory units shall have a static weight of not less than 4 tons. The amount of compactive effort shall be as directed by the Engineer, but in no case shall be less than 4 complete passes of the compacting equipment being used. 26. Disturbed areas shall be top soiled, seeded with grass and mulched in a manner conforming to the recommendations of the "Guidelines for Soil Erosion and Sediment Control", published by The Connecticut Council on Soil and Water Conservation, May 2002. 27. After the areas to be topsoiled have been brought to grade, the subgrade shall be loosened by scarifying to a depth of at least 2" to ensure bonding of the topsoil and subsoil. 28. Topsoil shall be friable and loamy with high organic content. It shall be free of debris, rocks larger than 2" and roots. Topsoil shall have at least 1.5 percent by weight of fine textured stable organic material and no greater than 6 percent. Topsoil shall not have less than 20% fine textured material (passing the No, 200 sieve) and not more than 15% clay. pH range shall be 6.0-7.5 and soluble salts shall not exceed 500ppm. 29. Fill or topsoil shall not be placed nor compacted while in a frozen or muddy condition or while subgrade is 30. Excavation for pipes or concrete pavement repair may require either a braced excavation or open cut designed according to the requirements of OSHA, 29 CFR Part 1926. The lateral support systems and slopes should also be designed such that building footings, slabs on grade, adjacent pavement and existing ut ilities are protected and supported and not allowed to settle. The contractor shall be responsible for having a Professional Engineer, registered in the State of Connecticut design the excavation support method. The designs shall be submitted to the owner or his geotechnical engineer for review. The contractor shall submit plans showing the type, limits, design and sequence of construction for the lateral support system. 31. During the excavation, it is anticipated that existing utilities and sewers may be exposed. The contractor shall provide protection and support of these facilities and repair any damage caused by the work in a manner satisfactory to the owner. The condition of the existing facilities shall be observed by the owner's representative who shall determine if the facilities shall be replaced. Replacement of the facilities shall be done in a manner satisfactory to the owner and in compliance with applicable Codes. STORM AND SANITARY SEWER SYSTEMS: 32. All pipe shall be installed straight and at the vertical and horizontal alignment shown. Pipes shall have a uniform slope as specified. 33. Minimum cover on all pipes shall be two feet (2') unless otherwise noted. All storm pipe specified as Poly Vinyl Chloride Pipe (PVCP) shall be SDR 35 with rubber gasketed joints and meet the requirements of ASTM D3034 and D3212. 35. All High Density Polyethylene Pipe (HDPE) for the stormwater system shall be ADS N-12 or equivalent with O-Ring joints (Pro-series) suitable for water tight installations. 36. All sanitary sewer pipe shall be Poly Vinyl Chloride Pipe (PVCP) and shall be Schedule 40 with solvent weld 37. Dig test pits at utility and sewer crossings to check actual clearances with these facilities prior to construction. Dig test pits at the connection points to existing sanitary sewer pipes to confirm that the elevation of the proposed gravity sewer is appropriate. If conflicts are found the contractor shall notify the engineer at which time the sewer in question shall be redesigned. If such redesign is not possible, the existing pipes or utilities shall be relocated to avoid conflict.

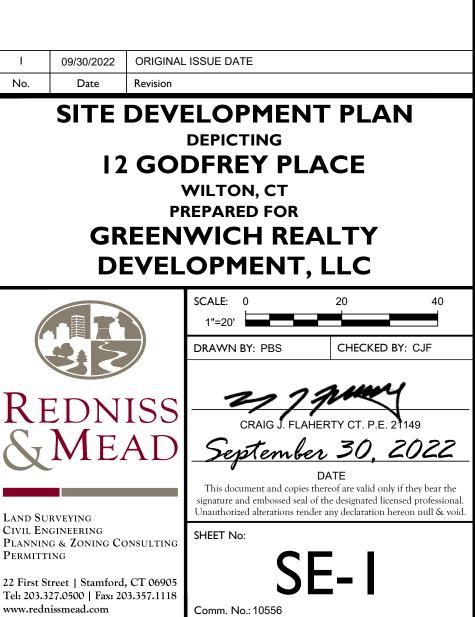
- 38. All area drains shall have a two foot (2') sump with bell traps or 90° PVC elbows.
- 39. All existing and proposed area drains, junction boxes and utility facilities shall be raised or lowered to be flush with finished grade.
- 40. Locate and abandon existing sanitary laterals at the property line with the end capped and mortared. Other existing utilities shall be abandoned in accordance with the requirements of the utility owner(s). 41. When connecting new pipes to existing structures such as manholes and catch basins, the structure shall be completely cleaned out. The hole made in the structure shall be made as small as possible. The structure shall be repaired to match its original type of construction. The joint between the structure and
- the pipe shall be made watertight by filling the joint with mortar. 42. Flow in existing sewer system must not be interrupted. Any temporary routing of this sewer flow must be done in conformance with all applicable rules and regulations.
- 43. Under no circumstances shall trench water be allowed to drain off through sanitary sewer lines.
- 44. All crushed stone shall be Gradation No. 4 as per CT DOT Form 818, Article M.01.02. Stone shall consist of sound, tough, durable particles free from soft, thin, elongated, laminated, friable, micaceous, or disintegrated pieces of mud, dirt or other deleterious material.
- 45. Sanitary Sewer Testing: The sanitary sewer line shall be Low Pressure Air Tested, at the expense of the contractor; Testing to be in accordance with recommended procedure in "Unibell's" "Recommended Practice for Low Pressure Air Testing of Installed Sewer Pipe" UNI B-6. The minimum starting pressure for the test is 3.5 P.S.I. (in excess of the groundwater pressure at the top of the pipe) and there shall be no more than 0.5 P.S.I. drop in five (5) minutes. Manholes to be visually inspected. Lateral plugs shall be airtight to allow proper testing. Inspecting Engineer and the Engineering Bureau shall be informed of testing schedule three days in advance so they can witness the testing.
- 46. At the end of construction, after the site has be fully stabilized, all new and previously existing storm sewer facilities including, but not limited to, catch basins, area drains, manholes, junction boxes, flow control structures, pipes, oil grit separators, permeable pavers and porous pavement shall be fully cleaned with equipment designed for that purpose to the satisfaction of the inspecting engineer. UTILITIES:

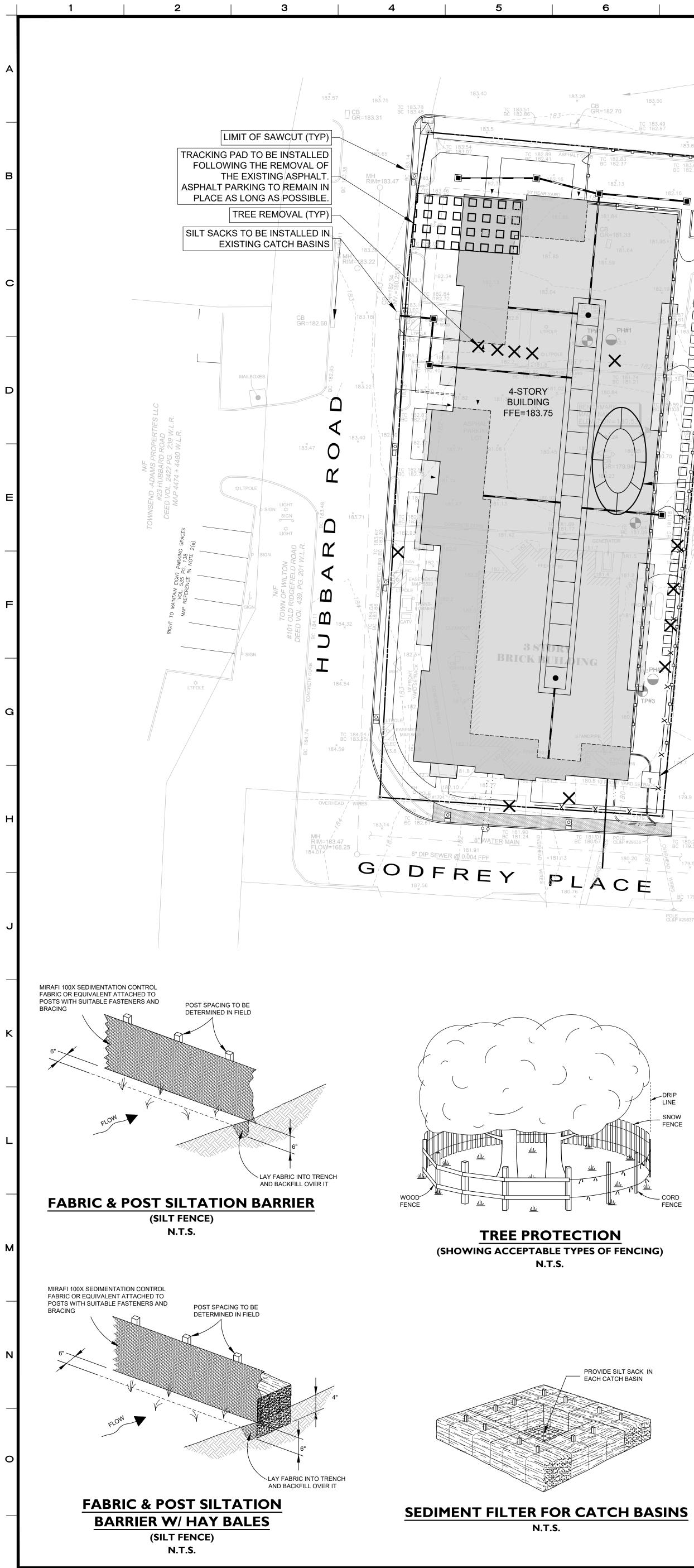
47. Utilities shown on these plans are "not guaranteed" to be complete or correct. Prior to any site activities, the contractor shall be responsible for verification of clearances of proposed utilities from existing utilities. This verification shall include physical observation by means of test pits of the locations of affected utilities. The contractor shall notify the site engineer immediately of any conflict.

- 48. Easements may be required in favor of the various utility companies.
- 49. Electric, telephone, cable, and water services shall be installed in conformance to the requirements of the governing utility companies.
- 50. It is the contractor's responsibility to install utilities as shown on this sheet. The contractor shall work with the utility companies and site engineer to insure the installation is in conformance to the requirements of the governing utility company. All conduits shall be concrete encased as may be required by the governing utility company. Proposed electric, telephone, cable and water services are shown for schematic purposes only and are subject to change pending utility company review. These utilities shall be designed by others and installed in conformance to the requirements of the governing utility companies.
- 51. All proposed utility facilities shall be raised or lowered to be flush with finished grade.
- 52. Where necessary, existing utilities shall be reinstalled to meet all minimum coverage requirements. 53. Utility connections at building face shall be coordinated with the building contractors.
- 54. The contractor must supply and install drag lines with all conduits.
- 55. Assume one 2" PVCP conduit for all site lighting. Service location to be determined.
- 56. In general, each utility shall have a minimum clearance of three feet to any other underground utility.
- 57. Any and all utilities abandoned shall be capped or removed in accordance with utility companies' requirements.
- Planning & Zoning Consult PERMITTING
- 22 First Street | Stamford, CT 06905 Tel: 203.327.0500 | Fax: 203.357.1118 www.rednissmead.com
- - LAND SURVEYING **CIVIL ENGINEERING**

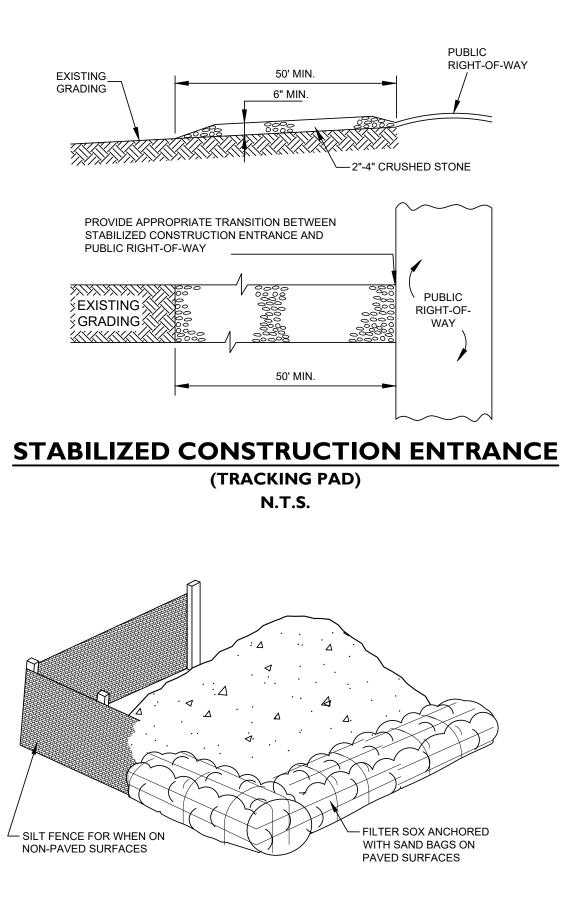
	19		20	
-		•	ion Water Company requirements. Ilicable Zoning setbacks.	
			cation tape shall be buried at least the buried utility piping or service.	
Conduit ic Line Marker: Ma	Red Orange Yellow Blue Blue Green Orange anufacturer's stan	Caution T Caution G Caution W Caution Fi Caution S Caution S Conc. N/A	lectric Line Buried Below Gelephone Line Buried Below Gas Line Buried Below Vater Line Buried Below Frinkler Line Buried Below Sewer Ewer Line Buried Below A Anent, bright-colored detectable	
l plastic tape, inten	ided for direct-bu	rial service;	; not less than 6" wide X 4 mils	
ENT MARKING	iS:			
halt pavement rep	air détail. The fin	ished grade	is project shall be replaced in e of asphalt paving shall blend to o slopes exceeding 4%.	
but not limited to dditional cost to th		l pavement	damaged by construction activities	
ea to be excavated	l. Saw cut shall be	straight an	d vertical.	
n testing of the bas	se and each course preconstruction r	e of paveme	naterial by means of a sieve analysis ent. Site Engineer shall review with e Engineer shall approve base	
	y will conduct and	d interpret	perform field inspections and tests tests and state in each report ments.	
ents. Remove and	replace or install a	additional h	mine compliance of corrected work ot-mix asphalt where test results or lents as directed by the Site	
e to place the hot CT DOT FORM			in the drawings, details and the	
			18 (latest edition), Section 4.06 action of each course of pavement	
ment, it shall be wa a sufficient amount sitive drainage on r than or equal to or to final accepta lacement with asp cut asphalt must b	ater tested for low of water on all pa- all areas of the pa- 3/16" in depth) is nce. These areas shalt mixture as pe- be treated with tak- inspecting A/E sha	w spots, are avement sea avement. A left standin must be sa er the origir ck oil prior	to f a water truck without marking eas of little or no drainage, etc. A ctions to observe the drainage of any visible low spots where g, shall be clearly marked for the wcut and removed down to the nal approved design. The base to new section of asphalt being ed 48 hours in advance of water	
g, samples to be te rade, base course omplies or deviate shall contact inspe	ested and compact and asphalt layers s from the specific ecting engineer to	tion testing s prior to th ed requiren determine	nents at the preconstruction protocol will be discussed. Testing he installation of the next layer to nents. Prior to installation of the the suitability of the subgrade e may be required.	
ree of ``bird baths	and be smooth a	at the slope	es specified on the plans.	
vithin 1/2 inch of th	nat noted on the o	drawings.		
ours after final rol d any other constr	ling. Maintain and ruction damage fo responsible for cl	f protect as r the remai learing, repa	the use of barricades, etc. for a phalt surface from scrapes, sears, inder of construction until Owner's airing, seal coating, patching, and val/acceptance.	
shown are after c	ompaction. Com	pact all laye	ers to 95% per ASTM D 1557	

76. All pavement striping and replacement shall conform to the Town of Wilton standards and the latest

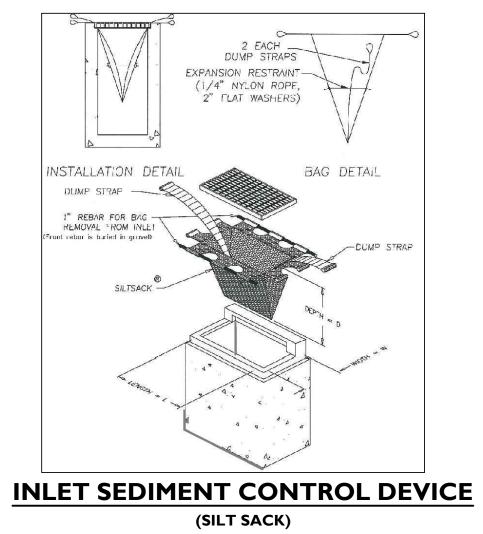




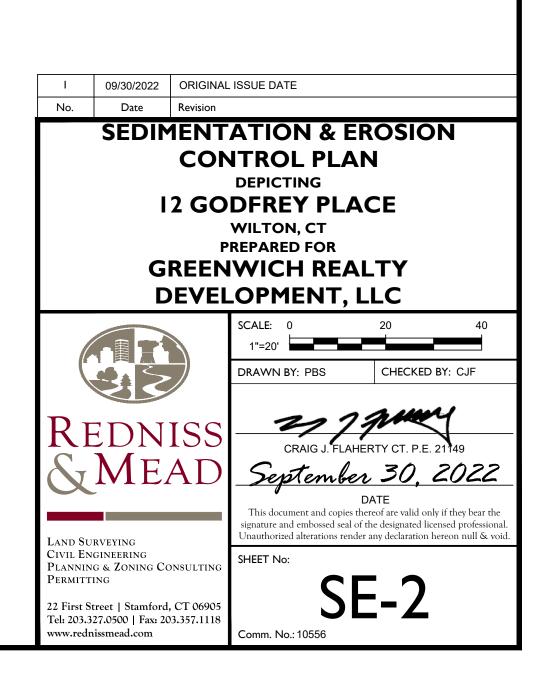
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AC Figure 1 Figure 2 F

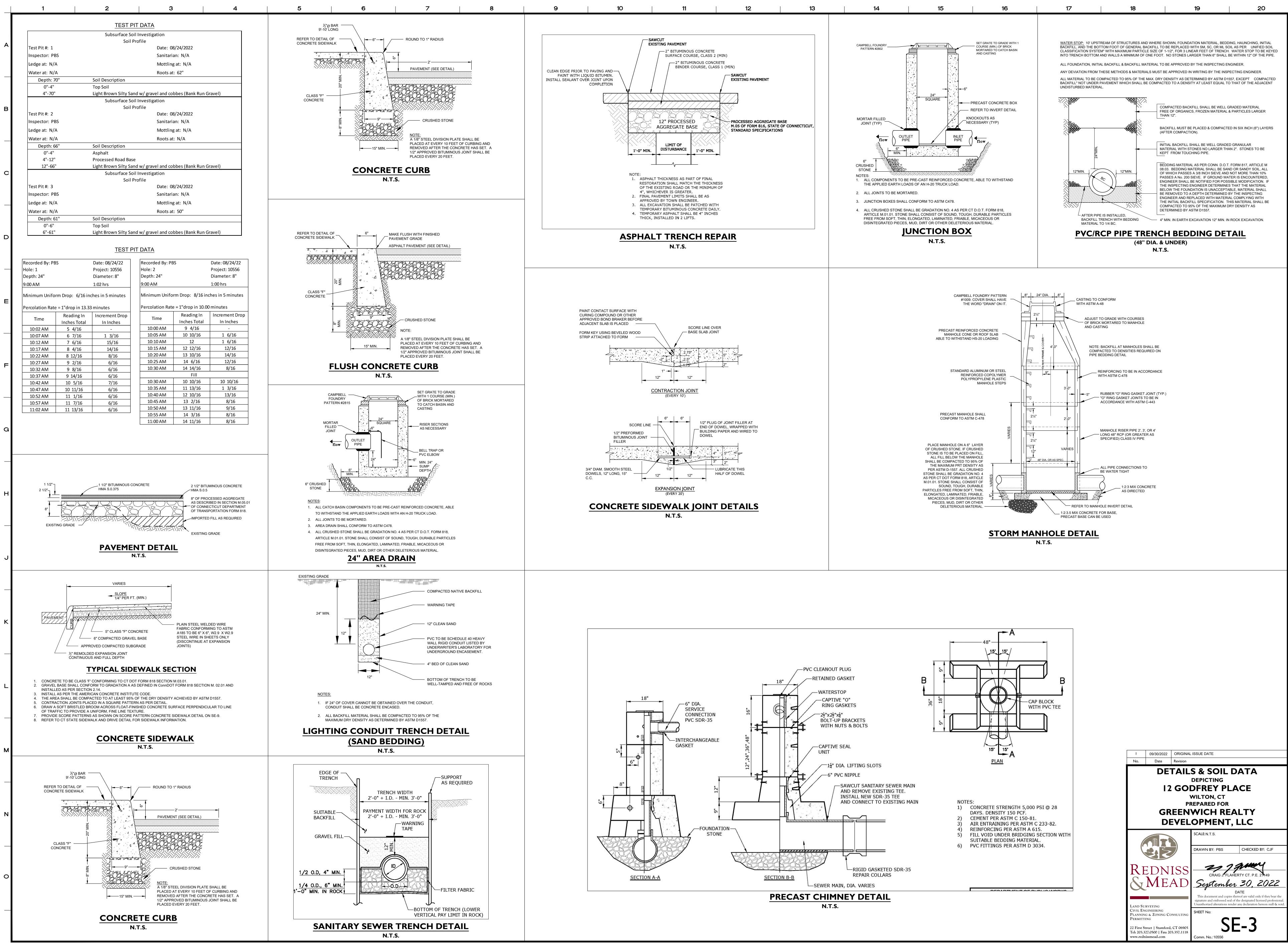


SEDIMENT FILTER FOR STOCK PILE N.T.S.

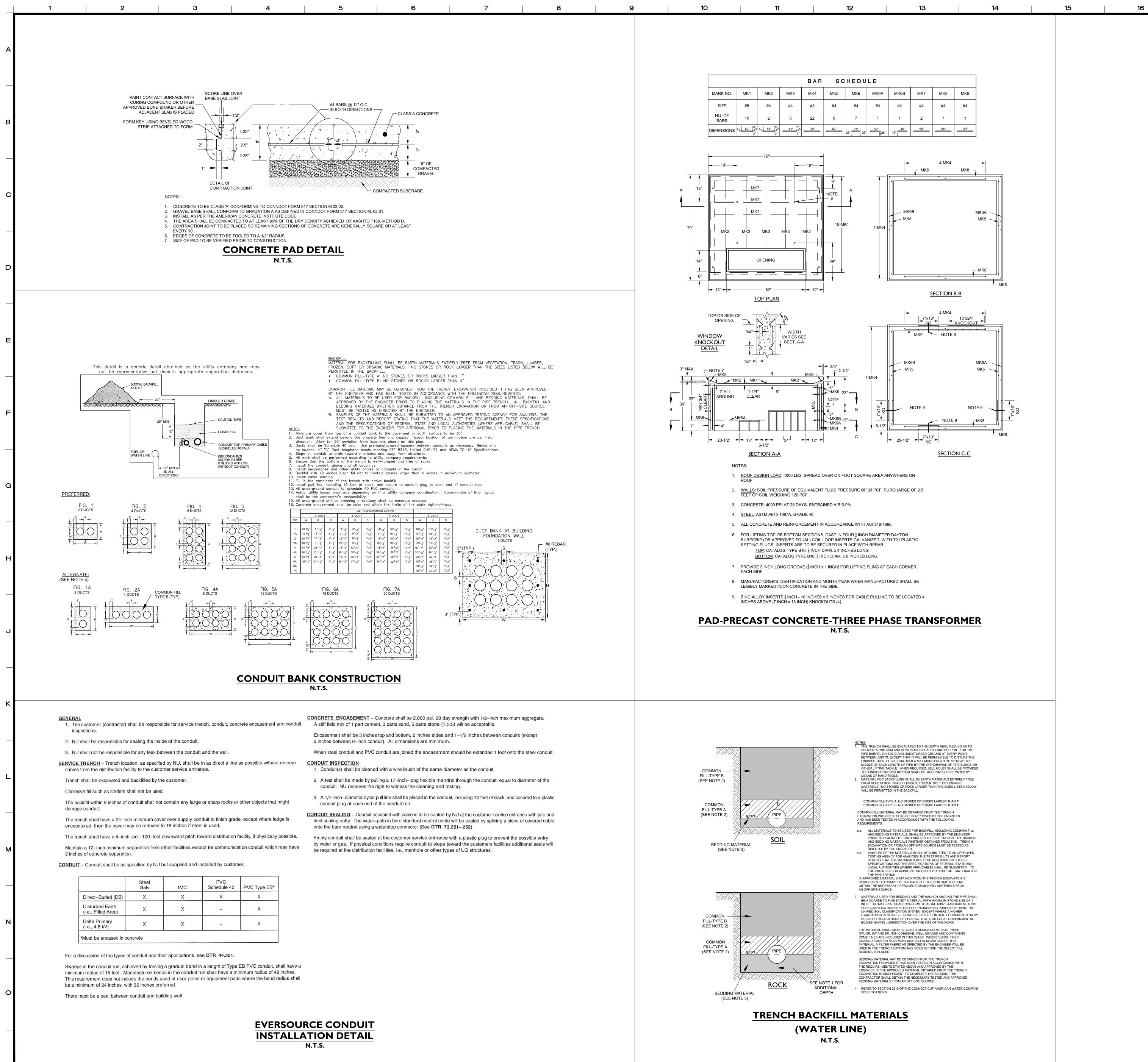


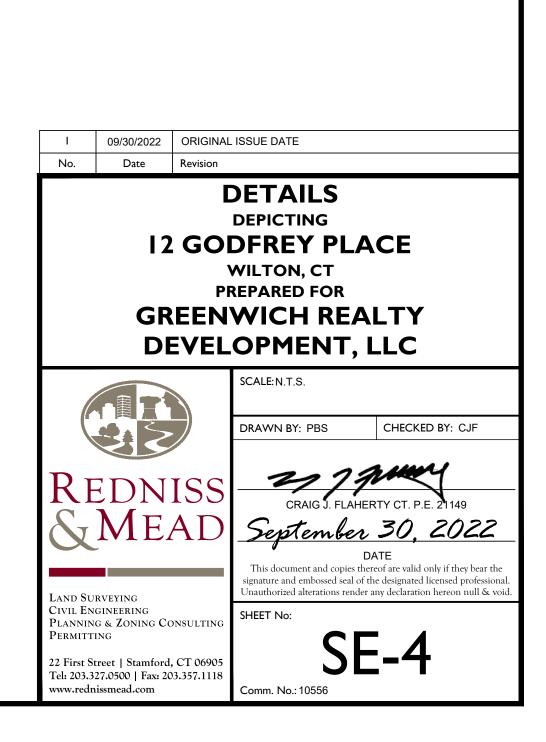
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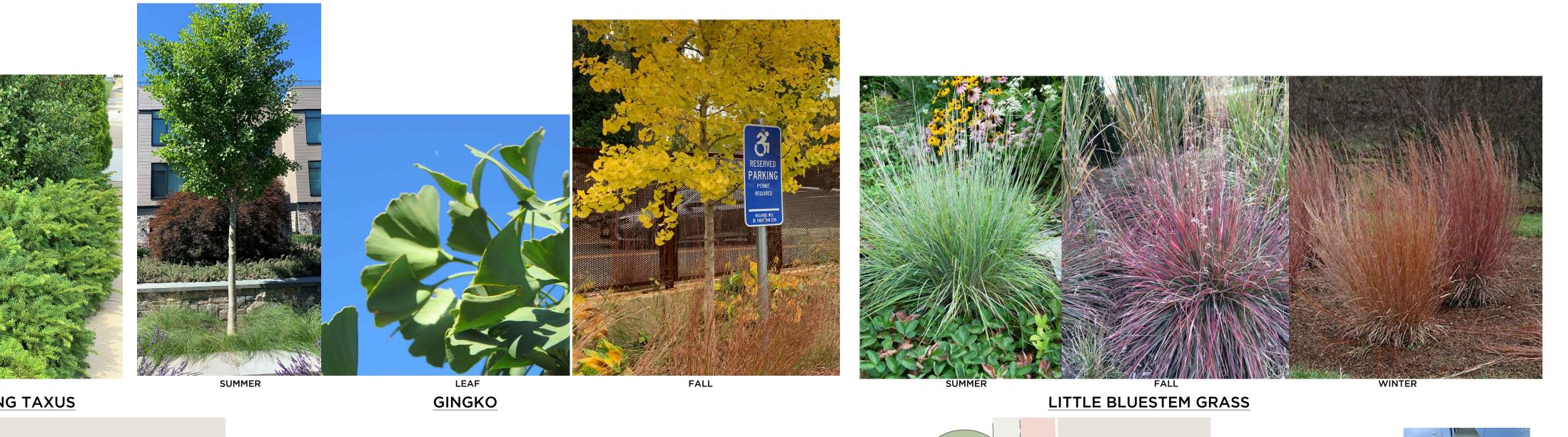


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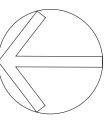
GRANOFF ARCHITECTS

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CONSULTANTS

CIVIL ENGINEER: REDNISS & MEAD 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

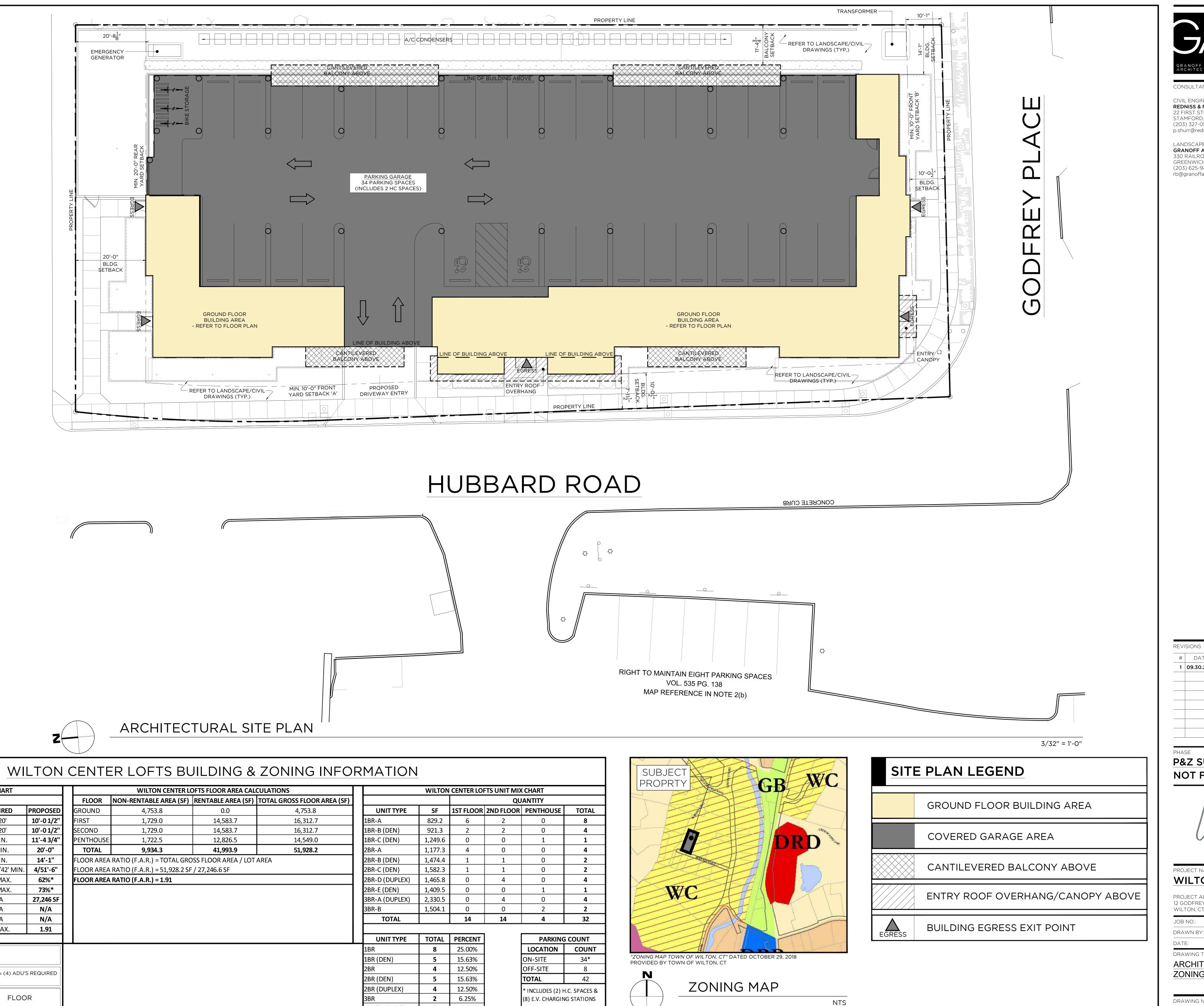
LANDSCAPE ARCHITECT: GRANOFF ARCHITECTS 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

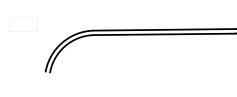


North

1 09.27.22 REVISED GENERATOR, TRANSFORMER PHASE P&Z SUBMISSION NOT FOR CONSTRUCTION PROJECT NAME: WILTON CENTER LOFTS PROJECT ADDRESS: 12 GODFREY PLACE WILTON, CT 06897 JOB NO.: 22013 DRAWN BY: RB PROJ. MANAGER: RG DATE: **09.09.22** SCALE: 1" = 10' DRAWING TITLE LANDSCAPE PLAN DRAWING NO. **L100** © 2022 GRANOFF ARCHITECTS

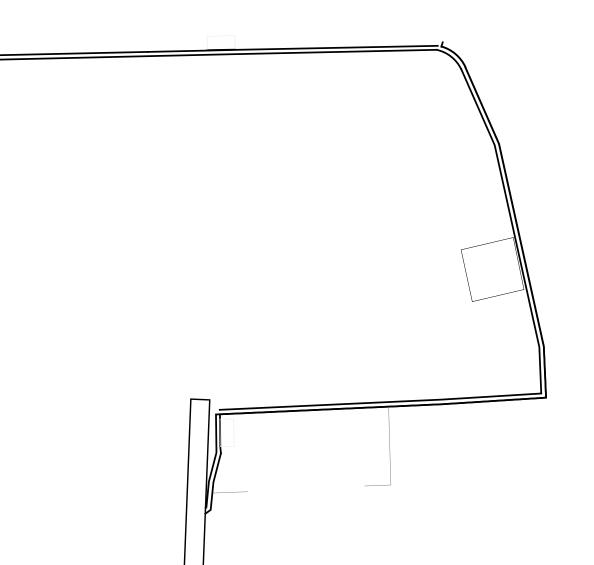
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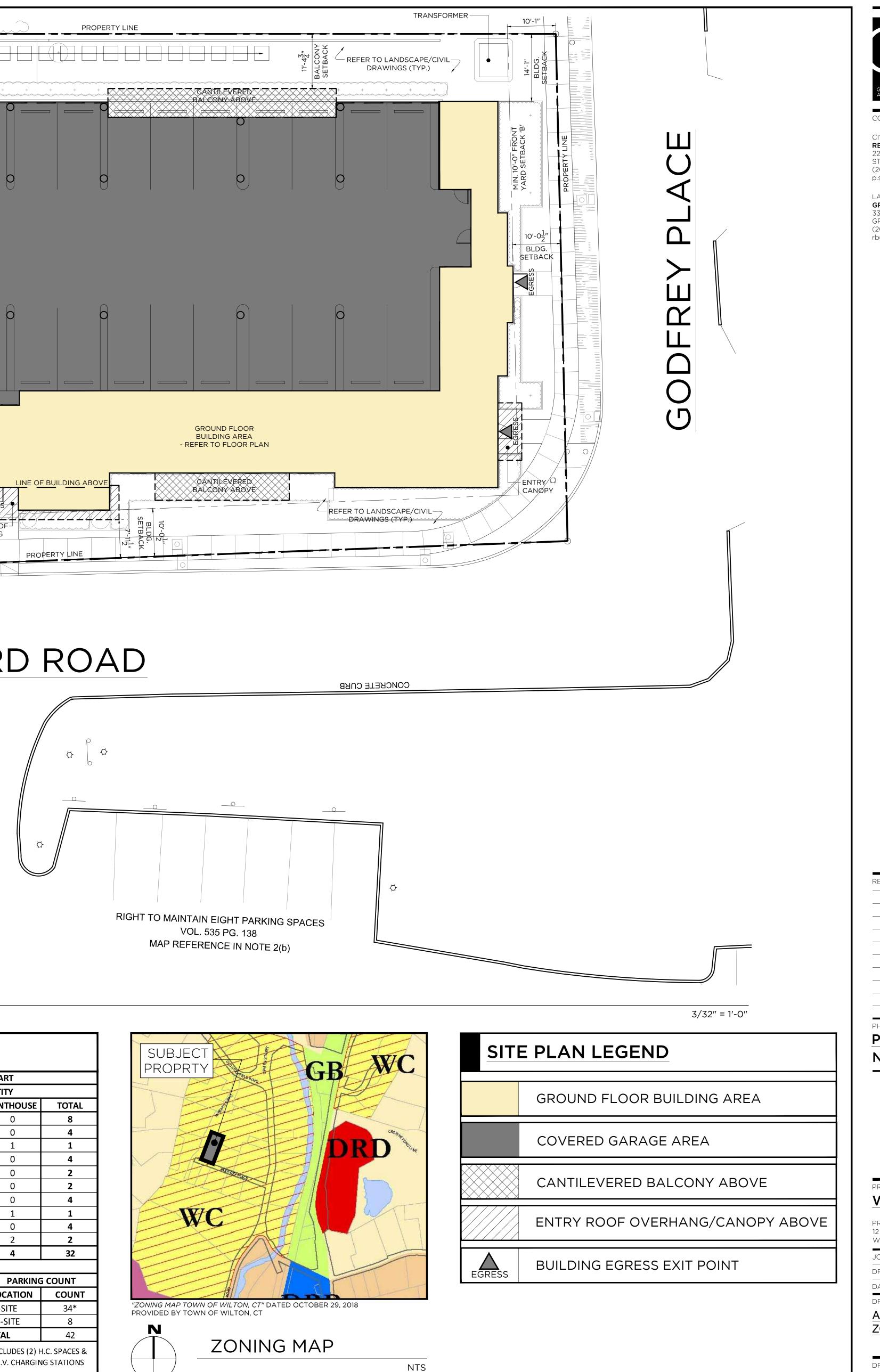




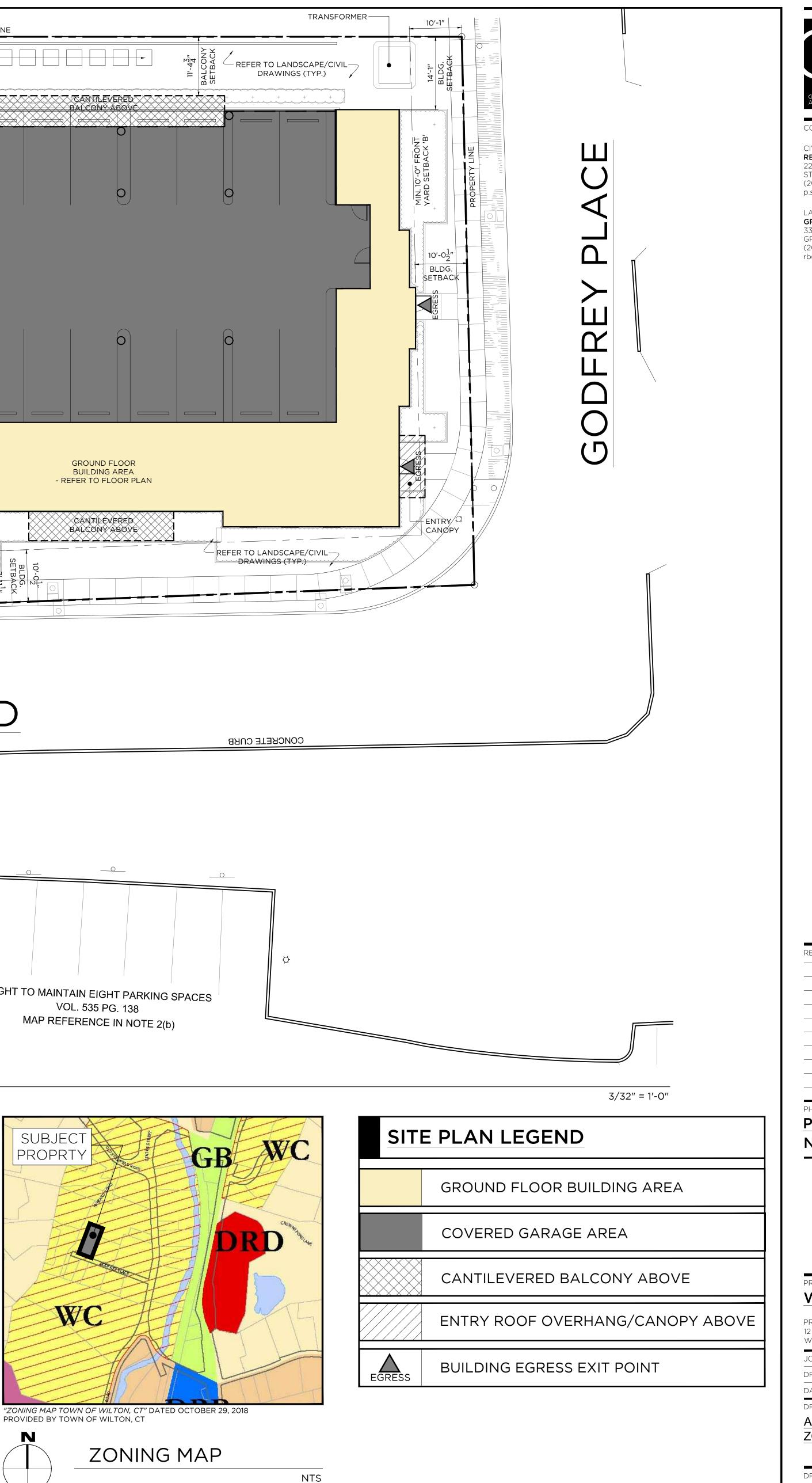


	WILTON CENTER LOFTS	ZONING CHART			WILTON CENTER LO	OFTS FLOOR A
ZONING D	ISTRICT: WC WILTON CENTER			FLOOR	NON-RENTABLE AREA (SF)	RENTABLE A
	ITEM	REQUIRED	PROPOSED	GROUND	4,753.8	0.0
FRONT YA	RD SETBACK 'A' (MIN./MAX.)	10' /20'	10'-0 1/2"	FIRST	1,729.0	14,583
FRONT YA	RD SETBACK 'B' (MIN./MAX.)	10' /20'	10'-0 1/2"	SECOND	1,729.0	14,583
SIDE YARD	SETBACK	0' MIN.	11'-4 3/4"	PENTHOUSE	1,722.5	12,820
	D SETBACK	20' MIN.	20'-0"	TOTAL	9,934.3	41,993
PARKING/	LOADING SETBACK	0' MIN.	14'-1"	FLOOR AREA	RATIO (F.A.R.) = TOTAL GRO	SS FLOOR AR
BUILDING	HEIGHT (STORIES/FEET)	3 STORIES/42' MIN.	4/51'-6"	FLOOR AREA	RATIO (F.A.R.) = 51,928.2 SF	² / 27,246.6 SF
BUILDING	COVERAGE (%)	30% MAX.	62 %*	FLOOR AREA	RATIO (F.A.R.) = 1.91	
SITE COVE	RAGE (%)	80% MAX.	73%*			
LOT SIZE		N/A	27,246 SF			
LOT FRON	TAGE	N/A	N/A			
LOT WIDTH	4	N/A	N/A			
FLOOR AR	EA RATION (F.A.R.)	0.5 MAX.	1.91			
* REFER TO) CIVIL DRAWINGS					
	PROPOSED AFFC DWELLING UNIT					
	I 10% ADU'S REQUIRED: (32) UNITS S PROPOSED: SEE BELOW FOR AD		S REQUIRED			
UNIT #	UNIT TYPE	FLOC)R			
103	<u>IBR-A</u> - ONE BEDROOM, ONE BATH	FIRST FLOOR				
104	2 <u>BR-B (DEN)</u> - TWO BEDROOM, TWO BATH, W,	DEN FIRST FLOOR				
205	1BR-A - ONE BEDROOM, ONE BATH	SECOND FLOO	DR			
301	<u>3BR-B</u> - THREE BEDROOM, TWO BATH	PENTHOUSE F	LOOR			





	LATIONS		WILTON	CENTER LO	FTS UNIT MIX	(CHART	
;) T(OTAL GROSS FLOOR AREA (SF)		QUANTITY				
	4,753.8	UNIT TYPE	SF	1ST FLOOR	2ND FLOOR	PENTHOUSE	TOTAL
	16,312.7	1BR-A	829.2	6	2	0	8
	16,312.7	1BR-B (DEN)	921.3	2	2	0	4
	14,549.0	1BR-C (DEN)	1,249.6	0	0	1	1
	51,928.2	2BR-A	1,177.3	4	0	0	4
TAF	REA	2BR-B (DEN)	1,474.4	1	1	0	2
		2BR-C (DEN)	1,582.3	1	1	0	2
		2BR-D (DUPLEX)	1,465.8	0	4	0	4
		2BR-E (DEN)	1,409.5	0	0	1	1
		3BR-A (DUPLEX)	2,330.5	0	4	0	4
		3BR-B	1,504.1	0	0	2	2
		TOTAL		14	14	4	32
		UNIT TYPE	TOTAL	PERCENT		PARKING	COUNT
		1BR	8	25.00%		LOCATION	COUNT
		1BR (DEN)	5	15.63%		ON-SITE	34*
		2BR	4	12.50%		OFF-SITE	8
		2BR (DEN)	5	15.63%		TOTAL	42
		2BR (DUPLEX)	4	12.50%		* INCLUDES (2) H	.C. SPACES &
				C 250/		. ,	
		3BR	2	6.25%		(8) E.V. CHARGIN	GSTATIONS
		3BR 3BR (DUPLEX)	2 4	6.25% 12.50%		(8) E.V. CHARGIN	



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CONSULTANTS

CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: GRANOFF ARCHITECTS 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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148 OLD RIDGEFIELD ROAD, WILTON CT



■ THE IVY AT WILTON CENTER - 3 HUBBARD ROAD WILTON, CT



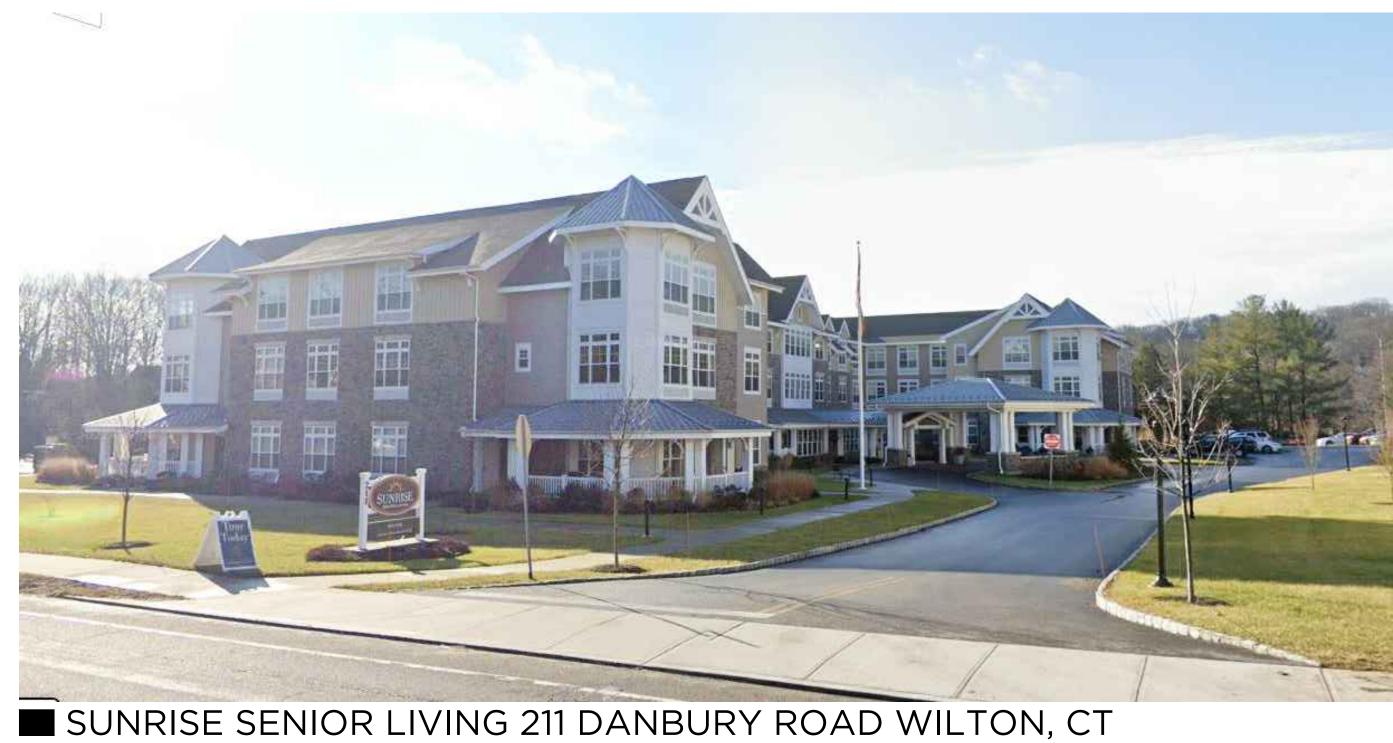




23 HUBBARD ROAD WILTON, CT



195 DANBURY ROAD, WILTON CT (OFFICE)







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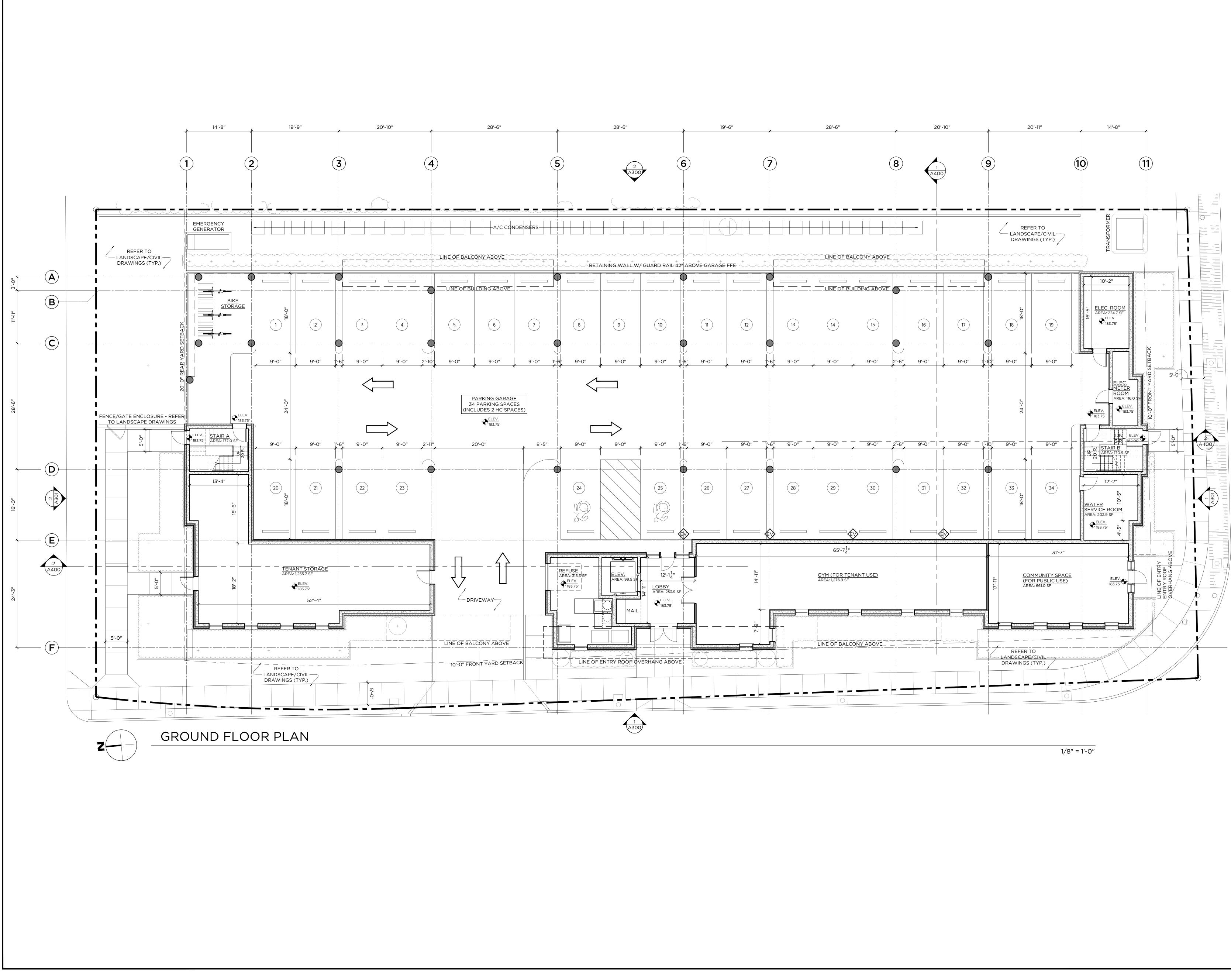
330 RAILROAD AVENUE GREENWICH, CT 06830 203.625.9460 WWW.GRANOFFARCHITECTS.COM

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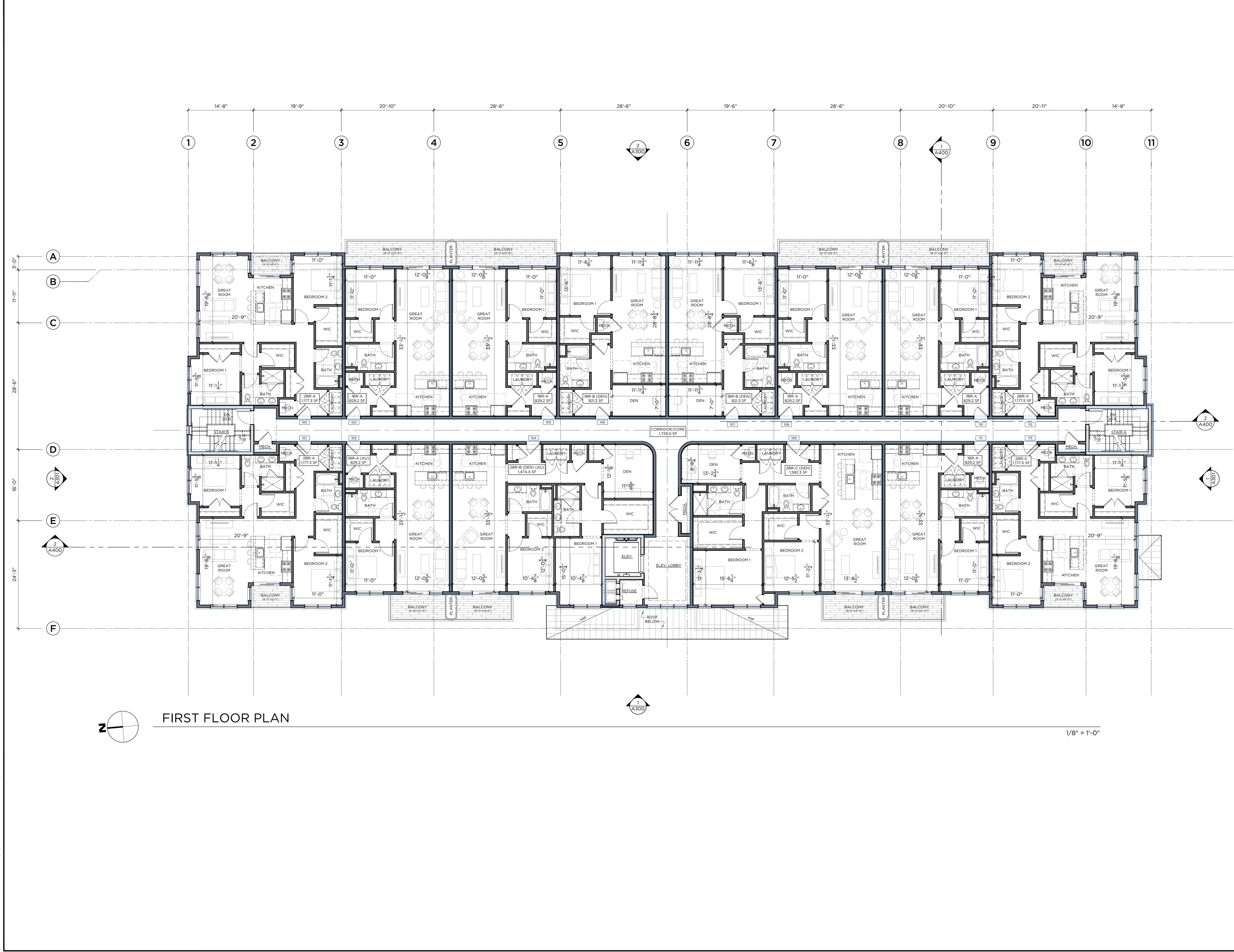
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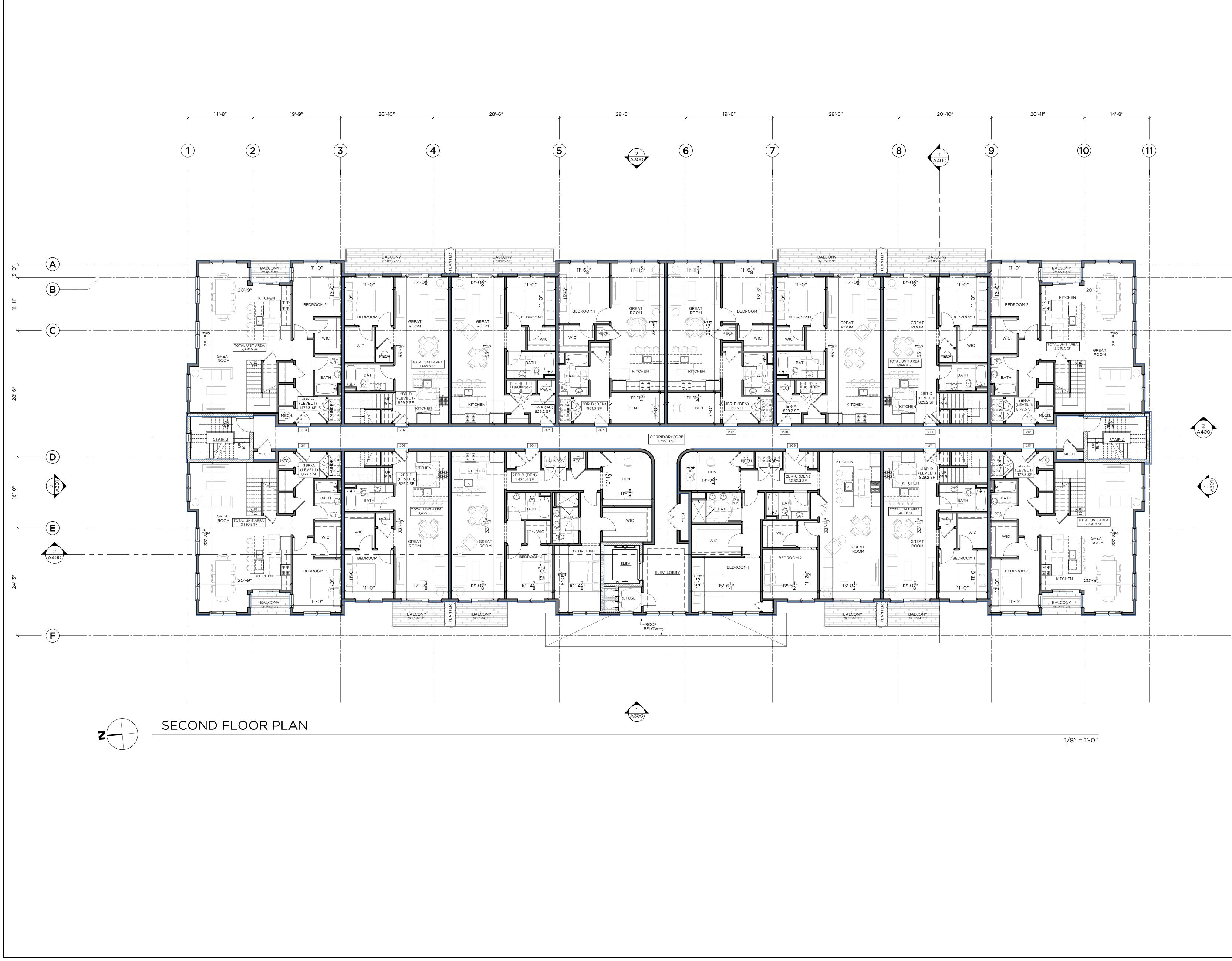
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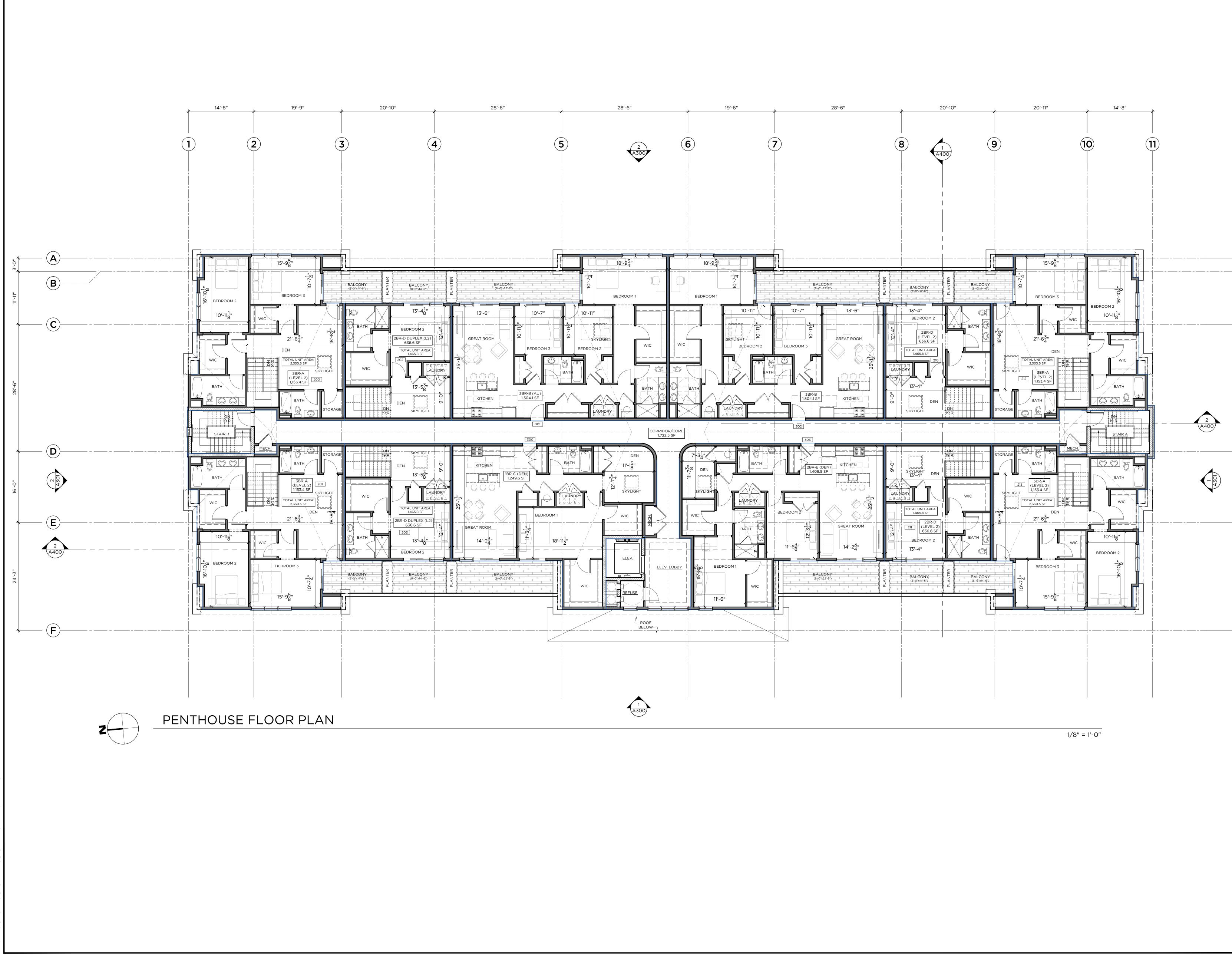
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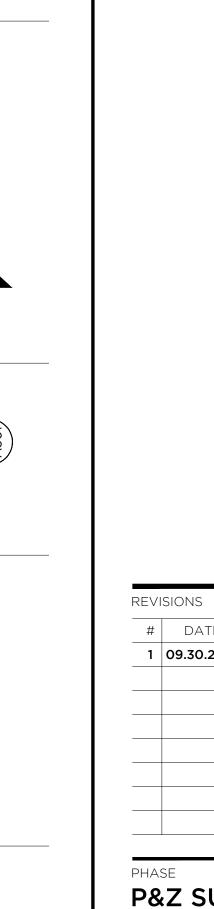
CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

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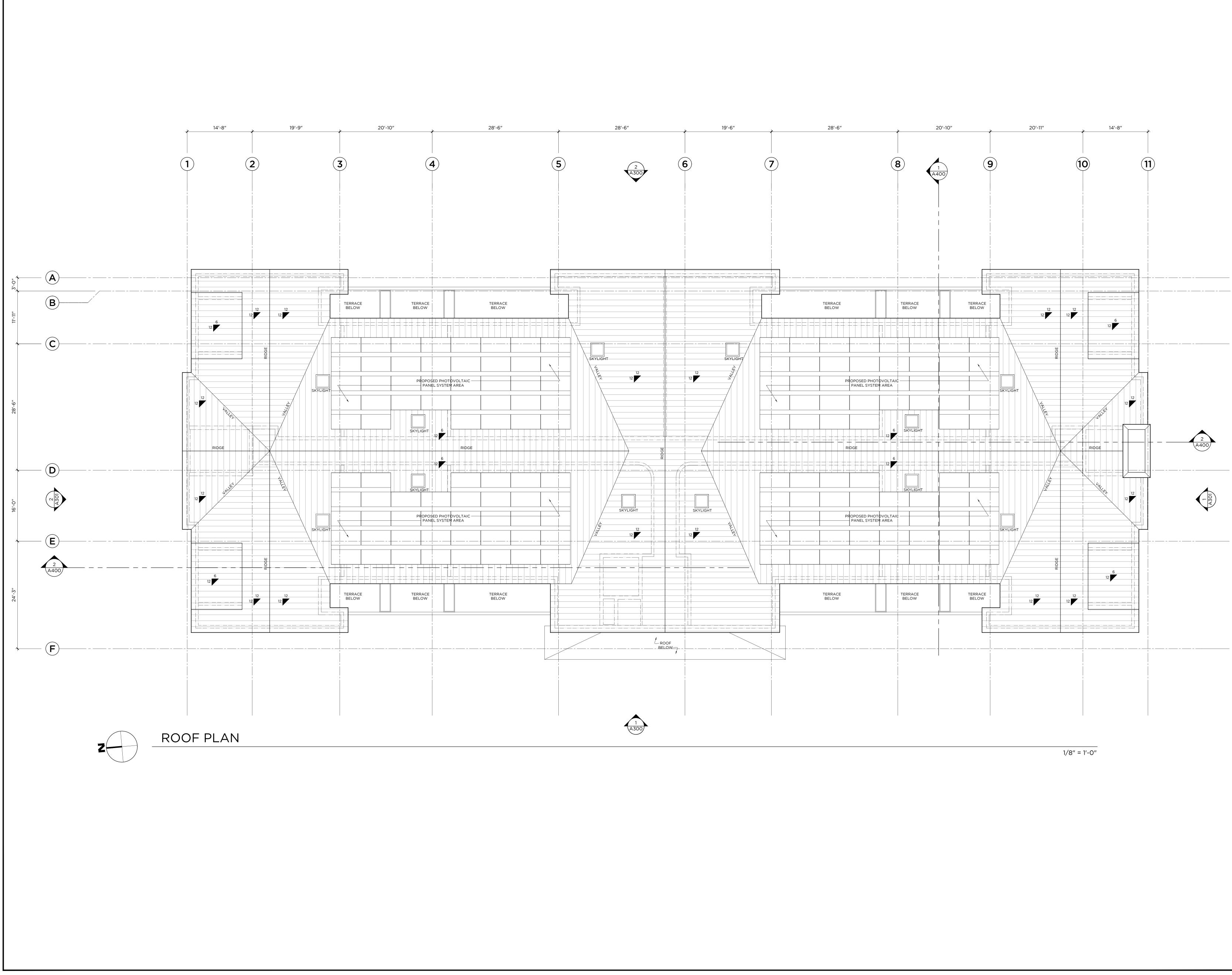
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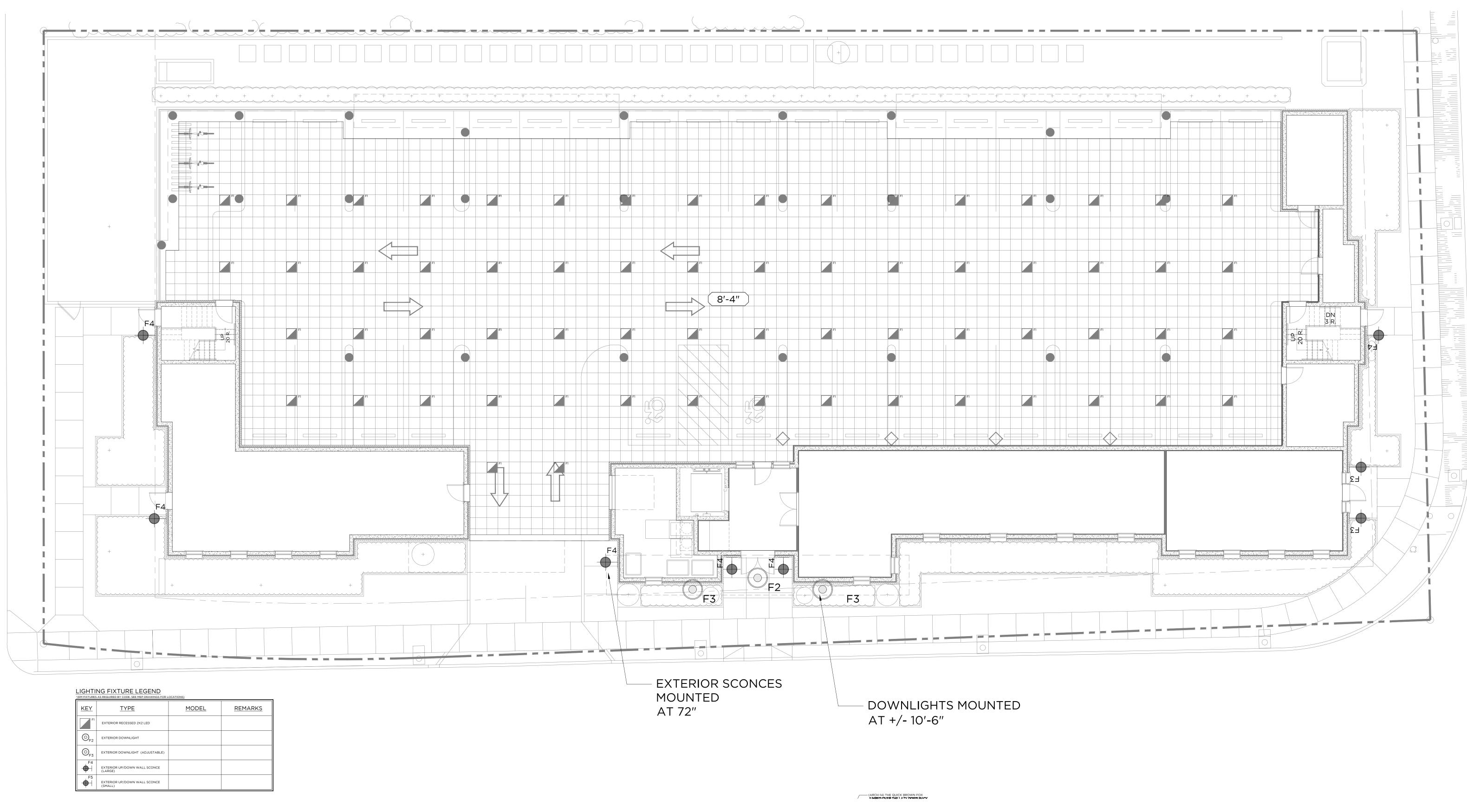
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GROUND FLOOR EXTERIOR LIGHTING PLAN _____ GARAGE



1/8" = 1'-0"



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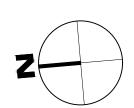
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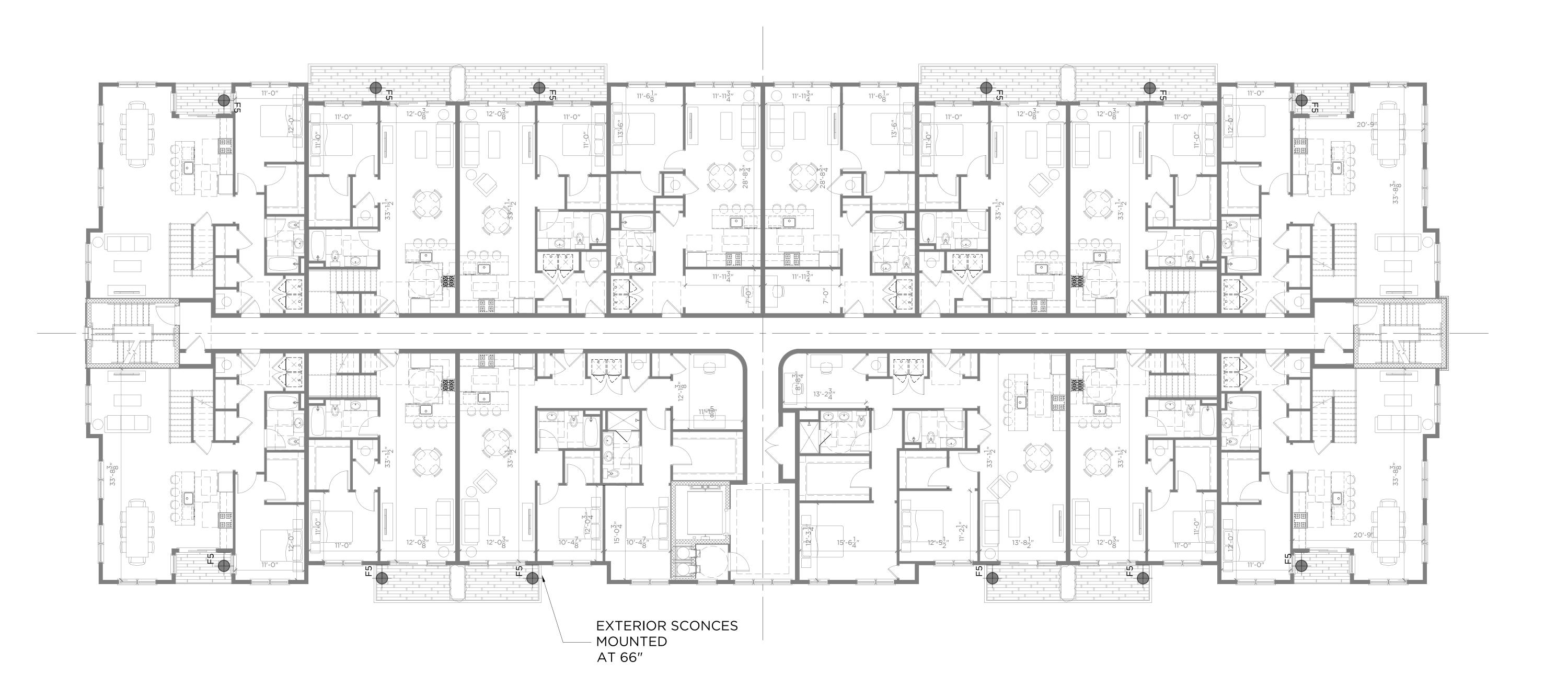




FIRST FLOOR EXTERIOR LIGHTING PLAN _____

<u>KEY</u>	TYPE	MODEL	<u>REMARKS</u>
F1	EXTERIOR RECESSED 2X2 LED		
() F2	EXTERIOR DOWNLIGHT		
⊚ _{F3}	EXTERIOR DOWNLIGHT (ADJUSTABLE)		
₽F4	EXTERIOR UP/DOWN WALL SCONCE (LARGE)		
₽ ^{F5}	EXTERIOR UP/DOWN WALL SCONCE (SMALL)		

LIGHTING FIXTURE LEGEND





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1/8" = 1'-0"



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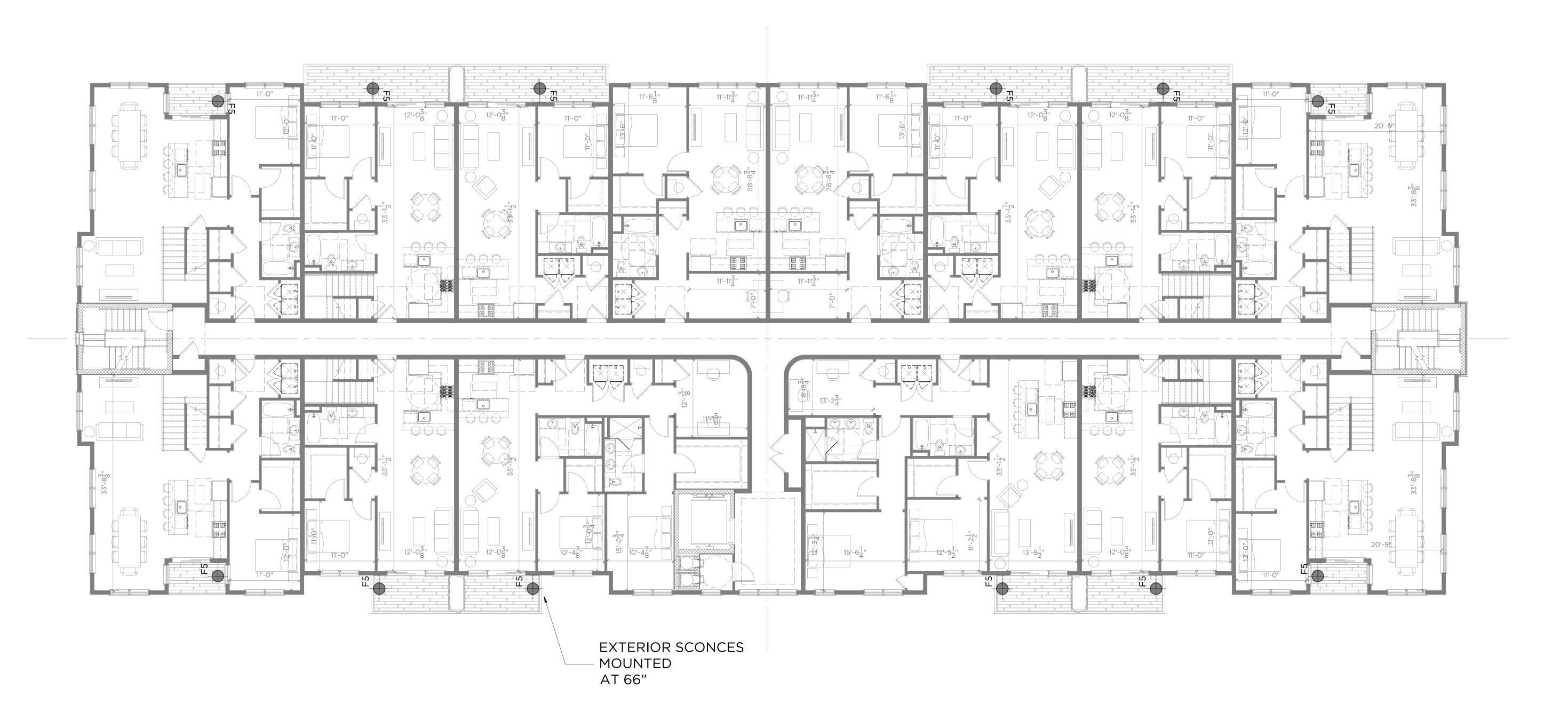
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LIGHTING FIXTURE LEGEND *(EM FIXTURES AS REQUIRED BY CODE. SEE MEP DRAWINGS FOR LOCATIONS)

<u>KEY</u>	TYPE	MODEL	REMARKS
F1	EXTERIOR RECESSED 2X2 LED		
() F2	EXTERIOR DOWNLIGHT		
0 _{F3}	EXTERIOR DOWNLIGHT (ADJUSTABLE)		
F4 ↓	EXTERIOR UP/DOWN WALL SCONCE (LARGE)		
₽ ^{F5}	EXTERIOR UP/DOWN WALL SCONCE (SMALL)		



SECOND FLOOR EXTERIOR LIGHTING PLAN



1/8" = 1'-0"



GRANOFF ARCHITECTS

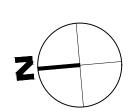
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LANDSCAPE ARCHITECT: **GRANOFF ARCHITECTS** 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

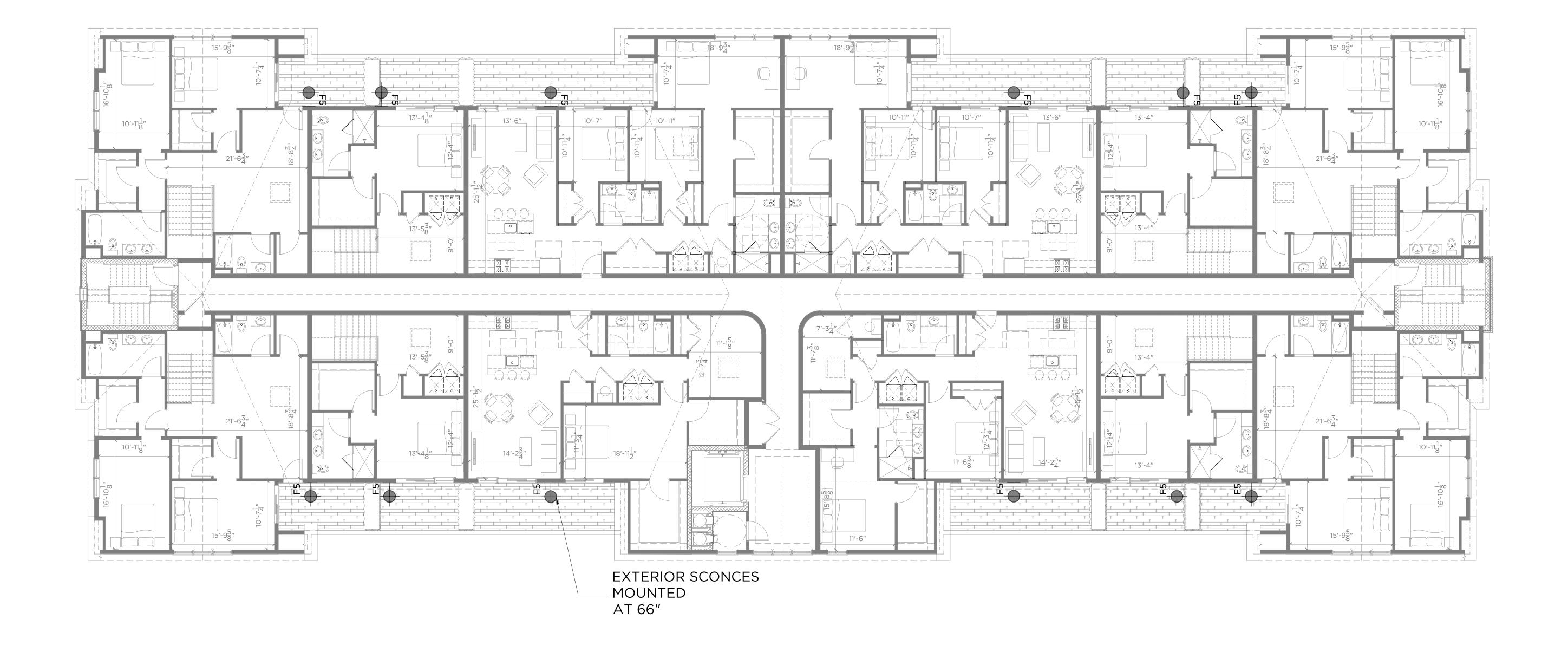
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PENTHOUSE EXTERIOR LIGHTING PLAN _____

<u>KEY</u>	TYPE	MODEL	<u>REMARKS</u>
F1	EXTERIOR RECESSED 2X2 LED		
() F2	EXTERIOR DOWNLIGHT		
() _{F3}	EXTERIOR DOWNLIGHT (ADJUSTABLE)		
₽ ^{F4}	EXTERIOR UP/DOWN WALL SCONCE (LARGE)		
₽ ^{F5}	EXTERIOR UP/DOWN WALL SCONCE (SMALL)		

LIGHTING FIXTURE LEGEND



1/8" = 1'-0"

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CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: **GRANOFF ARCHITECTS** 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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2 EAST ELEVATION (SIDE)

ITEM #	COMPONENT	MATERIAL AND FINISH
(1)	METAL ROOFING	SNAP ON STANDING SEAM METAL ROOF W/ SEAMS @ 16" O.C.
2	HALF ROUND GUTTER SYSTEM	HALF ROUND GUTTER W/ DOWNSPOUTS - PAINTED WHITE TO MATCH TRIM
3	1x FASCIA BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)
4	12" FRIEZE BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)
5	POLY ASH NICKEL GAP SIDING	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) W/ 7" EXPOSURE (COLOR: T.B.D.)-VERTICAL
6	POLY ASH NICKEL GAP SIDING	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) W/ 7" EXPOSURE (COLOR: T.B.D.)-HORIZONTAL
7	TRANSITION TRIM	$\frac{5}{4}$ x6 POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)
8	WINDOW TRIM	$\frac{5}{4}$ x6 POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)
စ	POLY ASH RAILING SYSTEM	RAILING SYSTEM (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)
10	$5\frac{1}{2}$ " CORNER TRIM BOARD	POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)
[1]	18" WATERTABLE TRIM BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)
12	SLOPED STONE CAP	2" NOM. NY BLUESTONE W/ CHISELED EDGE
13	2" NOM. STONE VENEER	ROUGHLY SQUARE & RECTANGULAR W/ NATURAL WEATHERED FACES; RANDOM BROKEN COURSED ASHI
14	ALUMN. RAILING SYSTEM HORIZ.	
15	POLY ASH BRACKETS	
16	POLYASH V-GROOVE SOFFIT	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) POLYASH BEADBOARD V-GROOVE SOFFIT
17	METAL CHIMNEY CAP	
18)	EXT. WALL SCONCE 4"	RECANGULAR EXTERIOR WALL SCONCE SEE LIGHTING PLAN FOR DETAILS

	NOTES
	GREY
	WHITE- VERTICAL ORIENTATION
	WHITE- HORIZONTAL ORIENTATION
HLAR PATTERN	GREY
	GREY

1/8″=1′-0″

REVISIONS



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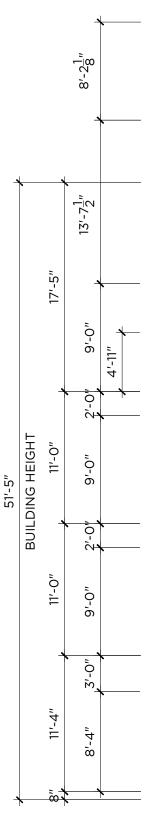
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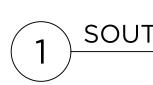
CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

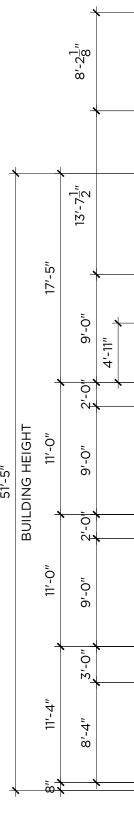
LANDSCAPE ARCHITECT: GRANOFF ARCHITECTS 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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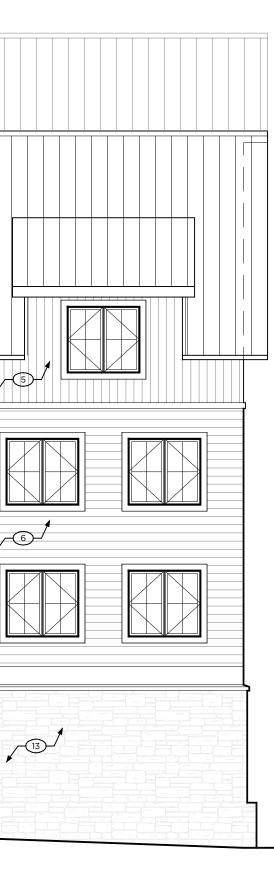
EM #	COMPONENT	MATERIAL AND FINISH	NOTES
1 M	METAL ROOFING	SNAP ON STANDING SEAM METAL ROOF W/ SEAMS @ 16" O.C.	GREY
2 +	HALF ROUND GUTTER SYSTEM	HALF ROUND GUTTER W/ DOWNSPOUTS - PAINTED WHITE TO MATCH TRIM	
3 1:	x FASCIA BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)	
4 1	2" FRIEZE BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)	
5 P	POLY ASH NICKEL GAP SIDING	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) W/ 7" EXPOSURE (COLOR: T.B.D.)-VERTICAL	WHITE- VERTICAL ORIENTATION
	POLY ASH NICKEL GAP SIDING	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) W/ 7" EXPOSURE (COLOR: T.B.D.)-HORIZONTAL	WHITE- HORIZONTAL ORIENTATION
7) т	FRANSITION TRIM	$\frac{5}{4}$ x6 POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)	
8 V	WINDOW TRIM	$\frac{5}{4}$ x6 POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)	
9) P	POLY ASH RAILING SYSTEM	RAILING SYSTEM (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)	
10 5	$5\frac{1}{2}$ " CORNER TRIM BOARD	POLY ASH TRIM BOARD (BORAL 'TRUEXTERIOR' OR SIM.) - PAINTED (COLOR - T.B.D.)	
11 1	8" WATERTABLE TRIM BOARD	1x POLY ASH (BORAL 'TRUEXTERIOR' OR SIM.) FASCIA BOARD - PAINTED (COLOR - T.B.D.)	
2) s	SLOPED STONE CAP	2" NOM. NY BLUESTONE W/ CHISELED EDGE	
	2" NOM. STONE VENEER	ROUGHLY SQUARE & RECTANGULAR W/ NATURAL WEATHERED FACES; RANDOM BROKEN COURSED ASHLAR PATTERN	GREY
	LUMN. RAILING SYSTEM HORIZ.		
15) P	OLY ASH BRACKETS		
6) P	OLYASH V-GROOVE SOFFIT	PREFINISHED (TRUEXTERIOR OR APPROVED EQ.) POLYASH BEADBOARD V-GROOVE SOFFIT	
17) M	1ETAL CHIMNEY CAP		
18) E	XT. WALL SCONCE 4"	RECANGULAR EXTERIOR WALL SCONCE SEE LIGHTING PLAN FOR DETAILS	GREY

ROOF (PEAK) EL. = 247'-10 1/2"	
GABLE HEIGHT (PEAK) EL. = 239'-8 1/2"	
BUILDING HEIGHT (MID POINT OF ROOF) EL. = 234'-6"	
TOP PLATE (HIGH) EL. = 226'-1" TOP PLATE (LOW) EL. = 222'-0"	
PENTHOUSE FLOOR (RESIDENTIAL) 7 EL. = 217'-1" 1 LEVEL 2 CLNG. 1 EL. = 215'-1" 8	
e	
EL. = 206'-1"	
EL. = 204'-1"	
FIRST FLOOR (RESIDENTIAL)	
V EL. = 195′-1″ DROPPED CEILING GARAGE 1	
DROPPED CEILING GARAGE	
GROUND FLOOR / PARKING LEVEL EL. = 183'-9" (CIVIL: 183.75)	
GRADE PLANE EL. = 183'-1" (CIVIL: 183.1	
✓ EL. = 183'-1" (CIVIL: 183.1	

SOUTH ELEVATION (FRONT 'B')

ROOF (PEAK)					
EL. = 247'-10 1/2"					
GABLE HEIGHT (PEAK) EL. = 239'-8 1/2"					
BUILDING HEIGHT (MID POINT OF ROOF)	-		4		
	_				E
♥ EL. = 226'-1"					
PENTHOUSE FLOOR (RESIDENTIAL)	_ (7)				$ \downarrow \checkmark$
Ψ EL. = 217'-1" $ \rightarrow$ LEVEL 2 CLNG $ -$					-
EL. = 215'-1"	8				
SECOND FLOOR (RESIDENTIAL)					
VEL. = 206'-1"					
- UEVEL 1 CLNG. EL. = 204'-1"					
FIRST FLOOR (RESIDENTIAL)					
- + FIRST FLOOR (RESIDENTIAL) EL. = 195'-1"					
DROPPED CEILING GARAGE	_				
4° EL. = 192'-1"		X			
GROUND FLOOR / PARKING LEVEL EL. = 183'-9" (CIVIL: 183.75)					
GRADE PLANE					
VEL. = 183'-1" (CIVIL: 183.1	_			- ?	

2 NORTH ELEVATION (REAR)



1/8″=1′-0″



1/8″=1′-0″



REVISIONS



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CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: **GRANOFF ARCHITECTS** 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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RENDERING-MAIN ENTRY WEST ELEVATION



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RENDERING-CORNER GODFREY AND HUBBARD

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RENDERING-WEST ELEVATION



RENDERING-MAIN ENTRY WEST ELEVATION

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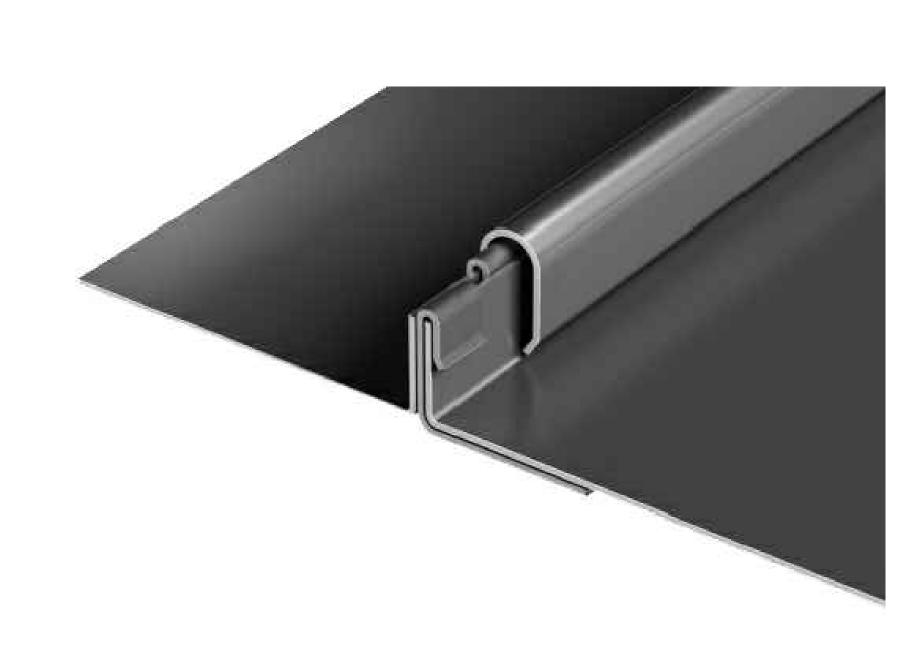
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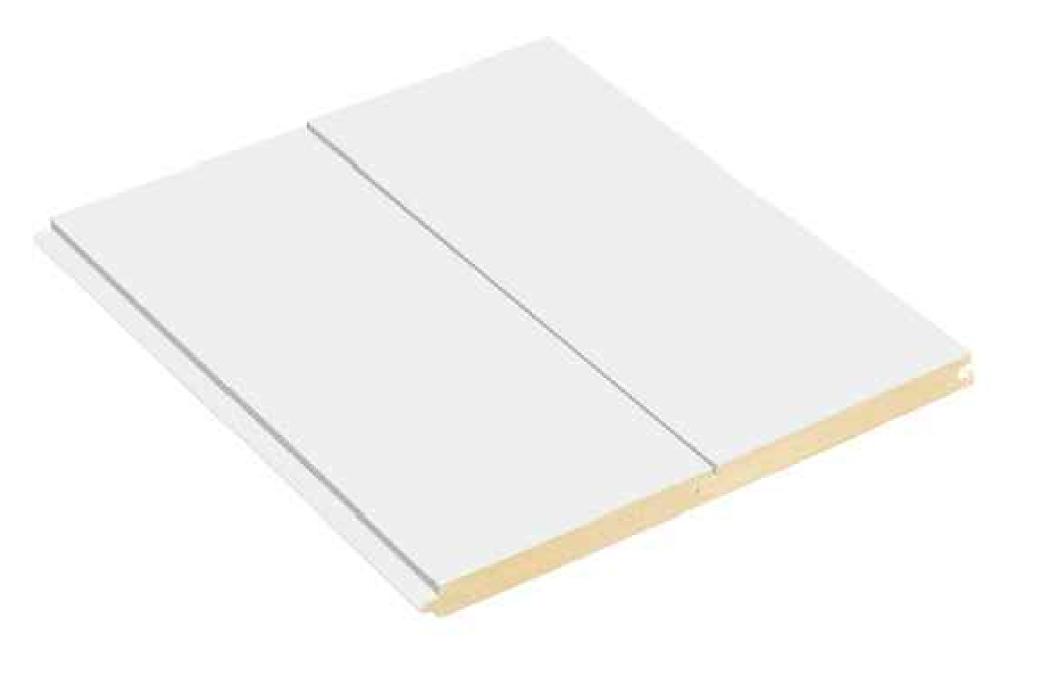


STANDING SEAM METAL ROOF (16IN O.C.) CHARCOAL

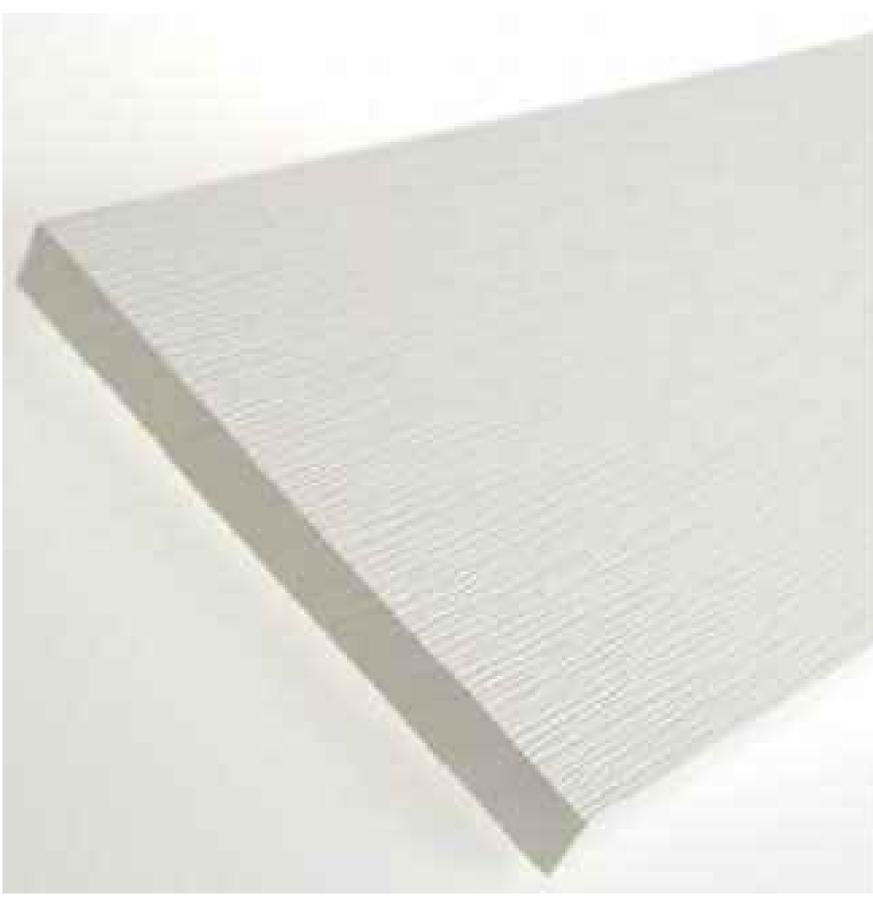


GALVANIZED HALF ROUND GUTTERS





POLYASH (TRUEXTERIOR) NICKEL GAP SIDING WHITE







LINEAR EXTERIOR WALL SCONCE-CHARCOAL



ALUMINUM CLAD WOOD CASEMENT WINDOW-2 OVER 2-CHARCOAL



METAL LINEAR BAR RAILING HORIZONTAL -CHARCOAL

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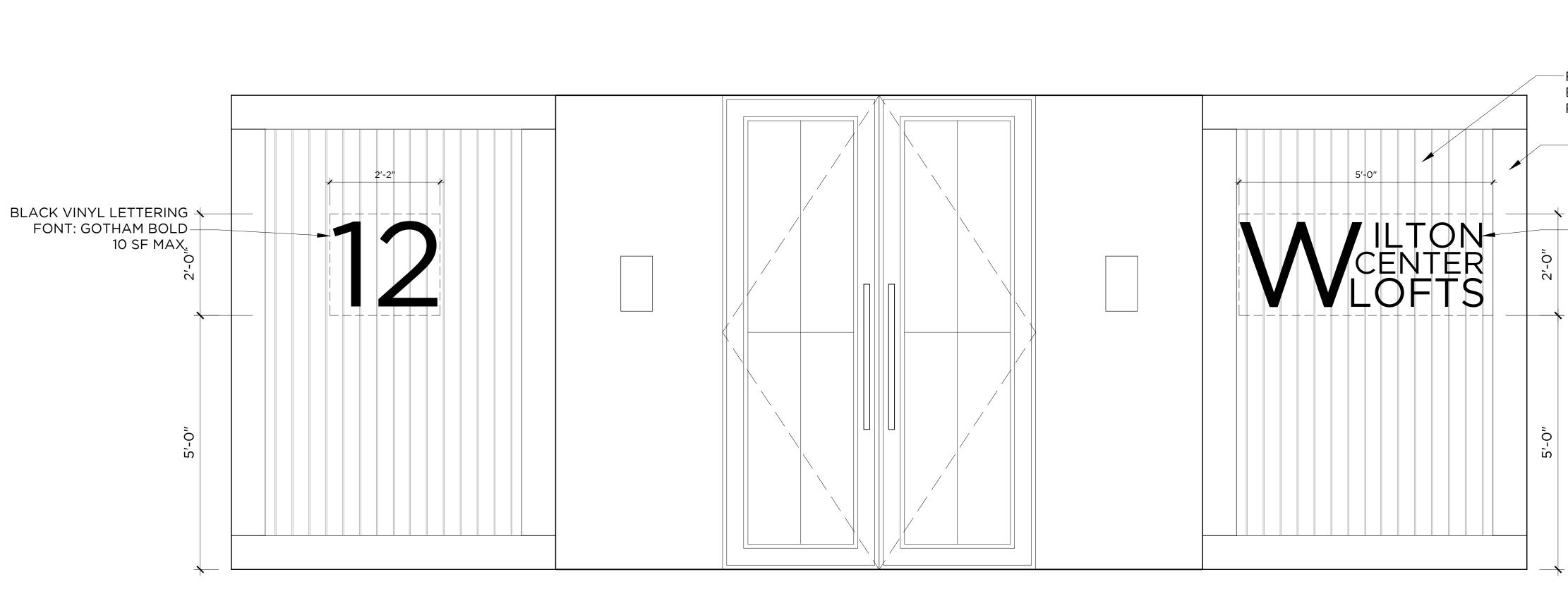
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SIGNAGE DIAGRAM AT MAIN LOBBY





RENDERING OF SIGNAGE AT ENTRY AT MAIN LOBBY

3/4"=1'-0"

-FIELD BUILT BARN DOOR-POLYASH PAINTED WHITE

-FIELD BUILT BARN DOOR-POLYASH PAINTED WHITE

BLACK VINYL LETTERING FONT: GOTHAM BOLD 10 SF MAX.

NTS



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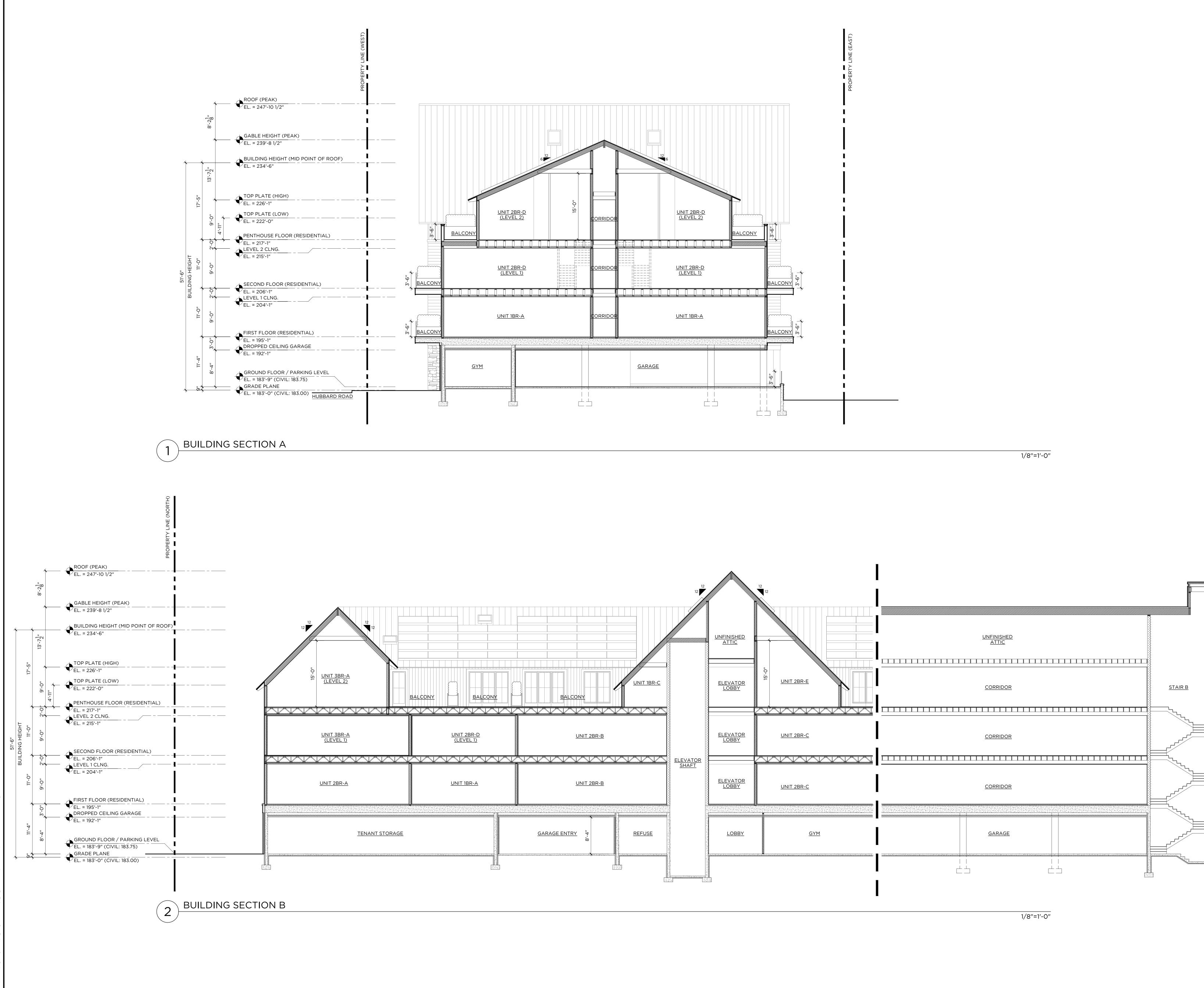
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CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: **GRANOFF ARCHITECTS** 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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GRANOFF ARCHITECTS

330 RAILROAD AVENUE GREENWICH, CT 06830 203.625.9460 WWW.GRANOFFARCHITECTS.COM

CONSULTANTS

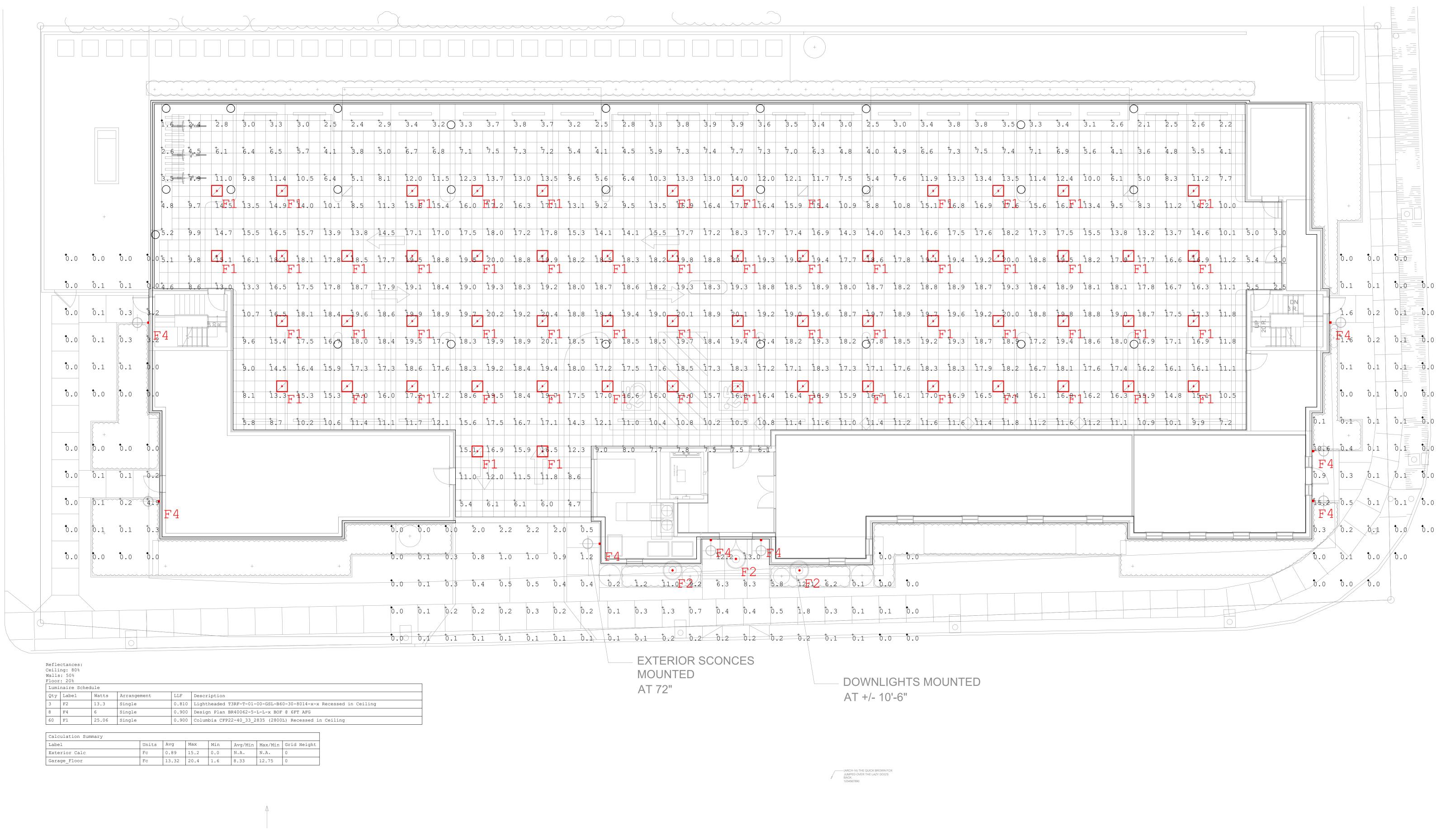
CIVIL ENGINEER: **REDNISS & MEAD** 22 FIRST STREET STAMFORD, CT 06905 (203) 327-0500 ext. 15174 p.shurr@rednissmead.com

LANDSCAPE ARCHITECT: GRANOFF ARCHITECTS 330 RAILROAD AVENUE GREENWICH, CT 06830 (203) 625-9460 ext. 16 rb@granoffarchitects.com

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REVISIONS _____



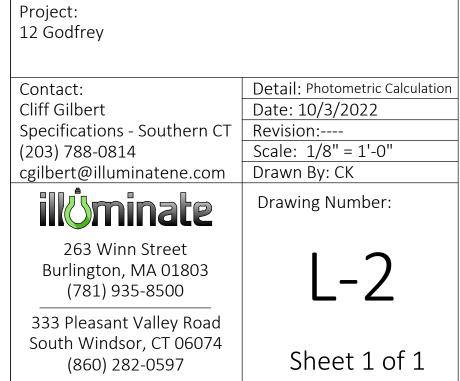


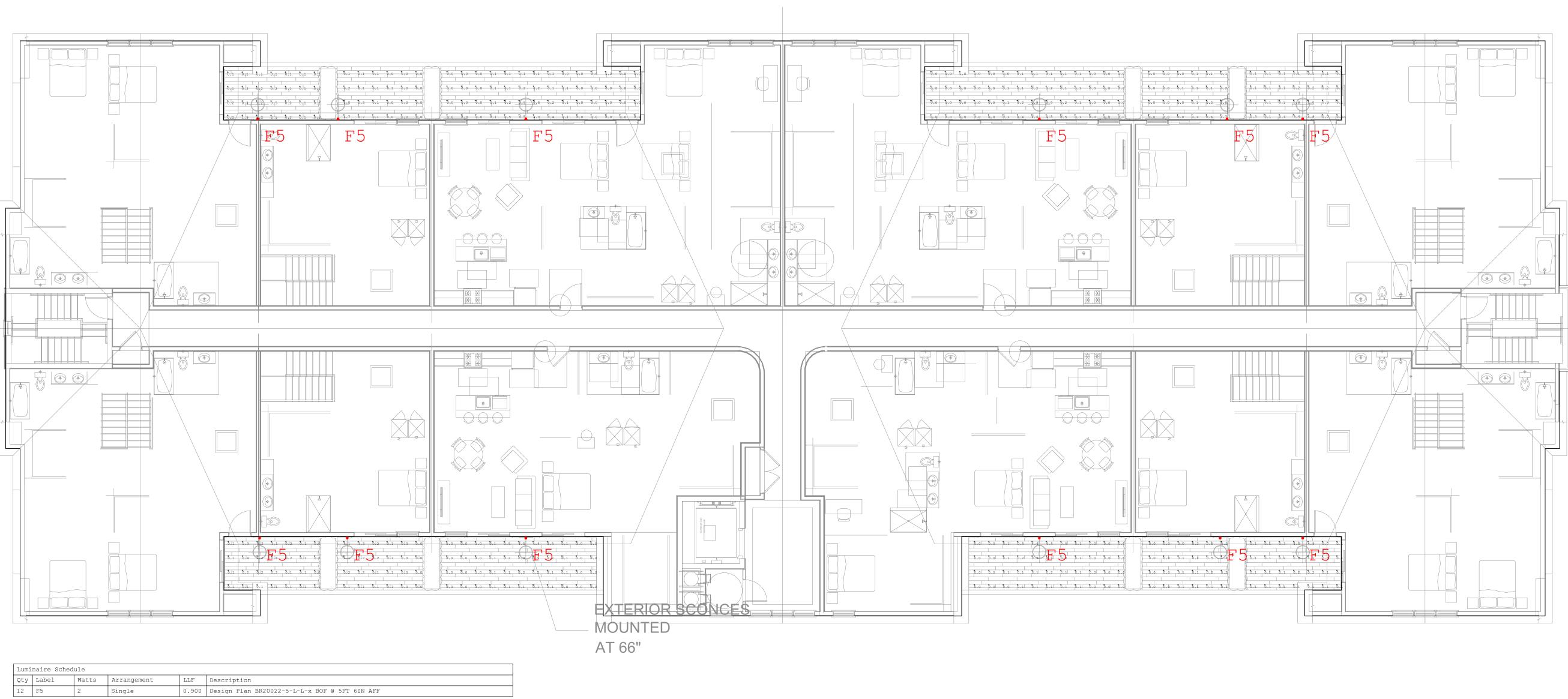
Project: 12 Godfrey

Contact: Cliff Gilbert (203) 788-0814









Qty	Label	Watts	Arrangement			LLF	Descr	iption					
12	F5	2	Single		0.90	0 Desig	n Plan B	20022-5-L-L-x BOF @ 5FT 6IN AFF					
Calculation Summary													
Label		Units	Av	g	Max	Min	Avg/Min	Max/Min	Grid	Height			
Balconies			Fc	0.37 5		5.2	0.0	N.A.	N.A.				

Project: 12 Godfrey

Contact: Cliff Gilbe Specificat (203) 788-cgilbert@

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cifications - Southern CT	Revision:
3) 788-0814	Scale: 1/8" = 1'-0"
bert@illuminatene.com	Drawn By: CK
llôminate	Drawing Number:
263 Winn Street Burlington, MA 01803 (781) 935-8500	L-3
33 Pleasant Valley Road	
uth Windsor, CT 06074 (860) 282-0597	Sheet 1 of 1



Drainage Summary Report

12 Godfrey Place

Prepared by

Redniss & Mead, Inc. 22 First Street Stamford, CT (203) 327-0500

Issued on: September 30, 2022

Issued for: Site Plan Approval

Craig J. Flaherty, CT Lic. No. 21149

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HydroCAD Model	Appendix 3
NRCS Soils Information	Appendix 4



Drainage Summary Narrative

Greenwich Realty Development LLC, the owner of 12 Godfrey Place, is proposing to replace the existing office building with a four-story residential building consisting of 32 apartments. The property is 0.625 acres and lies in the Wilton Center District. The property is located northeast of the intersection of Godfrey Place and Hubbard Road. It is bordered to its east by multi-family housing owned by the Wilton Library Association and to the north by a commercial property owned by the Town of Wilton and developed with multiple storefronts.

The site is located within Zone X as depicted on the Federal Emergency Management Agency – Flood Insurance Map Community No. 090020 Panel 383 Suffix F, effective date June 18, 2010. The site is served by public water and sanitary sewer service.

Existing Conditions

The site is currently developed with a three-story office building situated on the southern half of the site. Two parking lots are located in the northern half of the property. Impervious surfaces cover 18,653 square feet (68.5%) of the site.

The site lies in the Norwalk River Watershed. Runoff from the site drains overland to the north into Hubbard Road and to the southwest into Godfrey Place. Catch basins in Hubbard Road drain north then east through the Town of Wilton property, across Old Ridgefield Road and into the Norwalk River. Stormwater in Godfrey Place is captured and conveyed through the Stop & Shop property before crossing Old Ridgefield Road and discharging into the Norwalk River. Study points were established along both Hubbard and Godfrey.

The site currently has dry wells located in each of the parking lot. Both drywells are designed without outlet. The north lot dry well captures runoff from the surrounding pavement and theoretically overtops in the 25-year storm via the curb cut into Hubbard Road. The south lot dry well captures runoff from the surrounding pavement and building and theoretically overtops in the 10-year storm. Both drywells were factored in the existing conditions analysis with below and above-grade storage modeled. An exfiltration rate of 1.02 inches per hour was modeled, reflecting the Default (Rawls) infiltration rate for HSG B Sandy Loam soils consistent with those found on-site.

Proposed Conditions

The proposed work includes the demolition of the existing office and parking and construction of the new four-story residential building. Parking is provided on-grade, under the second story of the building. The improvements result in 20,665 (75.8%) of impervious coverage, an increase of 2,012 square feet. Atlas-14 rainfall rates were used in the drainage analysis.

The impacts resulting from the increase in impervious coverage and removal of the existing drywells are mitigated using an infiltration system consisting of (18) 5'-tall Retain-It units. The infiltration system is located within the footprint of the building, below the on-grade parking. The entire building, in addition to the area north and east of the building, is directed to the system. Water



Quality treatment is provided to the tributary area via infiltration (Appendix 2). The infiltration system is sized to fully infiltrate runoff through the 25-year storm. In the 50 & 100-year storm, stormwater will discharge via a 6" pipe connected to the catch basin in Hubbard Road. Area Drain #4, located along the east side of the building, serves as the high overflow for the system in the event of an anomaly or greater than 100-year storm. It is not designed to discharge through the 100-year storm and is intended as a precaution for more severe rain events.

The remainder of the site bypasses the infiltration system and flows into Godfrey and Hubbard. These areas consist of the landscaping, walks and driveway which pitch away from the building and towards the back of curb. Given that the existing site only discharges to Hubbard when the north lot drywell overtops, the Hubbard Study Point does witness a minor increase in peak flows. The tables below compare existing and proposed conditions for both study points:

Peak Flow (cfs)								
Return Period (yrs)		Godfrey	Place	Hubbard Road				
renou (yis)	Ex	Pr	Change	Ex	Pr	Change		
10	0.30	0.23	-0.07	0.00	0.17	0.17		
25	0.42	0.32	-0.10	0.05	0.23	0.18		

*Runoff values taken from the HydroCAD Report found in Appendix 3

Summary

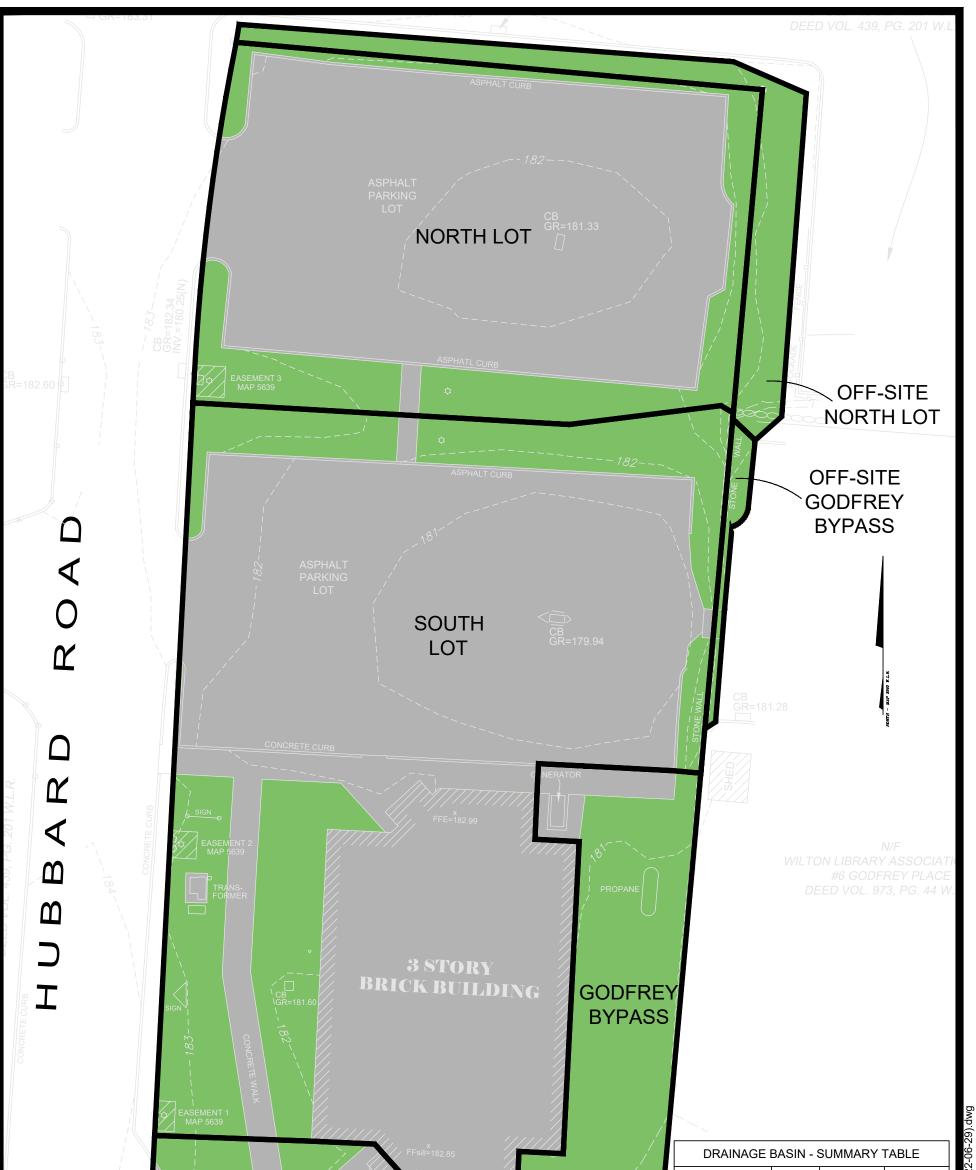
The proposed stormwater system is designed to capture and treat runoff originating from 80% of the site. The system is sized to infiltrate all tributary runoff through the 25-year storm. Minor areas of landscaping, walks, and drive discharge to the gutters along Hubbard Road and Godfrey place. It is our belief that the proposed drainage improvements are robustly designed and will not negatively impact downstream properties.



Appendix 1

Drainage Basin Maps





			Ţ		
	BASIN	CN	SIZE (sf)	TC (min.)	(2022
	NORTH LOT	86.3	3,903	5.0	1 (2
	SOUTH LOT	88.8	15,167	5.0	ster
\circ POLE \sim CL8P #1704 \sim 782	GODFREY BYPASS	68.6	4,082	5.0	Maste
GODFREY PLACE EXISTING CONDITIONS DRAINAGE BASI 12 GODFREY PLACE	ΝΜΑΡ		LAND SURVEYIN CIVIL ENGINEER PLANNING & ZO PERMITTING 22 First Street S Tel: 203.327.0500 www.rednissmead	1NG NING CONSULTING Stamford, CT 06905 Fax: 203.357.1118 .com	H:\Jobfiles2\10000\10500\10556\DWG\10556
WILTON, CT			сомм. no.: 10556	DATE: 09/30/2022 SCALE: I"=20'	0/3/2022 8



06-29).dwg

/// FFsill=182.8	_		-		<u>,</u>
	BASIN	CN	SIZE (sf)	TC (min.)	(2022
	INFIL#1	91.1	22,303	5.0	~
Т	HUBBARD BYPASS	80.7	1,858	5.0	Ister
	GODFREY BYPASS	69.7	3,552	5.0	8 Ma
GODFREY PLACE PROPOSED CONDITIONS DRAINAGE BAS 12 GODFREY PLACE WILTON, CT	SIN MAP		PERMITTING 22 First Street S	ING NING CONSULTING Stamford, CT 06905 Fax: 203.357.1118	M H:\

Appendix 2

Water Quality Volume Calculations 72-Hour Drawdown Calculations



oject: 12 Ga	odfrey Place		Project #:	10556	Date:	9/30/2022
cation: Wilto	n, CT	By:	PBS	Checked:	CJF	
		Infil#1 Basir	1			
	Inf#1	Basin				
	Area=	0.533	acres			
	Impervious Area=	0.433	acres			
	I=	0.812	а			
	R=	0.781	b			
	WQV=	0.035	ac. ft. ^c			
			2.1			
	WQV=	1,510.1	ft. ^{3 a}			
^b R=0.0	ent Impervious Coverage 5+0.009(I); Volumetric runoff Coe		on taken from 2	2004 Conr	necticut	
	water Quality Manual section 7.4.1					`
	=(1"xRxA)/12; Water Quality Vol water Quality Manual section 7.4.1		aken from 200	4 Connect	ticut	



72-Hour Draw Down Ca	lculation	IS		
Project: 12 Godfrey Place	Project #:	10556	Date:	9/30/2022
Location: Wilton, CT	By:	PBS	Checked:	CJF
Location: Wilton, CT	By:	PBS	Checked:	CJF

Inf#1		
Surface Area of Infiltration System (SA)	1,776	ft ²
Volume of Storage of Infiltration System (VS)	4,623	ft ³
Infiltration Rate (IR)	2.20	in/hr ^c
Theoretical Water Column Height	31.24	in ^a
Time of Draw Down	14.20	hr [⊳]

Note: The surface area reflects the footprint of the cultecs and perimeter stone. The volume of water is the storage in the system below the outlet.

^a Theoretical Water Column Height (WCH) = VS/SA*12

^b Time of Draw Down = WCH/IR

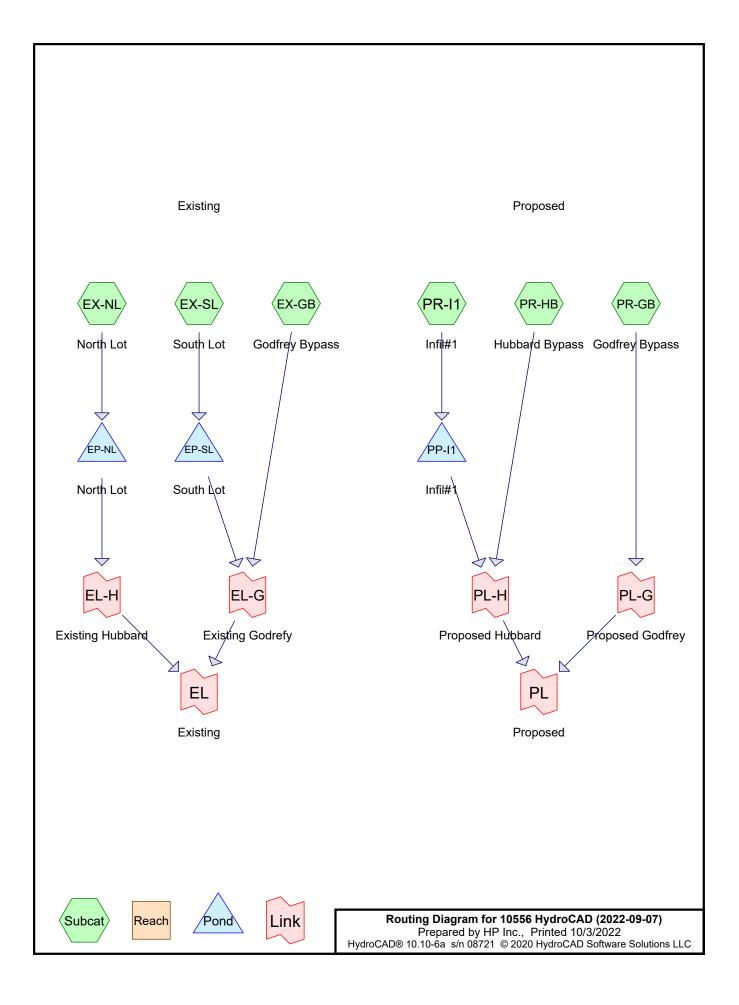
^c Infiltration Rate (IR) taken from PH#1 with FOS of 2 applied (1" in 13.33 min x 2)



Appendix 3

HydroCAD Report





10556 HydroCAD (2022-09-07) Prepared by HP Inc.	Type III 24-hr 2-Year Rainfall=3.55" Printed 10/3/2022
HydroCAD® 10.10-6a s/n 08721 © 2020 HydroCAD Software Solutions	SLLC Page 2
Time span=0.00-24.00 hrs, dt=0.0100 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond ro	, Weighted-CN

Subcatchment EX-GB: Godfrey Bypass	Runoff Area=4,082 sf 20.63% Impervious Runoff Depth>0.96" Tc=0.0 min CN=68.6 Runoff=0.12 cfs 327 cf
Subcatchment EX-NL: North Lot	Runoff Area=9,364 sf 68.38% Impervious Runoff Depth>2.17" Tc=5.0 min CN=86.3 Runoff=0.57 cfs 1,690 cf
Subcatchment EX-SL: South Lot	Runoff Area=15,167 sf 75.22% Impervious Runoff Depth>2.38" Tc=5.0 min CN=88.8 Runoff=1.00 cfs 3,012 cf
Subcatchment PR-GB: Godfrey Bypass	Runoff Area=3,552 sf 23.42% Impervious Runoff Depth>1.02" Tc=5.0 min CN=69.7 Runoff=0.09 cfs 302 cf
Subcatchment PR-HB: Hubbard Bypass	Runoff Area=1,858 sf 53.18% Impervious Runoff Depth>1.73" Tc=5.0 min CN=80.7 Runoff=0.09 cfs 267 cf
Subcatchment PR-I1: Infil#1	Runoff Area=23,203 sf 81.22% Impervious Runoff Depth>2.60" Tc=5.0 min CN=91.1 Runoff=1.64 cfs 5,019 cf
Pond EP-NL: North Lot Discard	Peak Elev=182.24' Storage=1,238 cf Inflow=0.57 cfs 1,690 cf ed=0.01 cfs 495 cf Primary=0.00 cfs 0 cf Outflow=0.01 cfs 495 cf
Pond EP-SL: South Lot Discard	Peak Elev=181.24' Storage=2,464 cf Inflow=1.00 cfs 3,012 cf ed=0.01 cfs 549 cf Primary=0.00 cfs 0 cf Outflow=0.01 cfs 549 cf
Pond PP-I1: Infil#1 Discarded=	Peak Elev=178.62' Storage=2,326 cf Inflow=1.64 cfs 5,019 cf 0.13 cfs 4,810 cf Primary=0.00 cfs 0 cf Outflow=0.13 cfs 4,810 cf
Link EL: Existing	Inflow=0.12 cfs 327 cf Primary=0.12 cfs 327 cf
Link EL-G: Existing Godrefy	Inflow=0.12 cfs 327 cf Primary=0.12 cfs 327 cf
Link EL-H: Existing Hubbard	Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf
Link PL: Proposed	Inflow=0.18 cfs 569 cf Primary=0.18 cfs 569 cf
Link PL-G: Proposed Godfrey	Inflow=0.09 cfs 302 cf Primary=0.09 cfs 302 cf
Link PL-H: Proposed Hubbard	Inflow=0.09 cfs 267 cf Primary=0.09 cfs 267 cf

Total Runoff Area = 57,226 sf Runoff Volume = 10,619 cf Average Runoff Depth = 2.23" 31.29% Pervious = 17,908 sf 68.71% Impervious = 39,318 sf

10556 HydroCAD (2022-09-07) Prepared by HP Inc. <u>HydroCAD® 10.10-6a s/n 08721 © 2020 Hydro</u>	Type III 24-hr 10-Year Rainfall=5.42"Printed 10/3/2022CAD Software Solutions LLCPage 26
Runoff by SCS TR	4.00 hrs, dt=0.0100 hrs, 2401 points -20 method, UH=SCS, Weighted-CN ans method - Pond routing by Stor-Ind method
Subcatchment EX-GB: Godfrey Bypass	Runoff Area=4,082 sf 20.63% Impervious Runoff Depth>2.23" Tc=0.0 min CN=68.6 Runoff=0.30 cfs 760 cf
Subcatchment EX-NL: North Lot	Runoff Area=9,364 sf 68.38% Impervious Runoff Depth>3.89" Tc=5.0 min CN=86.3 Runoff=1.00 cfs 3,034 cf
Subcatchment EX-SL: South Lot	Runoff Area=15,167 sf 75.22% Impervious Runoff Depth>4.15" Tc=5.0 min CN=88.8 Runoff=1.70 cfs 5,246 cf
Subcatchment PR-GB: Godfrey Bypass	Runoff Area=3,552 sf 23.42% Impervious Runoff Depth>2.32" Tc=5.0 min CN=69.7 Runoff=0.23 cfs 688 cf
Subcatchment PR-HB: Hubbard Bypass	Runoff Area=1,858 sf 53.18% Impervious Runoff Depth>3.33" Tc=5.0 min CN=80.7 Runoff=0.17 cfs 515 cf
Subcatchment PR-I1: Infil#1	Runoff Area=23,203 sf 81.22% Impervious Runoff Depth>4.40" Tc=5.0 min CN=91.1 Runoff=2.71 cfs 8,504 cf
Pond EP-NL: North Lot Discarded	Peak Elev=182.59' Storage=2,474 cf Inflow=1.00 cfs 3,034 cf d=0.01 cfs 561 cf Primary=0.00 cfs 0 cf Outflow=0.01 cfs 561 cf
Pond EP-SL: South Lot Discarded=0.0	Peak Elev=181.65' Storage=4,193 cf Inflow=1.70 cfs 5,246 cf 01 cfs 629 cf Primary=0.03 cfs 447 cf Outflow=0.04 cfs 1,077 cf
Pond PP-I1: Infil#1 Discarded=0.	Peak Elev=180.20' Storage=4,253 cf Inflow=2.71 cfs 8,504 cf 20 cfs 7,403 cf Primary=0.00 cfs 0 cf Outflow=0.20 cfs 7,403 cf
Link EL: Existing	Inflow=0.30 cfs 1,207 cf Primary=0.30 cfs 1,207 cf
Link EL-G: Existing Godrefy	Inflow=0.30 cfs 1,207 cf Primary=0.30 cfs 1,207 cf
Link EL-H: Existing Hubbard	Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf
Link PL: Proposed	Inflow=0.40 cfs 1,203 cf Primary=0.40 cfs 1,203 cf
Link PL-G: Proposed Godfrey	Inflow=0.23 cfs 688 cf Primary=0.23 cfs 688 cf
Link PL-H: Proposed Hubbard	Inflow=0.17 cfs 515 cf Primary=0.17 cfs 515 cf

Total Runoff Area = 57,226 sf Runoff Volume = 18,748 cf Average Runoff Depth = 3.93" 31.29% Pervious = 17,908 sf 68.71% Impervious = 39,318 sf

10556 HydroCAD (2022-09-07) Prepared by HP Inc.	<i>Type III 24-hr 25-Year Rainfall=6.59"</i> Printed 10/3/2022
<u>HydroCAD® 10.10-6a_s/n 08721_© 2020 Hydro</u>	CAD Software Solutions LLC Page 50
Runoff by SCS TR	4.00 hrs, dt=0.0100 hrs, 2401 points -20 method, UH=SCS, Weighted-CN ans method - Pond routing by Stor-Ind method
Subcatchment EX-GB: Godfrey Bypass	Runoff Area=4,082 sf 20.63% Impervious Runoff Depth>3.14" Tc=0.0 min CN=68.6 Runoff=0.42 cfs 1,068 cf
Subcatchment EX-NL: North Lot	Runoff Area=9,364 sf 68.38% Impervious Runoff Depth>5.00" Tc=5.0 min CN=86.3 Runoff=1.27 cfs 3,903 cf
Subcatchment EX-SL: South Lot	Runoff Area=15,167 sf 75.22% Impervious Runoff Depth>5.28" Tc=5.0 min CN=88.8 Runoff=2.14 cfs 6,676 cf

Subcatchment PR-GB: Godfrey Bypass Runoff Area=3,552 sf 23.42% Impervious Runoff Depth>3.25" Tc=5.0 min CN=69.7 Runoff=0.32 cfs 961 cf

Subcatchment PR-HB: Hubbard Bypass Runoff Area=1,858 sf 53.18% Impervious Runoff Depth>4.39" Tc=5.0 min CN=80.7 Runoff=0.23 cfs 680 cf

Subcatchment PR-I1: Infil#1Runoff Area=23,203 sf81.22% ImperviousRunoff Depth>5.54"Tc=5.0 minCN=91.1Runoff=3.37 cfs10,718 cf

Pond EP-NL: North LotPeak Elev=182.65' Storage=2,731 cfInflow=1.27 cfs3,903 cfDiscarded=0.01 cfs592 cfPrimary=0.05 cfs724 cfOutflow=0.06 cfs1,316 cf

Pond EP-SL: South LotPeak Elev=181.67' Storage=4,297 cfInflow=2.14 cfs6,676 cfDiscarded=0.01 cfs661 cfPrimary=0.15 cfs1,842 cfOutflow=0.16 cfs2,503 cf

 Pond PP-I1: Infil#1
 Peak Elev=181.22' Storage=5,502 cf
 Inflow=3.37 cfs
 10,718 cf

 Discarded=0.24 cfs
 9,046 cf
 Primary=0.00 cfs
 0 cf
 Outflow=0.24 cfs
 9,046 cf

Link EL: Existing

Link EL-G: Existing Godrefy

Link EL-H: Existing Hubbard

Link PL: Proposed

Link PL-G: Proposed Godfrey

Link PL-H: Proposed Hubbard

Total Runoff Area = 57,226 sf Runoff Volume = 24,006 cf Average Runoff Depth = 5.03" 31.29% Pervious = 17,908 sf 68.71% Impervious = 39,318 sf

Inflow=0.42 cfs 3,634 cf

Inflow=0.42 cfs 2,911 cf

Inflow=0.05 cfs 724 cf

Primary=0.05 cfs 724 cf

Inflow=0.55 cfs 1,641 cf

Inflow=0.32 cfs 961 cf

Inflow=0.23 cfs 680 cf Primary=0.23 cfs 680 cf

Primary=0.32 cfs 961 cf

Primary=0.55 cfs 1,641 cf

Primary=0.42 cfs 2,911 cf

Primary=0.42 cfs 3,634 cf

Summary for Subcatchment EX-GB: Godfrey Bypass

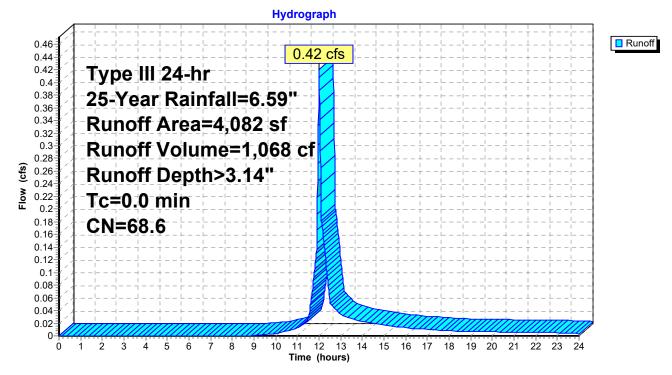
[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.42 cfs @ 12.00 hrs, Volume= Routed to Link EL-G : Existing Godrefy 1,068 cf, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

	Area (sf)	CN	Description
*	842	98.0	Impervious
*	3,240	61.0	On-Site Lawn, HSG B
	4,082 3,240 842	68.6	Weighted Average 79.37% Pervious Area 20.63% Impervious Area

Subcatchment EX-GB: Godfrey Bypass



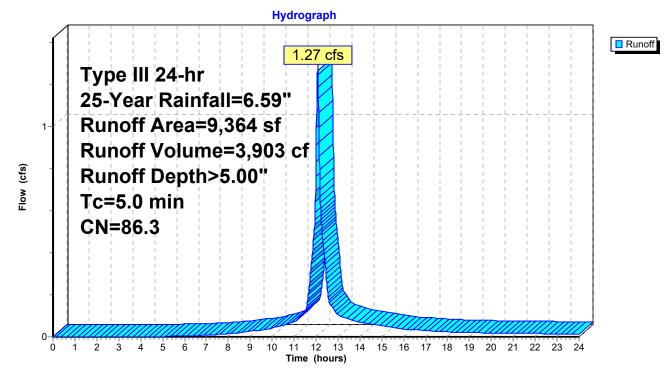
Summary for Subcatchment EX-NL: North Lot

Runoff = 1.27 cfs @ 12.07 hrs, Volume= Routed to Pond EP-NL : North Lot 3,903 cf, Depth> 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

-	A	rea (sf)	CN	Descriptio	n		
*		6,403	98.0	Imperviou	IS		
*		1,771	61.0	On-Site L	awn, HSG	B	
*		1,190	61.0	Off-Site L	awn, HSG	B	
		9,364 2,961 6,403	86.3	Weighted Average 31.62% Pervious Area 68.38% Impervious Area			
(r	Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	I	
	5.0					Direct Entry,	

Subcatchment EX-NL: North Lot



Summary for Subcatchment EX-SL: South Lot

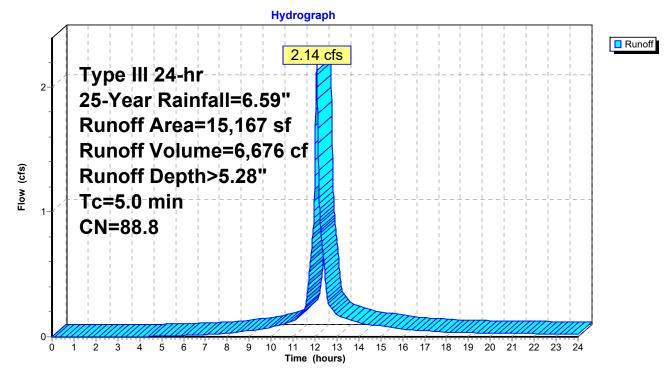
2.14 cfs @ 12.07 hrs, Volume= Runoff = Routed to Pond EP-SL : South Lot

6,676 cf, Depth> 5.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

	A	rea (sf)	CN	Descriptio	n		
*		11,408	98.0	Imperviou	IS		
*		3,582	61.0	On-Site L	awn, HSG	B	
*		177	61.0	Off-Site L	awn, HSG	B	
		15,167 3,759 11,408	88.8	Weighted Average 24.78% Pervious Area 75.22% Impervious Area			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)		
	5.0					Direct Entry,	

Subcatchment EX-SL: South Lot



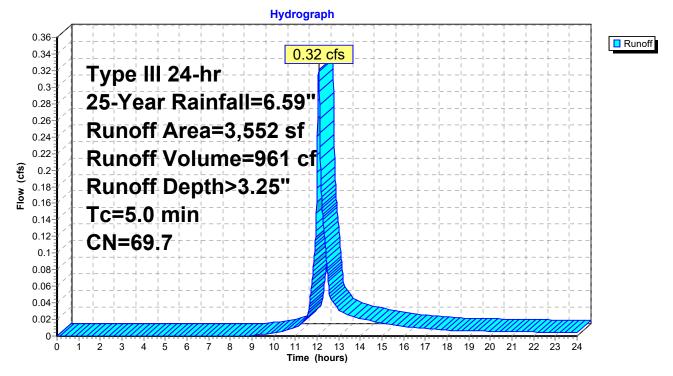
Summary for Subcatchment PR-GB: Godfrey Bypass

Runoff = 0.32 cfs @ 12.08 hrs, Volume= Routed to Link PL-G : Proposed Godfrey 961 cf, Depth> 3.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

	Area	a (sf)	CN	Descriptio	n						
*		832	98.0	Imperviou	Impervious						
*	2	,720	61.0	On-Site La	awn, HSG	В					
	3	,552	69.7	Weighted Average							
	2	,720		76.58% Pervious Area							
		832		23.42% Impervious Area							
					- ··						
		ength	Slope	Velocity	Capacity	Description					
(m	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
:	5.0					Direct Entry,					

Subcatchment PR-GB: Godfrey Bypass



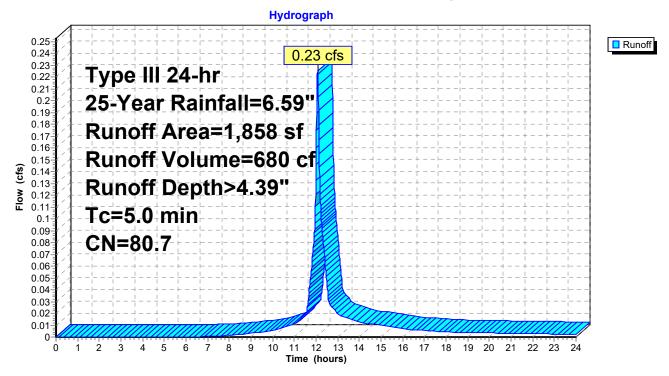
Summary for Subcatchment PR-HB: Hubbard Bypass

Runoff = 0.23 cfs @ 12.07 hrs, Volume= Routed to Link PL-H : Proposed Hubbard 680 cf, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

	Area (sf)	CN	Description							
*	988	98.0	Imperviou	Impervious						
*	870	61.0	On-Site L	awn, HSG	В					
	1,858 870 988	80.7	Weighted Average 46.82% Pervious Area 53.18% Impervious Area							
T (mir	c Length n) (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
5.	0				Direct Entry,					

Subcatchment PR-HB: Hubbard Bypass



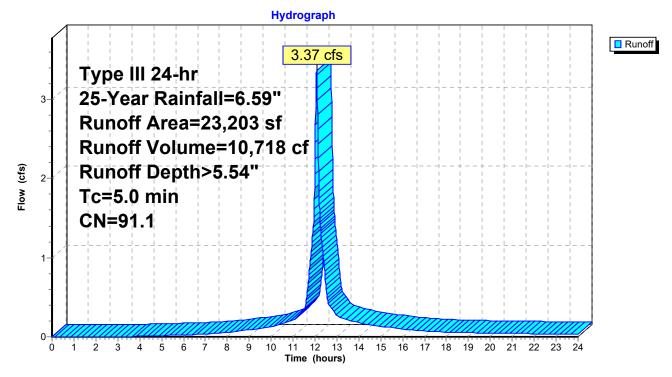
Summary for Subcatchment PR-I1: Infil#1

Runoff = 3.37 cfs @ 12.07 hrs, Volume= Routed to Pond PP-I1 : Infil#1 10,718 cf, Depth> 5.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Type III 24-hr 25-Year Rainfall=6.59"

_	A	rea (sf)	CN	Descriptic	n	
*		18,845	98.0	Imperviou	IS	
*		2,991	61.0	On-Site L	awn, HSG	В
*		1,367	61.0	Off-Site L	awn, HSG	В
	Тс	23,203 4,358 18,845 Length	91.1 Slope		Average ervious Are npervious A Capacity	Area
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	5.0					Direct Entry,

Subcatchment PR-I1: Infil#1



Summary for Pond EP-NL: North Lot

Inflow Area =	9,364 sf, 68.38% Impervious,	Inflow Depth > 5.00" for 25-Year event					
Inflow =	1.27 cfs @ 12.07 hrs, Volume=	3,903 cf					
Outflow =	0.06 cfs @ 14.48 hrs, Volume=	1,316 cf, Atten= 95%, Lag= 144.6 min					
Discarded =	0.01 cfs @ 14.48 hrs, Volume=	592 cf					
Primary =	0.05 cfs @ 14.48 hrs, Volume=	724 cf					
Routed to Link EL-H : Existing Hubbard							

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Peak Elev= 182.65' @ 14.48 hrs Surf.Area= 4,718 sf Storage= 2,731 cf

Plug-Flow detention time= 345.2 min calculated for 1,315 cf (34% of inflow) Center-of-Mass det. time= 210.1 min (1,002.1 - 792.1)

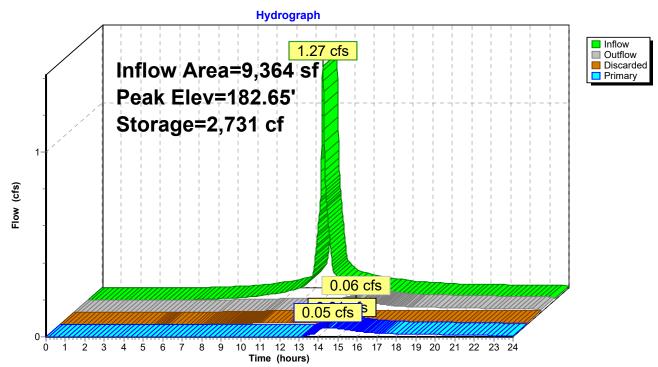
Volume	Invert	Avail.Storage	Storage Description
#1	174.40'	50 cf	Dry Well Stone (Prismatic)Listed below (Recalc)
			300 cf Overall - 174 cf Embedded = 126 cf \times 40.0% Voids
#2	174.40'	174 cf	Concrete Dry Well (Prismatic)Listed below (Recalc) Inside #1
#3	181.33'	4,421 cf	On-Grade Storage (Prismatic)Listed below (Recalc)
#4	180.40'	6 cf	CB from DW to Grade (Prismatic)Listed below (Recalc)
		4,651 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
174.40	50	0	0
180.40	50	300	300
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
174.40	29	0	0
180.40	29	174	174
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
(feet)	Surf.Area (sq-ft) 0	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0
	<u>(sq-ft)</u> 0		
(feet) 181.33	(sq-ft)	(cubic-feet) 0	(cubic-feet) 0
(feet) 181.33 182.00	(sq-ft) 0 1,486	(cubic-feet) 0 498	(cubic-feet) 0 498
(feet) 181.33 182.00 183.00 Elevation	(sq-ft) 0 1,486 6,361 Surf.Area	(cubic-feet) 0 498 3,924 Inc.Store	(cubic-feet) 0 498 4,421 Cum.Store

Device	Routing	Invert	Outlet Devices
#1	Primary	182.61'	Driveway Opening to Hubbard, C= 3.27
	-		Offset (feet) 0.00 0.01 25.44 25.45
			Height (feet) 0.85 0.00 0.43 0.85
#2	Discarded	174.40'	1.020 in/hr Sandy Loam (HSG B) Exfiltration over Surface area below 174.41'
			Conductivity to Groundwater Elevation = 173.40' Phase-In= 0.01'

Discarded OutFlow Max=0.01 cfs @ 14.48 hrs HW=182.65' (Free Discharge) **2=Sandy Loam (HSG B) Exfiltration** (Controls 0.01 cfs)

Primary OutFlow Max=0.03 cfs @ 14.48 hrs HW=182.65' (Free Discharge) —1=Driveway Opening to Hubbard (Weir Controls 0.03 cfs @ 0.27 fps)



Pond EP-NL: North Lot

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10556 HydroCAD (2022-09-07) Type III 24

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Stage-Area-Storage for Pond EP-NL: North Lot

Summary for Pond EP-SL: South Lot

Inflow Area =	15,167 sf, 75.22% Impervious,	Inflow Depth > 5.28" for 25-Year event					
Inflow =	2.14 cfs @ 12.07 hrs, Volume=	6,676 cf					
Outflow =	0.16 cfs @ 13.12 hrs, Volume=	2,503 cf, Atten= 93%, Lag= 62.8 min					
Discarded =	0.01 cfs @ 13.12 hrs, Volume=	661 cf					
Primary =	0.15 cfs @ 13.12 hrs, Volume=	1,842 cf					
Routed to Link EL-G : Existing Godrefy							

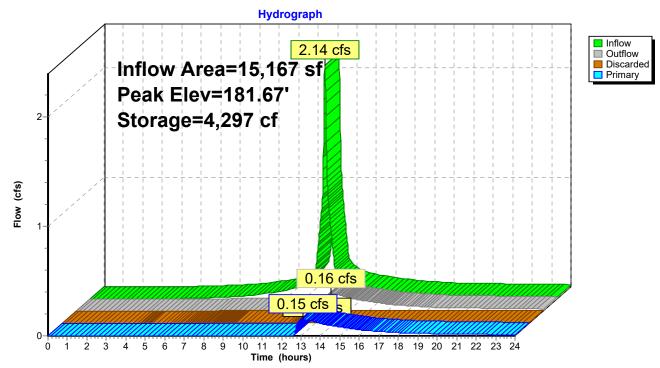
Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs Peak Elev= 181.67' @ 13.12 hrs Surf.Area= 4,989 sf Storage= 4,297 cf

Plug-Flow detention time= 295.4 min calculated for 2,503 cf (37% of inflow) Center-of-Mass det. time= 163.0 min (947.3 - 784.3)

Volume	Invert	Avail.Stor	rage	Storac	ge Description		
#1	173.00'	Ę	50 cf			atic)Listed below (Re	
"0	170 001	۸.	74-6		-	Embedded = $126 \text{ cf } x$	
#2 #2	173.00' 170.04'					smatic)Listed below	
#3 #4	179.94' 179.00'	0,00				smatic)Listed below (Prismatic)Listed bel	
	179.00	<u> </u>			Available Storage	Prismancjeisien ser	
		0,11	11 0	Ιυιαι /	Avallable Storage		
Elevation	Sur	f.Area	Inc	.Store	Cum.Store		
(feet)		(sq-ft)		c-feet)	(cubic-feet)		
173.00		50		0	0		
179.00		50		300	300		
	C			~	O and Otama		
Elevation		f.Area		Store	Cum.Store		
(feet)	'	(sq-ft)	<u>uaus)</u>	<u>c-feet)</u>	(cubic-feet)		
173.00		29 20		0 174	0 174		
179.00		29		174	174		
Elevation	Sur	f.Area	Inc	Store.	Cum.Store		
(feet)		(sq-ft)		c-feet)	(cubic-feet)		
179.94		0		0	0		
181.00		2,805		1,487	1,487		
182.00		5,995	,	4,400	5,887		
Flawation	Sur	6 A A	Inc	Otoro	Cum Store		
Elevation (feet)		f.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)		
179.00		<u>(sq-it)</u> 6		0	0		
179.00		6 6		6	0		
170.01		0		U			
Device R	Routing	Invert	<u>Outl</u> ∈	et Devic	ces		
	Primary	181.64'			Sidewalk Overflow	w. C= 3.27	
			Offse	et (feet)) 0.00 0.01 18.86	6 18.87	
			Heigh	ht (feet)	ť) 0.50 0.00 0.04	0.50	
#2 D	Discarded	173.00'					ver Surface area below 173.
			Conc	Juctivity	y to Groundwater F	Elevation = 172.00'	Phase-In= 0.01'

Discarded OutFlow Max=0.01 cfs @ 13.12 hrs HW=181.67' (Free Discharge) **2=Sandy Loam (HSG B) Exfiltration** (Controls 0.01 cfs)

Primary OutFlow Max=0.07 cfs @ 13.12 hrs HW=181.67' (Free Discharge) —1=Southeast Sidewalk Overflow (Weir Controls 0.07 cfs @ 0.22 fps)



Pond EP-SL: South Lot

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	0 (01		o (01
Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
173.00	50	0	178.30	50	198
173.10	50	4	178.40	50	202
173.20	50	7	178.50	50	206
173.30	50	11	178.60	50	209
173.40	50	15	178.70	50	213
173.50	50	19	178.80	50	217
173.60	50	22	178.90	50	221
173.70	50	26	179.00	56	224
173.80	50	30	179.10	56	225
173.90	50	34	179.20	56	226
174.00	50	37	179.30	56	226
174.10	50	41	179.40	56	227
174.20 174.30	50 50	45 49	179.50	56 56	227 228
174.30	50 50	49 52	179.60 179.70	56	220
174.50	50	56	179.80	56	229
174.60	50	60	179.90	56	220
174.70	50	64	180.00	215	235
174.80	50	67	180.10	479	264
174.90	50	71	180.20	744	319
175.00	50	75	180.30	1,009	402
175.10	50	79	180.40	1,273	510
175.20	50	82	180.50	1,538	645
175.30	50	86	180.60	1,803	806
175.40	50	90	180.70	2,067	994
175.50	50	94	180.80	2,332	1,209
175.60 175.70	50 50	97 101	180.90 181.00	2,596 2,861	1,449 1,717
175.80	50	105	181.10	3,180	2,013
175.90	50	108	181.20	3,499	2,341
176.00	50	112	181.30	3,818	2,702
176.10	50	116	181.40	4,137	3,094
176.20	50	120	181.50	4,456	3,518
176.30	50	123	181.60	4,775	3,974
176.40	50	127	181.70	5,094	4,462
176.50	50	131	181.80	5,413	4,981
176.60	50	135	181.90	5,732	5,533
176.70	50	138	182.00	6,051	6,117
176.80	50	142	182.10	6,051	6,117
176.90	50 50	146 150			
177.00 177.10	50 50	150			
177.20	50	157			
177.30	50	161			
177.40	50	165			
177.50	50	168			
177.60	50	172			
177.70	50	176			
177.80	50	180			
177.90	50	183			
178.00	50	187			
178.10	50 50	191			
178.20	50	194			

Stage-Area-Storage for Pond EP-SL: South Lot

Summary for Pond PP-I1: Infil#1

23,203 sf, 81.22% Impervious, Inflow Depth > 5.54" for 25-Year event Inflow Area = 3.37 cfs @ 12.07 hrs, Volume= Inflow = 10.718 cf 0.24 cfs @ 13.21 hrs, Volume= 9,046 cf, Atten= 93%, Lag= 68.5 min Outflow = 0.24 cfs @ 13.21 hrs, Volume= Discarded = 9,046 cf 0.00 cfs @ 0.00 hrs, Volume= Primary = 0 cf Routed to Link PL-H : Proposed Hubbard

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs / 2 Peak Elev= 181.22' @ 13.21 hrs Surf.Area= 1,776 sf Storage= 5,502 cf

Plug-Flow detention time= 255.6 min calculated for 9,046 cf (84% of inflow) Center-of-Mass det. time= 190.6 min (967.0 - 776.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.50'	1,770 cf	12.00'W x 148.00'L x 6.17'H Field A
			10,952 cf Overall - 6,528 cf Embedded = 4,424 cf x 40.0% Voids
#2A	177.00'	4,848 cf	retain_it retain_it 5.0' x 18 Inside #1
			Inside= 84.0"W x 60.0"H => 36.41 sf x 8.00'L = 291.3 cf
			Outside= 96.0"W x 68.0"H => 45.33 sf x 8.00'L = 362.7 cf
			1 Rows adjusted for 394.8 cf perimeter wall
		6,618 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	180.70'	6.0" Round JB#2 to EX.CB L= 11.0' Ke= 0.500
	-		Inlet / Outlet Invert= 180.70' / 180.35' S= 0.0318 '/' Cc= 0.900
			n= 0.010, Flow Area= 0.20 sf
#2	Device 1	181.25'	6.0" Round JB#1 to JB#2 L= 15.0' Ke= 0.500
			Inlet / Outlet Invert= 181.25' / 180.80' S= 0.0300 '/' Cc= 0.900
			n= 0.010, Flow Area= 0.20 sf
#3	Device 2	180.50'	6.0" Round Infil#1 to JB#1 L= 52.0' Ke= 0.500
			Inlet / Outlet Invert= 179.70' / 180.50' S= -0.0154 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf
#4	Primary	182.00'	4.0' long x 0.5' breadth AD#4 - HIGH OVERFLOW
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#5	Device 4	179.50'	6.0" Round Infil#1 to AD#4 L= 29.0' Ke= 0.500
			Inlet / Outlet Invert= 178.90' / 179.50' S= -0.0207 '/' Cc= 0.900
			n= 0.010, Flow Area= 0.20 sf
#6	Discarded	176.50'	1.020 in/hr Sandy Loam (HSG B) Exfiltration over Surface area below 176.51'
			Conductivity to Groundwater Elevation = 175.50' Phase-In= 0.01'

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Discarded OutFlow Max=0.24 cfs @ 13.21 hrs HW=181.22' (Free Discharge) **G=Sandy Loam (HSG B) Exfiltration** (Controls 0.24 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=176.50' (Free Discharge) 1=JB#2 to EX.CB (Controls 0.00 cfs) 2=JB#1 to JB#2 (Controls 0.00 cfs) 3=Infil#1 to JB#1 (Controls 0.00 cfs) 4=AD#4 - HIGH OVERFLOW (Controls 0.00 cfs) 5=Infil#1 to AD#4 (Controls 0.00 cfs)

Pond PP-I1: Infil#1 - Chamber Wizard Field A

Chamber Model = retain_it retain_it 5.0' (retain-it®)

Inside= 84.0"W x 60.0"H => 36.41 sf x 8.00'L = 291.3 cf Outside= 96.0"W x 68.0"H => 45.33 sf x 8.00'L = 362.7 cf 1 Rows adjusted for 394.8 cf perimeter wall

18 Chambers/Row x 8.00' Long = 144.00' Row Length +24.0" End Stone x 2 = 148.00' Base Length 1 Rows x 96.0" Wide + 24.0" Side Stone x 2 = 12.00' Base Width 6.0" Stone Base + 68.0" Chamber Height = 6.17' Field Height

10.4 cf Sidewall x 18 x 2 + 10.4 cf Endwall x 1 x 2 = 394.8 cf Perimeter Wall 18 Chambers x 291.3 cf - 394.8 cf Perimeter wall = 4,848.2 cf Chamber Storage 18 Chambers x 362.7 cf = 6,528.0 cf Displacement

10,952.0 cf Field - 6,528.0 cf Chambers = 4,424.0 cf Stone x 40.0% Voids = 1,769.6 cf Stone Storage

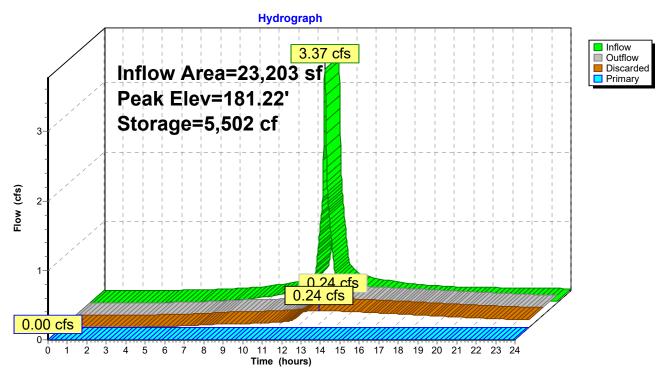
Chamber Storage + Stone Storage = 6,617.8 cf = 0.152 af Overall Storage Efficiency = 60.4% Overall System Size = 148.00' x 12.00' x 6.17'

18 Chambers 405.6 cy Field 163.9 cy Stone

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Pond PP-I1: Infil#1



10556 HydroCAD (2022-09-07) Type III 24-h

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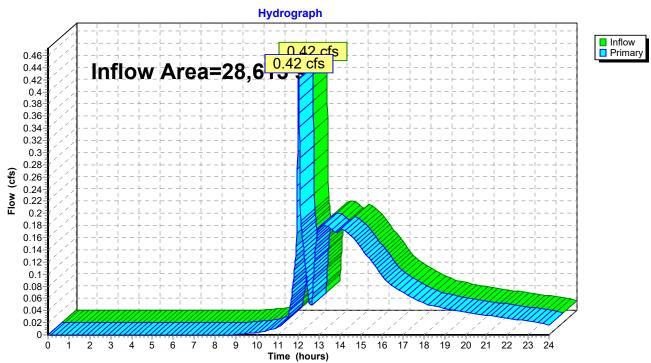
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
176.50	1,776	0	181.80	1,776	6,208
176.60	1,776	71	181.90	1,776	6,329
176.70	1,776	142	182.00	1,776	6,451
176.80	1,776	213	182.10	1,776	6,476
176.90	1,776	284	182.20	1,776	6,501
177.00	1,776	355	182.30	1,776	6,526
177.10	1,776	477	182.40	1,776	6,551
177.20	1,776	599	182.50	1,776	6,576
177.30	1,776	721	182.60	1,776	6,601
177.40	1,776	843			
177.50	1,776	965			
177.60	1,776	1,087			
177.70	1,776	1,209			
177.80	1,776	1,331			
177.90	1,776	1,453			
178.00	1,776	1,574			
178.10	1,776	1,696			
178.20	1,776	1,818			
178.30	1,776	1,940			
178.40	1,776	2,062			
178.50	1,776	2,184			
178.60	1,776	2,306			
178.70	1,776	2,428			
178.80	1,776	2,550			
178.90	1,776	2,672			
179.00	1,776 1,776	2,794			
179.10 179.20	1,776	2,916 3,038			
179.30	1,776	3,159			
179.40	1,776	3,281			
179.50	1,776	3,403			
179.60	1,776	3,525			
179.70	1,776	3,647			
179.80	1,776	3,769			
179.90	1,776	3,891			
180.00	1,776	4,013			
180.10	1,776	4,135			
180.20	1,776	4,257			
180.30	1,776	4,379			
180.40	1,776	4,501			
180.50	1,776	4,623			
180.60	1,776	4,744			
180.70	1,776	4,866			
180.80	1,776	4,988			
180.90	1,776	5,110			
181.00	1,776	5,232			
181.10	1,776	5,354			
181.20	1,776	5,476			
181.30	1,776	5,598			
181.40	1,776	5,720			
181.50	1,776	5,842			
181.60	1,776	5,964			
181.70	1,776	6,086			
			I		

Stage-Area-Storage for Pond PP-I1: Infil#1

Summary for Link EL: Existing

Inflow Are	a =	28,613 sf,	, 65.19% Impervious,	Inflow Depth >	1.52"	for 25-Year event
Inflow	=	0.42 cfs @	12.00 hrs, Volume=	3,634 c	f	
Primary	=	0.42 cfs @	12.00 hrs, Volume=	3,634 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs



Link EL: Existing

Summary for Link EL-G: Existing Godrefy

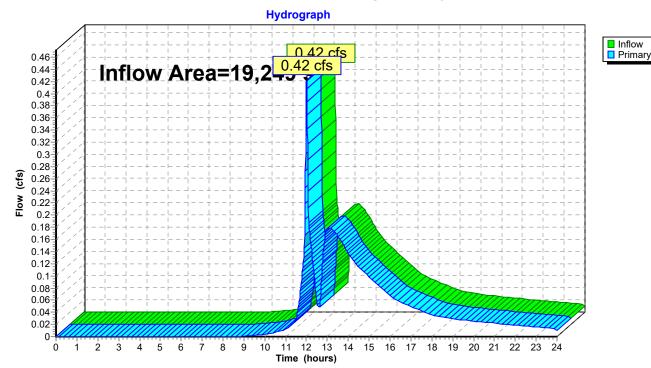
 Inflow Area =
 19,249 sf, 63.64% Impervious, Inflow Depth >
 1.81" for 25-Year event

 Inflow =
 0.42 cfs @
 12.00 hrs, Volume=
 2,911 cf

 Primary =
 0.42 cfs @
 12.00 hrs, Volume=
 2,911 cf, Atten= 0%, Lag= 0.0 min

 Routed to Link EL : Existing
 Existing
 12.00 hrs, Volume=
 2,911 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs

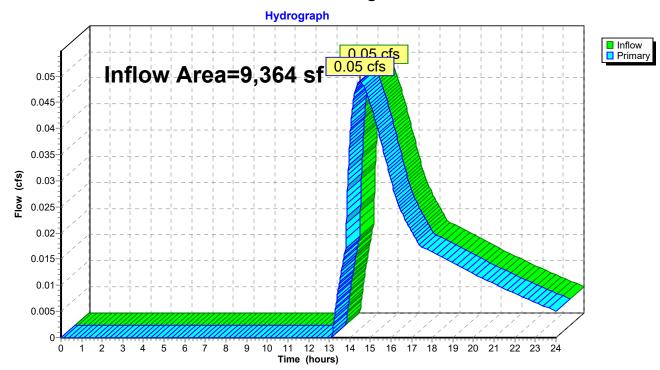


Link EL-G: Existing Godrefy

Summary for Link EL-H: Existing Hubbard

9,364 sf, 68.38% Impervious, Inflow Depth > 0.93" for 25-Year event Inflow Area = 724 cf Inflow = 0.05 cfs @ 14.48 hrs, Volume= 0.05 cfs @ 14.48 hrs, Volume= 724 cf, Atten= 0%, Lag= 0.0 min Primary = Routed to Link EL : Existing

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs

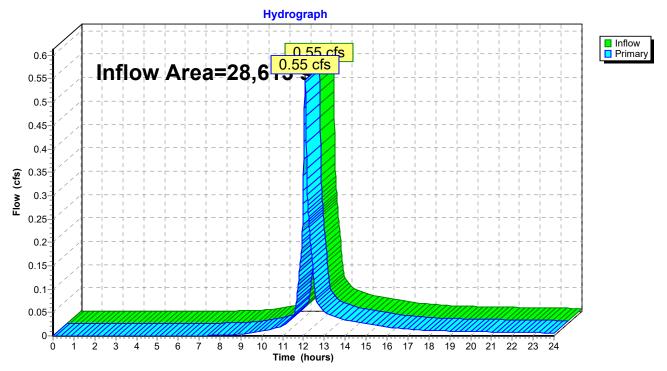


Link EL-H: Existing Hubbard

Summary for Link PL: Proposed

Inflow Are	a =	28,613 sf,	72.22% Impervious,	Inflow Depth >	0.69"	for 25-Year event
Inflow	=	0.55 cfs @	12.07 hrs, Volume=	1,641 c	f	
Primary	=	0.55 cfs @	12.07 hrs, Volume=	1,641 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs

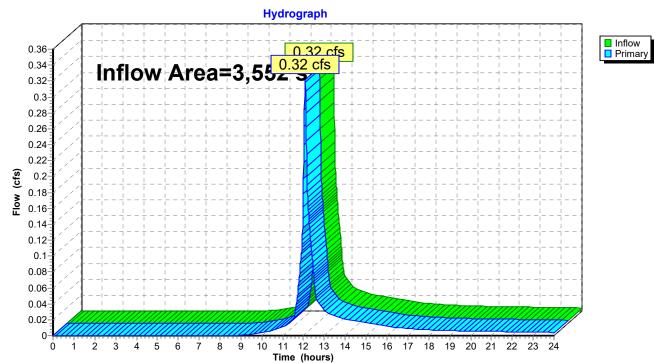


Link PL: Proposed

Summary for Link PL-G: Proposed Godfrey

Inflow Area = 3,552 sf, 23.42% Impervious, Inflow Depth > 3.25" for 25-Year event Inflow = 0.32 cfs @ 12.08 hrs, Volume= 961 cf Primary = 0.32 cfs @ 12.08 hrs, Volume= 961 cf, Atten= 0%, Lag= 0.0 min Routed to Link PL : Proposed

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs

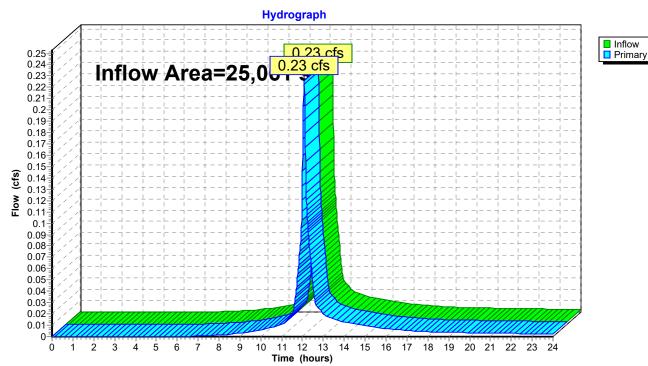


Link PL-G: Proposed Godfrey

Summary for Link PL-H: Proposed Hubbard

Inflow Area	a =	25,061 sf,	79.14% Impervious,	Inflow Depth >	0.33"	for 25-Year event
Inflow	=	0.23 cfs @	12.07 hrs, Volume=	680 c	f	
Primary	=	0.23 cfs @	12.07 hrs, Volume=	680 c	f, Atter	n= 0%, Lag= 0.0 min
Routed	to Link	PL : Proposed	b			

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.0100 hrs



Link PL-H: Proposed Hubbard

Runoff by SCS TR	Type III 24-hr 100-Year Rainfall=8.39" Printed 10/3/2022 DCAD Software Solutions LLCDCAD Software Solutions LLCPage 744.00 hrs, dt=0.0100 hrs, 2401 points -20 method, UH=SCS, Weighted-CN ans method - Pond routing by Stor-Ind method
Subcatchment EX-GB: Godfrey Bypass	Runoff Area=4,082 sf 20.63% Impervious Runoff Depth>4.64" Tc=0.0 min CN=68.6 Runoff=0.62 cfs 1,577 cf
Subcatchment EX-NL: North Lot	Runoff Area=9,364 sf 68.38% Impervious Runoff Depth>6.74" Tc=5.0 min CN=86.3 Runoff=1.68 cfs 5,260 cf
Subcatchment EX-SL: South Lot	Runoff Area=15,167 sf 75.22% Impervious Runoff Depth>7.04" Tc=5.0 min CN=88.8 Runoff=2.80 cfs 8,899 cf
Subcatchment PR-GB: Godfrey Bypass	Runoff Area=3,552 sf 23.42% Impervious Runoff Depth>4.76" Tc=5.0 min CN=69.7 Runoff=0.47 cfs 1,409 cf
Subcatchment PR-HB: Hubbard Bypass	Runoff Area=1,858 sf 53.18% Impervious Runoff Depth>6.07"

Subcatchment PR-I1: Infil#1Runoff Area=23,203 sf 81.22% Impervious Runoff Depth>7.32"
Tc=5.0 min CN=91.1 Runoff=4.38 cfs 14,147 cf

Tc=5.0 min CN=80.7 Runoff=0.31 cfs 940 cf

Inflow=1.31 cfs 7,607 cf

Inflow=1.20 cfs 5,599 cf

Inflow=0.27 cfs 2,008 cf

Inflow=1.09 cfs 4,351 cf Primary=1.09 cfs 4,351 cf

Inflow=0.47 cfs 1,409 cf

Inflow=0.95 cfs 2,941 cf Primary=0.95 cfs 2,941 cf

Primary=0.47 cfs 1,409 cf

Primary=0.27 cfs 2,008 cf

Primary=1.20 cfs 5,599 cf

Primary=1.31 cfs 7,607 cf

Pond EP-NL: North LotPeak Elev=182.70' Storage=2,965 cfInflow=1.68 cfs5,260 cfDiscarded=0.01 cfs628 cfPrimary=0.27 cfs2,008 cfOutflow=0.28 cfs2,637 cf

Pond EP-SL: South LotPeak Elev=181.72' Storage=4,544 cfInflow=2.80 cfs8,899 cfDiscarded=0.01 cfs699 cfPrimary=1.02 cfs4,022 cfOutflow=1.03 cfs4,721 cf

 Pond PP-I1: Infil#1
 Peak Elev=182.06' Storage=6,467 cf
 Inflow=4.38 cfs
 14,147 cf

 Discarded=0.28 cfs
 10,087 cf
 Primary=0.87 cfs
 2,001 cf
 Outflow=1.14 cfs
 12,088 cf

Link EL: Existing

Link EL-G: Existing Godrefy

Link EL-H: Existing Hubbard

Link PL: Proposed

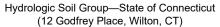
Link PL-G: Proposed Godfrey

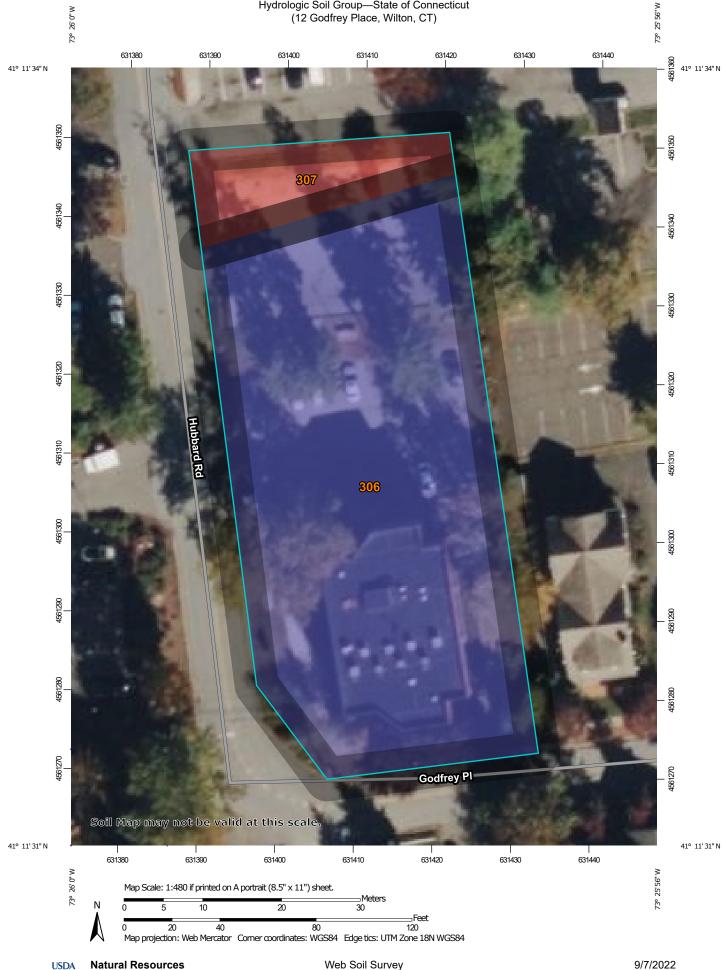
Link PL-H: Proposed Hubbard

Total Runoff Area = 57,226 sf Runoff Volume = 32,232 cf Average Runoff Depth = 6.76" 31.29% Pervious = 17,908 sf 68.71% Impervious = 39,318 sf Appendix 6

NRCS Soil Information

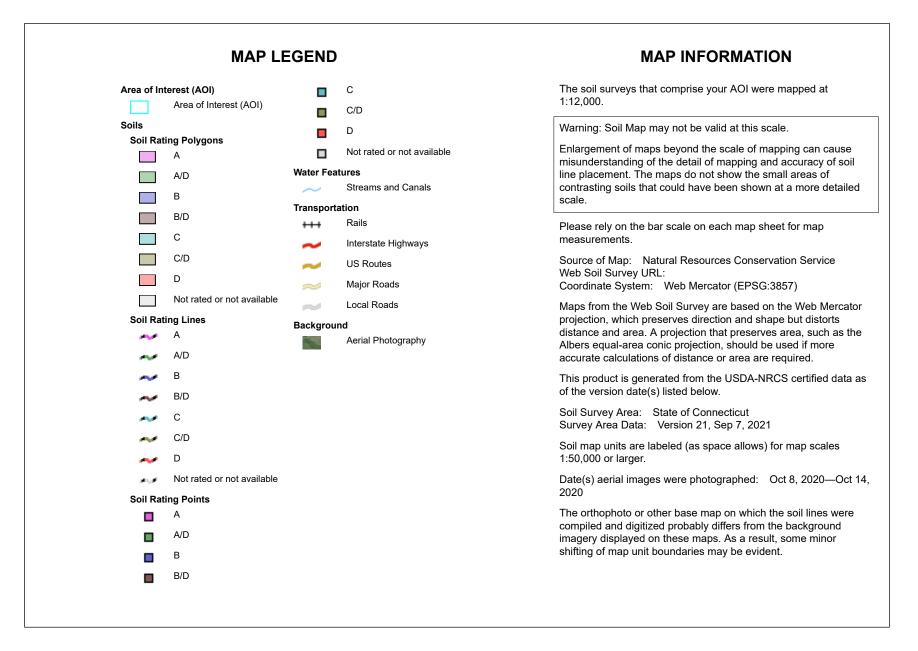






Conservation Service

Web Soil Survey National Cooperative Soil Survey





Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
306	Udorthents-Urban land complex	В	0.6	88.9%
307	Urban land	D	0.1	11.1%
Totals for Area of Intere	st		0.7	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

USDA

SANITARY SEWER REPORT

12 Godfrey Place

Prepared by

Redniss & Mead, Inc. 22 First Street Stamford, CT (203) 327-0500

Issued on: September 30, 2022

Craig J. Flaherty, CT Lic. No. 21149



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Study Pont #1 Capacity Calculation	Appendix 3

Sanitary Sewer Narrative

The proposed redevelopment of the site includes the demolition of the existing office building and construction of the new four-story residential building with ground level parking. The apartment building will consist of 13 one-bedroom, 13 two-bedroom, and 6 three-bedroom apartments. The proposed change in use for the building is estimated to generate an average daily flow of 8,550 gallons per day, representing an increase of 7,463 gallons per day over existing conditions (Appendix 1-Sanitary Flow Calculations). A new lateral connection is proposed south of the building, connecting to the 8" ductile iron pipe in Godfrey Place via a chimney connection. The existing office building previously discharged via a sanitary lateral connecting to the main in Hubbard Road.

Effluent from the site is tributary to an 8" main that runs east to west in Godfrey Place before ultimately reaching the 24" main in Old Ridgefield Road (Appendix 2 – Godfrey Place Sewershed Map). An analysis along the final length of 8" main in Godfrey Place (Study Point #1) was done to confirm the existing infrastructure has the capacity to accommodate the proposed flows. This length of pipe receives the most effluent and maintains a slope very similar to the rest of the main (0.7%). The area tributary to Study Point #1 consists of the site and residential and commercial properties fronting on Old Ridgefield Road, Hubbard Road and Godfrey Place. Refer to the Offsite Properties sheet found in Appendix 1 for more information. Using Manning's Equation, the calculated capacity of the pipe is 1.008 cfs (Appendix 3). The proposed flow is 0.255 cfs (Appendix 1), accounting for 25.3% of the pipe's capacity, an increase of 4.3% over existing conditions.

Based on the narrative above supported by the calculations provided herewith, it is our opinion that the receiving municipal sewers have the capacity to accommodate flow from the redevelopment of the subject parcel and future development within the sewershed.

Appendix 1

Sanitary Flow Calculations

Project:	12 Godfrey Place		Project #:	10556	Date:	9/30/2022
Location:	Wilton, CT		By:	PBS	Checked:	CJF
		below represent th Godfrey Place. Of				
		Existing On-S	ite Flow			
	Location	Building Use	Floor Area (SF)	Design Flow (GPD/SF)*	Total Flow	
	12 Godfrey Place	Office	10,871	0.100	1,087	
	Existi	1,087	1			
		0.002				
	Peaking Factor					
	Total Existing Peak Flow (CFS)					
	Pote	ential Proposed	On-Site F	low		
	Location	Building Use	# of Bedrooms	Design Flow (GPD /	Total Flow	
	12 Godfrey Place	Residential	57	150	8,550]
	Proposed Sanitary Flow (GPD) 8,55					
	Peak Rate (CFS)]
	Peaking Factor					
Total Proposed Peak Flow (CFS) 0.05						



Offsite Sanitary Sewer Flow Estimates							
Project:	12 Godfrey Place		Project #:	10556	Date:	9/30/2022	
Location	Wilton, CT		By:	PBS	Checked:	9/30/2022	
	The flows listed below repres main in Godfrey Place connec		-	tributary to t	he sewer		
	I	Existing O	ffsite Flow:				
	Туре	Unit	GPD / Unit*	Flow (GPD)		
	Bedrooms	18	150	2,700			
	Retail (sf)	66,170	0.10	6,617			
	Office (sf)	17,678	0.10	1,768			
	Restaurant (est. seats)**	8,488	1.00	8,488			
	Medical Office	6,102	0.200	1,220			
	Day Care***	8,828	0.15	1,324			
	Sub-Total F	flow (GPD)		22,117			
	Factor o	f Safety		1.5			
	Total Flor	w (GPD)		33,176			
	Flow Rat	te (CFS)		0.051			
	Peaking	Factor		4			
	Peak Flow	Rate (CFS)		0.205			
	*Per State of CT Public Healt **30 GPD per seat. Assumed Group Child Care Homes Reg indoor usable program space program space".	1 50% of sf is gulation there	is a minimum o	f 35 square f	eet of total	floor area	



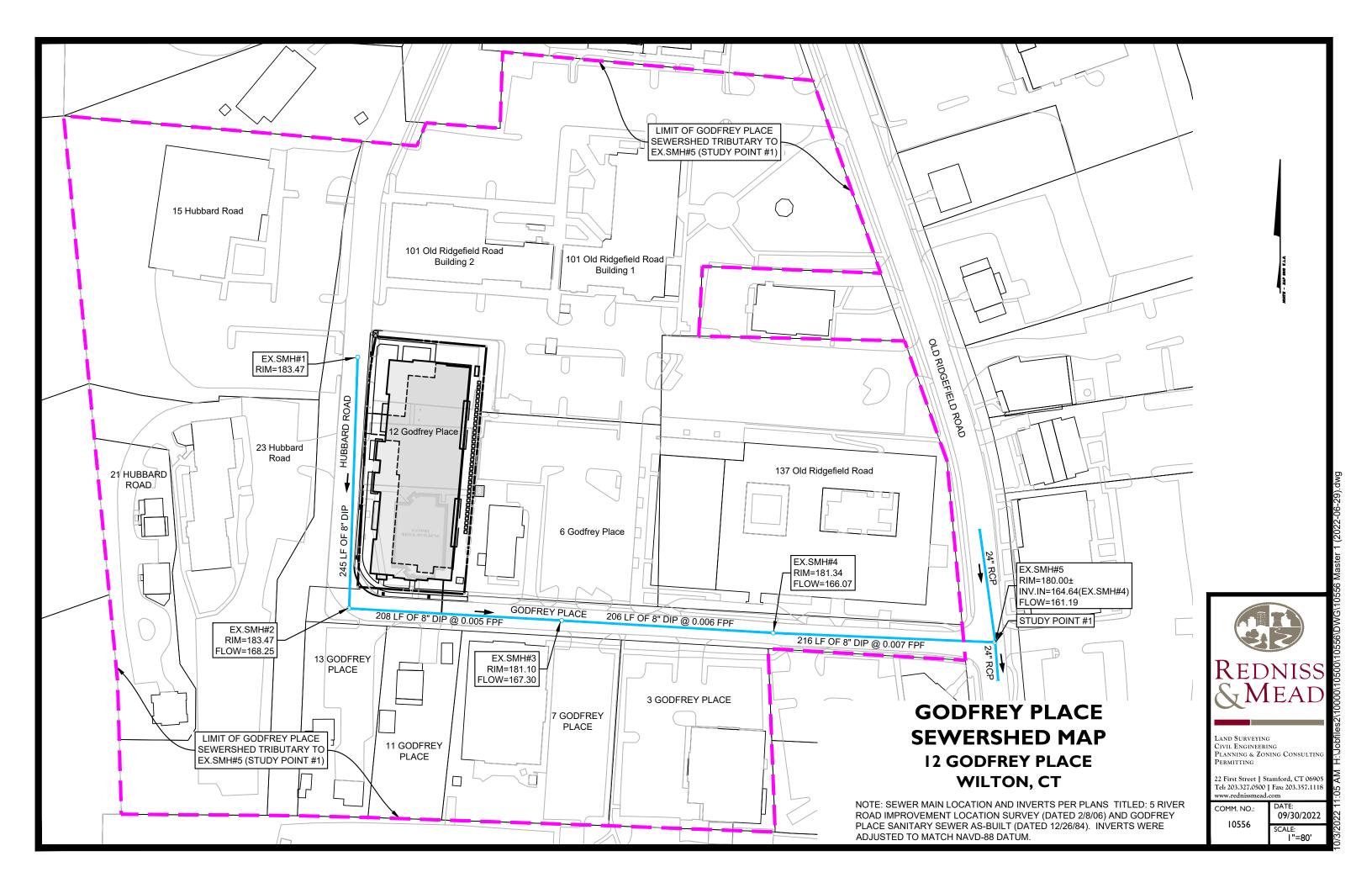
		Offsite	Properties List						
Project:	roject: 12 Godfrey PlaceProject #:10556								
Location	Wilton, C	CT	By:	PBS	Checked	CJF			
		Offsite Properties Tribu	tary to Study Point #1		1				
		Address	Use Type	Building SF/BDRM					
	1	101 Old Ridgefield Road Building #1*	Restaurant Medical Office Office	1,601 4,003 10,406					
2101 Old Ridgefield Road Building #2*315 Hubbard Road		101 Old Ridgefield Road Building #2*	Restaurant Bank	6,887 2,296					
		15 Hubbard Road	Retail (Post Office)	11,309	1				
	4	23 Hubbard Road**	Office Medical Office Residential	6,297 2,099 4					
521 Hubbard Road613 Godfrey Place711 Godfrey Place87 Godfrey Place		21 Hubbard Road	Residential	5	1				
		13 Godfrey Place	Office	975	1				
		11 Godfrey Place	Residential	3	1				
		7 Godfrey Place	Daycare	8,828]				
	9	6 Godfrey Place	Apartment	6					
	10	3 Godfrey Place	Retail (Pet Store)	5,702					
	11	137 Old Ridgefield Road	Retail (Library)	46,863					

'Use type break down approximated based off of Town Green at Wilton Center Leasing Package **Use type break down approximated assuming that the four tenants equallly split leasable area



Appendix 2

Godfrey Place Sewershed Map



Appendix 3

Study Point #1 Capacity Calculation

		ng's Equatio	-			
Project:	12 Godfrey Place		Project #:	10556		
Location:	Wilton, CT		By:	PBS	Date:	9/30/2022
Description:	8" Sanitary Main in God	lfrey Place	Checked:	CJF	Date:	9/30/2022
	-	Point #1 - 8" ate the flow ca		-	s equation.	
	Pipe material	Cast Iron Pipe (CIF))		•	
	Manning's n	0.013				
	Pipe diameter, D	0.666 ft				
	Area, A _{full}	0.35 ft ²		$A = \frac{\pi}{4}D^2$		
	Wetted perimeter, P_{full}	2.09 ft		$P = \pi D$		
	Hydraulic radius, R _h	0.17 ft		$R_h = \frac{A}{P}$		
	Slope, S	0.0070 ft/	ft			
	Existing Pipe Capacity Flow, Q _{full}	y 1.008 cfs	Q	$=\frac{1.486}{n}$	$AR_{h}^{\frac{2}{3}}S^{\frac{1}{2}}$	
	Existing Peak Flow	0.212 cfs	5			
	% of Pipe Capacity	21.0%				
	Proposed	0.255 cfs	5			
	% of Pipe Capacity	25.3%				